

**Calibration and
validation of the
advanced E-Region
Wind Interferometer**

S. K. Kristoffersen et al.

Calibration and validation of the advanced E-Region Wind Interferometer

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The advanced E-Region Wind Interferometer (ERWIN II) combines the imaging capabilities of a CCD detector with the wide field associated with field widened Michelson interferometry. This instrument is capable of simultaneous multi-directional wind observations for three different airglow emissions (oxygen green line ($O(^1S)$), the $^PQ(7)$ and $^PP(7)$ emission lines in the $O_2(0-1)$ atmospheric band and $P_1(3)$ emission line in the (6,2) hydroxyl Meinel band) on a three minute cadence. In each direction, for 45 s measurements for typical airglow brightness the instrument is capable of line-of-sight wind precisions of $\sim 1 \text{ ms}^{-1}$ for hydroxyl and $O(^1S)$ and $\sim 4 \text{ ms}^{-1}$ for O_2 . This precision is achieved using a new data analysis algorithm which takes advantage of the imaging capabilities of the CCD detector along with knowledge of the instrument phase variation as a function of pixel location across the detector. This instrument is currently located in Eureka, Nunavut as part of the Polar Environment Atmospheric Research Laboratory (PEARL). The details of the physical configuration, the data analysis algorithm, the measurement calibration and validation of the observations are described. Field measurements which demonstrate the capabilities of this instrument are presented. To our knowledge, the wind determinations with this instrument are the most accurate and have the highest observational cadence for airglow wind observations of this region of the atmosphere and match the capabilities of other wind measuring techniques.

1 Introduction

Interferometric methods have been the primary means for the past thirty years to passively observe mesospheric and thermospheric winds using Doppler shifts in airglow emissions. Progress in detector technologies have led to advances in the observation capabilities of these instruments by allowing the interference fringes and/or the scene of interest to be imaged. Apart from the Wind Imaging Interferometer (WINDII) on the Upper Atmosphere Research Satellite (Shepherd et al., 1993), publications on

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working instruments have generally been associated with the Fabry-Perot (Aruhliah et al., 2010; Anderson et al., 2012; Shiokawa, et al., 2012) and Spatial Heterodyne Spectroscopy (SHS) techniques (the Doppler Asymmetric Spatial Heterodyne (DASH) of Englert et al., 2012). The success of these instruments demonstrates how incorporating imaging capabilities improves the accuracy and temporal resolution over earlier configurations.

In this paper, a configuration which implements these imaging capabilities in combination with a field widened Michelson interferometer is described. The approach builds on the foundation developed during work on the WINDII instrument. The imaging capability permits simultaneous viewing in multiple directions (as opposed to sequential viewing in each direction) and allows the fringe profile to be imaged and analysed on a bin-by-bin basis using new data analysis algorithms. The resulting instrument, termed the advanced E-Region Wind Interferometer (ERWIN II), generates simultaneous wind observations in 5 directions (the four cardinal directions and zenith) at three different heights using three different emissions (the oxygen green line (O(1S)) at 557.7 nm, the $^{\text{P}}\text{P}(7)$ and $^{\text{P}}\text{Q}(7)$ lines in the O_2 (0–1) atmospheric band at 859.9 and 860.0 nm and the $\text{P}_1(3)$ emission line in the OH(6,2) Meinel band at 843.5 nm) every three minutes. The wind accuracy is $\sim 1 \text{ ms}^{-1}$ for all the emissions and the precision is $\sim 1 \text{ ms}^{-1}$ for the green line and hydroxyl observations and $\sim 4 \text{ ms}^{-1}$ for the O_2 observations for standard operating conditions.

ERWIN II is based on the E-region wind interferometer (Gault et al., 1996) which was built in the mid-1990's using a photo-multiplier tube as a detector. Winds were obtained by sequentially viewing different directions. This instrument was stationed at Resolute Bay for close to a decade and several papers on the associated observations published (Fisher et al., 2000, 2002; Bhattacharya and Gerrard, 2010). In 2005, funding through a Canadian Foundation of Innovation grant became available and was used to design and build an improved version of the instrument. The interferometer and filters from the old version of the instrument were retained but the optical configuration and imaging detectors were new. The imaging capability allowed a new data analysis

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algorithm to be developed which improved the accuracy and precision of the instrument. Once completed, ERWIN II was moved to the Polar Environment Atmospheric Research Laboratory (PEARL) in Eureka, Nunavut (80° N, 86° W) in February 2008. It operated satisfactorily for three winters till spring 2011 when some minor issues with its operation occurred. These have been fixed and normal operations will resume in the winter of 2012/2013.

This paper is organized as follows. The next two sections deal with concepts and details necessary for understanding the instrument namely the measurement and instrument concept, and a description of the new instrument and its operation. In the subsequent section, the data analysis algorithms are described. A section on the precision and accuracy of these measurements and their validation follows this. Some initial results along with a comparison with other wind measuring instruments and a brief summary of the planned scientific studies with this instrument are then presented. The paper finishes with some concluding remarks.

2 Measurement and instrument concept

Doppler shifts in isolated quasi-monochromatic emissions when viewed through an ideal Michelson interferometer are seen as changes in the modulation of the interference fringes as a function of path difference. The measured irradiance $I(\Delta, \lambda, x)$ for an isolated monochromatic emission line has the following form:

$$I(\Delta, \lambda, x) = I_0 \left(1 + UV \cos\left(\frac{2\pi}{\lambda} \Delta + x\right) \right) + I_B \quad (1)$$

Here I_0 is the irradiance of the emission, Δ is the path difference of the interferometer, λ is the wavelength of the emission, x represents small variations in path (typically less than λ) that the experimenter can introduce into the interferometer to sample a fringe, U is the relative reduction in fringe amplitude due to instrument effects, V is the relative reduction in fringe amplitude due to the finite width of the emission line and the path

difference and I_B is the sum of the background irradiance of the scene being viewed and the dark count.

The phase, θ , of the fringe is defined as $\frac{2\pi}{\lambda}\Delta$. A small change in wavelength due to a Doppler shift, $\lambda + \delta\lambda$, results in a change in phase of $\delta\theta = -(\frac{2\pi}{\lambda^2})\Delta\delta\lambda$ plus a small correction associated with the dispersion of the glass. For small line of sight velocities, v_{los} , the Doppler shift is $\delta\lambda = -\lambda(v_{\text{los}}/c)$ with positive line of sight velocities corresponding to a velocity towards the observer. Hence the phase change associated with this Doppler shift is:

$$\delta\theta = \frac{2\pi\Delta v_{\text{los}}}{c\lambda} \quad (2)$$

Observation of the phase shift relative to the zero wind phase allows the line-of-sight velocity to be derived.

As described in detail elsewhere (Shepherd, 2002), Doppler Michelson interferometry determines winds by determining phase shifts in the interference by measuring the irradiance passing through the interferometer at specific path differences and determining the fringe parameters from these measurements. Typically the interferometer path is varied in phase steps of $\pi/2$. The standard 4-point algorithm (for ideal conditions: no background or dark count) uses irradiance measurements at four such sequential steps to derive the fringe parameters, (irradiance, visibility and phase) as follows:

$$I_0 = \frac{I_1 + I_2 + I_3 + I_4}{4}$$

$$UV = \frac{\left[(I_1 - I_3)^2 + (I_4 - I_2)^2 \right]^{1/2}}{2I_0} \quad (3)$$

$$\theta = \tan^{-1} \left(\frac{I_4 - I_2}{I_1 - I_3} \right)$$

In passive remote sensing of winds using airglow emissions, the fundamental parameter controlling the measurement quality is the instrument throughput, $A\Omega$ defined as the

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product of the area, A , over which the signal is detected multiplied by the solid angle at the detector, Ω , that the scene of interest subtends. A field-widened Michelson interferometer is a configuration of this interferometer which minimizes the path variation as a function of angle through the interferometer (Shepherd, 2002; details and references pertinent to the following summary can be found in this monograph). Generally the field is collimated through the interferometer so the phase variation as a function of angle through the interferometer is projected onto the observed scene. The field widening is achieved by optimally inserting excess glass in one of the arms of the interferometer and positioning the mirror in the other arm at the apparent position of the mirror of the arm with the excess glass in it so that the conditions when the arms are the exactly the same are approximately achieved. This configuration eliminates the second order dependence of path as a function of angle and can eliminate the fourth order dependence for specific mirror positions (Zwick and Shepherd, 1971).

The precision of a wind measurement is basically related to how well the sinusoidal variation associated with a variation in path can be discerned relative to the inherent noise associated with that measurement. For a shot noise limited observation under the ideal conditions described above, a reasonable estimate of accuracy of the phase determination is the standard deviation in θ , σ_θ which is given by Ward (1988)

$$\sigma_\theta = \frac{1}{aUV\sqrt{I_0}} \quad (4)$$

where a is a constant which depends on the number of steps used to determine the fringe phase. For the four point measurement described above $a = 2$. For the 8 step scans used for ERWIN II, $a = 2\sqrt{2}$.

The two fringe-related parameters in this equation are the net visibility, UV , and $\sqrt{I_0}$ which is the signal to noise ratio. In practice, the measurement precision can be reduced by increasing the signal (longer integration times and enhanced instrument responsivity) or the visibility. The visibility is determined by the emission line-width, background emissions, the instrument imperfections and the phase variation over the

region used to detect the light (essentially the aperture effect discussed by Hilliard and Shepherd, 1966).

Contributions of background or dark signal to the observed irradiance also affect the measurement precision. In terms of the above formulation for ideal conditions this can be accommodated by determining effective irradiances and effective visibilities where the effective irradiance is $I_0^e = I_0 + I_B$ and the effective visibility is $UV^e = UV(I_0/(I_0 + I_B))$. In the rest of this paper, for simplicity, expressions will be provided for the ideal conditions (i.e. no dark and no background) with the understanding that for non-ideal conditions, the effective irradiance and visibility can be used without any change to their form.

The wind accuracy is a function of both the measurement precision and knowledge of the phase for a stationary source, termed here the zero-wind phase. Generally, practical sources for the airglow emissions are not available so the zero-wind phase is determined by using lamps with emission lines at wavelengths close to the airglow emissions and using nightly averages of the wind in the vertical direction under the assumption that vertical motions average to zero.

3 Instrument description and operation

ERWIN II differs from the original instrument in that the photomultiplier tube was replaced by an imaging detector, the optics were modified so that light from the four cardinal directions and the vertical could be viewed simultaneously, and the interferometer was placed in an air-tight housing to prevent pressure changes associated with weather fronts from affecting the phase. The interferometer, airglow emissions, calibration lines and the filters used are the same as ERWIN and are described in detail in Gault et al. (1996).

In summary, the interferometer is a three glass design with the mirror position controlled using piezoelectric cylinders and a capacitive feedback system. The front face is square with sides of 7.62 cm. It was designed to accept a beam with a 2.5 degree

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half angle. The interferometer is set to a path difference slightly larger than 11 cm and the glass lengths were chosen so that the interferometer is field widened at all wavelengths and thermally compensated. The specific path difference was selected to suppress possible fringes from thermospheric oxygen green line emissions, and to ensure the fringes of the pair of O₂ lines and the Λ doubled hydroxyl lines were each in phase. The calibration lines used are the 557.0 nm Krypton line, the 840.8 nm Argon line and the 866.7 nm Argon line.

Figure 1 is a schematic view of the mechanical layout of ERWIN II. It shows a cut through the centre of the instrument such that two of the cardinal viewing directions and the vertical can be seen (the other viewing directions project out of the plane of the figure). The centers of each cardinal viewing direction are at an elevation angle of 38.7 degrees relative to the horizontal. Light from the sky from all the viewing directions is collected and focused on what is termed the quad mirror where they are combined into a single beam and then passed through the interferometer. The interferometer is tilted 1.77 degrees horizontally and 1.77 degrees vertically relative to the optical axis of the system to ensure that no light was reflected off optical components and recycled back through the system. The optical components which collect the light and collimate it through the interferometer form what is termed the front telescope. After the interferometer, a second optical system, termed the back telescope directs the light to the filters where the light is again collimated. Both telescopes are 1 : 1. The camera system then focuses the beam onto the detector.

The quad mirror consists of four trapezoidal mirrors canted appropriately with a square hole in the middle. This serves to redirect light from each direction so that they combine with the zenith light into a single beam through the rest of the optical system. Each of the cardinal directions views an irregularly shaped piece of the sky approximately 0.0013 steradians at an elevation angle of 38.7 degrees. Zenith is viewed with a solid angle of 0.0007 steradians. Light from each of the cardinal directions is focused onto one of the trapezoidal facets of the quad mirror using spherical mirrors and zenith is focused onto the plane of this mirror. The quad mirror is located at the field stop of

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the front telescope. The light from these various viewing directions is passed as collimated light through the interferometer and then focused using a second telescope and camera onto the detector. The sky from each direction is thus focused onto different regions of the detector so that each of these five directions is simultaneously measured.

5 The effective field of view of the instrument is the same as that allowed through the interferometer, a beam of 2.5 degrees half angle.

The camera was built in house at York University and uses a 512 by 512 pixel, back-thinned, low-noise, frame-transfer CCD (E2V Technologies CCD57-10) with an active area of 6.656 by 6.656 mm. The CCD camera is used with 16 by 16 binning, resulting in a final image size of 35 by 32 bins. It has a quantum efficiency of 0.85 for the $O(^1S)$ emission and 0.45 and 0.4 for the O_2 and OH emissions. This is a significant improvement over the photomultiplier tube for which the quantum efficiency was ~ 0.14 , 0.08 and 0.06 for the same emissions. An additional advantage arises because, as noted above because of the imaging capability, measurements could be made with enhanced visibility over the original instrument. The increased sensitivity allows for a decrease in the exposure times, while still maintaining comparable signal to noise.

Figure 2 illustrates the manner in which the field is imaged onto the CCD detector. The dark bins indicate where the edges of the areas illuminated by the various regions of the sky. The light from each viewing direction is imaged such that the top is east, the bottom-west, the right-north, the left-south, and centre-zenith. The background colors indicate the how the interferometer phase in radians varies across the field and indicate how much variation there is across each region. Variations in phase away from this background along with consideration of the zero wind provide a measure of the Doppler shift in each viewing direction.

25 The observation procedure of ERWIN has been updated relative to that described in Gault et al. (1996). Since all viewing directions are now viewed simultaneously there is no need to cycle through the viewing directions. The basic procedure is to cycle through the three emission measurements in sequence and then after a user specified number of cycles to perform a set of calibrations. A measurement consists of 8 exposures of

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the detector each at a different value of the Michelson path. The steps (relative to the reference phase which coincides with the initial mirror position) are set to 0, $\pi/2$, π , $3\pi/2$, $3\pi/2$, π , $\pi/2$, and 0 radians. These steps are different for each emission with 2π radians corresponding to a physical change in path of λ , the wavelength of the emission being viewed. A calibration consists of measurements (again one for each emission) using the calibration lamps and a dark measurement. Initially a calibration was undertaken after every eight emission scans but later this was changed to every set of emission scans to provide better precision for determining the interferometer drift. Overall, this results in a set of observations (wind determinations for 5 directions and all three emissions) approximately every 3 min.

The observing geometry is illustrated in Fig. 3. All three emission layer are shown schematically and occur roughly at nominal heights of 97, 93 and 87 km for the O(¹S), O₂ and OH emissions respectively. Thus by cycling through the different emissions information on various heights in the mesopause region is acquired. The azimuthal viewing directions are at an elevation angle of $\alpha = 38.7$ degrees from the horizontal.

Since winds are determined by observing Doppler shifts in the emission frequencies, the observed, line-of-sight winds are combinations of the horizontal and vertical winds (save for the zenith line-of-sight winds, which observes the vertical winds).

The meridional wind, v , is determined using the difference of the line-of-sight north and south winds

$$v = \frac{(V_S^{\text{LOS}} - V_N^{\text{LOS}})}{2 \cos \alpha} \quad (5)$$

where

$$V_N^{\text{LOS}} = -v \cos \alpha + w \sin \alpha \quad (6)$$

$$V_S^{\text{LOS}} = v \cos \alpha + w \sin \alpha \quad (7)$$

Here w is the vertical component of the wind and α is the viewing angle of the azimuthal look directions relative to the horizontal.

Similarly, the zonal wind, u , can be determined using the east and west line-of-sight winds,

$$u = \frac{(V_W^{\text{LOS}} - V_E^{\text{LOS}})}{2 \cos \alpha} \quad (8)$$

The vertical winds can also be obtained using several different approaches. The first is to simply use the zenith line-of-sight winds

$$w = V_Z^{\text{LOS}} \quad (9)$$

Less directly, the vertical winds can be determined using the cardinal direction line-of-sight winds,

$$w = \frac{V_N^{\text{LOS}} + V_S^{\text{LOS}}}{2 \sin \alpha} = \frac{V_E^{\text{LOS}} + V_W^{\text{LOS}}}{2 \sin \alpha} \quad (10)$$

In theory, this provides the means to check the internal consistency of the wind determinations. In practice, however, the effects of gravity waves of scales of the same order as the distance between the viewing points in the airglow layer mean that these comparisons can only be undertaken in some sort of average sense.

4 Data analysis procedure

The essential issue for wind measurements is distinguishing the phase increments, $\delta\theta$, associated with Doppler shifts in the emission of interest from the phase associated with other factors. In general, the observed phase is a combination of the phase associated with the instrument configuration as manifested for the emission of interest (motionless) plus a shift associated with atmospheric motion of the source region being viewed. In practice, for imaging applications, the phase associated with the instrument configuration can be separated into three terms:

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– $\theta_B(i, j)$: a term associated with the phase variation across the field as a function of angle through the interferometer (or pixel location (i, j) on the detector) relative to the phase associated with rays passing at normal incidence through the interferometer (background phase). This variation is illustrated in Fig. 2.

– $\theta_T(t)$: a term giving the thermal drift phase relative to the phase at a particular time (thermal drift term).

– θ_0 : a term identifying the phase that a motionless source would have (zero wind phase).

Hence the measured phase, θ_a , can be expressed as a function of time, t , and location on the field as

$$\theta_a(i, j, t) = \theta_B(i, j) + \theta_0 + \theta_T(t) + \delta\theta(t) \quad (11)$$

This formulation of the phase assumes that the background phase stays constant (generally satisfied for carefully maintained interferometers) and temporal variations can be tracked with a single phase parameter, the thermal drift which is only a function of time.

In theory, the zero wind phase should be easy to determine since it only requires a stationary source for the emission of interest. In practice however, this is difficult to achieve since portable sources for the airglow emissions are unavailable and the atmosphere is generally in motion. As with other ground based wind instruments, a daily average of the observed vertical wind is used to determine this parameter. In the case of ERWIN II this average is measured using the quadrant looking vertical. For measurements at Eureka, where close to 24 h each day is observed, this determination is expected to be a good measure of the actual zero wind; all periods of tidal motions are covered during this time period, variations associated with gravity waves are expected to average to zero, vertical winds associated with planetary waves are of the order of cm s^{-1} and mean vertical winds are small (an ascent or descent of 10 km day^{-1} corresponds to a vertical velocity of 0.11 m s^{-1}).

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For ERWIN II, the background phase determination was more difficult than expected. Initially, it was thought the phase variation associated with the reference emissions would be suitable to use since they were within a few Ångstroms of the emission of interest. However, it was found that use of such a background resulted in phase variations of $\sim 10 \text{ ms}^{-1}$ across several of the quadrants when daily averages of the winds were calculated. Instead, the background phase which was used was determined using wind observations from a period when it was known to be cloudy (this phase variation is illustrated in Fig. 2 for the green line). Light from the sky was suitably scattered so that all directions gave the same Doppler shift. Daily averages of this wind for the oxygen green line and hydroxyl observations using this background are presented in Fig. 4. The resulting wind variations are minimal in each quadrant and the mean wind in each quadrant provides a measure of the mean wind for the day. Details of the analysis which lead to this choice of background wind are contained in Kristoffersen (2011).

Although the analysis approach described in Gault et al. (1996), could be implemented for ERWIN II by integrating the signal in each quadrant and treating each quadrant as a single detector, a new bin-by-bin least mean squares approach similar to that implemented in Ward (1988) was preferred. The latter approach was more precise since it avoids any visibility reduction that occurs as a result of the integration over the phase in each quadrant and it allows bins contaminated by stars or cosmic ray hits to be eliminated. In addition, a rigorous determination of the wind error can be undertaken.

For this approach, a non-linear least mean squares analysis using the Levenberg Marquardt method (as described in Press et al., 2007) is implemented. The irradiance variation during the k th 8-point scan is modeled according to the following equation:

$$I(j, j, t_k, s) = I_0(t_k)(1 + UV(t_k) \cos(\delta\theta(t_k) + \theta_l(j, j, t_k, s))) \quad (12)$$

where the parameters being solved for are $I_0(t_k)$, the irradiance, $UV(t_k)$, the net visibility, and $\delta\theta(t_k)$, the phase variation associated with the wind. Here t_k is the time of the k th scan. To ensure that the variation in phase angles being determined is small, all the

known phases associated with a particular bin are added together so that $\theta_l(i, j, t_k, s) = \theta_B(i, j) + \theta_0 + \theta_T(t_k) + (\Delta\theta_s)$ where $(\Delta\theta_s)$ is the step size increment associated with mirror step of index s (expressed as a phase angle).

The merit function is

$$\chi^2 = \sum_{s=1}^N \frac{\left(\bar{I}_s(i, j, t_k, s) - y(l(i, j, t_k, s); \mathbf{a}_l) \right)^2}{\sigma_s^2(i, j, t_k, s)} \quad (13)$$

where

$$y(l(i, j, t_k, s); \mathbf{a}_l) = a_l(1) (1 + a_l(2) \cos(a_l(3) + \theta_l(i, j, t_k, s)))$$

$$\mathbf{a}_l = (I_{0_l}(t_k), UV_{I_l}(t_k), \delta\theta_{I_l}(t_k))$$

$\bar{I}_s(i, j, t_k, s)$ is the irradiance measured for step s , bin (i, j) and scan k , and $\sigma_s^2(i, j, t_k, s)$ is the variance (estimated as shot noise) of this irradiance. l is the iteration index so $y(l(i, j, t_k, s); \mathbf{a}_l)$ is the irradiance determined using the constants determined on the l th iteration. $\theta_l(i, j, t_k, s)$ with $\Delta\theta_s = 0$ is used to seed the first iteration of this method. Typically only a few iterations are needed for convergence to a solution.

In practice, there are two approaches used to determine the zero wind and thermal drift phase, one using the calibration lamp phase determinations (the standard procedure) and the other when the calibration lamp phase is not available (as occurred for the O₂ and OH emissions when the lamps malfunctioned). For the standard procedure, the calibration phase was determined on a regular basis throughout the night by calculating the average Michelson phase over the full field of the calibration lamp using the same 8-point scan as for the airglow observations. The resulting time-series of calibration phase is interpolated using cubic splines to the airglow observation times to provide the variation in thermal drift phase. The relative airglow phase throughout the observation period is then calculated using the non-linear approach with the zero wind phase set to zero. The actual zero wind phase then provides an offset to this relative

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phase and is determined using the mean of the zenith over the entire day. The winds are determined by shifting the relative airglow phase by the zero wind phase and using Eq. (2) to convert the phase to velocity.

If the calibration lamps are not available, then the zenith measurements can be used to estimate the phase associated with the thermal drift and zero wind. In this case, the analysis approach as described above is undertaken but with the thermal drift and zero wind terms set to zero. For each image, the phase for the vertical view is then taken as an estimate of the sum of these two terms and subtracted off the four other quadrants. The disadvantage of this approach is that the vertical wind cannot be determined and phase variations associated with vertical winds are mixed into the phase determinations for each of the cardinal directions. This reduces the precision and accuracy of the radial wind determination. Nevertheless, the meridional and zonal wind determinations are unaffected by the lack of an independent zero wind determination since they are determined through a difference in radial wind determinations in opposite directions and hence the zero wind contribution to the two directions is eliminated (see Eqs. 5 and 8).

There are several advantages associated with the standard approach described above. This algorithm can be run for fewer than the 8 steps comprising a typical scan. Because the steps are in phase multiples of $\pi/2$ and all phases steps are repeated twice, anomalous irradiances are identified by comparing steps of the same phase and examining the sums of steps which are π radians apart. If one or two anomalous steps are identified in a scan they are eliminated from the phase determination thereby reducing the likelihood of outliers. In addition, there are ~ 150 bins used for wind determinations in each of the cardinal directions and ~ 80 bins for the vertical. As a result, any additional outliers beyond three standard deviations of the mean wind phase in each of the quadrants can be identified and are eliminated and the standard error associated with the wind determination for each quadrant calculated. Implementation of these checks results in a robust statistical framework for the wind determinations with this instrument.

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5 Measurement validation

In this section, results which verify the precision and accuracy of the ERWIN II instrument are presented. Crucial is an accurate determination of the background phase variation across the field, the thermal drift and the zero wind. Each of these aspects of the wind determination contributes to the measurement precision and accuracy. Evaluation of the measurement quality in terms of these aspects is possible because of redundancies in the approach and tests which were undertaken to investigate specific aspects of the measurement approach.

As noted above, the background phase was determined using observations taken on 28 January 2009 during a period when it was cloudy so that the directional asymmetry in the Doppler shifts was negligible as a result of scattering in the clouds. During the eight hours of observations used to determine this phase variation, ~ 160 measurements were taken. The background phase was determined by taking the average of these measurements. For the fringe parameters associated with these measurements, the standard deviation of the wind determination for each bin on each scan was $\sim 15 \text{ ms}^{-1}$ so that the standard error for the background phase determination was $\sim 1.1 \text{ ms}^{-1}$ for each bin. Since winds are determined by averaging the phases determined on a bin-by-bin basis in each sector, this error makes a negligible contribution to the measurement precision.

Equally important is determining whether there are any systematic errors in the background determination. This is important since the winds in opposite directions are determined relative to the background phase so errors in the background phase would result in systematic errors in these winds. Figure 4 shows the daily average wind image measured on 26 January 2009 for the oxygen green line and hydroxyl observations. Shown for each emission is the daily average of each bin in the image. The average of each sector gives the mean radial wind in each direction for this day. Two things of particular note are the uniformity of the winds in each quadrant and that opposite quadrants are close to the same magnitude but oppositely signed. The uniformity indicates

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that the background phase has been effectively removed from the wind determinations, since the gradient associated with the angular dependence of the background phase is not observed. The fact that the winds in opposing directions are consistent with what would be expected geometrically indicates that errors in the background phase determination are minimal and do not result in systematic errors in the radial wind determinations. The wind is defined as positive towards the instrument so the observation of a positive (negative) wind in one sector would correspond to a wind of the opposite sign in the opposite quadrant.

This self-consistency of ERWIN is further demonstrated by considering the averages of these sectors for several days, shown in Table 1. Since the winds in opposing directions should have the same magnitude but opposite sign, the sum of these values should be zero. The table provides the values of the average daily phase for each of the four sectors corresponding to the cardinal directions for three days in January 2009 for the hydroxyl and green line observations. The means for each sector over the three days is calculated (4th column) and then the sum of the phases of opposite sectors determined. Since the winds in opposing directions should have the same magnitude, but opposite sign, the sum of these values should be close to zero, as observed. On average, the difference is of the order of a meter per second. This further validates that the background is suitable for the wind determinations and at most a systematic error of 1 ms^{-1} is introduced into the radial wind observations. The use of this phase background has been checked for the subsequent years and it is a stable feature of the interferometer.

These results also demonstrate that on average the thermal drift is being calculated properly. Since the thermal drift would be a constant value added to the phase for every bin, at a given time, this value would have the same sign for each section. This would result in an addition of the thermal drift terms, rather than the cancellation of the winds, as is observed.

Depending on the thermal stability of the instrument short term measurement errors can also be introduced if the thermal drift is not followed with sufficient precision. As

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described earlier, initially calibration phase measurements were taken on a slower ca-
 dence than the measurements. For the first two years of observations, one scan of the
 calibration lamps was taken for every eight scans of the atmospheric emissions. For
 the third year (March 2010 to March 2011) this was increased to a calibration every
 5 measurement scan of the atmospheric emissions.

Figure 6 gives an indication of the precision of the thermal drift determination. Panel
 a (upper panel) shows a time series of the green line zenith phase (blue points) along
 with the phase determined with the calibration lamp (red dots – corrected with the zero
 wind offset so that both time series have the same daily average). On this figure the
 10 uncertainties in the phase determinations is smaller than the diameter of the dots in
 the plots. The two phase determinations follow each other closely.

Panel b (lower panel) is a time series of the difference between the observed zenith
 phase and the calibration phase interpolated using cubic splines to the times of the
 atmospheric observations. In this figure the measurement precision is close to the
 15 size of the dots. The standard deviation of the difference is 1.02 degrees or 4.5 ms^{-1} .
 This number includes geophysical variability (vertical winds, irradiance variations) and
 Schott noise and hence is not a clean measure of the uncertainty introduced through
 the thermal drift calibrations.

To explore this aspect of the measurement in more detail, an experiment which in-
 20 cluded frequent calibration measurements was performed (a calibration measurement
 was taken after every atmospheric measurement). The resulting calibration phase time
 series was compared to one constructed by sampling this time series at a the same
 rate as other typical days and then interpolating (using cubic splines) these measure-
 ments to the times of the original time series. This process duplicated the thermal
 25 phase determinations associated with the atmospheric measurements.

Figure 6 shows the result of this experiment. The phase error in the cubic spline
 is never more than a degree, and the standard deviation of the phase error over the
 duration of this experiment is 0.389 degrees (1.69 ms^{-1}). This is significantly smaller
 than the standard deviation of the difference of the calibration phase and the zenith

emission phase, which was 1.02 degrees (4.5 ms^{-1}). This demonstrates that the errors associated with the cubic spline are acceptably small compared to the other errors and geophysical noise. This uncertainty is reduced for observations with the more frequent calibration cadence.

Using the value of “a” appropriate for the 8 step scan, and Eqs. (2) and (4), the precision of a wind measurement is estimated by the standard deviation

$$\sigma_w = \frac{c\lambda}{4\sqrt{2}\pi\Delta_{\text{eff}}UV\sqrt{I}} \quad (14)$$

Here σ_w is the error in ms^{-1} , Δ_{eff} is the effective path difference, UV is the visibility, I is the observed irradiance, c is the speed of light, and λ is the wavelength of the emission. The wind standard deviation is inversely proportional to the visibility, the path difference and the square root of the irradiance. Comparison of the estimated variance using this formula to the observed variance provides an indication of how closely the observations conditions during individual scans match the assumptions associated with the derivation of this formula (namely that the irradiance and visibility remain constant during a scan).

This is illustrated in Fig. 7 which provides time series of the actual standard error and the standard error estimated using Eq. (14) (calculated as a variance for each bin in the sector using Eq. (14) and then averaged in the same way as the actual standard error is calculated) for the north sector on 22 December 2008. The variability in both data sets is due to variations in the irradiance and visibility during that day. It is striking that the two measures follow each other so closely since this indicates that intensity and visibility variations during scans is generally insignificant. If it was a factor then the standard error would be significantly larger than the estimated precision.

Figure 8 shows time series of the standard error for all four cardinal direction sectors for 26 January 2009. For this date, some twilight was present in the afternoon centered at $\sim 17:00$ LT. The increase in the standard error in the vicinity of this time is the expected result of increases in the background relative to the emission irradiance

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(see discussion at the end of Sect. 2). The time series of all four sectors follow each other well. The daily average of the green line standard error for the zenith section is 1.91 ms^{-1} , and that for all of the cardinal directions is 1.22 ms^{-1} . The daily average of the precision based on the visibility and intensity of the green line emission for zenith is 1.88 ms^{-1} , and that for the cardinal directions is 1.24 ms^{-1} . The values for zenith are greater than for the cardinal directions because of geometrical considerations. The effective layer thickness (and hence irradiance) is greater by $1/\cos(\alpha)$ where α is the inclination angle relative to zenith (here $\alpha = 51.3$ degrees). The irradiance during this day was lower on average so these values are slightly higher than the typical precision of these measurements.

Plots of the winds provide a final, and satisfactory, check that the results are accurate. Meridional winds from 23 January 2009 for green line and hydroxyl calculated in several different ways are shown in Fig. 9. The meridional, north direction and south direction winds are calculated using Eqs. (5), (6) and (7), respectively. The time series designated “without subtracting zenith”, is a time series of the wind determined from the northern sector without zenith subtracted. The meridional winds are reasonable, and indicate that there was a significant semi-diurnal tidal variation present. The manner in which this wind is determined renders it independent of vertical wind and thermal drift. Although perturbations due to gravity waves will result in small deviations from the true large scale meridional wind above the station, to good approximation this time series can be considered a good measure of the true meridional wind. Issues with thermal drift, zero wind or background phase will result in the meridional winds determined solely from the north or south directions deviating significantly from this time series.

All the green line winds agree well with each other. The north and south winds, which are the winds determined from the respective sectors with the zenith phase subtracted off to remove any thermal drift, follow the meridional wind very closely. This demonstrates that the winds viewed from the different directions are self-consistent. The fourth wind plotted on this figure is the north wind without the zenith phase subtracted. Since this also fits the meridional wind very closely, it demonstrates that the

thermal drift has been effectively removed from the wind phase for observations with this emission.

The OH observations are taken during the time when the associated calibration lamp was not working. As with the green line observations the north and south winds follow the meridional wind closely. In contrast the north wind without zenith subtracted deviates significantly from the other winds. As expected since there are no calibration measurements to provide thermal drift information, omission of the zenith phase results in winds which exhibit significant systematic errors.

Since the contribution of the thermal drift variance to the wind observations is $\sim 2.85 \text{ m}^2 \text{ s}^{-2}$ for the time when the longer cadence calibration period was implemented, it is possible to use the zenith phase to examine the vertical wind (for the shorter cadence calibration period this will be even more feasible). While the exploration of this possibility will require careful analysis, an indication that this is plausible comes from a comparison (see Fig. 10) between the vertical wind determined using the zenith phase (blue dots), and the vertical wind determined using Eq. (10) (black dots). Both of these methods provide similar results on the larger temporal scales. Over the day, the vertical wind is modulated sinusoidally by a few ms^{-1} . This could be due to a diurnal tide although since this day was during the 2009 major stratospheric warming other dynamical effects could be present. The variance in the directly measured vertical wind is $30.9 \text{ m}^2 \text{ s}^{-2}$, which is significantly greater than the contribution associated with the thermal drift determination. The variance in the indirect determination of the vertical wind is $89.4 \text{ m}^2 \text{ s}^{-2}$. This calculation however also includes contributions from horizontal motions. Further analysis of the vertical winds will be undertaken in the future to determine whether definitive geophysical results are possible.

In this section, the various factors affecting the precision and accuracy of the ERWIN II wind results have been discussed and results demonstrating the internal consistency of the winds presented. The main factors affecting the measurement precision are the uncertainties associated with the Schott noise and the thermal drift determination. For the observations with the low cadence calibration measurements the net

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variance is $\sim 4 \text{ m}^2 \text{ s}^{-2}$ (i.e. $(1.22)^2 + (1.69)^2$) for the green line and OH observations and $\sim 19 \text{ m}^2 \text{ s}^{-2}$ (i.e. $(4.0)^2 + (1.69)^2$) for the O_2 observations. These values depend on the manner in which the thermal drift varies and for the observations taken with the high cadence calibrations will be close to the Schott noise values alone. The O_2 values are significantly greater than the other two emissions because its irradiance is significantly smaller. For all the emissions, the precision is dependent on the irradiance and visibility and there are occasions when the irradiance is close to a factor of four greater than that for the days used in this paper to validate the instrument and on these days the variance will be less than $1 \text{ m}^2 \text{ s}^{-2}$ for high calibration cadence observations.

The measurement accuracy for radial winds is determined by the uncertainty in the background phase determination ($< 1 \text{ ms}^{-1}$) and uncertainties in the zero wind determination. Based on the arguments presented in Sect. 4, this is expected to be less than 1 ms^{-1} also. Hence, for the best observation procedure (high cadence calibrations), the precision and accuracy are both $\sim 1 \text{ ms}^{-1}$.

6 Discussion

Comparisons between the capabilities of ERWIN II and other optical wind measuring instruments are not straightforward. Few papers have discussed the precision and accuracy of a technique in as much detail and as clearly as has been undertaken in this paper. In part this is because a standard for comparison has not been developed, in part because the precision is dependent on the integration time (i.e. amount of light collected), instrument aperture and field of view, and thermal stability, and in part because clear identification of the zero wind is difficult in practice. Instead, estimates of the measurement precision tend to be embedded in measurement papers using the particular technique in question. Since most techniques use some sort of average of the vertical wind over a night to estimate the true zero, unless there are other systematic errors, one can assume that the measurement accuracies are similar. As a result the measurement precision (taken as the standard deviation of the velocity determination) and

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the integration time needed for the measurement as quoted in the literature are the only pragmatic means to use in comparing different instruments.

For ERWIN II, five velocity measurements at a precision of 1 ms^{-1} in 45 s are observed for an airglow brightness slightly below average. In a recent paper on multiple order Fabry-Perot wind observations (Shiokawa et al., 2012) (similar to the observation technique used by Makela et al., 2011; Meriwether et al., 2011) random errors ranging from 2 to 13 ms^{-1} are quoted for a single wind observation with an exposure time of 60 s. Assuming that observing conditions in the middle of this range correspond to those for ERWIN II, it would take this instrument ~ 5 min to observe the same five velocities with a precision of $\sim 7 \text{ ms}^{-1}$.

The Scanning Doppler Interferometer (SCANDI) described by Arulia et al. (2010) is used for all-sky auroral imaging by using multiple fringes. They note that it takes ~ 7 –8 min to obtain a 25 sector wind measurement for these emissions which are about an order of magnitude greater in brightness than they are at mid-latitudes (i.e. airglow as with ERWIN II). For measurements on 8 March 2007 an uncertainty of 15 ms^{-1} is quoted. Assuming that the measurement uncertainty scales roughly as the reciprocal of the square root of the brightness, the uncertainty in these measurements would be $\sim 45 \text{ ms}^{-1}$ (i.e. $15 \text{ ms}^{-1} \cdot \sqrt{10}$) for a brightness an order of magnitude less than that observed. If this was reduced to a 5 sector measurement by combining the observed irradiances then the precision would be $\sim 20 \text{ ms}^{-1}$ (i.e. $45/\sqrt{5}$) for a ~ 7 min measurement.

The DASH instrument (Englert et al., 2007) was recently used in field measurements at a mid-latitude site to compare results to a Fabry-Perot interferometer (Englert et al., 2012). For this comparison, 5 min integrations were taken and the oxygen red line was observed. Uncertainties at the one sigma level ranged from ~ 5 to 15 ms^{-1} based on the plots in this paper. It would take > 25 min to achieve the five measurement cycle of ERWIN II at a precision $\geq 5 \text{ ms}^{-1}$.

This comparison indicates that ERWIN II is a significantly superior wind measuring instrument than any other ground based airglow wind instrument. Of these, the

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multiple order Fabry-Perot of Shiokawa et al. (2012) comes closest to the ERWIN II performance. Even with this instrument (again assuming the uncertainty scales with irradiance as described above) it would require an integration time of 225 min ($5 \text{ min} \cdot 7^2$) to achieve the 1 ms^{-1} precision that ERWIN II achieves. These comparisons are not definitive since the instruments described in these papers do not necessarily represent their optimal configuration. However, the advantage shown by ERWIN II is unlikely to be matched by minor changes in the configurations of these instruments. At this time it provides the most precise and rapid airglow wind measurements in the world.

Lidar and radar are two other techniques used to measure winds in the mesopause region. She et al. (2003) state that their sodium lidar has a vertical resolution of 2 km and measures winds between 81 and 107 km. The wind precision is $\sim 1.5 \text{ ms}^{-1}$ at the peak of the layer ($\sim 91 \text{ km}$) and $\sim 15 \text{ ms}^{-1}$ at the upper and lower bounds of their measurements for a one hour integration during night. In a comparison between radar (Middle and Upper atmosphere (MU) radar (meteor mode)) and Fabry-Perot winds observed over Shigaraki, Japan, Fujii et al. (2004) quote uncertainties of $2\text{--}5 \text{ ms}^{-1}$ for 1 km resolution and 30 min integrations at $\sim 93 \text{ km}$ which is close the height of maximum meteor trail detection. Radial wind uncertainties associated with a meteor radar in a paper by Frank et al. (2004) which compares lidar winds to meteor radar winds are quoted as being a few ms^{-1} for (time/height) bins of (60 min/4 km). For the lidar used in this study, vector winds were obtained with $\sim 1 \text{ ms}^{-1}$ precision between 85 and 100 km with a 12 min cycle and vertical resolution of $\sim 1 \text{ km}$ (Liu and Gardener, 2005).

As discussed by Frank et al. (2004) and Fujii et al. (2004) the geometries of the observing conditions associated with the various wind measuring instruments are different. They are sensitive to different temporal and spatial scales, so the measurement variances are affected differently by geophysical variability. ERWIN II views a brightness weighted wind so it can be considered to provide winds for a volume of atmosphere of $\sim 5 \text{ km}$ in the vertical and 5 km by 6 km in the horizontal. (It will not be sensitive to vertical scales less than approximately half the thickness of the airglow layer

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(~ 5 km)). The horizontal dimension is determined from the beam width at 90 km (~ 5 degree lateral cross section) and elevation angle of 38.7° . In contrast, the lidar collects information from volumes with heights of 1 km and a diameter of ~ 50 m and the meteor radar collects information per velocity measurement from a volume 4 km thick and 200 km diameter (Franke et al., 2005). The sampling area of the MU radar per velocity measurement is from a volume 1 km thick and 200 km in diameter. Based on the height range and vertical resolution of the best of these various instruments, the lidar achieves 15 velocity measurements at a 1 ms^{-1} precision in 12 min, and the MU radar achieves 40 velocity measurements at a $3\text{--}5 \text{ ms}^{-1}$ precision (recent upgrades to the MU radar may have enhanced its capabilities). At a vector wind measurement every 45 s at a precision of $\sim 1 \text{ ms}^{-1}$ ERWIN II has similar capabilities to these instruments.

Figure 11 shows time series of the meridional and zonal winds observed by ERWIN II on 22 December 2012 for all three emissions. As expected for larger scale upward propagating waves, the phase progression is downward with the green line winds leading, followed by O_2 and then OH. Standard errors for each wind measurement are smaller than the dots in the figure for green line and OH and about the size of the dot for O_2 . The smaller scale variations are real and provide the opportunity to investigate the wind fields at these heights on smaller temporal scales than previously possible. Given that ERWIN II simultaneously provides observations of the relative brightness of the airglow emissions that it observes, the relationship between the winds and airglow can be explored in detail. Of particular interest, is the investigation of gravity waves and the associated vertical velocities and airglow variations.

The PEARL facility where ERWIN II is currently located, houses three other instruments which take measurements in the upper mesosphere and lower thermosphere. These include an All Sky Imager (ASI) (observes OH, Na, $\text{O}(^1\text{S})$, $\text{O}(^1\text{D})$ and N_2^+), a Spectral Airglow Temperature Imager (SATI: O_2 , OH; Sargoytchev et al., 2004; Shepherd et al., 2010), and a meteor radar (Manson et al., 2009). The measurement cadence of the ASI and SATI are of the order of minutes and the meteor radar provides an hourly vertical profile of horizontal wind in the mesopause region. Intercomparisons

between simultaneous observations taken with these instruments open up many possibilities for new scientific studies. The dynamical signatures of specific events (such as stratospheric warmings), wave signatures and the relationships between temperature, wind and emission rate over a broad range of scales are topics which this research station is uniquely capable of investigating.

7 Conclusions

The construction of ERWIN II and the completion of new data analysis algorithms have resulted in a powerful new capability for investigating the dynamics of the mesopause region. The most important physical changes to the instrument include the addition of a quad mirror to the ERWIN optical train so that multiple viewing directions can be simultaneously observed and the inclusion of a CCD camera so that each of these directions can be simultaneously imaged. The new data analysis algorithm takes advantage of the imaging capabilities of the new instrument to provide a more precise and better monitored wind and irradiance observations.

In this paper, the capabilities of this instrument have been thoroughly discussed. For the standard observation sequence, wind measurements have a precision and accuracy of $\sim 1 \text{ ms}^{-1}$ and a three minute observation cadence which incorporates observations in five viewing directions for each of three different emissions. This accuracy, precision and observing cadence was shown to the best to date for optical instruments which use airglow to measure winds. Comparisons with superior radar and lidar systems indicate that ERWIN II wind observations are among the best in the world.

New science is anticipated with this instrument. On its own, vertical winds and relationships between the wind components and airglow irradiance can be investigated at temporal scales previously unachievable. Of particular interest in this respect is the investigation of the relationships between these variables in gravity waves and tides, and the investigation of the velocity spectra at these heights.

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The installation of ERWIN II at PEARL along with several other instruments which observe temperature, airglow and wind in the mesopause region establishes a unique and potent capability both amongst Arctic observatories and worldwide. These instruments include a SATI, an All Sky Imager and a meteor radar. Together they support the investigation of the spatial and temporal variability of the temperature, wind and airglow on temporal scales of minutes to months and spatial scales from kilometers to hundreds of kilometers.

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Table 1. Comparisons of the mean differences of the daily averages of the opposite sight directions for the green line and OH emissions using the 28 January 2009 background phase.

Green line – 28 Jan Background						
	Mean Phase (rad)					Difference (ms ⁻¹)
	23 Jan	25 Jan	26 Jan	Mean	Difference	
Bottom-West	-0.0396	-0.0913	-0.0754	-0.0688	-0.0057	-1.4216
Top-East	0.0381	0.0977	0.0534	0.0631		
Left-South	-0.0412	-0.0074	0.0223	-0.0088	-0.0002	-0.0416
Right-North	0.0612	-0.0030	-0.0324	0.0086		
OH – 28 Jan Background						
	Mean Phase (rad)					Difference (ms ⁻¹)
	23 Jan	25 Jan	26 Jan	Mean	Difference	
Bottom-West	-0.0329	-0.0463	-0.0510	-0.0434	0.0034	0.8563
Top-East	0.0338	0.0598	0.0469	0.0468		
Left-South	-0.0439	-0.0484	-0.0156	-0.0360	0.0038	0.9477
Right-North	0.0602	0.0407	0.0184	0.0398		

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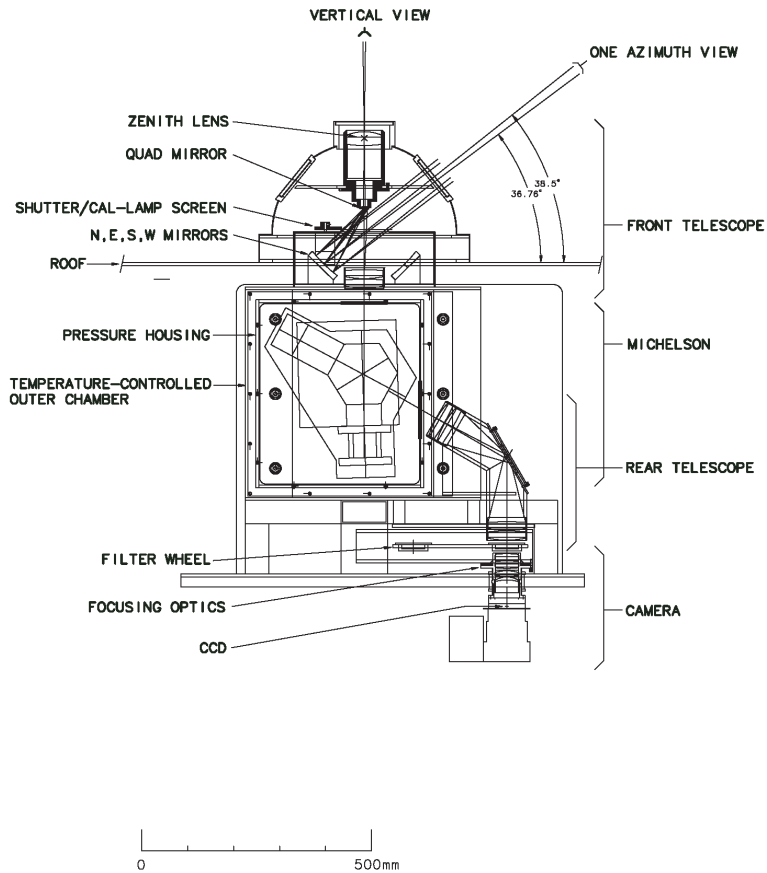
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ERWIN-2 MECHANICAL LAYOUT

Fig. 1. Diagram of ERWIN mechanical layout.

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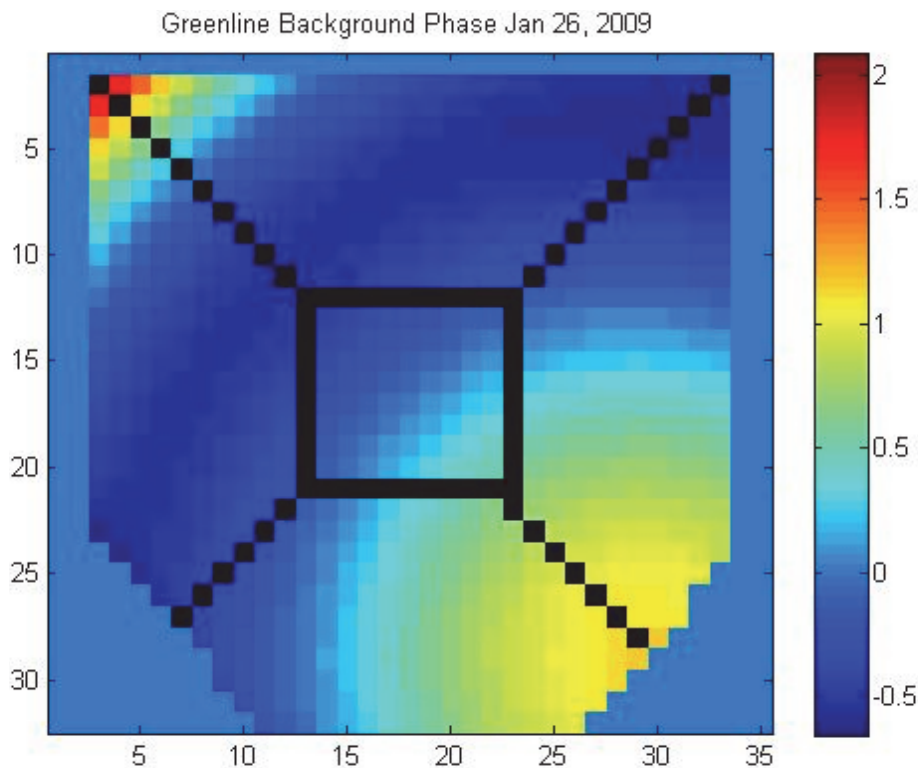


Fig. 2. Green line background phase (in radians) from 26 January 2009. The blackened bins represent the borders between the sections of the quad mirror. The top section measures east, the bottom, west, the left, south, the right, north, and the centre zenith.

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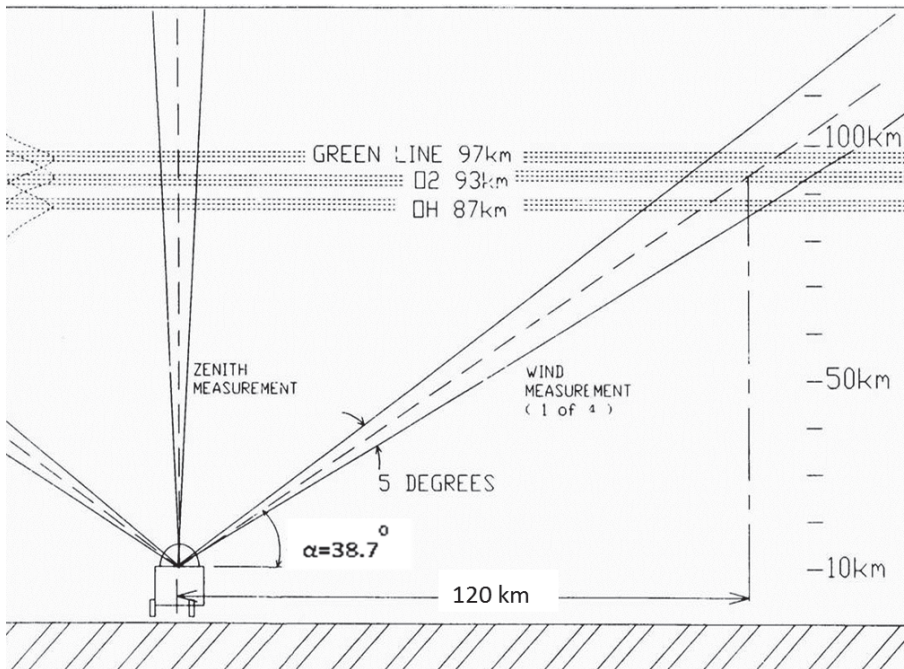


Fig. 3. Schematic of the viewing geometry of ERWIN II. This shows three fields of view. The other two are orthogonal to the plane of the page.

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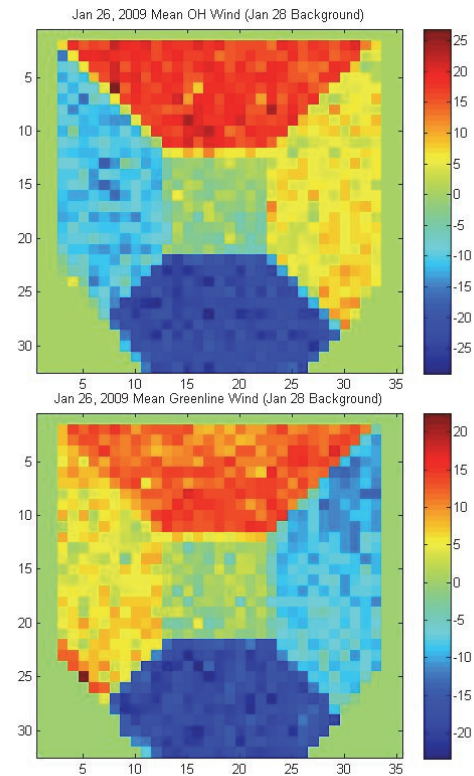


Fig. 4. An image of the daily averaged wind image (m s^{-1}) for the green line and OH observations on 26 January 2009, using the 28 January 2009 phase average for the background phase. The averages are calculated on a bin by bin basis. The sector averages of these images provide the daily mean winds in each direction. The uniformity of each sector and the fact that opposite sectors are of similar magnitude but opposite sign indicates that the phase background isn't introducing systematic errors into the wind determinations.

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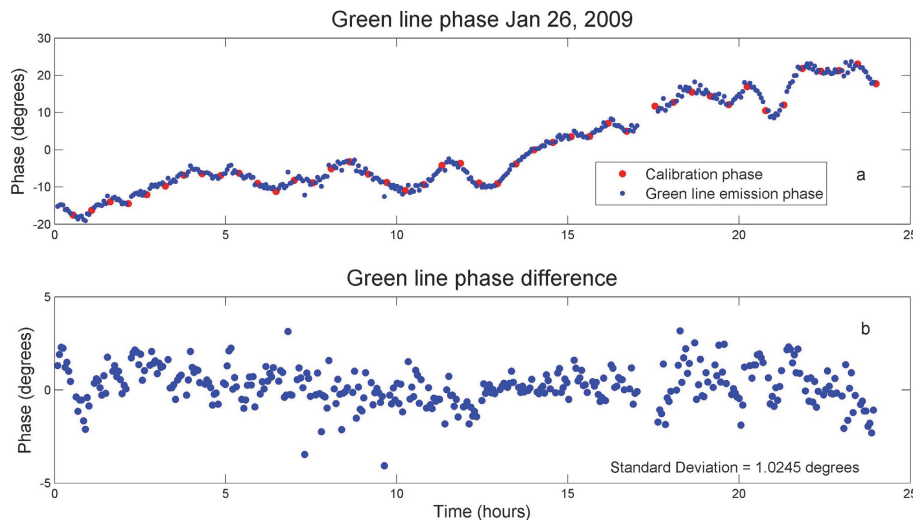


Fig. 5. (a) Plot of Green line emission zenith phase (blue dots) and the calibration phase (red dots) on 26 January 2009. The measurement uncertainty of the phase measurements is smaller than the size of the dots in this plot. (b) Plot of the difference between the zenith phase and the calibration phase interpolated using cubic splines to the times of the atmospheric observations. The zenith observations include geophysical variability.

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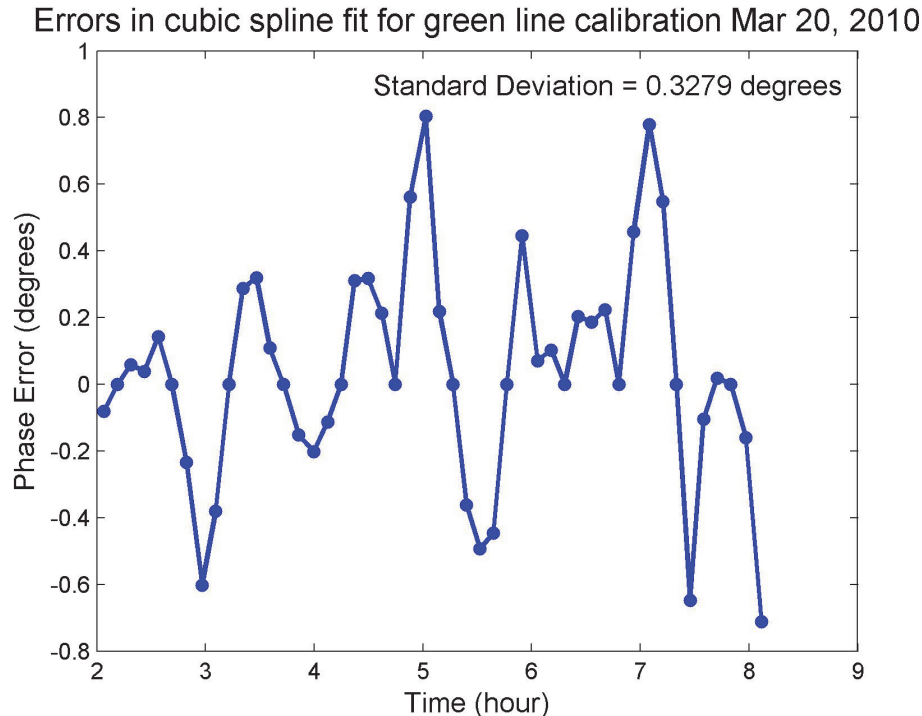


Fig. 6. Plot of the error in the cubic spline interpolation for the green line calibration lamp sampled every ~ 30 min relative to the original time series and interpolated to the times of the original time series. Every 8th point of the original time series is used for the interpolation (the error for these points is identically zero). The data was recorded on 20 March 2010.

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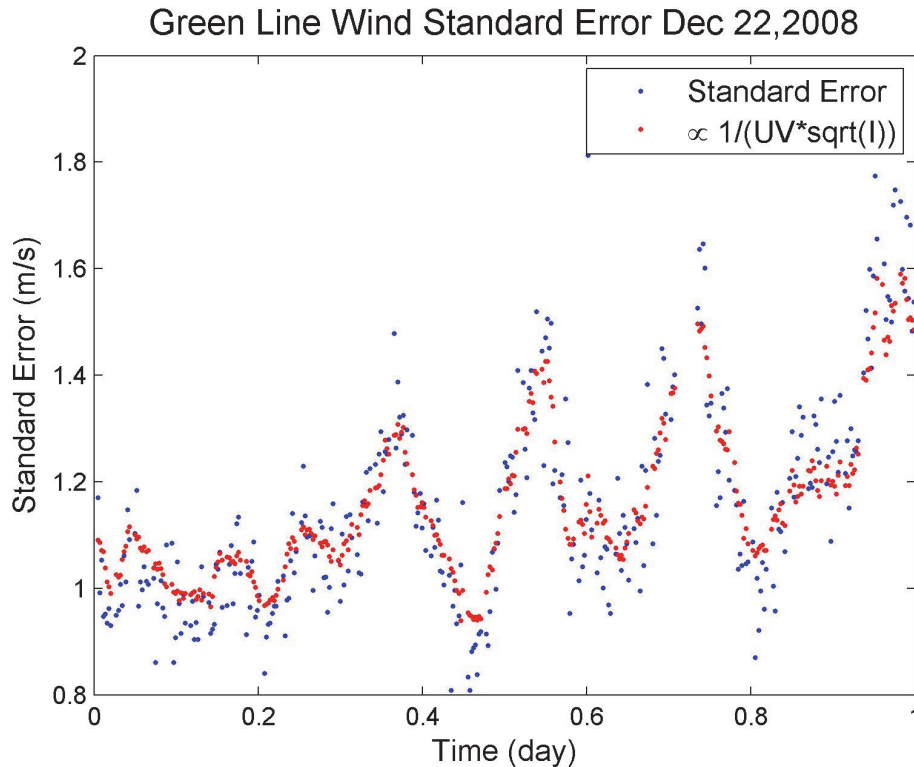


Fig. 7. Comparison of the standard error (blue points) for northern sector compared to the expected standard deviation (red points).

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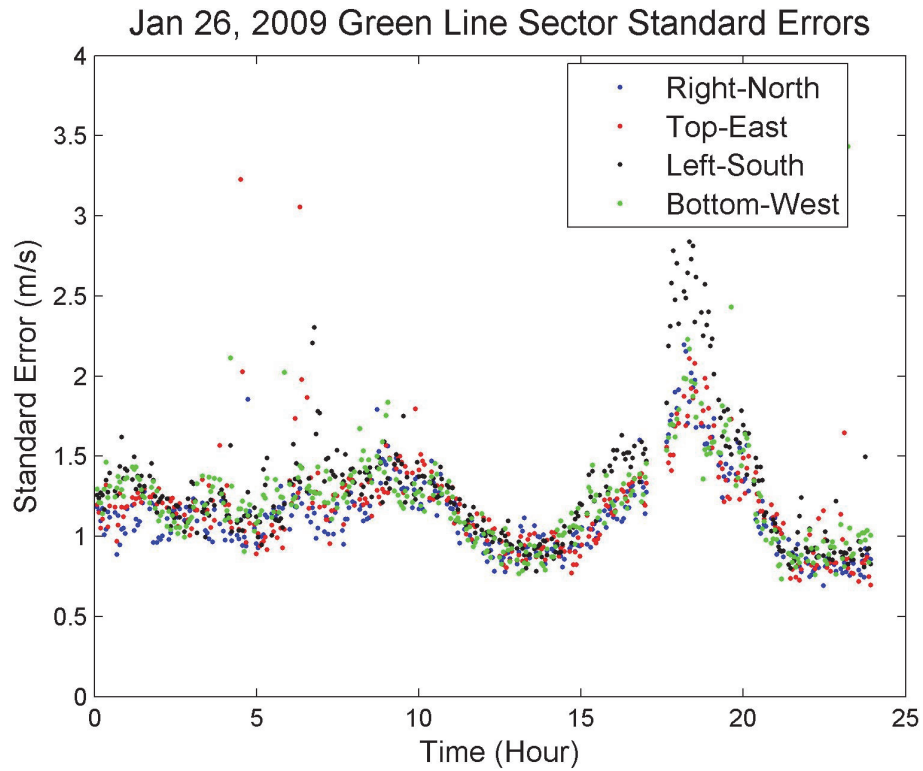


Fig. 8. Standard errors for each of the cardinal direction sectors of the CCD on from 26 January 2009.

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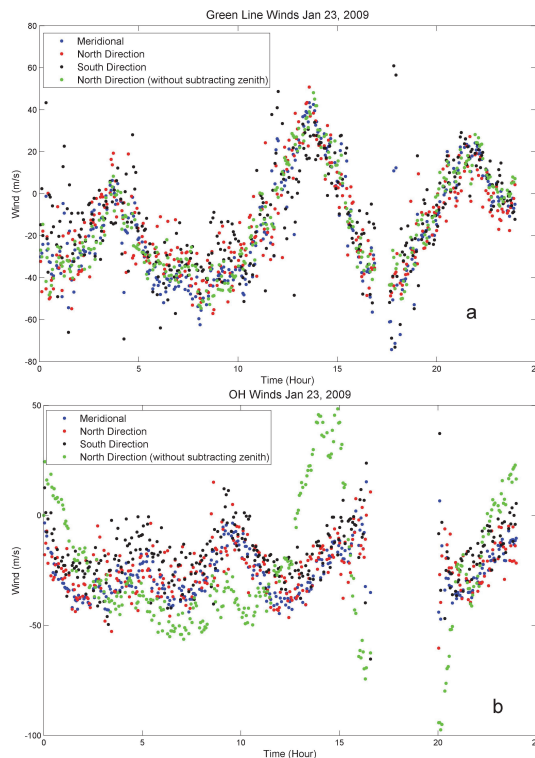


Fig. 9. Time series of meridional winds (ms^{-1}) from 23 January 2009 for the green line **(a)** and hydroxyl emission **(b)** observations showing the consistency of the observations in the north and south directions when thermal drift and zero wind are appropriately accounted for and the problems (green points in panel **b**) when they are not. The standard errors of these observations are approximately the size of the points in the figure. Detailed discussion is in the text.

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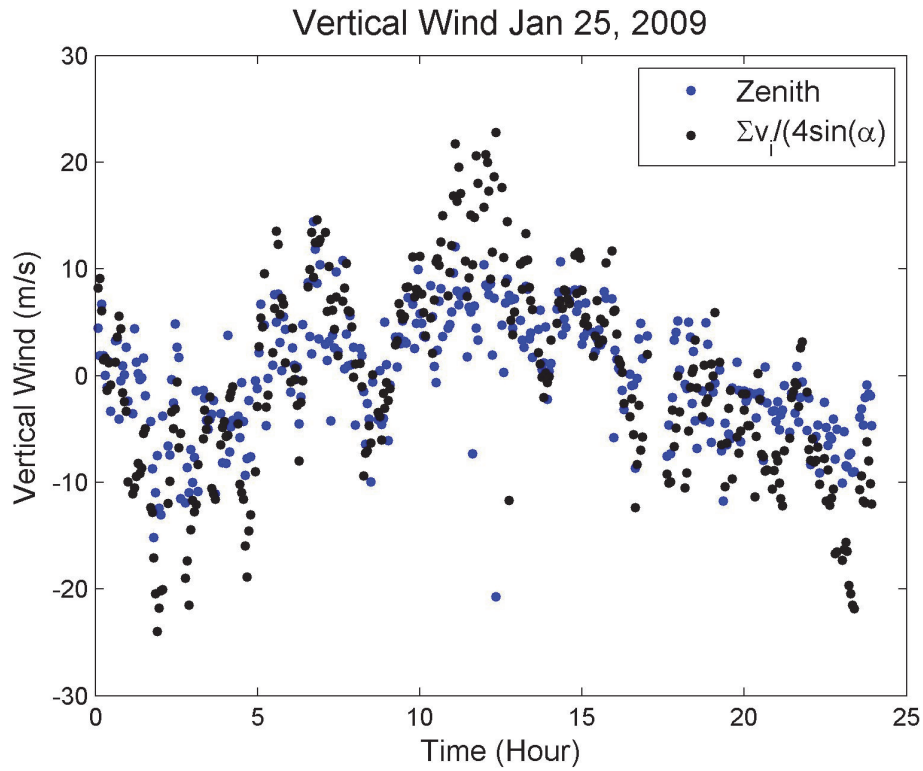


Fig. 10. Green line vertical wind (ms^{-1}) 25 January 2009 as directly observed (blue dots) and as calculated using the north and south winds (black dots) according to Eq. (10).

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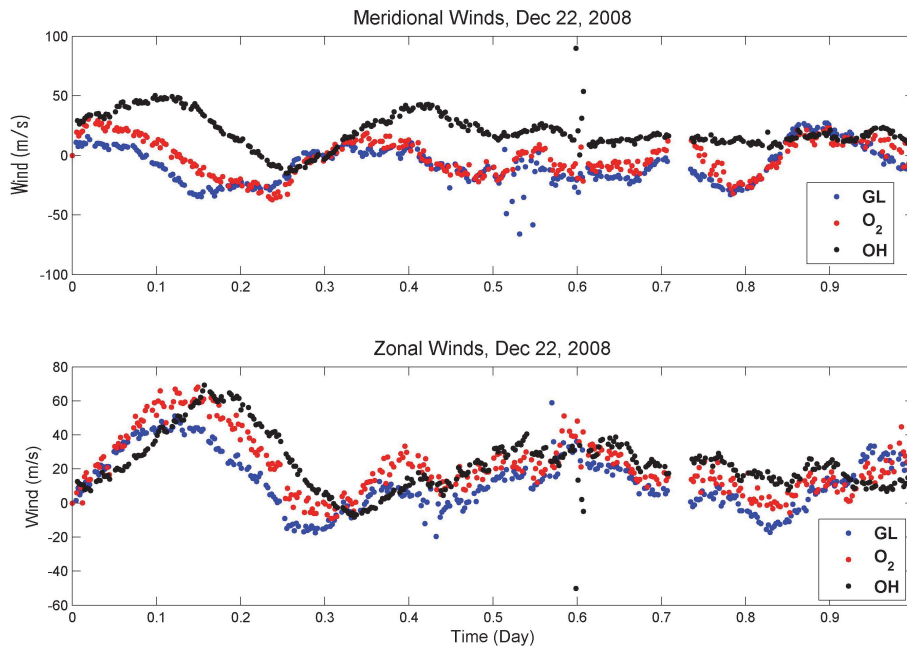


Fig. 11. Time series of the zonal and meridional winds for all three emissions on 22 December 2008. It is interesting to note that larger scale variations first show up in the green line winds, followed by O_2 and then OH. This is expected for upward propagating tides for which the phase front propagates downward. Standard errors for each wind measurement are smaller than the dots in the figure for green line and OH and about the size of the dot for O_2 .

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