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MAX-DOAS
instrument**

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A low power automated MAX-DOAS instrument for the Arctic and other remote unmanned locations

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Received: 27 August 2009 – Accepted: 12 September 2009 – Published: 2 October 2009

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Published by Copernicus Publications on behalf of the European Geosciences Union.

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Abstract

Multiple Axis Differential Optical Absorption Spectrometer (MAX-DOAS) systems are inherently very simple instruments, which have been shown to provide extremely useful information about a wide variety of environmental parameters. In order to exploit the potential of the technique we have developed a new field-deployable MAX-DOAS system that is automated and uses little power (<3 W). This new instrument utilizes a fully enclosed scan head that protects all moving parts and optics from harsh environments. Instrument diagnostics, such as tilt monitoring and frost accumulation detection and removal, are integrated into the main data acquisition program, which then acts to remedy problems that were discovered. This full automation and data quality checking make this instrument ideal for long-term deployment at remote, unmanned locations around the world, such as in polar regions or in the monitoring of trace gas emissions from volcanoes. This instrument was recently integrated into an ice-tethered autonomous buoy and tested in Elson Lagoon, near Barrow, Alaska to monitor halogen chemistry in the Arctic. During this investigation differential slant column densities (dSCDs) of BrO up to 6×10^{14} molecules/cm² were observed. Typical spectral fit residual RMS optical densities were less than 6×10^{-4} for solar zenith angles (SZA) < 80° and a 6-min integration time. Here we describe the design concepts and performance of this new MAX-DOAS instrument through detailed analyses of spectral quality, power usage, possible instrument response biases, and typical instrument operations.

1 Introduction

First used by Dobson and Harrison (1926) to measure atmospheric ozone, the technique of passive absorption spectroscopy has been in continual development for almost a century. Today, the advent of multi-wavelength array detectors, miniaturized electronics, and fiber optics has given rise to modern passive differential optical absorption spectroscopy (DOAS) methods in which UV/Vis (and/or IR) solar spectra are

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used to quantify accurately numerous chemical absorbers simultaneously (Platt, 1994). Using DOAS techniques, O_3 , SO_2 , HCHO, HONO, H_2O , NO_2 , NO_3 , IO, OClO, BrO, O_4 and $(CHO)_2$ can be detected in the UV/Vis region. In the IR region many other species, such as CO_2 , CH_4 , OIO, H_2O , and solid and liquid particles can also be observed. Additionally, cloud and aerosol light extinction coefficients can be derived from observations of the oxygen collisional dimer, $(O_2)_2$, also known as O_4 , whose abundance is primarily dependent on atmospheric pressure (Frieß et al., 2006). The DOAS technique usually measures the difference between two spectra, a measurement and a reference, which removes spectral contributions that are common between these two spectra in the case of solar spectra this is the Fraunhofer structure. The term “differential” refers to the fact that the spectral fitting exploits high-frequency variations that occur in molecular absorption spectra (typically vibronic bands) but are not present in aerosol scattering or other extinction processes that vary slowly with wavelength (for details see Platt, 1994; Platt and Stutz, 2008). This process combined with the absolute nature of the Beer–Lambert law allows for the calculation of slant column densities relative to the reference without calibration. It is important to note the distinction between passive DOAS, where scattered sunlight is used as the light source, and active DOAS, where an artificial light source is used. The MAX-DOAS method, in which the passive DOAS technique is applied using multiple view elevations (known as axes), was first employed by Hönninger and Platt (2002) at Alert, Canada. The near-horizon view geometries used in MAX-DOAS greatly enhance the sensitivity to boundary layer species, contrasted to satellite or zenith-sky DOAS techniques, which are mostly sensitive to total column abundances (Hönninger et al., 2004). The multiple view axes of MAX-DOAS also enable trace gas vertical profiles to be derived (Hönninger et al., 2004).

Low power consumption, inherent calibration, and the potential to derive vertical profiles are significant advantages of the MAX-DOAS technique; however, there are two main disadvantages to the passive DOAS technique in general. First, it can only operate during daytime or twilight hours as it requires scattered sunlight. Active DOAS

techniques, where a laser (e.g. Mount, 1992), arc lamp (e.g. Platt, 1994; Platt and Stutz, 2008), or light emitting diode (LED) (Kern et al., 2006) is used as the illumination source, eliminates this problem, but often requires high power, and is therefore more difficult to employ at remote locations. The second disadvantage of passive DOAS is that obtaining chemically relevant concentration or mixing ratio values from the raw measurements is a mathematically intensive process, which lacks accepted standard procedures and has complex error estimation (e.g. Wagner et al., 2004; Frieß et al., 2006). However, satellite remote sensing techniques apply similar spectral fitting and radiative transfer methods for their analysis, so the mathematical complexity of MAX-DOAS is similar to and not worse than other remote-sensing techniques. In fact, because of similarities between ground-based passive DOAS and satellite techniques, MAX-DOAS instruments represent an important resource that can validate and improve satellite measurements.

The DOAS technique has been successfully adapted to ground, air, and satellite based platforms, allowing for some of the most remote locations on Earth to be studied. A prime example is detection of bromine monoxide in the polar regions. Every spring-time in polar regions, reactive halogen species, including BrO, are photochemically sourced to the atmosphere from snow and ice surfaces (Barrie et al., 1988; McConnell et al., 1992; Fan and Jacob, 1992; Tang et al., 1996; Simpson et al., 2007a). These reactive halogens are an essential reactant in tropospheric ozone depletion events (ODEs) where surface ozone levels are periodically depleted to near zero, thereby significantly altering the oxidation pathways of the atmosphere (von Glasow et al., 2004; Hönninger and Platt, 2002; Jacobi et al., 2006; Simpson et al., 2007a). Additionally, reactive halogens are believed to be the primary oxidant of gaseous elemental mercury in polar regions, leading to the deposition of reactive mercury species into the snowpack (Schroeder et al., 1998; Lindberg et al., 2002). Much of our current knowledge about tropospheric BrO concentrations and spatial distribution in the polar regions comes from DOAS observations (e.g. Tuckermann et al., 1997; Hönninger and Platt, 2002; Frieß et al., 2001; Simpson et al., 2007b). Satellites such as GOME, OMI, and

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SCHIAMACHY have for years provided pan-Arctic/Antarctic vertical column densities of BrO from space (Richter et al., 1998; Wagner and Platt, 1998; Wagner et al., 2001; Hollwedel et al., 2004) and passive ground based DOAS instruments have been deployed at numerous Arctic and Antarctic locations such as Alert, Canada, Spitzbergen, Svalbard and Barrow, Alaska (Kreher et al., 1997; Wittrock et al., 2000; Frieß et al., 2001; Hönninger and Platt, 2002; Simpson et al. 2007b).

As successful as these satellite and ground based DOAS instruments have been in measuring BrO, they still possess inherent limitations. Satellites are limited by their spatial and temporal resolution, lack stratospheric and tropospheric vertical profile information, and often do not account for cloud interferences. Also, satellite methods require ground truth observations for validation. Ground-based MAX-DOAS instruments can easily differentiate whether a gas is in the stratosphere or in the boundary-layer and can account for cloud interferences, however, many MAX-DOAS instruments use tens of watts of power and require maintenance limiting their possible deployment sites to coastal places with infrastructure, which leaves the vast majority of the polar regions unexplored. Icebreakers have been successfully used as a mobile observation platform (Wagner et al., 2007), however these ships are limited by ice conditions and are not always readily available.

In the Arctic and at many other locations around the Earth, there is a great need for automated, low power instrumentation, which is capable of continuous long-term atmospheric monitoring. A number of miniaturized ground-based passive DOAS instruments have been recently developed. These instruments are smaller, use less power, and easier to use than previous instruments, however they still lack sufficient automation for long-term remote deployment. The Flyspec and Mini-DOAS instruments have been developed to quantify SO₂ emissions from volcanoes (Horton et al., 2006; Galle et al., 2002) and are a significant improvement from the now outdated COSPEC instrument (Moffat and Millan, 1971). However, the view telescope on some of these instruments must be manually moved to each different view axis, requiring a person to always be present during operation. Other DOAS instruments, such as the Mini-MAX

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(Hönninger et al., 2004), use a stepper motor to automate changes in view direction, however, there is still a lack of automated instrumental quality checks to ensure proper functioning during remote long-term deployment. The Mini-MAX also has a higher than desirable total power consumption due to use of Peltier-effect cooling to stabilize the spectrometer temperature.

To increase data collection of trace gases in the Arctic, and at other remote locations such as volcanoes, we have developed a new MAX-DOAS system that is low-power (<3 W), automated, and field deployable. Design features include: a separate, fully enclosed weatherproof optical scan head, frost detection and removal capability on the view window, integrated tilt meter to ensure correct view elevation angle, passively temperature-stabilized spectrometer, continually updated dark current and offset corrections to the spectrometer, fully automated data acquisition software, and compatibility with two-way satellite and ethernet communication devices.

2 Instrumental

A schematic of the overall instrument setup is shown in Fig. 1. There are two sub-systems, the scan head, which receives the scattered sunlight, and the spectrometer/computer unit, which runs the system and detects and stores the spectral data. The two sub-systems are linked by a UV/Vis fused silica fiber optic cable and a multi-conductor electronic cable.

2.1 Scan head sub-system

The scan head sub-system, shown in Fig. 2, is contained in a sealed aluminum housing with a cylindrical quartz window through which scattered sunlight is viewed. The housing is made airtight by sealing all unions with O-rings and using airtight glands and connectors for the electronic cable and fiber optic cable. This enclosed design protects internal optics and moving parts from physical obstruction or weathering and

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is important for successful long-term operation in the Arctic. Scattered sunlight is directed through the system using a set of two right angle fused silica prisms (Optics For Research, ADU-15 mm), where the outer prism is rotated about the axis between the two in order to obtain light from different view elevations. This design allows a scanning range of approximately 220° , from slightly below the horizon, up and over the zenith, and through the horizon on the opposite side.

Between the two prisms is a Schott BG3 bandpass optical filter (UV-VIS bandpass approximately 315–445 nm). The filter excludes light of wavelengths that are not in the region of interest and reduces the possibility for light to be scattered within the spectrometer, which could contribute to instrumental artifacts. From the second, i.e. non-rotating prism, the light passes through an f -stop ($f/4$) and a fused silica lens (Thorlabs, LA4936-UV, 30 mm focal length) that focuses the light into the entrance of the fiber optic cable. The fiber optic cable (Ocean Optics) is a three-fiber armored bundle with a triangular configuration on the scan head end, and a linear slit arrangement for the spectrometer entrance end. Each of the three fibers is $200\ \mu\text{m}$ in diameter and 0.22 numerical aperture.

2.2 Determination of view elevation angle

A geared stepper motor (Oriental Motors, PK223PA-SG36, 0.05° per step) rotates the movable prism to achieve different view elevation angles. Two limit switches are used to calibrate the prism orientation with respect to the scan head. The algorithm for determining the optical position takes into account the $\sim 1^\circ$ freeplay in the gear mechanism. To determine the telescope orientation with respect to the horizon, a tilt meter (Smart-Tool Technologies ISU-S, $\pm 0.1^\circ$ accuracy and 0.01° reported resolution) is mounted in the scan head and is used to convert the scan head based orientation into a true horizon oriented coordinate system.

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2.3 Frost detection and removal

Snow or frost buildup on the optical input window can be particularly problematic in polar regions. For this reason, this new MAX-DOAS system is equipped with a frost detection and window heating system, which ensures a clear instrumental view while conserving power by not heating the window when it is not needed. A near-UV LED (~395 nm) is used to illuminate the view window at an oblique angle, and the telescope/spectrometer receives this light when the window is frosted. The oblique illumination nearly eliminates scattering of LED light into the telescope when the window is clear. Daylight signals are removed by subtracting the intensity with the LED off from the LED on scattered light signal as shown in Fig. 3. The wavelength chosen for observation (395 nm) is in a large Fraunhofer dip to reduce the effect of ambient skylight while being near the emission maximum of the LED. Frost counts are measured and logged each time the view prism is rotated to a new view elevation angle.

When the frost signal exceeds a pre-set threshold, two small resistive heating elements (39 Ω total, 3.75 W at 12 V, Minco, HK5205R76.5L 12A) are turned on. These heaters are glued to the inside of the quartz window (see Fig. 1) using thermally conductive epoxy. In addition to the heaters, the inside of the quartz cylinder is painted black everywhere except at the viewing directions so that passive solar heating is maximized.

2.4 Dark current and offset corrections to the spectrometer

Each recorded spectrum is the sum of the measured skylight intensity, an electronic offset applied by the spectrometer, and time-accumulated thermal or dark current. Therefore, offset and dark current spectra must be subtracted from all measurement spectra to give signals directly proportional to light intensity. Since the offset and dark current can vary with time, new correction spectra must be periodically acquired. Two pieces of black, light absorbing photography paper cover the instrument window at two unused view elevation angles, approximately 30° from the zenith. To obtain new dark

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current and offset spectra, the view prism is oriented at the black paper and spectra are recorded with short and long exposure times. While scattered sunlight is not completely eliminated by the dark paper, it is reduced to the extent that dark current and offset correction spectra can be extracted.

5 2.5 Spectrometer/computer sub-system

The second sub-system consists of a single-board computer (SBC), a spectrometer, a stepper motor driver circuit board, and a signal routing interface circuit board as pictured in Fig. 4. The spectrometer is an Ocean Optics HR2000. The spectral resolution is 0.65 nm full width at half maximum, as determined by observation of the 334 nm mercury atomic emission line. This spectrometer has a wavelength range of 318–455 nm, which allows for detection of chemical species with absorption features in the UV wavelengths as well as the violet and blue regions of the visible spectrum, including O₃, HCHO, HONO, H₂O, NO₂, IO, O₄ and (CHO)₂. Shifting this spectral window to the UV would allow the instrument to detect SO₂ and ClO. The HR2000 spectrometer is extremely low power (about 0.5 W), compared to other models with similar specifications, and is also relatively inexpensive (~\$3400 USD).

Since the detector's wavelength-to-pixel relationship is sensitive to changes in temperature, the spectrometer is thermally contacted to the bottom of the aluminum housing. The aluminum housing can subsequently be thermally regulated by placing it in good thermal contact with a large heat sink, such as below the active layer of soil or in a large body of water. Alternatively, if power is locally available it can be temperature controlled by an electric heater and thermostat device.

The single-board computer is a Technologic Systems TS-7260 running linux, which is connected to the spectrometer using USB and to other peripherals using RS-232 ports and digital I/O. The computer is networked using Ethernet. The stepper motor driver (BC2D15-RS232, Peter Norberg Consulting) fires the motor windings at a specified speed and direction, and also receives the limit switch signals. The single-board computer controls the stepper motor driver using a serial (RS-232) port. An interface

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circuit board contains three solid-state relays (SSRs) to control power to the window heater, frost sensor LED, and tilt meter. Digital I/O on the computer control these SSRs to conserve power by turning the devices off when not needed. The tilt meter is turned on only when needed and reports the tilt angle over a serial (RS-232) port on the single-board computer.

3 Instrument operations

This instrument operates remotely without any maintenance. The main data acquisition program, which is executed on boot of the SBC, automatically records scattered light spectra at a series of elevation angles while simultaneously monitoring and correcting for varying instrument and environmental conditions.

3.1 Scan pattern

The instrument repetitively scans the telescope between a series of elevation angles (typically 2, 5, 10, 20, and 90° elevation from the horizon). An automatic algorithm optimizes the exposure time (typically 0.1–0.4 s for sunny conditions), and spectra are coadded for a short integration interval (typically 60–90 s) before advancing to the next elevation angle in the sequence. The elevation angle sequence is then repeated until the recording interval (typically about 30 min) is exceeded. The coadded spectra at each elevation angle, along with ancillary data, are then written into a data record. This record represents the inherent time resolution in this mode of operation and is set based upon a compromise between time resolution and file transfer size. The scan pattern is repeated multiple times in a single record so that short-term variability in clouds or other optical properties are averaged over. Dark and offset spectra are observed at the end of the scan pattern by rotating the telescope to the elevation of the dark blocker.

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3.2 Communications and data retrieval

At high-infrastructure locations, the SBC can report the data over the internet using automatic data transfers to a secure ftp site, and the instrument can be monitored and its operations modified over the internet. For more remote sites, the SBC can be connected to an iridium satellite transmitter/receiver, which is also capable of automatic data transfers and two-way communications (Knepp et al., 2009). Protocols for reprogramming the SBC have been established and we have successfully uploaded new versions of the operational software and parameters remotely.

3.3 Instrument function monitoring

Each time that the stepper motor is returned to a limit switch, the step angle is recorded as a check that the motor is not losing steps. The angle counter is then reset to the limit switch's position value. Under normal operating conditions the homing error is very low, with an RMS deviation of 0.015° over a 3 month operational period. In addition to using the tilt meter in the scan head to automatically adjust the telescope's position, the tilt meter's reading is recorded to verify proper operation of the sensor and identify if the instrument has been tilted (for example by shifting sea ice or disturbance by Polar Bears). The average frost signals at each elevation angle are also written into the data record.

4 Instrument performance

4.1 Light intensity at different view angles

To test the instrument's response at different view elevations, a fixed broadband light source (an unfiltered halogen lamp) was observed at a variety of positions between the two horizons. This was accomplished by manually rotating the entire scan head about its longitudinal axis, while rotating the view prism in the opposite direction by

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the stepper motor to observe transmitted light through a Lambertian diffuser (a back-illuminated teflon sheet). The teflon was mounted 50 cm from the scan head, and could be observed over an aperture of roughly 10° . Figure 5a shows the instrumental response as a function of scan head angle. Data points represent the average of six measured spectra at each angle and are shown for two distinct spectral ranges, 360–364 nm and 420–430 nm. Standard deviations of the intensities at each angle are less than one percent. Each angle showed similar average intensities, with the standard deviation of 1% between the angles. This observation indicates that the instrument has a uniform response to light intensity at all scan head view angles.

4.2 Polarization effects

Spectrometers generally have differing sensitivity to different polarization states of incoming light. Because scattered sunlight is polarized, it is necessary to understand the instrument's sensitivity to polarized light for accurate analysis of the MAX-DOAS signals. For this instrument we attempt to equalize the sensitivity to horizontal and vertical polarization by using the fiber optic cable to randomize the polarization. To test the polarization sensitivity, we modified the above procedure by adding a polarized sheet between the scan head and light source. At each scan head angle five spectra were recorded with the polarization filter oriented horizontally, and then five with the filter oriented vertically. Each horizontally filtered spectrum was subtracted from the average of all the vertically filtered spectra at the same scan head angle and divided by the average intensity of all (both horizontally and vertically filtered) spectra to give the percent residual polarization sensitivity. The converse method, subtracting the average of the horizontally filtered spectra from each vertically filtered spectrum and then dividing by average of all spectra, is used to calculate percent differences for the individual vertically filtered spectra. This procedure results in ten observations of the polarization sensitivity defined by $(V-H)/(V+H)/2$. Figure 5b and c shows average and standard deviations (1σ) of the residual polarization sensitivity, in percent. In Fig. 5b (360–364 nm) the observed small percent differences ($<\pm 3\%$) and the er-

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ror bars overlap zero indicating that the instrument has no polarization sensitivity in this wavelength region. At longer wavelengths, as shown in Fig. 5c (420–430 nm) the percent differences are consistently about 1% below zero and the error bars are small enough that they generally do not overlap zero. It is possible that the fiber optic cable is not long enough to scramble completely the polarized light at these wavelengths. However, this spectrometer bias to polarized light is around 1% and would not be expected have a large impact on spectral fitting results. Also, as noted below in Sect. 4.4 the spectral fitting window used for quantification of BrO is much closer to the 360–364 nm region shown in Fig. 5b.

4.3 Power budget

This instrument is designed for long-term automated data acquisition; therefore, it is essential to evaluate the power usage, so that sufficient power can be allocated to run the instrument for the duration of a projected campaign. The power consumption (at 12 V) and duty cycle of each individual component was measured in the laboratory and are listed in Table 1. The computer, stepper driver electronics, and spectrometer always draw current (duty cycle of 1) and establish a baseline instrument power consumption of 2.7 W. The other system components do not significantly contribute to the long-term power consumption due to the low duty cycle; however, they can cause large momentary spikes in the power consumption. For example, the stepper motor only moves for about 1% of the operational time, but when it does, it adds 1.3 W, bringing the total power consumption at that moment to 4.0 W. If both the window heater and the motor are simultaneously drawing current, the power consumption spikes up to the maximum power consumption, 7.7 W.

The duty cycle of the window heater is the biggest unknown in the power budget because the amount of heating required to keep the window free of frost is highly variable and depends on humidity, ambient temperature, wind, and amount of passive solar heating to the window. If frost is absent, the heater has a zero duty cycle and does not consume any power. If the window is frosted and it takes 2 h per day of heating to

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keep the window clear, then the duty cycle is 2 h/24 h (or 0.08), adding an average of 0.3 W to the average operational power consumption, bringing the total to 3.0 W. Snow buildup on the window takes longer to heat off than vapor deposited frost; however, wind and the curved shape of the quartz window usually prevent snow accumulation.

5 4.4 Spectral fitting

In the MAX-DOAS method, each measurement spectrum is referenced to a corresponding local (meaning at nearly the same time) zenith reference spectrum. The details of this fitting procedure are described by Donohoue et al. (2009). For BrO, the foundation of the spectral fitting procedure was the recommendations put forth in Aliwell et al. (2002), with some modification including the use of updated cross-section data and the extension of the fit window to 364 nm. These modifications improve our selectivity for BrO and allow more accurate O₄ measurements. In addition, since we use a local zenith spectrum as the reference the influence of stratospheric ozone is limited. Therefore, only one ozone cross-section is necessary to characterize the ozone, rather than the two ozone cross-section recommended by Aliwell et al. (2002). We performed an initial wavelength calibration using the emission lines of a mercury vapor lamp. This initial wavelength calibration is then refined by fitting the Fraunhofer dip features of a high-resolution solar spectrum for each local zenith spectrum. The wavelength-calibrated spectra are fit in the 346–364 nm window to molecular reference spectra using QDOAS spectral fitting software (<http://uv-vis.aeronomie.be/software/QDOAS/>). All molecular reference spectra are convoluted using an instrumental slit function determined from the 334 nm mercury emission line from a calibration spectrum that is recorded in the field at time of deployment. The QDOAS software calculates differential slant column densities (dSCD) as shown in Fig. 6. A third order polynomial and a first order offset spectrum (not shown) are also fit to the spectral data to account for slowly varying aerosol absorptions and instrumental effects, respectively.

This spectral fitting procedure was used to analyze data from Barrow, Alaska during Spring of 2009, when the instrument was tested on the O-buoy platform (Knepp

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et al., 2009). The maximum BrO dSCD observed during this time period was 6×10^{14} molecules/cm². Figure 7 shows an example of data for the day of March 18, 2009 AKST using the above spectral fitting procedure. On this day, the early hours of observations are affected by frost accumulation, as indicated on the middle panel.

5 When the frost signal is above the operational threshold, the plot is shaded grey. It is noticeable that when frost counts are high the dSCD values for all view elevation angles converge to near-zero values. This effect arises from the fact that frost scatters photons from all different directions into the telescope, making no difference in the spectra taken at nominally different elevation angles. After the frost is heated off the window, a pattern of higher dSCDs at lower elevation angles emerges, which indicates that BrO
10 is near the ground surface. During the middle of the day the BrO dSCD at low elevation reaches 5×10^{14} molecules/cm² at the 2° elevation angle, indicating significant halogen activation in the boundary layer. Analysis of the BrO dSCD as a function of view elevation angle utilizing a radiation-transfer model allows derivation of the vertical profile
15 of BrO, as described in Donohue et al. (2009). The average RMS fit error for spectra with SZAs less than $< 80^\circ$ is 5.4×10^{-4} , which is typical for this instrument and attests to the spectral data quality. These data are analyzed using local zenith reference spectra, giving sensitivity to boundary-layer absorbers. However, fitting the spectra with a single (typically a zenith spectrum at solar noon) reference spectrum provides a means to
20 quantify the stratospheric BrO vertical column abundance (e.g. see Aliwell et al., 2002 and Donohue et al., 2009).

5 Possible design modifications

Prospects for future instrument modification include making further power reductions, and exploring different scan head designs. While the instrument power consumption
25 is already quite low, it would be possible to further reduce power consumption of the stepper motor driver by using more efficient electrical components and by turning off power to the driver electronics when not in immediate use. Also, small computers

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with even lower power consumption may be available. The use of Seebeck elements could possibly help to power the instrument by exploiting an environmental temperature difference, for example warm sea water and cold arctic air. While the clinometer in the scan head housing is sufficient for measuring instrument tilt, it is more desirable to have a clinometer attached to the rotating prism mount itself to obtain a more direct measure of the view elevation angle. Another change to the scan head might be to reduce the size of the quartz viewing window, which would give similarly powered heaters a higher power density and facilitate frost removal. The scan head design could even be changed to eliminate the cylindrical window entirely, in which case the view prism tube would protrude through the front plate of the scan head and would be sealed with a rotary seal. This design would differ from the original intention of having no external moving parts; however, it would have the benefit of being able to face the view prism downward when not in use, to avoid snow or dirt accumulation. Testing would be required to determine the longevity and friction of the rotary seal, particularly at very low temperatures.

6 Discussion/conclusions

MAX-DOAS observations have the potential to contribute to our understanding of reactive trace gases through collaborative chemical process studies in which the relationships between multiple chemical compounds are explored and chemical mechanisms and models are tested and improved. Additionally MAX-DOAS can help validate and refine satellite observations so that our mechanistic understanding can be extrapolated to the global scale. The new features of this instrument expand the applicability of the MAX-DOAS method to include long-term data collection at remote unmanned locations. The low power demand allows the possibility to run the entire system using battery, solar, or wind power. The automated and self-correcting instrument checks ensure that all data is taken from the intended view direction and with a clear view path. Resulting spectra are of high quality and allow derivation of meaningful trace gas

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slant column densities and vertical profiles. The two-way communications allow for continuous monitoring and data retrieval, making real time data analysis a possibility. This instrument has recently been integrated into a chemical measurement ice tethered buoy. In the next few years these buoys will be distributed around the Arctic, providing year round trace gas data from remote sea ice locations. For more information on the O-buoy see Knepp et al. (2009).

While this instrument was originally developed for use in the polar regions, it is also very well suited to volcanic sites and other remote locations. Volcanoes have been shown to emit many chemically important species such as BrO and SO₂ (Bobrowski, 2003). However, the global contributions and effects of the reactive gases released by volcanoes are not accurately known. The logistical challenges of studying volcanic gases include lack of easy access, lack of power, settling of ash on instrumentation, and the ever-present danger of harmful out gassing or violent eruption. The automation, low power consumption, and two-way communications of this MAX-DOAS instrument make it well suited to volcano studies. Additionally, any ash or debris on the window would be detected by the frost detector and any movement of the instrument would be detected and accounted for by the tilt meter.

Acknowledgement. This work was supported by the National Science Foundation under grant (ARC-0612457). We thank the Barrow Arctic Science Consortium (BASC) for logistical support. We also thank our fellow collaborators in the o-buoy project (see Knepp et al., 2009), particularly T. Valentic, who greatly assisted in computer design and techniques for remote operations of this instrument. We also thank Z. Plovanic for assistance in programming the single-board computer. Plovanic's work was supported in part by a grant of HPC resources from the Arctic Region Supercomputing Center at the University of Alaska Fairbanks as part of the Department of Defense High Performance Computing Modernization Program.

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Table 1. The power budget of the MAX-DOAS instrument measured in the laboratory at 12 V DC. The weighted power is the product of the duty cycle and the power consumption of each component. The window heater is not included in the total power consumption because its duty cycle varies strongly with weather conditions.

Component	Current (A)	Power (W)	Duty cycle	Weighted Power (W)
Computer	0.11	1.26	1.00	1.26
Stepper motor Driver electronics	0.08	0.90	1.00	0.90
Spectrometer	0.05	0.54	1.00	0.54
Motor (moving)	0.11	1.32	0.01	0.01
Frost LED	0.03	0.36	0.01	<0.01
Window Heater	0.31	3.72	variable	variable
			Total power consumption:	2.71

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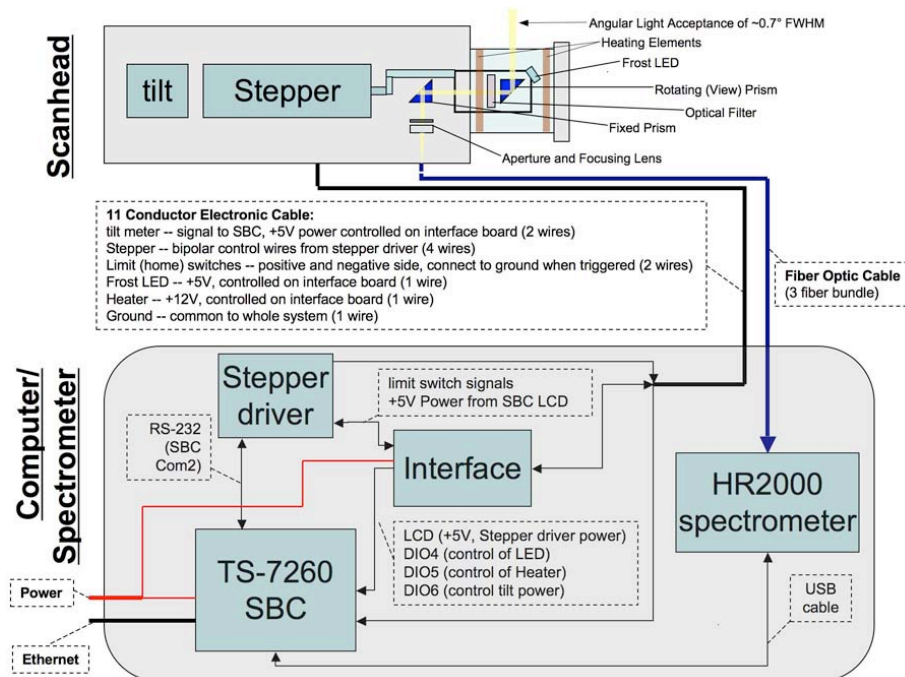


Fig. 1. Schematic of new MAX-DOAS system. The scan head (top) is connected to the computer/spectrometer (bottom) by a fiber optic cable and electronic cable.

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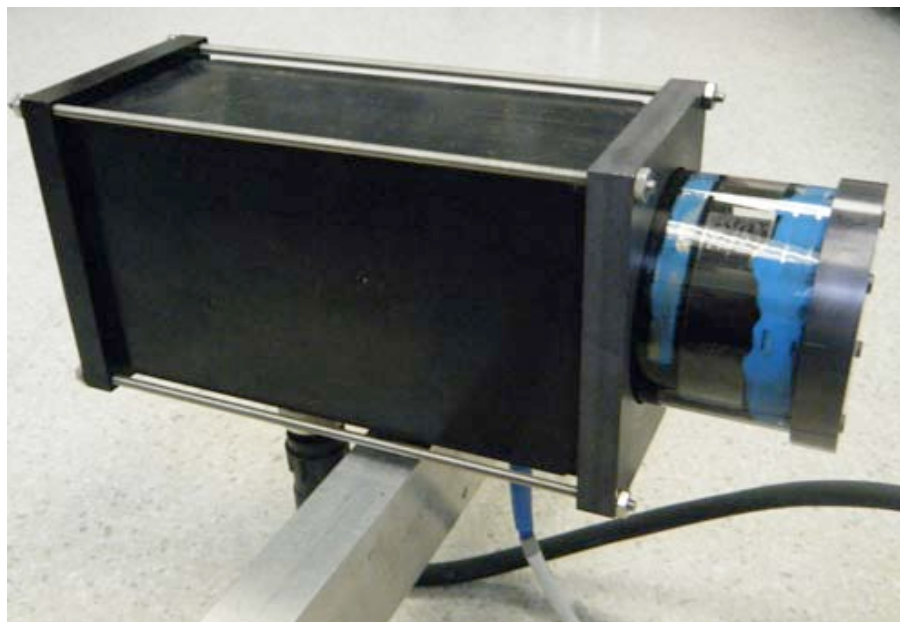


Fig. 2. A photograph of the scan head. The view window is the clear quartz region between two defroster heaters that appear blue due to the blue thermally conductive epoxy glue.

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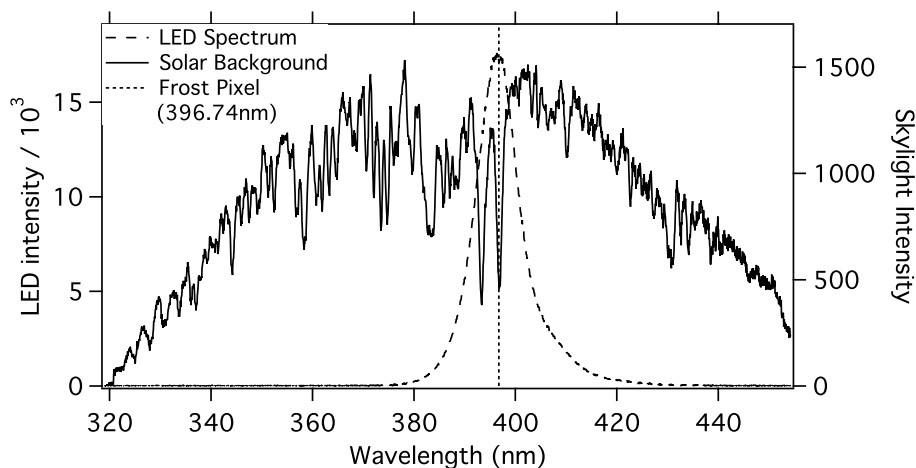


Fig. 3. Frost detection scheme example spectra. The dashed line shows the spectrum of the frost detection LED, while the solid line is an observed skylight spectrum. The frost detection wavelength, 396.7 nm, is chosen to be at the base of the Fraunhofer dip to minimize skylight interference in the frost measurement.

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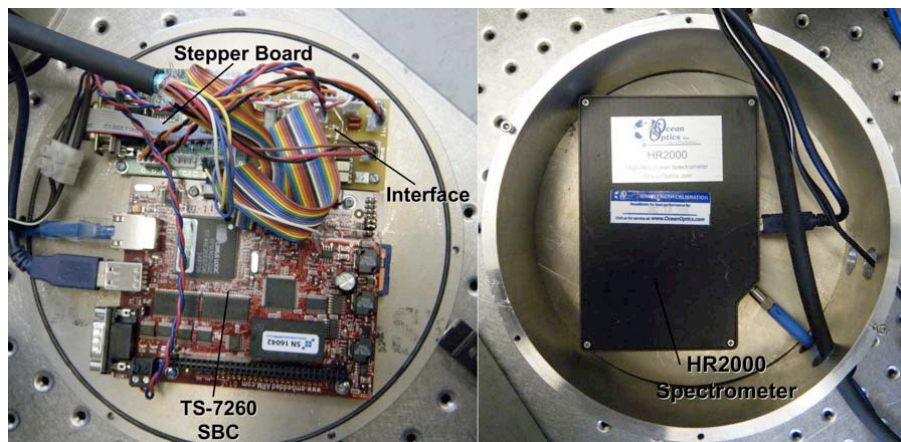


Fig. 4. The computer/spectrometer subsystem. In left panel is the top of the housing, where we have mounted the single-board computer (SBC), stepper motor driver, and interface circuit boards. The right panel shows the Ocean Optics HR2000 spectrometer thermally contacted to the aluminum housing base.

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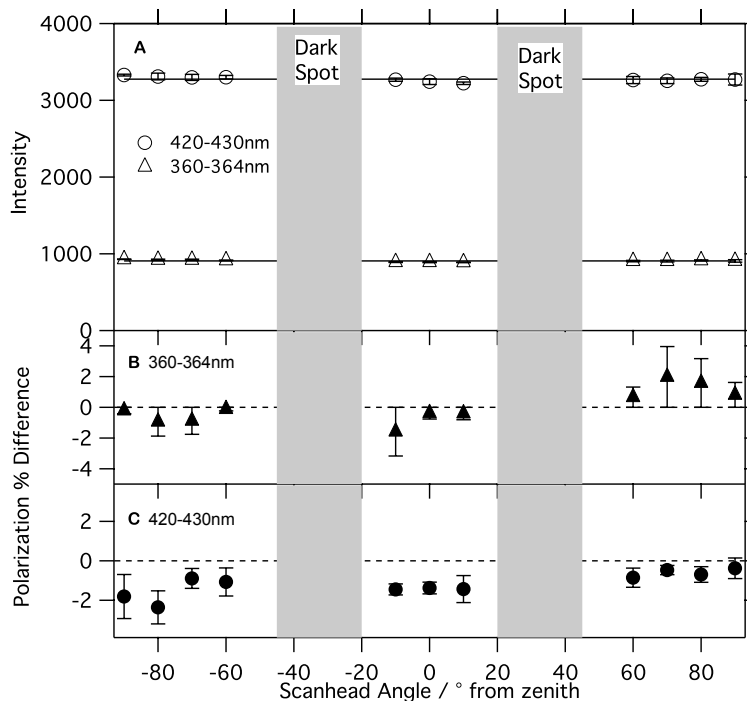


Fig. 5. Instrumental characterization. Panel A demonstrates constant light intensity observed at different scan head view angles over two different wavelength regions (420–430 nm and 360–364 nm). These data points are the average of six different spectra and show standard deviations (1σ) of less than one percent. Panels B and C show the average percent difference, $100\% \cdot (V-H)/(H+V)/2$, with $\pm 1\sigma$ error bars in intensity between horizontally and vertically polarization-filtered light. The small percent differences indicate that the system is minimally biased by polarized light.

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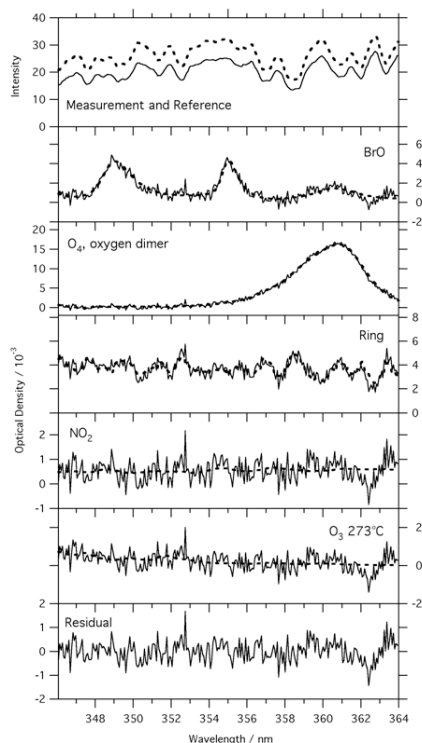


Fig. 6. Example of a spectral fit from Barrow, Alaska on March 18, 2009. The view elevation angle is 2° above the horizon and solar zenith angle (SZA) is 74° . In each panel, the solid line is the measurement spectrum and dotted line is the modeled partial fit, or the reference spectrum in the case of the top plot. The observed differential slant column densities (which are the fit coefficients) are as follows: BrO: 4.96×10^{14} molecules/cm², O₄: 3.83×10^{43} molecules²/cm⁵, NO₂: 1.17×10^{15} molecules/cm², O₃ at 273 K: 1.62×10^{18} molecules/cm². The RMS deviation of the residual spectrum from zero is 4.40×10^{-4} .

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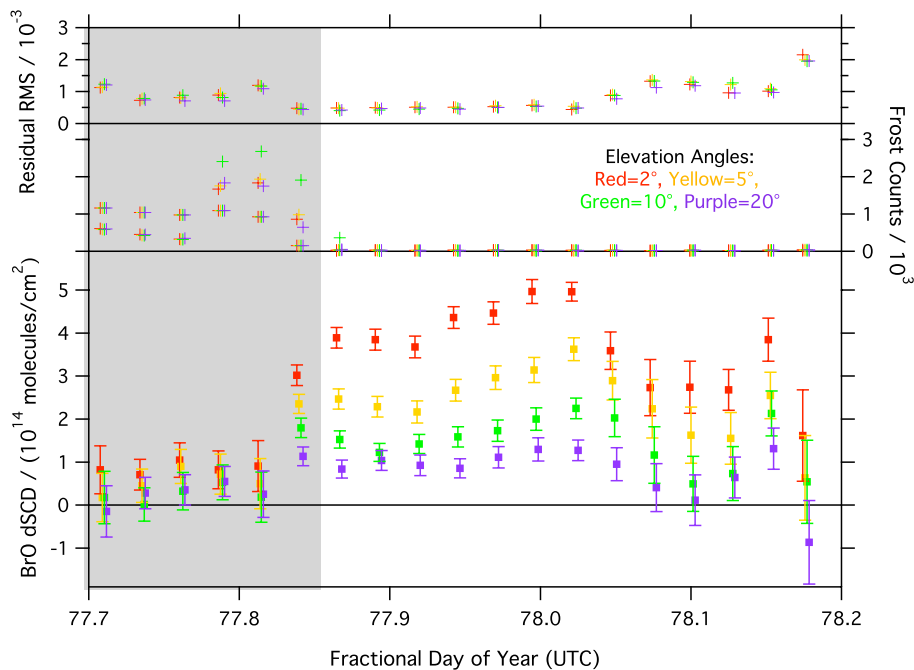


Fig. 7. MAX-DOAS observations on 18 March 2009 in Barrow, AK (fractional day of year 77.7–78.2 UTC). Top: spectral fit residual RMS values. Middle: frost count values. Bottom: local zenith referenced dSCD values of BrO with spectral fitting error bars. Frost on the instrument view window (times shaded in grey) causes the BrO dSCDs at all view elevation angles to be zero. Average midday RMS values (SZA less than 80°) are 5.4×10^{-4} .

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