



Supplement of

Triple oxygen isotope composition of CO_2 in the upper troposphere and stratosphere

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Figure 11 in the main text uses the discrimination of assimilation against $\Delta'^{17}O$ as established in Adnew et al. (2020) to parameterize the isoflux from assimilation. The results shown there are for a temperature of 15°C and relative humidity of 75 %. Here we illustrate the dependence of the results on pressure and temperature.

$$\Delta_A \Delta'^{17} O = (\Delta'^{17} O_{UT} - \Delta'^{17} O_M) \times (-0.150 \times e^{3.707 \times \frac{c_m}{c_a}} + 0.028)$$
(S1)

Figure S1 shows the sensitivity of the discrimination against $\Delta^{'17}O(\Delta_A \Delta^{'17}O)$ to relative humidity and temperature. The 5 value of $\Delta_A \Delta^{'17}O$ increases with rising relative humidity but decreases with increasing temperature. Both relative humidity and temperature influence equation S1 through $\Delta'^{17}O_M$ (see equation S2) (Adnew et al., 2020). An increase in relative humidity enlarges the difference betwen the three isotope slope of transpiration and the reference slope ($\theta_{trans} - 0.528$), which lowers $\Delta'^{17}O_M$. This, in turn, raises the $(\Delta'^{17}O_{UT} - \Delta'^{17}O_M)$ difference, leading to stronger discrimination (see Figure S1a). Conversely, when temperature increases, both $\alpha_{CO_2-H_2O}$ and α_{trans} decrease, resulting in a relatively enriched $\Delta'^{17}O_M$ value. 10

This reduces the $(\Delta'^{17}O_{UT} - \Delta'^{17}O_M)$ difference and, consequently, leads to a lower discrimination (see Figure S1b).

$$\Delta^{'17}O_M = \Delta^{'17}O_{MW} + (\theta_{trans} - 0.528) \times ln\alpha_{trans} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O}$$
(S2)



Figure S1. Relationship between c_m/c_a and $\Delta_A \Delta'^{17}$ O under varying conditions of relative humidity (a) and temperature (b), based on the experiments by (Adnew et al., 2020). Relative humidity and temperature are indicated by the colour bars.

The mass balance model discussed in the main text solves for the GPP flux based on assumptions of several other parameters.

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Here we illustrate the dependence of this calculation on these assumptions. Figure S2 illustrates the dependence of Gross Primary Production (GPP) on the net isoflux of Δ'^{17} O from the stratosphere to the troposphere (Δ'^{17} O_{ST}-isoflux, panel a) and the Δ'^{17} O value of the upper troposphere (panel b) for different c_m/c_a values (color bars in both panels). A higher net isoflux of Δ'^{17} O to the troposphere leads to an increase in GPP to maintain the steady state assumption (see Equation 5 in the main text and Figure S2a). Conversely, a higher $\Delta'^{17}O_{UT}$ results in a lower GPP, as it increases the $\Delta_A \Delta'^{17}O$ value (see Figure S2b). Figure S3 illustrates the sensetivity of GPP to relative humidity and temperature, again with different c_m/c_a ratios indicated as color bars. An increase in relative humidity leads to a decrease in GPP due to an increase in $\Delta_A \Delta^{'17}$ O. Conversely, an increase 20 in temperature results in an increase in GPP, as higher temperatures cause a decrease in $\Delta_A \Delta'^{17}$ O, as described above.

The $\Delta'^{17}O$ value of CO₂ equilibrated with ocean water and diffused back to the atmosphere ($\Delta'^{17}O_o$) is calculated from the $\Delta'^{17}O$ value of ocean water (OW) as $\Delta'^{17}O_o = \Delta'^{17}O_{OW} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{diff-water} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln\alpha_{CO_2 - H_2O} + (\theta_{CO_2 - H_2O} - 0.528) \times ln$



Figure S2. Sensitivity of GPP to the Δ'^{17} O stratosphere-troposphere isoflux and Δ'^{17} O value of upper troposphere. (a) The relationship between Δ'^{17} O stratosphere-troposphere isoflux and GPP, with different c_m/c_a ratios indicated by the color bar. (b) The relationship between Δ'^{17} O in the upper troposphere and GPP, with different c_m/c_a ratios indicated by the color bar.

 $ln\alpha_{diff-water}, \text{ where } \theta_{\text{diff-water}} \text{ is the oxygen triple isotope slope for CO_2 diffusion in solution (water). The } \Delta^{'17}O \text{ values of soil invasion and soil respiration are calculated from the } \Delta^{'17}O \text{ value of meteoric water (MW), as } \Delta^{'17}O_{SI} = \Delta^{'17}O_{MW} + (\theta_{CO_2-H_2O} - 0.528) \text{ and } \Delta^{'17}O_R = \Delta^{'17}O_{MW} + (\theta_{CO_2-H_2O} - 0.528) + (\theta_{diff-air} - 0.528) \times ln\alpha_{diff-soil}.$



Figure S3. Sensitivity of GPP to relative humidity (a) and temperature (b), with different c_m/c_a ratios indicated by the color bar.

Table S1. Information on flight numbers of the Caribic flights with the whole air sampler (WAS) from which samples were analyzed for this study, with flight dates and flight routes.

Sample	Date	Route
WAS-25	28-July-2000	Windhoek to Munich
WAS-28	18-Oct-2000	Male to Munich
WAS-29	05-Nov-2000	Male to Düsseldorf
WAS-30	03-Dec-2000	Capetown to Munich
WAS-31	19-Jan-2001	Colombo to Düsseldorf
WAS-32	01-Apr-2001	Colombo to Düsseldorf
WAS-33	14-May-2001	Holguin to Düsseldorf
WAS-34	19-May-2001	Düsseldorf to Isla Margartia
WAS-35	11-June-2001	Holguin to Düsseldorf
WAS-36	25-June-2001	Holguin to Düsseldorf
WAS-37	9-July-2001	Holguin to Düsseldorf
WAS-47	27-Apr-2002	Varadero to Düsseldorf



Figure S4. a) CARIBIC N_2O data de-trended to the year 2001 versus CO. b) Histogram of CARIBIC N_2O data de-trended to the year 2001. Red lines (313.5 ppb) indicate the cut-off between upper tropospheric and stratospheric air.

Table S2. Sampling altitude and coordinates, mole fraction of CO₂ and other trace gases, and the δ^{13} C, δ^{17} O, δ^{18} O, and Δ'^{17} O values of CO₂ for CARIBIC samples. WAS stands for whole air sample.

Sample	Long	Lat	CH4	CO_2	N ₂ O	δ^{14} CO	02	CO	$\delta^{13}C$	δ^{18} O	δ^{17} O	$\Delta'^{17}0$
WAS-25-1	16.01	-18.05	1751.13	368.02	314.88	8.471	60.28	96.62	-8.023	39.307	20.294	-0.266
WAS-25-2	14.49	-12.99	1744.27	368.7	314.67	8.387	62.89	73.98	-8.054	41.793	21.623	-0.226
WAS-25-3	12.91	-7.95	1744.35	368.65	314.67	61.592	65.49	75.55	-8.073	41.997	21.754	-0.201
WAS-28-1	70.13	8.72	1770.9	366.74	315.37	5.528	28.52	85.79	-7.951	40.914	21.164	-0.229
WAS-29-2	66.77	12.88	1744.97	368.03	315.01	7.652	57.94	94.99	-8.014	42.289	21.881	-0.224
WAS-30-1	18.58	-28.8	1728.63	368.59	314.7	8.565	67.73	65.13	-8.035	41.461	21.437	-0.240
WAS-30-2	17.71	-23.78	1751.8	369.03	315.29	7.062	63.57	90.08	-8.042	42.330	21.915	-0.212
WAS-30-3	16.23	-18.8	1746.11	368.48	315.3	6.694	46.17	95.75	-8.038	42.299	21.888	-0.222
WAS-30-4	14.7	-13.72	1743.99	368.42	315.13	6.879	44.82	98.83	-8.027	42.311	21.885	-0.232
WAS-30-5	13.2	-8.65	1767.5	367.76	315.43	6.931	42.94	110.1	-8.002	42.342	21.914	-0.218
WAS-30-6	11.15	-3.69	1748.38	368.81	315.41	-7.986	89.67	428.4	-8.033	42.084	21.792	-0.207
WAS-30-7	9.54	1.49	1776.6	369.77	315.68	8.129	51.37	140.8	-8.049	42.277	21.879	-0.220
WAS-30-8	9.18	7.3	1764.97	369.04	315.44	7.947	44.86	96.92	-8.034	41.837	21.661	-0.211
WAS-30-9	8.41	13.3	1759.65	369.06	315.52	7.862	55.25	95.27	-8.031	41.804	21.609	-0.244
WAS-30-10	7.88	19.14	1758.88	368.93	315.45	7.566	49.79	93.12	-8.031	41.828	21.651	-0.216
WAS-30-11	7.26	24.77	1770.74	368.58	315.17	10.169	54.73	77.49	-8.033	41.441	21.465	-0.201
WAS-30-12	6.85	30.18	1779.24	369.31	315.14	8.143	40.09	82.53	-8.077	41.284	21.377	-0.208
WAS-31-1	75.35	9.93	1763.85	369.87	315.62	7.251	27.15	95.77	-8.066	41.407	21.42	-0.229
WAS-31-2	71.15	13.34	1767.7	370.03	315.57	-8.035	113.8	624.8	-8.063	42.206	21.843	-0.220
WAS-31-3	67.04	16.52	1761.45	369.77	315.64	8.709	58.75	111.4	-8.055	42.209	21.837	-0.227
WAS-31-4	62.87	19.56	1757.4	369.61	315.61	8.126	51.62	102	-8.054	41.976	21.713	-0.230
WAS-31-10	40.79	40.41	1753.95	369.27	312.01	35.816	146.5	69.99	-8.082	41.307	21.464	-0.135
WAS-31-11	34.43	42.79	1734.7	368.31	308.5	59.519	238.8	51.1	-8.042	41.652	21.727	-0.052
WAS-32-1	74.9	10.3	1748	371.21	315.68	6.471	51.1	86.29	-8.113	41.902	21.694	-0.211
WAS-32-2	70.48	13.87	1745.58	371.01	315.52	6.55	46.73	83.49	-8.123	41.537	21.497	-0.219
WAS-32-3	66.1	17.22	1737.53	370.51	315.42	5.889	42.46	72.97	-8.097	41.967	21.715	-0.224
WAS-32-12	22.53	46.53	1756.2	371.74	312.08	26.277	136.2	100.77	-8.188	41.769	21.703	-0.135
WAS-33-1	-70.36	21.7	1750.6	373.2	315.7	-8.202	89.83	734	-8.217	41.662	21.562	-0.219
WAS-33-2	-64.63	24.14	1748.2	372.83	315.68	7.681	26.95	89.08	-8.200	41.817	21.636	-0.225
WAS-33-3	-59.14	27.34	1755.85	372.97	315.82	6.597	33.79	95.18	-8.211	41.827	21.636	-0.230
WAS-33-6	-40.34	35.8	1796.6	373.26	315.47	11.774	86.19	111.6	-8.244	42.066	21.771	-0.219
WAS-33-7	-33.58	38.68	1774.85	373.83	314.33	14.476	75.83	98.29	-8.281	41.810	21.681	-0.177
WAS-33-8	-26.6	41.13	1760.55	372.91	311.39	25.412	151.6	92.54	-8.233	41.908	21.892	-0.108
WAS-33-9	-19.64	43.11	1650.2	368.25	293.5	80.51	467.8	42.01	-8.040	41.623	22.107	0.335
WAS-33-10	-12.94	45.69	16/3.15	369.12	297.45	71.902	410.6	49.67	-8.075	41.833	22.11	0.231
WAS-34-1	-0.01	51.22	1/96.05	3/3.44	315.54	13.464	104	103.6	-8.247	41.680	21.5//	-0.214
WAS-34-7	-39.81	43.02	1698.67	370.42	301.93	54.689	332.4	59.86	-8.129	41.727	21.969	0.146
WAS-34-9	-48.46	35.4	1708.8	3/3.01	313.99	14.607	92.11	99.54	-8.254	41.680	21.613	-0.178
WAS-35-8	-23.18	40.51	1/34.9/	370.57	300.85	52.004	250.9	79.08	-8.118	42.067	21.974	-0.021
WAS-35-11	3	49.04	1083.88	370.14	299.7	55.924 7.40	50.42	270.0	-8.100	42.041	22.159	0.174
WAS-30-1	-//.51	20.03	1756.9	271.25	211.64	10 566	39.43	96.21	-6.204	41.044	21.038	-0.222
WAS-50-0	-34.89	49.77	1730.8	270.04	200.04	19.500	208.4	00.51	-0.130	41.915	21.825	-0.091
WAS-30-8	-33.93	52.79	1/42.00	268 67	202.5	20.088	474.0	03.3	-0.110	41.930	21.899	-0.028
WAS-30-9	-23.69	53.1	1710.25	370.07	292.5	38 /01	4/4.9	47.40	-0.040	41.034	22.109	0.579
WAS-30-10	-14.2	23.16	1750.8	371.46	315.39	7 660	62.36	76.7	-0.111	41.019	21.958	0.070
WAS 27 12	-12.23	51.02	1770.65	260.84	210.02	24.511	175 4	101.1	-0.139	41.000	21.000	0.190
WAS-57-12	57.34	36.08	1757.86	374.66	312.60	24.311	1/3.4	08.2	-0.09/	41.952	21.002	0.055
WAS-47-11	-10.21	49.73	1653.2	369.9	204.4	83.034	441	47.57	-8.057	41 866	21.072	0.101
WAS_47_12	_1 27	51.53	1646.6	369.73	293.18	86 573	461.7	45.88	-8.048	42 076	22.143	0.337
1110-47-12	-1.4/	51.55	1070.0	00.15	275.10	00.575	1 101.7	10.00	-0.0-0	12.070	44.544	0.557

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Sampla Nama		Lat	Long	NO	0	СЦ	CO	CO	s13C	\$170	s180	Λ'^{17} 0
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		15 208	22 70	20.05	327.02	03	1007	284.75	00	0 C	21.062	12 484	0.244
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	KL_F5_06	11.091	41.01	22.07	327.02		1907	402.72	51	-0.332	21.902	42.404	-0.244
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	KL-FL2-12	11.001	41.01	23.97	325.03		1832.9	402.72	70	-6./0/	27.249	45.117	-0.139
KL-FL3-05 17.57 34.65 27.34 320.35 1818.7 402.11 35 -8.7/2 17.785 43.506 -0.038 KL_FG_3O7 17.82 29.72 317.470 1824 402.07 38 -8.706 18.302 42.806 0.049 KL-FL3-04 17.545 35.11 26.12 311.74 1772.9 405.62 29 -8.720 15.173 42.585 0.177 KL-FL3-05 18.418 34.54 25.68 300.32 490 1723 401.61 17 -8.729 8.799 43.341 0.140 KL-FL2-05 18.418 34.54 25.68 300.32 490 1723 401.61 17 -8.729 8.799 43.341 0.140 KL-FL2-07 19.428 35.39 27.54 277.49 850 1622.3 399.83 14 -8.715 7.530 44.325 0.409 KL-FL2-08 19.417 35.60 30.42 275.99 1635.8 400.11 21 -8.610 11.269 43.900 0.652 KL-F12.01 19.98 39.06 </td <td>KL-FL2-13</td> <td>10.685</td> <td>40.91</td> <td>23.07</td> <td>320.85</td> <td></td> <td>1880.0</td> <td>401.62</td> <td>/9</td> <td>-8.600</td> <td>42.518</td> <td>40.464</td> <td>-0.267</td>	KL-FL2-13	10.685	40.91	23.07	320.85		1880.0	401.62	/9	-8.600	42.518	40.464	-0.267
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	KL-FL3-05	17.57	34.65	27.34	320.35		1818.7	405.11	33	-8.772	17.785	43.566	-0.038
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	KL_F3_07	17.607	33.82	29.72	317.470		1824	402.07	38	-8.766	21.917	42.072	-0.079
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	KL-FL3-01	14.834	36.56	22.58	317.23		1793.4	403.97	34	-8.502	18.302	42.806	0.049
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	KL-FL3-04	17.545	35.11	26.12	311.74		1772.9	405.62	29	-8.720	15.173	42.585	0.177
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	KL-FL3-03	17.545	35.58	24.89	311.5		1761	403.63	27	-8.752	14.430	42.898	0.133
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	KL-FL2-05	18.418	34.54	25.68	300.32	490	1723	401.61	17	-8.729	8.799	43.341	0.140
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KL-FL2-11	20.009	40.34	24.95	279.24		1629	399.83	14	-8.715	7.530	44.325	0.409
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KL-FL2-07	19.428	35.39	27.54	277.49	850	1622.3	399.21	16	-8.684	8.255	44.272	0.404
KL-FL2-08 19.417 36.70 27.07 268.32 1052 1584.3 398.6 20 -8.829 10.809 44.003 0.522 KL-FL2-10 19.98 39.06 25.57 260.43 1542.1 397.4 18 -8.445 9.549 43.509 0.683 KL_FL3-14 20.231 35.1 26.1 240.1 1493.1 397.15 17 -8.527 23.133 42.101 1.095 KT-FL2-04 15.565 29.2 81.6 329.03 89 1890.7 67 -8.720 36.082 42.941 -0.182 KT-FL2-04 15.5655 29.2 81.6 329.03 89 1890.7 67 -8.694 20.930 40.452 -0.224 KT-FL2-02 15.814 28.4 83.5 328.39 70 1902 67 -8.682 36.009 40.735 -0.225 KT-FL2-03 16.698 28.1 84.2 328.39 212 1872 32 -8.765	KL-F3-10	19.467	33.60	30.42	275.59		1635.8	400.11	21	-8.610	11.269	43.900	0.453
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KL-FL2-08	19.417	36.70	27.07	268.32	1052	1584.3	398.6	20	-8.829	10.809	44.003	0.522
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	KL-FL2-10	19.98	39.06	25.57	260.43		1542.1	397.4	18	-8.445	9.549	43.509	0.683
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	KL F3 12	20.01	34.52	27.79	255.67		1505	392.03	17	-8.527	23.133	42.101	1.095
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KL-FL3-14	20.231	35.1	26.1	240.1		1493.1	397.15	17	-8.569	8.762	43.478	1.095
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KT-FL4-04	17.182	29.1	81.7	330.29	131	1913		67	-8.720	36.082	42.941	-0.182
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KT_FL2_04	15.5655	29.2	81.6	329.03	89	1890.7		67	-8.904	20.930	40.452	-0.224
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KT-FL2-02	15.814	28.4	83.5	328.39	70	1902		67	-8.682	36.009	40.735	-0.225
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KT-FL5-15	18.168	28.1	84.2	328.39	212	1872		32	-8.765	17.073	42.790	-0.154
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KT-FL2-09	17.457	28.1	84.3	328.16	157	1890		59	-8.522	31.642	43.266	-0.180
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KT_FL5_07	16.9725	28.6	83.0	327.880	101	1878.9		81	-8.542	21.204	41.058	-0.263
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	KT-FL2-05	16.958	29.2	80.9	327.2	124	1882		57	-8.896	30.281	41.541	-0.145
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	KT-FL2-03	16.009	28.8	82.6	327	77	1892		69	-8.719	37.268	41.990	-0.141
KT-FL4-10 18.184 27.7 85.4 326.86 182 1859 45 -8.806 24.099 43.099 -0.188 KT_FL5_16 17.77 28.6 83.1 326.56 240 1832.3 23 -8.72 21.399 41.212 -0.134 KT-FL4-09 17.888 28.0 84.5 325.63 168 1879 50 -8.763 26.541 41.902 -0.167 KT-FL2-01 13.253 28.1 84.3 325.26 40 1892 79 -8.549 42.594 41.234 -0.179 KT_FL3_08 17.3735 21.4 79.7 322.61 145 1829.5 43 -8.764 21.518 41.315 -0.086 KT_FL3_10 19.797 22.5 79.6 282.13 771 1663 24 -8.593 12.641 42.102 0.417 KT_FL3_16 20.198 25.2 83.1 280.68 887 1645 23 -8.708 12.237 41.619 <td>KT_FL3_2</td> <td>16.5215</td> <td>25.7</td> <td>84.4</td> <td>326.95</td> <td>119</td> <td>1880.1</td> <td></td> <td>57</td> <td>-8.765</td> <td>20.491</td> <td>39.622</td> <td>-0.233</td>	KT_FL3_2	16.5215	25.7	84.4	326.95	119	1880.1		57	-8.765	20.491	39.622	-0.233
KT_FL5_16 17.77 28.6 83.1 326.56 240 1832.3 23 -8.72 21.399 41.212 -0.134 KT-FL4-09 17.888 28.0 84.5 325.63 168 1879 50 -8.763 26.541 41.902 -0.167 KT-FL2-01 13.253 28.1 84.3 325.26 40 1892 79 -8.549 42.594 41.234 -0.179 KT_FL3_08 17.3735 21.4 79.7 322.61 145 1829.5 43 -8.764 21.518 41.315 -0.086 KT_FL3_10 19.797 22.5 79.6 282.13 771 1663 24 -8.593 12.641 42.102 0.417 KT-FL3_16 20.198 25.2 83.1 280.68 887 1645 23 -8.708 12.237 41.619 0.428 KT-FL3_16 20.277 28.20 278.28 1049 1629 12.77 41.619 0.428	KT-FL4-10	18.184	27.7	85.4	326.86	182	1859		45	-8.806	24.099	43.099	-0.188
KT-FL4-09 17.888 28.0 84.5 325.63 168 1879 50 -8.763 26.541 41.902 -0.167 KT-FL2-01 13.253 28.1 84.3 325.26 40 1892 79 -8.549 42.594 41.234 -0.179 KT_FL3_08 17.3735 21.4 79.7 322.61 145 1829.5 43 -8.764 21.518 41.315 -0.086 KT_FL3_10 19.797 22.5 79.6 282.13 771 1663 24 -8.593 12.641 42.102 0.417 KT_FL3_16 20.198 25.2 83.1 280.68 887 1645 23 -8.708 12.237 41.619 0.428 KT_FL3_16 20.271 29.20 279.29 10.49 1629 23 -8.708 12.237 41.619 0.428	KT FL5 16	17.77	28.6	83.1	326.56	240	1832.3		23	-8.72	21.399	41.212	-0.134
KT-FL2-01 13.253 28.1 84.3 325.26 40 1892 79 -8.549 42.594 41.234 -0.179 KT_FL3_08 17.3735 21.4 79.7 322.61 145 1892.5 43 -8.764 21.518 41.315 -0.086 KT_FL3_10 19.797 22.5 79.6 282.13 771 1663 24 -8.593 12.641 42.102 0.417 KT_FL3_16 20.198 25.2 83.1 280.68 887 1645 23 -8.708 12.237 41.619 0.428 KT_FL3_16 20.27 29.2 279.29 10.49 1629 17 23 -8.708 12.237 41.619 0.428	KT-FL4-09	17.888	28.0	84.5	325.63	168	1879		50	-8.763	26.541	41.902	-0.167
KT_FL3_08 17.3735 21.4 79.7 322.61 145 1829.5 43 -8.764 21.518 41.315 -0.086 KT_FL3_10 19.797 22.5 79.6 282.13 771 1663 24 -8.593 12.641 42.102 0.417 KT_FL3_16 20.198 25.2 83.1 280.68 887 1645 23 -8.708 12.237 41.619 0.428 KT_FL3_16 20.27 29.2 278.28 10.49 1629 17 25.64 0.176 23.75	KT-FL2-01	13.253	28.1	84.3	325.26	40	1892		79	-8.549	42.594	41.234	-0.179
KT_FL3_10 19.797 22.5 79.6 282.13 771 1663 24 -8.593 12.641 42.102 0.417 KT_FL3_16 20.198 25.2 83.1 280.68 887 1645 23 -8.708 12.237 41.619 0.428 KT_FL3_16 20.27 28.2 83.1 280.68 887 1645 23 -8.708 12.237 41.619 0.428	KT FL3 08	17.3735	21.4	79.7	322.61	145	1829.5		43	-8.764	21.518	41.315	-0.086
KT-FL3-16 20.198 25.2 83.1 280.68 887 1645 23 -8.708 12.237 41.619 0.428 KT-FL3-16 20.271 28.2 83.0 279.29 1049 1670 17 8.604 0.177 42.097 0.275	KT FL3 10	19,797	22.5	79.6	282.13	771	1663		24	-8.593	12.641	42.102	0.417
VT FL2 1/ 20 271 28 2 92 0 279 29 1049 1/20 177 9 (04 0 177 42 00/ 0 275	KT-FL3-16	20.198	25.2	83.1	280.68	887	1645		23	-8.708	12.237	41.619	0.428
$ \mathbf{K} \mathbf{F} \mathbf{L} 2 0 20.2/1 28.3 83.9 2/8.38 1048 1629 -8.604 9.1/6 42.986 0.3/5$	KT FL2 16	20.271	28.3	83.9	278.38	1048	1629		17	-8.604	9.176	42.986	0.375
KT-FL3-11 20.168 23.0 80.3 277.04 929 1624 22.3 -8.632 11.817 41.434 0.464	KT-FL3-11	20.168	23.0	80.3	277.04	929	1624		22.3	-8.632	11.817	41.434	0.464
KT FL2 18 20.325 29.1 81.7 269.27 1061 1601 18 -8.563 9.416 41.939 0.741	KT FL2 18	20.325	29.1	81.7	269.27	1061	1601		18	-8.563	9.416	41,939	0.741

Table S3. Sampling altitude and coordinate, mole fraction of CO_2 and other trace gases and the $\delta^{13}C$, $\delta^{17}O$, $\delta^{18}O$ and $\Delta'^{17}O$ of CO_2 for StratoClim samples



Figure S5. Zonal average tropopause (pressure altitude versus latitude) as modeled with the TM5 model, together with locations of the collected samples analysed in this study. The color bar specifies the artificial transport tracer E90, which is a the tracer with surface emissions and an atmospheric lifetime of 90 days (E90) (Krol et al., 2018). The data points are colored in three groups based on their N₂O values, blue marker for N₂O \geq 313.5 ppb, gray marker for 313.5 > N₂O > 306 ppb and black marker for N₂O < 306 ppb.

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