



**Correcting  
aethalometer BC data  
for measurement  
artifacts**

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L.-S. Yang

# Correcting aethalometer black carbon data for measurement artifacts by using inter-comparison methodology based on two different light attenuation increasing rates

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## Abstract

In black carbon (BC) measurements obtained using the filter-based optical technique, artifacts are a major problem. Recently, it has become possible to correct these artifacts to a certain extent by using numerical methods. Nevertheless, all correction schemes have their advantages and disadvantages under field conditions. In this study, a new correction model that can be used for determining artifact effects on BC measurements was proposed; the model is based on two different light attenuation (ATN) increasing rates. Two aethalometers were used to measure ATN values in parallel at aerosol sampling flow rates of 6 and 2 L min<sup>-1</sup>. In the absence of sampling artifacts, the ratio of ATN values measured by the two aethalometers should be equal to the ratio of the sampling flow rates (or aerosol deposition rates) of these two aethalometers. In practice, the ratio of ATN values measured by the two aethalometers was not the same as the ratio of the sampling flow rates of the aethalometers because the aerosol loading effects varied with the aerosol deposition rate. If the true ATN value can be found, then BC measurements can be corrected for artifacts by using the true ATN change rate. Therefore, determining the true ATN value was the primary objective of this study. The proposed correction algorithm can be used to obtain the true ATN value from ATN values acquired at different sampling flow rates, and the actual BC mass concentrations can be determined from the true ATN change rate. Before BC correction, the BC concentration measured at the sampling flow rate of 6 L min<sup>-1</sup> was smaller than that measured at 2 L min<sup>-1</sup> by approximately 13 and 9% in summer and winter seasons, respectively. After BC correction by using the true ATN value, the corrected BC for 6 L min<sup>-1</sup> can be exactly equal to the corrected BC for 2 L min<sup>-1</sup>. Field test results demonstrated that loading effects on BC measurements could be corrected accurately by using the proposed model. Additionally, the problem of enhanced light ATN caused by light scattering at the unloaded filter can be overcome without using any light scattering coefficient. Therefore, the correction algorithm can be applied to a newly designed instrument to determine actual real-time BC concentrations by using

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ent sampling flow conditions (Drinovec et al., 2014). This dual-spot method involves a real-time model for determining the temporal variation of a compensation parameter for the loading effect. Cheng and Lin (2013) noted that different sets of ATN measurement results could differ significantly because of different aerosol deposition rates resulting from differences in the sampling flow rates or aerosol deposition areas among the used instruments. Therefore, a correction model for determining the artifacts on BC measurements based on different ATN increasing rates was developed in the current study. Two aethalometers were used to measure the ATN values at different aerosol sampling flow rates in parallel. In the absence of sampling artifacts, the ratio of the ATN values measured by these two aethalometers should be equal to the ratio of the sampling flow rates (or the aerosol deposition rates) of these two aethalometers. In practice, the ratio of the ATN values measured by these two aethalometers was not identical to the ratio of the sampling flow rates of these two aethalometers because of different aerosol loading effects resulting from different aerosol deposition rates. Hence, a simple algorithm, similar to the correction methods developed by Virkkula et al. (2007) and Drinovec et al. (2014), was used to determine the true ATN values. Field test results demonstrated that loading effects on BC measurements can be corrected accurately by using the proposed model. Moreover, the problem of enhanced light ATN because of light scattering at the unloaded filter can be overcome without using any light scattering coefficient. Field test results can also further provide users with a simple correction scheme during post-processing for correcting existing aethalometer BC data.

## 2 Methods

### 2.1 Correction model

For measuring BC with the filter-based optical technique, the optical ATN is defined as

$$\text{ATN} = -100 \cdot \ln \left( \frac{I}{I_0} \right) \quad (1)$$

where  $I_0$  and  $I$  are the intensities of light transmitted through a reference blank spot and a spot of aerosol on the filter, respectively. The factor 100 is introduced for convenience. The ATN change in a time interval ( $d\text{ATN}/dt$ ) is used to estimate the BC concentration as follows:

$$5 \quad \text{BC} = \frac{d\text{ATN}}{dt} \cdot \frac{A}{Q} \cdot \frac{1}{\sigma_{\text{ATN}}} \quad (2)$$

where  $A$  is the area of the sample spot,  $Q$  is the sampling flow rate, and  $\sigma_{\text{ATN}}$  is the black carbon optical mass cross section.

Drinovec et al. (2014) showed that the loading effect on BC can be corrected by using the following equation, which is similar to that proposed by Virkkula et al. (2007):

$$10 \quad \text{BC}_c = \frac{\text{BC}}{(1 - k \cdot \text{ATN})} \quad (3)$$

where  $\text{BC}_c$  and  $\text{BC}$  represent the corrected and measured black carbon concentration, respectively, and  $k$  is a correction factor. On the basis of the same principle as Eq. (2), the average BC ( $\overline{\text{BC}}$ ) from initial time  $t_0$  ( $t_0 = 0$ ) to time  $t$  can be expressed as

$$\overline{\text{BC}} = \frac{\Delta\text{ATN}}{\Delta t} \cdot \frac{A}{Q} \cdot \frac{1}{\sigma_{\text{ATN}}} = \frac{\text{ATN}}{t - t_0} \cdot \frac{A}{Q} \cdot \frac{1}{\sigma_{\text{ATN}}} \quad (4)$$

15 Then, Eq. (3) can be written as

$$\text{ATN}_c = \frac{\text{ATN}}{(1 - k \cdot \text{ATN})} \quad (5)$$

where  $\text{ATN}_c$  and  $\text{ATN}$  represent corrected and measured light ATN values, respectively.

In practice, if the true ATN value can be found, then the artifact effect on the BC measurement can be corrected from the true ATN change rate ( $d\text{ATN}/dt$ ). Therefore, determining the true ATN value was the main objective of this study. According to the

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from further treatment. Local meteorological data such as temperature and relative humidity were recorded using a Vantage Pro 2<sup>TM</sup> weather station (Davis Instruments). Table 1 shows the ambient temperature and relative humidity during the sampling periods. The average temperature during the summer season was significantly higher than that during the winter season by approximately 15 °C ( $p < 0.001$ ). The average relative humidity did not differ significantly between the summer and the winter seasons ( $p = 0.086$ ).

Before beginning field sampling, the performance of the two aethalometers was compared at the sampling site for two sampling flow rates, 6 and 2 L min<sup>-1</sup>, for 2–3 days. The hourly measured results obtained using the two aethalometers are shown in Fig. 1. The hourly average BC mass concentrations in units of nanogram per cubic meter were calculated using 5 min raw data. Statistical results indicated that the intercepts were -30.751 (95 % confidence interval (CI): -56.091 to -5.411) and -18.119 (95 % CI: -43.841–7.603) for the sampling flow rates of 6 and 2 L min<sup>-1</sup>, respectively, and the intercepts were not considerably different from zero ( $p = 0.019$  for 6 L min<sup>-1</sup> and  $p = 0.163$  for 2 L min<sup>-1</sup>). The slopes determined for these two flow rates were 0.991 (95 % CI: 0.985–0.997) and 0.988 (95 % CI: 0.980–0.997), respectively, and the slopes were significantly different from 1.0 ( $p < 0.001$  for both). These comparison results indicated that the performance of both aethalometers used in this study could be considered to be similar to each other.

### 3 Results and discussion

#### 3.1 ATN values and black carbon mass concentrations before and after correction

Figure 2 shows the relationships between ATN values for sampling flow rates of 6 and 2 L min<sup>-1</sup> before and after correction in the summer and winter seasons. Before ATN correction, the ATN<sub>F6</sub> value was smaller than the value of 3 × ATN<sub>F2</sub>, indicating

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the presence of the artifact effect on the ATN measurement result. When the  $ATN_{F6}$  value increased, it deviated considerably from the value of  $3 \times ATN_{F2}$ , especially for the 370 nm wavelength. The measurement results demonstrated that the loading effect on the ATN value at short wavelengths was stronger than that at long wavelengths.

After ATN correction using Eqs. (6)–(9), the ratio of the  $ATN_{F6}$  value to the  $ATN_{F2}$  value could fall to 3 : 1. That is, the true ATN values could be determined using the algorithms proposed in this study. Subsequently, the actual BC mass concentration could be estimated from the true ATN change rate. Before BC correction, the measured  $BC_{F6}$  was significantly smaller than the measured  $BC_{F2}$  by approximately 13 and 9 % in the summer and winter seasons ( $p < 0.001$  for both), respectively. After BC correction by using the true ATN value, the corrected  $BC_{F6}$  could be exactly equal to the corrected  $BC_{F2}$ . Figure 3 presents a comparison of BC corrected using the proposed model and that corrected using the correction model of Drinovec et al. (2014). The correction model of Drinovec et al. (2014) is presented in Eq. (3), and the correction factor in this model can be easily estimated from the following equation on the basis of the measurement results of BC and ATN at sampling flow rates of 6 and 2 L min<sup>-1</sup>:

$$k = \frac{BC_{F2} - BC_{F6}}{BC_{F2} \cdot ATN_{F6} - BC_{F6} \cdot ATN_{F2}} \quad (10)$$

The corrected BC estimated using the model proposed in this study was comparable with that obtained using the correction model of Drinovec et al. (2014) ( $p = 0.307$  for summer;  $p = 0.915$  for winter). The  $k$  value estimated using the model of Drinovec et al. (2014) exhibited significant variations between negative and positive values for the entire data set. By contrast, the  $k$  value determined using the proposed model approached a constant value steadily when the ATN value increased. The steady variation of the  $k$  value in the proposed model was due to  $k$  being determined from a cumulative ATN value, rather than an instant differential ATN value.

### 3.2 Influence of light scattering behavior on unloaded filter

The relationship between measured  $ATN_{F6}$  and  $ATN_{F2}$  is shown in Fig. 2, and it can be expressed as a power law relationship through measurement data fitting. On the basis of analytical results, the relationship between  $k$  and  $ATN/Q$  could be determined using Eq. (9) and the relationship between measured  $ATN_{F6}$  and  $ATN_{F2}$ , as shown in Fig. 4. Analytical results showed that the relationship between  $k$  and  $ATN/Q$  for sampling flow rates of 6 and  $2\text{ L min}^{-1}$  was similar, especially for long wavelengths. This result indicated that the assumption of the  $k$  value being fixed for an  $ATN/Q$  value in the proposed model was reasonable. Analytical results indicated that the  $k$  value was negative at extremely small  $ATN/Q$  values. The  $k$  value increased rapidly as  $ATN/Q$  increased, and then approached a constant value. Weingartner et al. (2003) noted that multiple scattering in the nearly unloaded fiber filter could enhance light absorption. Therefore, a negative  $k$  value could be observed at small  $ATN/Q$  values, which was reasonable in terms of the light scattering behavior of the nearly unloaded filter at a new sampling spot, especially at short wavelengths in the winter season. In this study, it was found that with increasing aerosol load on the filter, the influence of the light scattering behavior of the filter matrix could be eliminated. When a sufficient amount of aerosol was sampled on the filter,  $k$  initially increased as a positive value and then decreased gradually and steadily to a constant value. These observation results indicated that the proposed model could overcome the problem of enhanced light  $ATN$  resulting from light scattering at a new sampling spot, without using any light scattering coefficient.

### 3.3 Absorption Ångström exponent and emission source of black carbon

The absorption Ångström exponent  $\alpha$  can be used as an index to determine the type of BC emission sources (Sandradewi et al., 2008), and it is computed from the aerosol

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light absorption between 470 and 950 nm wavelengths as follows:

$$\alpha = \frac{\ln(b_{\text{abs},\lambda=470}/b_{\text{abs},\lambda=950})}{\ln(950/470)} \quad (11)$$

where  $b_{\text{abs},\lambda=470}$  and  $b_{\text{abs},\lambda=950}$  are the absorption coefficients of aerosol at 470 and 950 nm wavelengths, respectively. The absorption coefficient of aerosol can be determined from the change rate of ATN:

$$b_{\text{abs}} = \frac{d\text{ATN}}{dt} \cdot \frac{A}{Q} \cdot \frac{1}{C} \quad (12)$$

where  $C$  is a light enhancement parameter. It is associated with multiple scattering of the light beam at the filter fibers in the unloaded filter, and it is strongly dependent on the filter material (Weingartner et al., 2003). In this study,  $C$  was set as 2.14 for the quartz filter (Weingartner et al., 2003; Drinovec et al., 2014).

Kirchstetter and Novakov (2004) noted that the absorption Ångström exponent value ranged between 0.8 and 1.1 for diesel soot. Day et al. (2006) showed that the absorption Ångström exponent values were between 0.9 and 2.2 for fresh wood smoke aerosol, which strongly depended on the type of wood and burning conditions. Sandradewi et al. (2008) also demonstrated that the absorption Ångström exponent values were 1.1 and 1.8–1.9 for traffic and wood burning, respectively. A high absorption Ångström exponent value could be observed for wood combustion aerosol that is due to the compounds of the aerosol with strong absorption in the UV. However, the filter loading effect also strongly influences the calculation of the absorption Ångström exponent value. Table 2 shows the absorption Ångström exponent values calculated from measured  $\text{ATN}_{F_6}$  and  $\text{ATN}_{F_2}$  and from corrected ATN in the summer and winter seasons. Analytical results showed that the absorption Ångström exponent value could be improved from  $1.01 \pm 0.22$  (estimated from measured  $\text{ATN}_{F_6}$ ) and  $1.11 \pm 0.33$  (estimated from measured  $\text{ATN}_{F_2}$ ) to  $1.17 \pm 0.44$  (estimated from corrected ATN) in the summer

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extent of the aerosol loading effect on BC measurement results. Moreover, the aerosol loading effect on BC measurement results in the summer season was greater than that in the winter season by approximately 1–6%, and it depended on the sampling flow rate. This difference between seasons could be because of differences in the composition, source, and age of aerosols, in addition to the different weather conditions.

Figure 7 presents the results of a comparison between 5 min BC concentrations measured at sampling flow rates of 6 and 2 L min<sup>-1</sup> before and after correction. The BC was corrected using the proposed post-processing model. Results showed that the corrected BC<sub>F6</sub> mass concentrations were not significantly different from the corrected BC<sub>F2</sub> mass concentrations ( $p = 0.734$  for summer;  $p = 0.594$  for winter), indicating that the post-processing model could be effectively used to correct BC data for the loading effect.

### 3.5 Comparison with a previous correction model

Figure 8 presents the results of a comparison of BC corrected using the proposed post-processing model and the correction model of Weingartner et al. (2003). The correction model developed by Weingartner et al. (2003) is widely used to correct BC data on the basis of the measured ATN value, and it can be expressed as

$$BC_c = \frac{BC}{R(ATN)} \quad (13)$$

$$R(ATN) = \left( \frac{1}{f} - 1 \right) \frac{\ln(ATN) - \ln(10)}{\ln(50) - \ln(10)} + 1 \quad (14)$$

where  $f$  is a fit parameter dependent on the aerosol type. BC corrected using the post-processing model was comparable with that corrected using the correction model of Weingartner et al. (2003) for  $f = 1.21$  and 1.14 in the summer and winter seasons, respectively, at the sampling flow rate of 6 L min<sup>-1</sup>. For the sampling flow rate of 2 L min<sup>-1</sup>, BC corrected using the post-processing model was comparable with that

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corrected using the correction model of Weingartner et al. (2003) for  $f = 1.25$  and  $1.15$  in the summer and winter seasons, respectively. However, BC corrected using the post-processing model was slightly higher than that corrected using the correction model of Weingartner et al. (2003) ( $p \leq 0.019$ ), except for the sampling flow rate of  $6 \text{ L min}^{-1}$  in the winter season ( $p = 0.123$ ). BC corrected using the correction model of Weingartner et al. (2003) was significantly lower than that corrected using the post-processing model when ATN was small, and this is possibly because the function  $R(\text{ATN})$  in the correction model of Weingartner et al. (2003) was larger than  $1.0$  for  $\text{ATN} < 10$ . In other words, the corrected BC was smaller than that corrected using the post-processing model for  $R(\text{ATN}) > 1.0$ . Otherwise, the BC corrected using the correction model of Weingartner et al. (2003) was higher than that corrected using the post-processing model for  $\text{ATN} > 20$ , especially for  $\text{ATN} > 50$ . Moreover, the parameter  $f$  in the correction model of Weingartner et al. (2003) is significantly dependent on the aerosol type, and it was difficult to determine from field sampling data.

## 4 Conclusions

This study developed a new method based on two different light ATN increasing rates to improve the measurement of aerosol black carbon. The proposed correction model can overcome the light scattering effect and aerosol loading effect on BC measurement results simultaneously, and it can be used in a newly designed instrument to determine the actual BC concentration in real time by using two sampling spots under different aerosol deposition rates. Moreover, this study provided a simple empirical correction scheme for post-processing for correcting the existed aethalometer BC data. Although this simple correction scheme is dependent on the aerosol type, it can be used to correct BC data when the primary source of BC and the weather conditions are similar to those in this study. Moreover, two existed aethalometers under appropriate flow control can be used to create correction schemes for different environments.

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**Table 1.** Ambient temperature and relative humidity during the sampling periods.

| Season | Temperature, °C  |         | Relative Humidity, % |         |
|--------|------------------|---------|----------------------|---------|
|        | Average $\pm$ SD | Min–Max | Average $\pm$ SD     | Min–Max |
| Summer | 32 $\pm$ 3       | 25–39   | 68 $\pm$ 13          | 37–93   |
| Winter | 17 $\pm$ 3       | 10–28   | 69 $\pm$ 14          | 34–91   |

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**Table 2.** Absorption Ångström exponent values in the summer and winter seasons.

| Season | Ångström exponent estimated from |                     |                 |
|--------|----------------------------------|---------------------|-----------------|
|        | measured $ATN_{F6}$              | measured $ATN_{F2}$ | corrected ATN   |
| Summer | $1.01 \pm 0.22$                  | $1.11 \pm 0.33$     | $1.17 \pm 0.44$ |
| Winter | $1.01 \pm 0.18$                  | $1.10 \pm 0.20$     | $1.15 \pm 0.24$ |

Average  $\pm$  SD

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**Table 3.** Parameters of empirical equations used for predicting the  $k$  values.

| Season | Wavelength $\lambda$ | $k = a \times \left(\frac{ATN}{Q}\right)^b$ |         |
|--------|----------------------|---|---------|
|        |                      | $a$   | $b$     |
| Summer | 370 nm               | 0.0263                                      | -0.8383 |
|        | 470 nm               | 0.0168                                      | -0.7602 |
|        | 520 nm               | 0.0167                                      | -0.8127 |
|        | 590 nm               | 0.0149                                      | -0.7843 |
|        | 660 nm               | 0.0132                                      | -0.7491 |
|        | 880 nm               | 0.0149                                      | -0.8099 |
|        | 950 nm               | 0.0148                                      | -0.8569 |
| Winter | 370 nm               | 0.0088                                      | -0.5664 |
|        | 470 nm               | 0.0100                                      | -0.6623 |
|        | 520 nm               | 0.0092                                      | -0.6768 |
|        | 590 nm               | 0.0089                                      | -0.6835 |
|        | 660 nm               | 0.0087                                      | -0.6968 |
|        | 880 nm               | 0.0087                                      | -0.7532 |
|        | 950 nm               | 0.0101                                      | -0.8370 |

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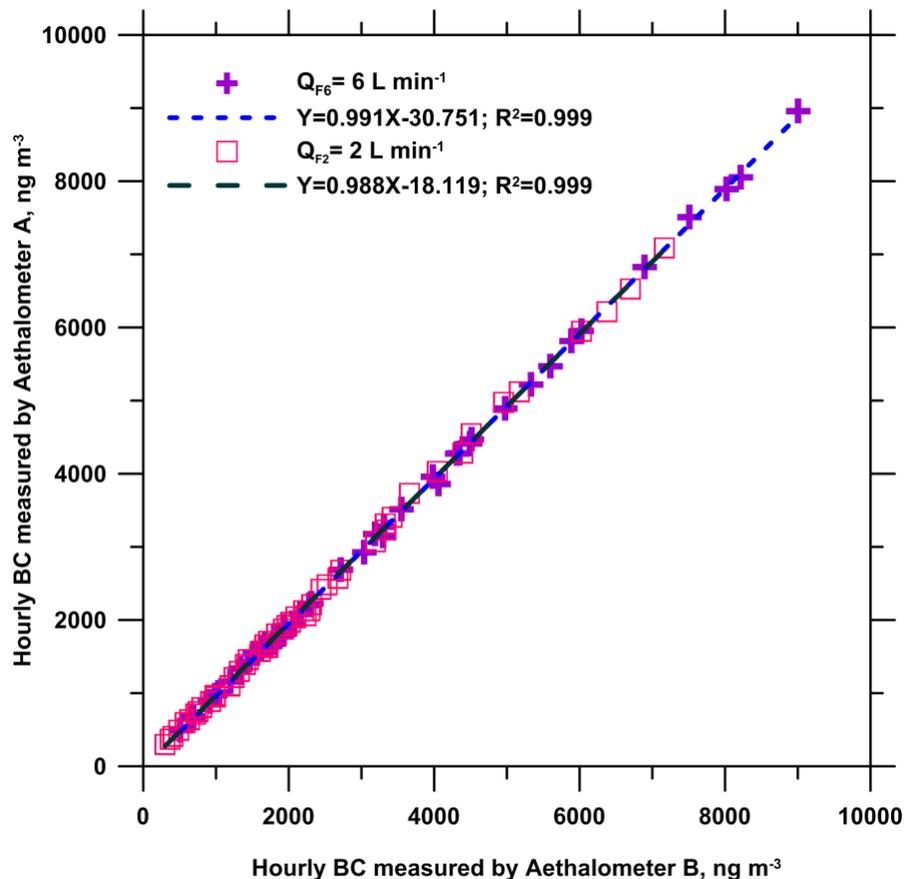
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**Figure 1.** Comparison of hourly BC mass concentration measurements obtained with the two aethalometers used in this study.

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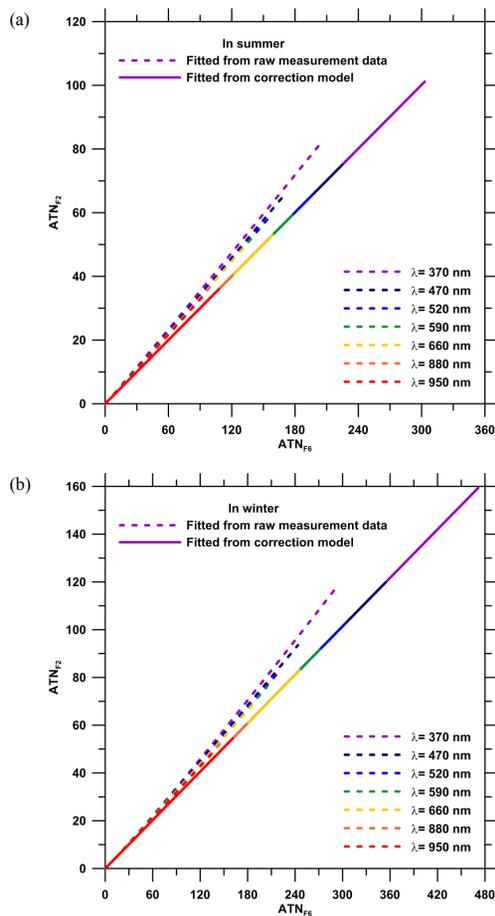
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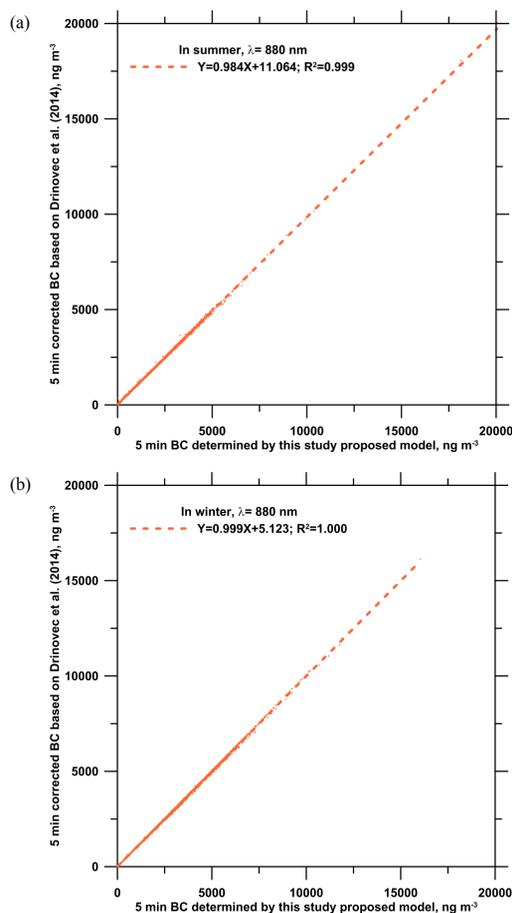


**Figure 2.** Relationship between ATN values for sampling flow rates of 6 and 2 L min<sup>-1</sup> before and after correction for the **(a)** summer season and **(b)** winter season.

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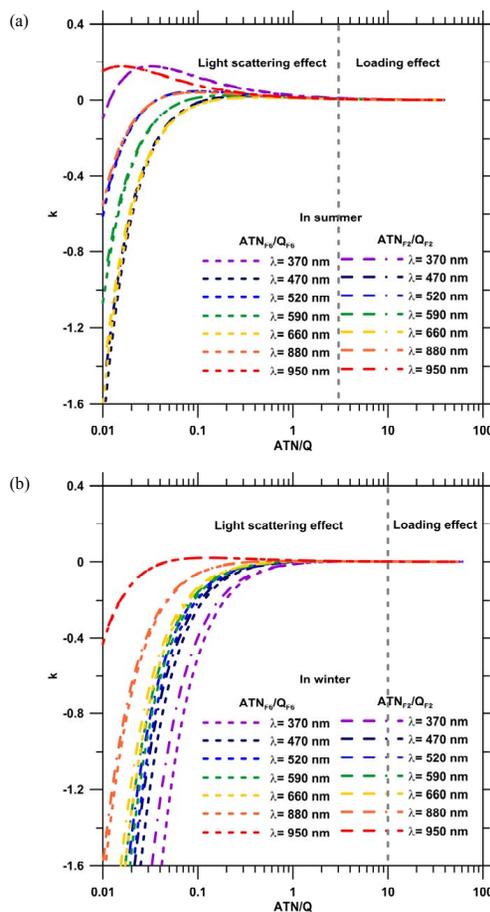
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**Figure 3.** Comparison of BC corrected using the proposed model with that corrected using the correction model of Drinovec et al. (2014) for the **(a)** summer season and **(b)** winter season.

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**Figure 4.** Relationships between  $k$  and  $ATN/Q$  for the **(a)** summer season and **(b)** winter season.

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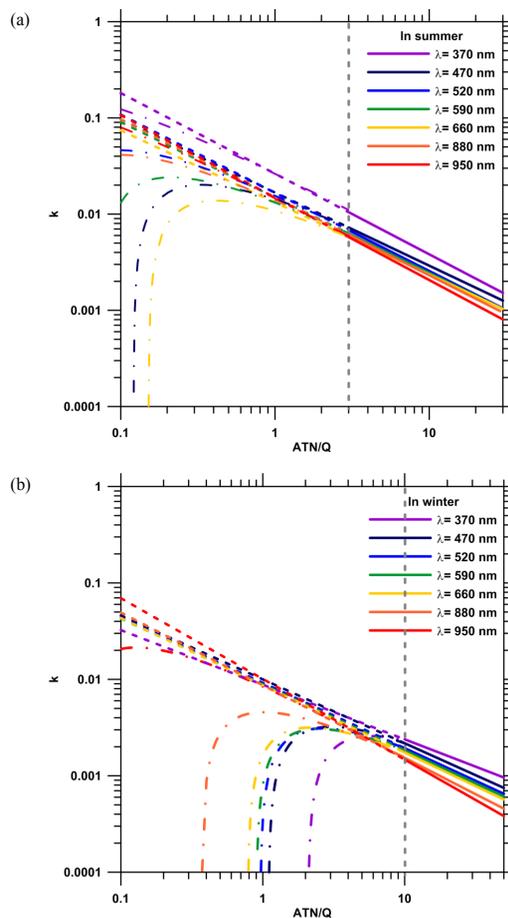
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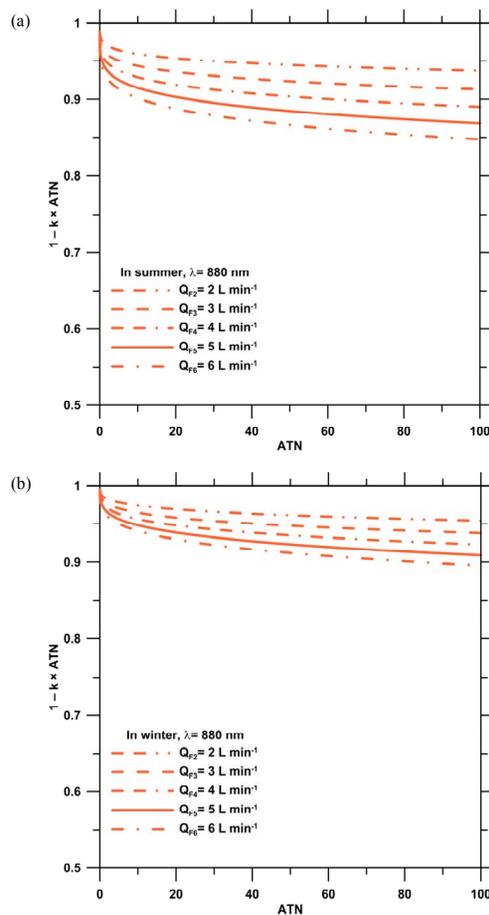


**Figure 5.** Power law relationship between  $k$  and  $ATN/Q$  (a) when  $ATN/Q > 3$  in the summer season and (b) when  $ATN/Q > 10$  in the winter season.

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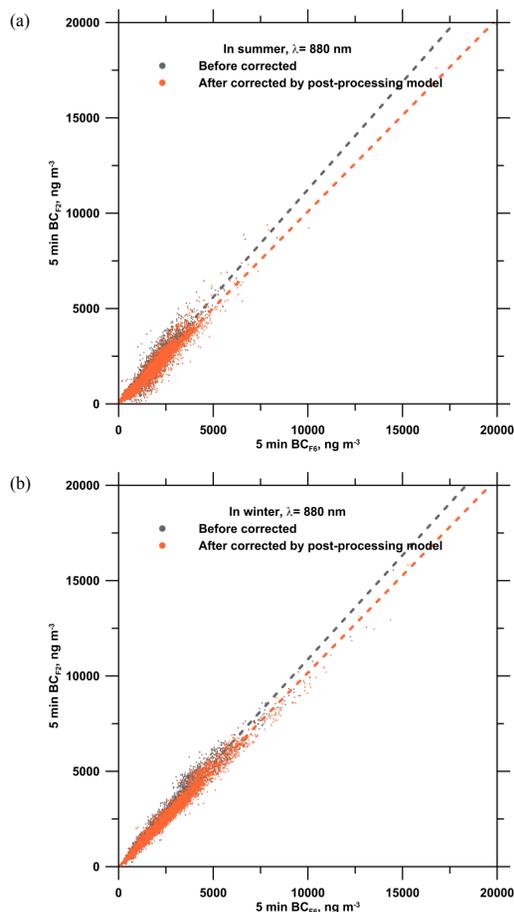


**Figure 6.** Relationship between  $(1 - k \times \text{ATN})$  and ATN at different sampling flow rates in the (a) summer season and (b) winter season.

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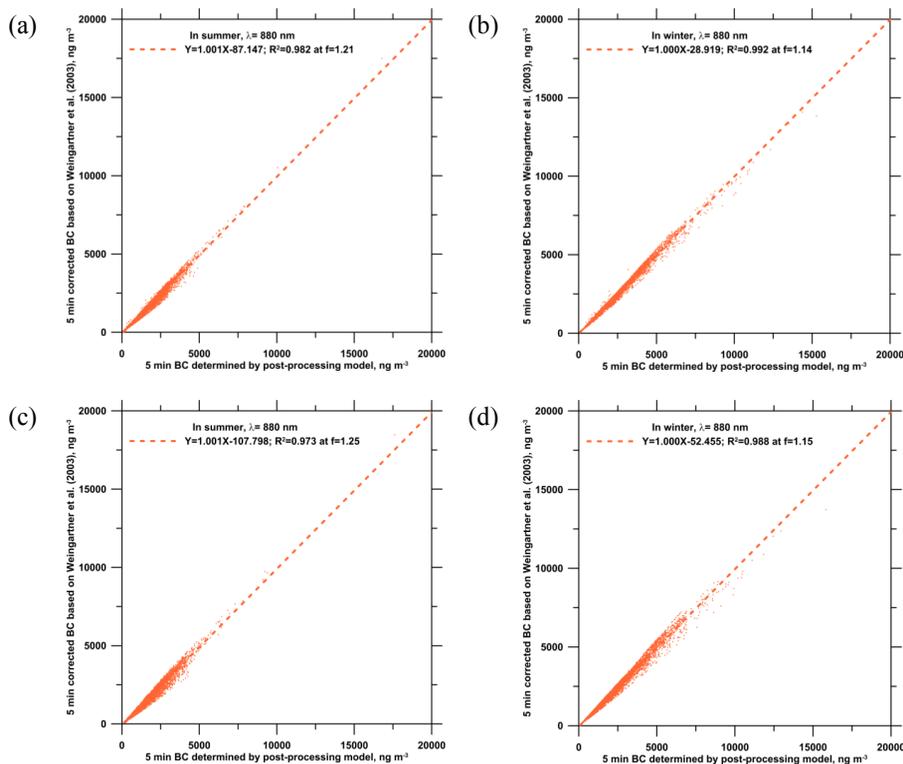
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**Figure 7.** Comparison of the 5 min BC mass concentrations measured at sampling flow rates of 6 and 2 L min<sup>-1</sup> before and after correction for the **(a)** summer season and **(b)** winter season.

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**Figure 8.** Comparison of the corrected BC obtained using the proposed postprocessing model with that obtained using the correction model of Weingartner et al. (2003) for sampling flow rates of (a)  $6 \text{ L min}^{-1}$  in the summer season, (b)  $6 \text{ L min}^{-1}$  in the winter season, (c)  $2 \text{ L min}^{-1}$  in the summer season, and (d)  $2 \text{ L min}^{-1}$  in the winter season.

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