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A Raman lidar at La Reunion (20.8° S, 55.5° E) for monitoring water vapor and cirrus distributions in the subtropical upper troposphere: preliminary analyses and description of a future system

C. Hoareau¹, P. Keckhut¹, J.-L. Baray^{2,4}, L. Robert², Y. Courcoux⁴,
J. Porteneuve¹, H. Vömel³, and B. Morel^{2,*}

¹LATMOS, UMR8190, INSU-CNRS, UVSQ, UPMC, 11 Boulevard d'Alembert,
78820 Guyancourt, France

²LACy, UMR8105, 15 avenue René Cassin – BP 7151 – 97715 St-Denis Cedex 09,
La Réunion, France

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³Deutsch Wetterdienst, Richard Assmann Observ, Lindenberg, Germany

⁴OSU Réunion, UMS3365, 15 avenue René Cassin – BP 7151 – 97715 St-Denis Cedex 09, La Réunion, France

*now at: LE2P, 15 avenue René Cassin – BP 7151– 97715 St-Denis Cedex 09, La Réunion, France

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Correspondence to: C. Hoareau (christophe.hoareau@latmos.ipsl.fr)

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Abstract

A ground based Rayleigh lidar has provided continuous observations of tropospheric water vapor profiles and cirrus cloud using a preliminary Raman channels setup on an existing Rayleigh lidar above La Reunion over the period 2002–2005. With this instrument, we performed a first measurement campaign of 350 independent water vapor profiles. A statistical study of the distribution of water vapor profiles is presented and some investigations concerning the calibration are discussed. The data set having several long acquisition measurements during nighttime, an analysis of the diurnal cycle of water vapor has also been investigated. Analysis regarding the cirrus clouds is presented and a classification has been performed showing 3 distinct classes. Based on these results, the characteristics and the design of a future lidar system to be implemented at the new Reunion Island altitude observatory (2200 m) for long-term monitoring is presented and numerical simulations of system performance have been realized to compare both instruments.

1 Introduction

Water vapor has long been recognized as one of the most important trace gases in the atmosphere. The measurements of water vapor profiles are important for understanding and forecasting of the moisture convection and horizontal transport. Water vapor plays also a crucial role in many aspects of the Upper Troposphere and Lower Stratosphere (UTLS). This requires an accurate determination. It contributes strongly to the radiative balance of the atmosphere and plays an important role in global climate (Forster and Shine, 2002; Kley et al., 2000). Measuring accurately the water vapor concentration in the UTLS region is a difficult task given its very low concentration and its large variability. Water vapor can be considered for the study of tropical and sub-tropical atmospheric dynamical phenomena and their roles in the local and global circulations and in climate changes through vertical and horizontal

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transport in particular through tropical and sub-tropical Stratosphere Troposphere Exchanges (STE). However, condensation into ice during cirrus formation redistributes water downward through subsidence effects of heavy particles. Upper tropospheric water vapor in the tropics and subtropics is strongly influenced by the Hadley Cell and the Walker circulation (Kley et al., 2000). Widening of the tropics may also lead to changes in the distribution of climatically important trace gases in the stratosphere. The Brewer-Dobson circulation moves air upwards from the troposphere into the stratosphere in the tropics. If the area over which this upwelling occurs increases, transport of water vapor into the stratosphere might be enhanced. This could lead to an enhanced greenhouse house effect, including tropospheric warming and stratospheric cooling, and reduced ozone (Seidel et al., 2008; Forster and Shine, 2002; Kirk-Davidoff et al., 1999). Tropospheric and stratospheric water vapor has been measured over the past decades by a large number of instruments with different characteristics and limitations (Kley et al., 2000). Water vapor measurements using the Raman lidar are not new (Cooney et al., 1970; Ferrare et al., 1995; Whiteman et al., 1992). This technique is one of the only ones which enables to probe the upper troposphere and tropopause region. Moreover, the possibility to acquire an elastic signal simultaneously with water vapor Raman signals is of great interest for providing information about ice crystal occurrence. Capabilities have been successively improved with larger commercial laser power availability (Sakai et al., 2007; Sherlock et al., 1999a; Leblanc et al., 2008; Whiteman et al., 1992). Some preliminary Raman channels have been setup on an existing Rayleigh lidar to perform first investigations and capabilities evaluations to measure water vapor in the upper troposphere and to design a future specific instrument. In this publication, a brief description of data retrievals and the design of the instrument have been described in Sects. 2 and 3. Data processing, regarding calibration and validation aspect, is exposed in Sect. 4. A statistical study of subtropical water vapor and scattering ratio profiles from Raman lidar is presented in Sect. 5 and the description of the design of a new specific Raman lidar to be implemented at the Maïdo altitude station is presented in Sect. 6.

2 Water vapor and cirrus cloud optical depth calculation from Raman lidar

2.1 Water vapor mixing ratio

The ratio of the mass of water vapor to the mass of dry air in a given volume, known as the water vapor mixing ratio, is a convenient measure of the amount of water vapor in the atmosphere. As atmospheric nitrogen forms a constant proportion of dry air (~78 %) in the lower atmosphere, normalizing the H₂O Raman return with the N₂ Raman profile allows mixing ratio to be derived. Accounting for the atmospheric differential transmission $\Gamma(z)$ and the calibration coefficient C , it can be calculated using the following expression (Sherlock et al., 1999a; Whiteman et al., 1992):

$$q(z) = c \cdot \Gamma(z) \cdot \frac{S_{\text{H}_2\text{O}}(z)}{S_{\text{N}_2}(z)} \quad (1)$$

The calibration aspect is an important issue to insure an accurate monitoring. Various approaches have been tested to calibrate the water vapor measurements of a Raman lidar system. However, calibration issues are still pending and debated (Whiteman et al., 2011; Leblanc et al., 2011). Though an absolute calibration of the entire lidar system is theoretically possible, the signal ratio is usually scaled to various external water vapor measurements (radiosonde, microwave radiometer, Global Positioning System (GPS)...) in order to deduce water vapor mixing ratio. Calibration coefficients determined from nearby radiosondes are commonly used, but their reliability for long-term continuity is questionable (Soden and Lanzante, 1996) and more independent techniques have been investigated (Sherlock et al., 1999b; Leblanc and McDermid, 2008). The Network for the Detection of Atmospheric Composition Change (NDACC) has recently established long-term monitoring of water vapor using Raman lidar as one of its core objectives (Leblanc et al., 2008). One of the principal needs for developing a long-term dataset for monitoring atmospheric trends is the calibration stability better than 10 % or less and that varies randomly around some mean and does not involve

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step jumps of unknown magnitude or significant drifts (Whiteman et al., 2011; Leblanc et al., 2011). For this reason, it is essential to carefully investigate any calibration techniques developed for ensuring stable, long-term calibrations.

2.2 Cirrus cloud optical depth retrieval

5 The optical thickness of cirrus is calculated in accordance with the aerosol Scattering Ratio profile (SR) which is defined as the ratio of the total (molecular and particle) backscatter coefficient divided by the molecular backscatter coefficient. Because molecular backscattering can be estimated by a dry air density profile, it can further be retrieved from the nitrogen signal, so SR can be derived from the ratio of the power in
10 the Rayleigh-Mie and Raman vibrational N₂ channels (Ferrare et al, 2001).

The optical thickness of cirrus, τ_{cirrus} , is calculated using a method similar to that described by Goldfarb et al. (2001), where τ_{cirrus} can be expressed by the following expression:

$$\tau_{\text{cirrus}} = (\text{LR})\sigma_{\text{rayleigh}} \int_{z_{\min}}^{z_{\max}} n_{\text{air}}(z)(\text{SR}(z) - 1)dz \quad (2)$$

15 Where $\beta_{\text{rayleigh}} = \sigma_{\text{rayleigh}} \cdot n_{\text{air}}(z)$ and the air density number $n_{\text{air}}(z)$ are calculated by the Mass Spectrometer Incoherent Scatter-Extended-1990 (MSISE-90) atmospheric model. A lidar ratio (LR) of 18.2 sr (Platt and Dille, 1984) is used, and $\sigma_{\text{rayleigh}}(532\text{nm}) = 5.7 \times 10^{-32} \text{ m}^2 \text{ sr}^{-1}$.

3 Technical description of the instrument

20 The Raman water vapor lidar system deployed at La Reunion is an upgrade of the receiving optics of the existing Rayleigh-Mie lidar system which operates on a routine basis at night, except in presence of low cloud at the Observatoire de Physique de l'Atmosphère de La Réunion (OPAR), hosted by Reunion Island university at 80 m

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above the sea level (a.s.l.) (Baray et al., 2006). Regular water vapor measurements have been realized with this configuration over the period 2002–2005. This long campaign allowed us to perform a preliminary study of water vapor monitoring capabilities and to evaluate the needs regarding a more specific lidar system to be implemented at the future altitude facility at Piton Maïdo mount (2200 m a.s.l.). During this period, about a hundred acquisition nights have been acquired using the Raman channels.

The Raman lidar system is based on a Nd:Yag laser source with a repetition rate of 30 Hz and the second harmonic is used. The pulse energy at 532.1 nm is 800 mJ pulse⁻¹ (9 ns pulse length). The radiation backscattered by the atmosphere is collected by means of a 4-telescope mosaic (0.53 m diameter each) of Newtonian type with a field-of-view of 1 mrad. A schematic representation of the Rayleigh lidar instrument is given in Fig. 1. In this ensemble, the received wavelengths are spectrally separated through a set of dichroic beam splitters, mirrors and bandwidth pass-band interference filters (BPIF). The beam reflected toward this ensemble is, firstly, filtered by an $\alpha - \varepsilon$ high-pass interference filter specially designed to reject the remaining 532 nm component with a rejection ratio between the transmitted and incident energy at 532 nm of 10^{-5} : this filter has a maximum transmission of 91.5 % at 607 nm and of 89.2 % at 660 nm. The filtered beam is then split by another dichroic beam splitter that reflects its 607 nm component toward the photomultiplier (PMT) of the Raman N₂ channel and transmits its 660 nm component toward a metallic mirror that finally reflects the 660 nm component toward an avalanche photodiode (APD) which is the detector of the Raman H₂O channel (Fig. 2). A BPIF with a maximum transmission of 57 % at 607 nm and a full width at half maximum (FWHM) of 1 nm is placed in front of the N₂ PMT and aims notably to reject the residual 532 nm component which passed through the $\alpha - \omega$ high-pass interference filter. A focusing lens with a focal length of 50 mm is placed after this filter to focus the Raman 607 nm component onto the photocathode of the N₂ PMT. Two three-cavity interference filters are used on the H₂O channel to ensure that the Rayleigh-Mie contribution and Raman contributions from N₂ and O₂ are less than 0.1 % of the water vapor signal in all measurement conditions. The BPIFs placed in front of

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the H₂O photodiode have a maximum transmission of 80 % and 57 % at 660 nm and respectively a FWHM of 5 nm and 1 nm. The detector used for the Raman N₂ channel is a multi-alkali 9-stages Hamamatsu R1477 circular-cage PMT that is cooled down to a temperature of about −20 °C through a Hamamatsu Peltier cooling mechanism. When cooled, this PMT has a low dark current (<5 counts per second): this is important for detecting the weak Raman N₂ returns. This PMT has a quantum efficiency of about 12 % at 607 nm and its typical voltage operation is less than 900 V to limit the signal-induced bias associated with the PMT response to an intense luminous pulse. PMT pulses are typically 8 ns in duration and the maximum count rate for a Poisson signal with exponentially distributed inter-arrival times is 45 MHz. An avalanche photodiode has been used for the Raman H₂O channel because of the better quantum detection efficiencies of these detectors at visible wavelengths compared to classical PMTs. In addition, the technology of photodiodes generally offers better overall detection efficiencies in the red and near-infrared parts of the spectrum. The APD model used for the H₂O channel is an EG&G SPCM AQ-232 photodiode. This photodiode is uncooled but has a very low temperature dependence of its characteristics. Its quantum efficiency is about 35 % at 660 nm. Contrary to PMTs, it is not possible to set the supply voltage of the photodiode and it must be noticed that the output of this detector is a standardized logic pulse: a 2 V logic pulse with a temporal length of about 40 ns correspond to each detected photon. The main drawback of this photodiode is its detection surface which is a disc with a diameter of 480 μm: this entails an important sensitivity of the H₂O channel to optical misalignment and also do not ease the alignments of the photodiode. It is essential to use very-low-noise detectors for detecting the very weak water-vapor returns. The maximum count rate for a Poisson signal with exponentially distributed inter-arrival times is 10 MHz.

4 Description of data processing

4.1 Methodology and validation

Raman lidar profiles of water vapor mixing ratio are determined by taking the ratio of Raman backscatter by water vapor to Raman backscatter by one of the well mixed gases such as nitrogen (e.g. Sect. 2.1). In the middle and upper troposphere, aerosols densities are generally small and ice clouds do not exhibit large wavelength attenuation dependence. Though it can be estimated with additional channels (Faduilhe et al., 2005), it has been proved that the relative transmission of the Raman returns, at 607 nm (N_2) and 660 nm (H_2O), corresponds to a 0–5 % overestimation in extreme aerosol loading conditions. Moreover, for altitude above 4 km the vertical gradient of atmospheric differential transmission is small and negligible ($<0.2\% \text{ km}^{-1}$). Consequently, no attenuation corrections have been applied (Sherlock et al., 1999a). Due to the large bandwidth of the interferential filter (1 nm), no temperature dependence corrections have been also applied. The water vapor mixing ratio profiles are obtained by averaging pre-accumulated lidar signals (typically 2 min) over an a-priori period of quasi-stationary conditions regarding statistical variability. To achieve a reasonable compromise between accuracy and atmospheric variability, the applied method consists of adjusting the integration time with the discontinuity of the flow sounded (Hoareau et al., 2009). Under the assumption that two successive profiles give a variability of the same order, they can be considered as independent measurements. In clear sky condition, this Raman lidar system allows to perform measurements of water vapor mixing ratio profiles that extend up to the tropopause region in nighttime conditions.

In 2005–2006, a campaign of CFH (Cryogenic Frost point Hygrometer) measurements was organized at Reunion Island. The CFH is sensor carried under a balloon which measures water vapor continuously between the surface and the middle atmosphere (Vömel et al., 2007). It is based on the chilled mirror principle and measures the temperature of a mirror carrying a thin dew or frost layer, which is maintained in equilibrium with the ambient water vapor. The optical phase sensitive detector measures

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the bulk reflectivity of the mirror and the microprocessor feedback controller regulates the mirror temperature such that the bulk reflectivity and hence the condensate layer remain constant. Under this condition the condensate layer on the mirror is in thermal equilibrium with the vapor phase of the air passing over the mirror. The mirror temperature is then equal to the ambient dew point or frost point temperature and the water vapor mixing ratio and relative humidity can be calculated from this observation using a variation of the Clausius Clapeyron equation. Like many chilled mirror instruments, CFH does not need to be calibrated for water vapor and can be considered as an absolute reference for water vapor measurements. The total uncertainty in frost point is better than 0.5 K throughout the entire profile, which means a mixing ratio uncertainty of about 4 % in the lower tropical troposphere and about 10 % in the middle stratosphere and tropical tropopause (Vömel et al., 2007). In Fig. 3, an intercomparison between H₂O Raman lidar, (CFH) sonde and the European Center for Medium-Range Weather Forecast (ECMWF) operational is shown. The water vapor mixing ratio profile obtained during the descent of the CFH sonde is used here to validate the lidar profile in the upper troposphere. The integration time of the water vapor mixing ratio profile is ~50 min, and the random error of the profile is inferior to 1 % up to ~5 km, reached 10 % from ~12 km and superior to 30 % from ~14 km.

4.2 Calibration

One of the most important issues concerning the water vapor monitoring from Raman lidar technique is the calibration of the instrument (e.g. Sect. 2.1). Even if some procedures of independent calibration as well as calibration using H₂O vertical total column have been explored (Sherlock et al., 1999b; Leblanc et al., 2008; Hoareau et al., 2009), the most commonly approaches consist in the normalization by radiosonde measurements. The lack of simultaneous and collocated radiosonde measurements over the site during the period 2002–2005 does not permit to use them in this first investigation. Consequently, the calibration procedure has been performed using the ECMWF operational water vapor profiles. These data from the archive are re-sampled

on a latitude-longitude resolution grid of 1.125° . Until August 2002, data used are provided on a vertical resolution of 21 pressure levels, after this date, the resolution is defined on 23 levels. To compare and calibrate lidar profiles with ECMWF profiles, relative humidity data provided by ECMWF were converted to water vapor mixing ratio by means of the empirical saturation vapor pressure over liquid water formulas of Hyland and Wexler (1983). Although this calibration method does not appear as the most appropriate method for the long-term commitment, it allows to get a first assessment of the water vapor mixing ratio profiles data set above La Reunion. The results indicate that the calibration coefficient values seem to be quite stable, with an observed mean variance of $\sim 13\%$ on the whole of medians. When a major instrumental change occurs, the mean variance observed in the jump of the coefficient medians can be very important and change by a factor more than 10, as shown in Fig. 4.

5 Preliminary data investigations

5.1 Dataset

During 2002–2005 period, the water vapor Raman lidar system recorded about one hundred measurement nights. The H_2O Raman channel being an additional channel of the existing Rayleigh-Mie lidar system, simultaneous measurements of water vapor and cirrus clouds have been realized. Based on the methodology regarding the integration time period described in Sect. 4.1, around 350 independent water vapor profiles have been obtained over this period with an average of 24 independent water vapor profiles per month. However, as seen in Fig. 5, there are more profiles from February to March and October to November. The reason for this is the duration of nighttime acquisitions that were longer during these periods. This allows to derive more profiles in a same night given the high temporal and spatial variability of water vapor. On average, according to the water vapor variability, the integration time of the water vapor mixing ratio profiles is around 34 min (Fig. 6).

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5.2 Water vapor seasonal cycle

The climatic context of the lidar station at La Reunion is typically that of an oceanic site dominated by the southern Hadley cell circulation (Baldy et al., 1996). Two typical seasons can be identified depending of the position of the Inter Tropical Convergence Zone (ITCZ) with respect to the island location. During the austral winter, the Inter Tropical Convergence Zone (ITCZ) position is distant from the island, and a strong influence of the Hadley and Walker cells generates steady easterly trade winds at low altitudes (<2 km) and westerly winds above the trade wind inversion (Taupin et al., 1999). During austral summer, the ITCZ comes within reach of the island and thus the trade wind influence is weaker. The trade wind inversion is almost likely to disappear during the summer. Water vapor from the marine boundary layer can also be vented to the upper troposphere by intensive deep convection. Relating to these seasons and to these dynamical considerations, an analysis of the water vapor profiles is compared for the moist and dry seasons (Fig. 7). A mean ratio between both seasons about 1.6 up to 9 km is observed, above this altitude the ratio is in mean inferior to 0.4 until 15 km. From 9 km up to 15 km, the water vapor contents have a similar decrease for both seasons with mean values between 0.25 g kg^{-1} at 9 km and 0.02 g kg^{-1} at 15 km.

5.3 Diurnal cycle

Based on water vapor distribution study at several altitudes, results have shown a systematic bimodal distribution in logscale of water vapor in lower layer of the troposphere at all altitudes up to ~ 4 km regarding mean distribution using all data available. However this bimodality in the distribution does not occur for each measurement. From one night to another, the distribution of water vapor mixing ratio can remain in one of the two modes or move from one mode toward another (Fig. 8). This variability seems in connection with the dynamical context of the island which is located in the influence of very regular east-south-easterly trade-wind. A wind inversion resulting from the descending branch of Hadley cell circulation is the main characteristic of the wind vertical

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distribution over Reunion: low-level easterlies are opposite to upper-level westerlies. The transition layer which delimits low-level trade-wind regime below and the upper westerly flow regime above, is known as the trade wind inversion (TWI) which is located between 2 and 5 km (Baray et al., 1998; Taupin et al., 1999). However, more investigations need to be performed for a better interpretation of these results. Steep topography, dynamical influence on the synoptic trade-wind flow and various diurnal thermal effects make complex this analysis. Others results, established from long acquisition measurements during nighttime, suggest that the atmospheric variability of water vapor seems greater than diurnal cycle which allow to keep a measurement protocol during nighttime independently of time (Fig. 9).

5.4 Cirrus clouds analysis

In the upper troposphere, a fraction of the water condenses to generate cirrus clouds. Cirrus clouds are a main uncertainty in climate change assessments (Houghton et al., 2001). They have been identified as one important regulator of the radiation balance of the earth-atmosphere system (Twomey et al., 1991). It is important to investigate the altitude range and vertical extension of cirrus clouds, which are critical parameters for the radiative balance of the atmosphere. A cirrus cloud at high altitudes and, hence, a cold cloud, influences more strongly the infrared flux than the same cirrus at lower altitudes. In contrast, a cirrus cloud at low altitudes has a weaker effect (cirrus cloud reflecting back to space the incoming solar radiation). Currently, the vertical transport of water vapor and ice particles in the vicinity of the tropopause is not perfectly known. The processes involved are debated (Pommereau et al., 2011; Kiemle et al., 2008) and different formation processes could lead to different cloud characteristics that require to be identified before specific statistical analysis (Keckhut et al., 2006). A first climatology of sub-tropical cirrus clouds from Reunion Island lidar dataset for the period 1996–2001 has been already published (Cadet et al., 2003). The updated analysis realized here for the period 2002–2005 is in good agreement with these previous results regarding the cirrus clouds optical depth distribution (Fig. 10). In both cases, the percentages

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have to be associated with the value of lidar ratio equal to 18.2 sr and SVC are defined with an optical depth $\tau \leq 0.03$ (Sassen et al., 1989). However, Cadet et al. (2003) indicated that the cirrus clouds occurred 7 % of the time for the total observation period versus 15 % for the updated analysis. Cirrus occurrence frequency is obtained as the ratio of cirrus detection time versus the total measurement time.

Moreover, complementary analyses have been performed regarding cirrus cloud classification according to geometrical macrophysic properties and some investigations regarding origin have been regarded. The optical thickness of cirrus cloud is calculated in accordance with the scattering ratio profile (SR) using a method as described in Sect. 2.2. In order to identify different cirrus cloud classes, a probability distribution study of diverse parameters of cirrus clouds (optical thickness, top, mean altitude and geometric depth of cirrus cloud) is realized. Results regarding the probability density functions (PDFs) show no single mode Gaussian distribution which suggests possible different types (Fig. 11). To discriminate the different classes, a cluster analysis is performed. The approach consists in applying a Hierarchical Ascendant Classification (HAC). Dissimilarity is calculated using euclidean distance and the Ward's method, described in Ward (1963), is used for the agglomerative clustering method. Classification results indicate clearly three distinct classes. The mean and standard deviation for all parameters of each cirrus class are listed in Table 1. To ensure the robustness of these results, a discriminant factor analysis (DFA) is performed. DFA permits the identification of the optimal set of orthogonal projection axes which best separate the classes; these axes are the discriminant factor. As three classes have been previously identified, the analysis is done according two discriminants axes, F1 and F2. Results show a better discrimination of the different classes regarding the discriminant factor F1 which represents 93.31 % of discrimination (Fig. 12). Other results indicate 99 % of correlation between the discriminant factor F1 and the top of cirrus clouds which seems to be the most important parameter for the discrimination of the classes. DFA corroborates to the HAC results at 98.85 % with only one different affection on 87 observations. A complementary analysis regarding the origin of the different classes is

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realized. Images from geostationary METEOSAT satellite are used in this analysis. During the 2002–2005 period, EUMETSAT (Europe's Meteorological Satellite Organization) was operating the Meteosat 5 satellite providing centered observations over the Indian Ocean (repositioned at 63° E in 1998 for the Indian Ocean Experiment: IN-DOEX). Images used here are from infrared channel in spectral range 10.5–12.5 μm with resolution at nadir of 5 km and observations taken every 30 min. with based on Meteosat images have been investigated. From the images, which have been linked with lidar observations, three types of atmospheric motions have been identified and appear to be associated with the different classes: middle latitude front, tropical convection and tropical cyclone. Among the different cirrus clouds classes obtained, the first one (Class I) is related to a middle latitude front with a top of cirrus cloud located at 11.3 km in mean and an occurrence of 44 %. The Class II and III are related to the tropical cyclone and tropical convection respectively (Fig. 13). For the Class II which is associated to the tropical cyclone, the top of cirrus clouds is located at 15.9 km and represents less of 20 % of occurrence. The mean geometrical thickness of the cirrus clouds belonging to this class is 3 km. The Class III indicates a mean altitude of 14.3 km for the top of cirrus clouds with thickness of cirrus around twice lower than the class II, 1.4 km, and an occurrence of 37 %.

6 Future lidar system

The results presented in the Sect. 5 demonstrate the capabilities of water vapor monitoring in upper troposphere from lidar instrument over a subtropical site. The challenge is now to monitor water vapor with a lidar system able to measure in the upper troposphere with a smaller random error and to reach the lower stratosphere. The future Raman lidar which will be implemented in Piton Maïdo facility at Reunion Island at the end of 2011 is designed to reach UTLS. The station is located above the boundary layer, in the less cloudy part of the island at an altitude of 2200 m a.s.l. The future instrument, under construction, is principally dedicated for the water vapor measurements

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in the lower stratosphere and upper troposphere but also for the measurements of stratospheric temperature using Rayleigh scattering. It will detect light backscattered by molecules and particles in the atmosphere from outgoing laser beam at 355 nm. Inelastic Raman backscatter from nitrogen will be detected at 387 nm. It will allow the direct retrieval of the aerosol extinction coefficient α and will be used to retrieve the water vapor mixing ratio using the channels at 407 nm which will detect vibrational Raman scattering from H₂O molecules.

6.1 Choice of the excitation wavelength

The emitted wavelength was chosen to improve the overall efficiency and is based on several factors: water vapor backscattering cross-section, laser source availability and power, detector efficiency. Molecular scattering follows a λ^{-4} law, therefore short wavelengths are more efficient and the near ultraviolet (UV) band is the most indicated. UV bands allow better detector efficiency than in the visible and near infrared bands. The light source of this lidar consists in two commercial Quanta Ray Pro-290-30 Nd:Yag lasers with frequency tripling, generating laser pulses with about 375 mJ at 355 nm with a repetition rate of 30 Hz and a duration pulse of 9 ns. Pulses of both lasers can be synchronized and output beams can be coupled through polarization cubes to emit 750 mJ pulses at 355 nm. This flexibility will enable a power increase, if needed, to reach UTLS. In the laser coupling and optics design, we also thought about using both lasers emitting at 532 nm for potential intercomparison and if for operational reasons it is decided to change.

6.2 Optical ensemble

Regarding the optical ensemble, the radiation backscattered by the atmosphere is collected by a 1.2 m – diameter telescope that was previously used at Biscarrosse for Rayleigh temperature and Raman measurements (Hauchecorne et al., 1991; Keckhut et al., 1990). A narrow field of view of 1 mrad is used to reduce as little as possible sky

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background and detector noise. Contrary to the lidar system used during the period 2002–2005, the future one will not use optical fibers in the focal plane of the telescope to transfer the backscattered signals to the optical ensemble. This will avoid a systematic bias in water vapor measurements due to fluorescence contribution in fiber-optic cables, even if this transfer protocol permits to obtain constant illumination conditions at the optical fiber output and that even telescope alignment changes. This is not the case in conventional systems (without optical fiber) where optical alignment change can lead to important variations ($\sim 2\text{--}5\%$) in response system, and thus the calibration coefficient (Whiteman et al., 1992; Nedeljkovic et al., 1993). However, even if OH-rich fibers were used for the preliminary system, resulting in a reduction in the estimated fluorescence contribution, the bias introduced by the fiber fluorescence can be significant to be corrected for on a routine basis (Sherlock et al., 1999a). Consequently, we designed a configuration with a direct optical path between the secondary mirror of the receiver and the detection box (Fig. 14).

6.3 Rayleigh-Mie and Raman signals separation

The backscattered signals collected by the telescope are, firstly, transferred toward an optical ensemble through a set of lens and mirrors. A spectral separation of the light is then realized through a set of dichroic beam splitters as well as BPIF. The beam reflected is split by dichroic beam splitter that reflects 532 nm component toward an auxiliary optical ensemble. The filtered beam is then split by another dichroic beam splitter that reflects its 355 nm component toward the photomultiplier of the Rayleigh-Mie channel coupled with a BPIF with a maximum transmission of 55.3 %. The transmitted beam is filtered by an $\alpha - \varepsilon$ high-pass interference filter designed to reject the remaining at 355 nm. This filter has a maximum transmission of 90 % and 85 % at respectively 407 nm and 387 nm. Another dichroic beam splitter is then used to reflect the 387 nm component toward the photomultiplier of the N_2 Raman channel and transmits its 407 nm component toward the photomultiplier of the H_2O Raman channel. A BPIF with a maximum transmission of 63.7 % at 387 nm and a FWHM of 3 nm is placed in

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the front of the N₂ PMT. An $\alpha - \varepsilon$ high-pass interference filter designed to reject the remaining 387 nm component and a BPIF are placed between the last dichroic beam filter and the lens which focalized the beam onto the photocathode of the H₂O PMT. The BPIF has a maximum transmission of 60.6 % at 407 nm and a FWHM of 1 nm. In the case we decided to work in visible wavelengths in the future, the optical subsystem containing the splitters, dichroic mirrors and detectors can be upgraded with a second ensemble adapted to the useful wavelengths. A schematic view of the optical ensemble is shown in Fig. 16.

6.4 Photo detection

Relating to the photon detector, we will use new Hamamatsu R7400- 03 g or 20 g (depending of the wavelengths we will emit) mini-photomultiplier tubes equipped with electronic gating. Since these tubes are less sensitive than cooled R1477, we will have more tests to conduct with different emitted energy per pulse. The PMT are gated ones in order to avoid saturation due to the high level of signal expected at low altitudes. Data acquisition consists in eight Licel PR 10-160P Transient recorders for photon-counting detection. Available TR 20-160 transient recorders for both analog and photon-counting should be used if necessary.

The limiting factor for a PMT in photon counting mode is the dark current. This current that contributes to the noise in the measurements can be used to categorize the limit of detection of a PMT. It can be expressed in term of Equivalent Noise Input (ENI) that is an indication of the photon-limited signal-to-noise ratio. It refers to the amount of light to produce a signal-to-noise of unity in the output of PMT and can be expressed as follows:

$$ENI = \frac{2 \cdot q \cdot I_{db} \cdot G \cdot \Delta f}{S} \quad (3)$$

Where q is the electronic charge, I_{db} is the anode dark current, G is the gain, Δf is the bandwidth of the system and S is the anode radiant sensitivity at the wavelength of peak response.

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Also smaller ENI have been indicated for Hamamatsu R7400-03 compared to Hamamatsu R1477 at wavelengths 355 nm, 387 nm and 407 nm, with respectively a decrease of ~40 %, ~30 % and ~20 % of the ENI values.

6.5 Calibration

Regarding the future calibration of the instrument, coaxial geometry for emission and reception was chosen, as shown in Fig. 15; indeed this design will avoid parallax effect, extend measurement down to the ground and contribute to ease the alignment. It will allow to perform, in better conditions, calibration using H₂O total column measurements from ancillary instruments (GPS, radiometer. . .) as well as comparison on the full height range with radiosonde which could be realized on daily basis at the meteorological station that is 20 km far away. It is important to collocate GPS and radiosonde station. It has been shown that a small spatial separation for the radiosonde and GPS station could bring about a significant PW difference, especially in the region where strong gradients exist (Wang and Zhang, 2008). In the mechanical design, we defined and built an integrated and removable support for a calibration lamp to complement the calibration with total H₂O measurements to use the hybrid technique according to the NDACC future recommendations. Although instrumental changes can be detected following calibration method using radiosondes, those using calibration from lamp or passive zenith daytime observations are better. It is therefore important to implement one of these methods for the instrument monitoring, which is necessary for long term monitoring.

6.6 Numerical evaluation of lidar signals

Numerical simulations of lidar signals can be performed for studying the expected system capability. The range interval for which a lidar can be operational is limited by the geometrical form factor function and saturation in the lower altitude and the fast decreasing signal-to-noise ratio (SNR) at far altitude range. For a first performance

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simulation, we suppose the R7400-03 Hamamatsu PMT with a typical dark count rate of 80 s^{-1} to evaluate the detector noise contribution compared to sky background in measurements. The quantum efficiency of the R7400-03 PMT is around 22 % for 407 nm wavelength. Based on these component properties and H₂O channel efficiency (Table 2), simple numerical simulation of the system performance has been performed and compared to the previous system which used SPCM AQ-232 APD for H₂O channel.

For measurements at a given emitted wavelength λ_0 , the lidar signal $N(\lambda_H, z)$ in photon counts, corresponding to the range z , can be calculated by the following equation:

$$N(\lambda_H, z) = \frac{K}{z^2} \cdot n_H(z) \cdot \frac{d\sigma_H(\pi)}{d\Omega} \cdot e^{(-\int_0^z \alpha(\lambda_0 z') dz' + \int_0^z \alpha(\lambda_H, z') dz')} + N_0 + N_D \quad (4)$$

Where K is a proportionality constant for H₂O channel that accounts for the system optical efficiency, the telescope receiver area, the photomultiplier tube (PMT) spectral efficiency, the overlap function and the laser output energy; $d\sigma_H(\pi)/d\Omega$ is the Raman backscattering cross section for H₂O molecule; $n_H(z)$ is the H₂O number density; the exponential factor gives the two-way atmospheric transmission, where α is the total extinction coefficient; N_0 is the sky background and N_D represents the detector dark counts.

The background term can be evaluated as follows:

$$N_0 = \eta_0 \cdot \eta_q \cdot \frac{\lambda_H}{h \cdot c} \cdot W \cdot A \cdot f \cdot \Delta t \cdot \Delta \lambda_H \cdot \frac{2\Delta R}{c} \cdot \Omega \quad (5)$$

Where W is the background radiance, $\Delta \lambda_H$ is the receiver bandwidth, and Ω is the observation solid angle. And the dark count rate, expressed in function of d (s^{-1}), can be estimated as follows:

$$N_D = \frac{2f}{c} \cdot d \cdot \Delta R \cdot \Delta t \quad (6)$$

To perform the numerical simulations, water vapor mixing ratio profiles from ECMWF ERA-40 re-analysis is used as reference profile, and the atmospheric profile has been

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derived taking account extinction due to Rayleigh scattering. Rayleigh scattering profiles have been computed using International Standard Atmosphere. Absorption by ozone and other trace gases is negligible at the wavelengths used and the extinction due to aerosol do not have been considered due to altitude station (2200 m). Due to the large bandwidth of the interferential filter (1 nm), no temperature dependence corrections have performed. Based on measurements to the 15 March 2005 for the current system, the detector noise (N_D) to sky background (N_0) ratio has been shown of around 2. The derived night sky radiance of $4.6 \cdot 10^{-9} \text{ W m}^{-2} \text{ sr}^{-1} \text{ nm}^{-1}$ is in agreement to the night sky radiance range values indicated in literature at return wavelength and similar weather conditions (Höhn and Büchtemann, 1973; Turnrose, 1974). Höhn and Büchtemann (1973) measured the sky brightness from 400 to 800 nm in a range of weather conditions and under various aspects both experimentally and theoretically. We chose their spectrum to estimate night sky radiance and perform the numerical simulations for the future lidar system (Table 3). Usually to reduce the statistical noise, in addition to the temporal integration and to extend the altitude range in the upper troposphere, vertical integration is applied. In the numerical simulations, only temporal integration has been regarded according to mean time integration (~ 30 min) which corresponds to the mean time integration to access water vapor variability, as described in Sect. 5.1.

Simulations indicate a ratio of ~ 150 at lower altitude (~ 3 km) with a decrease to ~ 20 around the tropopause (~ 16 km) between both lidar systems for Raman H_2O channel for one laser in operation at 355 nm (Fig. 17). This ratio decrease is essentially due to the altitude squared dependence in return signal. Although performances improvement are the result of the emission wavelength which implies a greater backscattering of molecules at return wavelength, the receiver area and detection efficiency, the altitude of the station permits to improve the backscattered power principally in lower altitude since the factor is ~ 11 at ~ 3 km and decreases to ~ 1.3 at ~ 16 km. In this development stage, the altitude expected within an error of 15 % for H_2O measurements, regarding random error (principally sky background and photon counting error) and a

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pre-accumulated signal of 30 min, is of ~ 15.6 km in clear sky and moonless condition and ~ 14.9 km with thinly covered sky and moonlit. For the same measuring conditions, random error reaches 30 %, respectively at around ~ 17.8 km and ~ 16.1 km. Coupling both lasers, the altitude expected within an error of 15 % are 16.8 km and 15.8 km respectively for clear sky and moonless condition.

Concerning the actual system, simulation results have been compared to the experimental measurements. Comparison indicated a ratio of ~ 4 for H_2O channel between the expected results from simulation and those from the instrument. And regarding the numerical simulation, the expected altitude for a random error at 15 % and 30 % is respectively around 11.8 km and 13 km in clear sky and moonless conditions.

7 Conclusions

We have presented preliminary data of water in upper troposphere from lidar instrument over a subtropical site. Performing analysis of the preliminary system lidar dataset, advantages and drawbacks have been pointed out. Present configuration of the lidar system permits to cover a large altitude range, from the ground up to the upper troposphere (~ 14 – 15 km) within a random error of 30 % for a temporal integration of ~ 50 min during nighttime and presence of any clouds. Regarding statistical analysis, some results based around 350 independent water vapor profiles have been presented. Mean vertical profiles of water vapor in respect to the seasons have shown a mean ratio of 1.6 up to 9 km. This ratio decreases within 0.4 in mean between both seasons above 9 km up to 15 km. Concerning analysis established from long acquisition measurements during nighttime, results suggest that the atmospheric variability of water vapor seems greater than diurnal cycle. Temporal series of the water vapor content showing no significant evolution according to long acquisition measurements, this allow to keep a measurement protocol during nighttime independently of time. About cirrus cloud analysis, according to different parameters of cirrus clouds, 3 distinct

classes have been obtained. Following to these different classes and complementary analysis based on Meteosat images, origin of the classes have been identified and related to the tropical convection (class III), tropical cyclone (class II) and midlatitude front (class I); with respectively 37 %, 19 % and 44 % of occurrence. The most discriminatory parameter associated to the classification seems to be the top of the cirrus cloud. These altitudes have been demonstrated at 11.3 km for the first class I, 15.9 km for the second, and 14.3 km for the third. Although these analyses have shown good results regarding water vapor and cirrus data, some aspects needed to be resolved in order to improve the measurements from the future lidar system. Based on these analyses and encountered difficulties to derive water vapor mixing ratio profiles, the characteristics and the future design of the instrument deployed to the Maïdo station has been presented. According to a simple numerical simulation of the system performance the results have shown a ratio of 4 for H₂O channel between theoretical curves and instrumental measurements with one laser in operation. The maximum altitude expected, taking account to a random error within 15 % and pre-accumulated signal of 30 min, has been indicated at 11.8 km for H₂O channel in clear sky and moonless condition. Based on characteristics and design of the future lidar system, and regarding the numerical simulation of both systems, the performances seem to be improved by a factor 20 for H₂O channel around 16 km. The improvements of these performances are principally due to a better detection efficiency of the optical ensemble and backscattering cross-section at shorter wavelength, the size of the telescope and the altitude of the new observatory (2200 m a.s.l) which permit to improve the backscatter power of a ratio ~150 at ~3 km. Concerning the design of the future instrument, some modifications have been chosen compared to the preliminary system in order to avoid systematic bias in water measurements removing the optical fiber and to facilitate the calibration choosing coaxial emission. Consequently, with an expected altitude of ~15.6 km for H₂O channel, within a random error of 15 % and a temporal integration of 30 min, and regarding the characteristics and the design of the future lidar system and different calibration aspects, this lidar could be suitable for long-term monitoring of water in the

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upper troposphere – lower stratosphere. The future system will allow us to provide data for the validation of present satellite experiences like AURA-MLS, AQUA-AIRS or future like the Indian-French project MEGHA TROPIQUES which launching is scheduled at the end of 2011 and which will host the instruments SAPHIR (micro-wave radiometer).

- 5 Flexibility in the design (emitted power, wavelengths, calibration techniques. . .) will enable to improve the performances of this instrument on the long-term to fully reach on operational system in the tropic for water vapor monitoring up to the low stratosphere.

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Table 1. Characteristics of the three cirrus classes.

Class type	I. Midtroposphere thin cirrus	II. Thick upper troposphere cirrus	III. Upper troposphere thin cirrus
Occurrence (%)	44	19	37
Mean altitude (km)	10.3 ± 0.9	14.3 ± 0.6	13.6 ± 0.6
Thickness (km)	2 ± 1.1	3 ± 0.7	1.4 ± 0.5
Optical depth	0.04 ± 0.04	0.09 ± 0.06	0.02 ± 0.02
Top altitude (km)	11.3 ± 0.8	15.9 ± 0.4	14.3 ± 0.6

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Table 2. System Parameters for H₂O channel for the actual and future lidar system.

System Parameter	Parameter Value	
	Actual lidar	Future lidar
Received wavelengths	660.5 nm	407.5 nm
Filter Bandwidth	1 nm	1 nm
Filter transmission	0.14	0.39
Detector	EG&G SPCM AQ-232 photodiode	R7400-03 Hamamatsu photomultiplier
Quantum Efficiency	0.35	0.22
Total H ₂ O channel efficiency	3.2 %	7.6 %

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Table 3. Sky Spectral Radiance for different weather conditions and corresponding sky background for the H₂O channel future lidar system (integration time of 30 min is considered).

Reference	λ [nm]	Period	L_{λ} [$\text{W m}^{-2} \cdot \text{sr}^{-1} \cdot \text{nm}^{-1}$]	N_0	N_0/N_D
Höhn and Büchtemann (1973)	400	Night ^{1,2}	$3.4 \cdot 10^{-9}$	5.6	1.3
Höhn and Büchtemann (1973)	400	Night ³	$1.9 \cdot 10^{-8}$	31.2	7.3
Höhn and Büchtemann (1973)	400	Night ⁴	$5 \cdot 10^{-8}$	82	19.0

¹ Clear sky (moonless), ² Thinly covered sky, haze or thin fog (moonless) ³ Clear sky (moonlit), ⁴ Thinly covered sky, haze or thin fog (moonlit) The typical dark count rate of R7400-03 Hamamatsu photomultiplier $d = 80 \text{ s}^{-1}$ is used. N_0 and N_D are, respectively, the night sky background and the detector noise (in photon).

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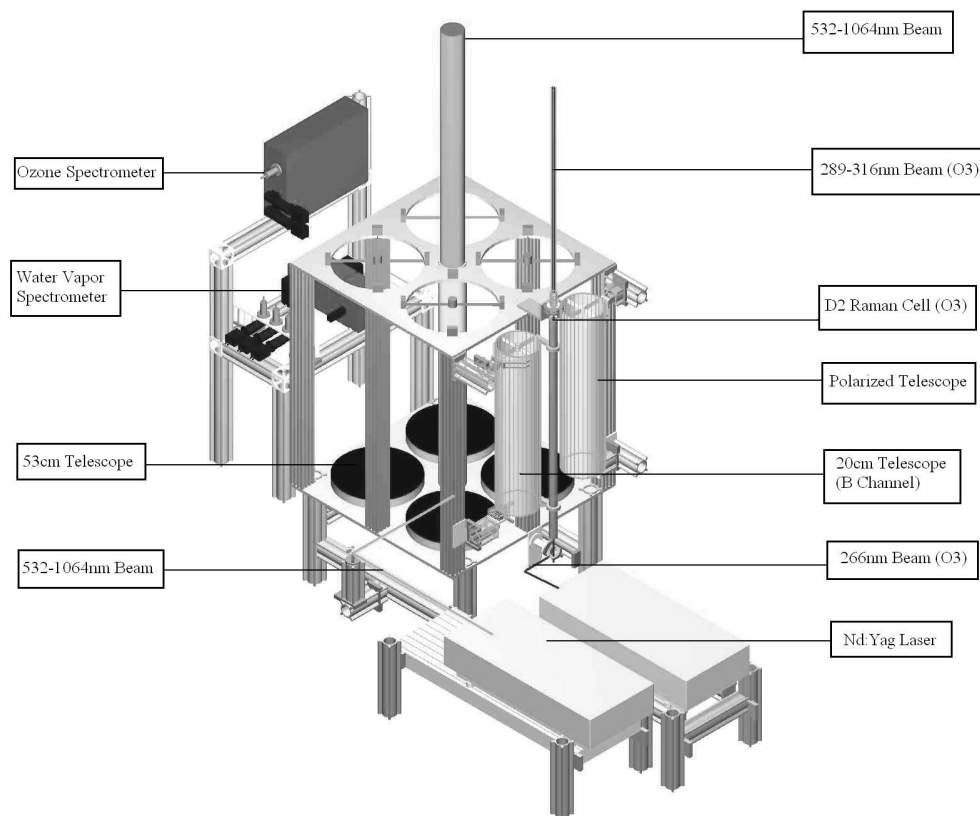


Fig. 1. Representation of the lidar instrument at Reunion Island university during the 2002–2005 period.

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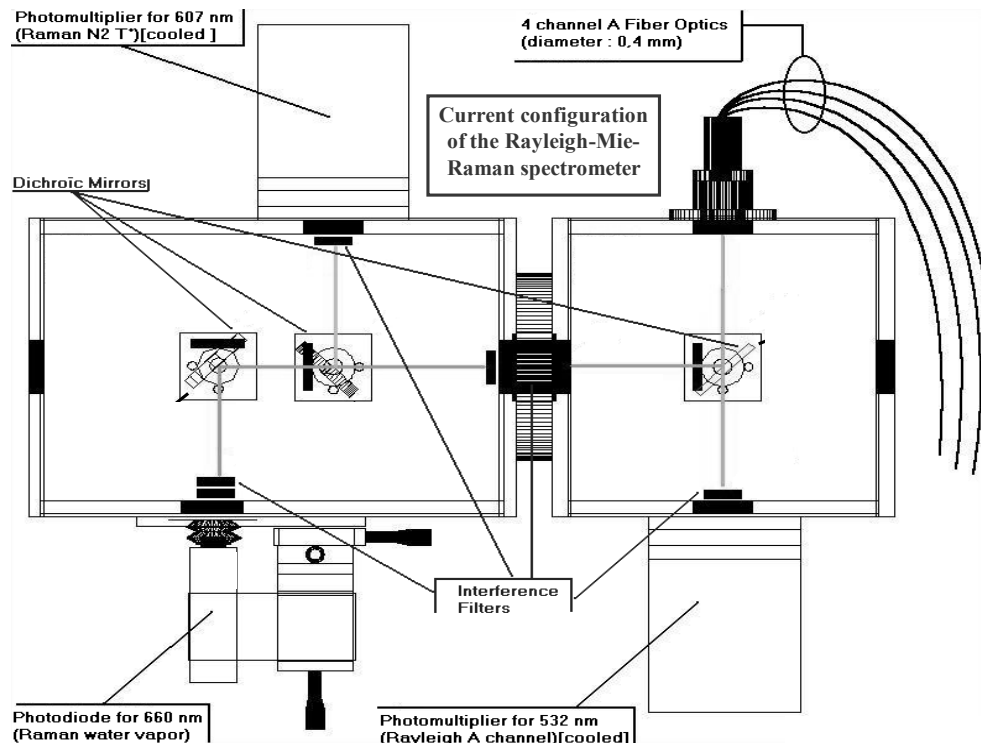


Fig. 2. Schematic representation of the current configuration of the Rayleigh-Mie-Raman spectrometer of the preliminary lidar system.

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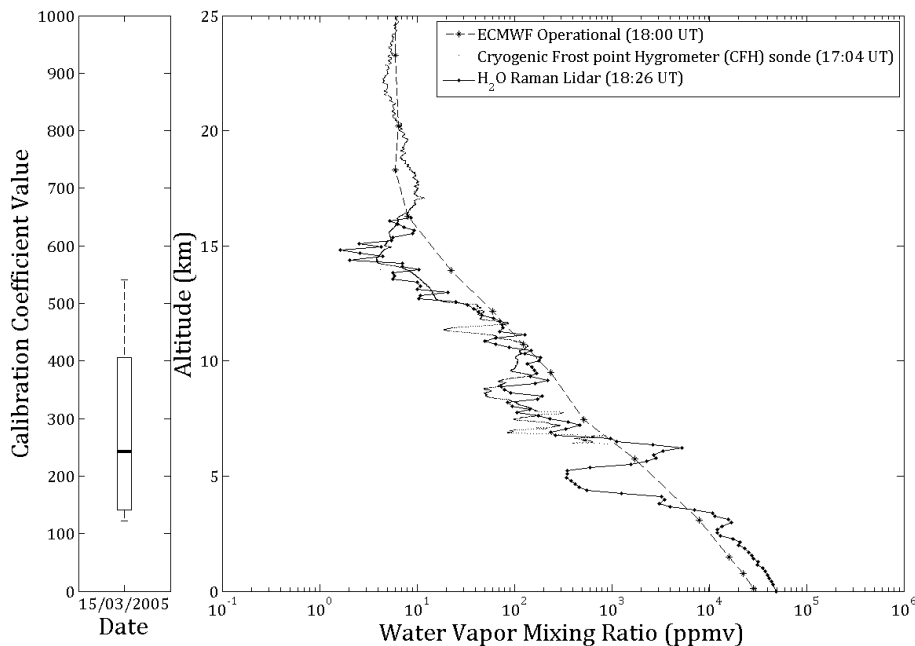


Fig. 3. Intercomparison between H₂O Raman lidar, Cryogenic Frost point Hygrometer (CFH) sonde and ECMWF operational analysis on 15 March 2005. The calibration coefficient and his error are shown on the left. Calibration has been realized using ECMWF Operational data before comparison with CFH.

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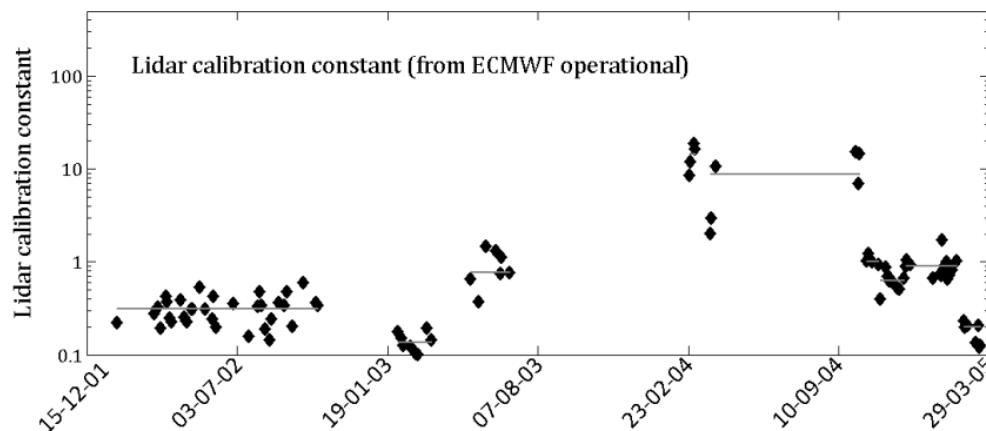
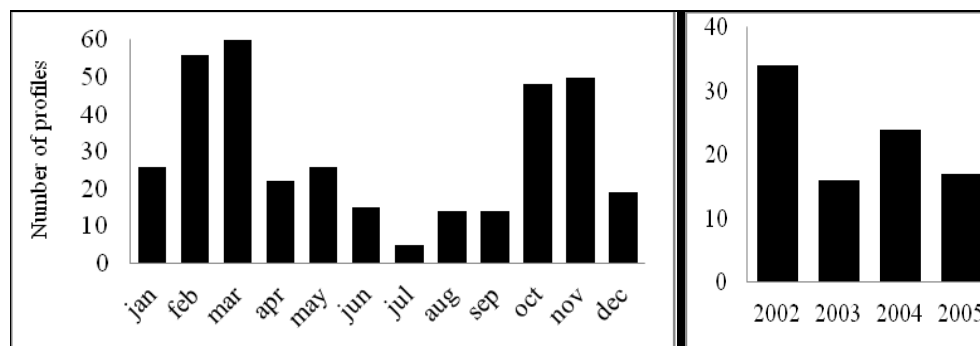


Fig. 4. Time evolution of the actual lidar calibration constant over the period 2002–2005. The horizontal grey lines represent the median of these coefficients.

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**Fig. 5.** Dataset histogram over the period 2002–2005.

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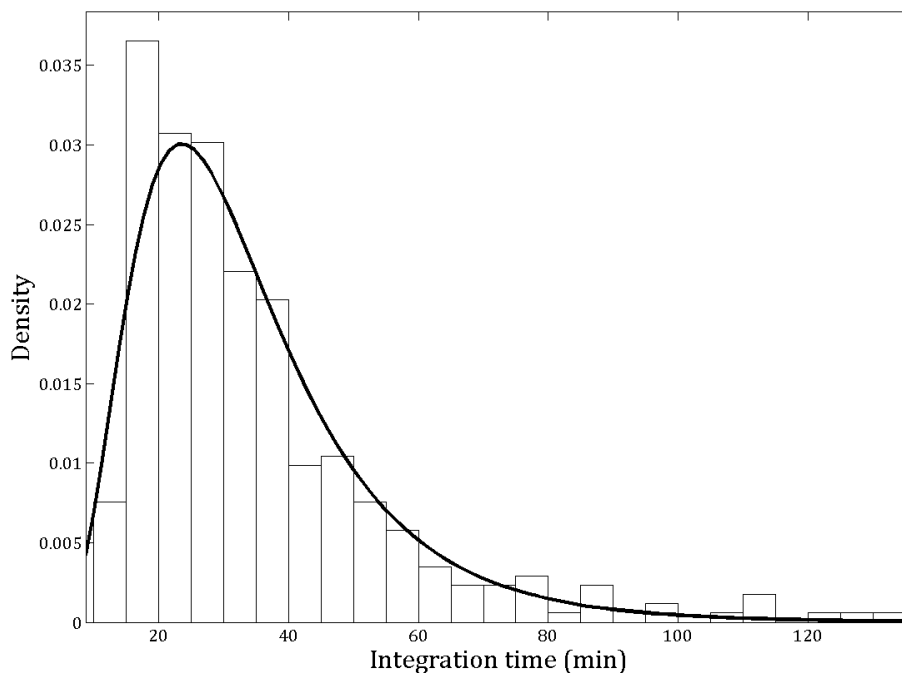


Fig. 6. Integration time distribution of the vertical profiles of water vapor mixing ratio. The bold black line represents a log-normal fit of the distribution which represents an adequate approximation of the histogram.

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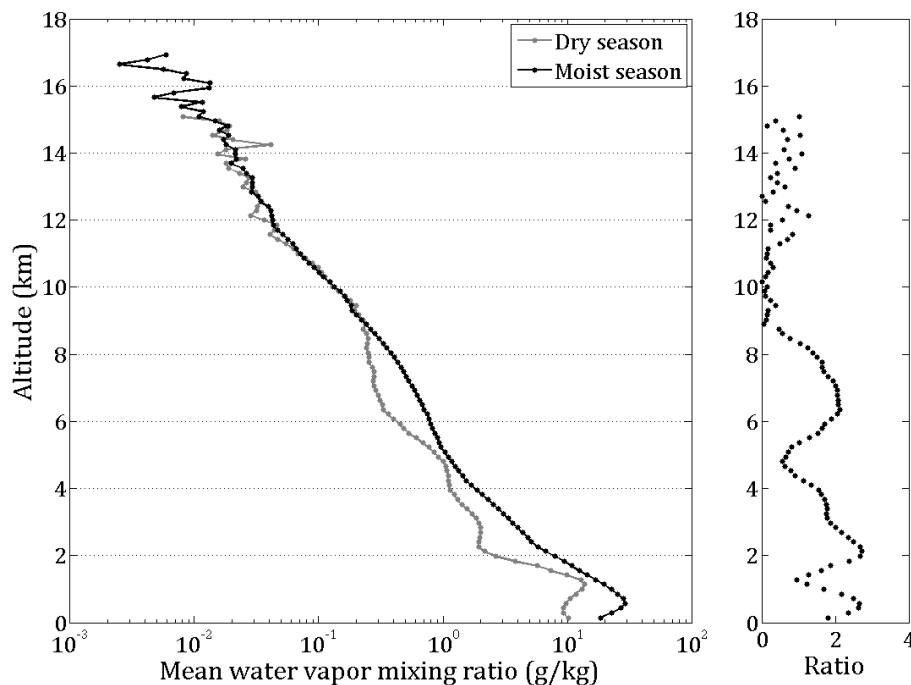


Fig. 7. Mean water vapor mixing ratio vertical profiles during the period 2002–2005 regarding the moist and dry season (right panel) and relative difference between the seasons (left panel)

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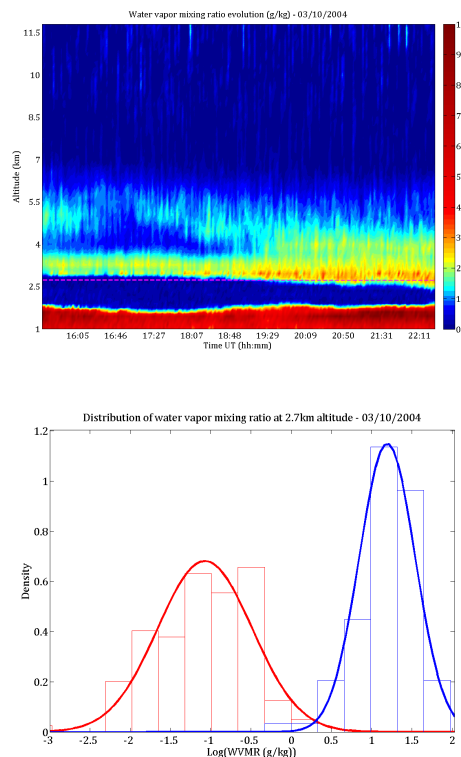


Fig. 8. Evolution of water vapor mixing ratio to 3 October 2004 (top panel). Pink dotted line represents an example of location (here at 2.7 km altitude) where the distribution of water vapor are bimodal (bottom panel). On the right panel, red line represents the water vapor distribution before 19:30 UTC and the blue line the distribution after 19:30 UTC.

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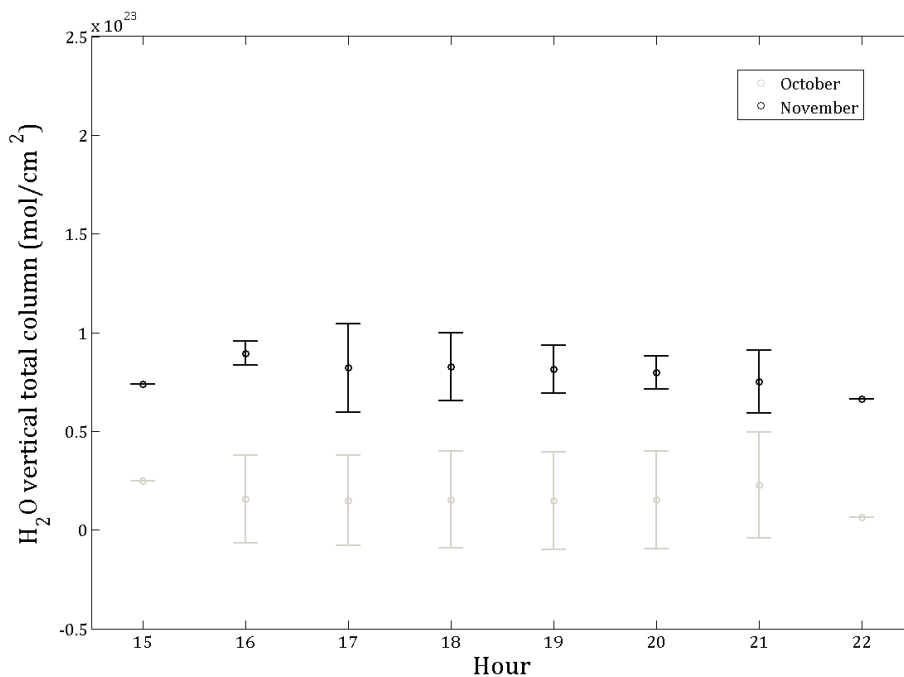


Fig. 9. Mean evolution of the H₂O vertical total column content for October and November 2005. The grey dots represent the mean evolution of the H₂O total column during long night acquisitions for October 2005 and the black dots for November 2005. The vertical bars represent the standard deviation.

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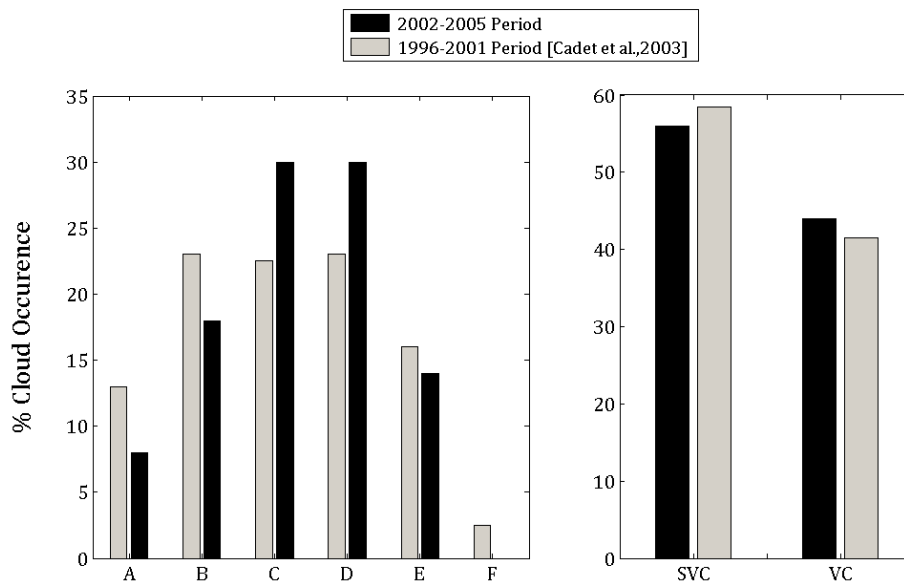


Fig. 10. Histograms of cirrus optical thickness binned on a log scale. Lettering along the abscissa (left panel) corresponds to the following optical thickness intervals: A = (0.001–0.003), B = (0.003–0.01), C = (0.01–0.03), D = (0.03–0.1), E = (0.1–0.3), F = (0.3–1.0). The right panel shows the combined results according to subvisible cirrus (SVC) and visible cirrus (VC). Categories A–C comprises the SVC component and D–F comprises the VC component.

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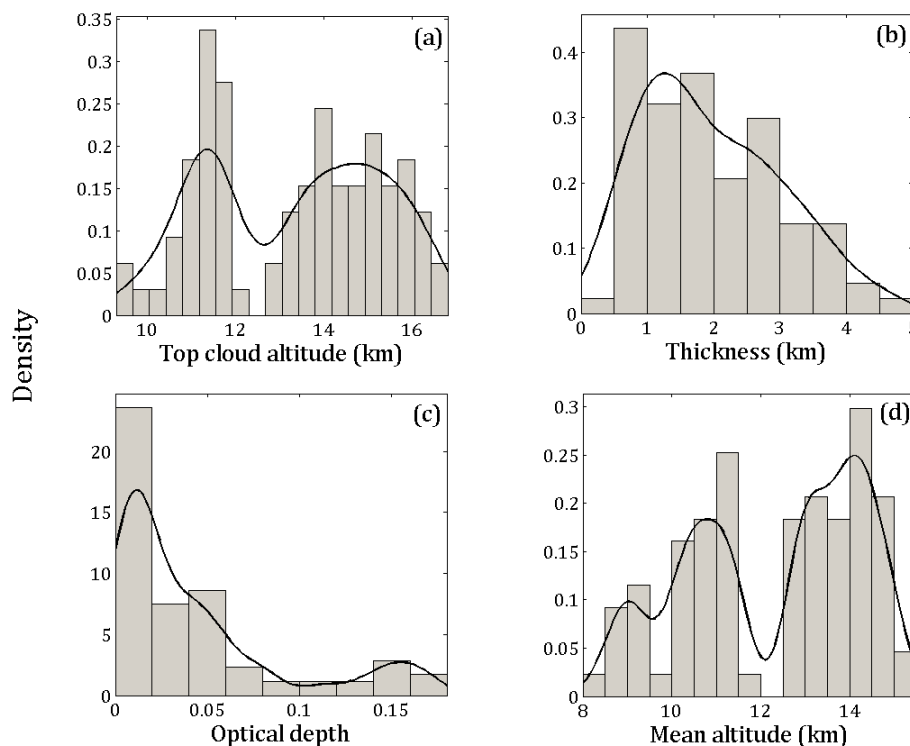


Fig. 11. Probability Density Function (PDF) of the different characteristics of cirrus clouds observed at Reunion Island over the period 2002–2005. The panels (a), (b), (c) and (d) represent respectively the top of cirrus clouds, geometrical thickness, the optical depth and the mean altitude.

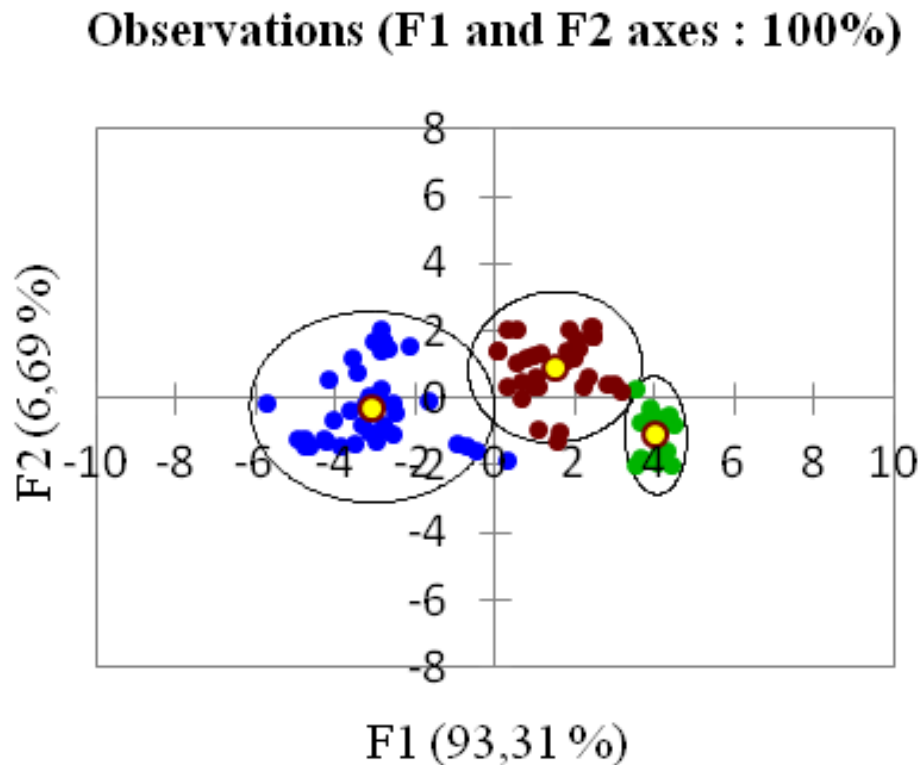


Fig. 12. Virtual representation of the observations on discriminated axis showing the different classes. Circles represent different identified classes with a confidence interval of 5%. Blue dots represent the first class (midtroposphere thin cirrus), red dots represent the second one (thick upper troposphere cirrus) and the green dots represent the third class (upper troposphere thin cirrus).

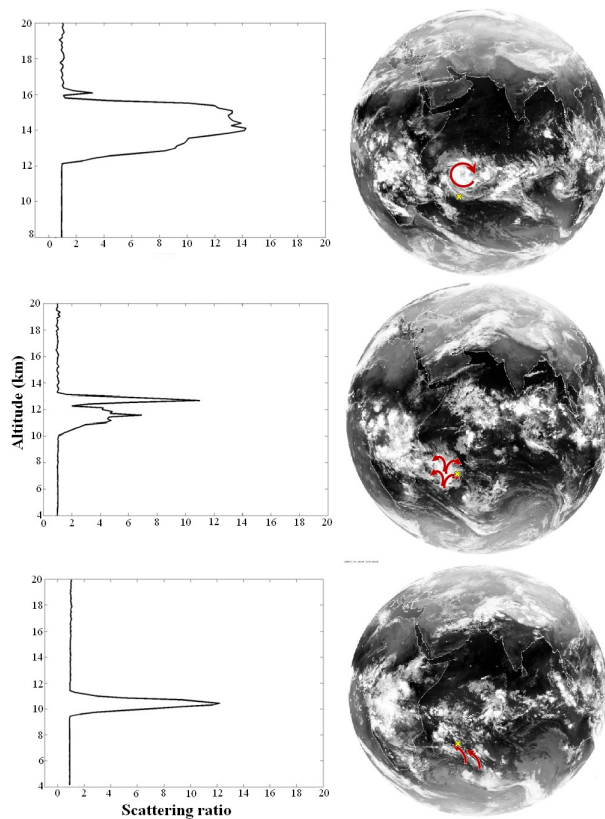


Fig. 13. Representation of different cirrus cloud classes. Left panels represent the scattering ratio profiles for each class and right panels represent the corresponding MeteoSat image. Reunion Island is indicated by yellow cross. Atmospheric move is represented by red arrows. The corresponding dates are 16 March 2005, 15 December 2004 and 9 February 2003 (from the top to the bottom).

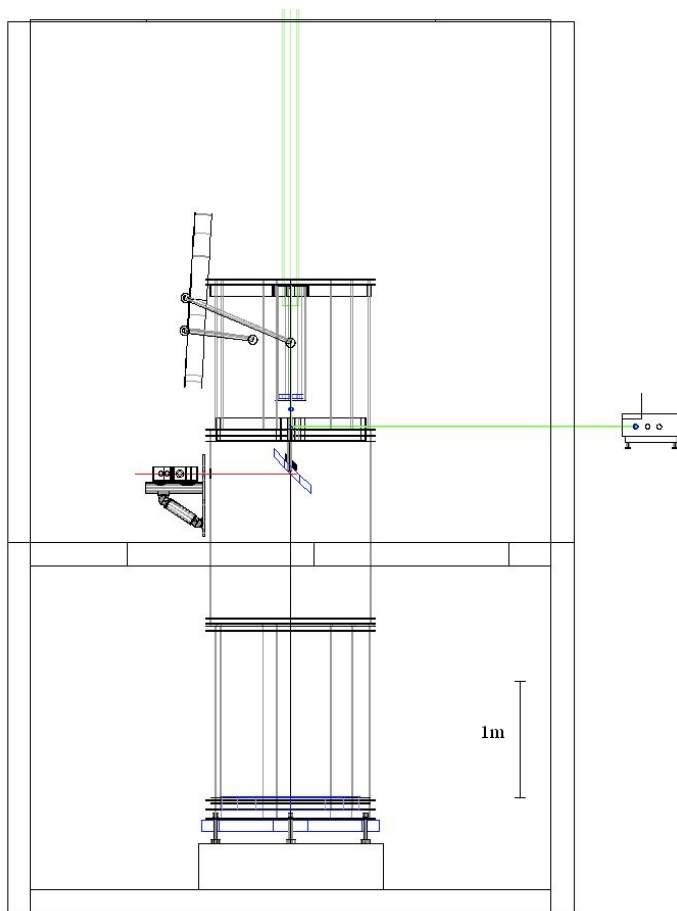


Fig. 14. Configuration with a direct optical path between the secondary mirror of the receiver and the detection box.

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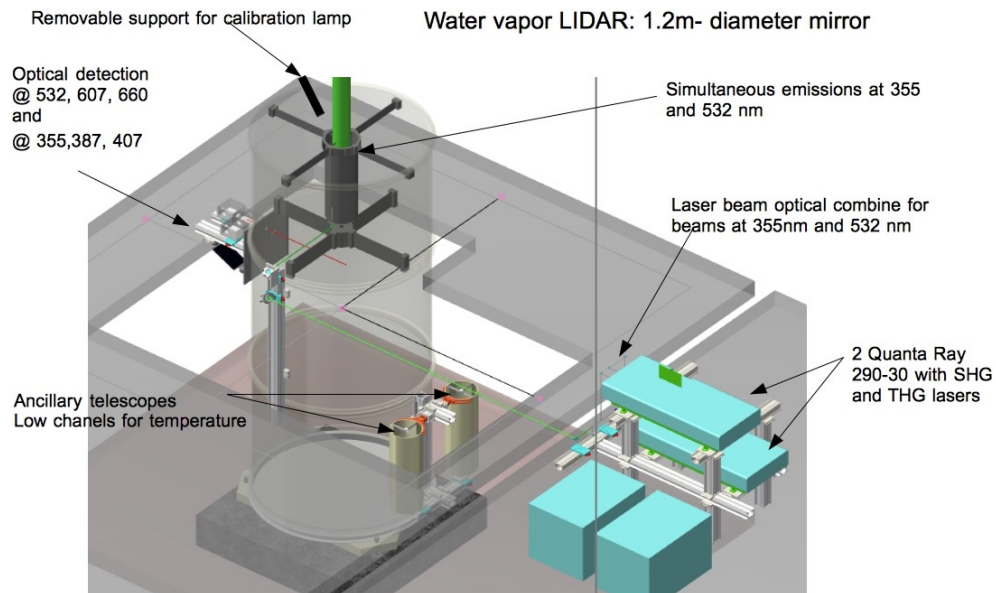


Fig. 15. Representation of the design of the future lidar implemented at the Reunion Island altitude observatory.

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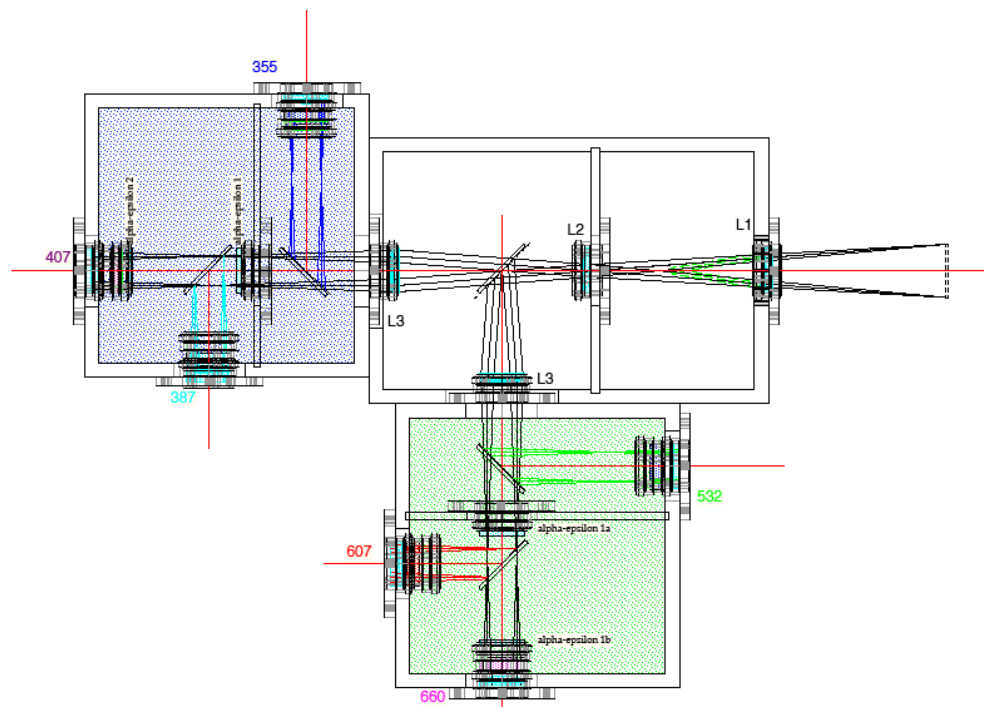


Fig. 16. Schematic view of the optical ensemble of the future lidar implemented at Observatoire de Physique de l'Atmosphère de La Réunion (OPAR).

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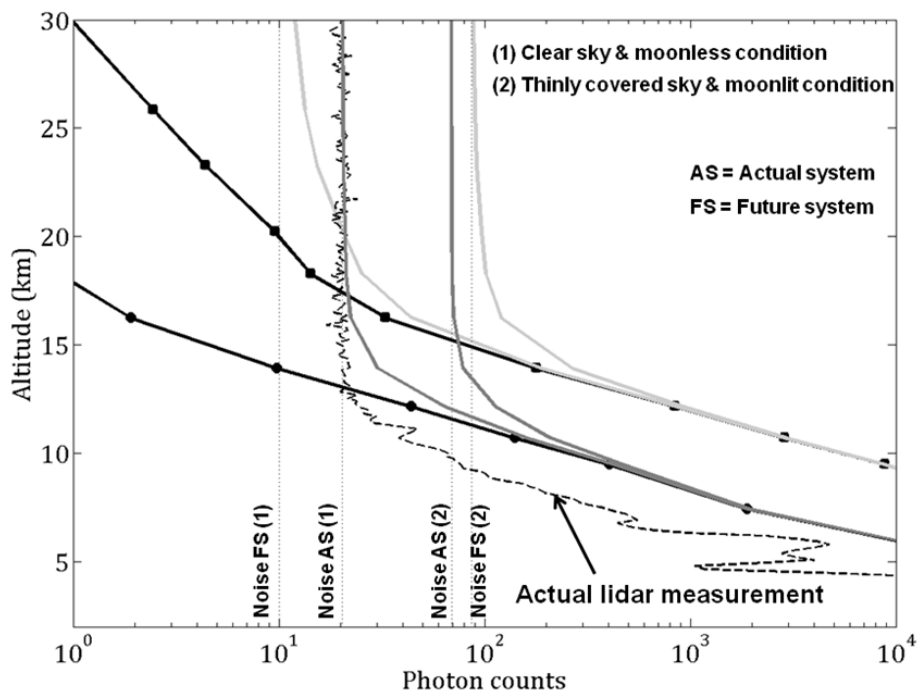


Fig. 17. Raman H_2O backscattered signal comparison (30 min time integration). The bold black line with dots corresponds to the numerical simulation regarding the current lidar system and the bold black line with square for the future one with one laser. The grey lines correspond to the numerical simulation + noise (sky background and detector noise) following different weather conditions: dark grey lines for the actual system and light grey lines for the future system. Weather conditions are indicated on the figure.

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