



## Water Vapor Inhibits Hydrogen Sulfide Detection in Pulsed Fluorescence Sulfur Monitors

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**Abstract.** The Thermo Scientific 450 Hydrogen Sulfide - Sulfur Dioxide Analyzer measures both H<sub>2</sub>S and SO<sub>2</sub>. SO<sub>2</sub> is measured by pulsed fluorescence, while H<sub>2</sub>S is converted to SO<sub>2</sub> with a molybdenum catalyst prior to detection. The 450 is widely used to measure ambient concentrations, e.g. for emissions monitoring and pollution control. An air stream with a constant H<sub>2</sub>S concentration was generated and the output of the analyzer recorded as a function of relative humidity. The analyzer under-reported H<sub>2</sub>S as soon as the relative humidity was increased. The fraction of undetected H<sub>2</sub>S increased from 8.3 % at 5.3 % RH (294 K) to over 34 % at RH > 80 %. H<sub>2</sub>S mole fractions of 573, 1142, and 5145 ppb were tested. The findings indicate that previous results obtained with instruments using similar catalysts should be re-evaluated to correct for interference from water vapor. It is suspected that water decreases the efficiency of the converter unit and thereby reduces the measured H<sub>2</sub>S concentration.

### 1 Introduction

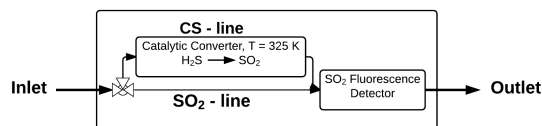
Hydrogen sulfide (H<sub>2</sub>S) is a malodorous, very poisonous, and flammable gas first described by Swedish chemist Carl Wilhelm Scheele (Scheele, 1777). It is produced by the anaerobic bacterial decomposition of organic material, for example in sediments, livestock manure, sewers, and biogas production. In addition, large amounts are given off by hydrodesulfurization in petroleum refineries. It is therefore of great interest to monitor H<sub>2</sub>S in the atmospheric environment.

Analytical instruments used to quantify H<sub>2</sub>S include pulsed fluorescence gas analyzers (Harman, 1981), e.g. the Thermo Scientific 450 Hydrogen Sulfide - Sulfur Dioxide Analyzer, in the remainder of this work called 450. This model has been used in many measurement campaigns worldwide, due to its broad detection range, sensitivity, durability, and reasonable cost. Examples include monitoring H<sub>2</sub>S emissions from poultry egg laying houses in California (Lin et al., 2012; Ni et al., 2012) as part of the National Air Emissions Monitoring Study (Cortus et al., 2010), where also odour was correlated to measured H<sub>2</sub>S concentrations (Akdeniz et al., 2012). These studies all utilized Standard Operating Procedure G5 for H<sub>2</sub>S (Diehl et al., 2006) proposed by the Environmental Protection



Agency (EPA) for monitoring H<sub>2</sub>S; this protocol advises the use of the 450. The instrument has also been used to study H<sub>2</sub>S emissions from anaerobic swine waste treatment (Blunden and Aneja, 2008), and to monitor emissions when altering diets of livestock including cows and pigs (Li et al., 2011; Liu et al., 2012). Furthermore the 450 has been used to determine H<sub>2</sub>S removal efficiencies for several air cleaning techniques, including biofilters at pig finishing facilities and swine waste water pits (Akdeniz et al., 2011; Janni et al., 2014; Lim et al., 2012), as well as biotrickling filters in laboratory studies (Liu et al., 2013). Another study monitored H<sub>2</sub>S concentrations in Reykjavik resulting from two nearby geothermal power plants (Thorsteinsson et al., 2013).

The 450 has two internal flow lines: a Combined Sulfur-line, referred to as the CS-line, and an SO<sub>2</sub>-line (Thermo Fisher Scientific, 2008). The CS-line directs the sample gas through a converter unit, consisting of a molybdenum catalyst at variable temperatures between 310 and 340 °C, which oxidises H<sub>2</sub>S to SO<sub>2</sub>. The SO<sub>2</sub>-line bypasses the converter, measuring the sample gas directly, as seen in Fig. 1. The flow system is used in three different measurement modes: SO<sub>2</sub>, CS, and CS/SO<sub>2</sub>. The



**Figure 1.** Schematic of the 450 Hydrogen Sulfide - Sulfur Dioxide Analyzer.

SO<sub>2</sub> mode only uses the SO<sub>2</sub>-line, bypassing the converter and therefore only detecting SO<sub>2</sub>. The CS mode uses only the CS-line, passing the gas stream through the converter unit before analysis, thereby detecting the amount of total sulfur in the air stream. When measuring in CS/SO<sub>2</sub> mode, the instrument uses a valve to alternate between the two lines, allowing determination of both SO<sub>2</sub> and CS. The CS/SO<sub>2</sub> mode is used to calculate the H<sub>2</sub>S mixing ratio by subtracting the measured SO<sub>2</sub> value from the measured CS value, assuming that all converted sulfur is H<sub>2</sub>S. However, the converter unit does not oxidise all H<sub>2</sub>S to SO<sub>2</sub>, rather it uses a conversion efficiency,  $\delta$ , determined by the manufacturer. The conversion efficiency varies from instrument to instrument, and is typically above 80 %. The conversion efficiency is taken into account when calculating the actual H<sub>2</sub>S mixing ratio using Eqs. 1 and 2 when measuring in the CS/SO<sub>2</sub> mode.

$$\chi_{\text{H}_2\text{S}} = \frac{\chi_{\text{CS}_{\text{detected}}} - \chi_{\text{SO}_2}}{\delta} \quad (1)$$

$$\chi_{\text{CS}} = \frac{\chi_{\text{CS}_{\text{detected}}} - \chi_{\text{SO}_2}}{\delta} + \chi_{\text{SO}_2} \quad (2)$$

Here  $\chi_{\text{SO}_2}$  is the measured SO<sub>2</sub> mixing ratio and  $\chi_{\text{CS}_{\text{detected}}}$  is the non compensated CS mixing ratio measured by the 450.



In CS mode it is assumed that only H<sub>2</sub>S is present. The 450 therefore uses Eq. 3 to calculate the actual CS content of the sample air.

$$55 \quad \chi_{\text{CS}} = \frac{\chi_{\text{CS}_{\text{detected}}}}{\delta} \quad (3)$$

The 450 can also be used to measure other reduced sulfur compounds such as Methanethiol (MT), Dimethylsulfide (DMS), and Dimethyldisulfide (DMDS). Gases such as these have different conversion efficiencies than H<sub>2</sub>S.

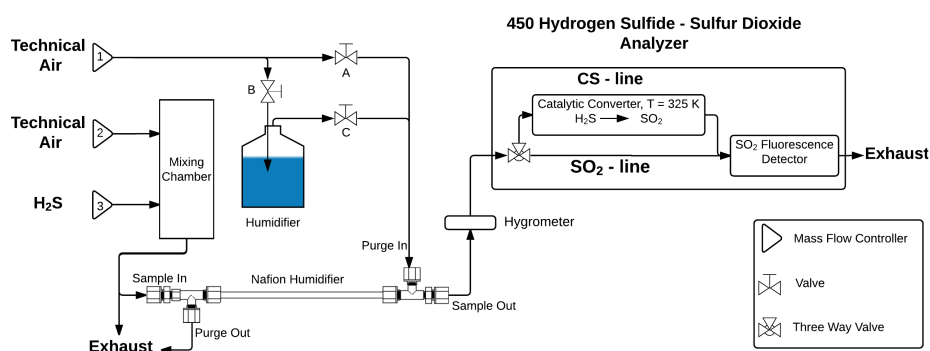
In this study it is shown that the H<sub>2</sub>S response of the 450 has a significant interference from water vapor, even at ambient humidities.

## 2 Method

In order to generate test gasses with predetermined H<sub>2</sub>S mixing ratios and varying relative humidity, flows combining H<sub>2</sub>S and technical air, were generated using three calibrated mass flow controllers (MFC), as shown in Fig. 2. The H<sub>2</sub>S content was controlled using MFCs 2 and 3, where MFC 3 determined the flow from a 100 ppm H<sub>2</sub>S bottle, while MFC 2 determined the flow of technical air for dilution. A mixing chamber was installed after the two MFCs, which ensured a homogeneous mixture before continuing. Part of the diluted H<sub>2</sub>S stream was lead through a Perma Pure Nafion dryer by the 450, while the rest was bled into a fume hood, avoiding overpressure on the sampling line. The Nafion dryer was used to humidify the dry test gas, by allowing water to permeate the Nafion membrane from a humid purge gas. Preliminary tests showed that the measured H<sub>2</sub>S concentration was unaffected by the Nafion dryer. The purge gas was produced with technical air using MFC 3, where valves A, B, and C controlled the amount of air bypassing or entering a humidifier, before reaching the purge inlet of the Nafion dryer. This made it possible to alter the humidity of the purge gas, and thereby also the amount of water transferred across the Nafion membrane into the test gas. Since H<sub>2</sub>S cannot permeate the Nafion membrane, the setup allowed a constant H<sub>2</sub>S concentration, while altering the relative humidity.

Once the test gas left the Nafion dryer, the relative humidity was measured, using a Rotronic HC2-C04 probe with an accuracy of (RH ± 1.5) %. After the humidity probe the air stream entered the 450, which measured the H<sub>2</sub>S content. The instrument used in this study was a model 450i purchased in late 2014, with a stated conversion efficiency of 93.1 %. All other materials and instruments used in the experiments are listed in Table 1.

The humidity response of the 450 was tested at three different H<sub>2</sub>S mole fractions, obtained by adjusting the flows from MFCs 2 and 3. All measurements were conducted in CS mode, since only H<sub>2</sub>S was present in the sample gas. The three initial H<sub>2</sub>S mole fractions were: 573 ± 4, 1142 ± 3, and 5145 ± 8 ppb. These measured values are close to the nominal mixing ratios of: 513 ± 26, 1019 ± 51, and 4756 ± 238 ppb, calculated from MFC settings and stated gas bottle concentration. The



**Figure 2.** Schematic of the experimental setup.

**Table 1.** List of materials and instruments used in the experimental setup.

Item	Manufacturer	Description
H <sub>2</sub> S gas	Yara Praxair	H <sub>2</sub> S in Nitrogen, certified 101 ppm ± 5 %
SO <sub>2</sub> gas	Yara Praxair	SO <sub>2</sub> in Synthetic air, certified 42 ppm ± 5 %
MFC-1	Brooks Instrument	Model: 4800 0-3 L min <sup>-1</sup>
MFC-2	Brooks Instrument	Model: 5850TR 0-10 L min <sup>-1</sup>
MFC-3	Brooks Instrument	Model: 5850S 0-100 mL min <sup>-1</sup>
Nafion dryer	Perma Pure	Model: MD-110-24F-4, 24" dryer

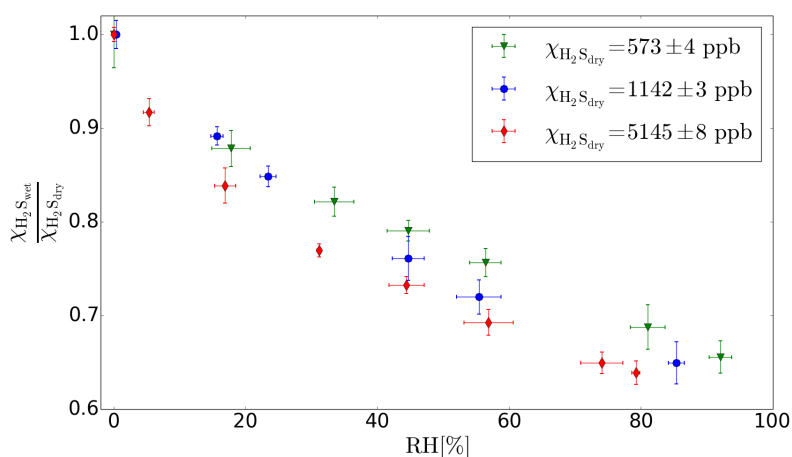
uncertainties of the MFCs were not included in this calculations, which could explain the observed offset.

- 90 In each experiment the H<sub>2</sub>S mixing ratio was measured initially under completely dry conditions, meaning that the two valves leading to and from the humidifier (valves B and C) were closed, while the bypass valve (A) was open. Once a stable concentration was obtained, measurements continued for 20-30 minutes, ensuring sufficient data for analysis. The humidity was then increased by slightly opening valves B and C. The system was allowed to equilibrate, typically for 30-60 minutes, fol-
- 95 lowed by another 20-30 minutes of measurements at stable H<sub>2</sub>S concentration and humidity. The procedure was repeated for several different humidities, with a stable temperature in all experiments of 294.2 ± 0.8 K.



### 3 Results & Discussion

In all experiments the H<sub>2</sub>S mixing ratio decreased within 1-2 minutes of increasing the humidity of the test gas, showing that the 450 responds very quickly to changes in water content of the sample air.



**Figure 3.** The ratio between measurements of H<sub>2</sub>S at wet and dry conditions for three initial mole fractions, plotted against the corresponding humidity at a temperature of  $294.2 \pm 0.8$  K. All errorbars have been multiplied by 5 for better visualization.

The ratio between the H<sub>2</sub>S mole fractions measured at wet and dry conditions were plotted against the relative humidity in Fig. 3. Already at a relative humidity of 5.3 %, a clear decrease from 5145 to 4718 ppb was observed, corresponding to a reduction of 8.3 % in measured H<sub>2</sub>S. Higher reductions were observed when increasing the humidity further, showing an almost linear correlation between the increase in humidity and the decrease in H<sub>2</sub>S mole fraction. At all three initial mixing ratios more than 34 % of the H<sub>2</sub>S content passed the instrument undetected when measuring at relative humidities above 80 %. The largest decrease was observed at the high initial H<sub>2</sub>S mole fraction, indicating that the effect could be even greater at higher concentrations.

A similar experiment was conducted with SO<sub>2</sub> instead of H<sub>2</sub>S, and no interference from water was observed. This led to the conclusion that the interference from water was produced in the converter unit, possibly due to inhibition of catalytic sites, thereby lowering of the conversion efficiency. According to our observations it is not necessary to dry the sample air when measuring SO<sub>2</sub>.

The interference from water calls earlier studies into question, unless sampling was performed under completely dry conditions. However a significant reduction in measured H<sub>2</sub>S was observed already at 5.3 % relative humidity, which might pose difficulties for ambient sampling. The inter-



ference from water is not mentioned in the instrument manual, instead it is stated that the instru-  
ment functions at ambient conditions. Therefore most studies do not dry sample air before mea-  
suring, meaning that many earlier studies may have under-reported H<sub>2</sub>S levels. The fast response  
120 to changes in humidity, could make events such as rainfall result in significant under-reporting of  
H<sub>2</sub>S concentrations. Furthermore the interference could result in overestimations of removal effi-  
ciencies for certain biofilters, where high humidities are necessary for the filters to function. Our  
measurements indicate that the Standard Operating Procedure provided by the U.S. Environmental  
protection agency, should be revised to account for the water vapor interference. The water vapor  
125 interference may also occur in instruments that utilize a similar technique such as the Teledyne T101  
H<sub>2</sub>S analyzer (Teledyne, 2012), but this was not tested in present study. It is not clear how many  
instruments are affected, and users should therefore investigate if similar behaviours are observed in  
their instruments.

#### 4 Conclusions

130 It has been shown that the Thermo Scientific 450 Sulfur analyzer shows a significant water vapor  
interference when measuring H<sub>2</sub>S. Reductions of up to 1/3 of the dry H<sub>2</sub>S mixing ratio have been  
found at ambient conditions. Our analysis is that the interference occurs in the catalytic unit con-  
verting H<sub>2</sub>S to SO<sub>2</sub>. These findings indicate that earlier results obtained with the 450 and similar  
instruments are very likely to have under-reported H<sub>2</sub>S concentrations and should therefore be re-  
135 evaluated. Since it is not clear how many instruments are affected, users of the 450 should investigate  
if similar behaviour are shown with their instruments. Based on these findings it is recommended  
to dry the air stream prior to a catalytic H<sub>2</sub>S monitoring instrument using a Nafion dryer or another  
appropriate drying technique.

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