



Supplement of

On the calibration of FIGAERO-ToF-CIMS: importance and impact of calibrant delivery for the particle-phase calibration

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1 S1. Different P_{sat} values used in FIGAERO-ToF-CIMS calibrations in different studies

2

3 *Table S1.* Collection of literature-based P_{sat} (Pa) values used in various published FIGAERO
4 calibrations, P_{sat} values used in this study are taken from Lopez-Hilfiker et al., (2014).

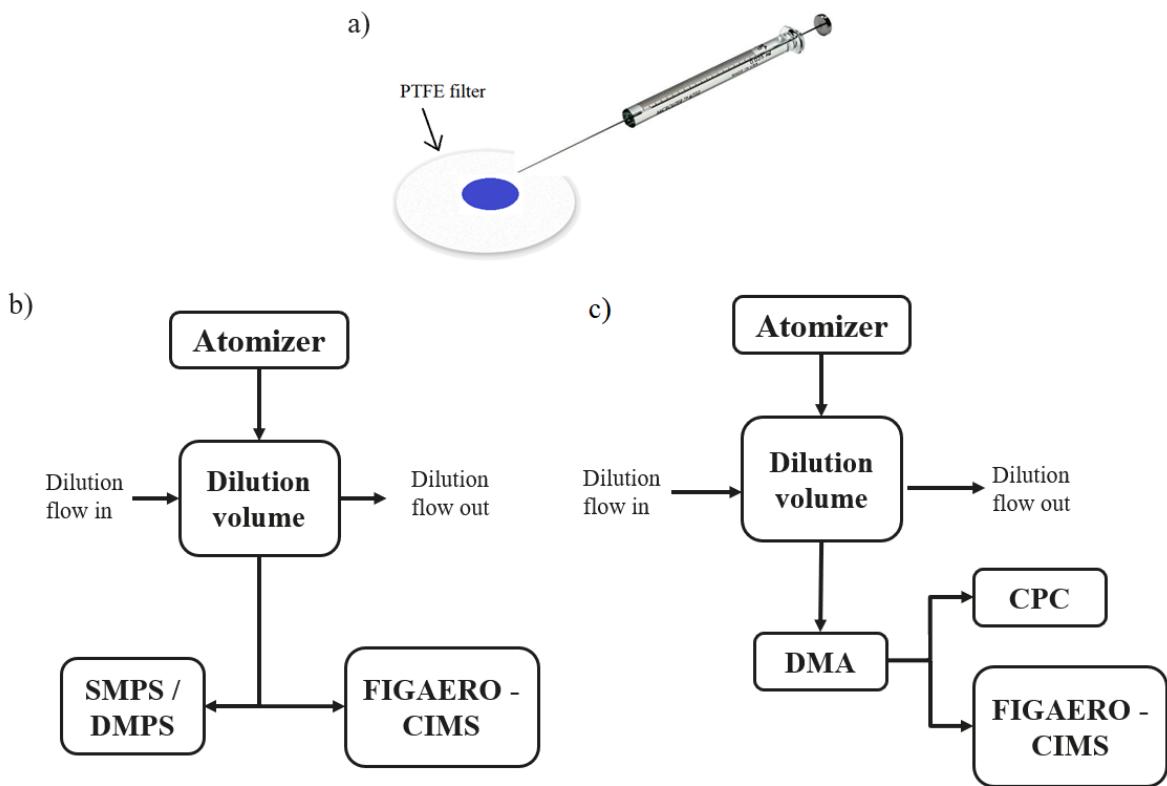
Saturation pressure (Pa)	Lopez-Hilfiker et al., (2014)	Stark et al., (2017)	Nah et al., (2019)	Bannan et al., (2019)	Ye et al., (2019)	(Wang et al., 2020)	This study
Glutaric acid		6.7×10^{-4}	1×10^{-3}	1×10^{-3}	4×10^{-4}	2.6×10^{-4}	
Cis-Pinonic acid	6×10^{-5}	0.03	7.8×10^{-4}	7.79×10^{-4}			
Pimelic acid	1.3×10^{-4}		2.6×10^{-4}				1.3×10^{-4}
Erythritol			6.3×10^{-5}				
Palmitic acid	1.4×10^{-4}		2.0×10^{-5}		5×10^{-5}	2.8×10^{-5}	1.4×10^{-4}
Azelaic acid	6×10^{-6}	6×10^{-6}	7.4×10^{-6}			1.4×10^{-6}	6×10^{-6}
Oleic acid	1×10^{-6}						
Stearic acid	1×10^{-5}		2.5×10^{-6}				1×10^{-6}
Sebacic acid	1.5×10^{-6}		1.5×10^{-6}				1.5×10^{-6}
Behenic acid	7×10^{-4}		4.9×10^{-8}				
Oleic acid	1×10^{-5}						1×10^{-5}
Tricarballylic acid		3×10^{-7}			3.1×10^{-7}	3.1×10^{-7}	
Pinic acid	6×10^{-5}	4.3×10^{-5}		3.2×10^{-5}	9.3×10^{-5}		
Citric acid					2.7×10^{-10}	2.7×10^{-10}	
Camphoric acid					2×10^{-4}	2×10^{-5}	
Dodecanoic/1 auric acid					0.01		
Succinic acid				1.3×10^{-3}			
Malonic acid				6.2×10^{-4}			
Adipic acid				1.8×10^{-4}			
Suberic acid				2.23×10^{-5}			

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8 S2. Measurement schematics



9
10 *Figure S1. Panel a) illustration of the syringe deposition method. Measurement setup schematics for*
11 *the atomizer method either with b) polydisperse particles or c) monodisperse particles. The dilution*
12 *volume is used in the atomizer method to ensure complete evaporation of the solvent before particle*
13 *characterization.*

14
15 S3. Measured T_{max} values

16
17 *Table S2. Average T_{max} values ($^{\circ}\text{C}$) and standard deviations based on three repetitions, as shown in*
18 *Figure 3 panel a). Used P_{sat} (Pa), based on Krieger et al., (2018), are shown in the bottom row.*

Experiment	PEG-4	PEG-5	PEG-6	PEG-7	PEG-8
Conc. 0.1 g L ⁻¹	49.9 ± 4.4	74.6 ± 3.1	94.6 ± 2.8	110.9 ± 2.4	123 ± 2
Conc. 0.01 g L ⁻¹		38.5 ± 1.2	58.5 ± 1.5	76.8 ± 1.2	90.9 ± 0.9
Conc. 0.003 g L ⁻¹		36.7 ± 1.9	57 ± 2.5	73.1 ± 2.9	88.7 ± 2.8
Atomizer		23.3 ± 0.5	39.9 ± 0.4	54.7 ± 0.4	65.5 ± 0.2
Saturation pressure (Pa)	0.0169	5.29 x 10 ⁻⁴	3.05 x 10 ⁻⁵	1.29 x 10 ⁻⁶	9.2 x 10 ⁻⁸

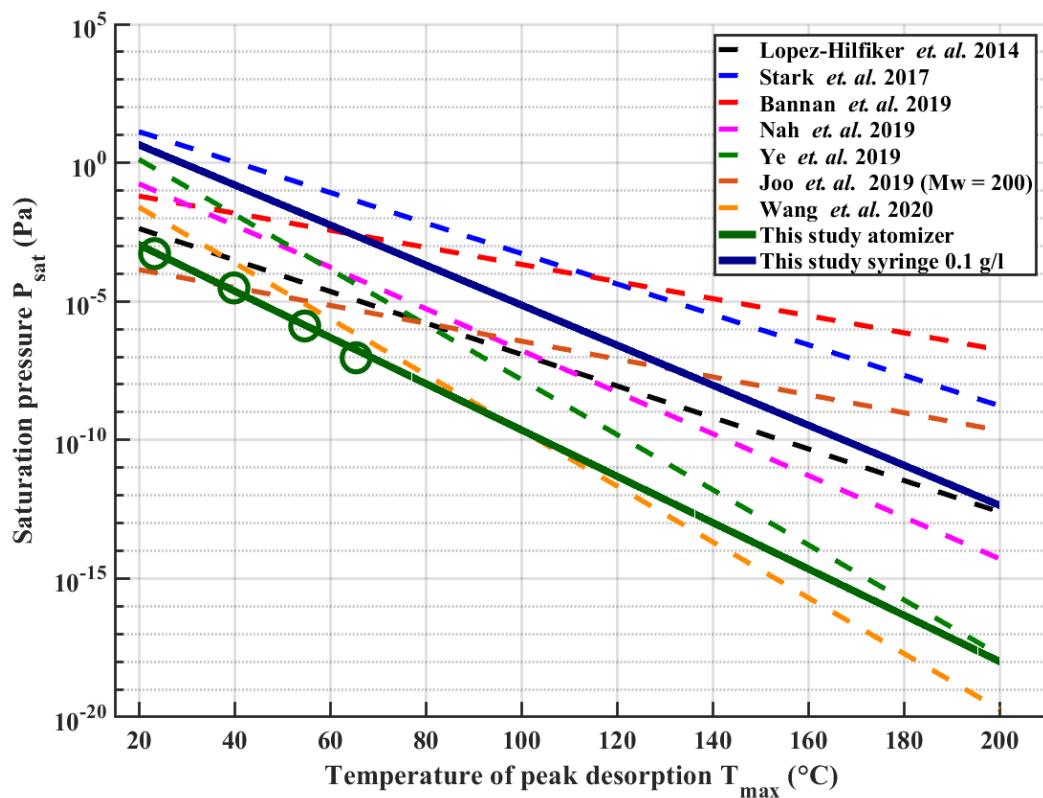
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22 *Table S3.* Average T_{max} values ($^{\circ}\text{C}$) and standard deviations based on three repetitions, as shown in
 23 Figure 3 panel b). Used saturation pressure (Pa) values are shown in the bottom row.

Experiment	Palmitic acid	Pimelic acid	Oleic acid	Azelaic acid	Stearic acid	Sebacic acid
Conc. 0.5 g L ⁻¹	55.8 ± 0.3	54 ± 0.1	61.8 ± 2.8	63.3 ± 0.3	64.7 ± 0.5	73.1 ± 0.1
Conc. 0.1 g L ⁻¹	48.9 ± 1	46.1 ± 1.1	51.2 ± 1.8	54.8 ± 1.2	55.8 ± 1	62.6 ± 1.2
Conc. 0.01 g L ⁻¹	40.6 ± 1.2	39.5 ± 2	43.9 ± 2.8	41.5 ± 1.5	44.8 ± 2.5	46.1 ± 0.4
Atomizer	36.6 ± 0.6	34 ± 0.4	34.7 ± 0.8	40.2 ± 0.7	43.5 ± 0.6	49.4 ± 1
Saturation pressure (Pa)	1.4 x 10 ⁻⁴	1.3 x 10 ⁻⁴	1 x 10 ⁻⁵	6 x 10 ⁻⁶	1 x 10 ⁻⁶	1.47 x 10 ⁻⁶

24



25
 26 *Figure S2.* Repeated Fig. 1 (dashed lines) with calibration lines from this study added for the atomizer
 27 method (green solid line) and the syringe method (for a solution concentration of 0.1 g L⁻¹, solid blue
 28 line). Both lines are for 30 min ramping times and the atomizer measurements used polydisperse aerosol
 29 with a median particle size of 60 nm. Green circles show the measured data where the line have been
 30 fitted.

31

32 S4. Error analysis for Figure 8.

33

34 Errors for deposited mass on the filter shown in Fig.8 are determined with propagation of error for
35 both methods. For syringe deposition the equation is of the form

36 $m_{\text{syringe}} = V_s C_s,$

37 where V_s (ml) is the injected volume and C_s (g l^{-1}) is the mass concentration of the solution. The
38 solution was prepared by weighting the analyte with a microscale and solving it to 200 ml of ACN to
39 make 0.2 g/l solution. The stock solution was then diluted into 50ml solution of 0.01 g/l
40 concentration. To account for the dilution, the equation now becomes to form

41 $m_{\text{syringe}} = \frac{V_{\text{syr}} V_{\text{pip}}}{V_{\text{fin}} V_{\text{sto}}} m_{\text{scale}},$

42 where V_{syr} is deposited volume to the filter, V_{pip} is volume pipetted from stock solution to make the
43 dilute solution, V_{fin} is the volume final dilute solution, V_{sto} is the volume of the stock solution and
44 m_{scale} is the analytes mass measured with the microscale. Now denoting

45 $R = \frac{V_{\text{syr}} V_{\text{pip}}}{V_{\text{fin}} V_{\text{sto}}}$

46 we get the equation to the form

47 $m_{\text{syr}} = R m_{\text{scale}}$

48 and formula for propagation of error becomes

49 $\Delta m_{\text{syringe}} = \sqrt{\left(\frac{\partial m_{\text{syr}}}{\partial R}\right)^2 \Delta R^2 + \left(\frac{\partial m_{\text{syr}}}{\partial m_{\text{scale}}}\right)^2 \Delta m_{\text{scale}}^2},$

50 $\Delta m_{\text{syringe}} = \sqrt{m_{\text{scale}}^2 \Delta R^2 + R^2 \Delta m_{\text{scale}}^2},$

51 where

52 $\Delta R = \sqrt{\left(\frac{V_{\text{pip}}}{V_{\text{fin}} V_{\text{sto}}}\right)^2 \Delta V_{\text{syr}}^2 + \left(\frac{V_{\text{syr}}}{V_{\text{fin}} V_{\text{sto}}}\right)^2 \Delta V_{\text{pip}}^2 + \left(-\frac{V_{\text{syr}} V_{\text{pip}}}{V_{\text{fin}}^2 V_{\text{sto}}}\right)^2 \Delta V_{\text{fin}}^2 + \left(-\frac{V_{\text{syr}} V_{\text{pip}}}{V_{\text{fin}} V_{\text{sto}}^2}\right)^2 \Delta V_{\text{sto}}^2}.$

53 When using Class A glassware, tolerances for different measurement flasks can be found online.

54

55 Atomizer deposition

56 Amount of deposited particulate mass can be calculated with equation

57 $m_{\text{atom}} = F t V_c,$

58 where F is the flow through the filter [$\text{m}^3 \text{s}^{-1}$], t [s] is the collection time and V_c [$\mu\text{g m}^{-3}$] is the particle
59 mass concentration in the sample air. The propagation of error formula for this equation is of the form

60 $\Delta m_{\text{atom}} = \sqrt{\left(\frac{\partial m_{\text{atom}}}{\partial F}\right)^2 \Delta F^2 + \left(\frac{\partial m_{\text{atom}}}{\partial t}\right)^2 \Delta t^2 + \left(\frac{\partial m_{\text{atom}}}{\partial V_c}\right)^2 \Delta V_c^2},$

61 $\Delta m_{\text{atom}} = \sqrt{(t V_c)^2 \Delta F^2 + (F V_c)^2 \Delta t^2 + (F t)^2 \Delta V_c^2},$

62

63 where $\Delta F = 0.01 \times F$ (flow meter accuracy), $\Delta t = 1$ (assuming swift movement of the tray). When
64 using monodisperse aerosol sampling method as shown in Fig. S1 b), particle mass concentration can
65 be calculated by assuming spherical particle shape as

66
$$V_c = \frac{\rho d_p^3 \pi n}{6},$$

67 where ρ is the density of the aerosol particles, d_p is the set monodisperse particle size and n is
68 particle number concentration measured with CPC. The uncertainty of V_c is then

69
$$\Delta V_c = \sqrt{\left(\frac{3\rho d_p^2 \pi}{6}\right)^2 \Delta d_p^2 + \left(\frac{\rho d_p^3 \pi}{6}\right)^2 \Delta n^2},$$

70 where $\Delta d_p = 0.01 \times d_p$ and $\Delta n = 0.1 \times n$ with instrumentation described in Sect. 2.4.

71

72 Y-axis errors for Figure 8 are calculated by assuming Poisson-type measurement error for CIMS
73 measurements (Yan et al., 2016)

74
$$e_i = \sqrt{\frac{s_i}{\Delta t}} + a,$$

75 where s_i is the measured signal, Δt is the difference of two-time steps and a is constant accounting for
76 electrical noise.

77 When integrating over such data, we assumed error to be of the form

78
$$\Delta I = \pm 1.96 \sqrt{std(S)^2 + \sum e_i^2},$$

79 where $std(S)$ is the standard deviation over the whole thermogram.

80

81 **S5. P_{sat} of higher order PEGs**

82 We performed additional T_{max} measurements of an atomized PEG-400 solution (Sigma Aldrich),
83 which contains different PEGs so that the average molecular mass of the solution is about 400 g/mol.
84 Detected PEGs ranged from PEG-6 to PEG-16. Fig. S3 a) shows measured T_{max} values of different
85 PEGs versus the molecular mass of the compounds. The measured points follow well a second order
86 polynomial fitted to the points. It should be noted that T_{max} values of PEG-400 are about 5-7 °C higher
87 than values measured for individual PEGs, possibly due to additional stabilization compounds in the
88 product. Figure S3 b) shows a somewhat bold log-linear extrapolation of saturation pressures from
89 measured PEGs (4-8) up to PEG-16.

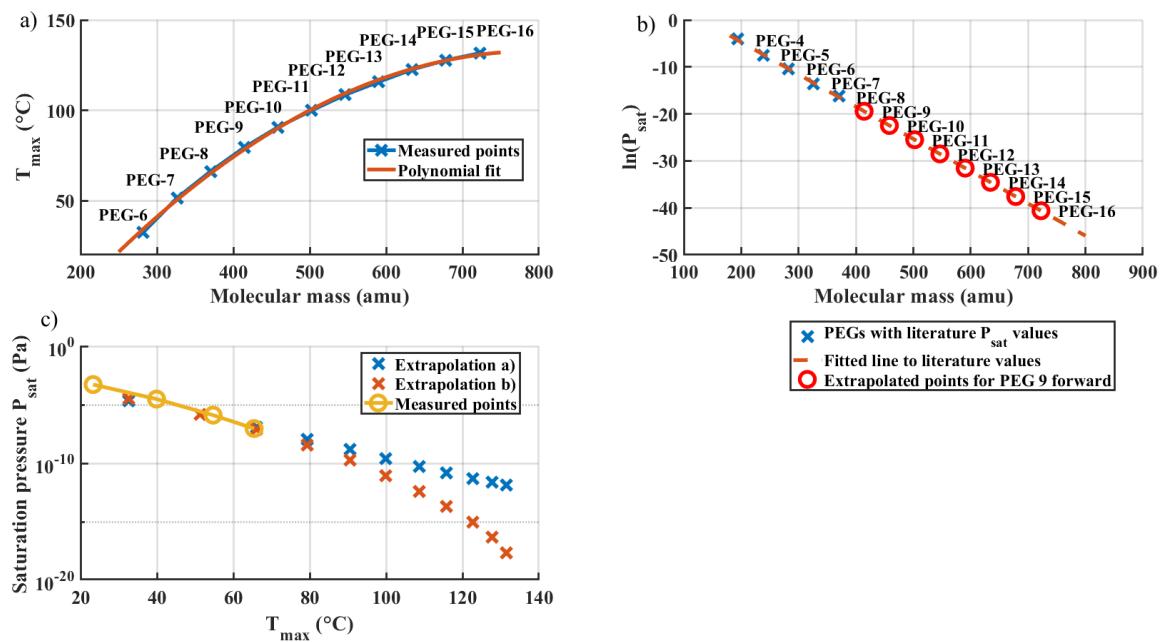
90

91 In Fig S3 c) we show two extrapolations for P_{sat} vs. measured T_{max} . Extrapolation a) was done by
92 substituting T_{max} values in eq. (2) with the polynomial fit to molecular mass ($T_{max} = d Mw^2 + e Mw +$
93 f , where Mw is molecular weight and d , e and f are fitted constants), shown in Fig. S3a, while using fit
94 coefficients a and b from eq. (2). I.e., extrapolation a) estimates P_{sat} values based on molecular mass.

96 Extrapolation b) was done by directly fitting the normal logarithm of P_{sat} vs molecular mass (Fig. S3
97 b).

98

99 As can be seen, the two extrapolation methods for P_{sat} lead to substantially different extended
100 calibration curves in the higher desorption temperatures. Our results anyhow strongly suggest that
101 higher order PEGs could be used for extending the volatility calibration range, if their saturation
102 vapor pressures were established by accurate independent measurements or estimated with high
103 enough certainty.



104
105 *Figure S3. Panel a) measured T_{max} values (crosses) vs. molecular mass of the PEGs contained in the*
106 *PEG-400 mixture, and a polynomial fit applied to the data. Panel b) natural logarithm of saturation*
107 *pressure vs. PEG molecular mass, and a linear fit to the literature-supported data sub-set (crosses),*
108 *extrapolated to extend to all other PEGs (circles). Panel c) saturation pressure P_{sat} vs T_{max} extrapolated*
109 *to cover all PEG, using extrapolations based on the fitted functions in panels a) and b).*

110

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