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**The new
sun-sky-lunar Cimel
CE318-T multiband
photometer**

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



- Data are stored and transferred with 32 bits. As a result, previous digital gains have been eliminated.
- The instrument is designed to run (both daytime and nighttime) with its usual solar panel, for better protection against lightning effects. The internal battery has been suppressed in order to simplify operations, and the power consumption has been reduced. The local interface is improved with a robust touch keyboard and a large backlit graphic LCD display.
- The atmospheric pressure is measured at each group of scenarios by a barometer integrated in the connector panel. The control box is also equipped with inputs to connect a pyranometer and is designed to support a SDI12 bus.
- The control box is equipped with a GPS receiver for improved time synchronization and automatic localization.
- It supports communications through local Serial, local USB and local radio, and remotely through GPRS mobile phone with automatic transfer via FTP or Web site. For isolated locations, it supports communication through satellite DCP with fully automated DCP configuration.

3 Measurement sites

The Izaña Atmospheric Observatory (<http://izana.aemet.es>) is a high mountain atmospheric monitoring station located at 2373 m a.s.l. in Tenerife, Canary Islands, Spain (28.31° N; 16.49° W). It is managed by the Izaña Atmospheric Research Center (IARC) from the State Meteorological Agency of Spain (AEMET). High quality atmospheric measurements are carried out at IZO since it is normally located above a strong and quasi-permanent subsidence temperature inversion typical of the subtropical regime which prevents pollution from lower parts of the island. Clear skies and high atmospheric stability make IZO a suitable site for atmospheric monitoring and calibration

from these paired instruments have been used to validate the new calibration transfer-
ence technique developed for CE318-T. Later, this secondary instrument was sent to
Granada station, where it was in operation during August 2014.

In this work we have used ancillary data collected at IZO from Cimel AERONET
instrument. AERONET Version 2 Level 2.0 AOD data was retrieved from the IZO master
#244 (<http://aeronet.gsfc.nasa.gov>). This information is quality-assured following the
AERONET protocol (Holben et al., 1998). We have also used AERONET Version 2
Level 1.5 not quality assured for data collected in 2015.

A 4-wavelength GAW PFR developed by the WORCC of the PMOD World Radia-
tion Center (<http://www.pmodwrc.ch/worcc/index.html>) is in operation at IZO since July
2001. This instrument provides AOD at 367.6, 412.1, 501.0 and 863.1 nm. The PFR
instrument of IZO is directly linked with WORCC-WMO AOD reference triad of PFRs
that operate at WORCC. During April, May and June, 2014, a PSR prototype (Gröbner
et al, 2012) was running at IZO, providing coincident measurements with PFR, CE318-
AERONET and CE318-T. This spectroradiometer is designed to measure direct solar
irradiance between approximately 300 and 1020 nm with a resolution varying between
1.4 and 6 nm over the wavelength range.

The final part of the AOD evaluation procedure involves CE318-T measurements
performed at Granada station. Nighttime AOD information was obtained using the EX-
CALIBUR star photometer (Astronómica S. L.) which belongs to IISTA-CEAMA. More
details of this system can be found in Pérez-Ramírez et al. (2008b, 2012a). This in-
strument acquires direct star irradiances at 380, 436, 500, 670, 880, 940 and 1020 nm
using a Schmid-Cassegrain telescope and a CCD camera as a detector device. Peri-
odical calibrations of the star photometer are performed at the high mountain station
Calar Alto (37.2° N, 2.5° W, 2168 m a.s.l.), following the calibration technique described
in Pérez-Ramírez et al. (2011). The instrument has been used both to follow day-night
time AOD evolution (Pérez-Ramírez et al., 2012b) and to retrieve aerosol microphysical
properties (Pérez-Ramírez et al., 2015).

The new
sun-sky-lunar Cimel
CE318-T multiband
photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Finally, we have used in this work vertical aerosol backscatter information extracted from a Micropulse Lidar (MPL), MPL-3 (SES Inc., USA) system (Spinhirne et al., 1995). This instrument has been operating at Santa Cruz de Tenerife station (28.5° N, 16.2° W; 52 m a.s.l.) since January 2005 and it is currently in operation within NASA/MPLNET network (<http://mplnet.gsfc.nasa.gov>). It is co-managed by the National Institute for Aerospace Technology (INTA, Spain) and the IARC. Further information about MPL and the calibration techniques can be found in Campbell et al. (2002) and in Welton and Campbell (2002).

4.2 Independent PWV measurements

For PWV intercomparison study we have used, in addition to AERONET level 2.0 PWV measurements, a LEICA GRX1200GGPRO GNSS receiver which belongs to the Spanish National Geographical Institute (IGN), operating at IZO (IZAN station, IERS code 31309M002) within the European Reference Frame network (EUREF, Bruyninx, 2004) since July 2008. This instrument is part of the EUMETNET (Network of European Meteorological Services) GNSS water vapor programme (E-GVAP). It provides instantaneous Zenith Total Delay (ZTD) values every 15 min (GNSS ultra-rapid orbits) by applying the Bernese software version 5.0 (Dach et al., 2007), meanwhile the Zenith Hydrostatic Delay (ZHD) is calculated at IZO with the actual surface pressure at the station, measured with a high-precision SETRA 470 barometer. The methodology to convert ZWD data to PWV is described in Romero et al. (2009). We have used 1 h resolution instantaneous ZTD post-processed values (GNSS precise orbits). The GNSS station at Granada (Granada station, EUREF code 13459M002), managed by the Instituto Andaluz de Geofísica, is equipped with a LEICA GRX1200PRO receptor. Only GNSS ultra-rapid orbits PWV data are available at Granada for the time period studied in this paper.

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



4.3 Lunar irradiance model

Barreto et al. (2013a) described that in lunar photometry it is necessary to use a lunar irradiance model to compute the Moon's extraterrestrial irradiance (I_0 , Eq. 4 of Barreto et al., 2013a), to predict the changes in this quantity through the night. The Robotic Lunar Observatory (ROLO) at the United States Geological Survey (USGS) in Flagstaff, Arizona, has developed a model for the lunar spectral irradiance (Kieffer and Stone, 2005) as part of a NASA-funded effort for on-orbit calibration of remote sensing satellite instruments. The ROLO model can provide the exo-atmospheric lunar irradiance for any given location and time within its valid geometry range, and for any instrument's spectral response within its valid wavelength range. The model is based on fitting thousands of lunar measurements acquired over more than eight years with the ground-based ROLO telescopes in 32 wavelength bands from 350 to 2450 nm. Kieffer and Stone (2005) found band-averaged residuals $\sim 1\%$ from fitting the ROLO dataset with a function of only the geometric variables of phase angle and the sub-solar and sub-observer points on the Moon, i.e. the lunar librations. This value is a measure of the precision of ROLO model predictions of the lunar irradiance over its full range of geometries. For a given night of lunar photometer measurements, the relative prediction precision is well below 1%. In this study, ROLO model computations of I_0 were provided by the USGS team as part of their support to AERONET.

5 Aerosols and PWV determination using the new CE318-T

5.1 Instrument's calibration

Similarly to the standard CE318-AERONET calibration, the CE318-T calibration during daytime period can be performed applying the standard Langley-Bouguer calibration at high mountain stations, using an integrating sphere for sky radiances calibration, or by

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



means of a cross-calibration transference technique. These methods are extensively described in Holben et al. (1998).

According to Barreto et al. (2013a), calibration under nighttime conditions can be also attained by transference from a calibrated instrument (using the ratio of moon measurements, hereinafter called Moon Ratio technique or $\text{Ratio}_{\text{moon}}$) but the absolute calibration can not be performed using the Langley-Bouguer technique. The reason is that, unlike the sun, the moon is a highly variable source which changes continuously with the lunar viewing geometry. Thus, Barreto et al. (2013a) developed the Lunar Langley Method modifying the usual Langley technique to be applied under variable illumination conditions, avoiding the determination of the instrument calibration every night. In this method the calibration coefficient for the instrument i (master with the superscript “M” or secondary with the superscript “S”) can be expressed as,

$$V_{0,\lambda}^i = I_{0,\lambda} \cdot \kappa_{\lambda}^i \quad (1)$$

where $I_{0,\lambda}$ is the extraterrestrial irradiance in a certain channel with a central wavelength at λ , and κ_{λ}^i is the instrument’s calibration constant, which depends on the instrument features. $I_{0,\lambda}$ is calculated using the ROLO model (Kieffer and Stone, 2005). κ_{λ} constant strictly accounts for the instrument’s photometric responsivity and any residual systematic offset difference between ROLO predicted $I_{0,\lambda}$ and the real exoatmospheric irradiance.

Regarding the cross-calibration, and taking the advantage of the increased digital resolution and the simplicity that supposes the use of fixed internal gains, it is possible to establish a new way to transfer the moon absolute calibrations from a CE318-T master to an uncalibrated secondary CE318-T instrument using only daylight period measurements. In this case, we can consider similar the ratio master-secondary of averaged coincident raw data (digital counts or DCs) measured at daytime ($\overline{\text{DC}}_{\text{D}}^i$) and

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



at nighttime ($\overline{DC_N^i}$). Therefore,

$$V_{0,\lambda}^S = V_{0,\lambda}^M \cdot \frac{\overline{DC_N^S}}{\overline{DC_N^M}} \sim V_{0,\lambda}^M \cdot \frac{\overline{DC_D^S}}{\overline{DC_D^M}} \quad (2)$$

with $\frac{\overline{DC_D^S}}{\overline{DC_D^M}} = \text{Ratio}_{\text{sun}}$. This new method avoids the use of nocturnal measurements between master and secondary (or $\text{Ratio}_{\text{moon}}$), which are affected by higher uncertainties and have to meet restrictive criteria about moon illumination. Thus, the called Sun Ratio transference calibration makes the calibration of CE318-T instruments simpler and easier. It implies that, combining Eqs. (1) and (2), once a master instrument is moon calibrated using the Lunar Langley Method (κ_λ^M) it is possible to find the spectral calibration constants for the secondary (κ_λ^S) by means of coincident daytime measurements:

$$\kappa_\lambda^S = \kappa_\lambda^M \cdot \text{Ratio}_{\text{Sun},\lambda} \quad (3)$$

Implicit in this assumption is the fact that the lunar irradiance model ($I_{0,\lambda}$) is the same for master and secondary coincident measurements and also the fact that the $\text{Ratio}_{\text{moon}}$ and the $\text{Ratio}_{\text{sun}}$ are very close, which, in turn, depends on the value of the fixed resistance gains installed in each instrument. These resistances link detector voltages and output voltages, with a different configuration (in parallel or in series) depending on the type of measurement (sun mode or moon/sky mode). As a result, the goodness of the Eq. (3) depends on how uncertain is the assigned value of these resistances ($\sim 1\%$, given by the manufacturer), and the variability of these values between different instruments.

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



5.2 AOD and AE determination

Once κ_λ 's are known, it is possible to determine instantaneous AOD from each individual measurement:

$$\text{AOD}_\lambda = \frac{\ln(\kappa_\lambda) - \ln\left(\frac{V_\lambda}{I_{0,\lambda}}\right) - m_{\text{atm}}(\theta) \cdot \tau_{\text{atm},\lambda}}{m_a(\theta)} \quad (4)$$

The subscript “atm” accounts for air mass and optical depth of all atmospheric attenuators with the exception of aerosols. This term includes the contribution of Rayleigh, O_3 and NO_2 optical depths, calculated using the same equations and resources as AERONET version 2. Atmospheric pressure has been estimated using the common hydrostatic equation because the information from the CE318-T integrated barometer was not available for the time period used in this study.

Since AE is a measure of the wavelength dependence of the AOD (Angström, 1929), it is a qualitative indicator of aerosol particle size (Kaufman et al., 1994) and useful to discriminate different atmospheric aerosol types. This parameter is usually retrieved using AOD within the spectral range between 870 and 440 nm. We can obtain AE using the following equation:

$$\ln(\text{AOD}(\lambda_j)) = \ln(\beta) - \text{AE} \cdot \ln(\lambda_j) \quad (5)$$

5.3 PWV determination

The Beer-Lambert-Bouguer Law must be modified in those spectral regions affected by strong spectral variation of molecular absorption. We do this taking into account the water vapor transmittance: $T_{w,\lambda}$ (Schmid et al., 1996). As Bruegge et al. (1992) and Halthore et al. (1997) showed, $T_{w,\lambda}$ present an exponential dependence with PWV:

$$T_{w,\lambda} = \exp(-a(m_w(\theta) \cdot \text{PWV})^b) \quad (6)$$

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



As shown by Barreto et al. (2013b) for nighttime period, the “*a*” and “*b*” constants can be determined by fitting the simulated $T_{w,\lambda}$ by a radiative transfer model for a specific filter function versus the PWV. Hence, PWV is obtained using the following expression:

$$PWV = \frac{1}{m_w} \cdot \left\{ \frac{1}{a} \cdot \left[\ln\left(\frac{I_{0,\lambda}}{V_\lambda}\right) + \ln(\kappa_\lambda) - m_R \cdot \tau_{R,\lambda} - m_a \cdot AOD_\lambda \right] \right\}^{\frac{1}{b}} \quad (7)$$

In this equation, m_w represents the water vapor optical mass, m_R is the Rayleigh optical mass and $\tau_{R,\lambda}$ is the Rayleigh optical depth within water vapor absorption band. All these values have been obtained using AERONET version 2 references. $I_{0,\lambda}$ is obtained from the ROLO lunar irradiance model, AOD in this spectral region is obtained by extrapolation of AOD at 870 and 440 nm, and “*a*” and “*b*” constants are obtained by simulation of water vapor transmittances using the radiative code MODTRAN 4.0 (Berk et al., 1999) ($a = 0.732$ and $b = 0.611$).

6 AOD combined standard uncertainty estimation

In order to perform a quantitative estimation of the uncertainty involved in AOD retrieved by the CE318-T, we have followed the uncertainty propagation procedure described by the Joint Committee for Guides in Metrology (JCGM, 2008). Equation (8) shows the estimated combined standard uncertainty in AOD (u_{AOD}) considering that the inputs (V_0 , V and m) are not correlated. It is calculated using summation in quadrature of each term u_{x_i} , which represents the standard uncertainty associated with each input. For the sake of brevity wavelength dependence on these inputs has not been included.

$$u_{AOD} = \sqrt{\frac{1}{m^2} \cdot \left[\left(\frac{\delta AOD}{\delta V_0} \right)^2 \cdot u^2(V_0) + \left(\frac{\delta AOD}{\delta V} \right)^2 \cdot u^2(V) + \left(\frac{\delta AOD}{\delta m} \right)^2 \cdot u^2(m) \right]} \quad (8)$$

For daytime period we can consider negligible the instrumental uncertainty due to electro-optical precision (Holben et al., 1998) and due to air mass calculation. Consequently the uncertainty associated with the calibration term $u(V_0)$ is much larger than

The new
sun-sky-lunar Cimel
CE318-T multiband
photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



the uncertainty associated with the other terms. As a result we can estimate the uncertainty in AOD during daytime ($u_{\text{AOD}}^{\text{D}}$) as a function of the error of the zero air mass term modulated by the air mass:

$$u_{\text{AOD}}^{\text{D}} = \frac{1}{m} \cdot \frac{u(V_0)}{V_0} \quad (9)$$

As Holben et al. (1998) and Eck et al. (1999) suggested, the combined standard uncertainty of atmosphere, instrument noise and calibration in CE318-AERONET instruments can be inferred by means of the coefficient of variation (CV) of several V_0 values obtained at a reference station such as Mauna Loa. They found relative uncertainties for reference instruments better than 0.2–0.5 and $\sim 1.5\%$ for field instruments in the visible and the near infrared (IR) range (Eck et al., 1999; Schmid et al., 1999). This yields an uncertainty due to calibration ($u(V_0)$) between 0.002 and 0.005 for reference instruments and ~ 0.015 for instruments calibrated by means of intercomparison techniques. Following Eck et al. (1999) and Toledano et al. (2007), it is necessary to include the errors associated with the estimation of Rayleigh optical depth and gaseous absorptions. In case of CE318-T at daytime period, we also expect negligible instrument uncertainty $u(V)$ (since dark current and triplets are considerably low) as well as similar estimations for Rayleigh and gases optical depths. Assuming the values proposed by Eck et al. (1999), a total AOD uncertainty ($u_{\text{AOD}}^{\text{D}}$) of ~ 0.002 – 0.009 is estimated for reference instruments, and ~ 0.010 – 0.021 for field instruments. Daytime calibration uncertainty due to Langley and intercomparison procedures are also expected to be similar for CE318-T and CE318-AERONET. These assumptions will be discussed in Sect. 6.1.

In case of nighttime measurements, taking into account Eq. (1), an alternative form of Eq. (8) is required, including three additional terms. Two terms attributed to the contribution of $u(V)$ and the uncertainty in the ROLO model ($u(I_0)$), and another term which includes the correlation coefficient r (often called covariance term) of the correlated inputs κ and I_0 (Eq. 10). Please note that the term $u(\kappa)$ corresponds to the uncertainty

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

⏪

⏩

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



due to calibration, and it is similar to the calibration term involved in Eq. (9) for daytime measurements ($u(V_0)$ in this case).

$$\begin{aligned}
 u_{\text{AOD}}^{\text{N}}{}^2 &= \frac{1}{m^2} \left(\frac{u^2(\kappa)}{\kappa^2} + \frac{u^2(I_0)}{I_0^2} + \frac{u^2(V)}{V^2} \right) + \\
 &+ \frac{2}{m^2} \cdot r_{\kappa, I_0} \cdot \left(\frac{\delta \text{AOD}}{\delta \kappa} \right) \cdot \left(\frac{\delta \text{AOD}}{\delta I_0} \right) \cdot u(\kappa) \cdot u(I_0) \\
 &\sim \frac{1}{m^2} \left(\frac{u^2(\kappa)}{\kappa^2} + \frac{u^2(I_0)}{I_0^2} + \frac{u^2(V)}{V^2} \right)
 \end{aligned} \tag{10}$$

Although the existence of a correlation between κ and I_0 can be anticipated, the covariance term is expected to be near 0. The reason for neglecting this term is the low impact of I_0 systematic uncertainties on κ during the Langley period (≤ 2 h). In any case, considering these two magnitudes are inversely correlated (negative covariance), by neglecting this term we are obtaining a conservative estimate of the total uncertainty for the nighttime period. Equation (10) presents a combined uncertainty in AOD measurements at nighttime related to the random uncertainties in calibration process as a result of the linear regression analysis ($u(\kappa)$) in addition to the systematic uncertainties due to ROLO estimations ($u(I_0)$) and instrument uncertainty ($u(V)$). Kieffer and Stone (2005) estimated a relative accuracy of this model $\leq 1\%$, and therefore we expect an additional error in computed AOD of ≤ 0.01 . The term in Eq. (10) associated with the instrument calibration can be obtained, similarly to daytime period, by means of CVs of the κ s obtained from Lunar Langley-calibrated instruments. The estimate of calibration uncertainty at nighttime for field instruments can be performed by analyzing the difference between sun and moon ratios in case of instruments calibrated using Moon Ratio technique. An additional error in AOD determination must be included when the Sun Ratio technique is applied. This term is dependent on the precision in the measurement of the internal resistance gains which relate the sun and moon/sky scenarios and therefore the $\text{Ratio}_{\text{sun}}$ and the $\text{Ratio}_{\text{moon}}$ values. We will estimate and discuss these

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



and full moon (quarter moon) conditions, with values up to 0.016 in 440 nm channel at higher phase angles. For near-IR wavelengths we have obtained a combined standard uncertainty estimation in AOD ranging from 0.012 to 0.017 for full moon conditions and between 0.013 and 0.018 for quarter moon.

6.2 μ_{AOD} estimation for field instruments

In order to estimate the combined standard uncertainty in AOD measurements for CE318-T field instruments we performed the calibration of a secondary instrument using coincident master/secondary measurements taken under stable atmospheric conditions in 22 consecutive days (from 9 to 30 June 2014) and 10 consecutive nights (from 9 to 20 June 2014) in order to ensure the validity of Eq. (3) for $\kappa_{\lambda}^{\text{S}}$ estimation. The different spectral ratio in this lunar cycle at each channel was calculated to show the ratio variability at daytime and nighttime conditions throughout the lunar cycle (Fig. 2 for 11 consecutive days and 10 consecutive nights). We observe that the ratio of measurements during day and night are quite similar in case of high moon illumination conditions, and the ratio performed using nocturnal measurements presents higher dispersion with decreasing moon's illumination. We have found similar standard deviations (σ 's) at daytime and at nighttime for ± 1 night around full moon conditions and ratio sun/moon relative differences (Δratio) $< 0.3\%$ for visible channels (see information included in this figure). Higher Δratio values were obtained for 1020 nm channel (0.57%), attributed to the temperature effect at this spectral range. It implies that a new uncertainty term must be assumed for instruments calibrated by means of the Moon Ratio technique (0.006 for 1020 nm channel and 0.003 for the rest of channels). Consequently, following Eq. (10), a CE318-T instrument calibrated by means of the Moon Ratio calibration technique has a combined standard estimated uncertainty for visible channels of 0.011–0.013 (0.012–0.014) under full moon (quarter moon) conditions, with the exception of 440 nm channel at higher phase angles, with values up to 0.017. In 1640 nm range, we have obtained uncertainties ranging from 0.013 to 0.017 (0.014

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



to 0.018) for full moon (quarter moon), and for 1020 nm channel these values range within 0.014–0.018 (0.015–0.019) for full moon (quarter moon).

In case of field instruments calibrated by means of the Sun Ratio technique we have to take into account the present precision $\leq 1\%$ in the instrumental resistance gains given by the manufacturer. In this respect we have studied the difference between $\text{Ratio}_{\text{sun}}$ and $\text{Ratio}_{\text{moon}}$ in near full moon events for seven different heads (all of them installed at IZO during 2014). Our results showed this relative difference is within the $\pm 1\%$ stated by the manufacturer as the precision limit, wavelength dependent (Fig. 3). Indeed, this figure shows relative differences $< 0.5\%$ for $\lambda \leq 870$ nm and values up to 0.8% for near-IR channels. With this information the additional uncertainty term in those instruments Sun Ratio calibrated can be fixed to values $\leq 0.8\%$ for near-IR channels and $\leq 0.5\%$ for channels in the visible range. Therefore, following Eq. (10), the combined nocturnal AOD uncertainty due to κ , I_0 and V uncertainties in a Sun Ratio calibrated field instrument is expected to be from 0.012 to 0.014 (0.013 to 0.015) for visible wavelength channels at full (quarter) moon conditions with the exception of 440 nm, with values up to 0.017 in case of low moon illumination. For near-IR channels we obtained values from 0.015 to 0.019 (0.016 to 0.020) for 1640 nm channel under full (quarter) moon events, and between 0.016 and 0.020 (0.017 and 0.021) in the case of 1020 nm channel. It assures the validity of the Sun Ratio method for CE318-T calibration as a simple technique with relatively low uncertainties (maximum uncertainties expected to be ≤ 0.021), reducing considerably the complexities of the former Moon Ratio technique.

6.3 Case study to estimate CE318-T precision

Precision, defined as the capability of the instrument to perform measurements repeatedly and reliably, can be inferred from the information extracted from the triplets, as we did previously in Sect. 6.1. However, it is also possible to determine the precision in AOD through an analysis of the AOD measurements and their dispersion under very stable AOD conditions. Thus, the standard deviation in AOD ($\sigma(\text{AOD})$) in such condi-

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



**The new
sun-sky-lunar Cimel
CE318-T multiband
photometer**A. Barreto et al.

[Title Page](#)[Abstract](#)[Introduction](#)[Conclusions](#)[References](#)[Tables](#)[Figures](#)[Back](#)[Close](#)[Full Screen / Esc](#)[Printer-friendly Version](#)[Interactive Discussion](#)

tions provides the information about instrument's precision. For this purpose, we have selected a case study at IZO of three different days and nights between 15 and 18 March 2014, in which AOD conditions were quite stable and moon's illumination was high (full moon in 16 March). In fact, these conditions will be used in Sect. 8 to study into detail the CE318-T performance. We have coincident daytime AOD information in this time period from the CE318-T master, the CE318-AERONET master and the PFR, as well as nighttime AOD information from the same CE318-T master.

Averaged AOD values at daytime of 0.019, 0.013 and 0.013 were found for PFR, CE318-AERONET and CE318-T, respectively, confirming the low aerosol loads in this period. Nighttime averaged AOD was 0.022. The stable AOD conditions were confirmed by means of the analysis of the σ (AOD) of each instrument, with daytime values of 0.009, 0.004 and 0.003 for PFR, CE318-AERONET and CE318-T, respectively, and nighttime values of 0.003. These results confirmed that the CE318-T precision is similar to other reference instruments for both daytime and nighttime (under near full moon conditions).

7 CE318-T intercomparison with reference instruments

The CE318-T AOD and PWV characterization and assessment was carried out at IZO and Granada. Daytime observations at IZO encompass daytime measurements in 2014 taken in 60 days from 1 March to 30 June, meanwhile at nighttime the study is focused on 32 nights, corresponding to four different moon cycles in 2014: 12–23 March, 7–19 April, 7–13 May and 9–16 June. Nocturnal evaluation performed at Granada station involves four nights of collocated measurements CE318-T/star-photometer on 7–8, 9–10, 11–12 and 14–15 August 2014.

7.1 Assessment of the Sun Ratio calibration method

In order to confirm the suitability of the nocturnal calibration transference using the Ratio Sun technique, we have computed the scatterplot of AOD coincident measurements performed at IZO by the master (direct sun and moon calibrated using the Langley and the Lunar Langley methods according to Sect. 6.1), and the secondary (sun calibrated using calibration transference and moon calibrated using both the Sun Ratio and Moon Ratio techniques) (see Fig. 4). The main statistics of the comparison are presented in Table 1. We observed a good agreement between the AOD retrieved at daytime from the master and the secondary (MB and RMSE values ≤ 0.002). For nighttime we obtained similar results by calibrating the secondary instrument using the Ratio_{sun} or the Ratio_{moon}, with MBs and RMSEs slightly higher using daytime ratios, but in all cases within the expected precision for a reference instrument (MBs < 0.004 and RMSEs < 0.008).

7.2 AOD daytime period intercomparison at IZO

We have used three independent and collocated measurements at IZO from PFR, PSR and CE318-AERONET to validate the master CE318-T performance during daytime. As WMO (2005) stated, the preferred method of traceability to evaluate the instrument's accuracy is by means of co-location of representative networks instruments performed at reference wavelengths, trying to ensure a minimum wavelength difference between their channels. Since CE318-T and PFR take measurements at different wavelengths, it is not possible to perform such comparison at all CE318-T channels. For this reason, we have selected for this intercomparison the channels centered \sim at 870 and 500 nm.

There are other specific limits established by WMO (2005) to ensure successful comparisons, besides the minimum wavelength criteria. These limits are: (1) more than 1000 coincident points, (2) minimum of five clear sky days, and (3) AOD values within 0.040–0.200 range during the comparison period. In this study we have satisfied all

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8, 11077–11138, 2015

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



also in agreement with those results found by Kazadzis et al. (2014) for AERONET-PFR comparison at Athens, but our results for 500 nm channel are considerably better.

Consequently, we have obtained similar AOD differences at daytime between CE318-T and reference instruments, as the current CE318-AERONET master and the PFR. As a result we can anticipate a precision of the new CE318-T at daytime similar to the other reference instruments, which is in agreement with the expected daytime accuracies presented in Sect. 6.

7.3 AOD nocturnal intercomparison at Granada

Coincident measurements of the CE318-T secondary instrument (Sun Ratio calibrated) and the star photometer in a temporal window of ± 15 min were performed at Granada during four nights in August 2014 (7–8, 8–9, 11–12 and 14–15). During this period, stellar information in 880, 500 and 440 nm channels, close to CE318-T wavelengths, were extracted. Main statistics of the comparison are presented in Table 2, showing high regression coefficients for the three channels and reduced MBs and RMSEs values in case of longer wavelength channels (≤ 0.001 for 870 nm and ≤ 0.013 for 500 nm). Higher discrepancies were found in the case of 440 nm channel (MB = -0.033 and RMSE = 0.018). The sequence of AOD measured at 500 nm by CE318-T at day and nighttime are displayed in Fig. 7 as well as star photometer nighttime AODs. The scatterplot of AOD extracted from these two instruments at 870, 500 and 440 nm channels is shown in Fig. 8. There is a good agreement between both instruments in the case of 870 and 500 nm channels, with discrepancies lower than the expected accuracies for the star photometer published by Pérez-Ramírez et al. (2011) and also lower than the errors presented in Sect. 6 for field instruments. On the contrary, the differences found in the case of 440 nm channel are higher than those expected for star photometry and slightly higher than the maximum uncertainty values for CE318-T field instruments in visible channels theoretically estimated using Eq. (10) (≤ 0.017 for secondary Sun Ratio calibrated instruments). This might be attributed to a calibration problem in the star photometer in this channel.

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



from 0.09 cm for $FI < 60\%$ to 0.05 cm under near full moon events. Daytime as well as nocturnal measurements are within the expected precision of CE318-AERONET and GNSS under such dry conditions, as reported by Schneider et al. (2010). These authors found a CE318-AERONET expected precision ranging from 7 to 25 %, from dry to humid conditions, the GNSS precision was within 10–20 %, in case of $PWV \leq 0.35$ cm, as in our case. These values also agree with the values found by Barreto et al. (2013b) in the comparison between CE318-U and GNSS PWV data.

PWV comparison at Granada allows us to extend the last evaluation procedure to wetter conditions, including GNSS data for nine different days and five different nights in August 2014 (Fig. 10c), with PWV values up to 3 cm. The comparison criteria is also ± 15 min. Since this information has been obtained using the secondary CE318-T instrument, it has served us as a new evaluation of the secondary's calibration. PWV averaged during this period is 1.70 cm for GNSS and 1.55 cm for CE318-T for daytime, and 1.90 and 1.98 cm, respectively, for nighttime. We have found MBs of -0.15 and 0.09 cm, for daytime and nighttime, respectively, both within the 7–25 % precision expected for CE318-AERONET and 10–20 % precision for GNSS. RMSEs of 0.14 and 0.07 cm and regression coefficients of 0.83 and 0.85 were obtained, respectively.

8 Demonstration case study

The purpose of these case studies is to assess in more detail the performance of the master CE318-T under both very clean free troposphere and dusty conditions, with a quick transition between the two scenarios. This case analysis also provides an opportunity to explore new potential scientific applications of CE318-T since it can measure diurnal changes of aerosols and water vapor (during daytime and nighttime periods) with high temporal resolution, helping to improve our understanding on short-term atmospheric processes.

8.1 IZO, June 2014

During the period 10–18 June 2014 three dust laden intrusions of the SAL, followed by clean background free troposphere conditions, were recorded at IZO with the MPL and the CE318-T (Fig. 11). The coherence between the backscatter signal (Fig. 11a) and the AOD evolution (Fig. 11b) can be seen in this figure. The onset of two of the three dust intrusions are clearly detected in both figures in the late hours of 12 June and also in the first hours of 15 June. The intrusion detected by CE318-T on 14 June was not recorded by MPL because the presence of thick clouds observed at altitudes below IZO, which completely attenuated the lidar signal. Regarding the AE evolution (Fig. 11c) we observe a good agreement between daytime and nighttime measurements during SAL conditions, as is the case of 13 June. However, we observe the presence of a diurnal cycle in AE under free troposphere conditions, with predominantly higher values of AE at nighttime. The first feature is a consequence of the homogeneity of SAL conditions in terms of aerosol properties (Smirnov et al., 1998), while the second feature is attributable to the strengthening of free-troposphere conditions driven by the katabatic regime during nighttime, causing an increase in AE associated with pristine near aerosol-free Rayleigh conditions. This figure also shows the expected higher dispersion in AE as moon's illumination drops. Other assessments can be done from the PWV records (Fig. 11d) within the three SAL events. The expected increase in PWV as a result of the dust intrusions is observed. Saharan air masses are characterized by relatively low and stable humidity levels but higher than those normally present under clean free troposphere conditions, driven by a subsidence regime. This is the case of 13 June at night and 14 June at noon, perfectly matching the dust intrusions. These features were similarly detected by GNSS.

8.2 IZO, March 2014

This is an example of free troposphere conditions affecting IZO during several days (Fig. 12). In this case, from 16 to 21 March, there existed pristine conditions, with AOD

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



0.015 (0.017) for visible (440 nm) channels and 0.015–0.021 for longer wavelengths. To summarize, maximum uncertainties of 0.017 are expected in visible channels and 0.021 in the case of longer wavelengths, all of them for low moon's illumination conditions. These values are the maximum expected values for a typical air mass value of $m = 1$.

We derived daytime AOD for 60 days in March, April, May and June 2014, at IZO using a CE318-T reference instrument (Langley-calibrated). We compared these observations with those extracted from independent reference instruments (CE318-AERONET and PFR) and the PSR prototype, as an assessment of the instrument performance. This AOD comparative study at daytime reported discrepancies similar to sun photometry precision in the AERONET or GAW-PFR networks (≤ 0.01), also similar to the $u_{\text{AOD}}^{\text{D}}$ estimated values. The nocturnal evaluation performed in Granada station using a star photometer and a secondary CE318-T showed similar low discrepancies for 870 and 500 nm channels (~ 0.01), within the $u_{\text{AOD}}^{\text{N}}$ expected values, but higher (~ 0.03) for 440 nm channel. We attributed this discrepancy to a calibration problem in the star photometer in this channel.

A subsequent coherence test for AOD at IZO using the CE318-T and CE318-AERONET masters was focused on the AOD daytime and nighttime differences between 1 h after and before sunset and sunrise. The results of this coherence test match reasonably well the $u_{\text{AOD}}^{\text{N}}$ estimated values in case of visible channels at all illumination conditions. However, in case of near infrared channels, this consistency was only attained in high FI conditions ($> 90\%$). This test also reflects the existence of a faint nocturnal cycle on AOD which impacts more significantly in 1640 nm channel. This cycle possibly reflects a problem in instrument calibration, in nighttime AOD calculation or in the lunar irradiance model, and further investigations must be carried on to properly identify and quantify the causes of the problem.

Regarding PWV, the comparison showed a good agreement between PWV CE318-T/CE318-AERONET and CE318-T/GNSS obtained at day and nighttime conditions for any illumination condition. MB and RMSE values < 0.1 cm were found in case of dry

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



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The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



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The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



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**The new
sun-sky-lunar Cimel
CE318-T multiband
photometer**A. Barreto et al.

[Title Page](#)[Abstract](#)[Introduction](#)[Conclusions](#)[References](#)[Tables](#)[Figures](#)[Back](#)[Close](#)[Full Screen / Esc](#)[Printer-friendly Version](#)[Interactive Discussion](#)

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The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Table 1. Statistics of the master vs. secondary AOD comparison: mean bias (MB), root mean square error (RMSE) and Pearson correlation coefficient (r).

DAYLIGHT ($N = 5566$)						
Channel (nm)	1020	1640	870	675	440	500
MB	0.001	0.002	0.001	0.001	0.001	0.002
RMSE	0.002	0.002	0.002	0.002	0.000	0.002
r	0.999	0.999	0.999	0.999	0.999	0.999
NIGHTTIME -Sun Ratio- ($N = 2319$)						
MB	-0.004	0.001	-0.001	-0.002	-0.002	-0.001
RMSE	0.006	0.003	0.003	0.004	0.008	0.005
r	0.996	0.999	0.998	0.998	0.992	0.996
NIGHTTIME -Moon Ratio- ($N = 2319$)						
MB	-40.001	0.000	-0.001	-0.000	-0.001	-0.000
RMSE	0.005	0.002	0.003	0.003	0.007	0.005
r	0.996	0.999	0.998	0.998	0.992	0.996

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Table 2. Statistics of the CE318-T and star photometer AOD comparison during August 2014: mean bias (MB), root mean square error (RMSE), Pearson correlation coefficient (r) and number of coincidences (N).

Channel (nm)	870	500	440
MB	−0.001	0.013	−0.033
RMSE	0.003	0.009	0.018
r	0.946	0.937	0.911
N	15	15	14

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Table 3. MB and RMSE values for AOD differences between CE318-AERONET daytime and CE318-T nighttime data during sunset-moonrise (SS-MR, defined as the last 1 h of daytime data versus the first 1 h of nocturnal data) as a function of the average moon's fraction of illumination (FI).

		SS-MR						
	# cases		1020	1640	870	675	500	440
60 % \geq FI > 50 %	2	MB	0.035	0.061	0.012	-0.015	-0.008	-0.019
		RMSE	0.037	0.062	0.017	0.018	0.014	0.022
70 % \geq FI > 60 %	2	MB	0.029	0.051	0.008	-0.014	-0.007	-0.015
		RMSE	0.029	0.051	0.009	0.014	0.008	0.016
80 % \geq FI > 70 %	1	MB	0.048	0.056	0.024	0.008	0.016	0.006
		RMSE	–	–	–	–	–	–
90 % \geq FI > 80 %	4	MB	0.016	0.027	0.001	-0.010	-0.012	-0.016
		RMSE	0.018	0.027	0.003	0.011	0.013	0.016
95 % \geq FI > 90 %	3	MB	0.001	0.010	-0.004	-0.010	-0.016	-0.016
		RMSE	0.003	0.010	0.006	0.012	0.017	0.017
FI \geq 95 %	8	MB	0.015	0.009	0.014	0.013	0.010	0.012
		RMSE	0.008	0.006	0.008	0.008	0.008	0.008

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Table 4. MB and RMSE values for AOD differences between CE318-AERONET daytime and CE318-T nighttime data during moonset-sunrise (MS-SR, as the first 1 h of daytime data versus the last 1 h of nocturnal data) as a function of the average moon's fraction of illumination (FI).

			MS-SR					
		# cases	1020	1640	870	675	500	440
50 % \geq FI > 60 %	1	MB	0.012	0.046	0.003	-0.009	-0.008	-0.006
		RMSE	–	–	–	–	–	–
60 % \geq FI > 70 %	1	MB	0.007	0.039	-0.002	-0.014	-0.005	-0.015
		RMSE	–	–	–	–	–	–
80 % \geq FI > 70 %	2	MB	0.007	0.034	-0.001	-0.012	-0.012	-0.017
		RMSE	0.010	0.034	0.003	0.012	0.013	0.017
90 % \geq FI > 80 %	4	MB	0.012	0.023	0.009	0.002	-0.001	-0.001
		RMSE	0.002	0.012	0.001	0.006	0.009	0.009
95 % \geq FI > 90 %	4	MB	0.011	0.016	0.007	-0.002	-0.002	-0.001
		RMSE	0.015	0.018	0.011	0.009	0.011	0.010
FI \geq 95 %	11	MB	-0.001	-0.003	-0.002	-0.004	-0.009	-0.006
		RMSE	0.002	0.004	0.002	0.004	0.008	0.006

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

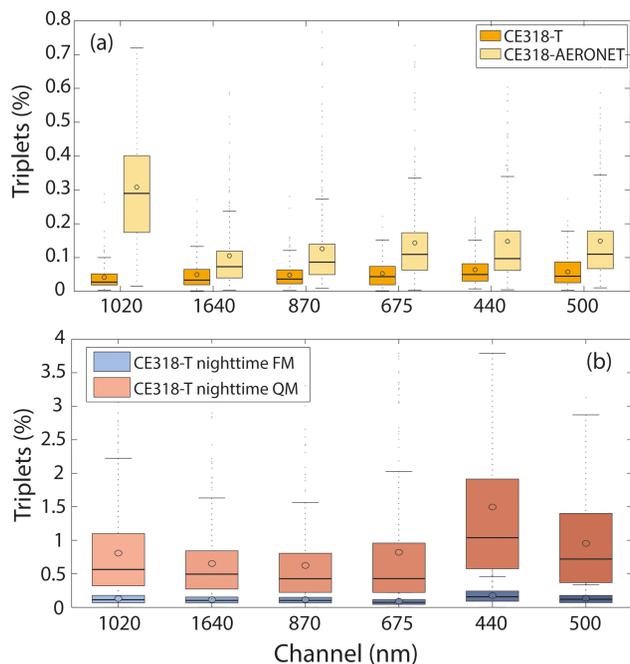


Figure 1. Boxplot of triplets (in %) measured at IZO for **(a)** CE318-T and CE318-AERONET in a daytime period of 23 days from February and March 2015, with pristine conditions ($\text{AOD at } 500 \text{ nm} \leq 0.02$), and **(b)** for CE318-T in a nighttime period of seven nights near full moon (FM, in blue) and five nights near quarter moon (QM, in red) between January and April 2015. In this figure circles represent the mean value while the horizontal line inside each box is the median value.

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

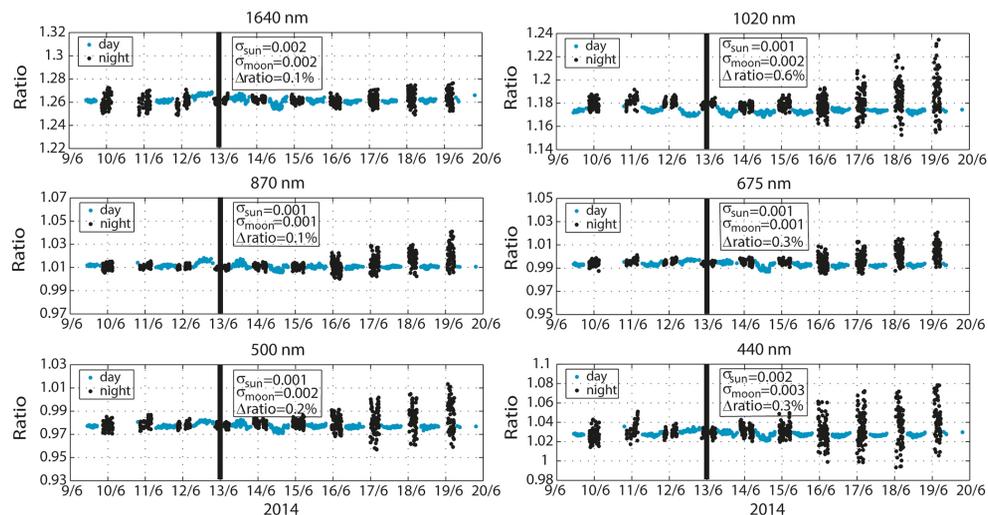


Figure 2. Ratio of simultaneous master/secondary signals at IZO performed in 11 consecutive days and 10 consecutive nights in June 2014. Vertical black line corresponds to the coincidence of full moon conditions. Standard deviations (σ) and ratio differences (Δ ratio) are depicted in each figure for sun midday and ± 1 night near full moon events ratios.

Title Page

Abstract Introduction

Conclusions References

Tables Figures

◀ ▶

◀ ▶

Back Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

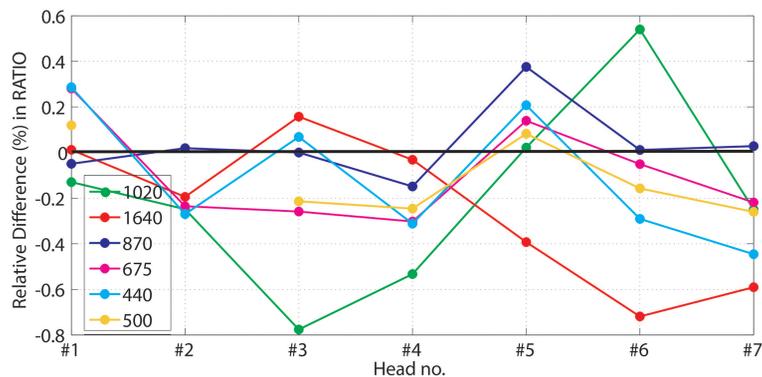


Figure 3. Relative differences between $\text{Ratio}_{\text{sun}}$ and $\text{Ratio}_{\text{moon}}$ for seven different heads at IZO.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

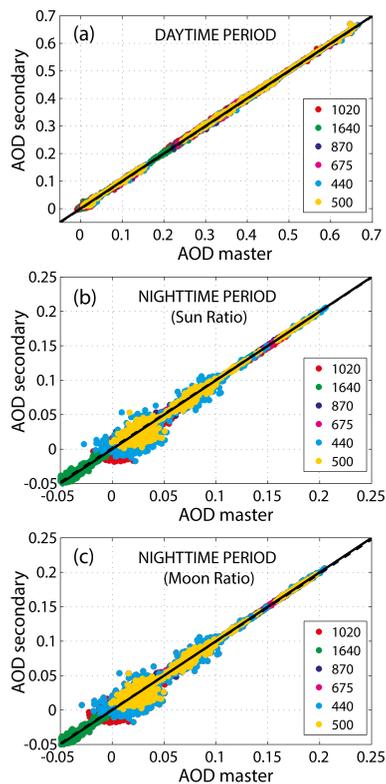


Figure 4. Scatterplot with CE318-T master versus secondary derived AODs for **(a)** a period of 22 consecutive days and **(b)** and **(c)** for a period of 10 consecutive nights in June 2014, with the secondary calibrated using the Sun Ratio and the Moon Ratio techniques, respectively.

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

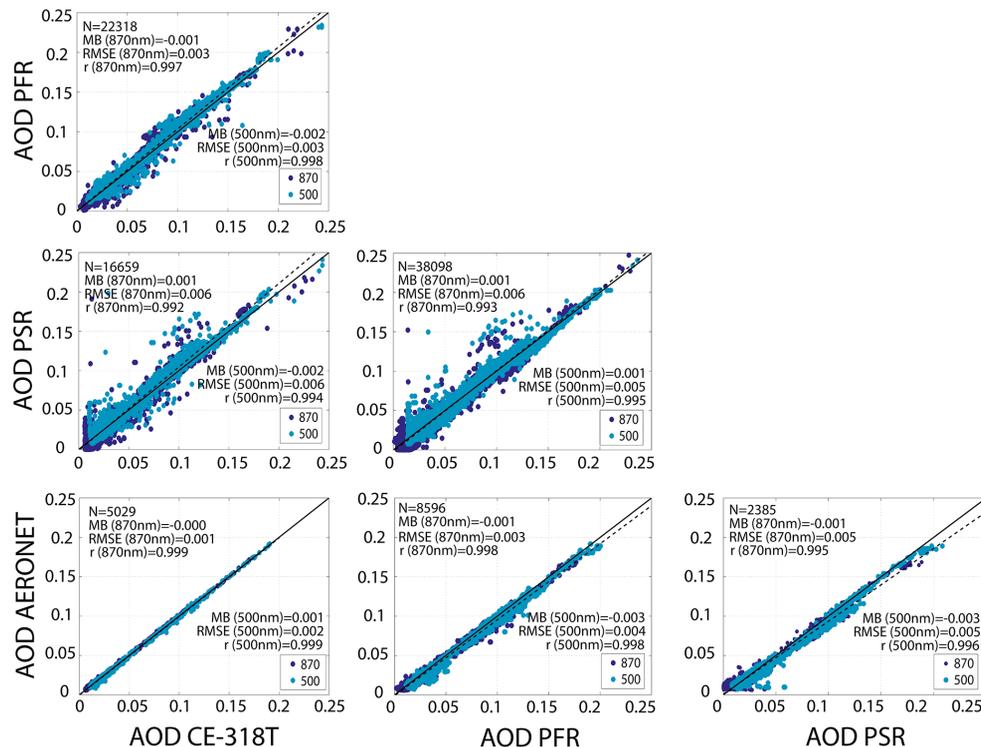


Figure 5. Scatterplots of AOD at 870 nm (blue) and 500 nm (cyan) using four different and independent measurements (CE318-T, CE318-AERONET, PFR and PSR) during March, April, May and June 2014 at IZO. In each figure, the dotted line represents the linear regression line, and the solid line is the diagonal.

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

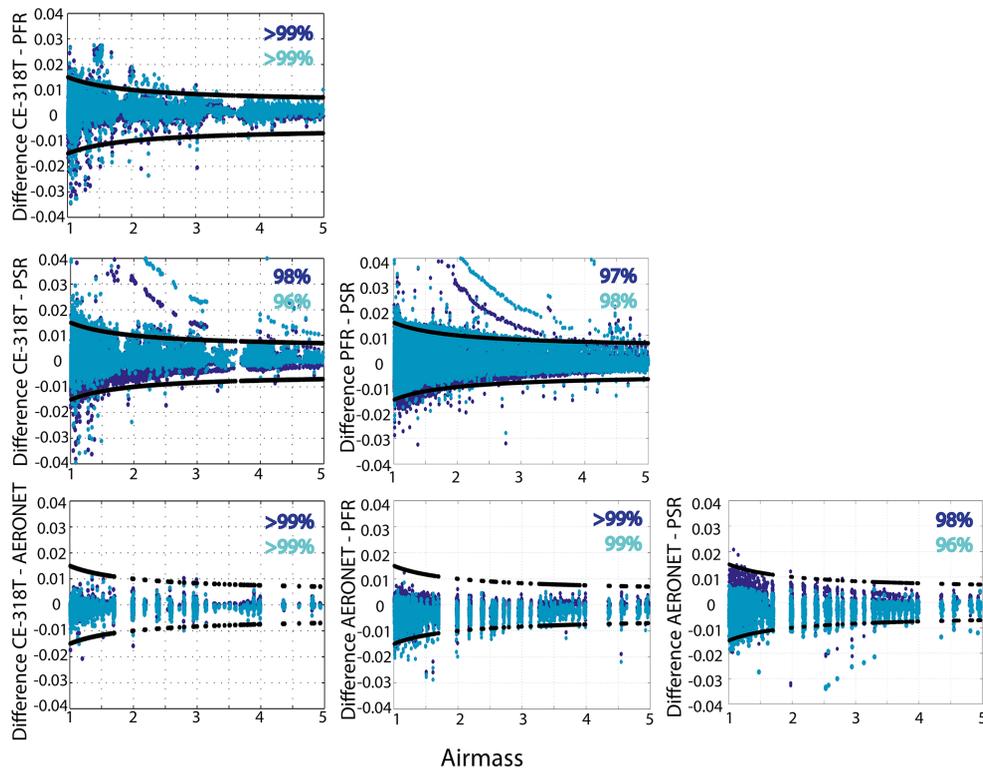


Figure 6. AOD differences versus airmass for channel centered at 870 nm (blue) and 500 nm (cyan). Solid line represents the U_{95} uncertainty limit. In each figure the percentage of points within the U_{95} limits is included.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



AMTD

8, 11077–11138, 2015

The new
sun-sky-lunar Cimel
CE318-T multiband
photometer

A. Barreto et al.

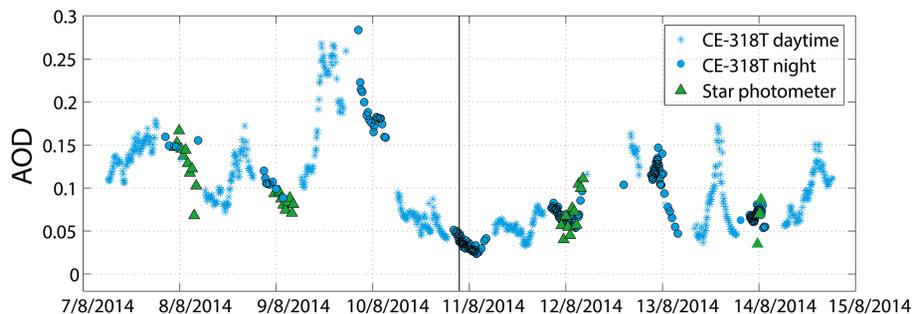


Figure 7. AOD at 500 nm channel from CE318-T at daytime and nighttime (in blue), and from the star photometer (in green) at Granada in eight consecutive days in August 2014. Vertical line represents the full moon phase.

[Title Page](#)[Abstract](#)[Introduction](#)[Conclusions](#)[References](#)[Tables](#)[Figures](#)[◀](#)[▶](#)[◀](#)[▶](#)[Back](#)[Close](#)[Full Screen / Esc](#)[Printer-friendly Version](#)[Interactive Discussion](#)

**The new
sun-sky-lunar Cimel
CE318-T multiband
photometer**

A. Barreto et al.

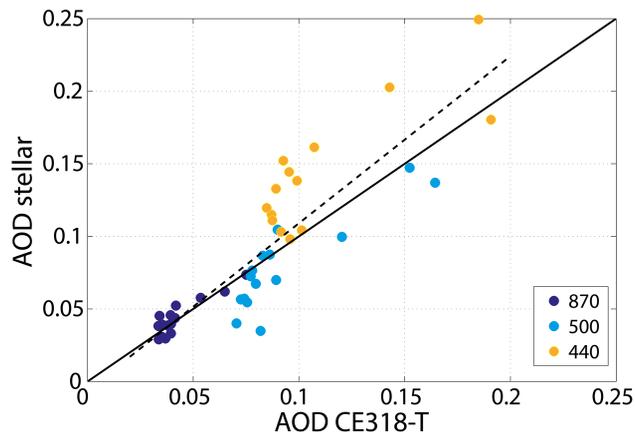


Figure 8. Scatterplot CE318-T AOD versus stellar AOD at Granada for four nights in August 2014. The dotted line represents the linear regression line, and the solid line is the 1 : 1 line.

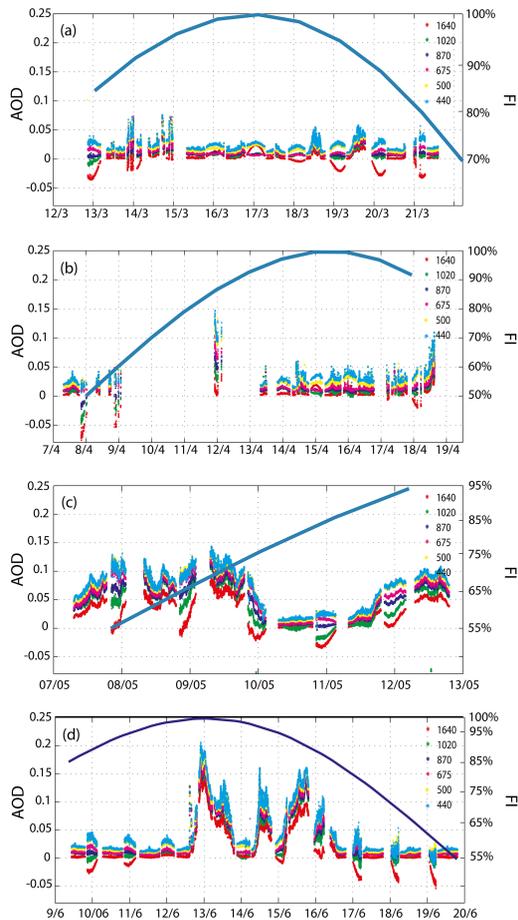


Figure 9. Diurnal CE318-AERONET/CE318-T AOD evolution during **(a)** March, **(b)** April, **(c)** May and **(d)** June 2014 at IZO. The blue line and right y-axis correspond to the evolution in this period of the moon's factor of illumination (FI).

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract Introduction

Conclusions References

Tables Figures

◀ ▶

◀ ▶

Back Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

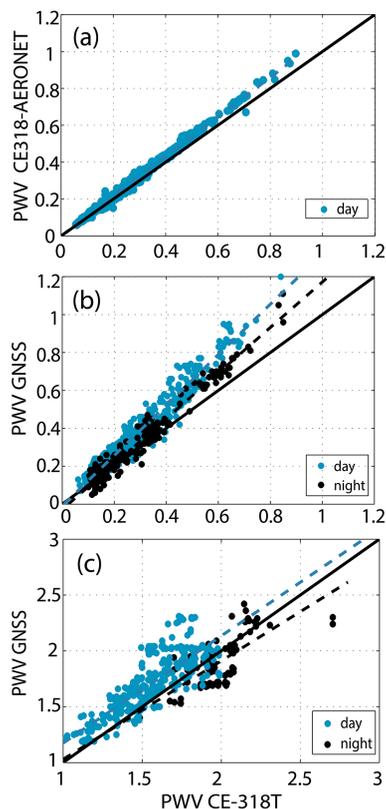


Figure 10. Scatterplot with daytime (in blue) master CE318-T PWV (in cm) vs. **(a)** CE318-AERONET, **(b)** daytime and nighttime master (black) CE318-T PWV's (in cm) vs. GNSS, and **(c)** daytime and nighttime PWV comparison performed at Granada station using the secondary CE318-T and GNSS ultra-rapid orbits. The dotted line represents in all figures the linear regression line and the solid line the 1 : 1 line.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

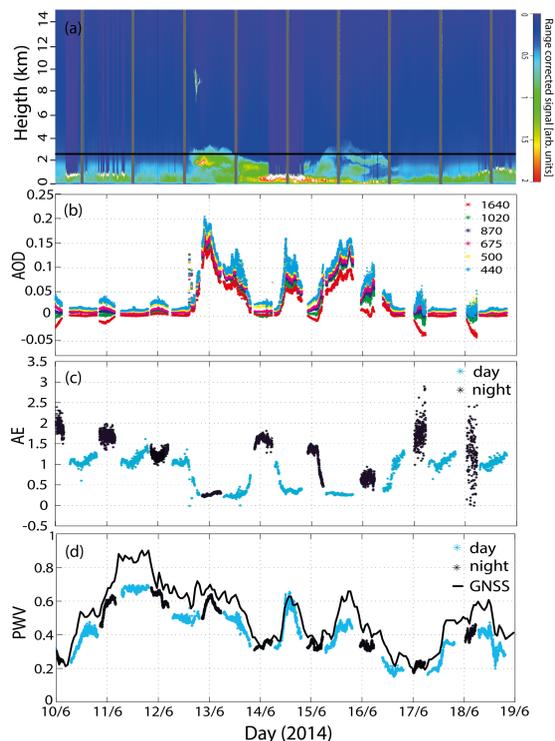


Figure 11. Case study at IZO in June, 2014, including information for (a) MPL corrected backscatter cross-section obtained from Santa Cruz de Tenerife station (60 m a.s.l.). Black horizontal line represents the altitude of IZO station. Grey vertical lines represent the absence of measurements. The CE318-T AOD, AE and PWV evolution from 10 to 19 June, 2014 are shown in (b), (c) and (d). PWV values from GNSS precise orbits are plotted with a black solid line.

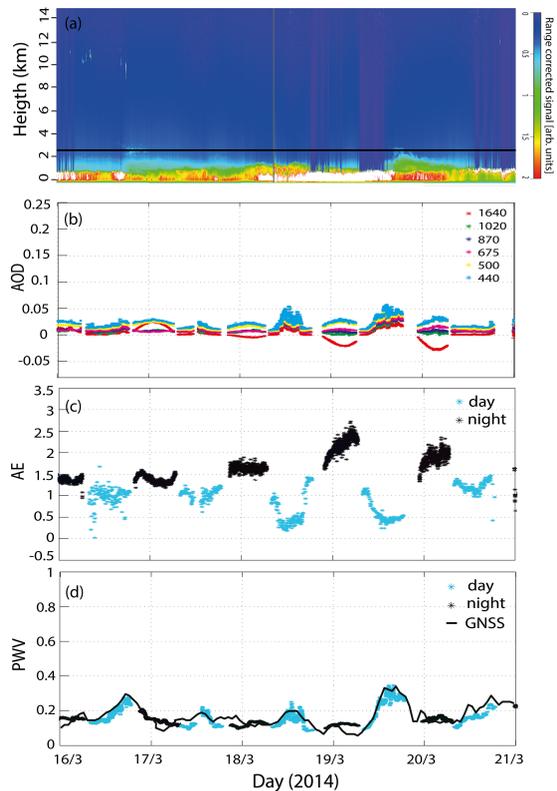


Figure 12. Case study at IZO in March 2014, including information for **(a)** MPL corrected backscatter cross-section obtained from Santa Cruz de Tenerife station (60 m a.s.l.). Black horizontal line represents the altitude of IZO station. Grey vertical lines represent the absence of measurements. The CE318-T AOD, AE and PWV evolution from 16 to 21 March, 2014 are shown in **(b)**, **(c)** and **(d)**. PWV values from GNSS precise orbits are plotted with a black solid line.

The new sun-sky-lunar Cimel CE318-T multiband photometer

A. Barreto et al.

Title Page

Abstract Introduction

Conclusions References

Tables Figures

◀ ▶

◀ ▶

Back Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion

