Dead time effect on the Brewer measurements: Correction and estimated uncertainties

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Abstract

Brewer spectrophotometers are widely used instruments which perform spectral measurements of the direct, the scattered and the global solar UV irradiance. By processing these measurements a variety of secondary products can be derived such as the total columns of ozone, sulfur dioxide and nitrogen dioxide, and aerosol optical properties. Estimating and limiting the uncertainties of the final products is of critical importance. High quality data have a lot of applications and can provide accurate estimations of trends.

The dead time is ~~characteristic~~ specific for each instrument and ~~non-~~improper correction of the raw data for its effect may lead to important errors in the final products. ~~It~~ The dead time value may change with time and, with the currently used methodology, i~~s~~t cannot be ~~not~~ always determined ~~sufficient to~~ accurately ~~determine the correct dead time~~. For specific cases, such as for low ozone slant columns and high intensities of the direct solar irradiance, the error in the retrieved TOC, due to a 10 ns change in the dead time from its ~~nominal~~ value in

use, is found to be up to 5%. The error in the calculation of UV irradiance ~~is about~~can be as high as ~~3-4~~12% near the maximum operational limit of light intensities. While in the existing documentation it is indicated that the dead time effects are important when the error in the used value is greater than 2 ns, we found that for single monochromator Brewers a 2 ns error in the dead time may lead to ~~uncertainties~~ errors above the limit of 1% in the calculation of TOC; thus the tolerance limit should be lowered. A new routine for the determination of the dead time from direct solar irradiance measurements has been created and tested and a validation of the operational algorithm has been performed. Additionally, new methods for the estimation and the validation of the dead time have been developed and are analytically described. Therefore, the present study, in addition to highlighting the importance of the dead time for the processing of Brewer datasets, also provides useful information for their quality control and re-evaluation.

1 Introduction

In the beginning of the 1980's, the increased concern for the stratospheric ozone depletion (Farman et al., 1985) and its effects on surface UV levels (Kerr and McElroy, 1993; Zerefos, 2002) stimulated the deployment of the first Brewer ozone spectrophotometers. Until 1996 Brewer instruments were manufactured by SCI-TEC~~Sci-Tec~~ Instruments Inc. at Canada. In 1996, SCI-TEC~~Sci-Tec~~ Instruments Inc. merged with Kipp and Zonen ~~Inc~~BV~~.~~ and since then ~~they~~ are produced at Delft, ~~Holland~~the Netherlands. Nowadays, more than 200 instruments are deployed worldwide. Brewers are either single monochromators (versions MKII, MKIV, and MKV) or double monochromators (version MKIII) and ~~are~~ may be equipped with ~~two types~~multiple-board (MB) or single-board (SB) ~~of~~ electronics ~~(old and new)~~. Although of the same make, the characteristics of individual instruments may differ significantly. The Brewer network provides a variety of products such as the total columns of ozone (TOC) (Kerr et al., 1981), SO2 (Cappellani and Bielli, 1995) and NO2 (Cede et al., 2006; Diémoz et al., 2014), the aerosol optical depth (AOD) (Bais et al., 2005; Gröbner and Meleti, 2004; Meleti and Cappellani, 2000), as well as global and direct irradiance spectra (Bais et al., 1996; Bais et al., 1993). These measurements have supported scientific research for more than 30 years, enabling the investigation of their short-and long-term variability (Glandorf et al., 2005; Weatherhead et al., 1998; Zerefos, 2002) and interactions among them and among other atmospheric constituents (Bernhard et al., 2007). Additionally, good quality ground based measurements are very useful for the validation of satellite products which, under specific conditions, may be highly uncertain (Fioletov et al., 2002).

The uncertainty in the TOC retrieval is estimated to about 1% (Kerr et al., 1985), while for well-maintained and properly calibrated instruments, the uncertainty of UV spectral irradiance is estimated to about 10% and 5% for the UVB and the UVA spectral regions respectively (Bais et al., 1996). More recent studies indicated that the measurements can be largely affected by the individual characteristics of each instrument (Gröbner et al., 2006) and that proper corrections are needed in order to keep the uncertainties within the above mentioned limits, or even reduce them further (Garane et al., 2006; Karppinen et al., 2014; Lakkala et al., 2008).

~~The non-ideal cosine response of the UV irradiance collector may lead to an underestimation of the diffuse component of the global irradiance by up to 12% (Garane et al., 2006) and to an underestimation of the direct component that may exceed 20% for solar zenith angles (SZAs) greater than 70° (Lakkala et al., 2008). The same studies suggest that the absolute response of the instruments may change by 0.2 – 0.3% per 1°C change of the internal temperature, depending on instrument and wavelength of the incident irradiance. Considering the TOC measurements from single monochromator Brewers, stray light effects can lead to underestimation of 2% - 6% for ozone slant columns between 1600 and 2000 Dobson Units (DU) (Karppinen et al., 2014).~~

Yet, there are ~~additional~~ uncertainties related to constructional, technical or operational characteristics of the instruments, which are not adequately investigated and documented, and it is debatable whether the applied relevant corrections are optimal. The dead ~~-~~time ~~(DT)~~ of the photon counting systems used in the Brewers is one of these characteristics. The dead time is a measure of how long a photon counting circuit is unable to detect a second photon after a first photon has been detected (SCI-TEC Instruments Inc., 1999). The probability that a photon reaches the counting system within this “dead” time interval increases with the rate of the overall incoming photons (i.e. with intensity of radiation). Thus, ~~measurements~~the recorded signals have to be properly corrected to compensate the non-linear response of the system due to the effect of the dead time. For the correction a dead-time constant (DT) is used, which is initially determined by the manufacturer, but during regular operation it is calculated and recorded on daily basis by the Brewer operating software. ~~For about one third of the instruments participating in the RBCC-E calibration campaigns the difference between~~

~~the calculated DT differs fromand the DT used in the data correction exceeds the specific value.by more than 2ns, which is the maximum tolerable difference according to Granjar et al (2008). Additionally, it is still not fully clear whether the current algorithm for the calculation of the DT and the correction of the data is the most appropriate (Redondas et al., 2012).~~ Although ~~there is some documentation for~~ the theoretical description of the dead time effect ~~DT~~ and the ~~for possible~~ methods to determine the ~~the~~ DT and apply corrections~~ing~~ to the data of Brewer spectrophotometers have been adequately documented (Fountoulakis and Bais 2014; Kerr, 2010; Kiedron 2007; Kimlin et al., 2005; Redondas and Rodriguez-Franco 2012; Rodriguez-Franco et al., 2014; Savastiouk 2005; SCI-TEC Instruments Inc., 1999), there is little information regarding the associated uncertainties. Additionally, it is still not clear whether the currently used algorithm in Brewers is the most appropriate (Redondas et al., 2012). ~~and for appropriate methodologies for correcting the measurements.~~ The ~~aim of the~~ present study aims at ~~is to~~ filling this gap ~~in~~ in knowledge and to effectively contribute to the reduction ~~limitation~~ of the uncertainties of the ~~final~~ products derived from Brewer spectrophotometers~~instruments~~.

The objectives of this study have been addressed both experimentally and theoretically. Data from five different Brewers were processed and analysed, specifically, from the double monochromator (type MKIII) Brewers with serial numbers 086 (B086), 157 (B157), 183 (B183) and 185 (B185) and from the single monochromator (type MKII) Brewer with serial number 005 (B005). B005 and B086 operate at the Laboratory of Atmospheric Physics, Aristotle University of- -Thessaloniki, Greece (40.634° N, 22.956° E, 60m a.s.l.). The Brewer ~~instruments~~ spectrophotometers B157, B183 and B185 form the RBCC-E~~RBCC-E~~ triad and are installed at the Izaña Atmospheric Research Center (28.309° N, 16.499° N, 2373m a.s.l.). The same instruments were used in the closure experiments conducted for this study.

2 Dead time: calculation and correction of signal

2.1 The radiation detection system

The Brewer spectrophotometers use a photomultiplier tube (PMT) and a photon counting circuit~~system~~ for the detection and counting of the photons passing through the exit slit of the monochromator. A fraction of the photons that reach the PMT generate photon pulses, according to the quantum efficiency ~~(QE)~~ of the PMT (Haus, 2010), and are recorded as counts. The quantum efficiency ~~QE~~ is a function of wavelength and is taken implicitly into account during the calibration. Low voltage pulses, which are more likely electronic noise and not radiation-induced signal, are filtered out using a voltage discriminator usually set to ~30 mV (Kerr, 2010). Thus, the recorded signal is the sum of counts that have been generated from photon pulses and counts from thermal noise of the electronics that were not filtered out by the discriminator. The latter are usually referred as “dark counts” (or dark signal) and have to be subtracted from the recorded signal. The dark signal is measured by blocking the incoming radiation as part of each sample and is stored on all data records.

~~Each photon pulse has a finite temporal width and if two or more photons arrive within this time interval then they merge into a single pulse which is registered as a single count. This~~ The ~~time interval is known as Dead Time~~ (DT ~~) and is characteristic for each instrument~~ depends on the type and the configuration of the used PMT (Kapusta et al., 2015), thus it is specific for each instrument. ~~(Kerr, 2010).~~ For most Brewers ~~spectrophotometers~~ the DT ~~constant, i.e. the nominal value used for the correction of measurements, ranges~~ is between 15 and 45 ns. The probability of a photon to reach the counting system within the dead time increases with increasing signal ~~The DT effect increases non-linearly as a function of the rate of the incident photons~~ (Kerr, 2010; Kipp & Zonen Inc., 2008; SCI-TEC~~SCI TEC~~ Instruments Inc., 1999); thus the effect of the dead time is more important for higher signals. ~~and the correction of the measurements is complicated.~~ During regular operation, ~~the~~ DT is calculated by measuring and comparing different levels of radiation ~~the irradiance~~ emitted by an internal quartz-halogen 20 Watt lamp (standard lamp). The accuracy of the determined DT ~~values~~ depends strongly on the signal to noise ratio, thus on the level of the lamp’s signal. A weak signal may lead to large uncertainties. Since the operation of the lamp depends on ~~the operation of~~ other electronic circuits in the instrument, it is not always easy to assess ~~determine~~ the effect of ~~how much~~ these factors ~~may~~ on ~~affect~~ the calculated values of ~~the~~ DT. ~~According to the manufacturer (Kipp & Zonen Inc., 2008; SCI-TEC Instruments Inc., 1999), the calculated values of the DT should not deviate from the nominal by more than 2ns. However, during the regular operation of the instruments differences ranging from 2 to 10ns are common (Redondas et al., 2012, Rodriguez et al., 2014). For B086 differences of up to 20 ns were found in the record of the monthly mean DT.~~

During the setup of a Brewer spectrophotometer, the high ~~-~~voltage of the PMT is set to a value where the slope of the intensity vs voltage is small, so~~for which~~ that small shifts in the high voltage do not affect significantly the signal, and the signal to noise ratio is adequately high the dark signal is less than 100 counts when the signal of a measurement is about 10^6 counts. This is translated into a signal to noise ratio of ~ 10000 (Kipp & Zonen Inc., 2008),). The characteristics of the PMT and the counting systemwhich, however, may gradually change with time to lower values. In this case so a proper that re-adjustment of the high voltage is occasionally necessary. Based on data from RBCC-E calibration campaigns (Redondas et al., 2012) we estimated that for most of the participated instruments the signal to noise ratio is above the suggested threshold. For low signal to noise ratiosIf the high voltage is not properly adjusted the response of the instrument is no longer linear, even for low-intensity signals and high uncertainties are induced in both in the calculation of the DT and the correction of the signal.

When the signal is very high (e.g. too highof the order of 10^7 counts·s^{-1}) the detection system is saturated and the measurements , it cannot be easily corrected for the non-linear response of the instrument.(Kapusta et al., 2015; Schätzel, 1986). –Thus, during regular operation, different neutral density (ND) attenuation filters are used to control keep the signal to within appropriate levels. below ~ $1.75\cdot10^6$ counts/sec. When the signal exceeds $4\cdot10^6$ counts/sec the measurements are interrupted to avoid damage of the PMT. The range of the detected signals is different for different types of measurements, thus different ND filters are required. For example, during direct--sun measurements ND filters are used to maintain the signal below ~ $2\cdot10^6$ counts·s^{-1}, and if for any reason the signal exceeds $7\cdot10^6$ counts·s^{-1} the measurements are automatically interrupted. For spectral scans of the global UV irradiance one specific ND filter is used in each instrument depending on its sensitivity. Although this filter keeps the signal below 10^7 counts·s^{-1}, strong signals of 3-$6\cdot10^6$ counts·s^{-1} are not unusual.

Measurements of very low signals have large uncertainties. For a mean rate of photons, N, that reach the detector, individual measurements may differ from each other due to the quantized nature of light and the independence of photon detection (Hasinoff, 2014). Since photon counting is a classic Poisson process, the Poisson (photon) noise of the measurements decreases with increasing sampling time. For N photons measured within a time interval t, the fractional 1σ precision is:

$$\frac{\Delta S}{S} = \frac{1}{\sqrt{Nt}} \qquad (1)$$

As further explained in the following, the sampling time of a measurement is defined by the rotating mask which moves (cycles) before the exit slits of the spectrometer. In each position of the mask photons from only one slit are allowed to reach the PMT, for a time interval of 0.1147 s. Examples of the uncertainty for different signal levels and commonly used sampling times (number of cycles of the mask multiplied by 0.1147 ns) are presented in Table 1. According to Grajnar et al., (2008) the ideal operating range for the Brewer is between one and two million counts·s^{-1}.

At the exit of the monochromator there are six exit slits through which the radiation dispersed by the monochromator is directed to the PMT. When the monochromator is set for ozone observations the nominal wavelengths ($\lambda_{0\rightarrow5}$) corresponding to each slit are 303.2, 306.3, 310.1, 313.5, 316.8 and 320.1 nm respectively. Each exit slit can be opened individually, while the others are blocked, by a rotating mask which is synchronized with the photon counting system. The six wavelengths ($\lambda_{0\rightarrow5}$) correspond to positions 0, 2, 3, 4, 5 and 6 of the mask, respectively. There are two extra positions: 1, when all slits are blocked and is used to determine the dark signal, and 7, when two slits corresponding to λ_2 and λ_4 are opened simultaneously, allowing the radiation of both wavelengths to reach the PMT.

The DT of a Brewer spectrophotometer is determined according to the following procedure: At the exit of the monochromator there are six exit slits through which the radiation dispersed by the monochromator is directed to the PMT. When the monochromator is set for an ozone measurement ("zerooperational" position) (Kipp & Zonen Inc., 2008;) the nominal wavelengths ($\lambda_{0\rightarrow5}$) corresponding to each slit are 303.2, 306.3, 310.1, 313.5, 316.8 and 320.1 nm respectively. Each exit slit can be opened individually, while the others are blocked, using a rotating mask which is synchronized with the photon counting system. The six wavelengths ($\lambda_{0\rightarrow5}$) correspond to the positions 0,2,3,4,5 and 6 of the mask respectively. There is are twoone extra positions (1 and 7) on the mask. When the mask is at position 1 all the slits are blocked; thus, position 1 is used to determine the dark signal. for whichWhen the mask is at position 7 two slits (corresponding to λ_2 and λ_4) are opened simultaneously. In order to determine the DT, tThe radiation emitted by spectral irradiance of the standard lamp at 306.3 and 313.5 nm is measured sequentially by setting the rotating mask at positions 3 and 5 respectively, followed by a simultaneous measurement of ~~at~~ both wavelengths by setting the mask to position 7.

~~This sequence is repeated 10 times (10 cycles) and the DT is calculated by the methodology that is described in the following paragraph. The same procedure is repeated 5 times for high intensity signal and 10 times for low intensity signal, and then the mean value and the standard deviation for each set of measurements is determined. Two filter wheels are interposed between the entrance of the optics and the PMT (Kipp & Zonen Inc., 2008), which will be referred as filter-wheel 1 (FW#1) and filter-wheel 2 (FW#2). Each wheel has six holes spaced at 60 degree intervals. One of the holes in each filter-wheel is empty while filters with different transmittance are placed in each one of the five remaining positions. Each hole can be selected to intersect the optical axis by rotating its filter-wheel. During the DT measurements, a quartz diffuser is selected for FW#1, while for FW#2, an empty aperture is selected for the high intensity measurements and a neutral density (ND) filter of optical thickness 0.5 (~0.316 transmittance) for the low intensity measurements.~~ The sequence is repeated 5 times for a high--intensity signal (using a filter with low -attenuation) and 10 times for a low--intensity signal (using a filter of high –attenuation) and the mean and standard deviation for each set are calculated. Measurements are considered reliable when the standard deviation is less than 2.5 ns for high--intensity and 20 ns for low--intensity signals (Grajnar et al., 2008). When the high voltage of the PMT is properly adjusted the results from the high- and the low--intensity measurements should agree to within two standard deviations of the former. Although the DT used for the correction of measurements should be within 2 ns of the value calculated daily, during the regular operation differences of 2 to 10 ns or even larger (e.g. in B086) are often encountered (Redondas et al., 2012, Rodriguez-Franco et al., 2014). It is not always easy to identify the causes of these differences between the calculated and the used DT or between the DT from the high and the low intensity measurements, and whether the DT in use should be set to a new value. Such differences may arise from problems in the optical, mechanical or electronic parts of the instrument (Grajnar et al., 2008).

2.2 Theoretical approach for determining ~~of~~ the dead-time constant ~~determination~~

~~For a mean rate N of photons that reach a detector, individual measurements may differ from each other due to the quantized nature of light and the independence of photon detections (Hasinoff, 2014). Photon counting is a classic Poisson process and the Poisson (photon) noise~~

~~of the measurements is reduced as the sampling time increases. The fractional 1 sigma precision (ΔS/S) is given by the reciprocal of the square route of the photons measured within the time t:~~

$$\frac{\Delta S}{S} = \frac{1}{\sqrt{Nt}} \qquad (1)$$

~~Due to DT loss of~~Since a portion of the photons are lost due to dead time, the Brewer measurements have no longer Poisson distribution. Thus, Eq. (1) underestimates the ~~1-~~1σ~~sigma~~ precision and should be replaced by the more precise Eq. (2) which takes into account the dead time ~~DT~~ effect (Kiedron, 2007):

$$\frac{\Delta S}{S} = \frac{1}{1-\tau \cdot N_I} \cdot \sqrt{\frac{1}{N_M \cdot t} - \frac{\tau}{t} \cdot \left(2 - \frac{\tau}{t}\right)} \qquad (2)$$

~~W~~where N_I and N_M ~~is~~ are the rate of ~~the incoming and~~photons that generate pulses (in photons·s^{-1}) and the detected ~~photons~~ pulses (in counts·s^{-1}) respectively, t is the sampling ~~total~~ time ~~of measurements~~, and τ is the DT. ~~and N_I is the rate of incoming photons.~~ As long as ~~N_I~~ N_M remains well below ~~~3~~3·10^6 ~~photons~~counts·s^{-1}, the results from Eqs. (1) and (2) agree to within ~~do not differ by more than 2~~2%, while even for count rates close to 6·10^6 the difference is less than 10% (Kiedron, 2007).

The algorithms that ~~which~~ have been developed for the calculation of ~~the dead time~~ DT and ~~for~~ the correction of the signal ~~for its effect~~ are both based on Poisson statistics. According to Schätzel (1986), the average number of ~~photons~~ pulses generated within ~~the dead time~~ τ ~~for a mean rate of N_I pulses per second~~ is given by:

$$\mu = N_I \cdot \tau \qquad (3)$$

For a Poisson distribution the probability P(k) of k pulses within τ is then given by:

$$P(k) = \frac{1}{k!} \cdot e^{-\mu} \cdot \mu^k \qquad (4)$$

The sum of probabilities for all values of k (=0 to infinity) ~~should be~~ equals ~~to~~ unity. ~~; thus t~~The~~he~~ probability of exactly one pulse within τ is ~~given by~~:

$$P(k=1) = \frac{1}{1!} \cdot e^{-\mu} \cdot \mu^1 = e^{-\mu} \qquad (5)$$

while the probability for one or more ~~photons~~ pulses within τ is ~~given by~~:

$$P(k \geq 1) = 1 - P(k = 0) = 1 - e^{-\mu} \qquad (6)$$

Using Eqs. (5) and (6), ~~T~~the ratio of the detected to generated photons pulses ~~pulse rate (N_M) against the overall number of pulses (N_I) using Eqs. (5) and (6)~~ is then:

$$R = \frac{N_M}{N_I} = \frac{P(k=1)}{P(k \geq 1)} = \frac{\mu \cdot e^{-\mu}}{1 - e^{-\mu}} \approx \frac{\mu \cdot e^{-\mu}}{1 - [1 - \mu + \frac{\mu^2}{2} - ...]} \approx e^{-\mu} \qquad (7)$$

By replacing μ from ~~Eq.~~ (3), ~~equation~~ (7) can be written as:

$$R = \frac{N_M}{N_I} = e^{-N_I \cdot \tau} \qquad (8)$$

In the Brewer software, Eq. (8) is applied separately to the count rates for ~~for λ_2 and λ_4 (at~~ slit-mask positions 3, 5 and 7 ~~and 5.) and to count rates for λ_2 and λ_4 simultaneously (slit mask position 7.)~~, by setting $N_I^0 = N_M$ as an initial guess and then by iterating (index j) over the rearranged expression:

$$N_{Ii}^{j+1} = N_{Mi} \cdot e^{N_{Ii}^{j} \cdot \tau^{j}} \qquad (9)$$

For e~~Finally~~ach iteration, ~~,~~ τ^j is determined by:

$$\tau^{j} = \frac{1}{N_{I7}^{j}} \cdot \ln\left(\frac{N_{I7}^{j}}{N_{M7}}\right), \quad \text{with} \quad N_{I7}^{j} = N_{M3}^{j} + N_{M5}^{j} \qquad (10)$$

After ~~9~~ 10 iterations of Eqs. (9) and (10), τ converges to a value that defines DT.

Once DT is determined, ~~and is used for the correction of~~ the signals (count rates) measured by the Brewer ~~ments~~ are corrected for the dead time effect ~~of DT,~~ through:

$$N_I^{j+1} = N_M \cdot e^{N_I^{j} \cdot \tau} \qquad (11)$$

~~Again,~~ After~~after~~ 9 iterations of Eq. (11) the result converges to the corrected ~~value of the~~ signal~~count rate~~ N_I^9.

~~Questions have been raised (Kiedron, 2007) whether the algorithms used for the calculation of the DT and the correction of the signal are the most appropriate and whether the simplifications in the algorithm used for the DT calculation can lead to systematic underestimation of its value and subsequently of the corrected signal. These issues are addressed below.~~

Given the Poisson nature of photon statistics, there are two formulas that are commonly used to calculate the DT (Schätzel, 1986; Yu and Fessler, 2000), which depend on the nature of the counting system. For Brewers, the relevant algorithm for the calculation of the DT is has been based on the assumption that all photons, either recorded or not recorded by the PMT counting system or lost, trigger a new dead time DT period (paralyzable system) and the extended DT formula is used (Eq. (8))is used. If it is we assumed that the dead time DT is triggered only byfrom the photons that are recorded byfrom the PMT counting system (non-paralyzable system) then the following, non-extended, non-extended DT formula applies (Schätzel, 1986; Yu and Fessler, 2000)should be used:

$$R = \frac{1}{1 + \tau \cdot N_I} \qquad (12)$$

Equation (12) is derived from Eq. (8) by assuming a very small value of τ dead time and by replacing the exponential term with its Taylor expansion. Though, it describes more accurately the effect of DT on non-paralyzable systems (Schätzel, 1986; Yu and Fessler, 2000). Subsequently, a new formulaequation corresponding to Eq. (11) can be derived:

$$N_I^{j+1} = N_M \cdot (1 + \tau \cdot \mathrm{N}_I^j) \qquad (13)$$

Although the extended formula is used in the Brewer operating algorithm, it is debatable whether the photon counting system of the Brewer is paralyzable or not. Kiedron (2007) has questioned the appropriateness of this formula It is not clear if the formula used for use in Brewers.the calculation of the DT in Brewers and for the correction of the measured signal is the most appropriate (Kiedron, 2007). Additionally, the simplifications of Eq. (7) and the assumption that $N_{I7}=N_{M3}+N_{M5}$ in Eq. (10) that are assumed applied in the Brewer algorithm for the DT calculation could lead to systematic underestimation of DT of its value and subsequently to underestimation of the corrected signal. These concerns are addressed in the following.

2.3 Experimental evaluation of the ~~DT~~ determination of DT

2.3.1 Extended and non-extended formula~~DT~~

The DT for five ~~different~~ Brewers was calculated using ~~by~~ the two different approaches, ~~(~~expressed by Eqs. (11) and (13)~~)~~, in order to assess the resulting differences. Typical count rates from the high-~~-~~intensity dead-time ~~DT~~ test of the Brewer operating software were used in the calculations. The results are presented in Fig. ~~(~~1a~~)~~. For both cases the calculated DT ~~values were found to~~ converges ~~simultaneously~~ after ~~9~~ 10 iterations ~~(Fig. (1a))~~, while the differences in ~~between~~ the final ~~derived~~ DT ~~values~~ are negligible. Specifically, ~~when~~ the DT derived from the non-extended ~~DT~~ formula (Eq. (13)) ~~is used the calculated DT~~ is smaller by less than 0.5 ns ~~lower~~ than ~~for~~ the DT from the extended ~~DT~~ formula (Eq. (11)).

In order to estimate the differences in~~between~~ the final products for a paralyzable and a non-paralyzable system, signals ~~count rates~~ from 0 to $7\cdot10^{6}$~~.5~~ counts$\cdot s^{-1}$~~/sec~~ were assumed and corrected for the dead time effect using both formulas for DT ~~nominal~~ values ranging from 15 to 45 ns (Fig~~s~~. ~~(~~1b~~) and (1c~~)). It is noteworthy that the corrected signal was found to converge after 4-~~-or~~ 5 iterations, for both methodologies. This implies that it might not be necessary to use 9 iterations in the Brewer software for the correction of the signal.

~~We notice that in all cases the results are already converging after 4 or 5 iterations, simultaneously for both methodologies. This implies that it might not be necessary to perform 9 iterations for the correction of the signal.~~ For signals ~~count rates~~ below ~~lower than~~ ~$2\cdot10^{6}$ counts$\cdot s^{-1}$ ~~/sec~~ the differences between the corrected signals ~~values~~ with the two methods are ~~lower~~ less than 0.~~1~~5%. For higher signals ~~count rates~~ the differences become more important; though, as long as the signal is below ~~between 10^{6} and~~ ~$3\cdot10^{6}$~~.5~~ ~~(~3.2 million)~~ counts$\cdot s^{-1}$~~/s, the differences become more important~~the differences are still less than 1.5%. Thus, even if the Brewer counting system is non-paralyzable, the currently used algorithm does not induce important errors for the usual range of signals in direct-sun measurements (between 0 and $2\cdot10^{6}$ counts$\cdot s^{-1}$). For signals higher than ~$3\cdot10^{6}$ counts$\cdot s^{-1}$, which are common for global UV irradiance measurements, and for DT greater than 30 ns the corrected signal may be significantly overestimated. ~~For DT values below 30ns the differences remain below 1% for the entire range of count rates, while for DT of 45ns, the differences exceed 1% only for count rates higher than $10^{6.4}$ (~2.5 million) counts/s.~~

2.3.2 Artificial biases

In order to determine the conditions under which the standard Brewer algorithm does not induce artificial biases in the results the following procedure was followed: Theoretical values ~~o~~for the measured count rates ~~count rates~~ N_M were estimated from Eq. (8) assuming ~~for~~ different rates of ~~incoming~~ photon pulses ~~rates~~ N_I and ~~for~~ different reference DT values and ~~by using Eq. (8). Then~~ the DT was recalculated from ~~Eqs.~~ (9~~)~~ ~~(~~) and (1~~1~~0). As long as the ratio of signals ~~between the count rates~~ at positions 3 (or 5) and 7 of the slit mask, N3/N7 (or N5/N7), remains between 0.25 and 0.5 and the ~~true~~ signal ~~count rate~~ at position 7 (N7) remains below 10^7 ~~counts/s~~counts·s^{-1} ~~(the maximum measured signal is usually below $3 \cdot 10^6$ counts/s)~~, the calculated and the reference DT coincide.

When the internal standard lamp is used to calculate DT, the ratio N3/N7 is usually ~0.4 and 10 iterations of Eqs. (9) and (10) are enough to provide an accurate result. However, as it will be discussed later, if a different radiation source (e.g. the Sun) is used to derive DT then the ratio N3/N7 might be much smaller. As shown in Fig. 2, when this ratio is less than ~0.25, more iterations are needed to achieve an accurate estimate of DT; otherwise DT is underestimated. For N3/N7 above 0.05, at least 50 iterations are required to derive an estimate close to the reference DT, while for N3/N7 above 0.01 the required number of iterations increases to 300. The results shown in Fig. 2 were found independent of the signal at position 7 for signal levels between 10^2 and 10^7 counts·s^{-1}.

~~On the other hand, as deduced from Fig. (2), the calculated DT is lower than the “real” DT when the ratio N3/N7 is below ~0.25 for all reference DTs. This result remains valid also for pulse rates different than 10^6 counts/s.~~

2.3.3 Dark signal

~~The thermal noise of the electronics is responsible for the dark signal which is recorded even when no radiation reaches the PMT. Thus i~~In the Brewer algorithm, prior to the dead time ~~dead time~~DT correction, the dark signal is subtracted from the measured signal (Kerr, 2010). However, Kiedron (2007) suggested that before subtracting the dark signal both the measured and the dark signals should first be corrected for the dead time effect. In the same study it was suggested that even though the dark pulses have no Poisson distribution, ~~using Eq. (12) for the~~ the correction of both the dark and the measured signals through Eq. (12) should lead to more accurate signals ~~correction~~ than without applying dead-time correction to the ~~if the~~ dark signal ~~is not corrected for the DT effect~~.

To assess the importance of this suggestion, an attempt was made to ~~In the following we attempt to~~ quantify the differences arising in the final signals. ~~results between the two approaches concerning the correction of the dark signal for the DT effect. To achieve that,~~ ~~d~~Different levels of measured signals~~count rates~~, ranging from 0 to 7·$10^{6.5}$ ~~counts/s~~counts·s^{-1}, were assumed, as well as dark signals, ~~were assumed. On these count rates different dark signals were added,~~ ranging from 0 to 10^5 ~~counts/s~~counts·s^{-1}, which were added to the former.~~.~~ T~~hen t~~he derived signals ~~count rates~~ were corrected for the dead time effect and the dark signal using both methods (operational in Brewers~~s~~ and suggested by Kiedron, (2007)) and the resulting corrected signals were compared. ~~For low dark signals (<10^4 00 counts/sec)~~ ~~no~~ The differences ~~could be detected~~are smaller than 0.2%~~.~~ for dark signals below 10^4 counts·s^{-1}~~/sec~~. Considering that the dark signal in Brewer measurements ~~These are becoming more important as the assumed signal, the dark signal, and the dead time are increasing. However, as long as the dark signal is below 10^4 counts/s, the difference between the results from the two methods is lower than 0.2%, even for a dead time of 60 ns. Since~~ during normal operation ~~of a Brewer the dark signal~~ is generally well below ~~lower than~~ this level, the correction of the dark signal for the effect of dead time ~~DT effect~~ would not have important impact on the final results. For exceptional cases when the dark signal exceeds this limit, ~~T~~the difference increases fast, ~~when the dark signal approaches 10^5 counts/sec,~~ but stays below ~1~~.6~~% even for a dark signal of 10^5 counts·s^{-1} and for ~~count rates of $10^{6.5}$ counts/s and~~ DT ~~dead time~~ of ~~60~~ 45 ns.

2.3.4 Simplifications in the algorithm

In order to assess the effect of ~~detect if the calculated DT is underestimated due to~~ the simplifications in Eq. (7) or due to other issues ~~if the algorithm is not proper for reasons~~ that have not been taken into account, the following experiment has been made:~~below described method has been developed.~~

Spectral ~~M~~measurements of the radiation ~~spectral irradiance~~ emitted by 3 different sources (the ~~s~~Sun, an external 1000 W~~att~~ DXW lamp and the internal ~~50~~ 20 W standard lamp) were performed in steps of 5 nm for the operational spectral range of the Brewers that were used~~-~~. ~~spectrophotometers using d~~Different levels of the signal were achieved using the internal ND filters~~ (different positions of FW#2)~~, different distances (for the external lamp), or different solar zenith angles (for the Sun).~~ and different levels of intensities. In order to achieve different levels of irradiance when the Sun is used as a radiation source, the measurements were performed for several solar zenith angles.~~ Measurements of the~~the~~ 1000 W~~att~~ lamp ~~intensity~~ (~~DXW lamp with~~ serial number 1005) were performed at the Izaña Atmospheric Research Center for different distances ~~(~~ranging from 40 cm to 115 cm, measured~~)~~ between the lamp and the center of the quartz window of the Brewer. ~~-~~The lamp mount could move vertically on a metal rod of 1 m length. When an external lamp is positioned at such short distances, the geometry of the radiation entering the fore-optics of the Brewer is very different from the geometry of the ~~s~~Sun's rays. Additionally, for different distances the radiation does not necessarily originate from the same area of the lamp's filament (Kazadzis et al., 2005). However, for the specific experiment these factors are not important because measurements at ~~for~~ different positions of the lamp are not compared to each other. What is important is that the spectrum of the emitted radiation does not change during measurements for each specific position of the lamp. This was ensured by monitoring continuously ~~T~~the intensity and the voltage of the lamp~~ were continuously monitored in order to ensure that the lamp irradiance was stable during the measurements.~~.

~~Then t~~The relative attenuation between ~~between the~~ different ND filters ~~positions of FW#2~~ was~~is~~ calculated (Sellitto et al., 2006; Redondas et al. 2011) for the standard lamp, ~~and~~ for different distances of the external lamp and for different angles of the ~~s~~Sun.

~~The~~ All measurements ~~d spectral irradiances from all the different light sources~~ were corrected for the dead time ~~DT~~ using several values of the DT ranging from zero to about twice the used DT ~~constant~~ in steps of 0.1 ns. Then, spectral ratios of the signals ~~ratios~~ (relative attenuation) for ~~between~~ all pairs of ~~the different~~ ND filters ~~positions of FW#2~~ were calculated.~~ for each wavelength. The transmittance of the ND filters is known to be independent of intensity.~~ Assuming that the response of each instrument is non-linear (intensity dependent) exclusively due to dead-time effect~~DT~~, correction of the signal with the proper DT ~~value~~ (and method) should eliminate the non-linearity. For all wavelengths, the optimal ~~DT~~ correction should lead to ~~signal~~ ratios ~~of pairs of FW#2 positions~~ that are independent of the intensity of the incident radiation. This also suggests that correcting the~~using an improper DT~~ ~~for correcting~~ measurements used to derive the relative ~~for the determination of the~~ attenuation of the ND filters with a wrong DT might lead to significant

~~important~~ errors. For these measurements, it is important ~~critical~~ that the high voltage of the PMT is optimal and that the separation between signal and noise works properly, otherwise the results may be misleading. An example for one pair of ND filters and one wavelength is shown for B185 in Fig. ~~(~~3~~)~~. From Fig. ~~(~~3a~~)~~, the optimum DT for which the calculated attenuation is independent of the measured signal ~~count rate~~ is found at 29.6 ns~~,~~ while for different values of DT the derived relative attenuation depends on the level of the signal.

~~while lower and higher DT values result in remarkable differences.~~

The above described procedure was repeated for all wavelengths and for all possible combinations of filters. ~~Irradiance values~~Measurements for which the ~~noise to signal ratio~~precision, according to ~~Eq.~~ (1), is lower than 2% ~~is very high~~ were not used in the analysis, as well as measurements with signals (before applying the dead time correction) above $5\cdot10^{6}$ counts$\cdot s^{-1}$. Additionally, some outliers resulting from spikes (Meinander et al., 2003) were rejected by visual inspection. The mean DT and the corresponding standard deviation ~~are~~ were then calculated ~~from the remaining values, as~~and are shown in Fig. ~~(~~3b~~)~~.

For B185, the DT that yields the optimum correction ~~DT~~ is very close to ~~both~~ the ~~nominal~~ DT ~~value~~ in use and the mean DT calculated regularly from the standard lamp measurements. The standard deviation is nearly 2 ns.

The same test was performed using ~~for~~ B086, operating at Thessaloniki. In this case moving the 1000 W~~att~~ lamp vertically was impossible; thus the lamp was fixed at ~~to~~ a standard distance of about 40 cm from the center of the quartz window and different intensities were achieved by adjusting the current of the lamp ~~current~~. ~~For B086 t~~The test was performed for two periods with different calculated mean DT. In both cases the results were within ~1 ns from the mean DT calculated with the standard procedure, and the standard deviation was again of the order of 2 ns. The test is more uncertain when applied on single-monochromator Brewers, mainly due to the stray-light effect (Karppinen et al., (2014) and references therein).

If the counting systems of B086 or B185 were non-paralyzable the corrected signal would be significantly overestimated for signals above $\sim3\cdot10^{6}$ counts$\cdot s^{-1}$ and would lead to overestimation of the ratios. Thus the estimated DT from the ND filters that provides the optimal correction would be lower than the DT calculated from the standard lamp. The fact that this is not happening is a strong indication that the photon counting systems of B086 and

B185 are paralyzable, so -the correction of the measurements using the extended formula is accurate. The results ~~discussed above~~also reveal that the algorithm currently used is reliable and provides an accurate estimation of the DT~~, as long as the count rates at positions 3 and 5 of the slit mask do not differ significantly~~. ~~However, as it is analytically explained in the following paragraphs, operational or technical issues of the instrument may affect the determination of the DT, leading to important errors in the measured signals, and consequently, in the derived final products.~~

2.4 Determination of DT from solar measurements

Using the standard lamp as a radiation source for the determination of the DT may occasionally lead to uncertain and noisy results, especially when the signal of the lamp (thus the ~~signal to noise ratio~~accuracy of the measurements) is weak~~low~~. In ~~S~~such cases~~results~~, in addition to ~~inducing~~ errors induced in the ~~proper~~ correction of the measured signals, it is ~~also make~~ difficult to ~~the~~ detect~~ion of~~ possible problems (of mechanical or electronic origin) that may affect the determination of the DT. The operation of the lamp is not independent of the operation of the other ~~rest~~ electronic circuits of the instrument. Thus, it is not always easy to detect if the observed changes in DT are real. The sun is a more reliable and stable (under specific conditions) source compared to the standard lamp; thus using the solar measurements for the calculation of the DT would eliminate a great part of the uncertainties. Problems may arise when the sun is partially or fully covered by clouds, resulting to rapidly changing or very low intensity, respectively, and increased uncertainties in the determination of DT–. Thus, this method is unsuitable for locations with long periods of cloudiness. Other factors that may increase the uncertainty of the derived DT are changes in intensity of direct solar radiation due fast changes in the SZA early in the morning or late in the evening and in the concentration of various absorbing or scattering atmospheric constituents.

New routines for the determination of the DT from direct~~-~~sun measurements were developed ~~created~~ and tested on Brewers 005, 086, 157, 183, and 185 for ~~during~~ a period of about 10 months.

The methodology ~~used for the DT determination from direct sun measurements~~ is very similar to that used with the standard lamp (~~described in~~ Sect. 2.1), but the number of iterations has increased from 10 to 50, to avoid underestimation of the calculated DT due to small values of the ratio N3/N7. Concerning ~~The main differences are in~~ the measurement procedure, ~~:~~ the zenith prism is directed ~~points~~ towards the S~~s~~un ~~instead to the internal lamp~~, ~~and~~ appropriate ND filters are used ~~in order~~ to avoid ~~PMT~~ overexposure of the PMT, and ~~.~~ the DT is calculated only for one signal level, instead of 2 ~~s~~ (high and low intensity) that are used with the standard lamp. The implementation of the specific routine aims mainly at reducing the uncertainty in the DT calculation, as -complementary to the standard algorithm that uses the standard lamp. Measurements at two different signal levels are not applicable in this case, since the DT is calculated for a wide range of intensities due to the large temporal variability of solar radiation. Usually 10 cycles of the slit mask were used for each DT measurement. For a certain period the routine was run in B185 with 40 cycles in order to increase the accuracy in the determination of the DT.

~~Different number of cycles (different signal integration times), ranging from 10 to 40 (integration time of ~1 to ~4.5s), was used in different instruments during different periods.~~ At Thessaloniki, five consecutive measurements were performed each time and then the mean DT~~dead time~~ and the standard deviation were derived. The gratings of B086 were moved to a position where the ratio N3/N7 remains ~~ratio remained within the acceptable limits~~ between about ~~~~ 0.3 and 0.5~~, as discussed previously~~. At Izaña, the mean DT~~dead time~~ and the standard deviation were derived from four consecutive measurements, with the gratings set at the ozone measurement position.~~-~~ ~~The main problem when using the sun as radiation source is the possibility of being partially or fully covered by clouds, resulting to rapidly changing or very low irradiance, respectively. In these cases, the uncertainty of the calculated DT is extremely high. Thus, i~~In this analysis ~~we rejected~~ all measurements with standard deviation higher than 1.5 ns and with signal ~~count rates~~ at position 7 ~~of the slit mask~~ below 10^5 ~~counts/s~~counts·s^{-1} -were rejected. To avoid very low signal levels at positions 3 and 5, only measurements for N3/N7 ratios between 0.15 and 0.85 were used. In Fig. ~~(~~4~~)~~, the DT derived for three of the five Brewers investigated ~~studied are~~is presented as a function of day of the year (DOY).

For B086, the DT derived from the standard lamp is much noisier than from the sun during the first months of the year. This is due to the very low intensity of the standard lamp used in that period. In April (DOY 94) the standard lamp was replaced with one of higher intensity, which resulted in substantial reduction of the noise in the estimated DT.~~ Accordingly, the noise in DT results was reduced.~~ Further improvement in the DT results can be observed after DOY 142, when the number of cycles was increased from 10 to 20. During the

~~analyzed~~analysed period, the DT derived ~~as calculated~~ from direct-sun measurements ~~of solar radiation~~ is very stable and less noisy than the DT from the standard lamp (from both ~~the~~ high- and ~~the~~ low-~~-~~intensity measurements). Prior to August 2014 (DOY 220) the direct-~~-~~sun based ~~measurements for the~~ determination of the DT was~~ere~~ performed only once per day near the local noon (SZAs ranging from ~ 63° in December to ~ 17° in June) in order to achieve ~~have very~~ stable and ~~solar irradiance with~~ high-~~-~~intensity signal~~ies~~. Although the noise was~~is~~ very low during that~~is~~ period, there are too few measurements available. Since the beginning of August, several measurements were performed each~~per~~ day at different SZAs~~solar zenith~~ ~~angles~~ between ~75° and the local noon; thus the amount of available data has increased, but also the ~~level of the~~ noise. The response of B086 is ~~a very~~ low~~insensitive instrument~~; therefore ~~any~~ reduction in ~~the level of~~ intensity is reflected immediately on the estimated DT. The DT derived during the period of study is about 38–39 ns, 3–4 ns lower than the used DT, and is independent of the radiation source.

For B157, the agreement between the DT from the standard lamp and the ~~sun~~ Sun is very good. Some outliers in DT derived from the direct-sun measurements are due to ~~the inclusion~~ data of low intensity recorded at large SZAs~~solar zenith angles when the intensity was low~~. As for B086, the DT derived for B157 from both the standard lamp and the sun is 4–5 ns lower than the DT of 32 ns used in regular operation. ~~It should be noted that in this case, as well as in the case of B086, the calculated DT (from both the internal standard lamp and the sun) is lower than the nominal.~~ Considering that B157 is ~~a~~ one of the standard Brewer triad instruments of AEMET, ~~well maintained instrument,~~ the DT used for the signal correction should be reduced by 4–~~-~~5 ns~~lower than the used DT constant of 32ns~~, at least for the specific ~~presented~~ period. The most possible reason for the difference between the calculated and the used DT is the gradual change of the characteristics of the photon counting system.

For B185, the second triad Brewer, the ~~DT from the sun is lower and noisier compared to the DT from the standard lamp. The main reason is the low ratio of the count rates between positions 3 and 7 of the slit mask when the DT is calculated from direct sun measurements. The ratio ranges between 0.05 and 0.25 for the majority of the direct sun measurements, while it remains within 0.4 and 0.5 when the irradiance of the standard lamp is measured~~results are similar with B157. For the first part of 2014 (before DOY 190), the mean measured DT is lower than the used DT ~~constant used~~ during this period. In this day the operationally used DT ~~constant~~ was changed from 33 to 29 ns, after ensuring that no realignment of the optics and no resetting of the PMT were needed, following the suggestions of ~~Kimlin~~ Grajnar et al., (~~2005~~2008). The mean DT from the sun and the standard lamp are in good agreement during the entire period of measurements. After DOY 190 the spread in the DT from the direct-sun measurements is smaller compared to the previous period (and compared to the high intensity DT from the standard lamp) as a result of the increase in the number of cycles from 10 to 40. The conclusions from the analysis of the DT for B086, B157 and B185 are valid also for B005 and B183; thus their results are not presented.

Rodriguez-Franco et al (2014) suggested that the calculated ~~dead time~~DT is not necessarily the one which provides the optimal signal correction and further investigation is needed. The present study showed that the procedure used for the determination of the DT provides accurate results as long as the measurements are performed under appropriate conditions (as already discussed in s~~S~~ections~~.~~ 2.1–2.3 and is further discussed in ~~Sect.~~Sect. 2.5). However, even if the correct DT ~~of the PMT~~ is known and used, there are other factors that might lead to non-linear responses of the photon detection system which might be falsely perceived as improper DT correction.

2.5 Factors affecting the determination of DT

In order to determine the optimum instrumental settings for the calculation of the DT, continuous direct-sun measurements were performed ~~during two consecutive very clear days~~ at Izaña with B185 during two consecutive cloud-free days with nearly zero aerosol optical depth. Every ~~A~~about ~~every~~ 40 min, five consecutive DT measurements were performed using each time different grating settings, corresponding to different wavelengths at ~~so that each time the irradiance passing through~~ the two exit slits~~ was of different wavelength~~. The five wavelengths corresponding to position 3 of the slit mask are~~were~~ 306.3, 317, 331.5, 345 and 354.5 nm, while for position 5 the five wavelengths are ~~were higher by~~ about 7 nm longer. This way, measurements for different intensities, wavelengths, and N3/N7 ratios were performed for very similar SZAs and atmospheric conditions. During the first day, 40 cycles were used for the first set of wavelengths (306.3 nm at ~~for~~ position 3) and 10 cycles for the other four sets. During the second day, the number of cycles was changed to 10 and 5 respectively.

Due to the different combinations of wavelengths ~~measurements~~ the recorded N3/N7 ratio ranges from 0.05 to 0.5. The DT derived from measurements with N3/N7 ratios between 0.~~3~~

15 and 0.5 is very close to the used DT constant (29ns). For the same value the optimum DT correction was achieved, as discussed in ~~Sect.~~Sect. 2.3. For ratios lower than 0.15 the spread of the derived DT is very large and its mean values are smaller than the used DT, -even after 10000 iterations of Eqs. (9) and (10), possibly due to the increased noise in the lower intensity measurement (at position 3 or 5). ~~As expected, for ratios lower than 0.3 the DT is underestimated.~~ The intensity of ~~irradiance~~ radiation ~~level~~ does not affect the ~~mean~~ calculated DT,~~;~~ but is important for the uncertainty of the measurements. The calculated standard deviation decreases with increasing signal~~count rates~~. For signal ~~count rates (~~at position 7~~)~~ between 500,000 and 1,000,000 ~~counts/s~~counts·s^{-1} -the standard deviation of DT is smaller than ~~~~~5% (~2ns) ~~of the calculated DT, as long as the N3/N7 ratio remains within the acceptable limits of 0.3 – 0.5 and~~ when 10 or more cycles are used in the measurements. For signals ~~count rates~~ higher than 10^6 ~~counts/s~~counts·s^{-1} -the standard deviation is below ~~smaller than~~ 3% (~1ns) ~~of the calculated DT~~ and decreases even more for higher signal~~count rates~~s. Larger ~~Increasing the~~ number of cycles leads to smaller ~~also decreases the~~ standard deviation and therefore reduced ~~the~~ uncertainty in the determination of the DT. When the number of cycles increases from 5 to 10 the standard deviation decreases by a factor of 2. The same fractional decrease in the standard deviation is found also when the number of cycles increases from 10 to 40. It should be noted ~~mentioned~~ that no wavelength dependence was detected in the determination of the DT.~~ The same occurs for the temperature effects.~~ Finally~~In order to look for possible dependencies from temperature~~, calculation of ~~finally,~~ the DT using the standard lamp ~~was calculated~~ for different temperatures within a specific day ~~by using measurements with the standard lamp and~~revealed no changes ~~was detected~~ for temperatures ranging from 17 to 35°C.

3 Effects of DT on the u~~U~~ncertainties of the final products

In the following, an attempt is made to quantify the main uncertainties in the calculation of UV irradiance, TOC and AOD due to ~~the uncertainties~~ errors in the estimation of the DT. Effects in the calculation of the total columns of SO_2 and NO_2 are not discussed, because uncertainties from other sources are much higher, due to the usually small column amounts (the order of a few DU) of these species (Fioletov et al., 1998; Wenig et al., 2008). ~~Dead time e~~Errors in DT are also expected to affect the results of different diagnostic tests in the Brewer, such as the measured intensity of the internal lamps and the determination of the transmittance ~~attenuation~~ of the ND filters, which ~~and~~ in turn may affect the accuracy of the final products. Although i~~I~~t is difficult to quantify these uncertainties~~; however~~, they are believed to be of less importance compared to those discussed below.

3.1 UV irradiance

The spectral irradiance~~s~~ measured by the Brewer generally ranges between 10^{-6} and 1 Wa~~tt~~·m^{-}~~1~~^{2}, and is calculated by multiplying the corrected for the effect of DT signal ~~count rates~~ N_I with a proper calibration function~~actor~~. Thus, uncertainties in N_I due to inaccurate DT correction of the raw signal N_M are directly transferred to the final product. The effect of a specific ~~DT~~ error~~s~~ in DT on ~~the calculated~~ UV irradiance depends on the measured signal N_M and the actual value of the DT, and ~~mainly on the intensity of the incident radiation~~can be estimated by Eq. (11). Fig. 5 shows the effect on irradiance caused by deviations in the used DT~~,~~ in the range ±2ns - ±10ns~~,~~ from ~~four~~ three characteristic reference values~~,~~ as a function of ~~the intensity~~ N_M ~~(photons/s) of the incident radiation~~. The effect of an error in DT was investigated for signals in the range 0 - 7·10^{6} counts·s^{-1}. For direct--sun measurements that are used for the retrieval of ~~to calculate~~ TOC and AOD the signal is usually kept below ~1.75·10^{6} counts·s^{-1} (dashed line in Fig. 5) using ND filters. As long as the ~~intensity count rate~~ signal remains below ~~10^{6}~~ that level~~photons/s~~, even a large change of 10ns in ~~the~~ DT leads to a corresponding change in the calculated irradiance of up to about ~~1~~2%. For higher intensities the effect increases ~~rapidly~~fast, so that for signals ~~intensities~~ near 5·10^{6}~~.5~~ ~~(~3.2 million photons/s)~~ counts·s^{-1} a change in ~~the~~ DT of only 2ns –a level that is commonly ~~usually~~ encountered in Brewers– causes ~~1~~ ~2% change in irradiance. Larger deviations, however, result in larger errors in irradiance that cannot be neglected. For example, a 10ns change in ~~the~~ DT leads to differences in ~~the calculated~~ irradiance ~~ranging~~ from ~~about 3~~5% to ~~5~~12%, depending on the actual value of ~~the~~ DT.

Given that for a properly maintained instrument the DT used for the correction of the measurements does not differ by more than ±2 ns from the calculated DT, we can estimate the fractional 1σ uncertainty in the measured UV irradiance based on the work of Bernhard and Seckmeyer (1999) and the results presented in Fig. (5):

$$u = \frac{E(-2ns) + E(+2ns)}{2 \cdot \sqrt{3}} \qquad (14)$$

where E(-2ns) and E(+2ns) are the errors in UV irradiance due to corresponding errors of -2 and +2 ns in the used DT respectively. For DT values between 15 and 45 ns, the 1σ uncertainties are 0.12 – 0.13%, 0.25 – 0.28% and 0.69 – 1.13% for signals of 1, 2 and 5 million counts·s^{-1} respectively. For a sampling time of ~-2.3 s (20 cycles), which is commonly used in direct--sun measurements to derive TOC and AOD, the combined uncertainty due to photon noise and DT errors is less than ~0.2%, as long as the measured signal is between -10^{5} and ~1.75·10^{6} counts·s^{-1}. For a shorter sampling time, ~0.23 s (2 cycles), commonly used in spectral UV scans, the same uncertainty of less than ~0.2% occurs for signals between ~-10^{6} and 1.75·10^{6} counts·s^{-1}. Finally, for sampling times between ~0.1 and 4.5 s (corresponding to 1— 40 cycles) the signal with the minimum uncertainty lies between 0.5 and 1.5 million counts·s^{-1}. Below and above the specific range, the uncertainties are dominated by photon noise and DT, respectively.

In order to ~~get~~ quantify ~~tative estimates of~~ the errors ~~that may be introduced~~ in ~~the~~ global spectral irradiance measurements due to uncertainties in the determination of the DT, data from Brewers ~~instruments~~ operating in Thessaloniki and Izaña were processed using different values of the DT. For ~~instruments with low sensitivity, such as~~ B086, the recorded signal for global UV irradiance measurements~~)~~ barely exceeds 2·10^{6} counts·s^{-1}, even at very small~~low~~ SZAs. Thus, a ~~large~~ change ~~in the DT~~ of 10 ns in ~~the~~ DT, relative to the ~~nominal~~ value in use ~~of~~ (42 ns), leads to a change in the noon ~~global~~ spectral irradiance of less than 2%~~,~~ ~~even~~ at UV-A wavelengths (strong radiation) during a ~~very clear (~~cloud-free -and ~~,~~low--aerosol day near the summer solstice (~17° SZA~~solar zenith angle~~ at Thessaloniki). At SZAs larger than 60° the maximum measured signal, is usually less than 10^{6} counts·s^{-1} and the uncertainties due to DT errors are negligible. However, at short wavelengths (e.g. $\lambda<305$ nm) the signal is usually of the order of 10^{4} counts·s^{-1} or lower, so the 1-σ uncertainty of the measurements solely due to the photon noise is 2% or higher. ~~The same~~A much smaller change of 2 ns in the DT for ~~an instrument with high sensitivity, such as~~ B185 (~~with a~~ DT in use ~~constant of~~ 29 ns) for which the recorded signal may exceed 6·10^{6} counts·s^{-1}, is enough to cause ~~leads to 4~~ a 2% change in noon irradiance ~~for local noon at Izana~~ (~6° SZA at Izaña~~solar zenith angle~~). ~~, and about 2.5% change in the daily integral of the irradiance at 350 nm. For smaller, and more usual, changes in the DT of 2ns, the corresponding change in irradiance at local noon is less than 1% while for the daily integral the change is negligible. Finally, when no correction for the DT is applied, the global irradiance is underestimated by up to 9%.~~ Due to the different atmospheric conditions at Izaña (compared to Thessaloniki) and the higher responsivity of

B185 (compared to B086), under cloud-free skies the signal of B185 at around 305 nm is usually higher than 10^4 counts$\cdot s^{-1}$ for SZAs smaller than 70°, and the 1σ uncertainties due to photon noise are less than ~2%. For wavelengths in the UV-B region, the effect of the DT is negligible since the radiation is much weaker for both instruments.

3.2 Total ozone column

The retrieval of TOC with a Brewer spectrophotometer is based on the analysis of near-simultaneous direct-sun spectral irradiance measurements at four wavelengths (Kerr et al., 1981). Five sets of measurements are performed within about 2 minutes and the mean TOC and the corresponding standard deviation are calculated. Before each set of measurements, the intensity of the irradiance is tested and an appropriate ND filter is used to keep the maximum recorded signal between ~-0.5$\cdot 10^6$ and 1.75$\cdot 10^6$ counts$\cdot s^{-1}$.~~is inserted in the radiation path to avoid overexposure of the PMT.~~ For the retrieval of TOC ~~from direct sun measurements it is also necessary to know the extraterrestrial~~the so-called extra-terrestrial constant (ETC) is required (Kerr et al., 1981). The ETC can be either calculated ~~by~~ using the Langley extrapolation method (Thomason et al., 1983) or transferred from a standard instrument through side-by-side comparison of TOC ~~ozone~~ measurements (Fioletov et al., 2005).

Because the correction for the DT applies to measurements of irradiance and its effect depends on the level of irradiance, the effect on ~~the retrieval of~~ TOC depends basically on the differences in the signal ~~count rates~~ at ~~different slits~~positions 3 – 6 of the slit mask (wavelengths 310.1, 313.5, 316.8 and 320.1nm). Such differences are caused by atmospheric influences on the solar spectrum (e.g., from ozone absorption, Rayleigh scattering, and SZA) and by the shape of the spectral response of the instrument. The latter may significantly differ between instruments, particularly for Brewers of different type. For example, the presence of the UG11-NiSO4 filters combination in single-monochromator Brewers changes significantly the shape of the spectral response, compared to double-monochromator Brewers, leading to different correlation between the levels of irradiance measured at the four slits.

Although the shape of the spectral response differs between instruments which are equipped with different ~~electronics~~ PMTs (e.g. for B086 and B185) these differences are ~~were~~ not ~~found to be~~ as important as between single- and double-monochromator Brewers. In the following, the effect of the DT correction on the determination of the ETC and the retrieval of TOC ~~from direct-sun measurements~~ are discussed for the single-monochromator B005 and the double-monochromator B185. The same analysis for the MKIII Brewers 157 and 183, not shown here, yielded similar results to those for B185.

3.2.1 ETC from Langley plots

~~Usually, in order t~~To derive the ETC from Langley plots, continuous measurements of direct-sun~~the~~ irradiance at ~~for the~~ wavelengths used for the calculation of TOC are performed during half days (morning to noon or noon to evening) with stable atmospheric conditions (clear sk~~y~~ies, stable TOC, low and stable AOD). Then the ratio of the logarithms of signals used for the calculation of TOC~~ (Kerr et al., 1981)~~ is derived and plotted against the air~~-~~-mass (secant of the SZA for SZAs greater than about 75°). The ETC is ~~equal to~~ the intercept of the resulting linear fit. Errors in the determination of ~~the~~ DT may in~~tro~~duce errors in the calculation of the ETC. ~~Although the irradiance levels increase with decreasing SZA,~~ Although ~~the use of the~~ ND filters are used to protect ~~prevents~~ the PMT from exposure ~~from exposure~~ to very high intensities ~~for~~ which are mostly affected by ~~the~~ dead time~~role of DT is critical~~, errors in~~. However, the effect of the~~ DT are still ~~errors remains~~ important when the signal is near the ~~its~~ high~~-~~-intensity threshold. Langley plots for about 10 days were derived from measurements with the MKIII Brewers 157, 183, and 185 in Izaña and the MKII Brewer ~~B~~005 in Thessaloniki. Although the atmospheric conditions at Thessaloniki are not usually favourable for application of the ~~the determination of the ETC with the~~ Langley method, a few days with relatively stable atmospheric conditions were found in ~~within~~ one year's record of measurements which were used indicatively for the purposes of this study. For the MKIII Brewers, the change in the derived ETC for a 2 ns change in ~~the~~ DT is typically less~~ower~~ than 3 units, rising to ~~up to~~ ~15 ~~units~~ for a 10 ns change~~ in the DT~~. The corresponding changes ~~in the ETC~~ for the MKII Brewer are 8 and 40 units respectively. Such errors in the determination of the ETC influence directly the calculated TOC. The ~~reasons for the~~ differences between the two types of Brewers are mainly caused by differences in the shape of their spectral response. ~~results for the two instruments are discussed in the following section.~~

~~In Fig. (6), changes in the calculated TOC due to changes in the ETC resulting from typical errors in the DT are presented. The error in TOC increases smoothly with decreasing ozone slant column. For B185, the change in TOC due to a 2ns change in the DT is generally less than 0.5%, rising to about 1.5% for a 10ns change in the DT for slant ozone columns lower than 500 DU. For B005, the change in TOC for a 2ns change in the DT is up to 1% for small ozone slant columns, increasing to ~4.5% for 10ns change in the DT.~~

3.2.2 Effect of DT on TOC fromon direct-–sun measurements used in TOC retrieval

In Fig. 6, changes in TOC due to changes in the ETC resulting from typical errors in the DT are presented. The error in TOC increases smoothly with decreasing ozone slant column. For B185, the change in TOC due to a 2 ns change in DT is generally less than 0.5%, rising to about 1.5% for a 10 ns change in DT, for slant ozone columns below 500 DU, while for B005 the corresponding changes are 1% and 4.5% respectively.

The effect of DT on TOC derived from direct-sun measurements during 20 days in June 2013 at Thessaloniki (B005) and Izaña (B185) has been investigated, by applying different offsets to the nominal value of the DT that is used to correct the measured irradiances (Fig. 7). For this analysis, the ETC has been kept constant, irrespective of the used DT. The effect of different offsets in DT on the calculated TOC is presented in Fig. (7) as function of the ozone slant column recorded at each station.

For all cases, the maximum changes in TOC occur become greatest just before (/after) a new ND filter of higher (/lower) optical density is set. At this point the change in intensity is large rises and the dead timeDT effect on the measured signal increases. This indicates that the effect on the calculated TOC becomes stronger for higher intensities of the direct solar irradiance. Additionally, the changes in TOC increases as the ozone slant column decreases, due to stronger intensityies of the incoming radiation and to changes in the distribution of radiation on different slits. In accordance with the results shown in Fig. 6of the sensitivity analysis presented in Sect. 3.2.1, for small changes in the DT (±2 ns) the effect on TOC derived from B185 is small, generally, below 0.5%, and for B005 up to ~1.5%. For larger changes in the DT (± 10ns) the effect on TOC is no more negligible for B185 and much stronger for B005, occasionally reaching 5%. The stronger effect of DT on TOC derived from single-monochromator Brewers was also confirmed by Redondas et al. (2011) and Rodriguez-Franco et al. (2014).

As already mentioned, the different effects of changes in the DT on TOC measurements (as well as on the determination of the ETC) between single- and double-monochromator Brewers is mainly caused by the different shape of their spectral response. The spectral

~~response determines the balance of the radiation levels at the four slits, which, in turn, affects calculated DT.~~

~~In old versions of the Brewer algorithm, there is an additional issue related to the effect of the DT on the measured signals when a ND filter is set. Before starting a direct-sun measurement, an automatic intensity check takes place in order to determine which ND filter should be used for the safe operation of the PMT. For this intensity check the signal at 320.1 nm (position 6) is measured.~~ In old versions of the Brewer operating software, the selection of the ND filter to be used in a direct-sun measurement is done through an automatic intensity check of the level of the signal at position 6 (320.1 nm). For double-monochromator Brewers, the signal at the other wavelengths (positions 3~~—~~5) is significantly weaker. Due to the shape of their spectral response, in~~lower than at 320.1 nm (position 6), due to the shape of the spectral response. Thus, only the signal at position 6 is actually affected by the DT when it reaches the threshold for setting a denser filter. This is not the case for~~ single-monochromator Brewers and f~~, which have different spectral responses. F~~or small ozone slant columns the signal at positions 4 and 5~~ (313.5 and 316.8 nm)~~ is higher compared to ~~than at~~ position 6 ~~320.1 nm~~ and occasionally higher than the threshold used to set a higher density filter. ~~.~~In such cases, the high-intensity signals are more susceptible to ~~the signals at these positions are greatly affected by the DT. As discussed in Sect. 3.1,~~ errors in DT, leading to errors ~~may induce important errors in the correction of high intensity signals, and consequently to~~in the derived TOC~~ values~~. As the ozone slant column increases the intensity at positions 4 and 5 ~~316.8 nm and at 313.5 nm~~ decreases faster and gradually becomes smaller ~~lower~~ than at position 6~~320.1 nm~~. Although the specific problem has been ~~is~~ solved in ~~the~~ more recent versions of the Brewer operating software~~algorithm~~, it remains important for past datasets or for instruments still operating with an ~~for cases when an~~ old version of the software~~algorithm is still in use~~.

~~3.2.2~~3.2.3 Combined effect of DT on ETC and TOC

In this section ~~In order to investigate~~ the combined effect of errors in DT ~~errors~~ on both the ETC derived by the Langley method and the direct-sun measurements used in the retrieval of ~~the~~ TOC is investigated.~~ measurements, an analysis similar with the previous section is followed.~~ Specifically, the dead time ~~DT~~ effects on the ETCs that were estimated for B005 and B185 in ~~Sect.~~Sect. 3.2.1 were applied to the ETC that is used in reprocessing the direct-sun measurements.

From Figs. (6), (77), and (8) it appears that the effect of falsely calculated ETC due to errors in DT in the calculation of the ETC lead to changes in TOC of opposite sign compared to those caused by the correction of the signal with wrong DT.changes on TOC due to DT errors. The first effect of DT errors on the ETC is dominant for large ozone slant columns, while the second effect on the calculation of TOC is dominant for small ozone slant columns. Specifically, for large ozone slant columns the results are similar with those of Fig. (6), while for small ozone slant columns the large changes in TOC shown in Fig. (7) are suppressed since the two effects are balanced. Even in this case, a 10 ns change in DT leads to 3% change in the calculated TOC for B005.

3.2.33.2.4 Transfer of the ETC calibration from a reference instrument

The ETC is usually transferred from a reference to the Brewer being calibrated, instrument. To achieve that, the two collocated instruments collect using a series of simultaneous TOC measurements. Possible DT errors in DT in in either reference instrument or the instrument being calibrated may affect the calculation of the ETC.. Even if the reference instrument is a well maintained and calibrated MKIII Brewer for which the DT error is negligible, it is difficult to quantify the effects of DT errors on the ETC solely from the calibrated instrument. There are two different methods for transferring the ETC from the reference to the calibrated instrument (Redondas and Rodriguez-Franco, 2012): 1) the "one-point calibration", where only the ETC for the calibrated instrument is calculated and 2) the "two-point calibration", where the differential ozone absorption coefficient is calculated at the same time with the ETC coefficient (Kerr et al., 1981). The effect of possible DT errors in DT depends on the method.

As shown in Fig. (7), the DT errors in DT affect the TOC measurements significantly when the intensity of the signal is high and/or the ozone slant column is smalllow. The difference in TOC due to the use of an incorrect DT value cannot be eliminated simply by replacing changing the ETC that has been derived from the incorrect DT. As it appears from Figs. (7) and Fig. (8), although a change in the ETC may partially or fully counteract the TOC errors for smalllow ozone slant columns and high intensities, it leads to larger higher deviations from the reference TOC for large high ozone slant columns and/or low intensities. If the two-point calibration is used, the differences observed in Fig. (7) can be balanced by a combined change of the ETC and the differential absorption coefficient used for the calculations. This way, the change of the ETC would suppress the effect of the DT error for low ozone slant columns, while the change of the differential absorption coefficient would counteract the differences in TOC for large ~~lower~~ slant columns~~paths due to the change of the ETC~~. It is obvious that the use of an incorrect DT leads to different ETCs between the one-point and the two-point calibrations. The DT effect when transferring the ETC from a reference instrument cannot be easily quantified for none of the two methods. However it is not expected to be more important than the impact of the same DT error on the ETC calculation with the Langley method.

3.3 Aerosol optical depth

Estimates of the AOD can be also derived from Brewer spectrophotometers using direct-sun spectral measurements (Meleti and Cappellani, 2000; Kazadzis et al., 2007). As the error in AOD is equal to the natural logarithm of the ratio between the erroneous and the correct signal, divided by~~with~~ the air mass,~~. We estimated that~~ changes in the measured irradiance of 1% and 5% lead to changes of opposite sign in the absolute levels of the derived AOD of about 0.01 and 0.05 respectively for air~~-~~mass close to unity. As can be seen from Fig. ~~(~~4~~)~~, for very high intensities errors of this level may arise from ~~can be induced for very high intensities by~~ changes in ~~the~~ DT of 2 ns and 10 ns, respectively.~~ The estimated errors in AOD are inversely proportional to air -mass.~~ Considering that the overall absolute uncertainties in the calculation of AOD range between 0.05 and 0.07 (Kazadzis et al., 2007), only ~~the effect of~~ large DT errors, of the order of 10 ns, have ~~is~~ important effects, even if the AOD has been derived for small air~~-~~mass using high intensity measurements.

4 Evaluation of the dead time for past datasets: Methods and difficulties

As already mentioned, in a Brewer's history there might be periods when the calculated DT may differ from the one in use ~~nominal~~ by more than 2 ns. Interventions on the instrument, ~~most of these cases,~~ such as repairing ~~problems in~~ the electronics, resetting the high voltage, or re-aligning the optics may ~~could~~ result in suppression of the differences between the calculated ~~DT~~ and used DT ~~constant~~ (Grajnar et al., 2008; Kimlin et al., 2005). However, during regular operation it is not always easy to ~~decide~~ assess whether the derived DT is the actual ~~real~~ and whether ~~if~~ its application would improve the quality of the measurements. In addition, unusual day-to-day variations of the calculated DT or indications of temperature or intensity dependence complicate further this assessment~~decision~~. For such cases, only analysis of TOC measurements before and after an ND filter~~s~~ is set, or comparison with TOC derived from co-located instruments or from satellites, can reveal whether the ~~Brewer~~ measurements are properly corrected for non-linearity effects~~ or not~~. Spectral UV irradiance is more sensitive to changes in ~~of the~~ atmospheric constituents ~~parameters~~ and ~~the~~ SZA; thus it is more difficult to get the same information by comparing datasets of spectral UV irradiance.

For example, in June ~~of~~ 2007 the preamplifier board of the PMT of B005 was replaced. Before the replacement the mean measured DT was ~23 ns while the used DT ~~constant~~ was 34 ns. After the repair ~~placement~~ the measured DT agreed ~~coincided~~ very well with the DT ~~constant~~in use. In order to assess whether the mean ~~measured~~ DT measured during ~~for~~ the two different periods provides the optimal signal correction, the TOC record was recalculated from intensities~~, then~~ corrected with the mean ~~measured~~ DT and ~~finally~~ compared with satellite data. The comparison was made for two periods: one month before and one month after the change of the preamplifier board. Data from the NASA EOS-Aura satellite, which carries the Ozone Monitoring Instrument (OMI) were used. The specific satellite passes over Thessaloniki, where B005 is located, daily close to local noon. For the comparison only clear-sky measurements of TOC for air~~-~~-mass below 1.15 were used. The ratio of the TOC derived from the Brewer using two different ~~for~~ DT corrections (~~equal to~~ 23 and 34 ns respectively) and the OMI-TO3 (Bhartia et al., 2002) ~~i~~was plotted as a function of the measured intensity ~~(from B005)~~ at 320.1 nm. If the Brewer measurements were~~are~~ properly corrected for non-linearity the ratio would ~~should~~ be independent of intensity. The ratios for the two periods, normalized with the mean over each period to remove absolute biases, are shown in Fig. ~~(~~9~~)~~.

For the first period, the ratio derived for the DT ~~constant~~ in use shows a clear dependence on intensity (Fig. ~~(~~9c~~)~~)~~,~~ which is practically removed when the measured DT ~~i~~was used (Fig. ~~(~~9a~~)~~). For the second period, the DT ~~constant~~ in use (which now coincides with the measured DT) results in very small dependence on~~from~~ ~~the~~ intensity (Fig. ~~(~~9d~~)~~), whereas when ~~if~~ the mean DT of the first period is ~~were~~ used the ~~ratio would~~ dependence is strong~~ly on intensity~~ (Fig. ~~(~~9b~~)~~).

In a similar study the DT for B070 ~~rewer with serial number 070~~ was found ~10 ns below the DT ~~constant~~in use, but when it was applied to the data the agreement with the TOC of the reference B183 became worse (Rodriguez-Franco et al., 2014). It must be clarified in this point that if the TOC ratio of a Brewer ~~between~~ and a reference instrument (~~the~~ ground-based or ~~and the~~ satellite borne) ~~TOC (or between two different ground based instruments)~~ is independent of the intensity of the signal, this does not necessarily mean that the used DT is the actual real DT of its the PMTphoton counting system. The dead time DT correction may also compensate for instrumental malfunctions or settings that lead to real or artificial non-linear behaviour of the instrument, as . fFor example, the combination of errors in the ETC and the differential absorption coefficient. might be "translated" in a DT that is different from the calculated, when the TOC from a Brewer is compared with the TOC from a satellite or another ground-based instrument. Thus the comparisons with the TOC from other instruments provides an indication only of whether there are any remaining non-linearity issues after the correction for the dead timeDT effect. Since non-linearity in the measurements of TOC may not be exclusively due to dead-timeDT, the DT that provides the optimal correction is not necessarily the actual real DT of the systemPMT. Therefore, Iit is safer to check the validity of DT with ND filters, as described in Sect. 2.3.

5 Conclusions

In this study, we assess the effects of dead time DT on different products that are delivered by Brewer spectrophotometers, such as, spectral UV irradiance, TOC and AOD. Moreover we assess the effectiveness of different methodologies to determine accurately the DT and the applied corrections to the measured radiation signals. The analysis of data from closure experiments and long--term measurements provides reliable estimates of the uncertainties associated with corrections applied for the dead time DT effects and reveals the importance for accurate determination of the DT.

From a or the theoretical point of view, the application of either the extended or the non-extended approaches on Brewer measurements provide similar estimates of the DT. However, differences are revealed when the two approaches are applied for the correction of the signals. For signals with count rates higher than ~2.5x10^{6} counts/scounts·s^{-1} the non-extended approach results in more than 1% lower signals compared to those derived from the extended approach for the same value of the DT. As the signal count rate is decreasesing these differences are gradually eliminated. There are strong indications that the photon counting system of the Brewer is paralyzable and the currently used extended theory for the calculation of DT and the correction of the measurements provides accurate results.

In the current Brewer algorithm, nine iterations of Eq. (12) are performed for the correction of the measured signals. Here wWe have found that the corrected signal converges already after

5 iterations, independently of intensity and the value of DT, for both the extended and the non-extended approaches. However, there is no reason to suggest reducing ~~e~~ the number of iterations operationally since the time saved from the extra iterations is imperceptible.

The correction of the dark signal for the dead time ~~DT~~ effect was found unnecessary, as long as the level of the dark signal remains below 10^4 ~~counts/s~~counts·s^{-1}.

Further evaluation of the current algorithm for the determination of ~~the~~ DT indicates that 10 iterations of Eqs. (9) and (10) are enough to give accurate~~the~~ results, ~~are accurate~~ as long as the signals at slit mask- positions ~~s~~ 3 and 5 are~~is~~ of similar level (i.e. within a factor of 2); otherwise the ~~. If the ratio between the count rates is outside these limits, then the DT constant is underestimated~~ number of iterations has to be increased. Fifty iterations were found ~~to be~~ enough to provide accurate results for signal ratios (N3/N5) between ~0.05 and 20. Increasing the signal and the number of cycles reduces the noise and the uncertainty of the final products. Specifically, as long as the signal level remains above 10^6 ~~counts/s~~counts·s^{-1}, measurements with 10 cycles are sufficient to keep the uncertainty of the calculated DT below 3% (~1 ns).

Measurements of the direct solar irradiance (which is usually stronger than ~~the radiation of~~ the Brewer's internal standard lamp) provide more accurate estimates of ~~the~~ DT with lower uncertainty. In order to achieve that, ~~the~~ measurements should be performed at wavelength settings~~s~~ resulting in ~~with~~ intensity ratio (N3/N7) ~~ranging~~ between 0.~~3~~ 15 and 0.~~7~~85 and~~,~~ ~~and~~ signal ~~level (~~at position 7~~)~~ above 10^6 ~~counts/s~~counts·s^{-1}, while the number of iterations of ~~Eqs.~~ (9) and (10) has to be increased to 50. Since at some locations or seasons direct-~~-~~sun measurements might not be achievable for long periods~~time~~, this method for estimating the DT ~~these~~ should be used only complementarily to the standard-~~—~~lamp-based method~~determination of the DT~~. Occasionally, the standard-lamp-based method ~~DT~~ can lead to ~~be~~ very noisy results so that the derived DT ~~values~~ might not be the most suitable for the correction of the signals. In such cases, and if direct-sun-based estimates of the DT are not available, the DT can be determined by optimizing the spectral transmittance of ND filters derived from measurements that are corrected with different DT values.

~~The DT that provides the optimal signal correction has been estimated by performing measurements of the irradiance from the sun and external lamps using different ND filters.~~ An independent check of the DT that provides the optimum correction to the measured signals has been ~~was also~~ achieved from short-term comparisons of the derived TOC with data from satellites. The specific methodology can be used alternatively or complementarily to the currently used methodologies~~. or from co-located stable instruments.~~ However, assessing the accuracy of DT by comparison with data from other instruments~~this method~~ might not be ~~very~~ safe because other parameters may interfere.~~.~~ Errors in parameters that are used to derive TOC (e.g. ETC, differential absorption coefficient) might lead to artificial non-linearity ~~in the final products~~ which is subsequently balanced by the use of an incorrect DT ~~when the data are compared against data from reference instruments.~~. Analysing TOC when ND filters change (Rodriguez-Franco et al., 2014) or irradiances as described in Sect. 2.3.4 can lead to safer conclusions.

Errors in ~~Considering the correction of the~~ UV irradiance spectral measurements are less than 2% ~~,~~ even for ~~an error of~~ 10 ns error in ~~the~~ DT ~~does not induce errors greater than ~1.52% on the calculated irradiance~~, as long as the signal ~~count rate~~ remains below $2 \cdot 10^6$ ~~counts/s~~counts$\cdot$s^{-1}. However, ~~T~~the ~~maximum~~ signal ~~count rate for global or direct sun UV scans does not usually~~may be as high as ~~exceed be of the order of 3 – 3.5x~~6 – 7 million ~~10^6 counts/s~~counts$\cdot$s^{-1}. As the incident irradiance is getting closer to this limit the errors are becoming more important. For such high signals~~count rates~~, a 2 ns error in ~~the~~ DT results into ~~an error of ~1~~2 – 4% error in ~~the~~ irradiance, ~~which~~ rising~~es~~ to ~~~5~~10% for 10 ns error ~~in the DT~~. For the calculation of TOC, the uncertainties related to dead time effect ~~the DT~~ are highly dependent on the shape of the instrument's spectral response; thus on the type of the instrument. For ~~the~~ double-monochromator Brewers, the error in TOC does not exceed 2%, even for 10 ns error in ~~the~~ DT, while for single-monochromator Brewers the error may increase ~~escalate~~ to ~~~~~5%. The tolerance of 2 ns suggested by ~~the manufacturer for the DT error (Kipp & Zonen Inc., 2008; SCI-TEC Instruments Inc., 1999)~~Grajnar et al. (2008) has a negligible effect ~~impact~~ on TOC for double-monochromator Brewers, and up to 1% for single-monochromator Brewers. Thus, according to Eq. (14), the 1-σ uncertainty in TOC from single--monochromator Brewers, solely due to errors in DT is ~0.6%. As the target for the total uncertainty in TOC measurements is 1% (Kerr et al., 1985), it is obvious that the suggested ~~this~~ tolerance for ~~the~~ DT has to be lowered. The effect of DT errors in the calculation of AOD is found to be ~~of~~ less important~~ce~~ compared to errors in UV irradiance and TOC.

Based on the results of this study we can summarize the following recommendations~~suggestions~~:

- The determination ~~For the calculation~~ of ~~the dead time~~DT from direct-sun measurements ~~of the sun, these~~ should be used as ~~performed~~ complementary to the standard method with the internal standard lamp. Measurements for ~~for wavelengths and SZAs that ensure comparable~~ signals at the ~~two~~ slit-mask positions ~~s (~~3 and 5~~)~~ that differ by more than an order of magnitude should not be used to derive DT.~~,~~ To achieve uncertainty below ~1 ns in the determination of DT, it is recommended that 10 or more cycles are used with ~~and for~~ the signals at positions~~slit~~ 7 ~~that remain~~ above 10^6 ~~counts/s~~counts·s^{-1}.~~.~~ The number of iterations of Eqs. (9) and (10) in the processing algorithm should be increased to 50 when the ratio N3/N7 is less than ~0.3.

~~For the correction of the signal the nine iterations of Eq. (12) can be reduced to five without affecting the quality of the Brewer products. This will reduce the time required for several operational routines.~~

- Regarding the TOC measurements from single-monochromator Brewers, the tolerance of 2 ns in the DT error should be reduced ~~changed~~ to 1 ns. Additionally, before a ND filter is set, the intensity at slit-mask positions 5 and 6 (~~for both the 320.1 and the~~ 316.8 and 320.1 nm) should be checked in order to keep the maximum signal at all slits below the PMT safety ~~defined~~ threshold.

- Lowering the intensity threshold for both the single- and the double-monochromator Brewers is not recommended. Although it would ~~lead to smaller~~reduce the uncertainties in TOC and AOD due to DT errors~~.~~, it would also reduce the accuracy of the measurements, especially at slit-mask positions 2 and 3.

- In ~~During~~ global spectral irradiance measurements the signal may reach ~~levels (~~$\sim$~~3.5x~~6·10^6 ~~counts/s~~counts·s^{-1}~~)~~ where the effect ~~impact~~ of ~~the DT~~ errors in DT ~~is~~ becomes~~ing~~ very important. However, using different ~~a~~ ND filters ~~in order~~ to reduce ~~limit~~ this ~~e~~ effect ~~impact of the DT errors~~ might result in ~~to~~ increased uncertainties due to errors in the determination of the ND filters' transmittance (Redondas et al., 2011). Using a standard ND filter to reduce the responsivity of Brewers that measure such high signals would also reduce the accuracy of the ~~for~~ measurements at shorter~~lower~~ wavelengths. However, by using two different ND filters, ~~the~~ one that is currently used for short~~lower~~ wavelengths and one of stronger attenuation for longer wavelengths, the signal can be kept within the desired levels for the entire operational spectral range. The attenuation of the two ND filters can be implicitly taken into account during calibration. Furthermore, keeping the uncertainties in the calculation of DT below 1 ns and applying an appropriate –post-correction to the measurements using the optimal DT can also reduce errors to less than 2%.

This study has been accomplished in the framework of COST 1207 which aims at~~o~~ establishing a coherent network of European Brewer Spectrophotometer monitoring stations and, among other~~s~~, to harmonize operations and achieve consistency in quality control and quality assurance. The results and ~~the~~ suggestions of the present study will hopefully contribute to improve the quality of the Brewer products. Given that some Brewers are in operation since the early 1980's, more accurate ~~DT~~ correction for the dead time effect would lead to more accurate detection of trends in ozone, global UV irradiance and other products, and to more reliable data that can be used for the validation of satellite products, and other ~~for several~~ applications in physical (Erickson III et al., 2015) and health (Lucas et al., 2015) sciences.

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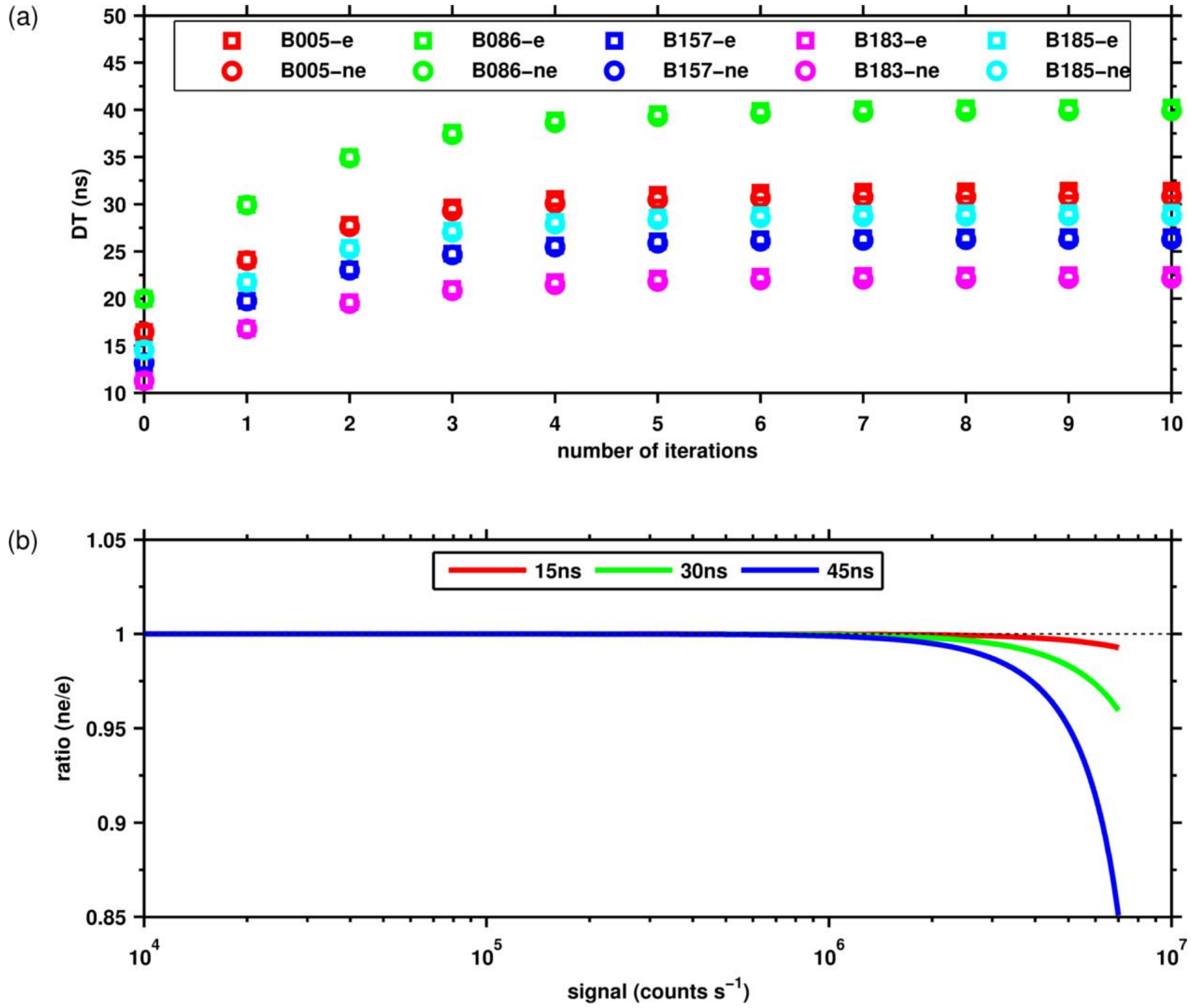

Figure 1. (a) DT derived with the Eextended (e) and the non-extended (ne) approach DT for five Brewers with DT constants ranging from 19 to 42 ns as a function of the number of iterations. (b) Corrected counts/sec for different number of iterations and different DT. (cb) Ratio between signals the corrected using the non-extended and the non-extended approach DT as a function of the logarithm of the measured, uncorrected for the dead time DT, signal (in counts·s^{-1}), for 3 different values of DT rate.

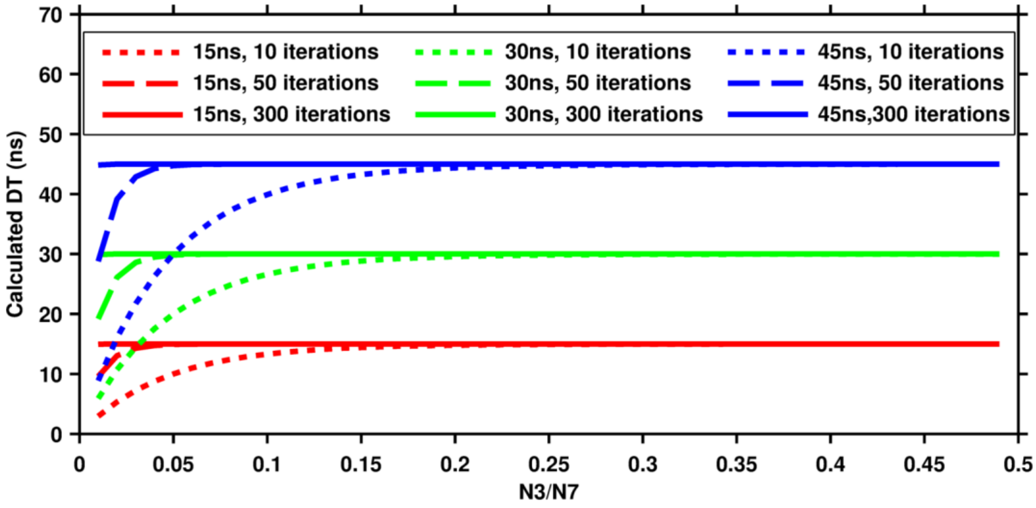

Figure 2. DT as derived by it is calculated with the standard Brewer Brewer algorithmsoftware as a function of the ratio of signals at slit-mask, positions 3 and 7 (for different N3/N7) ratios and for 4 3 different reference DT values (15, 30 and 45 ns) using 10, 50 and 280 iterations.

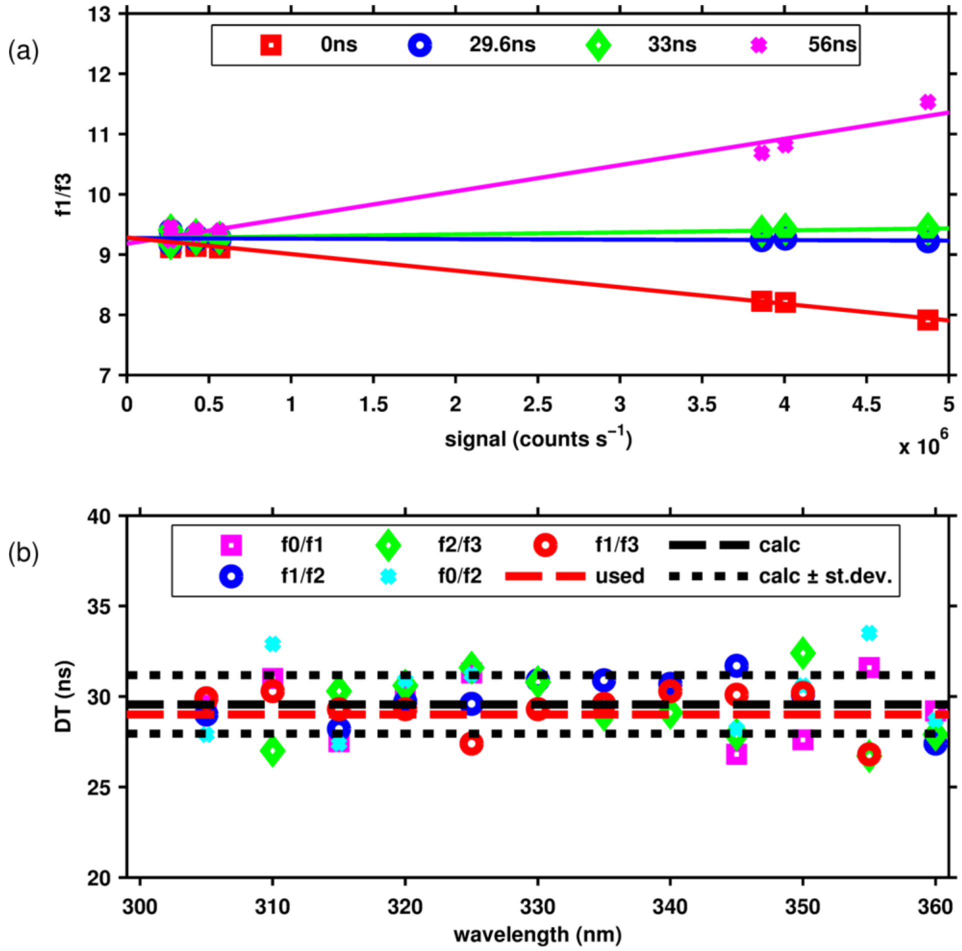

Figure 3. (a) Ratio of signals at 345 nm measured with ND filters 1 and 3 (optical densities 0.5 and 1.5) and corrected with four different values of DT as a function of the signal measured with ND filter 1.~~Relative attenuation between positions 0-~~1~~ and 1-~~3~~ of FW#2 for irradiance signals at .~~ (b) The optimum calculated DT ~~value~~ for different wavelengths and different relative attenuations (pairs of ND filters). The derived mean values and the used DT constant are also shown. All the results are for B185.

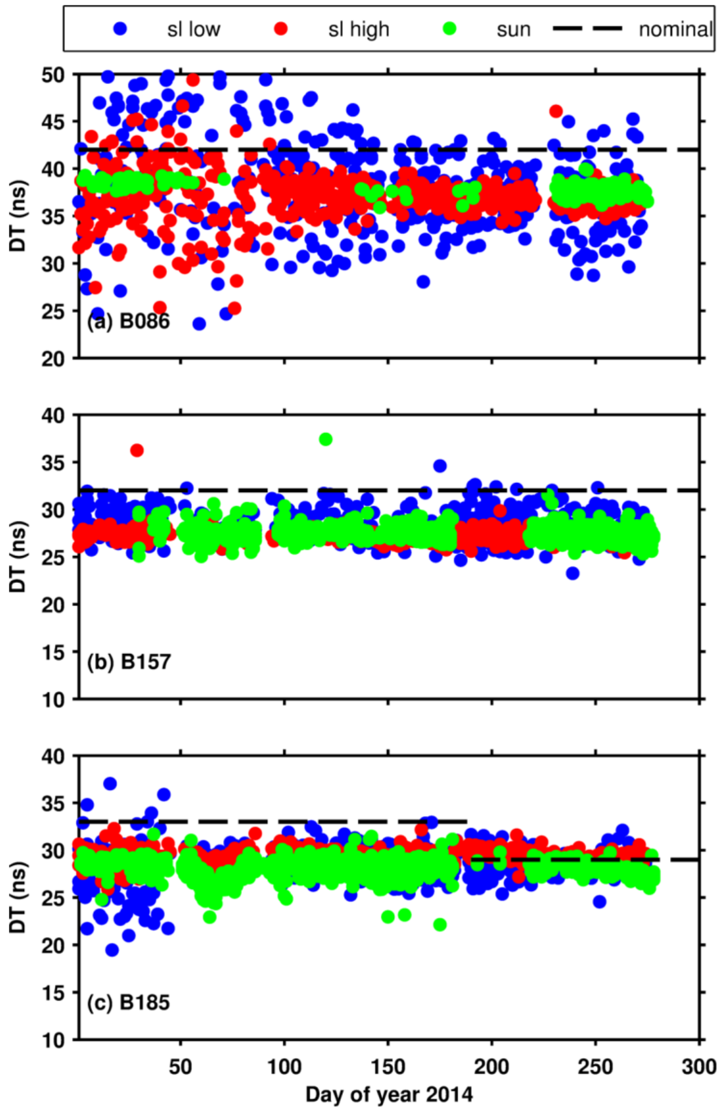

Figure 4. DT calculated from measurements of the standard lamp (high and low intensity) and the sun as a function of day of year 2014 for three Brewers (a) B086, (b) B157, and (c) B185. ~~The results are for 2014 and are presented as a function of DOY.~~ Dashed lines represent the DT constant used by the instruments in each period.

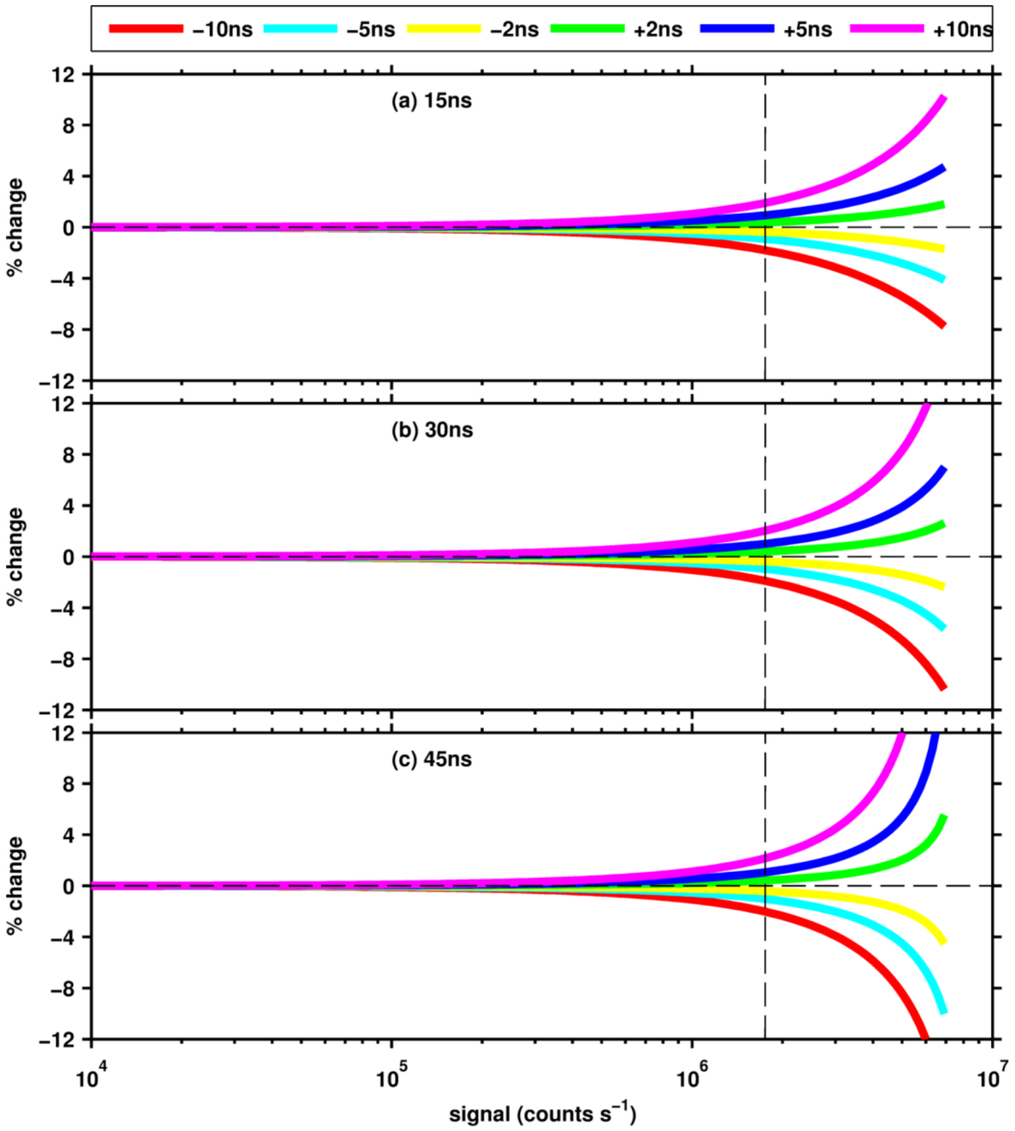

Figure 5. Changes in UV irradiance as a function of ~~intensity~~ the measured signal due to errors in the determination of ~~the~~ DT, for different values of the reference DT: (a) 15ns, (b) 30ns, and (c) 45ns~~, and (d) 60ns~~. The vertical dashed line marks the cut--off limit of ~$1.75 \cdot 10^6$ counts$\cdot s^{-1}$~~,~~ used for direct--sun measurements.

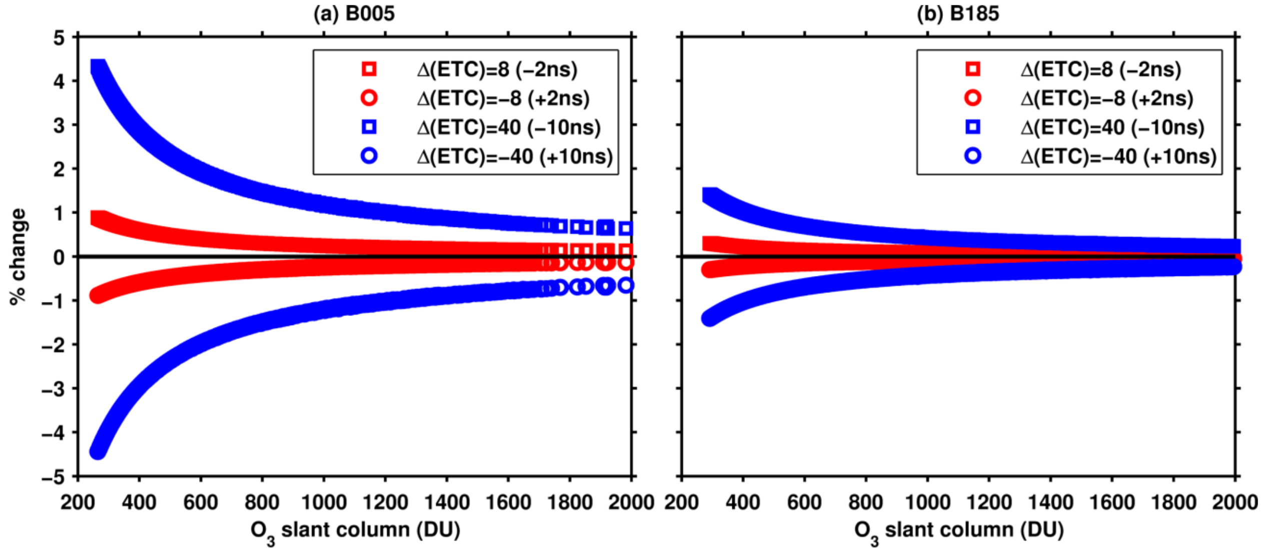

Figure 6. Changes (%) in the calculated TOC ~~as a consequence of~~ due to changes in the ETC ~~change~~ resulting from ~~due to~~ ±2 ns and ±10 ns change in ~~the~~ DT, as a function of the slant column of ozone for ~~. Results are presented for~~ B005 (a) and B185 (b). For B005 the used ETC has been changed by ±8 units for a ±2 ns change of the DT and by ±40 units for a ±10 ns change of the DT. For B185, the corresponding changes of the ETC are ±3 units and ±15 units.

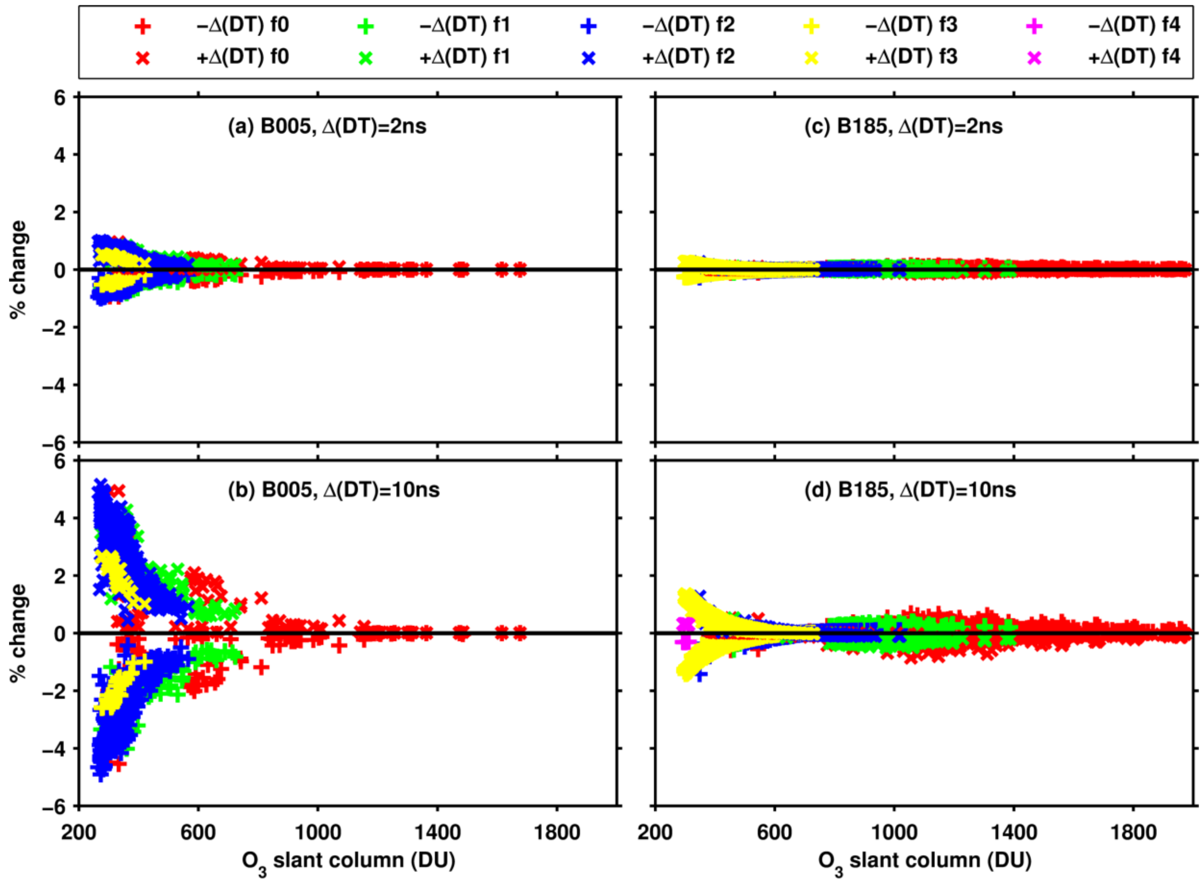

Figure 7. Changes (%) in TOC derived ~~calculated~~ from direct-sun measurements due to offsetting the DT by ±2 ns (a, c) and ±10 ns (b, d) ~~changes in the DT~~, as a function of ozone slant column, for B005 (a, b) and B185 (c, d). Different colors refer to data measured without (red) and with neutral density filters of optical density 0.5 (green), 1 (blue), 1.5 (yellow) and 2 (magenta). The reference DT is 34 ns for B005 and 29 ns for B185.

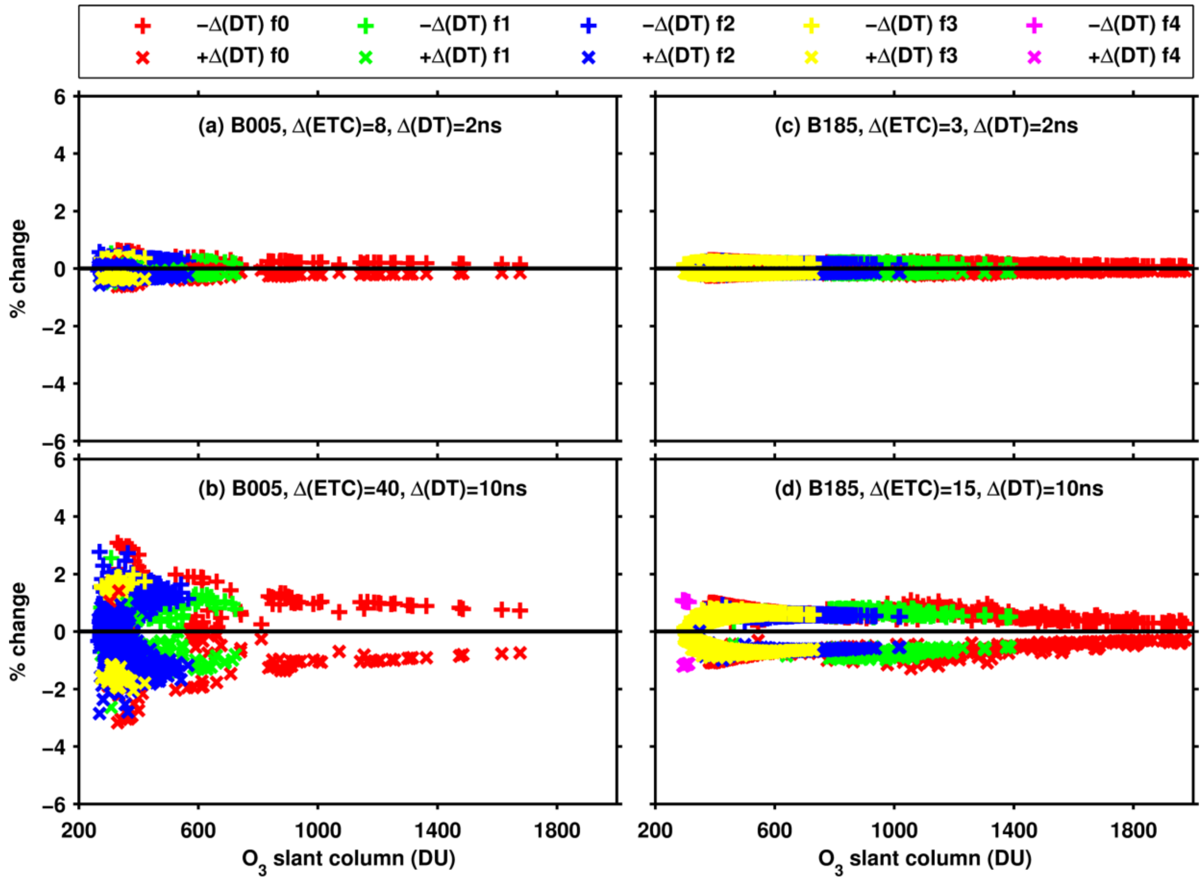

Figure 8. Changes (%) in TOC calculated from direct-sun measurements due to ±2ns (a, c) and ±10ns (b, d) changes in the DT, as a function of ozone slant column, for B005 (a, b) and B185 (c, d). For each change of the DT, the ETC used for the calculations is subjected to the changes described in ~~Sect.~~Sect. 3.2.1. Different colors refer to data measured without (red) and with neutral density filters of optical density 0.5 (green), 1 (blue), 1.5 (yellow) and 2 (magenta). The reference DT is 34 ns for B005 and 29 ns for B185.

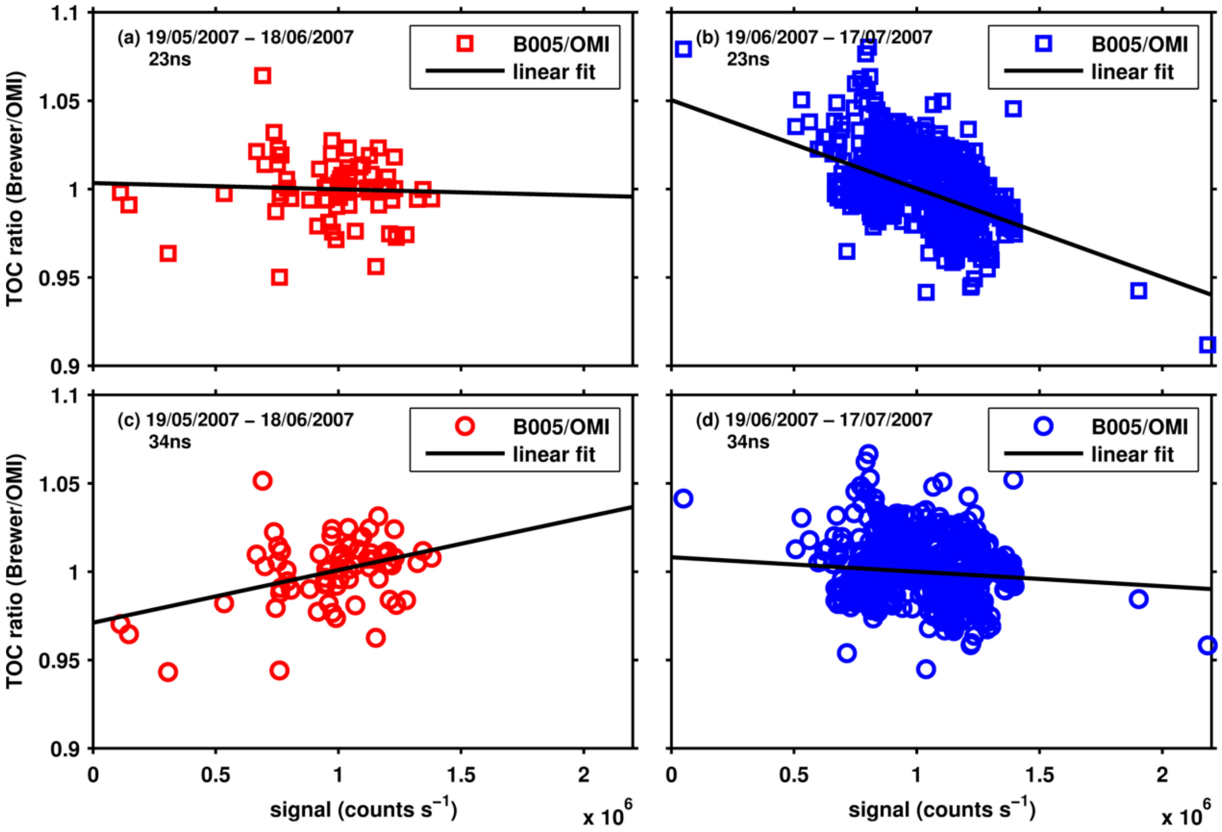

Figure 9. Ratio of TOC derived from B005 for different DT values and OMI, as a function of the Brewer measured signal at slit-mask position 5 (320.1 nm).

Table 1. Uncertainty (1σ) in % of in the measured signal due to photon noise for different levels of the signal and number of cycles.

Counts·s^{-1}	1 cycle	2 cycles	4 cycles	6 cycles	10 cycles	20 cycles	30 cycles	40 cycles
10^2	29.53	20.88	14.76	12.05	9.34	6.60	5.39	4.67
10^3	9.33	6.60	4.67	3.81	2.95	2.09	1.70	1.48
10^4	2.95	2.09	1.48	1.21	0.93	0.66	0.54	0.47
10^5	0.93	0.66	0.47	0.38	0.30	0.21	0.17	0.15
10^6	0.29	0.21	0.15	0.12	0.09	0.07	0.05	0.05