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**Development of an
autonomous sea ice
tethered buoy**

T. N. Knepp et al.

Development of an autonomous sea ice tethered buoy for the study of ocean-atmosphere-sea ice-snow pack interactions: the O-buoy

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Abstract

A buoy based instrument platform (the “O-buoy”) was designed, constructed, and field tested for year-round measurement of ozone, bromine monoxide, carbon dioxide, and meteorological variables over Arctic sea ice. The O-buoy operated in an autonomous manner with daily, bi-directional data transmissions using Iridium satellite communication. The O-buoy was equipped with three power sources: primary lithium-ion battery packs, rechargeable lead acid packs, and solar panels that recharge the lead acid packs, and can fully power the O-buoy during summer operation. This system was designed to operate under the harsh conditions present in the Arctic, with minimal direct human interaction, to aid in our understanding of the atmospheric chemistry that occurs in this remote region of the world. The current design requires approximately yearly maintenance limited by the lifetime of the primary power supply. The O-buoy system was field tested in Elson Lagoon, Barrow, Alaska from February to May 2009, and here we describe the design and present preliminary data.

1 Introduction

The Arctic has been a source of fascination and study since the time of Aristotle (Strabo, 1966), with significant scientific interest and discovery beginning in the early twentieth century (Whitfield, 1900; Warren, 1911). Polar regions are unique in that atmosphere/surface interactions, which determine the composition of the troposphere, are significantly impacted by air-ice (e.g. aerosol, gas, snow) heterogeneous physical and chemical processes.

During polar spring, air masses that are in contact with sea ice undergo significant ozone depletion events (ODEs) in which the mole fraction of tropospheric ozone decreases to nearly zero in a relatively short period of time (e.g. 1 d). These ODEs were first observed in the mid-1980s (Bottenheim et al., 1986; Oltmans and Komhyr, 1986; Barrie et al., 1988), and have continued to be a source of intense study. Such ODEs

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are believed to result from bromine chemistry that catalytically destroys ozone (Barrie et al., 1988), with inter-halogen reactions (especially those with chlorine) possible. Satellite (Richter et al., 1998; Wagner and Platt, 1998; Kaleschke et al., 2004) and other observations (Simpson et al., 2007a) indicate that air masses that have been in contact with sea ice, particularly the saline first-year sea ice, exhibit halogen chemistry and ozone depletion, leading to the conclusion that sea salt is the primary halogen source (Fan and Jacob, 1992; Tang and McConnell, 1996; Simpson et al., 2007b). However, the mechanism by which sea salts are converted to reactive halogen gases is unclear, and a number of theories exist. Frost flower surfaces have been proposed to be involved (Rankin et al., 2000), and a number of studies have investigated this hypothesis (Kaleschke et al., 2004; Dominé et al., 2005; Kalnajs and Avallone, 2006). Snow contaminated with sea salts may also hold a key role (Impey et al., 1997; Dominé and Shepson, 2002; Simpson et al., 2005, 2007a). Direct production of halogen gases from salt-contaminated snowpack has been observed (Foster et al., 2001), as well as indirect observations of halogen losses from snowpack (Simpson et al., 2007b; Alvarez-Aviles et al., 2008). Aerosol surfaces, possibly from the breakup of frost flowers, are also a candidate (Fan and Jacob, 1992; Kaleschke et al., 2004). Modeling studies have also attempted to simulate halogen activation and ozone depletion.

Global atmospheric CO₂ mole fractions are at the highest levels of the past 25 million years. Current levels of CO₂ have increased by 35% from 280 ppm in pre-industrial times to ~387 ppm today, and they continue to rise. For the decade of the 1990s, an average of about 6.3 Pg C per year as CO₂ was released to the atmosphere from the burning of fossil fuels (Ding et al., 2001). Only half, on average, of the CO₂ from anthropogenic emissions has remained until now in the atmosphere (Ciais et al., 1995; Keeling et al., 1996; Battle et al., 2000). Analyses of the decreasing ¹³C/¹²C and O₂/N₂ ratios in the atmosphere have shown that land and oceans have sequestered the other half, in approximately equal proportions but with temporal and spatial variations. The Arctic Ocean is usually not included in these calculations as models presume a sea-ice capped region without much ocean/sea, ice/atmosphere exchange.

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Because global climate models show large deviations in their simulations of current conditions in the Arctic region (Proshutinsky et al., 2005), the effect of changing ice cover (at $\sim 7\%$ decrease/decade, Comiso, 2002) and thickness on $p\text{CO}_2$ fluxes in the Arctic Ocean is not clear. Furthermore, the role of sea ice as a barrier to, or an integral player of, CO_2 air/sea and/or air/ice fluxes (Papakyriakou et al., 2004; Semiletov et al., 2004) is least understood, with both the direction and amount of CO_2 transfer between air and sea/ice varying in the thaw/freeze and open water seasons due to sea-ice melt ponds, open brine channels, leads and photosynthesis.

It is important to note that the Arctic has changed rapidly over the past fifty years (Holland et al., 2006; Lindsay and Zhang, 2006), with large increases in first year sea-ice. This will likely induce significant changes in the surface interactions with respect to ODEs, and the extent to which the Arctic Ocean will become a more important sink for CO_2 . Climate models predict a predominantly ice-free Arctic Ocean in summer by the end of the century (Johannessen et al., 2004; Holland et al., 2006; Stroeve et al., 2007), implying a change in the sea-air fluxes of CO_2 . Validation of such models will require independent information on spatial and temporal patterns of CO_2 sources and sinks in the Arctic Ocean in order to improve our ability to predict future regional and global CO_2 fluxes.

Though there have been many land-based measurements throughout the Arctic, these measurements have been spatially limited (e.g. no measurements from the Siberian side of the Arctic Ocean), with the majority of campaigns taking place in the spring. Additionally, there have been several late-spring and summer ice breaker cruises (Weller and Schrems, 1996; Jacobi et al., 2006) to study a variety of atmospheric and oceanic phenomena over the sea ice; however, such cruises are relatively short, often spatially limited, and expensive due to the cost of ice breaker operation. Such limited efforts, though extremely useful, fail to provide a full picture of atmospheric chemical processes over the Arctic Ocean as a function of time and space, especially in the more remote northern latitudes and during the dark winter/early spring months. Acquisition of year-round measurements of atmospherically relevant chemical species

and meteorological parameters will be highly elucidative for the purpose of understanding chemical mechanisms, transport pathways/processes, and understanding the necessary conditions for Arctic unique chemistry.

Acquisition of such data has proven to be difficult and potentially dangerous to researchers and instrumentation due to the extremely harsh environment in the Arctic: e.g. extreme low winter temperatures, variable sea-ice conditions, sea-spray, and wildlife. To date, there have been very few surface CO₂, BrO, or O₃ measurements over the Arctic Ocean, although there are land-based year-round monitoring stations at Barrow, Alert, and Zeppelin Station. The only long term record of O₃ observations has recently been obtained during the 16 month drift of the schooner TARA (Bottenheim et al., 2009). For several years, the International Arctic buoy Program (IABP) has successfully monitored sea-ice and ocean temperatures/salinity (Rigor et al., 2000; Haas et al., 2008). However, the IABP has, to date, not studied the chemistry occurring in this region. Clearly, there is a significant gap in our understanding of this region as compared to other, more accessible regions of the world, and more work must be done. To this end, an autonomous sea-ice tethered, buoy-based instrument platform, capable of operating under Arctic Ocean conditions for a time period on the order of a year to record gas-phase O₃, CO₂, and BrO data, with daily transmission of data via satellite, was developed. We discuss the details of this O-buoy and its performance during a test phase deployment at Barrow, AK herein.

2 Instrumentation

2.1 O-buoy hull and mast

An autonomous O-buoy system capable of year-round measurement of O₃, CO₂, and BrO, while deployed in sea-ice, was designed and constructed. A critical design objective for the O-buoy was to operate the instruments with (necessary) temperature control, but at minimal power cost, since winter operation will be powered via on-board

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batteries. Thus, the design put the three main instruments at the bottom of the O-buoy, which was immersed in the sea-water below the ice, to maintain near constant temperature (i.e. -1.5°C).

The O-buoy hull was constructed from quarter-inch aluminum at the US Army Corps of Engineers Cold Regions Research and Engineering Laboratory in New Hampshire, and is represented schematically in Figs. 1 and 2. The main O-buoy housing was an aluminum cylinder 2.4 m long and 0.3 m in diameter. Three primary lithium battery packs, two cylinders containing CO_2 calibration gases (at 368.6 ppm and 396.6 ppm), Iridium communication equipment, the O_3 instrument, power control and supervisory computer, data logger (CR1000 Campbell Scientific Instruments), Iridium modem, CO_2 , and MAX-DOAS instruments were placed inside the main housing. A 2 m high tower was placed on top of the hull, from which meteorological sensors, camera, global positioning system (GPS), and the MAX-DOAS's scan head were mounted (Fig. 2). Connections were made between the tower and the main housing using Amphenol Class E Environmental connectors. A flotation collar (Gilman Corporation Type 1000) provided buoyancy in case the O-buoy melted free of the ice. The collar was 1.1 m OD \times 0.64 m H and provided 482 kg of buoyancy. The instruments, computer, and lithium-ion batteries were secured to an aluminum tray (Fig. 1) that could be slid into, and out of, the hull. The tray was constructed of eighth-inch aluminum with aluminum supports. The overall dimensions of the O-buoy were 4.2 m tall, 1.1 m wide, and 280 kg.

2.2 Ozone instrument

Ozone was measured with a 2B Technologies model 205 dual-beam UV-absorption sensor that was specially constructed for this endeavor. It functions by UV-absorption at 254 nm, with one flow path scrubbed of O_3 for the I_0 measurement. The instrument's modifications involved addition of a lamp heater, a back-up pump, back-up ozone scrubber, an ozone generator, and the ability to remotely control the instrument's state, the ozone generator's output, the state of the lamp heater, and the ability to switch the pump and scrubber. The 2B was housed in an aluminum case (positioned

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approximately 0.5 m from the bottom of the O-buoy, Fig. 1), with the lid acting as the bottom of the power control board and supervisory computer case. The electrical connectors between the inside and outside of the 2B's case were Amphenol connectors, and the plumbing connections were PTFE Teflon Swagelok. The sample inlet line was 4 mm PTFE Teflon (4 m long), and the exhaust line was 8 mm PTFE Teflon (4 m long). The inlet line was inserted into the exhaust line to make a coaxial configuration, which allowed the outlet gas to warm the inlet gas, thus reducing the chance of condensation on the lines. The sample lines were connected between the mast and hull using a custom built bulkhead which maintained the coaxial configuration. The lines were configured in such a way that the exhaust exited the mast at a distance of approximately one meter from the inlet. The instrument's inlet was approximately 1.5 m up on the mast, and had a 90 mm quartz fiber filter (Pall Life Sciences Membrane Filter) held in place by a machined stainless steel filter holder.

Due to the limited power supply, power minimization for each instrument was extremely important. As compared to other UV absorption ozone sensors, the 2B is a relatively low power instrument. The power consumed in a variety of operation states was recorded and plotted (Fig. 3; average 7.3 W). Figure 3 is representative of the type of power measurements done for each instrument on the O-buoy. Such information was useful not only for budgeting power, but also for minimizing the risk of system failure due to transient draws from multiple components. The ozone instrument was operated for three hours per-day (centered around solar noon) from 11 February to 2 March. It was then set to collect data all day (10 s averages; except during data transmission) from 2 March to the time the O-buoy was recovered on 19 May.

Calibration: Though the 205's internal processor accounts for cell temperature and pressure fluctuations in the calculation of ozone mole fraction, verification of the accuracy/precision of this calculation was performed. The 205 was calibrated as a function of environment/ cell temperature by placing the instrument in a temperature controlled freezer (Fig. 4). The 205 was controlled through a serial connection to a Linux box, and supplied with ozone from a TECO-49 ozone generator. The TECO's

ozone generation was self-monitored to allow subtraction of any fluctuations in its production from the 205's signal. The slopes and intercepts for the different temperatures showed no statistically significant differences ($<2\sigma$; i.e. there was no temperature dependence of instrument sensitivity over the range of possible operating temperatures during deployment). Additionally, changing the pump or scrubber had no effect on the reported O_3 mole fraction.

The ozone instrument was field calibrated using a 2B Technologies model 306 ozone generator (output flow rate 3.5 L min^{-1}). The 306 ozone generator required an internal temperature of 40°C ($\pm 1^\circ\text{C}$) to produce consistent mole fractions of ozone. Since the ambient temperature was -30°C the 306 was operated in a heated tent next to the O-buoy with additional heating from heat tape that was wrapped around the instrument with the applied voltage controlled by a variac, with power supplied by a generator. The 306 was programmed to produce 0 ppb, 5 ppb, 15 ppb, 30 ppb, 55 ppb, and 95 ppb ozone for 5 min per mole fraction. The O_3 generator's outlet (1/4" PTFE Teflon tube; 7 m long) was run from inside the tent to the ozone inlet on the O-buoy. The O-buoy's inlet was covered with aluminum foil that was secured to the filter holder using zip ties. The 306 generator outlet tube was inserted through a hole in the foil to flow ozone standard air directly onto the inlet filter. We are confident that there was no mixing of outside air that would alter the calibration gas for the O-buoy's ozone instrument as that instrument sampled at a rate of 750 mL min^{-1} as compared to the generator's flow rate of 3.5 L min^{-1} .

2.3 CO_2 instrument

An autonomous CO_2 sensor was built around the LI-COR 820 IR instrument, a single path, dual wavelength, non-dispersive infrared gas analyzer that allows measurement of absolute concentrations of CO_2 in air. This instrument was adapted for buoy deployment as part of the TAO/TOGA buoy array in the equatorial Pacific and for numerous coastal buoys and drifters where the primary focus was the measurement of sea surface $p\text{CO}_2$ (Friederich et al., 1995; Friederich et al., 2008); see

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http://www.pmel.noaa.gov/co2/moorings/. Measurement precision and accuracy were improved by almost an order of magnitude for the O-buoy deployment where the measurement of atmospheric $p\text{CO}_2$ was one of the main goals. The precision of the deployed system was about ± 0.1 ppm and the accuracy was estimated to be ± 0.2 ppm due to uncertainties in the standard gases as well as residual errors in the temperature and pressure corrections.

The CO_2 system was controlled by a low power controller (ONSET TT8v2) equipped with a set of custom made interface boards that scheduled the analyzer, pumps, and valves, collected and formatted the data, and stored all information in flash memory before passing it on to the supervisory computer for transmission. A sampling frequency of 8 measurements per day was selected; this frequency allowed the resolution of significant events while conserving power. A complete sampling cycle took 6 min and had a mean power consumption of 3.5 W. The standby power consumption was less than 0.04 W. Power requirements were kept low by operating the infrared analyzer at ambient temperature without stabilization. Temperature of the measurement cell was monitored at all phases of the sample cycle and data were corrected to a common temperature using laboratory and field derived calibrations. Another factor that kept power consumption low was the choice of gas switching and distribution valves (ASCO Series AM33) that were magnetically latching and only required a 100 ms pulse to change position. Gas aspiration and circulation was achieved with a small diaphragm pump (KNF Neuberger UNMP015M) operated at reduced voltage with additional flow restriction to limit gas flows to about 100 mL min^{-1} . Prior to entering the infrared analyzer all gases were dried and filtered through $0.22 \mu\text{m}$ hydrophobic filters. Drying was accomplished in sequential sections of Nafion (Permapure) tubing embedded in molecular sieve 4A. Nafion allows the passage of water vapor but has no effect on CO_2 or major components of air and these dryers work especially well at low temperatures (Leckrone and Hayes, 1997). The capacity of these dryers was designed to provide drying of water saturated samples at 0°C for several years of sampling. Laboratory tests indicate that the absolute water vapor dilution of the samples was equivalent to less than 0.1 ppm

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CO₂ and that the difference between the water vapor pressure of the standards and the samples were on the order of 0.005 kPa, thus generating uncertainties on the order of 0.02 ppm in the final CO₂ results. Water vapor changes in the gas stream were estimated with a humidity sensor designed for measurement of low humidity (Humirel HM1520LF) mounted in the outlet of the infrared analyzer.

A complete sampling cycle consisted of several distinct operations that are described below:

Zero (power up): Power is applied to the infrared analyzer which has a “warm up” time of 1 min. While waiting for the analyzer to stabilize, the valves in the gas manifold are switched to form a closed loop with the analyzer, pump, a soda lime cartridge and the Nafion dryers. The pump is started up and the trapped gas is circulated for one minute until all CO₂ has reacted with the soda lime and removed from the gas stream. A reading of all parameters (CO₂, cell temperature, pressure and water vapor) is made immediately before turning the circulation pump off. A second reading is taken 10 s later; those readings are used in the final calculations of $p\text{CO}_2$ since they occur in a more noise-free environment and at a cell pressure that is closer to the ambient atmospheric pressure. Comparison of the two measurements allowed an estimate of pump effectiveness and the condition of the in-line filters. The zero values had a predictable offset of $-1.2 \text{ ppm } ^\circ\text{C}^{-1}$ and had a long-term drift of about $-0.3 \text{ ppm per month}$.

Standards: After determining the instrument response at zero CO₂ levels, two gas standards are analyzed sequentially. To conserve standard gases this analysis was performed during alternate sample cycles. The gases were contained in 1 L aluminum cylinders with stainless steel manifolds. Delivery was controlled with a small two stage regulator (Scott Specialty Gases Model 14) coupled to a needle valve. Flow rates were set at 100 mL min^{-1} near the expected internal buoy temperature (-1°C) and tested over a temperature range of -40°C to 24°C . Gas delivery increased with decreasing temperature at a rate of about 1% per degree and good flushing of the analytical system was maintained under all conditions. During a standard cycle the valve manifold

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opens a path from one of the standard cylinders through the Nafion dryers and into the infrared analyzer. The exhaust is vented to the outside via the outer shell of the atmospheric sampling inlet. Gas flows for one minute after which valves are switched to vent any overpressure to the atmosphere. The procedure is then repeated for the second cylinder. Data were collected when the gas is flowing and when it is stopped and the pressure difference between the two readings is a measure of gas flow. No change in flow rate was detected during the 6 month test phase. The standards indicate that instrument sensitivity at the 400 ppm CO₂ level decreased at a rate of about 0.4 ppm per month during the deployment.

Air sampling: Following the standard gas analysis, the valve manifold is switched into air sampling mode. In this mode, air is aspirated from the external inlet located on the buoy mast and then passes through the Nafion dryers before entering the infrared analyzer. The exhaust gases exit via the outer shell of the coaxial inlet line. The sample is actively pumped for one minute to flush the analytical manifold. Data were collected before turning the pump off and again after a 10 s relaxation period. Air enters the inlet system near the top of the buoy mast through a protected hydrophobic 0.45 μm pore size membrane (Pall Supor-450R). The air then enters a length of Nafion tubing in a small chamber which contains the exhaust gas. Since the exhaust gas is always drier than ambient air, the freshly sampled air will have some of its moisture removed and is less likely to form ice in the inlet line while traveling down the mast. The inlet line from the top of the mast to the instrumentation consists of coaxial FEP tubing with the incoming air flowing down in the center and the warmer exhaust gas flowing up in the sheath. This arrangement aids in the temperature equilibration of the incoming air and may decrease the possibility of ice formation in the incoming gas stream; an additional benefit is better organization of tubing inside the mast. Data from the pressure sensor while the system was being pumped indicate that the intake filter and gas path remained unobstructed during the entire deployment.

Zero (power down): Before removing power from the analytical system, a final zero CO₂ measurement is obtained in manner identical to the zero obtained at the start.

This procedure put the system in an identical rest state between samples and also provides another temperature calibration point since the final temperature is about one degree higher than the starting temperature.

Calibration: Prior to deployment the instrument was placed in an environmental chamber and subjected to temperatures as low as -35°C to examine the limits of operation. At temperatures below -25°C the gas switching valves became unreliable and power consumption of the gas circulation pump increased; the infrared analyzer continued to operate reliably at all temperatures. Since it was expected that the internal buoy temperature would remain near the freezing point of seawater ($\sim -1.9^{\circ}\text{C}$), we limited the testing and calibration to temperatures between -20°C and 5°C . During the Barrow deployment the temperature of the CO_2 instrument ranged from -0.5°C to -2.8°C . Laboratory calibration consisted of operating the instrument at a variety of temperatures (-20°C to 5°C) and supplying it with up to six standard gases ranging from 200 ppm to 600 ppm CO_2 in air. The gases were obtained from the National Oceanic and Atmospheric Administration's (NOAA) Earth Systems Research Laboratory (ESRL). The calibration obtained in the laboratory was augmented in the field with a 3-point calibration done via a soda lime chamber to generate a zero standard and two small, high pressure CO_2 gas standards contained in the buoy housing. The two gas standards (368.6 and 396.6 ppm supplied by ESRL) spanned the annual range of $p\text{CO}_2$ that has been observed at the NOAA Barrow Observatory in recent years. Standard gas calibrations were performed 4 times per day throughout the campaign and a 24 h running mean was utilized to make final adjustments to the data stream. Deployment data also indicated that there was a small residual pressure correction that was not accounted for in the original infrared analyzer firmware. The pressure correction adjustment was derived empirically from the analysis of the standards during the deployment and then applied to the entire record.

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2.4 MAX-DOAS (BrO Instrument)

The MAX-DOAS instrument used in this study is described in detail in Carlson et al. (2009); we provide a brief description here. The MAX-DOAS instrument observes scattered light spectra and derives the slant column abundance of UV-absorbing gases in the observation path (e.g. BrO, IO, O₃, NO₂, HONO, etc.) as a function of view elevation angle in the atmosphere (Hönninger et al., 2004). These “elevation scans” can be inverted to give vertical profiles of the absorbers. The technique is analogous to satellite remote-sensing techniques, but with enhanced sensitivity to boundary-layer gases and vertical profiling capabilities; therefore, gaining insight into satellite measurements of BrO. Similar MAX-DOAS instruments have been used at fixed ground-based locations in the Arctic to observe halogen chemistry (Hönninger and Platt, 2002; Hönninger et al., 2004; Simpson et al., 2007b).

The instrument consisted of two portions, the scan head, which resided above the sea ice to receive skylight, and the computer/spectrometer, which resided below the ice for better temperature stability, with the two being connected by a fiber optic cable. The scan head oriented a narrow-field telescope to scan the sky for scattered radiation and then this skylight was coupled into the fiber optic connected to the spectrometer for spectral analysis. The computer/spectrometer module consisted of a low-power single-board computer (Technologic Systems TS-7260), a stepper motor driver (Stepperboard BC2D15), interface electronics, and a miniature charge-coupled device based spectrometer (Ocean Optics HR2000, 318–455 nm).

The scan head had two important features for long-term autonomous operations: defrost and tilt sensing. The defrost system used a near-ultraviolet (395 nm) light emitting diode (LED) to illuminate the optical input window at an oblique angle. If the window was clear, little of the LED light was scattered into the optical axis of the spectrometer, while when snow or frost was present, LED light was scattered into the spectrometer’s field of view. Based upon the difference of light detected by the spectrometer at the LED wavelength with the LED on minus LED off, we quantified the degree of frost

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coverage and turned on a heater if the frost signal exceeded a user-defined threshold. The tilt sensing system used a digital inclinometer (Smart Tool Technologies ISU-S) to measure the tilt of the scan head housing. We used this housing tilt to correct the horizon setting of the stepper motor to maintain accurate alignment of the view directions with respect to the true horizon. If the O-buoy's tilt were to have changed due to ice deformation or a curious polar bear, the instrument was capable of adjusting up to 20° of tilt.

The instrument operated on a schedule set by the supervisory computer. When the MAX-DOAS was switched on, its computer booted and began data acquisition, typically on a half-hourly schedule. During a half-hour measurement period, the instrument performed a number of cycles (typically four) of elevation scans from horizon to zenith. A typical scan pattern observed light at 2, 5, 10, 20, and 90 degrees elevation angles on the side of the instrument away from the sun. The sun's location with reference to the MAX-DOAS instrument's view direction was calculated from the GPS location, orientation, and coordinated universal time (UTC) time. The tilt, frost signal, various temperatures, and raw spectra were compiled in half-hourly data "records". When the supervisory computer (SC) decided to shut down the MAX-DOAS, the SC requested the instrument to complete the current acquisition, archive the data to internal storage within the MAX-DOAS, and pass the data to the supervisory computer to be uploaded to the satellite communications system.

The MAX-DOAS instrument consumed an average of 2.7 W when operating. The spectrometer consumed 540 mW, the stepper motor driver required 900 mW, and the computer used 1.3 W. The window heater consumed around 3.8 W at times when the frost sensor indicated snow or frost on the window, which was typically the first 2 h of daily operation.

Details regarding the MAX-DOAS calibration are discussed in a separate paper (Carlson et al., 2009).

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2.5 Meteorological sensors and data logger

A suite of meteorological sensors consisting of a wind monitor (RM Young Model 05103), a humidity and temperature probe (Vaisala HMP45C), and a barometer (Vaisala PTB110) were housed on the O-buoy mast. A GPS (Garmin 16HVS) was also included to determine the position of the O-buoy. For the testing phase, the ice flow did not rotate, so the orientation of the buoy was static. However, for future deployment, a solid-state compass (Ocean Server OS 5000-US) has been integrated. A Campbell data logger (CR-1000) performed five minute averages on these data, and reported the most recent five minute average to the supervisory computer on an hourly basis.

2.6 Control systems

2.6.1 Supervisory computer

The Supervisory Computer (SC) was based on a Technologic Systems TS-7260 single board computer (SBC) and additional peripheral components. The SBC had two character-buffered, flow-controlled (16C550 type) serial communication ports, two USB 2.0 ports, a 10/100 Mbps Ethernet port, an integral SPI interface, 64 MB of RAM memory, 128 MB of Flash memory, an SD card socket, a battery backed-up real time clock, a 16 bit PC-104 expansion interface, an on-board temperature sensor and user selectable capability for RS-232 or RS485/422 compatibility on its COM 2 serial port. Each of the above capabilities was used to operate the buoy. Its ARM9 processor was pre-specified to operate at a clock rate of 200 MHz. The software operating system was the Debian Linux distribution as adapted for the TS-7260 SBC. The SBC was fitted with an additional four-port 16C550 type serial expansion card and a second Ethernet port (these features were connected via a PC-104 expansion interface). The SBC and its options were specified at the time of purchase for operation to -40°C . Typical power consumption on the buoy was observed to be approximately 2.3 W while running a de-

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manding computation benchmark with all ports operating at high data rates. This value may be regarded as the high end limit for SC power consumption.

Upon start-up the computer performed an initial boot from its Flash memory in the YAFFS internal file format followed by a “pivot boot” to the full operating system in EXT file format. The full Linux operating system was contained on a 512 MB solid state disk drive. A 16 GB solid-state USB “memory stick” was installed to provide an on-board archive of all data that were obtained from every instrument and sensor. In the event of a possible failure in the satellite communications system, data records from the buoy might be available should the buoy be recovered.

The SC was operated at all times; therefore it represents the baseline power demand of the O-Buoy system. This device was the only subsystem on the buoy that was normally kept in continuous operation.

2.6.2 Power sources/control

Power distribution, monitoring and control were done via a custom built circuit (Fig. 5) that was directly managed by the supervisory computer. Power input was from either or both of two possible sources: (A) A conventional lead-acid (LA) battery bank that was recharged from a solar cell array (ASE-50-ATF/17; 50 W max/panel×4 panels); or (B) A non-rechargeable lithium-ion (Li) battery bank. The solar cell array was composed of four solar panels (96.5 cm×45.2 cm) connected in series, and arranged so one panel faced in each direction (N,S,E,W; Fig. 6). The power circuit was based on a negative common design. The input circuit was equipped with a separate current steering diode in series with each positive connection to the LA bank and the Li bank, respectively. Additionally, an electronic switch was located “upstream” of the Li steering diode to allow the Li bank to be positively turned off by the SC under software control or explicit satellite derived command (Fig. 5). This single switch plus the two steering diodes creates three possible modes of power input to the buoy system:

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1. High solar elevation – The Li bank is switched off by software command because the solar cells are sufficient to operate the buoy system and provide sufficient power to fully charge the LA batteries. The voltage of the LA bank is monitored by the SC through an external 12-bit digitizer and multiplexer. As long as the LA voltage cycles between 14.5 V and 11.5 V the LA pack will be the source of power. This voltage range is determined by a pulse width modulated controller (Morningstar SS-10) that arbitrates between the unregulated solar array and the LA battery bank.

2. Solar elevation near or below the horizon – The solar cells may not be capable of maintaining the charge on the LA batteries (LA voltage level falls to ≤ 11.5 V). At this control point, the SC software turns on the Li bank. The Li batteries will exhibit an open circuit voltage above this level (> 11.5 V) until they are almost completely exhausted. Our calculations indicate that the Li battery bank will last at least one winter for normal operation of the buoy.

3. Intermediate solar elevation – The solar array is able to provide significant power to the buoy via scattering from the sky and ice surfaces at intermediate solar angle. Both battery banks are on line where passive diode steering alone apportions the current load. This mode was tested during the deployment in Elson Lagoon from February–May 2009. Despite the sun being not much above the horizon, the solar array provided sufficient power to operate the buoy from the LA bank charge alone on a 24 h basis by mid-March 2009.

Power distribution was managed by the SC via the power control circuit. Identical electronic switches supplied the unregulated DC power to all scientific devices, meteorological instruments and a pre-packaged satellite transceiver system. The power control circuit provided regulated voltage at +3.3 V for its own analog and digital circuits. This circuit utilized a set of voltage and current sensing amplifiers which were read via a multi-input multiplexer via the SPI port on the SBC. There were sufficient parameters available that the system software could report the distributed voltage level

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and all significant current loads in the system.

2.6.3 Scheduling

Based on a predetermined scientific observation schedule (which was based, in turn, on the solar elevation angle), individual instruments were sequenced into operation as needed. The objective was to provide a maximum number of scientific observations achievable with the power available (maximum of 16 W). The power consumption of each instrument and the SC is shown in Table 1. The satellite transceiver is excluded due to its great variability. Scientific functions were scheduled for operation and data acquisition between satellite service intervals (once every 24 h for a 2 h interval). Typically data from the buoy were uploaded to the satellite during this time. Revised programs and schedules could also be downloaded to the O-buoy during an open satellite window. The results of these changes were seen at the next satellite window for the buoy 24 h later.

A more power efficient version of the SC system is now being developed. It is practical to reduce the power consumption of this part of the buoy system by a factor of two. This improvement may extend the unattended lifetime of the buoy to two years of operation in high latitude polar environments.

2.7 Communications

Satellite communication was done through an Iridium phone (NAL Research AL3A-SA). All communication to and from the buoy was achieved through this transceiver and was controlled by the SC. During transmission, the files (typically totaling >200KB) were aggregated and put into 10 KB chunks to limit the amount of data required to be resent should the transmitting signal be temporarily interrupted. Moreover, the data were routinely backed-up on the SC in case all transmission capabilities were lost. The data were transferred from the SC every day at 18:00 UTC, and were sent to a repository at SRI International (<http://transport.sri.com/obuoy/monitor>) where it could

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be accessed by the various groups involved via an Internet connection.

3 Deployment

The O-buoy was field tested in Elson Lagoon at Barrow, Alaska from 3 February to 18 May 2009. The O-buoy was transported from Barrow to the deployment site by a sled pulled by snow-machine. A two meter long, half meter wide, slit was cut in the sea-ice (≈ 1 m thick) to allow the O-buoy to be slid off the sled horizontally, and allow the bottom to be lowered into the slit, thus positioning the O-buoy in a fully upright configuration (Fig. 6; http://www.youtube.com/watch?v=2ijCZ_arhzE for video).

4 Results and conclusions

The data obtained during this field test can be found at <http://transport.sri.com/obuoy/monitor>. As an example of the quality of data obtained from the O-buoy we show a time series of O_3 and CO_2 mole fractions, and BrO slant column densities for the period 5–21 March 2009 in Fig. 7. The top panel contains the O-buoy ozone data, as well as ozone data from the NOAA ESRL laboratory in Barrow, AK (Oltmans, S. J., personal communication, 21 May 2009), highlighting the similarity between the two measurements' temporal patterns (average difference of 0.9 ppb). While the data agree well, it is not necessarily the case that they should, depending on the spatial heterogeneity of the ozone depletion and BrO chemistry, the elucidation of which is an objective of the O-buoy effort. The data in Fig. 7 were chosen to show two ODEs on the days of 7 March, and 14–16 March. In the lower panel of Fig. 7 we show the CO_2 data from the O-buoy, along with CO_2 data from the NOAA ESRL lab in Barrow. As shown, the data for these dates are consistent with the expected mole fractions for winter northern hemisphere, and agree well. Additionally, meteorological data, including the temperature near the bottom of the buoy (steady at approximately $-2.5^\circ C$), are presented

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(Fig. 8) during the time from 5–21 March 2009. However, we note that the wind speed measurement may be in error, as our recorded wind speeds are significantly different from those measured at the ESRL site at low wind speeds. This is most likely due to icing on the wind-bird's propeller.

From the data collected it can be seen that the O-buoy system is fully operational and capable of functioning for extended periods of time in the harsh Arctic environment. We present these data as a proof of concept that such measurements are achievable over long periods, thus providing invaluable information regarding chemistry that occurs in this region.

5 Future work

This buoy will be re-deployed in the fall of 2009 in multi-year sea ice in the Beaufort Sea. It will be collocated with buoys measuring the ice mass balance and the physical properties of the upper ocean creating an autonomous observing station. Given the success of the O-buoy, additional units will be constructed and deployed throughout the Arctic Ocean to provide a better understanding of where and how chemistry in the Arctic is occurring, and to further study and observe any future variations in Arctic atmospheric chemical composition and meteorological parameters. Data from these buoys could be used to validate satellite measurements, and to improve their interpretation. The MAX-DOAS instrument is selectively sensitive to tropospheric chemical species (whereas satellites measure total column abundances). By making a comparison between long term O₃ and BrO measurements on the buoy we will learn more about their relationship in the troposphere, with the opportunity to compare these data with satellite measurements to improve their inversions.

Supplementary information for the O-buoy design:

<http://www.atmos-meas-tech-discuss.net/2/2087/2009/amtd-2-2087-2009-supplement.pdf>

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Table 1. Monthly energy consumption (Wh) for each instrument/component of the O-buoy. Each monthly value accounts for each instrument's power draw and duty cycle in normal deployment mode.

Component	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual Wh	Percent power
DOAS	0	373	535	674	535	546	546	482	578	450	0	0	4720	14%
Ozone	75	686	1082	1082	1345	247	247	247	445	247	75	75	5853	18%
CO ₂	97	97	97	97	97	97	97	97	97	97	97	97	1164	3%
Supervisory Computer	1684	1684	1684	1684	1684	1684	1684	1684	1684	1684	1684	1684	20203	61%
GPS	33	33	33	33	33	33	33	33	33	33	33	33	395	1%
Iridium	39	74	100	127	100	102	102	89	108	83	39	39	1001	3%
TOTAL	1928	2948	3530	3696	3794	2708	2708	2632	2944	2593	1927	1927	33336	100%

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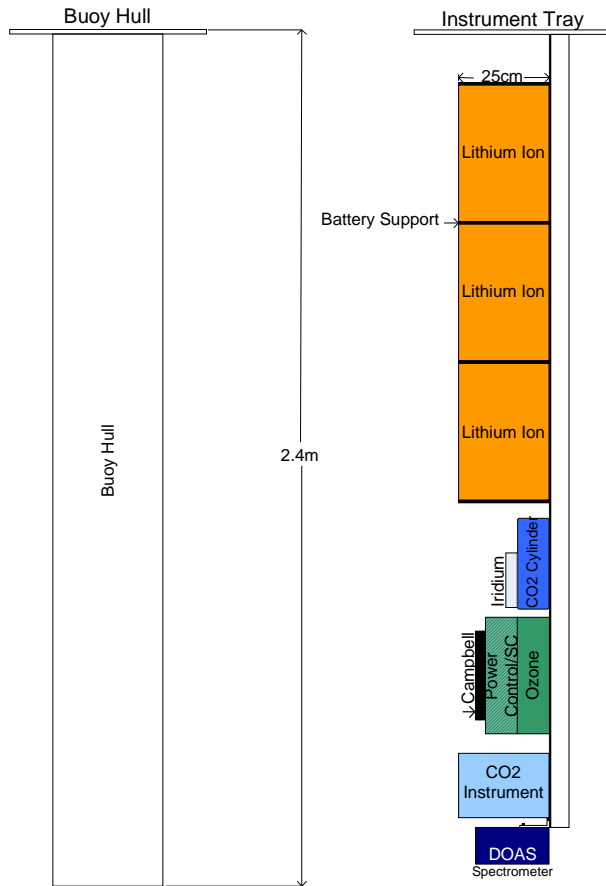



Fig. 1. Schematic drawing of the O-buoy hull and instrumentation placement on the instrument panel.

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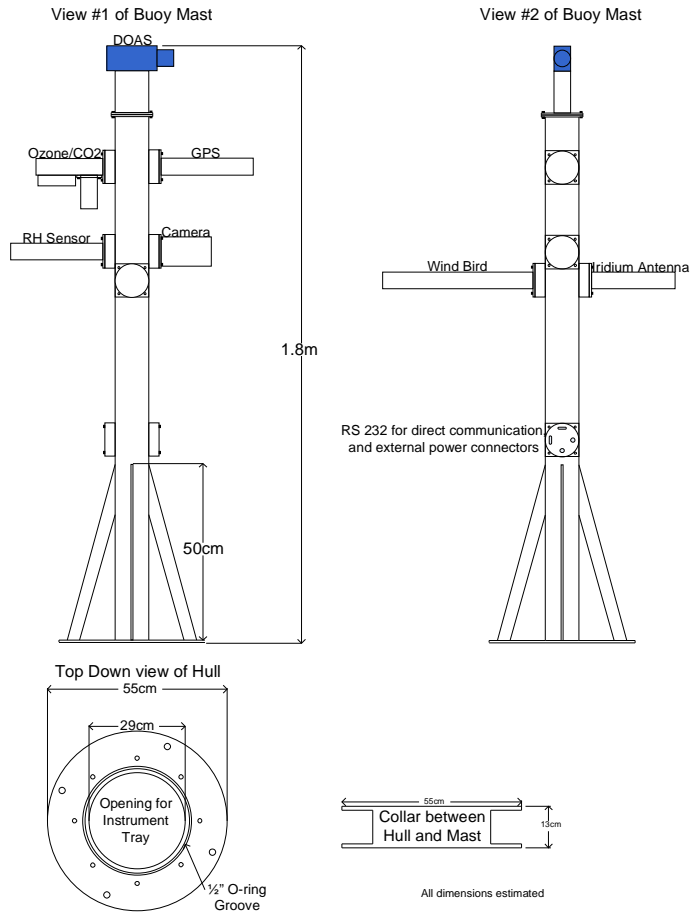


Fig. 2. A schematic representation of the O-buoy's mast and hull-to-mast connecting collar. View 2 is a rotation of view 1 about the y-axis by 90° to allow visualization of all instrument/inlet mounts on the mast.

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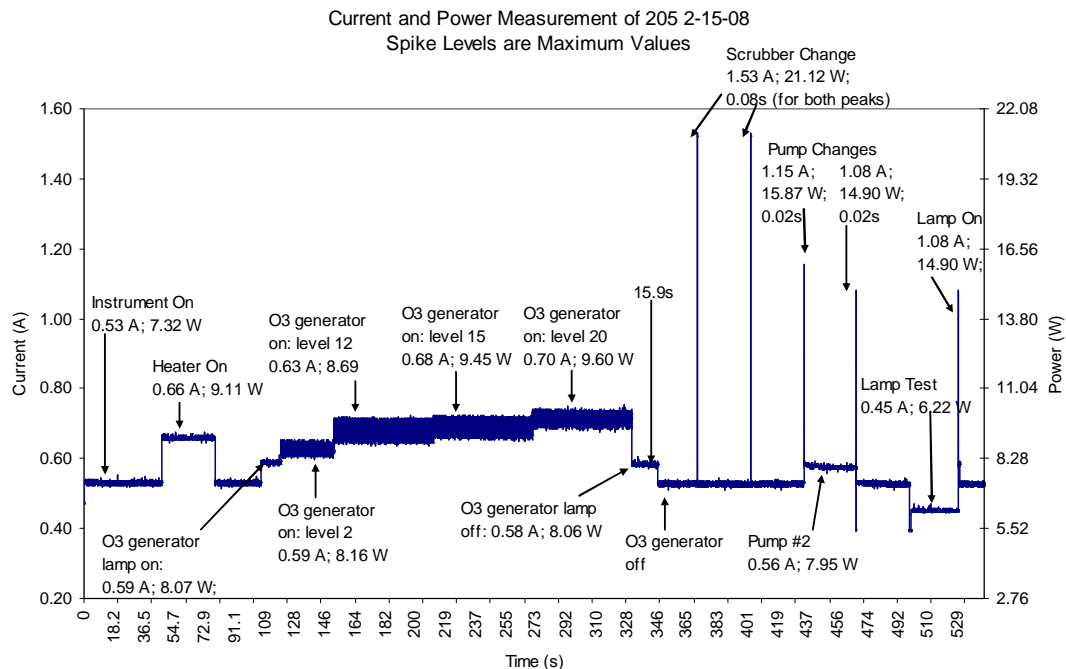


Fig. 3. Power plot of the ozone instrument in its various states of operation. In its baseline operation state the instrument draws approximately 7.3 W. Such a power measurement was done for all instruments on the O-buoy.

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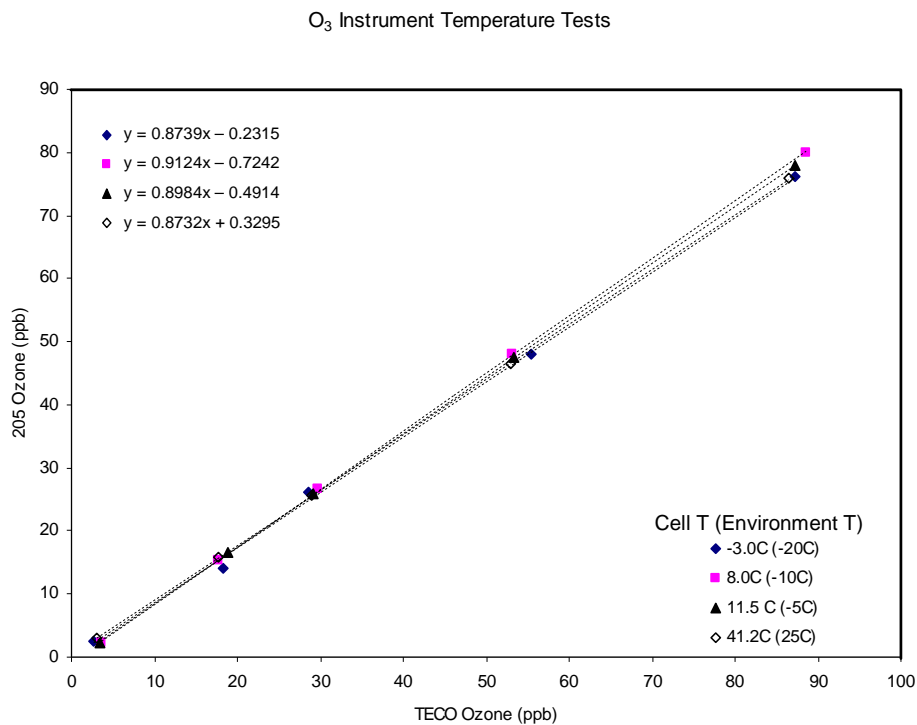
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**Fig. 4.** Temperature dependent calibration of the ozone instrument.[Title Page](#)[Abstract](#)[Introduction](#)[Conclusions](#)[References](#)[Tables](#)[Figures](#)[◀](#)[▶](#)[◀](#)[▶](#)[Back](#)[Close](#)[Full Screen / Esc](#)[Printer-friendly Version](#)[Interactive Discussion](#)

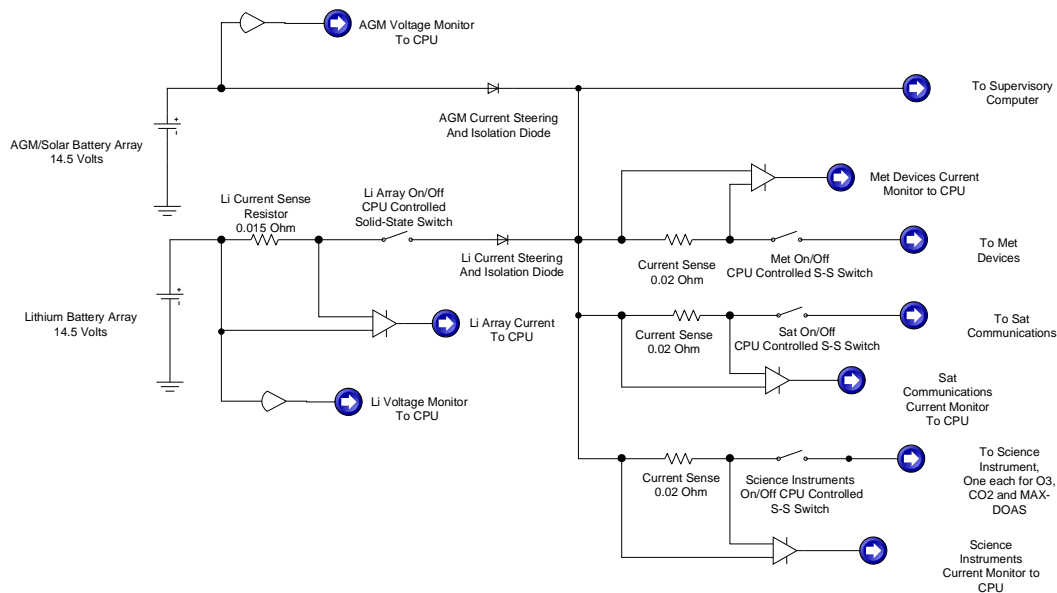


Fig. 5. Schematic representation of the power control board used on the buoy. For a full diagram see supplementary material.

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Fig. 6. Photograph of the O-buoy, solar panel array, and lead-acid battery box as deployed during the test phase. During future deployments the solar panels and lead acid packs will be part of the main O-buoy.

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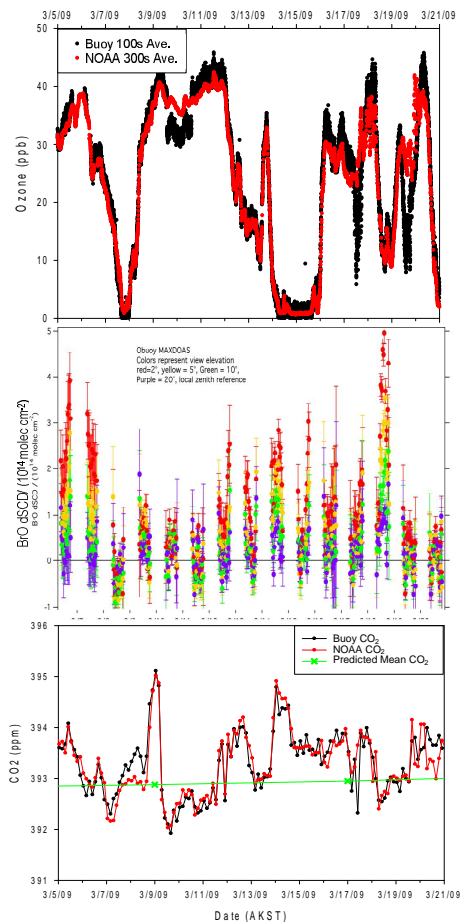


Fig. 7. Data plots from the three major instruments on the O-buoy (O_3 , BrO, and CO_2) during two ozone depletion events from 5 March through 21 March.

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Meteorological Sensor Data

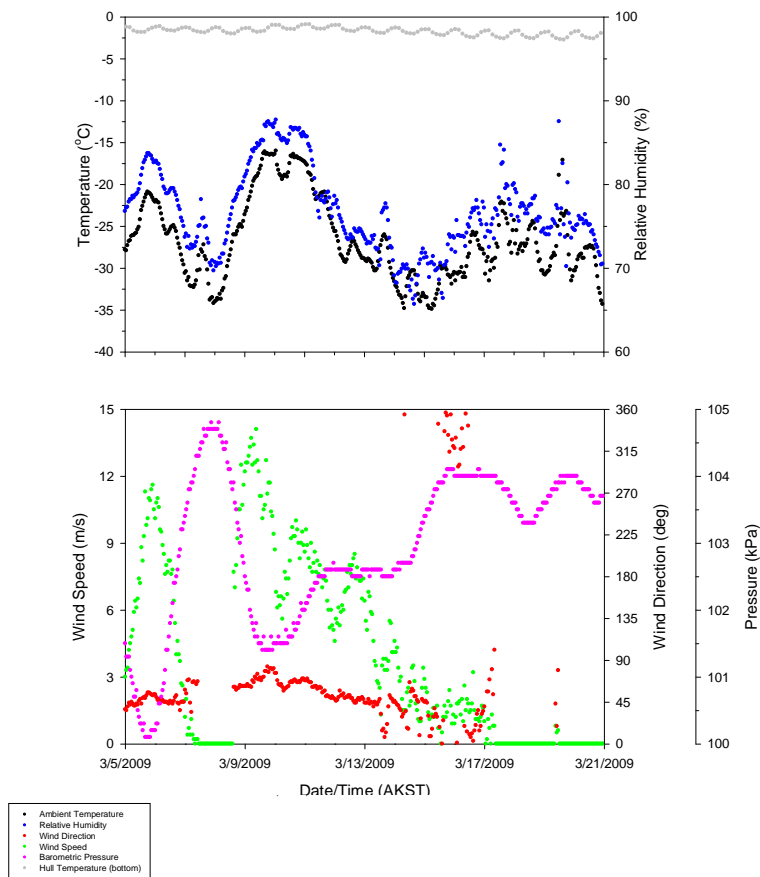


Fig. 8. Plot of the meteorological data acquired on the O-buoy during the two ozone depletion events in Fig. 7. Compass heading was not plotted as the O-buoy was in non-moving ice.

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