



**Multi-wavelength
optical measurement
to enhance
thermal/optical
analysis**

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Multi-wavelength optical measurement to enhance thermal/optical analysis for carbonaceous aerosol

L.-W. A. Chen^{1,2}, J. C. Chow^{1,2}, X. L. Wang¹, J. A. Robles¹, B. Sumlin¹,
D. H. Lowenthal¹, R. Zimmermann³, and J. G. Watson^{1,2}

¹Division of Atmospheric Sciences, Desert Research Institute, Reno, Nevada, 89512, USA

²Key Laboratory of Aerosol Science & Technology, SKLLQG, Institute of Earth Environment, Chinese Academy of Sciences, Xi'an, China

³Joint Mass Spectrometry Centre, Chair of Analytical Chemistry, Institute of Chemistry, University of Rostock, Rostock, Germany

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Correspondence to: L.-W. A. Chen (antony.chen@dri.edu)

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Abstract

A thermal/optical carbon analyzer equipped with seven-wavelength light source/detector (405–980 nm) for monitoring spectral reflectance (R) and transmittance (T) of filter samples allows “thermal spectral analysis (TSA)” and wavelength (λ)-dependent organic carbon (OC)-elemental carbon (EC) measurements. Optical sensing is calibrated with transfer standards traceable to absolute R and T measurements and adjusted for loading effects to determine spectral light absorption (as absorption optical depth [$\tau_{a,\lambda}$]) using diesel exhaust samples as a reference. Tests on ambient and source samples show OC and EC concentrations equivalent to those from conventional carbon analysis when based on the same wavelength (~ 635 nm) for pyrolysis adjustment. TSA provides additional information that evaluates black carbon (BC) and brown carbon (BrC) contributions and their optical properties in the near-IR to the near-UV parts of the solar spectrum. The enhanced carbon analyzer can add value to current aerosol monitoring programs and provide insight into more accurate OC and EC measurements for climate, visibility, or health studies.

1 Introduction

Thermal/optical analysis (TOA) quantifies particulate matter (PM) organic carbon (OC) and element carbon (EC) collected on quartz-fiber filters (Watson et al., 2005; Cao et al., 2007; Bougiatioti et al., 2013). TOA based on the IMPROVE_A protocol (Chow et al., 2007a, 2011) has determined OC and EC concentrations in tens of thousands of samples each year from long-term chemical speciation networks operated in the US (IMPROVE, 2014; USEPA, 2014), Canada (Dabek-Zlotorzynska et al., 2011), and China (Zhang et al., 2012). IMPROVE_A specifies stepped heating up to 580 °C in an inert helium (He) atmosphere (> 99.99 % purity), where most organic compounds are either evaporated or decomposed (Chow et al., 1993), followed by a second stage of stepped heating to 840 °C in 98 % He/2 % O₂ to remove EC on the filter. Since some

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of the OC is converted to EC through pyrolysis in pure He, as evidenced by darkening of the filter, IMPROVE_A also specifies a reflectance pyrolysis adjustment. Reflected light at wavelength $\lambda = 633$ nm is monitored throughout the heating (Huntzicker et al., 1982). OC and EC are defined as carbon evolved before and after the filter reflectance (R) returns to its initial level, respectively.

In addition to reflectance, some TOA protocols use transmitted light (T) to monitor the pyrolysis (Birch and Cary, 1996; Turpin et al., 1990). EC based on R or T splits are referred to as ECR and ECT, respectively. In addition to particle deposits, adsorbed organic vapors within the quartz-fiber filter (Chow et al., 2010; Watson et al., 2009) can pyrolyze during the analysis (Yang and Yu, 2002; Chow et al., 2004). ECR differs from ECT since the R signal is dominated by pyrolyzed OC (POC) on the filter surface while the T signal is influenced by POC both on and within the filter (Chen et al., 2004; Chow et al., 2004). Unlike IMPROVE_A which reports both ECR and ECT, other TOA protocols employ different temperature steps, often reporting only the ECT results (Birch and Cary, 1996; Cavalli et al., 2010; NIOSH, 1999; Schauer et al., 2003; Peterson and Richards, 2002).

The R and/or T measurements as part of TOA can infer the light absorption coefficient (b_{abs}), analogous to the principle of optical absorption monitors such as the aethalometer (Hansen et al., 1984), particle-soot absorption photometer (PSAP; Bond et al., 1999), and the multi-angle absorption photometer (MAAP; Petzold and Schönlinner, 2004). Both the aethalometer and PSAP apply T attenuation while the MAAP incorporates both R and T attenuations in the calculation of b_{abs} . In any case, it is necessary to compensate for multiple scattering and loading effects of the particle-filter matrix that causes deviations from the simple Beer's Law (Chen et al., 2004; Arnott et al., 2005b; Virkkula et al., 2005). Black carbon (BC) concentrations can be derived from b_{abs} by applying a mass- and wavelength-specific absorption efficiency (MAE_{λ} , typically in $\text{m}^2 \text{g}^{-1}$). Many collocated measurements showed high correlations but different slopes in BC/EC comparisons (Ahmed et al., 2009; Quincey et al., 2009; Reisinger et al., 2008; Snyder and Schauer, 2007; Chow et al., 2009). This confirms

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the overlapping concept of EC and BC but also signifies the complex nature of carbonaceous material and uncertainties in such measurements (Andreae and Gelencser, 2006; Moosmüller et al., 2009; Petzold et al., 2013; Lack et al., 2014).

While BC (or EC) absorbs light strongly across the solar spectrum (300–1000 nm), some organic compounds that evolve in the OC step can also absorb light, especially at shorter wavelengths (< 600 nm). These compounds have been termed “brown carbon” (BrC), and are associated with the smoldering phase of biomass burning and some end-products of secondary aerosol formation (Andreae and Gelencser, 2006; Clarke et al., 2007; Zhang et al., 2011). The spectral dependence of b_{abs} is often described by α :

$$\alpha(\lambda) = -\frac{d\ln(b_{\text{abs}}(\lambda))}{d\ln(\lambda)} \quad (1)$$

where $\alpha(\lambda)$ is the absorption Ångström exponent. For BC (or EC) with graphitic-like structure and a constant refractive index, $\alpha = 1$, and b_{abs} is proportional to λ^{-1} . For BrC and mineral dust, α varies with λ and is mostly > 1 (Moosmüller et al., 2009; Chen et al., 2014), causing b_{abs} to increase more rapidly towards shorter wavelengths (blue and ultraviolet) than is the case for BC. The aerosol deposit thus appears to be brown, or sometimes yellow, red, and chartreuse, as the longer wavelengths of illuminating light are reflected and the shorter wavelengths are absorbed. The multi-wavelength aethalometer has revealed different spectral patterns that are indicative of BC, BrC, dust, and their mixtures (Sandradewi et al., 2008; Favez et al., 2009; Yang et al., 2009).

Given the large number of samples per year analyzed by TOA worldwide, the optical data acquired as part of the analysis could be used, in addition to OC and EC, for studies relevant to source apportionment, human health, visibility, and climate. Described and characterized here is a retrofit of a TOA carbon analyzer that expands the single-wavelength R and T monitoring to seven wavelengths for the IMPROVE_A analysis, hereafter designated as Thermal/Spectral Analysis (TSA). Equivalence of the OC and EC fractions for TOA and TSA is demonstrated for several source and receptor sam-

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ples, and the wavelength dependence of OC-EC split is investigated. An approach to report spectral b_{abs} (as aerosol optical depth) and α for decoupling the BC and non-BC components is also introduced.

2 Instrument design and calibration

The 633 nm He/Ne (Ne) laser in the DRI Model 2001 carbon analyzer (Chow et al., 2011; Chen et al., 2012) is replaced with a package of 7 diode lasers with wavelengths (λ) of 405, 455, 532, 635, 780, 808, and 980 nm covering the visible and near infrared regions. The lasers are alternately pulsed (two consecutive pulses per laser, 14 pulses per cycle) and lock-in amplified at a frequency of 30 Hz, resulting in two cycles and ~ four pulses for each wavelength every second. The bifurcated fiber-optic for delivering the He/Ne laser to the reflectance light pipe is replaced with an eight-furcated optical-fiber bundle, one for each of the lasers and the last for transferring the light reflected from the filter punch (0.5 cm^2) to a photodiode (Fig. 1). Another light pipe on the opposite side of the filter directs the transmitted light toward a separate photodiode detector.

Photodiode signals are acquired with a NI6216 data acquisition system (National Instruments, Austin, TX) at a rate of up to 100 000 data points per second. The system integrates the product of photodiode and reference (30 Hz square wave) signals every second to suppress noise (e.g., from 60 Hz power supply and oven glow, random noise, and baseline drift). The resulting integrals are reported as the spectral laser reflectance and transmittance (LR_λ and LT_λ , respectively). Example thermograms with LR_λ and LT_λ are illustrated in Fig. S1 of the Supplement.

LR_λ and LT_λ are relative terms depending on not only optical properties of the sample but also laser intensity and response of the photodiode. They are related to absolute filter reflectance and transmittance (FR_λ and FT_λ , i.e., fraction of light reflected from or transmitted through the filter, respectively) using a set of transfer standards consisting of eight $\text{PM}_{2.5}$ quartz-fiber filters acquired using high-volume samplers from the Fresno

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Supersite (Watson et al., 2000; Chow et al., 2009), with EC loadings ranging from 0.9 to 15.8 $\mu\text{g cm}^{-2}$. The high-volume filters (406 cm^2) represent well-characterized urban aerosol while providing sufficient sample for extensive testing. FR_λ and FT_λ of the transfer standards were pre-determined using an integrating-sphere spectrometer (Lambda 35, Perkin Elmer, Massachusetts, USA, e.g., see Zhong and Jang, 2011; Chen et al., 2014) traceable to the National Institute of Standard and Technology for wavelengths between 300 and 1000 nm.

Figure 2 compares LR_λ and LT_λ with FR_λ and FT_λ , respectively, for the transfer standards. Within the range of FR_λ (0.1–0.8) and FT_λ (0.0001–0.1), highly significant linear relationships ($r^2 > 0.9$) demonstrate the stability of LR_λ and LT_λ measurements and the feasibility of converting them to FR_λ and FT_λ through calibration with a standardized spectrometer. Figure S1 in the Supplement illustrates the changes in FR_λ and FT_λ retrieved from LR_λ and LT_λ throughout a typical TSA. The uncertainty of FR_λ and FT_λ retrievals may be evaluated by the coefficient of variance of root mean square residual (CV-RMSR) in the $\text{FR}_\lambda/\text{LR}_\lambda$ and $\text{FT}_\lambda/\text{LT}_\lambda$ regression, respectively:

$$\text{CV-RMSR} = \frac{1}{Y_{\text{obs}}} \sqrt{\frac{\sum (Y_{\text{cal}} - Y_{\text{obs}})^2}{n - 2}} \quad (2)$$

where Y_{obs} is the FR_λ or FT_λ measured by integrating-sphere spectrometer, Y_{cal} is the FR_λ or FT_λ calculated from LR_λ or LT_λ , respectively, and n is the number of samples. $\text{FR}_{633\text{nm}}$ and $\text{FT}_{633\text{nm}}$ based on He/Ne laser of a typical Model 2001 analyzer exhibit a $\sim 3\%$ uncertainty (Fig. 2). For this retrofit, FR_λ uncertainties range from 3 to 11% and FT_λ uncertainties range from 5 to 18%, with the best precision shown at 455 and 808 nm.

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Schmid et al., 2001), consistent with organic vapors pyrolyzed within the filter leaving the sample after native EC and POC in the surface deposit have evolved (Chen et al., 2004). POC was least apparent for the diesel exhaust samples where optical adjustments were negligible.

5 Table 2 compares OC-EC splits for 635 nm with splits derived from shorter (455 nm) and longer (808 nm) wavelengths that have relatively low LR/LT uncertainties. Chow et al. (1993) observed that the operational definition for EC defined by a TOA protocol might contain some light-absorbing OC. When BrC is present, its contribution to EC would increase as the wavelength used for the OC-EC split decreases, with the 880 nm
10 split being the least sensitive to BrC. Even in the absence of BrC, pyrolysis adjustment can depend on wavelength due to different spectral dependences of MAE for EC and POC.

ECR based on the 635 nm split agree well with those based on the 808 nm split (i.e., slopes within the standard error from unity and $p(\text{RD}) > 0.02$) for all the sample
15 types. This suggests that the 633 nm R-split used for optical adjustment since Huntzicker et al. (1982) does not respond to the BrC and POC characteristics more than longer visible or infrared wavelengths. For ECT, the 880 nm split yielded higher values than the 635 nm split, especially for biomass burning dominated samples. This is consistent with ECT being more influenced by POC within the filter, and this effect on
20 the T-split increases with decreasing wavelength (thus, increasing multiple scattering enhancement for absorption).

The 455 nm split appears to be sensitive to BrC content, as evidenced by larger ECR than those determined with 635 nm (except for diesel exhaust samples where BrC contents are low). The difference is largest for the aged Reno wildfire samples, which
25 may also contain some secondary organic aerosol formed during transport over the 200 km distance between Yosemite National Park and Reno, Nevada. As demonstrated in Fig. S1 in the Supplement, shorter wavelengths produce earlier splits, resulting in higher ECR concentrations. The increase of ECT due to a 455 nm optical correction is

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not evident, which may be due to the opposing effects of BrC and POC at the shorter wavelength.

4 Multi-wavelength absorption retrieval

Light absorption by particles on the filter is often estimated by transmittance attenuation (ATN):

$$ATN_{\lambda} = -\ln\left(\frac{FT_{\lambda,i}}{FT_{\lambda,f}}\right) \quad (3)$$

where i and f indicate FT_{λ} measured before and after thermal analysis, respectively. $FT_{\lambda,f}$ approximates a blank filter since all of the carbon has been removed. ATN_{λ} includes scattering and absorption within the substrate. On the other hand, the absorption optical depth ($\tau_{a,\lambda}$) measures only the light absorption. For diesel soot samples with negligible BrC and POC,

$$\tau_{a,\lambda} = MAE_{\lambda,EC} \cdot [EC] \quad (4)$$

where $[EC]$ is the areal concentration of EC on filter in $\mu\text{g cm}^{-2}$. If there were not filter effects, ATN and τ_a would be identical for a given λ as described by the Beer's Law. With the knowledge of sampling volume (V) and filter area (A), ambient b_{abs} can be calculated from $\tau_a \cdot A/V$.

The relationship of $[EC]$ and $ATN_{635\text{nm}}$ throughout the EC2 step (740°C in a 98% He/2% O₂ atmosphere) of IMPROVE_A analysis for a diesel exhaust sample is shown in Fig. 4. The temporal variation in $[EC]$, i.e., $d[EC]/dt$, is determined from carbon released and detected by the carbon analyzer. Arnott et al. (2005b) proposed a quadratic relationship between $[EC]$ and ATN , derived from:

$$\frac{dATN_{\lambda}}{dt} = \frac{M_{\lambda} \cdot MAE_{\lambda,EC}}{\sqrt{1 + \beta_{\lambda} \cdot [EC]}} \cdot \frac{d[EC]}{dt} \quad (5)$$

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and thus:

$$[\text{EC}] = \frac{\beta_\lambda}{4(M_\lambda \cdot \text{MAE}_\lambda)^2} \text{ATN}_\lambda^2 + \frac{1}{M_\lambda \cdot \text{MAE}_\lambda} \text{ATN}_\lambda \quad (6)$$

where M_λ and β_λ account for the wavelength-specific multiple scattering and loading effects, respectively. Eq. (6) fits the relationship in Fig. 4 ($r^2 > 0.99$), thereby allowing M_λ and β_λ to be estimated. EC (quantified by IMPROVE_A ECR or ECT) and initial $\text{ATN}_{635\text{nm}}$ (prior to TSA) of all other diesel exhaust samples exhibit a consistent pattern (Fig. 4). This supports the use of $\text{ATN}_{635\text{nm}}$ as a surrogate for EC and light absorption. Similar relationships hold between $[\text{EC}]$ and ATN for other wavelengths (Fig. S2 in the Supplement). The largest scatter for 532 nm corresponds to the highest uncertainty in $\text{FT}_{532\text{nm}}$ retrievals; it is attributed to low sensitivity of the transmittance photodiode detector at this wavelength, which has been addressed in a subsequent design of the retrofit optics.

To relate $\tau_{a,635\text{nm}}$ to $\text{ATN}_{635\text{nm}}$, a MAE (EC) of $7.4 \text{ m}^2 \text{ g}^{-1}$ at 635 nm was used. The MAE was derived from concurrent b_{abs} , by a photoacoustic sensor at 1047 nm, and EC, by IMPROVE_A, measurements during the Gasoline/Diesel Split Study (Arnott et al., 2005a) and assuming an α of 1 in Eq. (1). The quadratic relationship holds for all of the available wavelengths, as seen in Fig. 5. Light absorption is enhanced by the filter since any $\tau_{a,\lambda} < 1$ corresponds to a larger ATN_λ , with more amplification towards shorter wavelengths. These $\tau_{a,\lambda}$ – ATN_λ relationships would apply to any samples, regardless of the nature of light-absorbing material (e.g. EC, BC, BrC, or mineral dust). Particle penetration depth and, to a lesser degree, single scattering albedo and the asymmetric g factor can influence the $\tau_{a,\lambda}$ – ATN_λ dependence, though for a similar sampling configuration and filter material/thickness with typical loading, the perturbation is expected to be small (Chen et al., 2004; Arnott et al., 2005b).

Using the relationships in Fig. 5, $\tau_{a,\lambda}$ were calculated for all samples from the initially measured ATN_λ values, with average $\tau_{a,\lambda} \cdot \lambda$ by sample type compared in Fig. 6. The nearly constant $\tau_{a,\lambda} \cdot \lambda$ for diesel exhaust samples, i.e., $\tau_{a,\lambda} \propto \lambda^{-1}$, is consistent with

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the exclusive contribution of EC to light absorption. BC derived from the $\tau_{a,\lambda}$ would be equivalent to diesel EC. Averaged $\tau_{a,\lambda} \cdot \lambda$ increases by factors of 1.5, 3.0, and 3.9 from 980 nm to 405 nm for the Fresno ambient, Reno wildfire, and prescribed burning samples, respectively. This reflects different levels of non-EC contribution.

5 Separation of BC and BrC contributions

A simplified two-component model consisting of BC and BrC, each with explicit absorption Ångström exponents (α_{BC} and α_{BrC}), is used to explain the spectral dependence of $\tau_{a,\lambda}$ in the samples:

$$\tau_{a,\lambda} = q_{BC} \cdot \lambda^{-\alpha_{BC}} + q_{BrC} \cdot \lambda^{-\alpha_{BrC}} \quad (7)$$

where q_{BC} and q_{BrC} are fitting coefficients. This is analogous to the approach of Sandradewi et al. (2008) who considered the two components to be traffic and wood burning particles. Assuming a α_{BC} of 1 the same as diesel EC, then:

$$\tau_{a,\lambda} \cdot \lambda = q_{BC} + q_{BrC} \cdot \lambda^{-(\alpha_{BrC}-1)} \quad (8)$$

Fitting coefficients in Eq. (8) were obtained for any given α_{BrC} between 2 and 8 by least-square linear regression, and the α_{BrC} that led to the overall best fit in terms of r^2 was selected as the effective absorption Ångström exponent of BrC with which $\tau_{a,\lambda,BC}$ and $\tau_{a,\lambda,BrC}$ can be calculated from the first and second terms of Eq. (7). For each of the 44 samples, Fig. S3 (Supplement) shows that fitted $\tau_{a,\lambda}$ are within $\pm 5\%$ of the measured values for $\tau_{a,\lambda} > 0.01$. Examples of the $\tau_{a,\lambda}$ decomposition as a function of wavelength are shown in Fig. S4 in the Supplement.

Table 3 summarizes the apportionment of $\tau_{a,635\text{nm}}$ into BC and BrC fractions along with average α_{BrC} , “diesel-EC-equivalent” BC (termed BC_d hereafter), ECR, and ECT by sample type. Consistent with Fig. 5, BrC contributions to $\tau_{a,635\text{nm}}$ are much higher in prescribed burning than in diesel exhaust samples (averaging 46 % vs. 1 %) while

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somewhere in between (10–26 %) for Fresno and Reno wildfire samples. Effective α_{BrC} compare well among Fresno, Reno wildfire, and prescribed burning samples (4.2–4.8), and are consistent with BrC of a similar nature from biomass burning (Bahadur et al., 2012; Kirchstetter and Thatcher, 2012). Even in the infrared region BrC accounts for 3, 6, and 24 % of $\tau_{\text{a},980\text{nm}}$ for the Fresno, Reno, and prescribed burning samples, respectively, on average. α_{BrC} in diesel exhaust, detectable in 5 of 11 samples, appears to be significantly lower (2.3 ± 0.1) than other sample types.

Table 3 shows that BC_{d} as determined from $\tau_{\text{a},635\text{nm},\text{BC}}/\text{MAE}_{635\text{nm}}$ ($7.4 \text{ m}^2 \text{ g}^{-1}$) are lower than $\text{ECR}_{635\text{nm}}$. The differences are especially significant (i.e., p value of $\text{RD} < 0.01$) for Reno wildfire and Tahoe prescribed burning samples with relatively high BrC contributions. The comparisons do not change with $\text{ECR}_{808\text{nm}}$ (with low BrC influence) replacing $\text{ECR}_{635\text{nm}}$. A continuum of light-absorbing carbon, ranging from BrC, char, to soot, from biomass burning as suggested by Pöschl (2003) and Masiello (2004) may explain the discrepancy. As char and soot resulting from pyrolysis and high-temperature graphitization, respectively, are both quantified as EC by TOA (Han et al., 2009), they may have distinct optical properties. BC_{d} that was calibrated against diesel EC would more represent just the soot fraction because there is little char material in diesel exhausts. $\text{ECT}_{635\text{nm}}$ is substantially lower than $\text{ECR}_{635\text{nm}}$ due to the aforementioned POC effect, and is much closer to BC_{d} for the Reno and Tahoe biomass burning samples but not the Fresno and diesel exhaust samples.

6 Conclusions

Thermal/optical analysis that combines thermal separation and optical monitoring is potentially a powerful tool for analyzing carbonaceous aerosol on filters. Spatiotemporal variations and long-term trends in aerosol loading, chemical composition, sources, and effects have been inferred from OC and EC measurements (e.g., Chen et al., 2012; Hand et al., 2012; Malm et al., 1994; Murphy et al., 2011; Park et al., 2006). As many archived samples may be retrieved for reanalysis and $\sim 40\,000$ new samples are col-

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lected per year in the US long-term networks alone, an enhanced multi-wavelength thermal/optical analyzer would benefit the scientific community that uses the data.

The seven-wavelength (visible to near-infrared regions) TSA with both R and T sensors allows determination of OC-EC split at different wavelengths and light absorption measurements to be made with wavelength-specific loading corrections. In the selected ambient and source $PM_{2.5}$ samples, contributions of BC and BrC to light absorption were decoupled, assuming an absorption Ångström exponent of unity for BC and much higher values for BrC. Thus, BC concentrations optically equivalent to diesel exhaust EC, i.e., BC_d , can be calculated. BrC with average absorption Ångström exponent of 4.2–4.8 is found to be enriched in samples influenced by biomass burning.

Despite the modifications in light source and detection technique, it is shown that the TSA measures OC_{635nm} and EC_{635nm} equivalent to OC_{633nm} and EC_{633nm} from conventional TOA following the same IMPROVE_A protocol with either R or T pyrolysis adjustment. ECR_{635nm} is also consistent with those determined with longer wavelengths (e.g., 808 nm), though OC-EC splits with shorter wavelengths (e.g., 455 nm) increase ECR appreciably showing the effect of BrC. For ECT, the BrC effect is somewhat canceled by an opposite POC effect. The optically derived BC_d underestimate ECR_{635nm} or ECR_{808nm} in biomass burning dominated samples with relatively high BrC content though the agreements are good for other samples. This discrepancy calls for further studies on the optical properties of EC, including soot and char, from biomass burning in contrast to those of diesel soot particles.

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Table 1. Comparison of TC, OCR, OCT, ECR, and ECT between the 633 nm (TOA) and 635 nm (TSA) optical split following the IMPROVE_A protocol.^a

Sample Type	Optical Split (nm) ^b		Sample # and avg. ^c			Corr. r^2	Deming Regression: $y = m \cdot x + b$		RD: $2(y - x)/(y + x)$	
	x	y	n	\bar{x}	\bar{y}		m^c ($\pm 1\sigma^d$)	b^c ($\pm 1\sigma^d$)	mean $\pm 1\sigma$	p^e
TC										
Fresno Supersite	635	633	10	20.30	20.05	1.00	0.97 ± 0.05	0.38 ± 0.75	-0.01 ± 0.04	0.56
Reno Wildfire	635	633	14	30.69	30.21	1.00	0.91 ± 0.06	2.14 ± 1.18	0.04 ± 0.09	0.15
Prescribed Burn	635	633	9	19.27	20.11	1.00	1.06 ± 0.09	-0.32 ± 1.12	0.01 ± 0.14	0.91
Diesel Exhaust	635	633	11	8.10	7.78	0.97	0.99 ± 0.05	-0.26 ± 0.48	-0.06 ± 0.15	0.21
All	635	633	44	20.34	20.23	0.99	0.95 ± 0.07	0.89 ± 1.00	0.00 ± 0.12	0.85
OCR										
Fresno Supersite	635	633	10	16.02	15.91	0.99	0.97 ± 0.06	0.44 ± 0.76	0.00 ± 0.05	0.85
Reno Wildfire	635	633	14	27.62	26.99	1.00	0.90 ± 0.07	2.09 ± 1.27	0.03 ± 0.09	0.30
Prescribed Burn	635	633	9	17.22	18.25	1.00	1.07 ± 0.06	-0.12 ± 0.76	0.03 ± 0.13	0.65
Diesel Exhaust	635	633	11	4.08	3.91	0.52	0.95 ± 0.35	0.04 ± 1.35	-0.04 ± 0.17	0.46
All	635	633	44	16.97	16.91	0.99	0.94 ± 0.08	0.90 ± 0.99	0.00 ± 0.12	0.68
OCT										
Fresno Supersite	635	633	10	17.80	17.82	1.00	1.01 ± 0.03	-0.17 ± 0.43	0.00 ± 0.04	0.85
Reno Wildfire	635	633	14	29.07	28.64	1.00	0.92 ± 0.06	1.93 ± 1.19	0.03 ± 0.08	0.14
Prescribed Burn	635	633	9	18.11	18.92	1.00	1.07 ± 0.05	-0.37 ± 0.72	0.01 ± 0.13	0.65
Diesel Exhaust	635	633	11	4.42	4.14	0.46	1.01 ± 0.46	-0.33 ± 1.91	-0.07 ± 0.20	0.32
All	635	633	44	18.10	18.07	0.99	0.96 ± 0.07	0.74 ± 0.94	-0.01 ± 0.13	0.75
ECR										
Fresno Supersite	635	633	10	4.28	4.15	1.00	0.99 ± 0.06	-0.11 ± 0.17	-0.06 ± 0.08	0.06
Reno Wildfire	635	633	14	3.07	3.22	0.99	1.04 ± 0.07	0.02 ± 0.15	0.12 ± 0.23	0.14
Prescribed Burn	635	633	9	2.05	1.86	0.88	0.92 ± 0.18	-0.03 ± 0.34	-0.13 ± 0.25	0.25
Diesel Exhaust	635	633	11	4.02	3.87	0.99	0.97 ± 0.07	-0.03 ± 0.23	-0.17 ± 0.30	0.12
All	635	633	44	3.37	3.31	0.99	1.00 ± 0.03	-0.05 ± 0.08	-0.04 ± 0.25	0.17
ECT										
Fresno Supersite	635	633	10	2.50	2.23	0.99	0.78 ± 0.12	0.29 ± 0.22	-0.07 ± 0.14	0.13
Reno Wildfire	635	633	14	1.62	1.57	0.98	0.82 ± 0.02	0.24 ± 0.07	0.10 ± 0.30	0.33
Prescribed Burn	635	633	9	1.16	1.18	0.85	0.87 ± 0.10	0.17 ± 0.13	0.07 ± 0.30	0.50
Diesel Exhaust	635	633	11	3.68	3.64	0.99	0.92 ± 0.13	0.24 ± 0.30	-0.08 ± 0.33	0.70
All	635	633	44	2.24	2.16	0.98	0.90 ± 0.03	0.14 ± 0.06	0.01 ± 0.28	0.74

^a TC: Total Carbon; OCR: Organic Carbon by Reflectance; OCT: Organic Carbon by Transmittance; ECR: Elemental Carbon by Reflectance; and ECT: Elemental Carbon by Transmittance following the IMPROVE_A thermal/optical carbon analysis protocol (Chow et al., 2007). TOA: Thermal/Optical Analyses; and TSA: Thermal/Spectral Analyses.

^b x is by modified 7-wavelength carbon analyzer; y is by conventional single-wavelength (633 nm) DRI Model 2001 thermal/optical carbon analyzer.

^c Concentration in $\mu\text{g cm}^{-2}$; m is the slope; b is the intercept in $\mu\text{g cm}^{-2}$.

^d σ : Standard deviation.

^e Student's t test p values.



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Table 2. Comparison of TSA-determined 635 nm ECR and ECT with 880 nm and 455 nm following the IMPROVE_A protocol.

Sample Type	Optical Split (nm) ^a		Sample # and avg. ^b			Corr.	Deming Regression: $y = m \cdot x + b$		RD: $2(y - x)/(y + x)$	
	<i>x</i>	<i>y</i>	<i>n</i>	\bar{x}	\bar{y}		r^2	$m^b (\pm 1\sigma^c)$	$b^b (\pm 1\sigma^c)$	mean $\pm 1\sigma$
ECR										
Fresno Supersite	635	455	10	4.28	4.74	1.00	1.23 ± 0.04	-0.55 ± 0.13	0.01 ± 0.13	0.82
Reno Wildfire	635	455	14	3.07	4.29	0.95	1.90 ± 0.58	-1.55 ± 1.24	0.14 ± 0.25	0.06
Prescribed Burn	635	455	9	2.05	2.14	0.98	1.41 ± 0.23	-0.74 ± 0.39	-0.03 ± 0.16	0.57
Diesel Exhaust	635	455	11	4.02	3.93	1.00	1.00 ± 0.01	-0.10 ± 0.06	-0.08 ± 0.11	0.06
All	635	455	44	3.37	3.86	0.90	1.36 ± 0.28	-0.71 ± 0.66	0.02 ± 0.19	0.76
ECT										
Fresno Supersite	635	808	10	4.28	4.12	1.00	0.95 ± 0.08	0.06 ± 0.22	-0.05 ± 0.05	0.03
Reno Wildfire	635	808	14	3.07	3.22	1.00	1.04 ± 0.08	0.03 ± 0.17	0.15 ± 0.23	0.02
Prescribed Burn	635	808	9	2.05	2.12	0.99	1.00 ± 0.09	0.06 ± 0.17	0.03 ± 0.09	0.30
Diesel Exhaust	635	808	11	4.02	4.00	1.00	1.00 ± 0.00	-0.02 ± 0.02	-0.01 ± 0.02	1.00
All	635	808	44	3.37	3.40	1.00	0.99 ± 0.03	0.05 ± 0.07	0.04 ± 0.16	0.19
ECT										
Fresno Supersite	635	455	10	2.50	2.44	1.00	1.00 ± 0.02	-0.05 ± 0.07	-0.04 ± 0.08	0.16
Reno Wildfire	635	455	14	1.62	1.35	0.99	0.85 ± 0.06	-0.02 ± 0.06	-0.20 ± 0.14	0.00
Prescribed Burn	635	455	9	1.16	1.07	0.98	1.06 ± 0.25	-0.16 ± 0.22	-0.08 ± 0.24	0.16
Diesel Exhaust	635	455	11	3.68	3.59	1.00	0.97 ± 0.01	0.01 ± 0.04	-0.04 ± 0.06	0.07
All	635	455	44	2.24	2.10	0.99	0.97 ± 0.02	-0.08 ± 0.03	-0.10 ± 0.16	0.00
ECT										
Fresno Supersite	635	808	10	2.50	2.67	1.00	1.03 ± 0.04	0.10 ± 0.08	0.08 ± 0.04	0.00
Reno Wildfire	635	808	14	1.62	2.00	0.99	1.24 ± 0.04	-0.01 ± 0.08	0.18 ± 0.18	0.00
Prescribed Burn	635	808	9	1.16	1.27	0.99	1.10 ± 0.12	-0.01 ± 0.12	-0.09 ± 0.60	0.13
Diesel Exhaust	635	808	11	3.68	3.53	1.00	0.99 ± 0.01	-0.11 ± 0.07	-0.24 ± 0.41	0.01
All	635	808	44	2.24	2.38	0.99	1.01 ± 0.07	0.11 ± 0.12	0.00 ± 0.38	0.02

^a *x* and *y* are both by modified 7-wavelength carbon analyzer, but with optical pyrolysis adjustment at different wavelengths.

^b Concentration in $\mu\text{g cm}^{-2}$; *m* is the slope; *b* is the intercept in $\mu\text{g cm}^{-2}$.

^c σ : Standard deviation.

^e Student's *t* test *p* values.

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Table 3. Average $\tau_{a,635\text{nm}}$ for four sample types and their respective BC and BrC fractions, BrC absorption Ångström exponent, and diesel-EC equivalent BC (BC_d) concentration. IMPROVE_A ECR and ECT determined by the 635 nm optical adjustment are compared to BC in terms of average and p value of the relative difference (RD).

Sample Type	$\tau_{a,635\text{nm}}$	$\tau_{a,635\text{nm},\text{BC}}$	$\tau_{a,635\text{nm},\text{BrC}}$ (% in τ_a)	α_{BC}^a	α_{BrC}	BC_d^b ($\mu\text{g cm}^{-2}$)	ECR ($\mu\text{g cm}^{-2}$)	ECT ($\mu\text{g cm}^{-2}$)	p value ($\text{RD}_{\text{BC,ECR}}$)	p value ($\text{RD}_{\text{BC,ECT}}$)
Fresno (Ambient)	0.33	0.30	0.03 (10%)	1	4.8 ± 1.5	4.0	4.3	2.5	0.02	0.87
Reno (Wildfire)	0.10	0.07	0.02 (26%)	1	4.8 ± 1.7	1.0	3.1	1.6	0.00	0.00
Prescribed Burning	0.04	0.02	0.02 (46%)	1	4.2 ± 1.8	0.3	2.1	1.2	0.00	0.00
Diesel Exhausts	0.26	0.26	0.00 (1%)	1	2.3 ± 0.1	3.5	4.0	3.7	0.05	0.06

^a Pre-assumed values.

^b Calculated from $\tau_{a,635\text{nm},\text{BC}}/(7.4\text{m}^2\text{g}^{-1})$.

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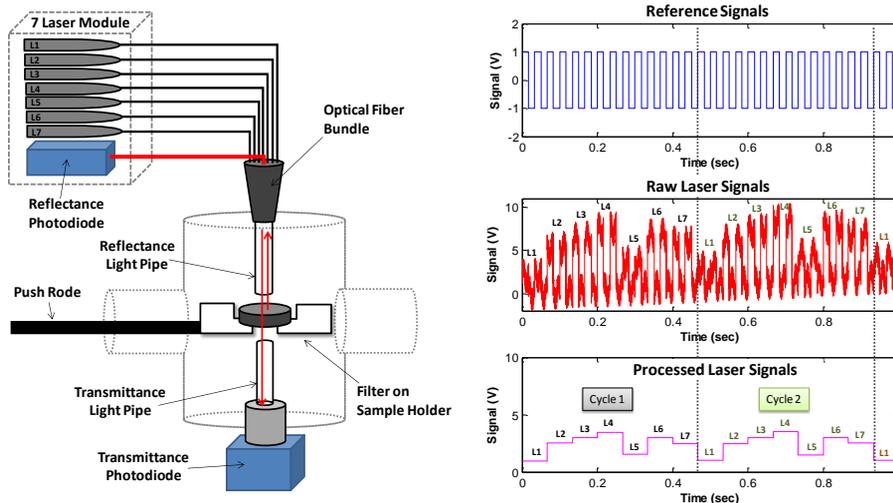


Figure 1. Configuration of optical sensing (left) modified from the DRI Model 2001 analyzer (Chen et al., 2012). The 7-laser module (i.e., L1–L7) represents 7 diode lasers with wavelengths of 405, 455, 532, 635, 780, 808, and 980 nm. Reference (top right) and laser (middle right) signals are modulated at 30 Hz for a lock-in amplification of the reflectance or transmittance signals (bottom right). Only 30 Hz signals with the same phase as the reference are amplified at gains proportional to the reference signal voltage and number of data points integrated.

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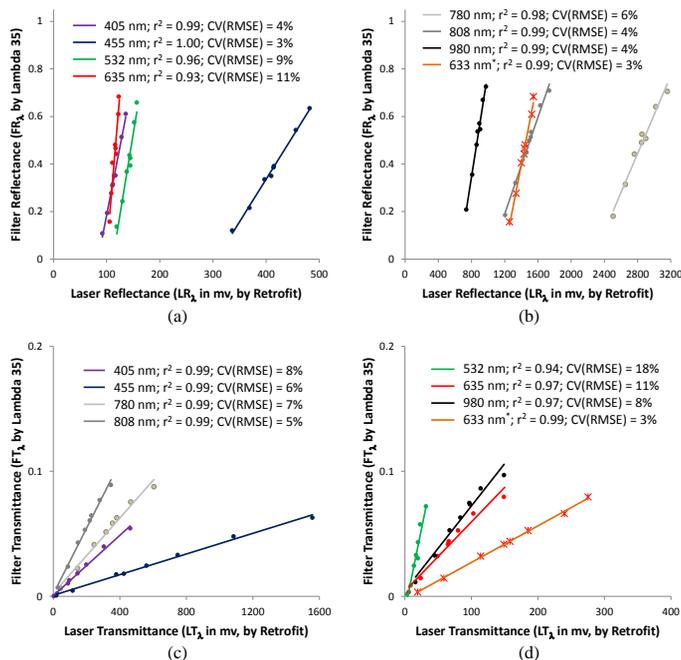


Figure 2. Calibration of spectral laser **(a)**, **(b)** reflectance and **(c)**, **(d)** transmittance measurements (LR_λ and LT_λ , respectively, in millivolts) by the retrofitted 7-wavelength carbon analyzer at room temperature against absolute filter reflectance and transmittance (FR_λ and FT_λ , respectively) quantified by the Lambda integrating-sphere spectrometer, using 8 Fresno ambient samples (5/6, 6/6, 6/19, 7/3, 9/29, 11/4, 11/13, and 12/28 of 2003) of various loadings as transfer standards. The 633 nm data are from a conventional carbon analyzer. r^2 and CV(RMSE) evaluate the regression performance.

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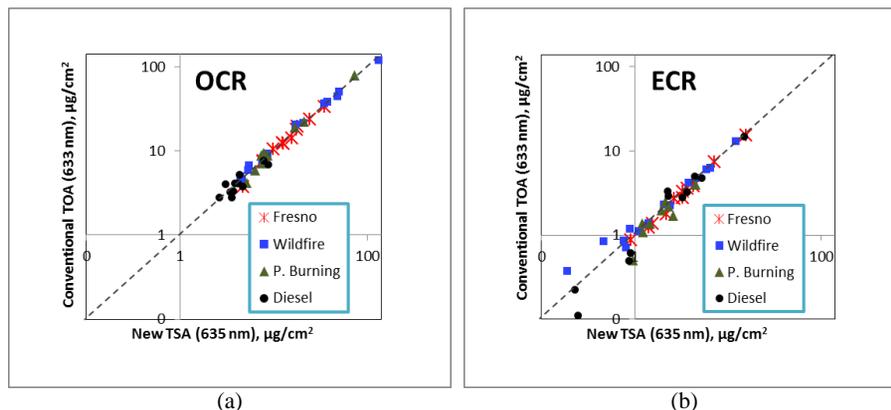


Figure 3. Comparison of organic and elemental carbon by reflectance optical correction (i.e., OCR and ECR, respectively) between the conventional thermal/optical analysis (TOA based on 633 nm optical split) and 7-wavelength thermal/spectral analysis (TSA based on 635 nm optical split) following the IMPROVE_A protocol. Note that both x and y are on log scales.

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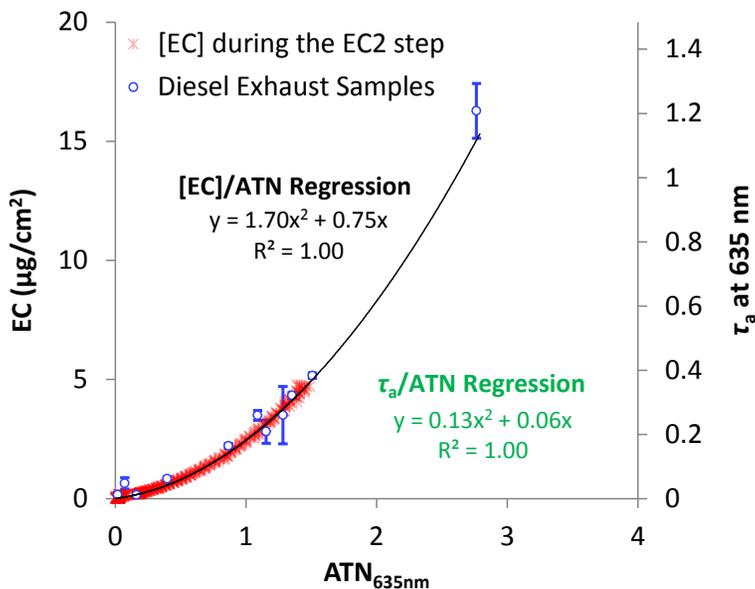


Figure 4. Relationship of EC concentration, [EC], vs. ATN_{635nm} from all 1 s measurements during the EC2 step (740 °C in a 98 % He/2 % O₂ atmosphere) of IMPROVE_A analysis for a diesel exhaust sample (CIFQ074 from the Gas/Diesel Split Study; Fujita et al., 2007). Also shown are paired [EC]- ATN_{635nm} of 11 diesel exhaust samples where EC is determined from IMPROVE_A and ATN_{635nm} from initial filter transmittance. Circles and error bars indicate the average and spread, respectively, of EC by transmittance and reflectance (i.e., ECT and ECR, respectively). $\tau_{a,635nm}$ was further calculated from a MAE of $7.4 \text{ m}^2 \text{ g}^{-1} \times [\text{EC}]$ and the regression result between $\tau_{a,635nm}$ and ATN_{635nm} is shown in green.

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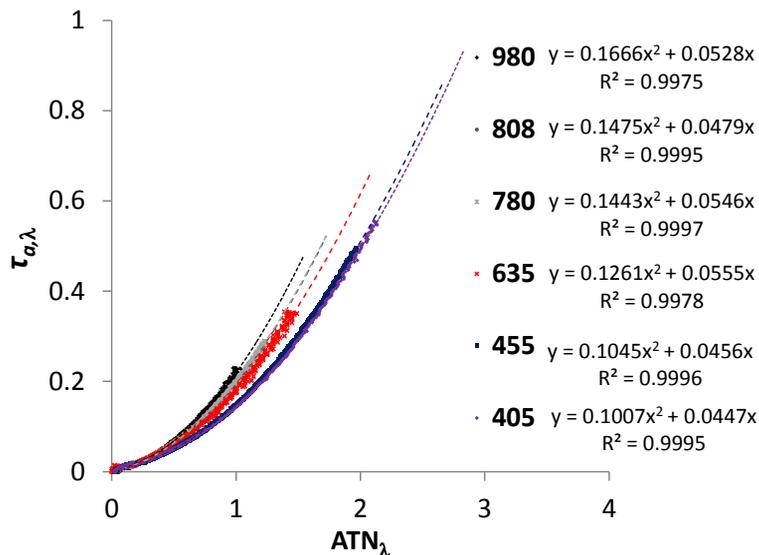


Figure 5. $\tau_{a,\lambda}$ – ATN_{λ} relationships for 405–980 nm wavelengths, based on a diesel exhaust reference sample. Results for 532 nm are not shown owing to lack of sufficient detector signal-to-noise ratio at this wavelength.

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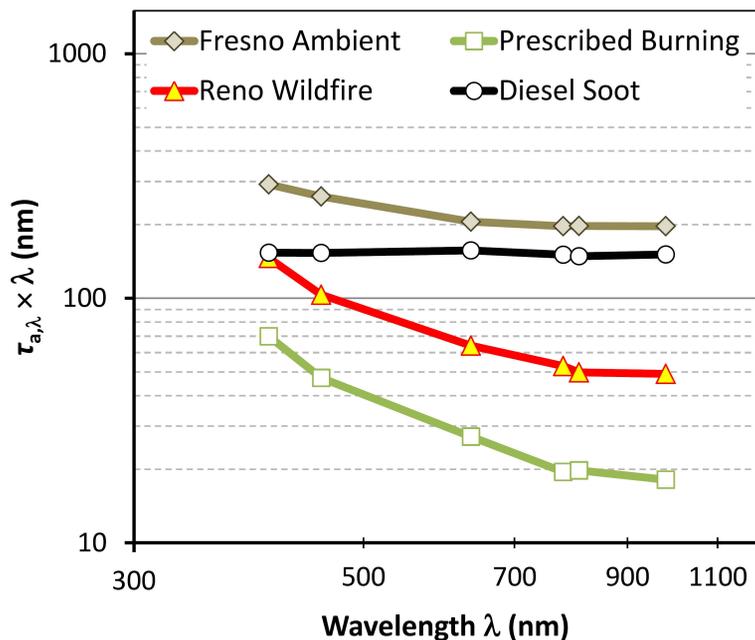


Figure 6. Product of absorption optical depth ($\tau_{a,\lambda}$) and wavelength (λ) as a function of λ by sample type. $\tau_{a,\lambda}$ shown represents averages over each of the sample types.