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**Relaxed Eddy
Accumulation
(REA)-GC/MS system**

K. E. Hornsby et al.

A Relaxed Eddy Accumulation (REA)-GC/MS system for the determination of halocarbon fluxes

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Abstract

Very short lived halocarbons (VSLH) play an important role in the transport of halogen atoms to the troposphere and lower stratosphere. Here we describe the development of a relaxed eddy accumulation system using gas chromatography coupled to a mass spectrometer (REA-GC/MS) to determine surface fluxes of VSLH with a time resolution of about 0.5 h. Laboratory tests showed that use of a common inlet for upward, downward and deadband flow paths resulted in mixing of upward and downward moving air masses, therefore we recommend the use of separate inlets. The modified system underwent field trials at Mace Head on the west coast of Ireland, where there are dense kelp beds known to emit a range of halocarbons. Over a 16 h period in mid-September 2007, the mean fluxes obtained were 51.7 ± 5.9 , 2.9 ± 0.4 and 0.9 ± 0.1 nmol m⁻² day⁻¹ for CH₂Br₂, CH₂ICl and CH₂I₂, respectively.

1 Introduction

Volatile organic halogens are ubiquitously observed in marine environments (Carpenter et al., 1999; Abrahamsson et al., 2004; Chuck et al., 2005; Butler et al., 2007). They are thought to be produced mainly by micro and macroalgae (Ek Dahl et al., 1998; Carpenter et al., 1999; Laturnus, 2001; Dembitsky, 2006) in seawater. VSLH, comprising bromine and/or iodine-containing hydrocarbons, photolyse in the troposphere or lower stratosphere to give halogen atoms which, via a variety of catalytic pathways, deplete surface ozone concentrations and perturb free radical populations (von Glasow et al., 2004; Yang et al., 2005). Iodine oxide radicals produced as a result of these interactions potentially produce new aerosol particles and result in the formation of cloud condensation nuclei (O'Dowd et al., 2002; McFiggans et al., 2004), which in turn affects climate.

The data available on the distributions and concentrations in air and in seawater of VSLHs are rather limited (Atlas et al., 1993; Connan et al., 1996; Yamamoto et al.,

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2001; Carpenter et al., 2007). Determination of sea-air fluxes from simultaneous air and water measurements are even more limited and subject to significant spatial and temporal uncertainty (Baker et al., 2000; Chuck et al., 2005; Butler et al., 2007; Zhou et al., 2008). Sea-air fluxes of trace gases are calculated from such measurements using Eq. (1),

$$F = k_w \left(C_w - \frac{C_a}{H} \right) \quad (1)$$

where C_w and C_a are the concentrations in surface sea water and in air, respectively, H is the dimensionless Henry's law coefficient and k_w is the gas transfer velocity (Liss and Merlivat, 1986) which in turn is usually calculated from an empirical equation dependant on wind speed. In order to calculate the transfer velocity, the Schmitt number for the species is required. For some halocarbons there are no measurements of this parameter, therefore an approximation can be made using the Schmitt number of CO_2 (Wanninkhof, 1992; Nightingale et al., 2000). Shown in Eq. (2) is the Nightingale parameterisation for k_w ,

$$k_w = \left(0.222u^2 + 0.333u \right) \left(\frac{Sc}{660} \right)^{-1/2} \quad (2)$$

Where u is the wind speed in m s^{-1} and Sc is the Schmitt number of the gas in question.

Whilst Eq. (1) allows calculation of sea-air fluxes for trace gases which are relatively well dispersed in the oceanic mixed layer, the difficulty in measuring true surface water concentrations can lead to errors in flux calculations, particularly for compounds which exhibit strong near surface gradients in seawater, such as the dihalomethanes CH_2I_2 and CH_2ICl (Jones and Carpenter, 2006; Martino et al., 2006). Furthermore, determination of fluxes over exposed seaweed beds is not possible with this technique, despite the fact that these are known to produce large quantities of VSLHs (Nightingale et al., 1995; Ekdahl et al., 1998; Baker et al., 2001). Consequently, a reliable method for coastal quantification and direct measurement of halocarbon fluxes in the marine environment is required.

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Relaxed Eddy Accumulation (REA) is a conditional sampling technique which has been developed as a relaxation of the Eddy Accumulation (EA) approach suggested by Desjardins (1974) and is related to the widely used eddy covariance technique (EC), e.g. Foken (2008), Pryor et al. (2007). EC uses a fast response sensor to make real-time concentration measurements of the target compound and uses data from a sonic anemometer and air sampled at a rate proportional to the vertical wind speed to calculate the flux. However due to the challenges in using eddy covariance for determining fluxes for a variety of trace gas species, work has focused on the application of REA. REA is a derivative of EA that was first proposed by Hicks and McMillen (1984) and formulated in detail by Businger and Oncley (1990). REA can therefore be used to measure trace atmospheric gases for which fast response sensors (>10 Hz) required for EC are not available (Businger and Oncley, 1990). In REA, upward moving air (from the surface) and downward moving air (bulk air considered to be well mixed) created from eddies in the air column, are separated into reservoirs and fluxes are calculated using Eq. (3),

$$F = \beta \sigma_w \Delta C \quad (3)$$

where ΔC is the difference in mean concentration of the upward and downward moving eddies, σ_w the standard deviation of the mean vertical wind velocity and β an empirical coefficient (Businger and Oncley, 1990) calculated from in-situ eddy correlation measurements of the sensible heat flux using Eq. (4) (Zemmelink et al., 2004),

$$\beta = \frac{\overline{w'\theta'}}{\sigma_w (\overline{\theta_u} - \overline{\theta_d})} \quad (4)$$

where θ_u and θ_d are the average temperatures in the upward and downward wind directions and $\overline{w'\theta'}$ is the sensible heat flux. Values of β are typically around 0.56 and are weakly dependant on the stability of the wind regiment at the time of the measurement. The benefit of REA is that the separated upward and downward moving

air masses can be stored then analysed using relatively slow methods such as gas chromatography coupled with mass spectrometry at a later date. REA has been successfully developed and validated by means of EC for measurements of fluxes of CO₂ (Pattey et al., 1993; Brut et al. 2004), volatile organic compounds (VOCs) such as isoprene and monoterpenes (Bowling et al., 1998; Lee et al., 2005) and aerosols (Schery et al., 1998; Gaman et al., 2004; Grönholm et al., 2007.), however it is still technically challenging. Uncertainties in fluxes derived by the REA technique are discussed by Pattey et al. (1993) and Kramm et al. (1999).

Here we describe the development and initial field trials of an REA-GC/MS system for the measurement of halocarbon fluxes.

2 Methods

2.1 REA system

The initial design for the REA system consisted of a common inlet split into three flow paths: up and down sampling reservoirs and a “dead band”. The up and down sampling reservoirs consist of thermal desorption tubes, 5” stainless steel pre-packed tubes filled with 3 different carbon based adsorbents (Carbopack B, Carbopack C and Carbo-seive III, Supelco, UK. Supplied by Marks International, UK) packed in increasing order of strength. The tubes were arranged to allow continuous sampling by connecting them to a 16-port Vici trapping/flow-through multi-position valve with a common inlet and a common outlet, allowing each tube to be isolated from the atmosphere until required for sampling. The dead band flow path was used to prevent sampling during rapid changes in the vertical wind speed and distortion of the observed fluxes (Zemmelink et al., 2004) by removing air moving at wind speeds of $\leq \pm 0.05 \text{ ms}^{-1}$. The deadband flow limit could be increased or decreased depending on the size of the eddies observed. All three flow paths through the system were of equal length and flow restriction to reduce fluctuations in flow rate as a result of switching. All flow paths

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were bracketed by a pair of fast switching valves (Sirai, Italy) to isolate the reservoirs while not required for sampling. Air samples were dried prior to trapping on the tubes by a NafionTM membrane (Brunswick Instruments, USA) molecular sieve dryer. Flows through the system were monitored by a mass flow meter (Alicat) and controlled using a Venturi handled needle valve (Swagelok, USA) acting as a critical orifice (Fig. 1a). Usually, REA flux measurements must be corrected for the influence of water vapour and volumetric flow rate (Webb et al., 1980), however in this system there is no need for such corrections because of the use of a drier and mass flow meter, meaning that fluctuations in humidity and pressure are already accounted for.

The fast switching valves were controlled from a sonic anemometer (Gill UK, Model R3) with the sonic transducer assembly mounted in the vertical. The minimum response time of the sonic anemometer was 0.020 s and the sonic transducer pathlength was 15 cm. The serial output data from the sonic anemometer was coupled to a computer running data acquisition software written in LAB View 8. The fast switch valves had a response time of 0.1 s so the data from the sonic anemometer were averaged and recorded at the same rate to prevent lag within the system which would create mixing of the air masses and distort the results. The electronics and switching valves were mounted in a small box (9×12×20 cm) downstream of the sonic anemometer (which is 70 cm tall) with the air inlet co-located with the sonic anemometer sample volume to ensure concurrent vertical velocity and air mass concentration measurement. The 16-port valves, flow meters and adsorbent tubes were placed in a second housing, 150 cm further downwind of the switching valve housing and sonic anemometer, to further minimise flow distortion at the sonic anemometer.

The sonic EC system also provided supporting measurements of latent heat flux using a Krypton Hygrometer (Campbell Scientific Ltd., response time <0.02 s) and temperature and relative humidity, as well as pressure (Vaisala Models HMP-100 and PTB-100, respectively).

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2.2 Tube and on-line air analysis by GC-MS

Commercially available traps of three adsorbents supplied pre-packed in the thermal desorption tubes were used in this study. The strength of sorbent increases through the tube in the direction of flow, the more volatile compounds are trapped on the stronger sorbent. These have been shown to be capable of trapping volatile organic compounds from large volumes of ~3–4 L without breakthrough (Watson, 2008).

The tube samples were analysed using a Perkin Elmer (USA) Turbomass GC-MS system connected to a Perkin Elmer Automated Thermal Desorption unit (ATD). Each tube was desorbed for 30 min at a flow rate of 30 ml min⁻¹ and a temperature of 300°C onto the cold microtrap of the ATD, consisting of a 3-stage carbon-based adsorbent (Air monitoring trap, Perkin Elmer UK) maintained at -30°C. The cold microtrap was then flash heated to 360°C and injected onto a 60 m DB5 GC column (Supelco). The oven program started at 35°C and was held for 9 min before ramping up to 180°C at a rate of 10°C min⁻¹, holding for 1 min and finally ramping to 200°C at a rate of 25°C min⁻¹. The oven was held at 200°C for 15 min before cooling. The MS was run in selective ion recording (SIR) mode with a dwell time of 0.15 s on each of the two ions used for identification and quantifications (Table 1).

Online air measurements were made by trapping air dried by passage through a NafionTM membrane (Brunswick Instruments, USA) molecular sieve dryer directly onto the cold trap of the ATD before analysis using the same oven program and MS conditions as the tube samples. The online air samples were trapped for 30 min at -30°C every 45 min during the REA sampling period.

2.3 Calibration and system performance

The GC-MS was calibrated using a two stage process. A gas standard containing low-pptv mixing ratios of the target halocarbons (Table 1) was prepared. This gas standard was used in the field to calibrate the GC/MS and was quantified in our laboratory against an in-house built permeation system (Wevill and Carpenter, 2004) immediately

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after the campaign. The standard was prepared by injecting μmol amounts of the pure compound into 70 ml HPLC grade methanol (Fisher UK), without head space. $4\ \mu\text{l}$ of this solution was injected into 1.1 l of HPLC water (Fisher UK) without head space. 20 ml of the resulting solution was purged at a temperature of 90°C with zero grade nitrogen (BOC UK) and collected in an evacuated, cleaned Aculife cylinder (10 L, CK Gases). The resulting gas standard was diluted by a factor of 300 with zero grade nitrogen (BOC UK). The permeation system used to calibrate the standard consists of permeation tubes (EcoScientific) filled with pure liquids (Sigma Aldrich) placed inside one of two gas-tight glass ovens mounted in aluminium heating blocks held at 40 and 70°C with a constant flow of nitrogen at $100\ \text{ml}\ \text{min}^{-1}$. The halocarbon permeation tubes were positioned in the two ovens based on the halocarbon volatility, with the less volatile species placed in the hotter oven. Slugs of permeation gas were injected into a stream of nitrogen gas by means of a two flow path Vici valve connected to a $10\ \mu\text{l}$ sample loop (Restek UK), allowing specific volumes of the permeation gas to be introduced.

The estimated errors of the online air and tube analyses are shown in Table 1. The error includes the uncertainty on the slope of the calibration curve, the uncertainty of the permeation tube weightings and the precision of the online air/tube measurement made using the GC-MS. Precisions for the tubes were determined by analysis of 5 consecutive tubes loaded with halocarbon standard (Table 1) and 5 consecutive online standards for the online air. The error on the flux measurements is discussed in Sect. 3.

Breakthrough volumes were assessed in the field using three pairs of tubes loaded concurrently with ambient air. The flow rates were set such that 3, 4, and 5 L were trapped in the same 20 min sampling period. The GC/MS analysis showed that these volumes were below the breakthrough volume of the tubes.

2.4 Foot print calculations

Footprints were calculated using measured wind velocities, friction velocity and sensible heat flux from the sonic anemometer at the site as input to the 3 dimensional

analytical approximation of Schmid (1994).

The roughness length, z_0 , for terrestrial surfaces used in this model can be calculated using the following equation,

$$z_0 = \frac{z_m - d}{\exp\left(\frac{kU}{u_*\Phi_m}\right)} \quad (5)$$

5 where z_m is the measurement height, d is the zero plane displacement, k is the von Karman constant (~ 0.41 , empirically determined), U is the wind speed, u_* is the friction velocity and Φ_m is the stability parameter. For water surfaces which may influence some observations at coastal zones in the transition from low to high tide, z_0 can be determined using the relationship described by e.g. Zilitinkevich (1969)

$$10 \quad z_0 = c_1 \frac{\nu}{u_*} + \frac{u_*^2}{c_2 g} \quad (6)$$

where c_1 and c_2 are coefficients with highly variable values, $c_1 \sim 0.0-0.48$, and c_2 ranges from ∞ to 81.1 (the commonly used Charnock (1955) relationship employs $c_1=0.0$ and $c_2=81.1$ although this may underestimate z_0 for open/rough seas), u_* is the friction speed, g the acceleration due to gravity and ν is the kinematic viscosity.

15 **3 Results and discussion**

3.1 Laboratory testing of REA GC-MS

The REA GC-MS system underwent two testing phases to ensure that complete separation of the upward and downward moving air masses could be achieved, which is essential for quantitative calculation of fluxes. The test rig for these experiments consisted of two additional pairs of fast switching valves, set such that there was no build up of pressure in the system. One pair of gas valves was synchronised with the updraft

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valve and the other with the downward draft valve. The standard was connected to the updraft switching valves and used to supply the system with “updraft” air. Connected to the other pair of switching valves was clean N₂ to supply “downdraft” air.

For the first test, the system switched between the updraft and downdraft reservoirs at regulated frequencies of 10, 5 and 1 Hz. A flow rate of 300 ml min⁻¹ was used and the percentage of “updraft” air present on the updraft tube of the pair was calculated by summing the peak areas on both tubes and calculating the percentage present on the updraft tube, and was used to gauge how much mixing had occurred between the two flow paths. The second test used data recorded by the sonic anemometer from a field experiment at a coastal site in northern France. This “real world” turbulence file was used as a reference to simulate switching frequencies and to control switching between the updraft and downdraft reservoirs with a variable deadband. Two simulations were conducted. In simulation A, the deadband flow limit was 0.05 m s⁻¹ and in simulation B the dead band flow limit was increased to ±0.1 m s⁻¹. The purpose of these simulations was to assess any change in the amount of mixing that occurred when the switching became irregular and the extent to which the deadband was able to recover the resolution of the two reference air masses.

Shown in Fig. 2 are the results for 3 representative halocarbons (CH₂Br₂, CH₂ICI and CH₂IBr) for the five test scenarios. For CH₂Br₂, the percentage of updraft air in the updraft tube increased as the switching rate decreased. This was as expected because slower switching rates mean longer periods of uninterrupted air. However, for some compounds like CH₂ICI, there was no discernable increase in the discrimination as the switching frequency decreased, although improvement occurred with the introduction of the deadband during real sonic file tests. The simulations also showed that the larger the deadband, the more efficiently the compounds were separated. However, the effect of increasing the deadband flow limit from 0.05 ms⁻¹ to 0.1 ms⁻¹ was that in the 20 min sampling period, the volume trapped on the individual tubes was reduced from 2.5 l to just under 2 l, i.e. the sensitivity of the measurement for a particular time period was reduced. In order to both prevent mixing of up and down-draft air and maintain a

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relatively small deadband flow rate, the REA system was modified so that each flow path had an individual inlet to prevent mixing (Fig. 1b).

3.2 Reproducibility and sensitivity

Because of the highly photolabile nature of some of the target halocarbons, it is expected that the concentrations in many of the tubes (particularly downdraft tubes) would be lower than the limit of detection (LOD). Discarding this data would lead to low data coverage. For samples where a tube was under the detection limit, fluxes were calculated using (i) the measured value, (ii) the LOD and (iii) half the LOD, in place of the measured value. In this way it is possible to estimate an upper and lower limit for the calculated fluxes. In practice, the variability introduced into the fluxes by taking this approach was less than the calculated precision of the flux results. In REA, the concentration observed in the downdraft is subtracted from the concentration in the updraft. Consequently, the precision of an REA measurement is the Gaussian propagated precision for the analyses of two tubes (Sect. 2.3 and Table 1, also see e.g. Kramm et al., 1999). A limit of calculable flux (LOCF) is calculated from the product of the percentage precision (Table 1) and the highest concentration in the tube pair. A particular flux measurement will be above the LOCF if ΔC is greater than this quantity. The LOCF is expressed as a flux using Eq. (3).

3.3 Summary of results from BIOFLUX II campaign

The REA system was first deployed as part of an INTROP exchange trip, the Biogenic Flux Experiment phase II (BIOFLUX II), which took place at the Atmospheric Research Station at Mace Head on the West Coast of Ireland (53°19'33 N, 9°54'00 W) (Simmonds and Derwent, 1991), between the 20 August and the 15 September 2007. The REA system was sited at a height of 8 m on the pre-existing 23 m tower at the site (Heard et al., 2006). The samples were taken in 5 hourly batches with each REA collection period lasting 35 min. The samples were run within 24 h of collection. Shown in Table 2 are

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the range and mean fluxes of all the species observed and in Fig. 3 are a time series of three representative halocarbon species along with the LOCF, wind speed and tidal height. All three halocarbon species exhibit higher fluxes during periods of low tide than those observed at high tide, $203\% \pm 23\%$ for CH_2Br_2 , $15\% \pm 2.1\%$ for CH_2I and $120\% \pm 15.0\%$ for CH_2I Br, as expected given that seaweeds are the major source at this site (Carpenter et al., 1999). The wind direction during the REA sampling period was fairly constant (Fig. 3). In the first sample period the sample fetch remained between west and south west and during the second sample period between the south west and the south

Dibromomethane showed a deposition during high tide and low wind speeds. This species is much longer lived (CH_2Br_2 has a tropospheric lifetimes of 47 days, Mossinger et al., 1998) than the iodocarbons (CH_2I has lifetime of around 90 min (Roehl et al., 1997) and CH_2I Br around 45 min at midday (Mossinger et al., 1998)) and may therefore be transported from surrounding oceanic/coastal regions to the site. Looking at the seaweed map in Fig. 4 it can be seen that there are large *Laminaria* beds containing both *hyperborea* and *digitata* about 2.5 km southwest of the site.

Deposition of bromocarbons has not previously been observed in coastal waters, in fact CH_2Br_2 is generally found to be supersaturated particularly in coastal waters (Butler et al., 2007). However, because Mace Head is surrounded by many seaweed-rich bays it is possible that air masses passing over exposed seaweed beds containing higher levels of CH_2Br_2 than the air in the immediate vicinity of the tower would present as downdraft air, causing an apparent deposition. The foot print of the REA system is further discussed in Sect. 3.4.

Macroalgae (seaweed) have been found to emit halocarbons more prolifically when under oxidative stress (e.g. sunlight) (Nightingale et al., 1995; Laturnus et al., 2004; Palmer et al., 2005). Further, rapid photolysis of the iodine-containing photolabile halocarbons during daylight hours is expected to give rise to a strong concentration gradient from the surface, which potentially could give rise to a stronger upward flux at the surface. Although the data set is limited, by comparing periods with the same tidal

signature, the day time fluxes were found to be an average of 2–3 times greater than during the night (Table 2). However, as discussed in Sect. 3.4, another factor affecting the fluxes is the wind speed and on the night of observations, the average day time wind speed (5.6 m s^{-1}) was significantly higher than the average night time wind speed (3.7 m s^{-1}).

Shown in Table 3 are the range and average measurements made for all the halocarbons observed. Also shown in Table 3 are the mean fluxes as measured by Greenberg et al. (2005) at Mace Head during September 2003 using the gradient flux technique. The gradient flux measurements quoted here are values as reported in Greenberg et al. averaged over 26 measurements made between the Mace Head research station and the Martin Ryan Institute round the bay. Given the different study periods and positions and inherent differences in techniques, our measurements are in reasonable agreement. The average CH_2Br_2 flux measured in this work was a factor of 2 lower than that measured by Greenberg et al. (2005) and the average CH_2IBr fluxes are remarkably similar. It should be noted that the measurements of Greenberg et al. had a much larger footprint because the measurements were made at heights of 50 and 100 m. This will affect the amount of mixing which occur in the air mass before sampling meaning that the resultant sampled air would be much more homogeneous than those observed by the REA system described in this paper.

3.4 Foot print calculations

Having recorded differences in the fluxes between high and low tide as well as day and night, it is important to determine whether the variability is caused by changing surface conditions (exposure of seaweed at low tide) or by different meteorological conditions causing a change in the measurement footprint. Three tidal periods were chosen from the measurements including a high tide scenario during the day, and two low tide scenarios – one at night and one during the day where the measured fluxes were comparable. The three scenarios chosen for footprint modelling were high tide on the 10 September at 15:30, low tide on the 11 September at 00:15 and low tide on

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the 10 September at 11:30 (shown in Fig. 5). The measurement height changes with the tide which in turn alters the roughness length. The footprint modelling shows that at low tide the fetch is larger than at high tide, and also as the wind speed increases a larger area is sampled. This means that interpretation of the differences in high and low tide and day and night-time has to incorporate differences in the source footprint. Figure 5 shows that all the footprints have the greatest contribution to the updraft at roughly 25 m or more away from the base of the tower, which is approximately the location of the high water line during the period of investigation. As the tide recedes the foot print enlarges as the measurement height increases, giving a larger field of view. The waterline at low tide during this investigation was ~ 75 m further away from the tower than the high tide waterline.

Direct comparison of the night- and day time low tide scenarios (Fig. 5b and c) shows that when the wind speed increases during the day, the catchment area (defined here as capturing 95% of emissions) is increased from ~ 95 m to ~ 225 m. As discussed in Sect. 3.3 and shown in Table 2, daytime low tide fluxes were higher than nighttime low tide fluxes, by $32.7\% \pm 3.7$ for CH_2Br_2 , $76.4\% \pm 10.5$ for CH_2ICl and $108\% \pm 13.5$ for CH_2IBr . This could possibly be attributed to enhanced VSLH release from macroalgae during the day as a result of light induced oxidative stress. However, Fig. 5 shows that another plausible explanation is that the daytime measurements captured more of the emissions from the lower littoral and upper sub-littoral zones where *Laminaria* are prevalent (Yonge, 1949; Barnes, 1986). *Laminaria* species are among the most prolific emitters of VSLH, with measured release rates typically much larger than for other seaweeds such as *Fucus* that are found higher in the intertidal zonation (Nightingale et al., 1995). We conclude that the different footprints for the day and night mean that in our limited study, direct comparison of fluxes is not possible.

Whole air measurements were made simultaneously with the REA measurements. Shown in Fig. 6 are the online data with tidal height and wind speed. The halocarbons show a tidal signature with increases in concentration around low tide, particularly for CH_2ICl which has a shorter lifetime than that of CH_2Br_2 . These results are consis-

tent with other measurements made at Mace Head during September (Carpenter et al., 2005). Assuming a vertical loss to the free troposphere of $350 \text{ mol air m}^{-2} \text{ hr}^{-1}$ (WMO, 2003), a photolytic lifetime of 47 days for CH_2Br_2 , and a boundary layer of 1 km we estimate that the average fluxes observed (Table 3) are capable of supplying approximately ~ 6 pptv of CH_2Br_2 to the MBL. Therefore, the atmospheric concentrations observed at the site have been diluted by background air containing significantly lower concentrations of CH_2Br_2 .

4 Conclusions

A common inlet REA-GC/MS system has been developed and tested in a series of simulation tests to assess the mixing that occurs between updraft and downdraft air during sampling. Because these simulation tests showed that significant mixing occurred except at high deadband flow limits the REA system was modified to incorporate separate inlets for each flow path (updraft, downdraft and deadband) through the system such that mixing of the air masses could not occur. The introduction of a dryer before trapping and the use of mass flow meter negated the need to correct for the density effect due to changes in sensible and latent heat fluxes. The precision of the REA measurements were calculated by determining the reproducibility of the individual tube samples and propagating the error of the downdraft and updraft analyses, resulting in estimated errors of 11.4%, 13.8% and 12.5% respectively for CH_2Br_2 , CH_2ICl and CH_2IBr . The limits of calculable flux (LOCFs) is calculated for the data obtain at Mace Head were well below the measured fluxes in most cases.

The system was field tested at Mace Head and flux measurements of 3 halocarbon species were made concurrently with whole air measurements. The fluxes showed similar patterns to the whole air measurements, with an increase at low tide. Whilst higher concentrations were observed during the night in whole air presumably due to the fast photolysis of VSLH, lower fluxes were observed at night compared to the daytime by a factor of 2–3. This could be due to a number of factors including a vertical

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concentration gradient in halocarbons during the day caused by their rapid photolysis, oxidative stress of macroalgae leading to higher daytime fluxes, or by the drop in wind speed during the night, causing a reduction in the sample catchment area. The fluxes observed in this study were in good agreement with those of Greenberg et al. (2005).

- 5 *Acknowledgements.* We acknowledge the European Science Foundation INTROP exchange scheme and the European Community EUSAAR Infrastructure fund, as well as NERC grant NE/D006538/1 for financial support. KEH acknowledges NERC for her studentship funding and R. Leigh for assistance with data analysis.

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Table 1. Quantification ions, uncertainty in online air and REA measurements, precision for online air and REA measurements and concentration of in house standard.

Compound	Identification and quantification ions (<i>m/z</i>)	Uncertainty in online air measurements (%S.D. \pm)	Uncertainty in REA measurements (%S.D. \pm)	Precision of online air measurements (%S.D. \pm)	Precision of REA measurements (%S.D. \pm)	Standard concentration pptv
CH ₂ Br ₂	174, 176	3.1	4.2	11.2	11.4	19.2 \pm 1.6
CH ₂ Cl ₂	127, 176	2.5	8.9	11.0	13.8	15.5 \pm 1.2
CH ₂ I ₂	220, 222	6.0	6.4	12.4	12.5	36.0 \pm 4.5

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Table 2. Ratio of day to night fluxes comparing periods with the same tidal signature.

Compound	11:25 10/09/07 00:15 11/09/07	12:00 10/09/07 00:50 11/09/07	12:35 10/09/07 01:25 11/09/07	13:10 10/09/07 02:00 11/09/07	Average
CH ₂ Br ₂	1.3	2.9	6.8	3.0	3.5
CH ₂ ICl	0.6	3.1	1.8	1.3	1.7
CH ₂ IBr	2.1	2.0	4.5	0.3	2.2

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Table 3. Range and mean fluxes observed during the Bioflux II campaign and the fluxes obtained by Greenberg et al. (2005) at Mace Head using the Gradient flux method and averaged over seven samples.

Compound	Range 10 to 90% ($\text{nmol m}^{-2} \text{ day}^{-1}$)	Average flux ($\text{nmol m}^{-2} \text{ day}^{-1}$)	Average flux ($\text{nmol m}^{-2} \text{ day}^{-1}$)
CH_2Br_2	–11.9–45.6	11.6	29.3
CH_2ICl	–0.9–8.3	2.9	
CH_2IBr	–3.4–6.0	0.9	1.1

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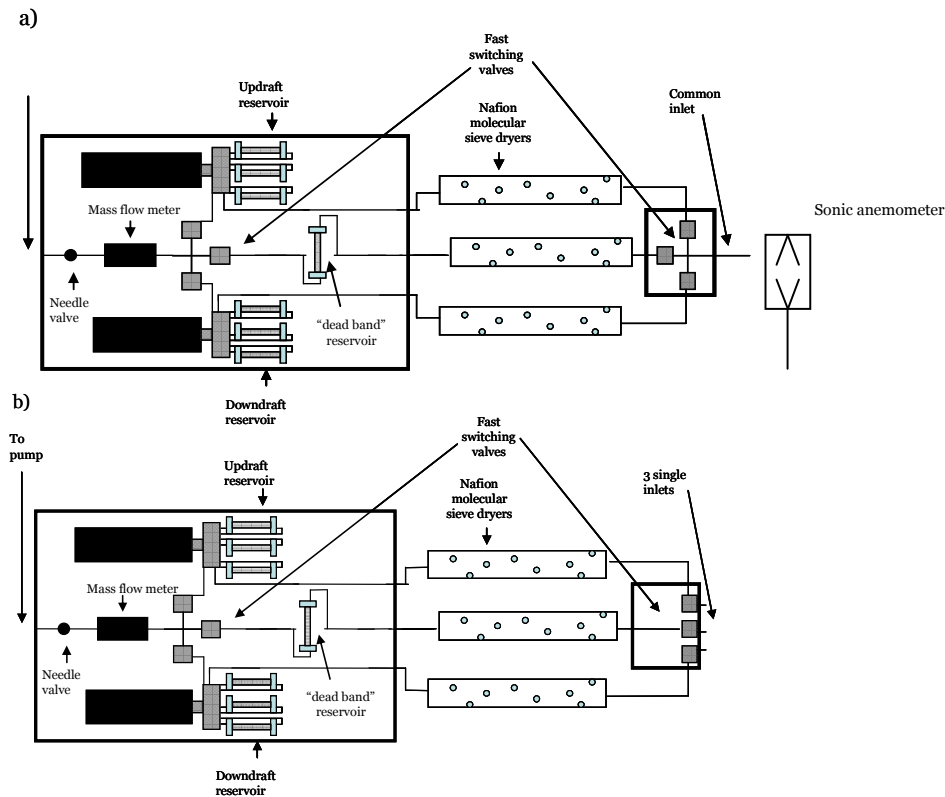


Fig. 1. (a) Initial REA system as trialed in the REA simulations, showing the position of the common inlet relative to the sonic anemometer. The inlet leads to the first set of fast switching valves followed by NafionTM molecular sieve dryers before the air enters the relevant reservoir. The air is stripped of the halocarbons then exists the system via a mass flow meter and needle valve, acting as a critical orifice, to the pump which is situated down stream; **(b)** the modified REA system as deployed in the field trials, with three separate inlets, one for each flow path through the system.

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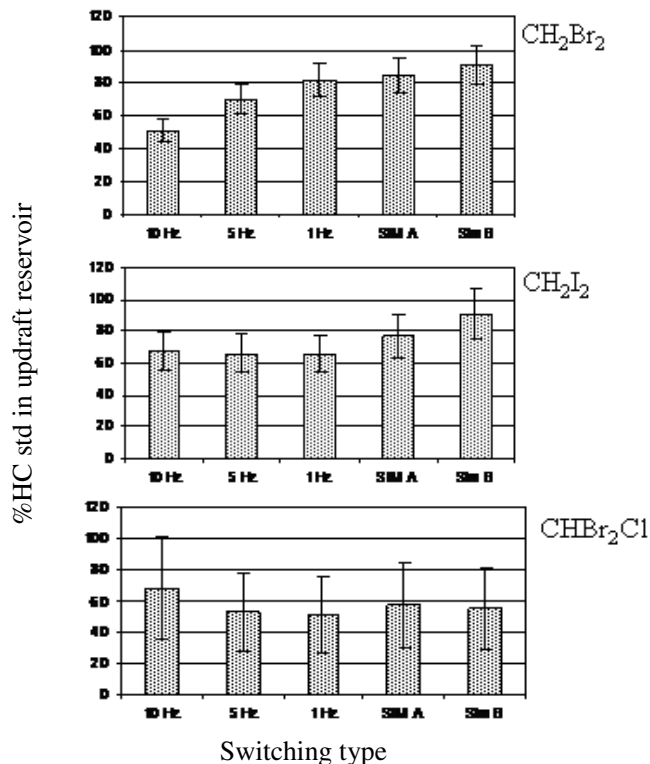


Fig. 2. Results from the simulation tests carried out on the initial REA system. The tests shown are for regulated switching at 10, 5 and 1 Hz. Two simulations, A and B, used dead-band values of 0.05 and 0.1 m s⁻¹. The results show improvement in separation for CH₂Br₂ as the switching rate decreases and the dead band increases and variations for CH₂ICI and CH₂I₂Br as the switching rate decreases but improvement with the introduction of the dead-band to the “real world” sonic turbulence file runs. The error bars indicate the precision of the measurement made using the adsorbent tubes.

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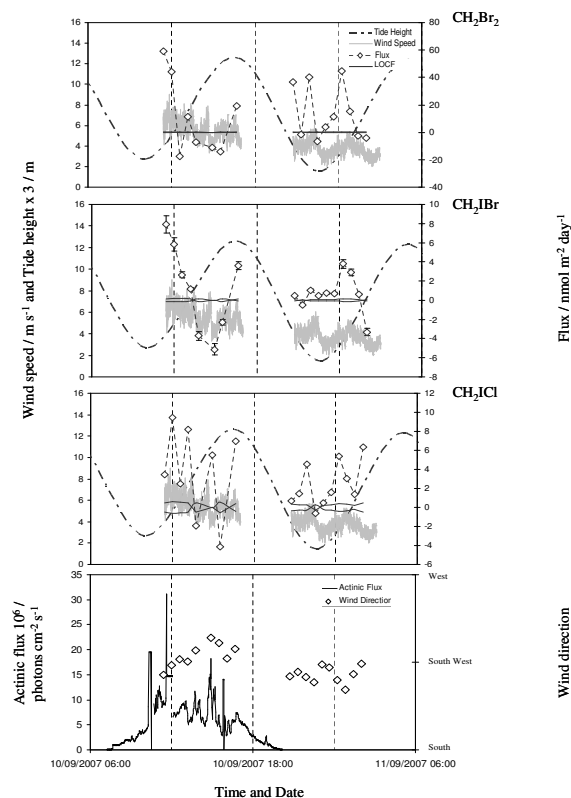


Fig. 3. Initial field results from the BIOFLUX II campaign showing: wind speed (grey solid line), tide height (dark dashed line), the measured fluxes for CH_2Br_2 , CH_2IBr and CH_2ICl in each panel respectively, are shown by the white diamonds; the solid black line shows positive and negative limit of calculable flux. Error bars show the 1σ precision of the flux measurements. The bottom panel shows total downward actinic flux (black line) and average wind direction (white diamonds) for each sample period. Grey shading indicates hours of darkness.

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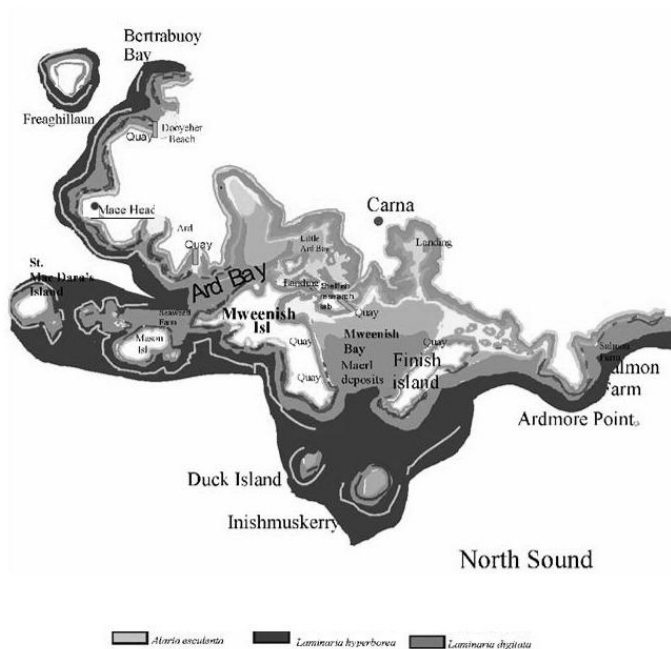



Fig. 4. Seaweed map showing the three main species and their location around the Mace Head area. *Laminaria digitata* in solid grey, *Laminaria hyperborea* in dark grey and *Alaria esculenta* in white line. Taken from the Connemara Seaweed Survey, by the seaweed centre, National University of Ireland, Galway.

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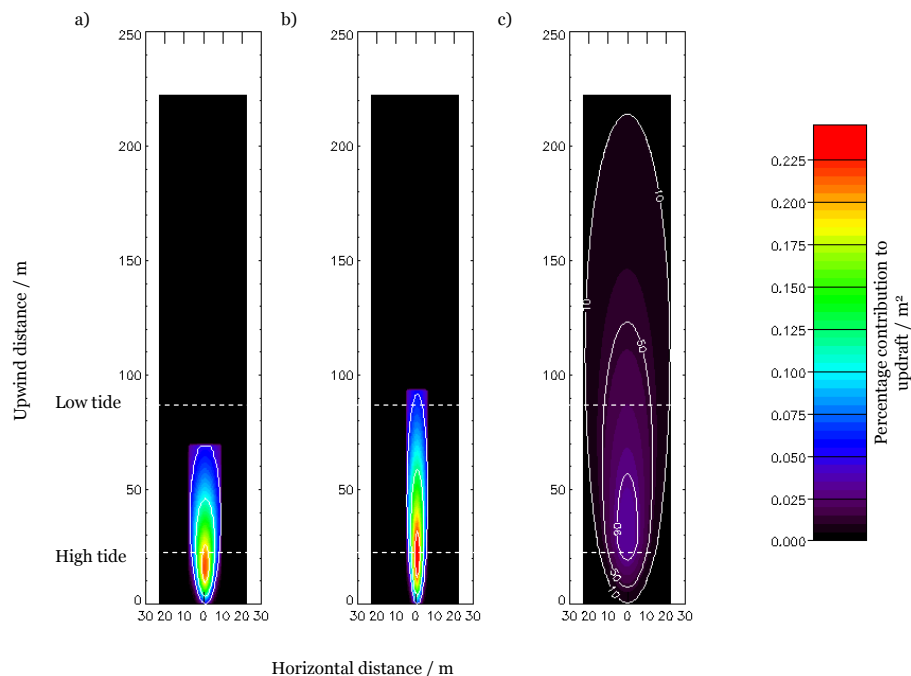


Fig. 5. Results of foot print modelling, **(a)** day time foot print at high tide, **(b)** night time foot print at low tide, **(c)** day time foot print at low tide. Tower location is at 0 on the horizontal axis. The white rings around the contours of the plot indicate the percentage contribution to the plot outside the ring. The white dotted lines indicate the position of high water and the approximate low water for the tidal period.

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**Relaxed Eddy
Accumulation
(REA)-GC/MS system**

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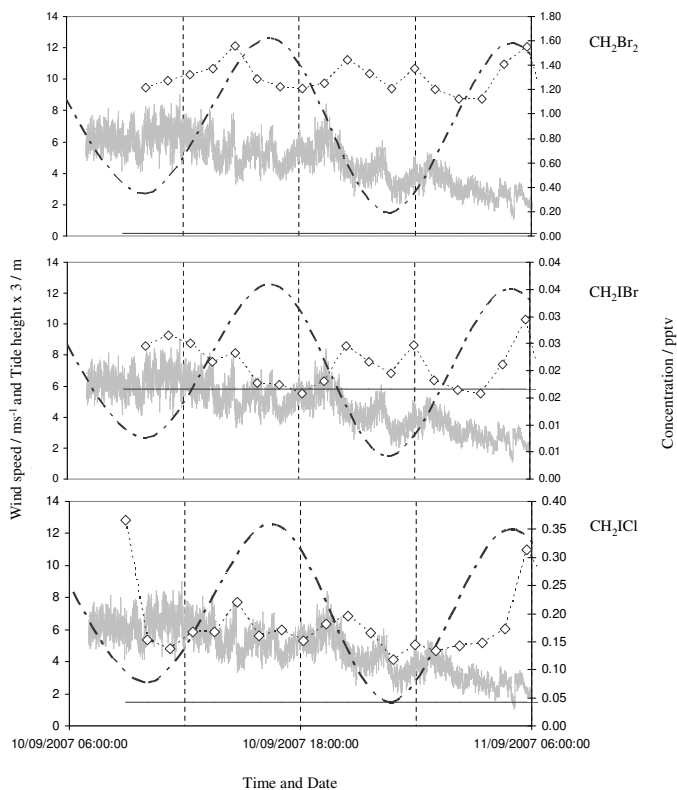


Fig. 6. Online air measurements co-located with the REA system. Tidal height, wind speed, limit of detection and concentration in pptv. Also shown are the precisions for the measurements as 1σ error bars. Shaded areas indicate hours of darkness.

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