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High-resolution measurements from the airborne Atmospheric Nitrogen Dioxide Imager (ANDI)

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Abstract

Nitrogen Dioxide is both a primary pollutant with direct health effects and a key precursor of the secondary pollutant ozone. This paper reports on the development, characterisation and test flight of the Atmospheric Nitrogen Dioxide Imager (ANDI) remote sensing system. The ANDI system includes an imaging (UV)-vis grating spectrometer able to capture scattered sunlight spectra for the determination of tropospheric nitrogen dioxide (NO₂) concentrations by way of DOAS slant column density and vertical column density measurements.

Results are shown for an ANDI test flight over Leicester City in the UK. Retrieved NO₂ columns at a surface resolution of 80 m × 20 m revealed hot spots in a series of locations around Leicester City, including road junctions, the train station, major car parks, areas of heavy industry, a nearby airport (East Midlands) and a power station (Ratcliffe-on-Soar). In the city centre the dominant source of NO₂ emissions was identified as road traffic, contributing to a background concentration as well as producing localised hot spots. Quantitative analysis revealed a significant urban increment over the city centre which increased throughout the flight.

1 Introduction

Statistical and epidemiological studies have linked atmospheric pollution in urban environments to health problems in humans (Latza et al., 2008). Recent studies estimate that the economic impact of poor air quality in the UK is as high as EUR 28 billion yr⁻¹ (HoCEAC, 2011). In Germany, this figure is even higher at EUR 33 billion yr⁻¹ due to industrial emissions alone (EEA, 2011). Nitrogen dioxide (NO₂) is an atmospheric pollutant abundant in urban areas owing to emissions from traffic exhausts, central heating systems and industrial activities. Correlations have been found between the atmospheric concentration of NO₂ and respiratory symptoms, cardiovascular symptoms and hospital admissions (COMEAP, 2011). NO₂ is also a known tracer/marker

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for other combustion products such as sub-micron particulate matter (Wehner and Wiedensohler, 2003) and is a precursor for ozone formation (Monks et al., 2009).

Road transport is the largest contributor to urban NO₂ concentrations, and reductions of NO₂ (and NO) over the last two decades have not been as large as anticipated with NO₂ levels being measured above legal limits at over 40 % of European roadside air monitoring stations in 2010 (Carslaw et al., 2011). In the city of Leicester the focus region, approximately 90 % of the atmospheric NO₂ is emitted by traffic, of which approximately 60 % is emitted by heavy goods vehicles and public transport, and like many cities in the UK Leicester is not meeting its European Commission regulatory limits on NO₂ concentrations (Davies, 2011).

Understanding the concentration of NO₂ in the urban atmosphere and its spatial distribution is high on many national agendas with the aim of minimising human exposure. Presently atmospheric NO₂ concentrations at street level are determined from sparse in-situ monitors which are often fed into dispersion models to provide estimates for its spatial distribution. However, relying on dispersion modelling introduces significant uncertainty to the NO₂ concentration estimates between measurement sites owing to the complex topography of the urban landscape and the atmospheric chemistry which occurs outside of the sensing volumes of the in-situ monitors (CERC, 2003; Vardoulakis et al., 2007).

To gain perspective on the distribution of NO₂ around urban environments a remote sensing instrument known as the Atmospheric Nitrogen Dioxide Imager (ANDI) was developed at the University of Leicester. The main component of the ANDI instrument is a compact imaging spectrometer known as CompAQS (Whyte et al., 2009), which was installed in a light aircraft alongside a series of ancillary systems and flown in a push-broom nadir configuration on the 28 February 2013. When flown at 900 m altitude the ANDI system produces maps of NO₂ differential slant column densities (dSCD) beneath the aircraft across swaths approximately 600 m wide with an across-swath resolution of approximately 5 m (see Sect. 2). The dSCDs are retrieved using the well established differential optical absorption spectroscopy (DOAS) technique (Platt and

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Stutz, 2008), which following post processing involving a radiative transfer model to generate air mass factors (AMF) converts them into vertical column densities (VCD) in units of molecules cm^{-2} . VCDs provide estimates for the NO_2 concentrations in vertical atmospheric columns having compensated for both viewing and solar geometries.

Aircraft are commonly used for testing and demonstrating new instruments and retrieval techniques, particularly for flight demonstrators of satellite instruments. For atmospheric measurements of NO_2 in particular, aircraft open opportunities for validation of atmospheric modelling activities and have previously been used for validating satellite retrievals during inter-comparison campaigns (e.g. Bucselä et al., 2008).

Imaging DOAS instruments which measure spectra across the nadir field of view have been previously employed in several flight campaigns (e.g. Heue et al., 2008; Popp et al., 2012; Schönhardt et al., 2014; General et al., 2014). As in the case of many satellite imaging instruments these operate a push-broom viewing geometry, in which spectra from multiple nadir viewing angles across the flight track are imaged onto the same CCD, which allows for high spatial resolution two-dimensional images of atmospheric pollution over the flight duration to be produced. These instruments are capable of imaging anthropogenic NO_2 distributions over heavily polluted regions, such as industrial point-source emissions over the Highveld plateau in South Africa (Heue et al., 2008), and pollution originating from traffic in Zurich (Popp et al., 2012).

This paper describes the ANDI system and its test flight which focused specifically on the mapping of an urban agglomerate at very high resolution. It is shown that with an appropriate flight plan, data collected by ANDI can provide insight into both spatial and temporal urban NO_2 dynamics in a single flight, highlighting variability which is hidden to lower resolution satellite measurements and in-situ monitors.

2 The ANDI system

The ANDI system comprises of multiple subcomponents mounted on a rigid plate with two viewing apertures. The components include a CompAQS spectrometer (Whyte

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et al., 2009), a Global Positioning System (GPS), an Inertial Monitoring Unit (IMU), a Digital Single Lens Reflex (DSLR) camera and a power system to condition and convert the 28 V provided by the aircraft's generators into the 12 and 19 V used by the ANDI instruments. The ANDI system design is shown in Fig. 1.

2.1 The CompAQS spectrometer

The CompAQS spectrometer was originally built as a technology readiness improvement exercise towards the development of a compact grating spectrometer suitable for a small satellite mission (Whyte et al., 2009; Leigh et al., 2015). For application in the ANDI system the optical bench of CompAQS was modified and strengthened to allow for a vertical (nadir) configuration. In addition the spectrometer's shutter mechanism was replaced with a CCD frame transfer system.

To minimise the transmission of vibration from the aircraft to the spectrometer and to protect the instrument from damage during landing, the spectrometer was mounted inside a secure metal frame using compressed foam as the fixing medium to prevent any hard contact between the spectrometer and the aircraft.

To mitigate the effect of electrical noise inherent in the production of power from the aircraft's generators a power conditioning unit was installed in the main circuit between the ANDI's power distribution hub and the aircraft's 28 V power supply (see Fig. 1).

The CompAQS spectrometer's across track field of view (FOV) is curved owing to the use of a two mirror Schwarzschild entrance optics configuration (Leigh et al., 2015). To provide an appropriate viewing geometry for data analysis purposes the spectrometer was mounted such that the curvature of its FOV pointed towards the aircraft's direction of travel. The instrument's FOV is approximately 34° spread over 128 pixels (600 m on the ground at 900 m altitude).

The along track spatial resolution of the CompAQS spectrometer is restricted by the maximum capture rate of the CompAQS CCD and its associated electronics. The capture rate during the test flight was approximately 1 Hz. The aircraft travelled with

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an average velocity of 155 knots (80 ms^{-1}), resulting in a forward spatial resolution of approximately 80 m.

The CompAQS spectrometer measures spectra in the visible region of the electromagnetic spectrum which are converted into dSCD and VCD measurements of atmospheric NO_2 using the well established DOAS technique (see Sects. 3.4 and 3.6). The specifications for the CompAQS spectrometer in its airborne configuration are given in Table 1 and Sect. 3.4.

2.2 Attitude sensors

To relate the NO_2 measurements provided by CompAQS to a location on the Earth's surface a GPS module was built based on a Parallax GPS chip, and software was written to extract the GPS sentences and convert them into longitude, latitude and altitude data with 1 s temporal resolution. In addition, an IMU was installed to provide banking and pitch data to compensate for changes in viewing geometry during the data analysis process. The IMU data were not used in the data analysis for the results presented in this paper owing to data corruption, therefore an alternative data source was derived to account for banking as described in Sect. 3.3.

3 Test flight and data processing chain

The ANDI system was installed and flown in a Cessna Reims F406 aircraft on the 28 February 2013 from 12:30 to 14:30 p.m. (GMT) The weather conditions were suitable for flying the instrument but were non-ideal. The visibility in the boundary layer was slightly limited due to haze, and because of the time of year the solar elevation angle was between 26 and 30° , resulting in a shallow light path for the slant column measurements which rendered them susceptible to air mass factor uncertainties and spatial artefacts.

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A flight plan was produced prior to the flight for operation at an altitude of 900 m with the sortie split into four separate stages, viz. a flight along the M1 motorway to investigate pollution from fast moving traffic, a flight over Ratcliffe-on-Soar Power Station to observe stack emissions, a repeated flight along a main route through Leicester City to investigate the temporal evolution of NO₂, and a regular grid over Leicester City centre to investigate the spatial distribution of NO₂ over the city centre. The latter portion of the flight plan formed the longest component of the flight, requiring 13 transects over the city centre to capture an area approximately 5 km × 10 km.

During the flight the ANDI instrument was accompanied by two operators, one to monitor the spectra collected by the CompAQS spectrometer, and one to monitor the DSLR and attitude data. All systems operated successfully throughout the flight except for a minor error with the spectrometer which occurred for approximately 46 s towards the end of the flight.

Following the flight the data collected by the ANDI instrument were collated on a server where algorithms were run to provide appropriate formatting and temporal offsets to account for clock differences between computers. The temporal offsets applied provided a first estimate to achieve temporal coherence between the data sets; however additional work to correctly synchronise the data sets was required (see Sect. 3.2).

3.1 Data gridding

During the test flight a GPS system provided longitude, latitude and altitude measurements at one second intervals. The first stage of the data gridding process involved allocating a GPS location to each measurement taken by the CompAQS spectrometer by running a nearest neighbour algorithm on their time stamps to synchronise the two data sets. The derivative of the GPS position data obtained from this process was then calculated to provide a direction of travel vector for the aircraft for each measurement throughout the flight.

Figures 2 and 3 present the geometry of the data gridding process and the variables which describe the orientation of the aircraft, respectively. The relative position on the

surface (in m) of each pixel within the CompAQS FOV was assigned based on the altitude of the aircraft, its position and its direction of travel at the time of the measurement using the GPS location to represent the centre of the instrument's FOV (see Eqs. 1 to 6).

For consistency with the GPS data a non-regular spatial grid was defined in longitude/latitude coordinates with a spatial resolution of 20 m covering an area of 27 km × 50 km. A search algorithm was used to fit each swath onto the grid, and any grid elements used more than once were averaged.

The calculation to determine the grid box locations for each surface pixel began with calculating the distance of each pixel from the centre of the instrument's FOV both in the across-track and the along-track directions. In the across-track direction the distance (d_{ik}) from the centre of the instrument's FOV is given as

$$d_{ik} = a_k \tan(\Phi_i + \psi_k), \quad (1)$$

where i is the index associated with an across track CompAQS pixel, k is the index associated with each measurement swath, a is the GPS derived altitude of the aircraft, Φ is the characterised CompAQS FOV angle for each pixel (see Fig. 3), and ψ is the banking angle of the aircraft calculated from the GPS data (see Sect. 3.3). In the along-track direction the distance c from the centre of the instruments FOV is given as

$$c_{ik} = a_k \tan(\sigma_i), \quad (2)$$

where σ is the along-track angle of curvature of the CompAQS field of view for each pixel (see Fig. 3). Using the results from Eqs. (1) and (2) the distance from the centre of the instrument's FOV in x and y coordinates is computed using

$$x_{ik} = d_{ik} \sin(\theta_k) + c_{ik} \sin(\pm 90 \pm \theta_k), \quad (3)$$

$$y_{ik} = d_{ik} \cos(\theta_k) + c_{ik} \cos(\pm 90 \pm \theta_k), \quad (4)$$

where x and y are the resultant pixel locations in m from the centre of the instrument's FOV, and θ is the aircraft heading vector angle relative to north (see Fig. 2). Finally,

using the results from Eqs. (3) and (4), the latitude and longitude coordinates of each pixel are computed using

$$\text{lat}_{ik} = \left(x_{ik} / F_k^{\text{lat}} \right) + \text{GPS}_k^{\text{lat}}, \quad (5)$$

$$\text{long}_{ik} = \left(y_{ik} / F_k^{\text{long}} \right) + \text{GPS}_k^{\text{long}}, \quad (6)$$

5 where F^{long} and F^{lat} are the conversion factors between metres and longitude and latitude respectively, GPS^{long} and GPS^{lat} are the GPS position coordinates of the aircraft for a given swath in longitude and latitude, and long and lat are the final longitude and latitude coordinates of each pixel in the CompAQS field of view which are fed to the gridding algorithm. Note the \pm signs in Eqs. (3) and (4) dictate that either a + or a -
10 should be used depending on the angular quadrant of the heading vector θ .

The 5m \times 80 m spatial resolution of the CompAQS spectrometer resulted in significant gaps in the gridded data product at 20 m resolution. To provide a spatially continuous data set, a linear interpolation algorithm was applied in the along track direction of flight only, combined with a 2×2 grid box smoothing algorithm to aid in the identification
15 of spatial features. Figure 4 presents an example of the effect of this process on the data, showing two data sets of surface intensity measurements from the test flight over the city centre at 442.7 nm before and after interpolation and smoothing.

3.2 Data temporal synchronisation

The temporal resolution of ANDI's GPS unit combined with the resolution of the CompAQS clock introduced an along track spatial bias of approximately 160 m following
20 initial temporal synchronisation. This uncertainty is sufficient to lead to potential spatial misinterpretation of data during the process of source attribution. To correctly georeference the NO_2 retrievals, the intensity data from the CompAQS CCD at 442.7 nm was plotted and compared to features over Leicester City centre. Features which appeared
25 significantly bright such as white industrial units were used as reference points to adjust the temporal synchronisation of the GPS and CompAQS data sets relative to one

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another until they were in good agreement. Figure 5 presents intensity measurements at 442.7 nm over the city centre to demonstrate the co-location of bright buildings with high intensity measurements following a 160 m relative shift in the data sets.

3.3 Aircraft attitude compensation

Throughout the flight the aircraft's necessary banking during manoeuvres introduced a variable FOV for the CompAQS spectrometer. To compensate for banking in the gridding process a data set of banking angles as a function of flight time was generated. This data would have been provided by the onboard IMU had the data not been corrupted; instead it was calculated by taking the temporal derivative of the aircraft's bearing vector derived from the GPS data combined with a scaling factor. The magnitude of the scaling factor was determined empirically by comparing the surface intensity measurements at 442.7 nm against bright surface features (see Fig. 6). The banking angle approximation would in future need to be replaced by the use of IMU data as the approximation's accuracy cannot be guaranteed for all banking situations.

3.4 NO₂ retrieval

The NO₂ differential slant columns were derived using the DOAS technique in a fitting window from 432–493 nm. The fitting routine was performed using the software, QDOAS (Fayt et al., 2013). Included in the fit were cross sections for NO₂, O₃, CHO-CHO, O₄, H₂O and the Ring Effect (Chance and Spurr, 1997), which were convolved with the wavelength-dependent Gaussian line shape calculated with the QDOAS software. These cross sections were also empirically corrected for the solar I₀ effect (Aliwell et al., 2002). A fourth order polynomial was used to remove broadband structures and no offset correction was applied. The fitting parameters are summarised in Table 2.

Each across-track pixel was attributed an individual reference spectrum, wavelength calibration and wavelength dependent instrument line shape. The wavelength calibration was performed using 6 sub-windows from 428–496 nm, with a single wavelength

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calibration used for each across-track pixel, following determination of negligible wavelength registration variability during the flight. The reference spectra were measured at $12:33:56 \pm 2$ s (GMT), over a region of farmland to the north of Leicester, which was determined to have minimal influence from local emissions of NO_2 , and therefore could be considered a uniform measure of background NO_2 for all across-track pixels. Errors on slant columns were calculated using the standard mechanism within QDOAS.

Data from the ANDI instrument exhibited striping on first analysis. This was likely caused by either unmixed NO_2 within the reference region, or differences in NO_2 sensitivity across the swath owing to changing instrument line shape. A correction was applied to remove this striping using all measurements recorded over Leicester and surrounding rural areas (4500 along-track pixels). Data over Ratcliffe-on-Soar Power station and East Midlands Airport were excluded to avoid any influence of significant discrete plumes. For each across-track pixel, a mean differential slant column density over the flight was calculated, and a second order polynomial fitted across all of these values. Outputs from this process are shown in Fig. 7.

Over the entire flight, deviation from this polynomial curve was interpreted as a bias in the measurement from the across-track pixel in question. Therefore a correction factor was applied to adjust the mean dSCD value for each across-track pixel, so that the mean dSCD over the flight lay on this polynomial. The effectiveness of this process is demonstrated by the lack of striping in the final dataset, despite significant inhomogeneity in NO_2 measurements. Such processes can only be applied when sufficient measurements are taken to ensure that a smooth polynomial can be assumed for the whole dataset, and no dominant NO_2 sources are present in calculated means. The polynomial fitted includes AMF enhancements to the dSCDs towards the edges of the swath, and this structure is retained in order to ensure VCD calculations using AMF corrections can be correctly implemented.

Variability in throughput and gain for each across-track pixel was corrected to ensure that calculations of surface albedo could be implemented across the swath. This correction was calculated using data for the entire flight for the same wavelength used for

the albedo calculations. A mean intensity for this pixel was calculated for the flight, and a correction factor applied to ensure that all across-track means were normalised.

3.5 Air mass factor computation

The dSCD measurements performed by the CompAQS spectrometer are the result of an integrated light path from the Sun to the ground pixel and then to the instrument. When the solar elevation angle is small (as it is in February in the UK) the dSCD measurements are difficult to interpret as a final data product owing to the shallow light path, therefore VCDs were derived by computing air mass factors (AMF). AMFs account for enhancements in the light's atmospheric path length due to factors such as viewing geometry, aerosol scattering, and surface albedo. Therefore, the VCD (Eq. 7) may be defined as the ratio of the SCD and AMF (Solomon et al., 1987).

$$\text{VCD} = \frac{\text{SCD}}{\text{AMF}}, \quad (7)$$

To compute the effects of atmospheric scattering the atmosphere can be modelled as a set of altitude-resolved discrete layers. For optically thin species such as NO₂ the AMF can be generalised as the linear sum of the contribution of each vertical layer to the total SCD divided by the total VCD (Palmer et al., 2001; Boersma et al., 2004):

$$\text{AMF} = \frac{\sum_l m_l (\hat{b}) x_{a,l}}{\sum_l x_{a,l}}. \quad (8)$$

Here, m_l is the box-AMF (BAMF), which represents the vertical sensitivity of layer l to NO₂. Computation of the BAMF is performed using a set of forward model parameters, summarised by the term \hat{b} . These parameters include the scene viewing geometry, surface albedo, NO₂ profile, and aerosol loading. Such parameters can either be derived from the instrument itself, or are determined from modelled datasets. An assumed a priori NO₂ profile, x_a , is partitioned to calculate the VCD for each layer,

$x_{a,i}$. Computation of the BAMF requires the use of a radiative transfer model (RTM). Further discussion of the derivation of the AMF can be found in Rozanov and Rozanov (2010).

For this work the AMFs were calculated using the SCIATRAN RTM (v. 3.1.27, Rozanov et al., 2005). This model has previously been employed to compute AMFs for ground-based MAX-DOAS measurements, (e.g. Kramer et al., 2008; Wang et al., 2012), as well as AMFs for satellite retrievals (e.g. Leitão et al., 2010; Hilboll et al., 2013). The observational geometry was provided using the positional data described in Sect. 3.1, while considerations for other forward parameters are discussed herein. An example of the vertical BAMF profile produced by the RTM is shown in Fig. 8. The AMF is mostly sensitive to conditions below the flight altitude, as the NO_2 and aerosol extinction profile chosen were at their largest below the boundary layer height.

A single NO_2 profile used for the entire flight is shown in Fig. 9. The NO_2 profile was taken from the spatial mean profile over Leicester at 12:00 p.m. (GMT) on the day of the flight as forecast by the MACC-II model ensemble (Stein et al., 2012), and was modelled using a mean surface height of 0.948 km. A high-resolution (5 m \times 5 m) digital elevation model (DEM) provided by BlueSky International Ltd. was used to correct for differences in local surface elevation assumed by MACC-II by scaling the profile to the DEM surface pressure using the technique explained in Zhou et al. (2009). The DEM data product provided by BlueSky International Ltd. did not include building topography. The effect of this on the retrieval is explored in the error analysis in Sect. 4.6.3.

A single aerosol scenario was assumed during the flight, the mixing state for which was defined using the World Meteorological Organization (WMO) database (Bolle, 1986), which assumes particle size distributions and spectral refractive indices for six components of atmospheric aerosol: water soluble, dust, oceanic, soot, stratospheric, and volcanic. Table 3 presents a summary of the scenario used in the AMF computation.

By applying the aerosol backscatter gradient method similar to that described by de Haij et al. (2009) to data from a Campbell Scientific CS135 ceilometer located at

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Lat: 58.7814°, Lon: -1.2844°, the boundary layer height during the flight was estimated at 0.7 km which has been reflected in the lowermost aerosol layer height in Table 3. For all scenarios the aerosol extinction profile was modelled as constant up to the boundary layer height, and then exponentially decaying with height afterward (scale height: 0.2 km). This profile was scaled to the mean AOD at 469 nm of 0.0798 forecasted over Leicester at the time of the flight by MACC-II.

In the absence of clouds and significant changes in the NO₂ vertical profile surface albedo uncertainty can be a considerable source of error in the tropospheric NO₂ AMF computation (Boersma et al., 2004). This uncertainty can be greatly exacerbated by the use of surface albedo data sampled from datasets that are coarser than the instrument resolution (Heckel et al., 2011). In the case of the APEX flight campaign (Popp et al., 2012) this was acknowledged and avoided by directly calculating the surface albedo from the measured radiances which resulted in the surface albedo having the same spatial resolution as the retrieved NO₂. For this work that approach could not be directly repeated, as the CompAQS spectrometer was not radiometrically calibrated pre-flight. Therefore instead the radiances from the CompAQS CCD were used to infer albedo with an empirical adjustment applied to the radiances. The first component of the adjustment was to compensate for the effect of aerosols on the measured surface reflectance, which was partially removed through the use of an empirical correction factor for each ground pixel. The correction factor was calculated by computing the expected intensity at 442.7 nm based on all forward model parameters using SCIATRAN for each ground pixel for scenarios with and without aerosol loading, and then taking the ratio of the two modelled intensities and multiplying them by the surface intensity measurements to generate an intensity data set with reduced aerosol influence.

Following the aerosol correction, the surface albedo of each ground pixel was approximated by linearly scaling the corrected surface intensities recorded by the spectrometer at a single wavelength (442.7 nm) between two reference albedo values. The intensities recorded over regions with water (albedo: 0.07; Clark et al., 2007) and white roofs (albedo: 0.56; Baldridge et al., 2009) were used as the references. For

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this method to be valid it is assumed that the sensitivity of the CompAQS CCD across the fitting window (432 to 494 nm) is correctly represented by 442.7 nm. In the absence of characterisation data for the CompAQS CCD the accuracy of this approximation cannot be determined, however a visual inspection of the intensity data across the fitting window did not reveal any significant sensitivity bias which would suggest the approximation is inappropriate.

A gridded dataset of the AMFs computed for this work is shown in Fig. 10. The variability present in the dataset is dominated by surface albedo, with bright surfaces (e.g. white roofs) coinciding with high AMFs and darker regions (e.g. parks, a canal/river) coinciding with lower AMFs. This is consistent with previous investigations (e.g. Boersma et al., 2004), in which the AMF is also shown to be most sensitive to surface albedo in the absence of clouds and significant variations in the NO₂ profile.

3.6 Vertical column density computation

To calculate VCDs from the ANDI dSCD measurements it is necessary to account for tropospheric and stratospheric NO₂ present in the DOAS reference region. The diurnal increase in stratospheric columnar NO₂ has been previously estimated to be approximately $1.0 \times 10^{14} \text{ molec cm}^{-2} \text{ h}^{-1}$ (Sussmann et al., 2005), which is negligible in comparison to the VCDs retrieved which were on average approximately $3.5 \times 10^{16} \text{ molec cm}^{-2}$. Therefore, it may be assumed that the stratospheric vertical column over the flight region remained approximately constant.

In a similar experiment involving imaging NO₂ from aircraft, Popp et al. (2012) attempted to correct for reference region tropospheric NO₂ in the retrieved dSCDs by adding a single offset estimated from previous air quality model studies (Huijnen et al., 2010). For the spatial scales covered in this work however this approach is unsuitable owing to the coarse spatial resolution offered by such models in comparison to the small region analysed. Instead, the dSCDs measured by ANDI are treated as the NO₂ increment above the lowest dSCD measured throughout the flight, implying the VCDs

calculated from the flight are defined as the increment above UK background levels on the afternoon of the 28 February 2013.

3.7 Uncertainty analysis methodology

The uncertainty in the VCD retrievals combines uncertainties in the SCD measurements and the AMF computation. The uncertainty associated with the SCD measurement is calculated as part of the DOAS fit process and was $7.0 \times 10^{15} \text{ molec cm}^{-2}$ (98 %) on average throughout the flight. The uncertainties associated with the forward model parameters used to produce the AMFs are more difficult to quantify, as each parameter contributes to the overall error budget and in many cases their errors are unknown. To provide a simplified estimate for the retrieval uncertainty associated with the AMF computation a perturbation analysis was performed and is presented herein. It is assumed the independent parameters for the AMF are uncorrelated (i.e. their effects are independent of each other). Each forward model parameter in turn was perturbed by an error estimate resulting in perturbed AMF and VCD values for all ground pixels. The resulting VCDs were subsequently compared against the original VCDs, and the resulting difference was calculated based on the mean deviation from the original values over the entire flight. The VCD modulations caused by the perturbations are representative of a constant bias in the perturbed parameter throughout the flight and therefore provide an estimate for the relative importance of each independent parameter. The details of the parameters perturbed are discussed herein.

The DEM dataset used in the AMF computation did not account for buildings, introducing a level of uncertainty to the VCDs measured over urban terrain owing to atmospheric path length uncertainties. To determine an approximation for the magnitude of the uncertainty associated with this omission, the DEM height used for each ground pixel was perturbed by $\pm 10 \text{ m}$, which is approximately the mean building height in Leicester.

According to the MACC-II validation report for February 2013 (Eskes et al., 2013) the modelled AOD at 469 nm over England had an average bias of -20% when com-

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pared with AERONET data. The AOD was therefore perturbed by $\pm 20\%$ for this study. Additional sources of potential error associated with aerosols not accounted for in this study were the vertical profile of the aerosols and their single scattering albedo. It has been found that these factors can influence the sensitivity of the retrieval to NO_2 below or within such layers (Leitão et al., 2010). For this work, no measurements that would yield information on such factors other than the boundary layer height were available, therefore error estimates of these properties could not be reliably defined.

A previous study has shown that uncertainties in the NO_2 profile shape can lead to AMF uncertainties of approximately 10% (Boersma et al., 2004). It is assumed in this work that the stratospheric NO_2 concentration is approximately constant throughout the flight, therefore the NO_2 profile uncertainty may be considered to be entirely associated with the correctness of the boundary layer NO_2 profile component only. To obtain an approximation for the influence of boundary layer NO_2 profile shape uncertainty on the VCD results, the MACC-II profile was altered to form two scenarios which would make sensible assumptions for the profile shape in the absence of additional information. The first scenario assumes the NO_2 in the boundary layer (i.e. < 0.7 km) is well-mixed, and the second assumes the NO_2 in the boundary layer decays exponentially with height. In both scenarios the net amount of NO_2 in the boundary layer remained the same, ensuring that only the profile shape influenced the AMF. The modified profiles are shown in Fig. 11.

To estimate the uncertainty in the surface albedo a reference surface type was chosen to provide a metric against which to compare the ANDI albedo results. The reference surface for this study was chosen to be asphalt as it can be easily distinguished in the ANDI albedo data along the M1 motorway, reducing the risk of georeferencing error. The data for the study were taken during a parallel flight along the M1 such that the $80\text{ m} \times 5\text{ m}$ pixels of the ANDI system lay entirely over the motorway and not the surrounding countryside. Using albedos modelled in the ASTER dataset for different road surface types (Baldrige et al., 2009) and estimates for the effect of aging on the albedo (Levinson and Akbari, 2002; Puttonen et al., 2009), the asphalt albedo was

determined to be approximately 0.12 for 440 nm with an uncertainty of approximately 0.02. The surface albedo derived from the spectral intensities over asphalt covered pixels were 0.1235 on average, with a standard deviation of approximately 0.0015. The ANDI measured values differ from the reference value by approximately 3% on average. Accommodating the significant uncertainty in the reference used for the albedo results in an estimated error of approximately 0.02 which is equivalent to an uncertainty of approximately 20% in the albedo estimate for the RTM calculations.

A summary of the perturbations applied to each parameter and the results from the perturbation study are given in Table 7 and detailed in Sect. 4.6.

4 Results

The test flight was divided into 4 components, three spatial regions: Leicester City centre, the M1 motorway and Ratcliffe-on-Soar Power Station, and a study on the temporal variability of NO₂ over Leicester City centre. The findings from each of these components are covered separately in the following sections.

4.1 Leicester City centre

The main component of the ANDI test flight consisted of a series of 13 transects flown over Leicester City centre between 12:43 and 13:43 (GMT). From the ANDI data a map of NO₂ VCDs was generated which is shown in Fig. 12.

The VCDs recorded over Leicester City centre were measured to be on average approximately 0.65×10^{16} molec cm⁻² (20%) higher than in two of the city's suburban areas (see Fig. 14 and Table 5 for where these areas are defined). Contributing factors for this enhancement are road traffic and a number of discrete emission sources within and around the city centre, including high VCDs around the train station (1), industry (2), heavily used car parks such as a supermarket and cinema car parks (3), and some particularly highly emitting roads and junctions (5) (see Fig. 12). The NO₂ VCD hot spots

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observed by ANDI were associated with various sources by identifying the land use directly beneath them. Any hot spots that were not easily associated with a particular source were not labelled in Fig. 12, however these sources are likely associated with road traffic as they are over areas where there are no obvious sources of industry or combustion activity.

Comparison of air masses in the city centre region (defined as region (c) in Fig. 14) with air masses which reside in the absence of busy roads and junctions such as over areas of vegetation and agriculture (4) provide an indication of the urban increment of atmospheric NO₂ for Leicester City centre. An area of particularly low NO₂ VCDs is given as region (a) ii in Fig. 14 and Table 5 where there are very few roads and no sources of industrial activity. The city centre (region c) has a 1.04×10^{16} molec cm⁻² (36 %) higher average VCD than region (a) ii, the majority of which is likely associated with Leicester's road traffic for reasons discussed.

A positive trend in atmospheric VCDs of 0.49×10^{16} molec cm⁻² h⁻¹ was measured over the city centre region from 12:43 to 13:43 (GMT), of which at least 0.23×10^{16} molec cm⁻² h⁻¹ has been identified as temporal in nature (see Sect. 4.4). Consequently the comparisons made between the city centre and other regions are only applicable to the time when the measurements were made. For the city centre (region c) the measurements were performed at approximately 13:10 (GMT).

A striping feature present in the north-south direction in Fig. 12 is believed to be caused by along-track spatial interpolation, and a shallow solar elevation angle (26 to 30°) during the flight resulting in artificially extended plumes (see Fig. 13).

4.2 M1 motorway

To investigate the contribution of the M1 motorway to local air quality the ANDI instrument was flown along a 24 km length of the M1 between 14:18 and 14:28 (GMT). Figure 14 highlights this component of the flight using two “M1” indicators. Towards the end of the M1 measurement region in the vicinity of Ratcliffe-on-Soar Power Station and East Midlands Airport (EMA), the VCDs became dominated by high concentra-

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It should be noted that the NO₂ emitted from Ratcliffe-on-Soar Power Station is released into the atmosphere from a 200 m high chimney stack. ANDI measures VCDs and therefore the vertical distribution of the power station emissions must be taken into account if surface concentrations are to be derived from this data.

4.4 Temporal variability of NO₂ VCDs

To investigate the validity of characterising a city's NO₂ distribution by measuring single instances of NO₂ VCDs, a number of transects were flown along Narborough road and the A6 (diagonally across the city centre) to observe the temporal variability of the NO₂ VCDs. The GPS navigation system used by the pilot did not enable precise returns along the same course however, restricting this part of the study to being largely qualitative. Figure 16 presents the NO₂ data for 4 transects flown between approximately 13:40 and 14:00 (GMT).

The results demonstrate both a temporal and spatial consistency in NO₂ VCDs throughout the 20 min the measurements were taken. On the left side of the transects (region A of Fig. 16) there is a temporally consistent area of relatively high NO₂ VCDs which coincides with industrial buildings and a major road junction leading onto the M1 motorway. Between this junction and Leicester City centre (region B) there is a temporally consistent area of relatively low NO₂ VCDs over an area of Leicester's suburbs. Towards the middle of each transect (region C) there is a relatively high area of NO₂ VCDs which is Leicester City centre, with a small but highly discrete area of relatively very low NO₂ VCDs near to the middle (region D). The area of relatively low NO₂ VCDs in the city centre is present in all four transects (though less obviously in the first and last transects), however its exact position and magnitude varies which may be associated with a combination of meteorological and emission variability, and to some degree georeferencing error on account of aircraft banking uncertainty, GPS precision and measurement location variability on account of ANDI's 80 m forward spatial resolution. The surface type beneath region D is parkland (Abbey Park), demonstrating the presence of a stable air mass with relatively few emissions beneath it.

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(56 %). During the time period shown in Fig. 17, the RH increased by approximately 8 %. To get a theoretical sense of how this change might impact the AOD and in turn the AMF, the OPAC aerosol model (Hess et al., 1998) was used to estimate the impact with a continental average aerosol configuration. The results showed that an increase in RH from 50 to 60 % would lead to an 8 % increase in AOD at 450 nm. However, as is shown in the perturbation study in Sect. 4.6, a 20 % increase in AOD was calculated to change the retrieved NO₂ VCD by less than 1 %. Therefore, given the information available the 6.4 % increase in NO₂ during this portion of the flight appears to be associated with an increase in atmospheric NO₂, possibly as a result of emissions build-up in the atmosphere owing to slow wind speeds during the flight (1.2 ms⁻¹ on average) combined with oxidation chemistry of NO to NO₂.

To separate the temporal from the spatial (east to west) contributions within the observed VCD gradient, a region of interest (defined as 2 in Table 5) was averaged for 5 time intervals where spatial coincidence was achieved throughout the flight, thus obtaining NO₂ measurements without significant spatial variability. The results are presented in Table 6. The first data point of the 5 available was measured during the first overpass of region (c) in Fig. 14, which was an hour prior to the following 4 data points which were taken during the repeated flights across Narborough Road and the A6.

The temporal gradient in the VCD measurements from the 5 data points is approximately 0.23×10^{16} molec cm² h⁻¹, confirming the existence of a temporal increase in NO₂ concentrations throughout the flight. The difference in magnitude between this result and the temporal trend over the city centre (0.49×10^{16} molec cm² h⁻¹) may be partially explained by the location of the region sampled, which was suburban and therefore will have lower NO₂ emissions than the city centre. In addition it must be considered that the data used for the latter study was very sparse both temporally (only 5 data points) and spatially (only 220 m × 220 m area) and therefore subject to significant uncertainty on account of local spatial and temporal variability in atmospheric composition and emission sources (see Fig. 16) as well as statistical error. In addition, the

ANDI surface pixel locations differ from scene to scene within the region of interest which could also have led to differences in the results.

With recognition of the significant uncertainties involved in quantifying and characterising the VCD trend over the city centre, it may be concluded that at least $0.23 \times 10^{16} \text{ molec cm}^2 \text{ h}^{-1}$ (47%) of the NO_2 trend is the result of a temporal increase in the atmospheric concentration of NO_2 over the city centre.

4.5 Spatial distribution of NO_2 VCDs

The ANDI test flight lasted two hours and covered three distinctly different regions of Leicestershire (see Sect. 4). When plotted as a continuous data set, the ANDI results produce an extensive map of atmospheric NO_2 VCDs covering multiple land use types (see Fig. 14). Within the full ANDI data set two separate spatial scales of interest are present: the larger scale ($> 1 \text{ km}$) was captured in the regional comparison study included in Sect. 4.3 and presented in Table 4, in which the accumulation of multiple emission sources over time associated with a particular region appear to contribute to spatially extensive regional biases in atmospheric NO_2 concentrations. The finer scale variability ($< 1 \text{ km}$) is present in both Figs. 12 and 16, in which individual sources likely in combination with local meteorology appear to influence the local magnitude and distribution of the atmospheric NO_2 concentrations. In the context of human exposure consideration of both scales is important, as the large scale variability demonstrated by the temporal trend discovered over the city centre (see Fig. 17) will modulate the finer scale distributions which are of interest where concentrations may exceed safe limits.

Repeat flights along Narborough road discussed in Sect. 4.4 demonstrated the presence of a temporal component to the NO_2 VCD trend observed over the city centre, however a contribution from an east-west spatial trend cannot be discounted.

Along track spatial biases introduced by the low solar elevation angle and along-track spatial interpolation were potentially contributing factors to the partial disappearance of the area of low NO_2 VCDs in the vicinity of Abbey Park in the top and bottom transects of Fig. 16. In addition, wind is likely to have also contributed to the differences

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observed in the transects, particularly over the Abbey Park area which may have been subject to import of NO₂ from the surrounding road network. The wind speed measured by the Leicester City Council meteorological station (Lat: 52.652°, Lon: -1.176°) was approximately 1.2 ms⁻¹ at 15° from north, which varied by < 0.2 ms⁻¹ and 5° from north during the flight. The contribution of the wind vector to the spatial distribution of atmospheric NO₂ is difficult to discern in the data sets owing to the spatial artefacts discussed previously and the low wind speed.

Region (a) i in Table 5 and Fig. 14 highlights an anomalous region of high NO₂ VCDs which is difficult to attribute to a particular source. The surface beneath region (a) i is farmland with only a single source of industry in the form of a small farm machinery factory, and no additional sources of industry or major roads within a 1.6 km radius of the area. Despite the apparent scarcity of sources the measured VCDs over this area are of a similar magnitude to Leicester City centre. A possible reason for the high NO₂ VCDs observed is the farm machinery factory emitting a significant quantity of NO₂ throughout the day, which may have increased the atmospheric concentration over time similar to the trend observed over Leicester City centre (see Fig. 17).

4.6 Perturbation analysis to estimate uncertainties

The error in the retrieved VCD measurements consists of uncertainties in both the SCD and AMF calculations.

The mean SCD error across the flight can be calculated from the DOAS fit process. For the entire flight this was calculated to be an average of 1.9×10^{16} molec cm⁻². Using Eq. (7) this value is converted into an uncertainty in the derived dSCD resulting in an error of 7.0×10^{15} molec cm⁻².

The uncertainty in the AMF computation is more difficult to determine as discussed in Sect. 3.7. An approximation for the uncertainty of some of the independent parameters associated with the AMF have been derived by means of a perturbation analysis. The results of the perturbation analysis are discussed for each parameter herein, with Table 7 presenting a summary of the uncertainties derived from the study.

The findings from the investigation demonstrate the dominant sources of uncertainty for the AMF computation are the NO₂ profile shape in the boundary layer followed by the albedo uncertainty, with AOD and DEM errors being less important.

Assuming the four parameters investigated for the AMF uncertainty are the most relevant of the associated error sources, and that they may be treated as uncorrelated and random in nature, then an overall error estimate for the AMF's may be approximated by combining the square of the errors for each AMF parameter. The total AMF contribution to the error using this method is calculated to be approximately 3.25×10^{14} molec cm⁻² which is ~ 8 % when applied to the flight data. Owing to the omission of some error contributors (see Sect. 3.7) and the nature of how this error estimate was derived, the quoted AMF contribution to the VCD error can only be considered to have an order of magnitude level of confidence.

4.6.1 Albedo error

The determination of absolute radiances from the recorded spectra would have led to an empirically derived albedo with comparatively little uncertainty (Popp et al., 2012); however the ANDI spectrometer was not radiometrically calibrated prior to the flight and therefore absolute radiances could not be computed from the measured intensities on the detector (see Sect. 3.7 for details). For the perturbation analysis, positive and negative perturbations respectively were applied with an uncertainty of 0.02 on the albedo estimates, this resulted in an average of -1.41×10^{14} molec cm⁻² (-2.4 %) and 1.8×10^{14} molec cm⁻² (2.8 %) errors in the VCD measurements (see Table 7).

4.6.2 Aerosol optical depth

The magnitude of the aerosol optical depth is a critical parameter used in the RTM for the AMF computation as it defines vertical sensitivity to NO₂ and atmospheric path length, both of which significantly influence the magnitude of the AMF (see Sect. 3.7). For positive and negative perturbations respectively the estimated uncertainty of ±20 %

on the AOD resulted in an average of $5.89 \times 10^{13} \text{ molec cm}^{-2}$ (0.90 %) and $-5.45 \times 10^{13} \text{ molec cm}^{-2}$ (-0.82 %) errors in the VCD measurements (see Table 7).

4.6.3 DEM error

The omission of building topography in the DEM data is likely to result in uncertainties in the AMF computation on account of incorrect atmospheric path length assumptions in the RTM (see Sect. 3.7). For positive and negative perturbations respectively the estimated uncertainty of $\pm 10 \text{ m}$ in the DEM resulted in an average of $1.91 \times 10^{13} \text{ molec cm}^{-2}$ (0.34 %) and $-1.5 \times 10^{13} \text{ molec cm}^{-2}$ (-0.26 %) errors in the VCD measurements (see Table 7).

4.6.4 Profile shape

As part of the AMF computation the RTM requires an assumed NO_2 profile shape to determine vertical sensitivity. The shape of the NO_2 profile was unknown at the time of the measurements, therefore a simulated profile was used for all retrievals from the MACC II ensemble product. To provide perturbation on the profile shape, two alternative profiles were formed (see Sect. 3.7), their affect on the AMF calculation is presented in Table 7. The use of a well mixed profile as opposed to the MACC II profile in the RTM simulations resulted in a significant modulation of the VCD results of -41.7×10^{13} (-6.5 %). The use of an exponential profile as opposed to the MACC II profile generated a less significant modulation of approximately -13.4×10^{13} (-1.9 %).

5 Conclusions

The results in this paper demonstrate that the ANDI instrument can provide a unique and informative perspective on atmospheric NO_2 distributions around an urban environment.

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of approximately 8 % was derived based on the information available. The majority of the AMF error is attributed to potential uncertainties in the NO₂ profile shape and the surface albedo. The latter contribution will be addressed in future flights through pre-flight radiometric calibration of the spectrometer, as will the uncertainty in the SCD measurements through improved optical alignment of the spectrometer.

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**Table 1.** Relevant specifications of the CompAQS spectrometer used in the ANDI system.

Component	Specification
Spectral range	420 to 590 nm
Spectral resolution	1.5 nm
Field of View (azimuth)	34°
Angular Resolution (across track)	0.26°
Detector type	CCD
Sensor size (post frame transfer)	512 × 1024
Spectral binning	2 (512 pixels)
Spatial binning	4 (128 pixels)

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**Table 2.** Fitting parameters used for the DOAS fits in this work.

Fitting Parameter	Value
Fitting Window	428–495 nm
Reference Spectrum	Row specific reference measured over remote farmland
Line Shape	Gaussian (wavelength dependent, calculated from QDOAS)
Solar Reference	Solar atlas (Kurucz et al., 1984)
Wavelength Calibration	NLLS fit of object and reference spectrum to solar reference.
Cross Sections	
NO ₂	Vandaele et al. (1996) ($T = 294$ K, I_0 correction: 1.0×10^{16} molec cm ⁻²)
O ₃	Bogumil et al. (2003) ($T = 223$ K, I_0 correction: 1.0×10^{20} molec cm ⁻²)
O ₄	Greenblatt et al. (1990)
Ring	Modelled by QDOAS (Chance and Spurr, 1997)
H ₂ O	Rothman et al. (2003)
CHOCHO	Volkamer et al. (2005)
Polynomial	Fourth order

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Table 3. The aerosol loading scenario based on the WMO climatology assumed for all ground pixels in this study.

Layer height (km)	Mixing state
0.0–0.7	Urban
0.7–20.0	Continental
20.0–50.0	Background
50.0–100.0	Background

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Table 4. VCD max, mean (\bar{x}) and standard deviations (σ) in ($\text{molec cm}^{-2} \times 10^{16}$) from selected areas within the ANDI gridded data (see Fig. 14).

Region	Time	Max	\bar{x}	σ
*Rural (a) i	14:15	5.93	3.58	0.52
Rural (a) ii	12:35	4.73	2.92	0.48
Suburbs (b) i	13:30	5.14	3.19	0.49
Suburbs (b) ii	13:05	4.84	3.42	0.43
City centre (c)	13:10	6.06	3.96	0.45
Power station (d)	14:25	9.27	6.33	0.79

* Rural (a) i is an anomaly discussed in Sect. 4.5. The times presented are the approximate measurement times for each region.

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Table 5. Coordinates for regions of interest, top 6 region identifiers are associated with Fig. 14, region 1 identifier with Fig. 16 and region 2 identifier with Table 6.

Region	Long. low	Long. high	Lat. low	Lat. high
(a)i	−1.292	−1.168	52.508	52.535
(a)ii	−1.226	−1.186	52.672	52.706
(b)i	−1.117	−1.092	52.606	52.627
(b)ii	−1.146	−1.123	52.663	52.682
(c)	−1.146	−1.120	52.630	52.648
(d)	−1.337	−1.204	52.846	52.914
1	−1.134	−1.132	52.645	52.646
2	−1.161	−1.158	52.617	52.620

(a) – Rural areas, (b) – Suburban areas, (c) – City Centre area, (d) – Power station area.

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Table 6. Average VCD measurements in $\text{molec cm}^{-2} \times 10^{16}$ for region 2 in Table 5 for 5 over-passes.

Measurement Time	NO ₂ VCD
12:40	3.75
13:43	3.94
13:49	4.01
13:54	3.94
14:01	4.11

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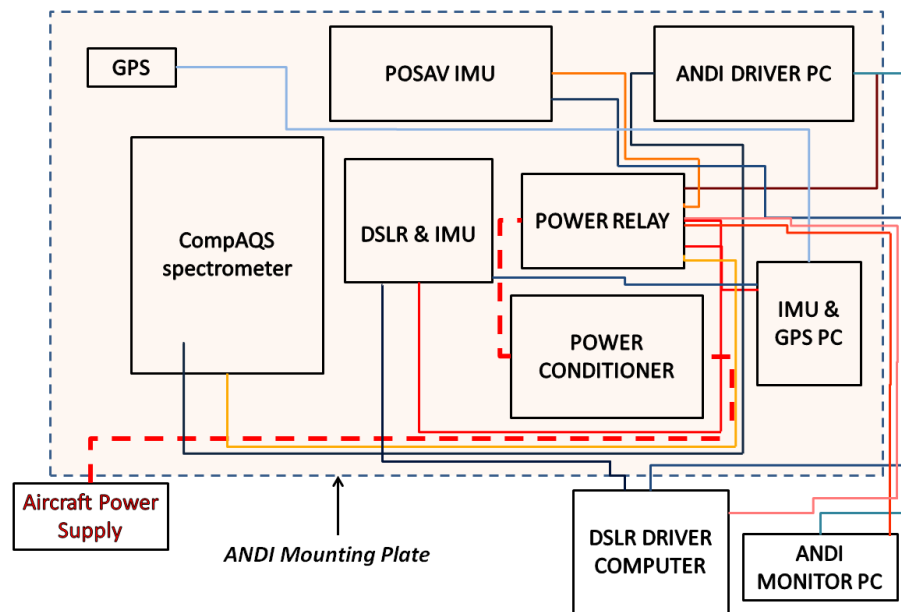


Figure 1. ANDI instrument schematic showing main components, red lines represent power connections, blue lines represent communication connections.

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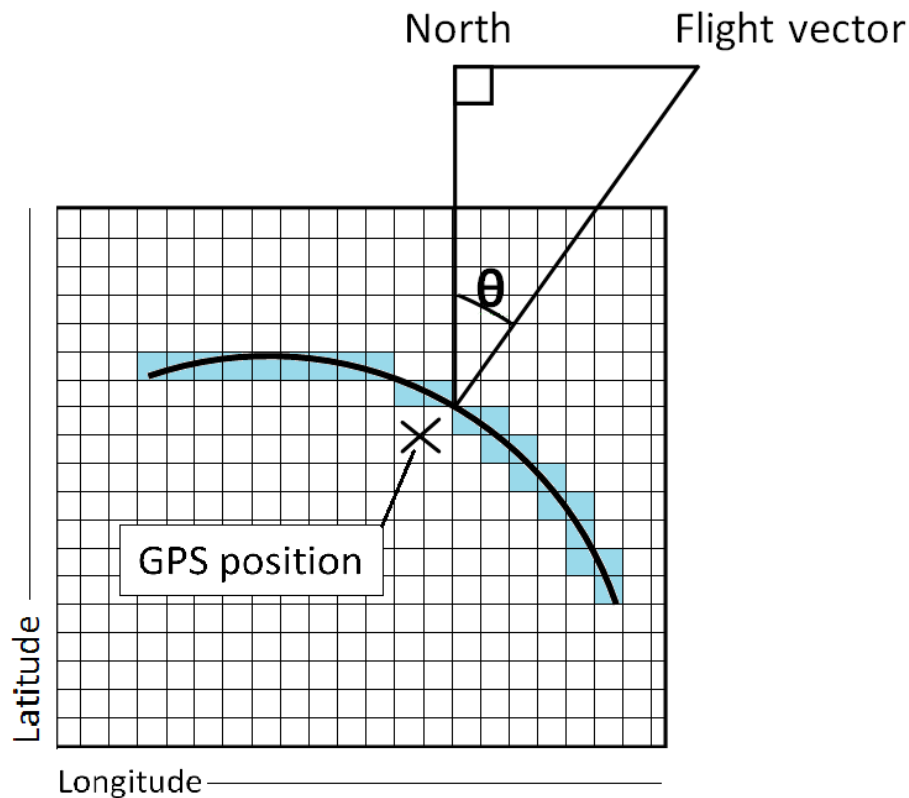


Figure 2. Schematic of the gridding process, showing the GPS location relative to the ComPAQS field of view (curvature exaggerated for display purposes) shown as the black curve.

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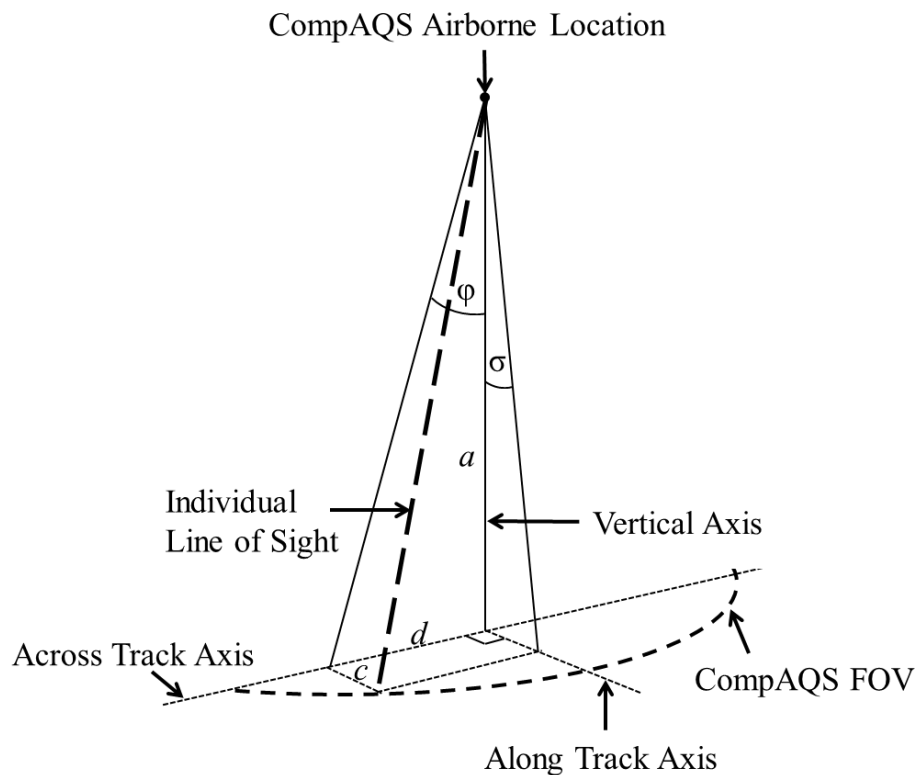


Figure 3. Schematic demonstrating the dimensions and geometry used to define the terms given in Eqs. (1) to (6).

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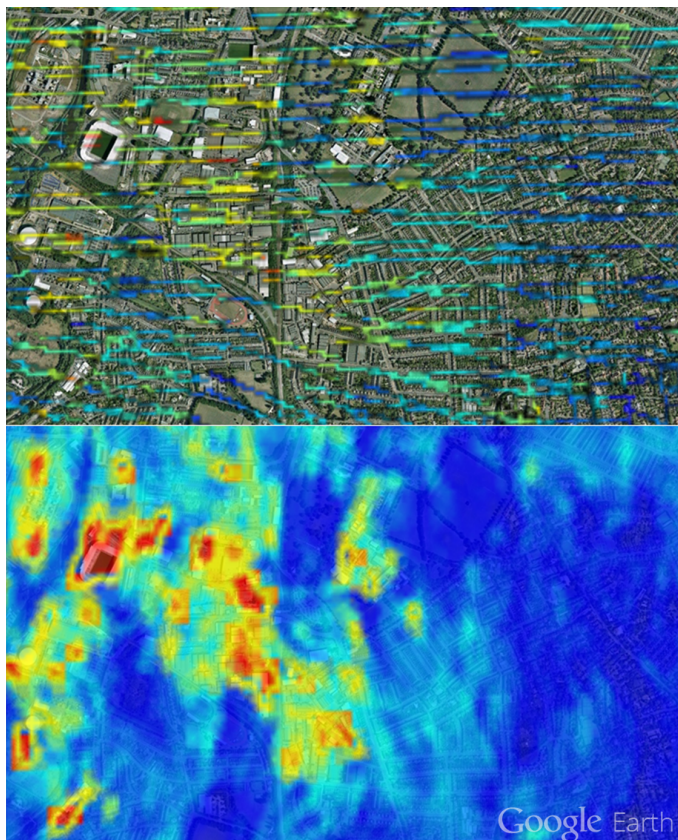


Figure 4. 20 m resolution surface intensity (442.7 nm) with (bottom) and without (top) along-track linear interpolation and 2×2 grid cell smoothing, colours represent surface intensity, red is brighter, blue is darker.

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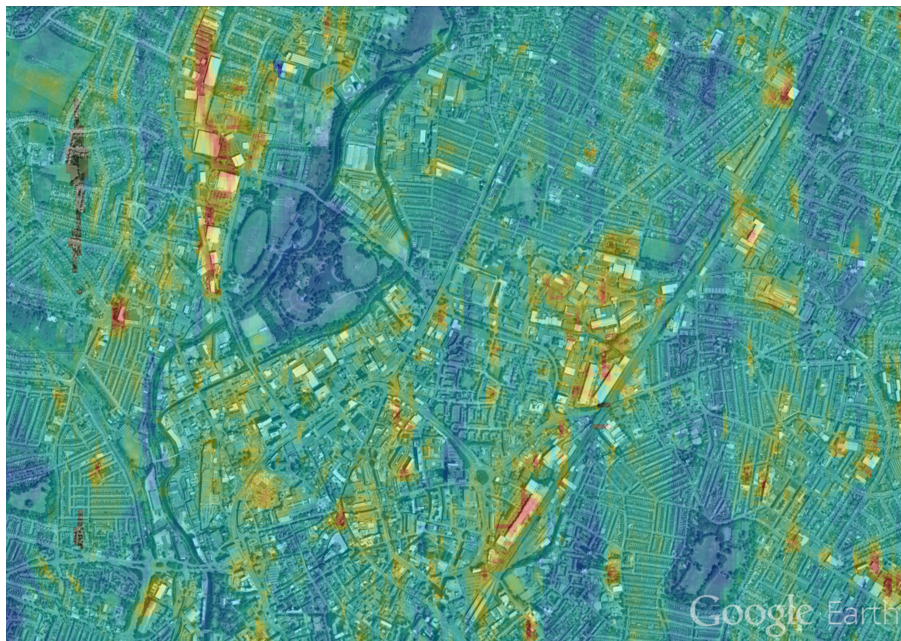


Figure 5. CompAQS 442.7 nm forward interpolated intensity data showing co-location of bright industrial units and high intensity data recorded by CompAQS.

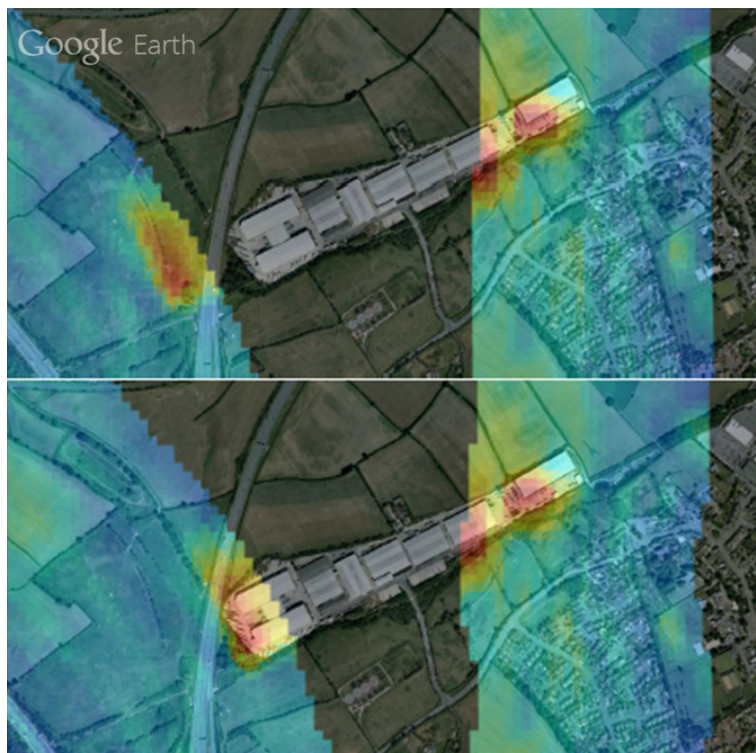


Figure 6. Top – CompAQS 442.7 nm intensity data showing incorrect georeferencing prior to banking correction. Bottom – CompAQS 442.7 nm intensity data showing improved georeferencing following banking correction. Two swaths are shown, one during banking (left) and one during level flight (right).

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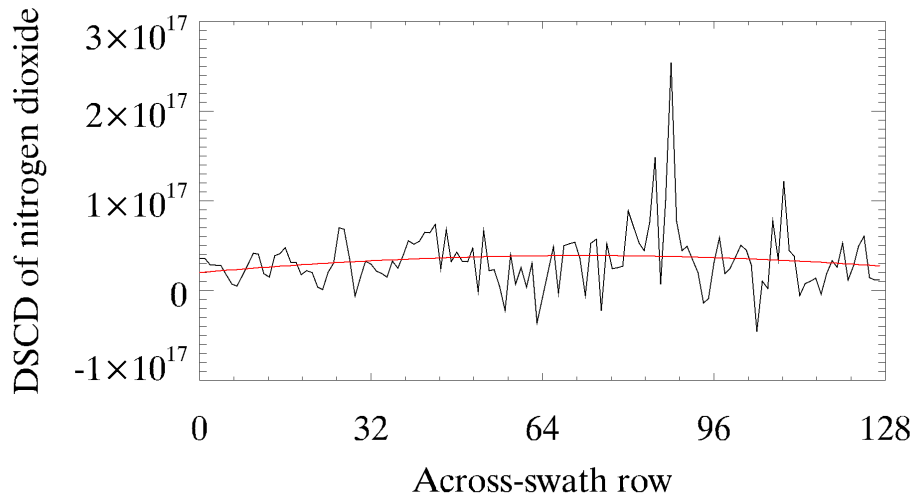


Figure 7. Destriping procedure on the data from the ANDI instrument. In black are mean differential slant column density measurements from each across-track pixel, averaged over the entire flight. In red are mean differential slant column densities after destriping has been applied.

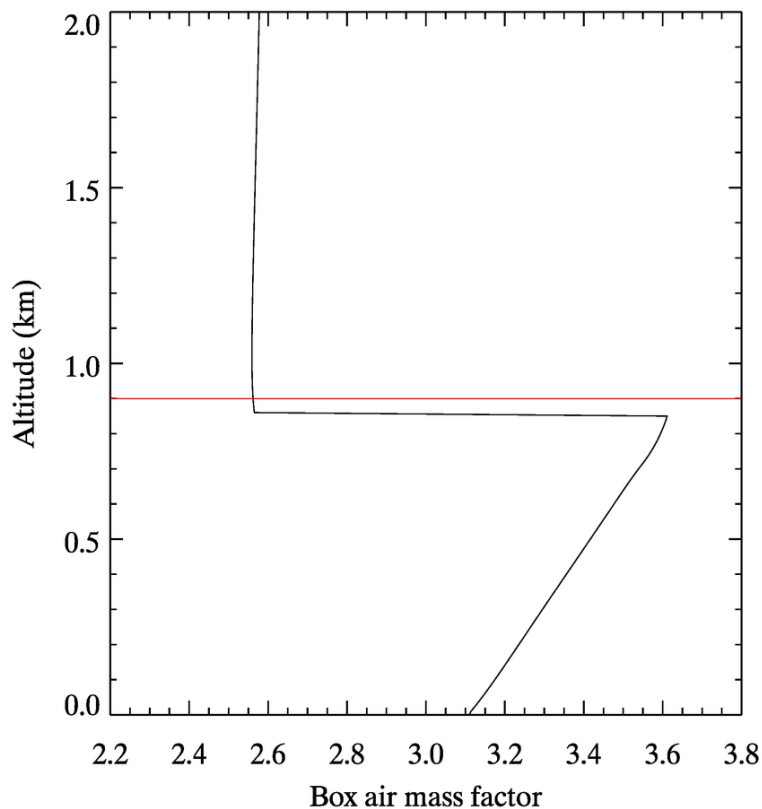


Figure 8. A typical box air mass factor calculated by the SCIATRAN RTM for a rural ground pixel. The red line indicates the instrument altitude (0.9 km) at the time of the measurement.

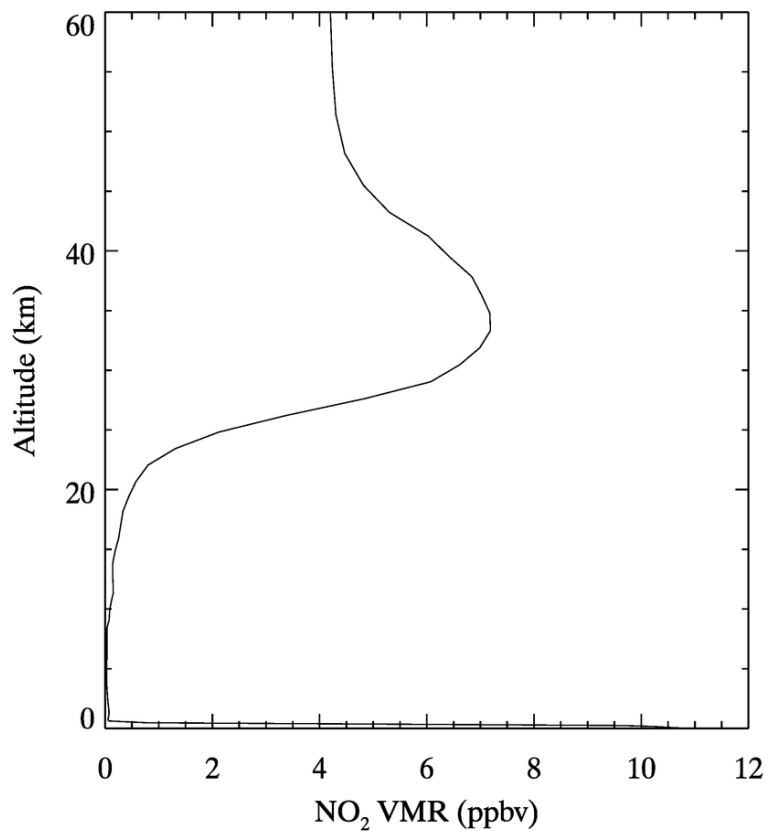


Figure 9. The mean MACC-II NO₂ profile forecast over Leicester at 12:00 p.m. on 28 February 2013.

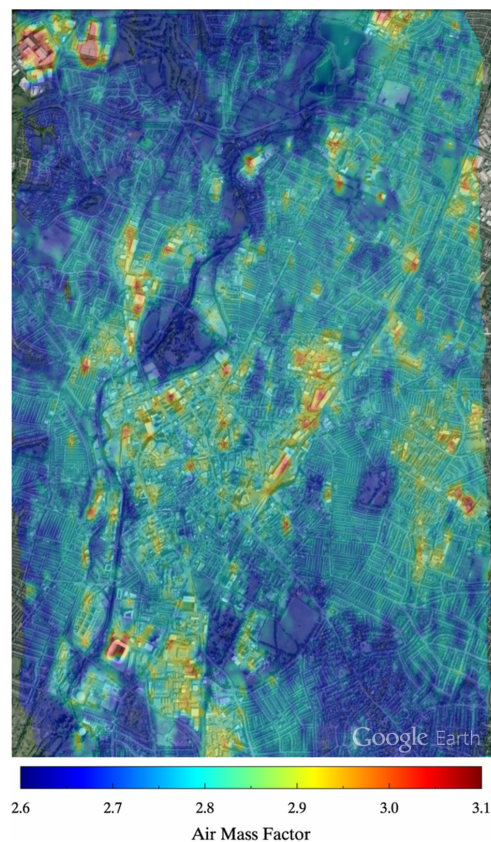


Figure 10. The gridded AMFs calculated for this work, showing the sensitivity of the AMF computation to surface albedo. Bright regions such as white roofs result in higher AMFs, while darker regions such as rivers, canals and parkland have lower AMFs.

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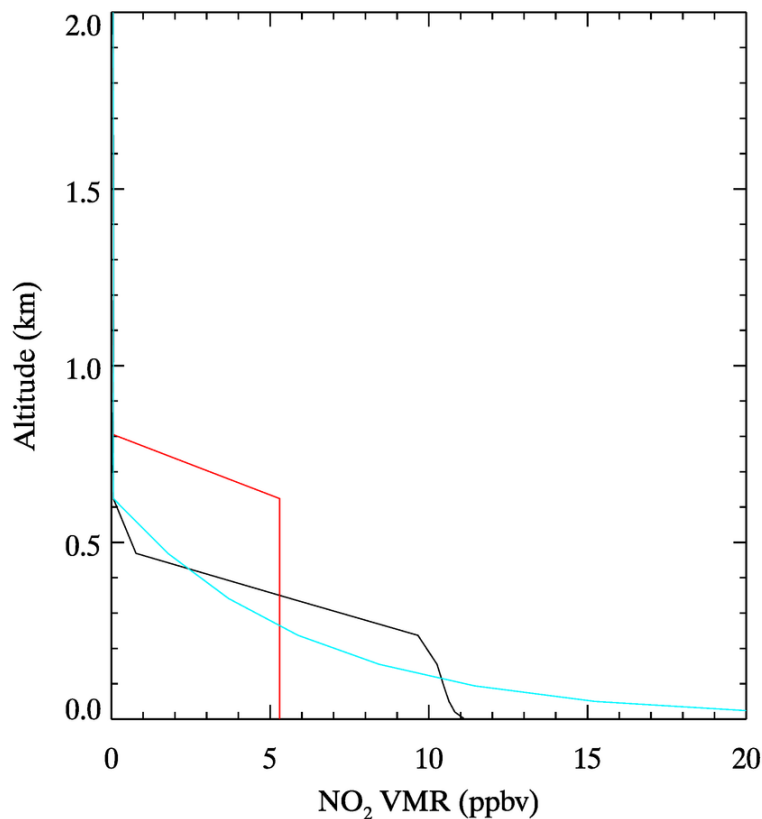


Figure 11. The constant (red) and exponential (blue) boundary layer NO_2 profiles used in the perturbation study. Above 2 km the profile is the same as Fig. 9 (black).

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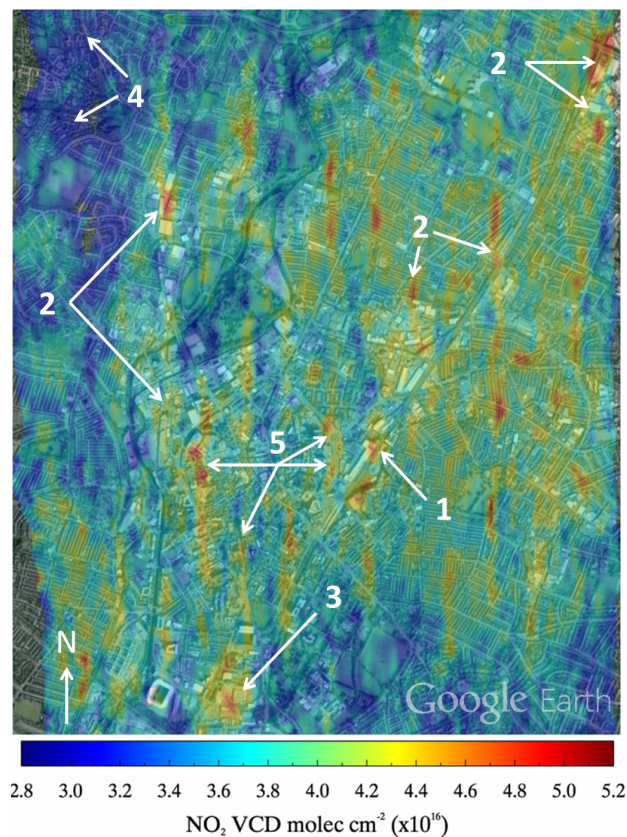


Figure 12. NO_2 VCD data recorded over Leicester City centre overlaid on Google Earth with areas of interest highlighted. Regions of interest labelled in the diagram are the train station (1), industrial areas (2), car parks (3), farmland (4), and highly emitting roads and junctions (5).

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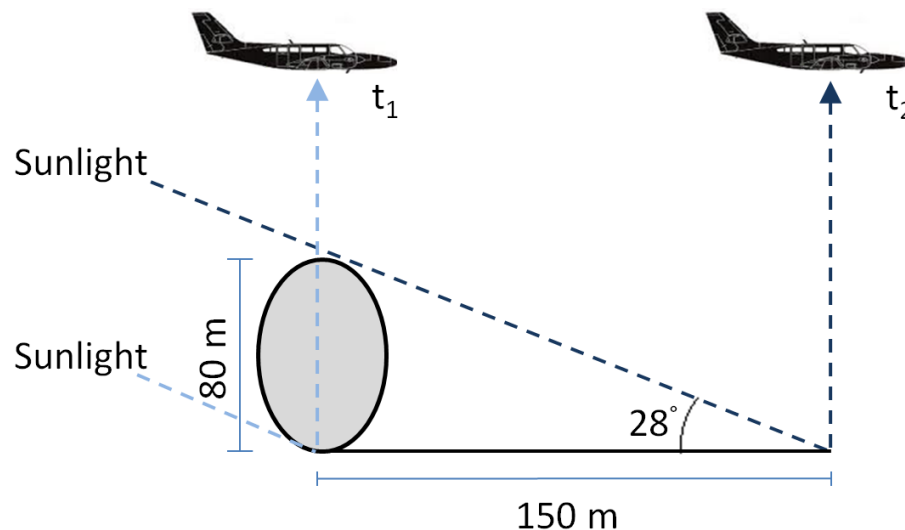


Figure 13. Schematic showing the contribution of solar geometry to the north-south striping seen in the data. Plumes 80 m high will produce 150 m artefacts on the surface. t_1 and t_2 correspond to two measurement intervals 150 m apart.

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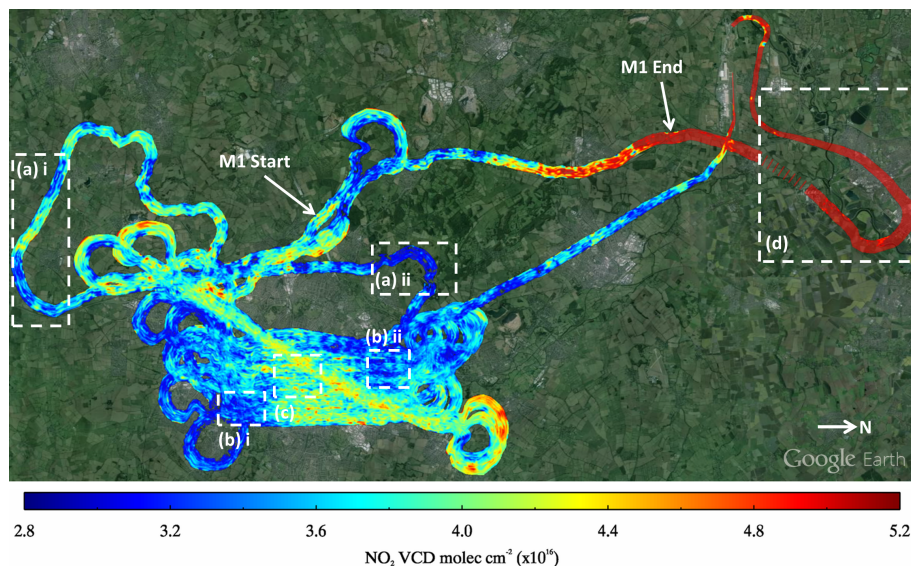


Figure 14. Complete ANDI data set from the test flight plotted in Google Earth with features of interest and areas used for regional averages highlighted. Coordinates for these regions are provided in Table 5.

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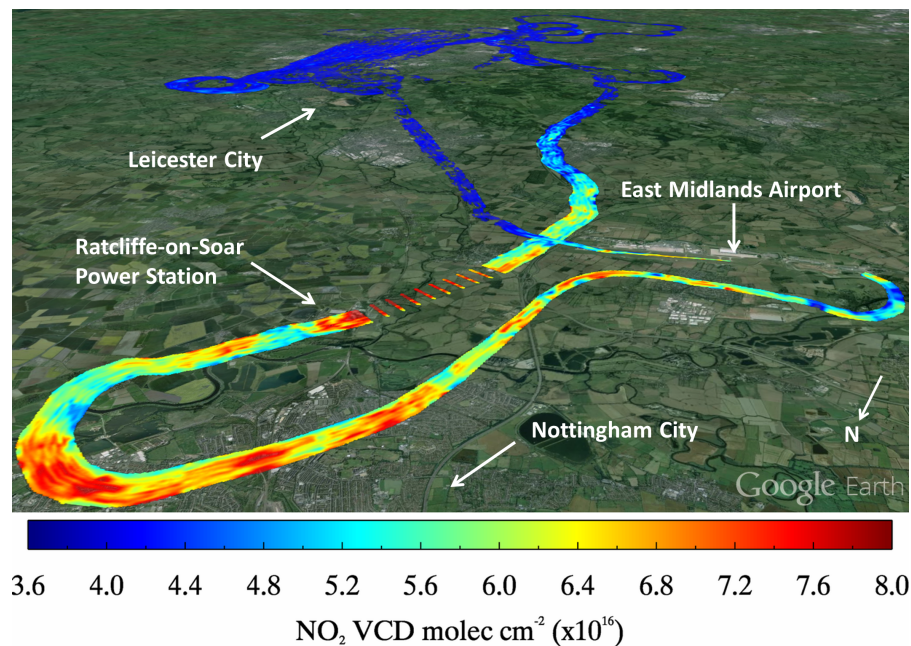


Figure 15. NO₂ VCDs over Leicester and an area close to Ratcliffe-on-Soar Power Station and EMA. The colour scale is appropriate to discern structure within the area. The emissions from the power station are likely elevated having been emitted from a 200 m high chimney. The gap in the data just prior to the power station is caused by the CompAQS spectrometer failing for 46 s.

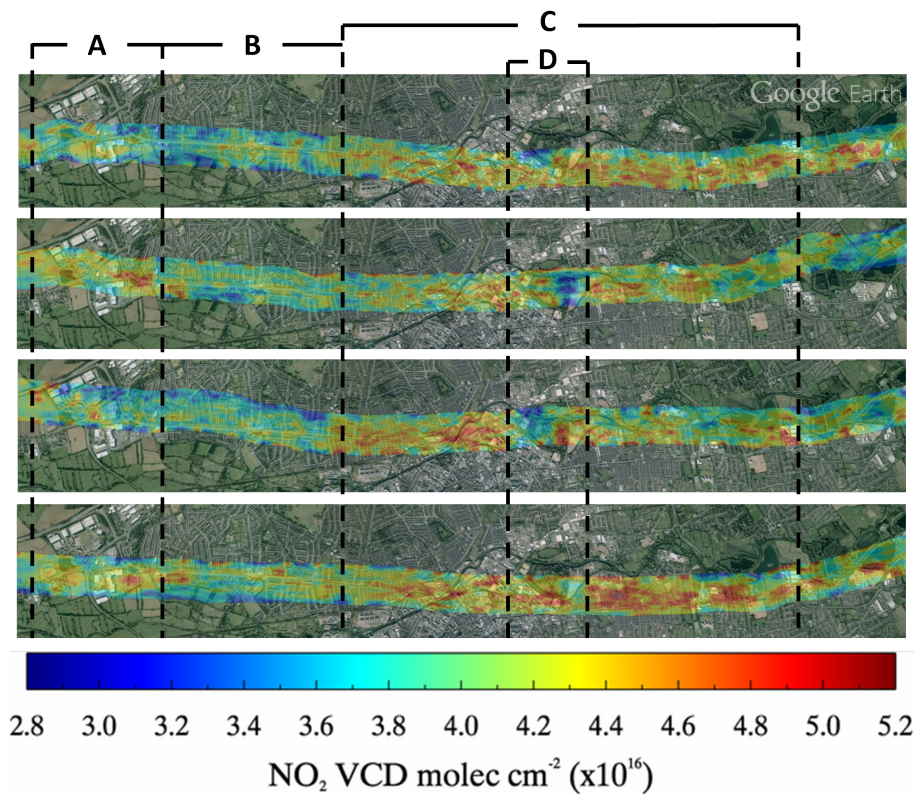


Figure 16. Repeat NO₂ measurements over Narborough road and the A6 moving through time from top to bottom. Each point on adjacent transects is approximately 6 min apart. Coordinates for the region are provided as region 1 in Table 5.

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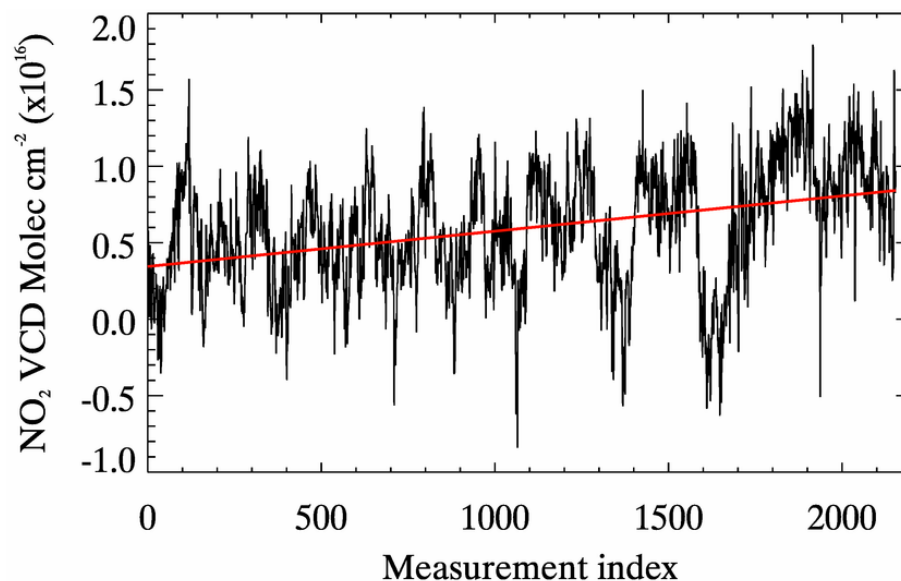


Figure 17. VCD measurements as a function of measurement index (time) with line of best fit presented in red. Measurements were averaged over ± 30 pixels from the nadir, taken from 12:43 to 13:43. Line gradient is $0.49 \times 10^{16} \text{ molec cm}^{-2} \text{ h}^{-1}$.

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