



## Abstract

The sensible heat flux ( $H$ ) is a significant component of the surface energy balance (SEB). Sonic anemometers simultaneously measure the turbulent fluctuations of vertical wind ( $w'$ ) and sonic temperature ( $T'_s$ ), and are commonly used to measure  $H$ . Our study examines 30-min heat fluxes measured with a Campbell Scientific model CSAT3 sonic anemometer above a subalpine forest. We compare  $H$  calculated with  $T_s$  to  $H$  calculated with a co-located thermocouple and find that for horizontal wind speed ( $U$ ) less than  $8 \text{ m s}^{-1}$  the agreement is  $\approx \pm 30 \text{ W m}^{-2}$ . However, for  $U > \approx 8 \text{ m s}^{-1}$ , the CSAT3  $H$  becomes larger than  $H$  calculated with the thermocouple, reaching a maximum difference of  $\approx 250 \text{ W m}^{-2}$  at  $U \approx 18 \text{ m s}^{-1}$ .  $H$  calculated with the thermocouple results in a SEB that is relatively independent of  $U$  at high wind speeds. In contrast, the SEB calculated with  $H$  from the CSAT3 varies considerably with  $U$ , particularly at night. Cospectral analysis of  $\overline{w'T'_s}$  suggest that spurious correlation is a problem during high winds which leads to a positive (additive) increase in  $H$  calculated with the CSAT3. At night, when  $H$  is typically negative, this CSAT3 error results in a measured  $H$  that falsely approaches zero or even becomes positive. Within a broader context, the usefulness of side-by-side instrument comparisons are discussed.

## 1 Introduction

Sonic anemometers have been used to measure three-dimensional wind vectors, temperature, and surface sensible heat and momentum fluxes since the early 1960s. They have played a pivotal role in studying the surface energy balance (SEB), which describes how the radiative energy at the earth's surface is partitioned between latent heat flux (evaporation and transpiration of water to the atmosphere) and sensible heat flux (heat exchange between the surface elements, ground, and atmosphere) (Stewart and Thom, 1973; Garratt, 1992; Blanken et al., 1997; Oncley et al., 2007; Foken, 2008). Despite improvements in instrumentation accuracy, most flux-measuring sites

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find that the measured sensible and latent heat fluxes only account for  $\approx 80\%$  of the available incoming energy (Wilson et al., 2002; Foken, 2008). The so-called “energy balance closure problem” has recently been reviewed (Foken, 2008; Foken et al., 2011) and the conclusion was reached that the imbalance can be mostly attributed to low-frequency flux contributions from heterogenous landscapes which are not measured by eddy-covariance techniques. The energy balance closure typically improves under windy/turbulent conditions when the ground and atmosphere are “well-coupled” (Franssen et al., 2010). Spatially homogeneous and moisture-limited environments such as deserts appear to be optimal for successfully closing the energy budget (Timouk et al., 2009; Foken, 2008).

This paper uses data from the Niwot Ridge Subalpine Forest AmeriFlux site (NWT) to examine the sensible heat flux with strong winds. Turnipseed et al. (2002) studied the energy balance at the NWT site and found that during the daytime the sum of the turbulent fluxes accounts for 80–90% of the radiative energy input into the forest. At night, under moderately turbulent conditions, the energy balance closure is comparable to the daytime. However, when the nighttime conditions are either calm or extremely turbulent, the sensible and latent heat fluxes only account for 20–60% of the net long-wave radiative flux. Turnipseed et al. (2002) discussed several possible reasons for this nighttime discrepancy (e.g., instrument error, footprint mis-match, horizontal advection), but none of these reasons could adequately explain the fact that the nighttime imbalance persisted in the presence of strong winds. They concluded that the sonic temperature did not have sufficient resolution to capture the small temperature fluctuations which led to inaccurate sensible heat fluxes.

In early 2008 the sonic anemometers at NWT were re-calibrated (details in Sect. 2.3). After the recalibration, the new sensible heat flux still did not improve the agreement between the daytime and nocturnal energy balance in windy conditions, and the imbalance was even more dramatic than before the re-calibration. The goals of the current study are to: (1) describe the discrepancy observed in the calculated sensible heat flux, (2) compare the sensible heat flux calculated using sonic temperature to that calculated

with a co-located thermocouple, and (3) re-visit the surface energy balance results from Turnipseed et al. (2002) in light of the results from item (2).

## 2 Data and methods

### 2.1 Site description

5 This study uses data from the Niwot Ridge Subalpine Forest AmeriFlux site (40°1'58" N, 105°32'47" W, 3050 m elevation, data version 2011.04.20). The site is located below Niwot Ridge, Colorado, 8 km east of the Continental Divide. The NWT measurements started in November 1998 as described in Monson et al. (2002) and Turnipseed et al. (2002, 2003). The tree density around the NWT Tower is  $\approx 0.4$  trees  $\text{m}^{-2}$  with  
10 a leaf area index (LAI) of  $3.8\text{--}4.2 \text{ m}^2 \text{ m}^{-2}$  and tree heights of 12–13 m (Turnipseed et al., 2002). In winter, NWT is a windy place. Between November–February, the 30-min average 21.5 m wind speed ( $U$ ) is around  $7 \text{ m s}^{-1}$  (standard deviation  $\approx 4.5 \text{ m s}^{-1}$ ) with a maximum  $U$  near  $20 \text{ m s}^{-1}$ . More information on NWT is available on-line at <http://public.ornl.gov/ameriflux/>.

### 15 2.2 Sonic anemometer thermometry

A few of the important relationships related to sonic anemometer thermometry are summarized here; a more complete description of the technology is readily available (e.g., Kaimal and Businger, 1963; Schotanus et al., 1983; Kaimal and Gaynor, 1991; Loescher et al., 2005, and many others).

20 A sonic anemometer-thermometer calculates air temperature ( $T$ ) by measuring the speed of sound ( $c$ ). The relationship between air temperature, the speed of sound, and specific humidity ( $q$ ) within the atmosphere is well-known,

$$T = \frac{c^2}{\gamma_d R_d} \left( \frac{1}{1 + 0.51q} \right), \quad (1)$$

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where  $\gamma_d = c_p/c_v = 1.4$  is the dry air specific heat ratio and  $R_d$  is the gas constant for dry air ( $287.04 \text{ J kg}^{-1} \text{ K}^{-1}$ ).

A sonic anemometer-thermometer sequentially transmits and receives sound pulses between two transducers separated by a path-length distance ( $d$ ). The sonic temperature ( $T_s$ ) is determined from the measured times to transit  $d$  ( $t_1$  in one direction and  $t_2$  in the opposite direction) and the geometry of the sound rays such that,

$$T_s \equiv \frac{c^2}{\gamma_d R_d} = \frac{1}{\gamma_d R_d} \left[ \left( \frac{d}{2} \right)^2 \left( \frac{1}{t_1} + \frac{1}{t_2} \right)^2 + V_n^2 \right], \quad (2)$$

where  $V_n$  is the wind component perpendicular to  $d$  (i.e., cross-wind). Equation (2) is for dry air.

In a real atmosphere (i.e., one with water vapor), air temperature is calculated from  $T_s$  as  $T_s^{\text{air}} = T_s (1 + 0.51q)^{-1}$ . If the measured variables are decomposed into mean and fluctuating components (e.g.,  $T = \bar{T} + T'$ , etc., see Schotanus et al., 1983), then the sensible heat flux  $H$  is calculated with,

$$H = \rho c_p \overline{w'T'} = \rho c_p \left[ \overline{w'T'_s} - 0.51 \bar{T} \overline{w'q'} + 2 \frac{\bar{T} \bar{u}}{c^2} \overline{u'w'} \right], \quad (3)$$

where  $\rho$  is the air density,  $c_p$  is the specific heat of air at constant pressure, and  $u$  and  $w$  are the horizontal and vertical wind components in streamwise coordinates. The  $\overline{u'w'}$  term is the so-called cross-wind correction term and most modern sonic anemometers take this into account with internal processing software (Loescher et al., 2005; Campbell Scientific, 2011).

### 2.3 Energy balance equation and instrumentation

The terms in the surface energy balance are,

$$R_a = R_{\text{net}} - G - S_{\text{canopy}} - S_{\text{soil}} = H + LE, \quad (4)$$

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where  $R_a$  is the “available energy”. At NWT, net radiation ( $R_{\text{net}}$ ) was measured at  $z \approx 25$  m above the ground with both a net (Radiation and Energy Balance Systems – REBS, model Q\*7.1) and four-component (Kipp and Zonen, model CNR-1) radiometer. The soil heat flux ( $G$ ) was measured with multiple soil heat flux plates (REBS, Model HFT-1) at a depth of  $-10$  cm. The two storage terms ( $S_{\text{canopy}}$  and  $S_{\text{soil}}$ ) account for the heat stored between the ground and the flux measurement heights, and are typically less than 10 % of  $R_{\text{net}}$  (Oncley et al., 2007). At NWT, Turnipseed et al. (2002) showed that the storage terms and  $G$  were small (less than 8 % of  $R_{\text{net}}$ ) and we neglect  $S_{\text{canopy}}$  and  $S_{\text{soil}}$  for this study.

Latent heat flux ( $LE$ ), and  $H$  were measured at  $z \approx 21.5$  m with a Campbell Scientific model CSAT3 sonic anemometer (hereafter “CSAT”; Campbell Scientific, 2011) providing the high-frequency vertical wind ( $w'$ ) and temperature ( $T'_s$ ) fluctuations, while water vapor ( $q'$ ) was measured with a co-located krypton hygrometer (Turnipseed et al., 2002). Winds are rotated from sonic to planar-fit coordinates prior to the flux calculations (Wilczak et al., 2001).  $T_s$  output by a CSAT is an average from three non-orthogonal paths. We use “ $H_{\text{CSAT}}$ ” to designate  $H$  calculated with  $T_s$  following Eq. (3). In our discussions, SEB refers to the ratio of the sum of the turbulent fluxes to ( $R_{\text{net}} - G$ ), i.e.,  $\text{SEB} = (H + LE)/(R_{\text{net}} - G)$ .

The CSAT can operate with either embedded code version 3 or version 4 (hereafter, ver3 and ver4) and uses advanced digital signal processing to determine the ultrasonic times of flight (e.g.,  $t_1$  and  $t_2$  in Eq. 2). Ver4 is designed to produce usable results when the signal is weak such as when liquid water is on the transducers, but degrades the  $T_s$  resolution from  $0.002^\circ\text{C}$  in ver3 to  $0.03^\circ\text{C}$  in ver4 (see Campbell Scientific, 2011 for more details about ver3 versus ver4).

Here, we briefly summarize the sequence of events that led to our study (also see Table 1). In 2008 we sent the three University of Colorado (CU) CSATs (all ver3) back to Campbell Scientific, Inc. for re-calibration and one of them (sn 0328) was upgraded to ver4. After deploying the ver4 CU CSAT at 21.5 m, we observed nighttime  $H_{\text{CSAT}}$  values that were frequently above zero, indicating heat was being transported from

the surface to the atmosphere at night. Though such conditions are possible for short periods (e.g., due to warm air advection), we have rarely observed such phenomena in the previous 10 years of measurements. These anomalous  $H_{\text{CSAT}}$  measurements were strongly correlated with high winds (Fig. 1).

Because we were curious/suspicious about these above-zero nighttime  $H_{\text{CSAT}}$  values, we deployed a CSAT from the National Center for Atmospheric Research (NCAR) Earth Observing Laboratory (EOL) at the same level as the CU CSAT (ver4). The EOL CSAT initially used ver3, which we changed to ver4 partway through our study (Table 1). To change from ver3 to ver4, the processing chip in the CSAT electronics enclosure was changed, but the sonic head was not disturbed. Additional air temperature information was provided near the 21.5 m level by a 0.254 mm E-type thermocouple that was located about 1.4 m from the CU CSAT and sampled at 1-Hz. Because we were concerned about flux loss due to horizontal separation and lack of high-frequency sampling, a second E-type thermocouple was deployed in May 2010 within 5 cm of the CU CSAT transducers and sampled at 10-Hz. The thermocouple temperature fluctuations ( $T'_{\text{tc}}$ ) are correlated with  $w'$  from the CU CSAT to calculate a sensible heat flux (e.g.,  $H_{T_{\text{tc}}} = \rho c_p \overline{w' T'_{\text{tc}}}$ ). The other temperature sensor at the 21.5 m level was a mechanically-aspirated slow-response temperature-humidity sensor (Vaisala HMP35-D probe) which we use as a “reference” sensor for time-averaged comparisons.

## 3 Results and discussion

### 3.1 Comparison of sensible heat fluxes

If  $H$  is calculated using the EOL CSAT, CU CSAT, and  $T_{\text{tc}}$  there are large  $H$  differences during periods of strong winds that are most obvious at night (Fig. 1). In a perfect sonic anemometer the path-length  $d$  is constant, however real world changes to  $d$  can occur as the sensor material expands and contracts due to temperature changes or wind-induced stresses or vibrations. Lanzinger and Langmack (2005) use a Thies

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energy budget (Sect. 3.2) and to make a link to the results from Turnipseed et al. (2002).

To gain further insight into the  $H_{\text{CSAT}} - H_{T_{\text{tc}}}$  differences, we examine the spectra of  $w'$ ,  $T'_s$ , and  $T'_{\text{tc}}$  and their associated cospectra and ogives (Friehe et al., 1991) for high-wind conditions (Fig. 3). The  $S_w$  and  $S_T$  spectra from the two CSATs are in good agreement, but show the effect of high-frequency noise and aliasing.  $S_T$  from  $T_{\text{tc}}$  (10-Hz) is attenuated at frequencies above  $\approx 1$  Hz because the thermal mass of the thermocouple wire limits the response time. In high-wind conditions (e.g., when the  $S_w$  and  $S_T$  energy peak is shifted to higher frequencies) we observe that  $H_{T_{\text{tc}}}$  (1-Hz) is about 10–20 % smaller than  $H_{T_{\text{tc}}}$  (10-Hz) due to the lower sampling rate as well as the horizontal separation. During the day the low-frequency part of  $S_T$  and  $(Co)_{wT}$  for the CSAT and thermocouple are in fairly good agreement (Fig. 3a). At night, however,  $S_T$  from  $T_{\text{tc}}$  has more energy than  $T_s$ , and  $(Co)_{wT_{\text{tc}}}$  differs dramatically from the cospectra of the two CSATs. The  $H$  ogive reveals nocturnal  $H_{T_{\text{tc}}} \approx -90 \text{ W m}^{-2}$  compared to  $H_{\text{CSAT}} \approx -30 \text{ W m}^{-2}$  (Fig. 3b).

It appears there is spurious correlation in  $\overline{w'T'_s}$  that enhances  $(Co)_{wT_s}$  during the day and degrades it at night. As  $U$  becomes smaller, the spectra and cospectra come into better agreement (Fig. 4).

We considered the possibility of tower/sonic vibration or movement affecting the transit times (e.g.,  $t_1$  and  $t_2$  in Eq. 2) and causing the  $\overline{w'T'_s}$  error. However, the main source of the problem appears to be with  $T'_s$  not  $w'$  because  $\overline{w'T'_{\text{tc}}}$ , which uses the same CSAT  $w'$ , produces reasonable heat fluxes, e.g., predominantly negative  $H$  at night. Also, similar high-frequency noise in CSAT  $S_T$  (not shown here) have been observed on a 30-m tower during high-winds in the CHATS field project (Patton et al., 2011). This suggests the problem is not specific to the NWT tower. Furthermore, discussions with Campbell Scientific, Inc. engineers have also led us to believe that sensor movement is not the cause of the problem. Without an independent measure of  $w'$  it is difficult to check the vertical wind, but we note that  $S_w$  in high winds is flatter than the expected  $-2/3$  slope (Fig. 3a–b). Finally, we also considered the  $\overline{w'q'}$  and  $\overline{u'w'}$  terms in Eq. (3),

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but found them too small to explain the discrepancy between  $H_{\text{CSAT}}$  and  $H_{T_{\text{tc}}}$  (results not shown).

In order to look further at the possibility of errors in  $T_{\text{s}}$ , we compare  $T_{\text{s}}^{\text{air}}$  and  $T_{\text{tc}}$  to an aspirated temperature-humidity sensor ( $T_{\text{asp}}$ ) as a function of  $U$ . At night (Fig. 5a and b), the  $T_{\text{tc}} - T_{\text{asp}}$  difference is less than  $\pm 0.1^\circ\text{C}$  and independent of  $U$ . However, during the day (Fig. 5c and d) there is a well-known radiation effect on  $T_{\text{tc}}$  that causes it to be larger than  $T_{\text{asp}}$  by about  $0.6^\circ\text{C}$  at low wind speeds but decreases to  $0.2^\circ\text{C}$  for high winds (e.g., Campbell, 1969; Burns and Sun, 2000). It is also well-known that  $T_{\text{s}}^{\text{air}}$  can contain a significant bias relative to true  $T$  due to uncertainties in the sonic path length (Loescher et al., 2005). Therefore, we adjust  $T_{\text{s}}^{\text{air}}$  with a linear fit to  $T_{\text{asp}}$  (the coefficients of the fit are listed in Fig. 5).

From Fig. 5 it can be seen that, during both day and night and for ver3 and ver4 CSATs,  $T_{\text{s}}^{\text{air}}$  shows a systematic decrease on the order of  $0.2^\circ\text{C}$  as  $U$  increases from around 8 to  $15\text{ m s}^{-1}$ . This negative  $T_{\text{s}}^{\text{air}}$  error correlated with increasing  $U$  explains the positive  $H_{\text{CSAT}}$  error in the NWT data. Since  $w'$  is negatively correlated with  $u'$  in the surface layer and the  $T_{\text{s}}'$  error is also negatively correlated with  $u'$ , the  $\overline{w'T_{\text{s}}'}$  error is positive, as observed.

### 3.2 Consideration of the surface energy balance

As mentioned in the introduction, Turnipseed et al. (2002) found that the nocturnal SEB closure during high winds varied between 0.2–0.6. In Fig. 6, the SEB is calculated using  $H_{\text{CSAT}}$  (CU ver3) and  $H_{T_{\text{tc}}}$  (1-Hz). As one would expect, the SEB with  $H_{\text{CSAT}}$  (CU ver3) closely matches the results of Turnipseed et al. (2002). At night (Fig. 6b), the SEB peaks at  $\approx 0.7$  for moderate  $U$ , and then becomes negative as  $U$  increases (or as friction velocity  $u_*$  increases as shown in Fig. 7 of Turnipseed et al., 2002). Also similar to Turnipseed et al. (2002), we find the nocturnal SEB with  $R_{\text{net}}$  from the Q\*7.1 sensor is about 15% closer to closing the SEB than with the CNR-1 sensor. For low winds, drainage flows form at the NWT site (Yi et al., 2005; Burns et al., 2011) and result in

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near-zero nocturnal SEB values due to decoupling, strong horizontal advection of temperature, and practical difficulties with the flux calculation (e.g., Mahrt, 2010). These low-wind conditions require knowledge of horizontal advection for a more complete understanding (Sun et al., 2007; Yi et al., 2008).

5 During the day (Fig. 6a), the SEB using  $H_{T_{tc}}$  and  $H_{CSAT}$  diverge at  $U \approx 6 \text{ m s}^{-1}$ . For  $U > 13 \text{ m s}^{-1}$ , the SEB with  $H_{CSAT}$  is close to 1. Knowing about the  $H_{CSAT}$  error in high winds (e.g., as discussed in Sect. 3.1 and shown in Fig. 3a) suggests that the daytime SEB approaching 1 is an artifact. In contrast, with  $H_{T_{tc}}$ , both the daytime and nighttime SEB values for  $U > 6 \text{ m s}^{-1}$  are in reasonable agreement at  $SEB \approx 0.65\text{--}0.75$ , and there is almost no dependence of the SEB on  $U$ . Unless there is a physical reason for the SEB to change with higher wind speeds, using  $H_{T_{tc}}$  appears more reasonable than  $H_{CSAT}$ . If true, SEB closure at NWT without considering the storage terms is around 70%. Taking into account the storage terms in Eq. (4) and the slight underestimation of  $H_{T_{tc}}$  (1-Hz) we would expect the SEB closure to improve by about 10–15%.

15 To better estimate the magnitude (in  $\text{W m}^{-2}$ ) of the SEB deficit we consider the 2006–2008 mean nocturnal values of  $R_{net}$  from the CNR-1 ( $\approx -85 \text{ W m}^{-2}$ ) and Q\*7.1 ( $\approx -60 \text{ W m}^{-2}$ ) sensors. This difference of  $25 \text{ W m}^{-2}$  results in a 15% difference in the SEB (Fig. 6b). These two  $R_{net}$  sensors are known to be accurate to only  $20 \text{ W m}^{-2}$  (Brotzge and Duchon, 2000; Foken, 2008; Michel et al., 2008) and within complex terrain radiation measurements are complicated (Oliphant et al., 2003). This suggests that a “field-calibration” of the current radiation sensors to a high-accuracy radiometer (e.g., Burns et al., 2003) could improve our understanding of the surface energy budget at the site, and possibly, help explain the remaining lack of closure. Other factors that might cause the lack of closure are discussed elsewhere (e.g., Turnipseed et al., 2002; Foken, 2008; Foken et al., 2011).

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## 4 Conclusions

We compared  $H$  calculated using sonic anemometer temperature to  $H$  calculated with a co-located thermocouple and found  $U$ -dependent  $H$  differences on the order of  $250 \text{ W m}^{-2}$  at high wind speeds. To better understand these  $H$  differences, we considered the surface energy budget. Using  $H_{T_{tc}}$ , the daytime and nighttime SEB values for  $U > 6 \text{ m s}^{-1}$  were fairly consistent (between 0.65–0.75). In contrast, using  $H_{CSAT}$  the SEB values in strong winds vary from below 0 (at night) to around 1 (during the day). Because there is no physical explanation for the wide variation in SEB with  $H_{CSAT}$ , we conclude that  $H$  calculated with the thermocouple is more reasonable. From analysis of the spectra and co-spectra of  $\overline{w'T'}$  in high winds, we conclude there is spurious correlation between  $w'$  and  $T'_s$  that lead to positive increases in  $H_{CSAT}$ . At night  $H$  is typically negative, and, for strong winds, the  $\overline{w'T'_s}$  correlation error makes the magnitude of nocturnal  $H_{CSAT}$  smaller than it should be. Because  $T_{tc}$  and  $T_s$  are both correlated with  $w'$  from the same CSAT, we conclude that  $T_s$  is the primary source of the error.

We have been in contact with Campbell Scientific, Inc. regarding our observed heat flux discrepancies. They subsequently performed their own independent experiments to confirm the sonic temperature issues we have presented. Their preliminary results with a CSAT ver4 indicate that the issue occurs at all wind speeds, but is significant for  $U > 8 \text{ m s}^{-1}$ . Campbell Scientific, Inc. is currently working to better quantify the magnitude of the error and will mitigate it with future hardware and/or software changes.

Though our study examines one specific model of sonic anemometer, the tests we have outlined with a thermocouple could (and should) be used with any field-deployed sonic anemometer. Furthermore, in a broader context, our temperature comparison shows the added value of *independent*, co-located, in-situ measurements in environmental research. Previous comparisons of sonic anemometers by Loescher et al. (2005) were very thorough, but performed the comparison up to a wind speed of  $\approx 6 \text{ m s}^{-1}$  so any issues at higher wind speeds were undetected. This emphasizes an important advantage of long-term in-situ comparisons – they cover the range of the

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observation. In short, our study provides a practical example of how valuable in-situ comparisons can be in evaluating sensor performance.

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**Table 1.** A summary of NWT AmeriFlux tower temperature measurements used in our study.

Sensor	Acronym	Sensor Height (cm)	Horizontal Separation <sup>a</sup> (cm)	Sample Rate <sup>b</sup>	Deployment Dates	Additional Comments
Vaisala HMP35-D	$T_{asp}$	2150	≈90	1	1 Nov 1998–present	slow-response platinum resistance thermometer in a mechanically-aspirated housing
E-type Thermocouple	$T_{tc}$ (1-Hz)	2198	≈136	1	20 Aug 2002–present	wire dia = 0.254 mm, unaspirated
	$T_{tc}$ (10-Hz)	2148	<5	10	5 May 2010–present	wire dia = 0.254 mm, unaspirated
Campbell Scientific CSAT3 Three Dimensional Sonic Anemometer <sup>d</sup>	CU CSAT <sup>c</sup> , ver3	2150	0	10	1 Nov 1998–14 Jan 2008	sn 0226, embedded code version 3
	CU CSAT <sup>c</sup> , ver3	2150	0	10	14 Jan 2008–21 Feb 2008	sn 0536, embedded code version 3 (on loan from EOL)
	CU CSAT <sup>c</sup> , ver3	2150	0	10	21 Feb 2008–31 Oct 2008	sn 0438, embedded code version 3
	CU CSAT <sup>c</sup> , ver4	2150	0	10	31 Oct 2008–28 Sep 2010	sn 0328, embedded code version 4, recalibrated in Oct 2008
	CU CSAT <sup>c</sup> , ver4	2150	0	10	28 Sep 2010–present	sn 0198, embedded code version 4
	EOL CSAT, ver3	2150	≈160	10	27 Sep 2009–17 Jan 2010	sn 0674, embedded code version 3
	EOL CSAT, ver4	2150	≈160	10	17 Jan 2010–21 Oct 2011	on 17 Jan 2010, changed sn 0674 control box from embedded code version 3 to version 4
	EOL CSAT, ver3	2150	≈160	10	21 Oct 2011–present	on 21 Oct 2011, changed sn 0674 control box back to version 3

<sup>a</sup> Horizontal distance from the University of Colorado (CU) CSAT sensor.

<sup>b</sup> Number of samples per second (Hz).

<sup>c</sup> The 2150 cm CU CSAT is used to determine the horizontal wind speed ( $U$ ).

<sup>d</sup> The CSAT3 sonic temperature ( $T_s$ ) corrected for humidity is  $T_s^{air} = T_s (1 + 0.51q)^{-1}$  where  $q$  is specific humidity. Also, CSAT data deemed unacceptable by the CSAT diagnostic flag were replaced with a linear fit between valid samples (for low wind wind speeds data were rarely flagged, but for higher winds around 2–4% of the samples were flagged).

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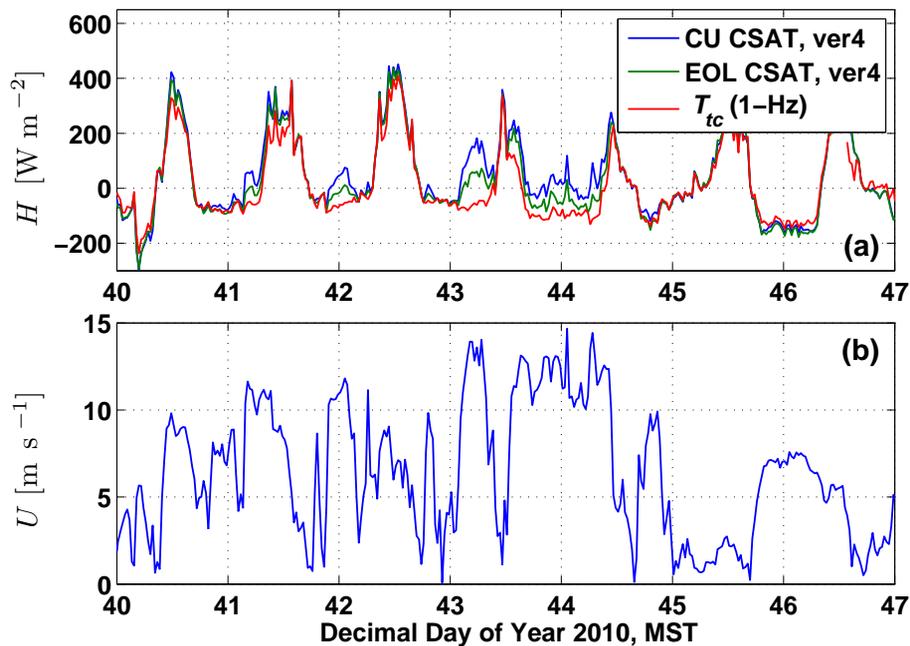
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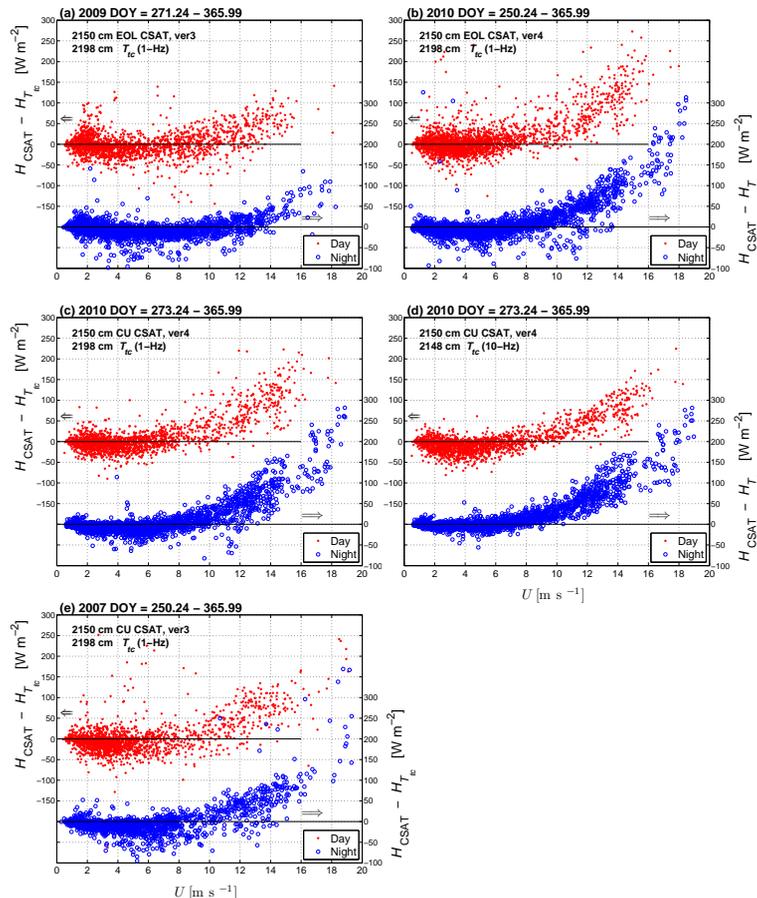


**Fig. 1.** Time series of 21.5 m (a) sensible heat flux  $H$  and (b) horizontal wind speed  $U$ .  $H$  is calculated using different temperature sensors as specified in the legend (see Table 1 for details).

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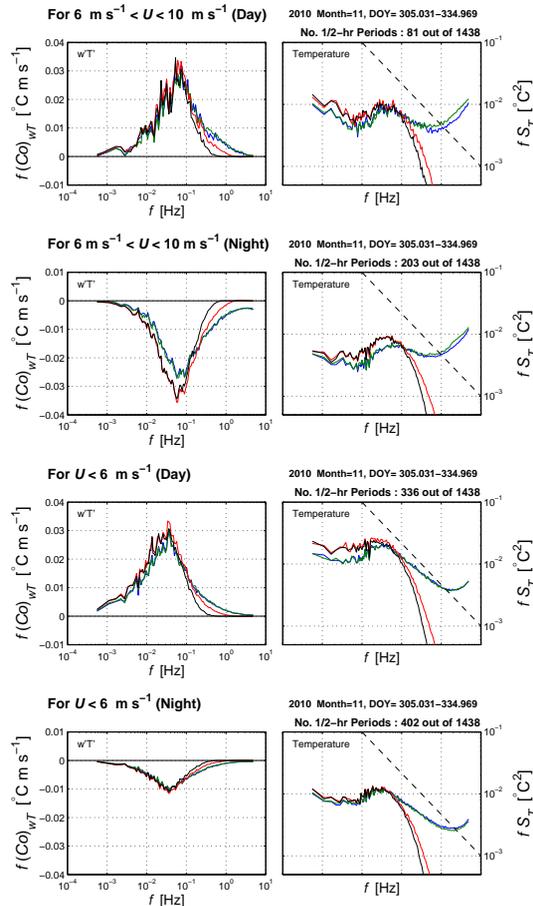


**Fig. 2.** The sensible heat flux difference calculated with the CSAT and thermocouple ( $H_{\text{CSAT}} - H_{T_c}$ ) versus the 21.5 m horizontal wind speed  $U$ . In (a)–(e), the time period (day of year, DOY) is specified along with the particular CSAT and thermocouple used (upper-left corner). (See Table 1 for sensor details.) Each point represents  $H$  calculated over 30 min, then separated into daytime (left-side axis) and nighttime (right-side axis) periods as shown by the horizontal arrows and legend.



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**Fig. 4.** The (left column)  $\overline{w'T'}$  cospectra  $(Co)_{wT}$  and (right column) temperature spectra  $S_T$  for medium- and low-wind conditions (see Fig. 3 for the legend and further details).

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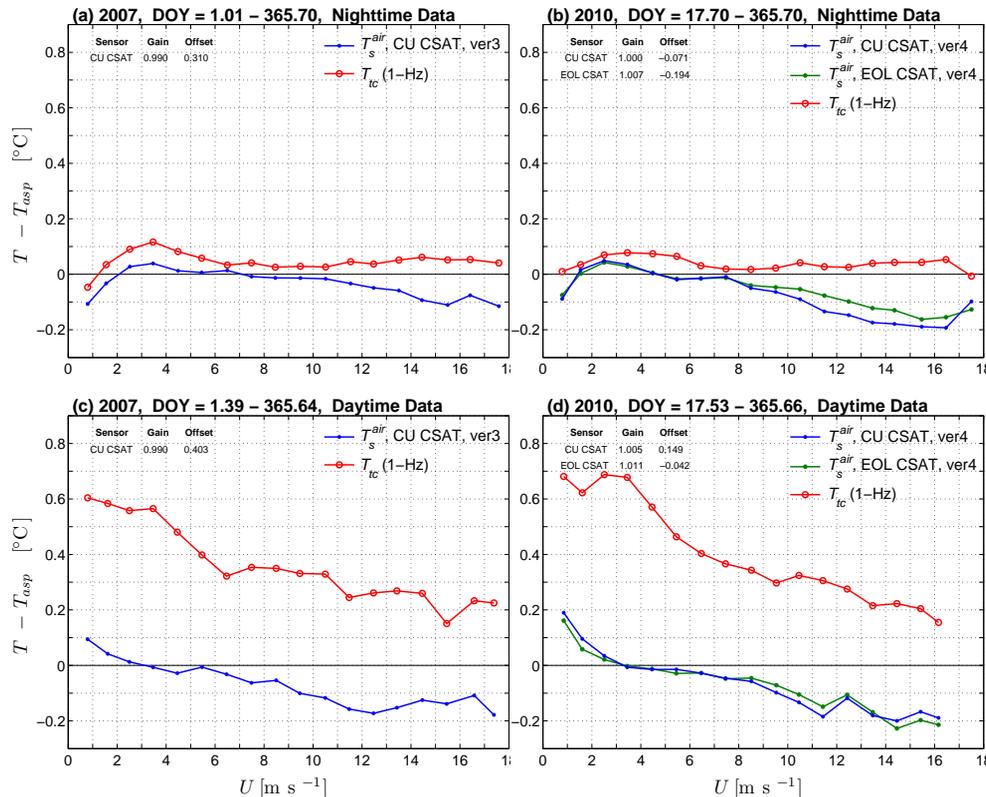
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**Fig. 5.** The **(a, b)** nighttime and **(c, d)** daytime mean temperature difference ( $T - T_{asp}$ ) versus 21.5 m horizontal wind speed  $U$ .  $T_{asp}$  is measured within a mechanically-aspirated housing and  $T$  is from either the humidity-corrected CSATs ( $T_s^{air}$ ) or a thermocouple ( $T_{tc}$ , 1-Hz) as specified in the legend (also see Table 1).  $T_s^{air}$  has been linearly adjusted to  $T_{asp}$  using the gain and offset shown in the upper left corner of each panel. The time period (day of year, DOY) used for each panel is shown.

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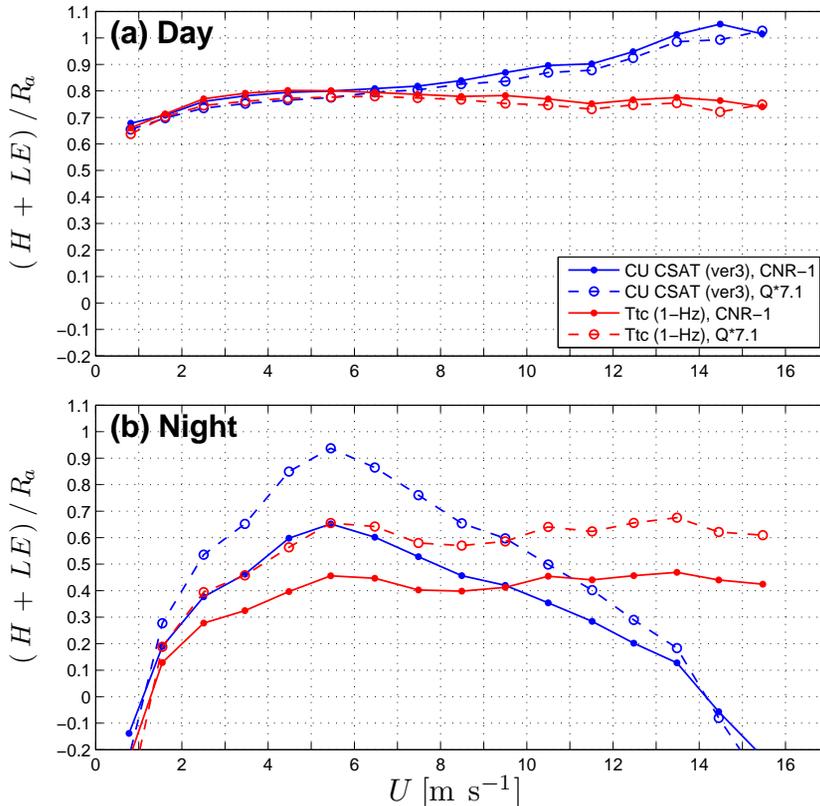
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**Fig. 6.** The surface energy balance [SEB =  $(H + LE)/R_a$ ] versus horizontal wind speed  $U$  from years 2006–2008 for **(a)** daytime and **(b)** nighttime conditions ( $R_a = R_{net} - G$  is the available energy, see text for details). The sensors used to calculate  $H$  (CU CSAT, ver3 or  $T_{tc}$ , 1-Hz) and  $R_{net}$  (Kipp and Zonen, model CNR-1 or REBS, model Q\*7.1) are specified in the legend. (This figure is comparable to Fig. 7 in Turnipseed et al., 2002.)

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