



17 **Abstract:**

18 X-band-radar-based quantitative precipitation estimation (QPE) system is increasingly
19 gaining interest thanks to its strength in providing high spatial resolution rainfall
20 information for urban hydrological applications. However, prior to such applications, a
21 variety of errors associated with X-band radars are mandatory to be corrected. In
22 general, X-band radar QPE systems are affected by two types of errors: 1) common
23 errors (e.g. mis-calibration, beam blockage, attenuation, non-precipitation clutter,
24 variations in the raindrop size distribution) and 2) “wind drift” errors resulting from
25 non-vertical falling of raindrops. In this study, we first assess the impacts of different
26 corrections of common error using a dataset consisting of one-year reflectivity
27 measurements collected at an X-band radar site and a distrometer along with rainfall
28 measurements in Beijing urban area. The common error corrections demonstrate
29 promising improvements in the rainfall estimates, even though an underestimate of 24.6%
30 by the radar QPE system in the total accumulated rainfall still exists as compared with
31 gauge measurements. The most significant improvement is realized by beam
32 integration correction. The DSD-related corrections (i.e., convective–stratiform
33 classification and local Z - R relationship) also lead to remarkable improvement and
34 highlight the necessity of deriving the localized Z - R relationships for specific rainfall
35 systems. The effectiveness of wind drift correction is then evaluated for a fast-moving
36 case, whose results indicate both the total accumulation and the temporal characteristics
37 of the rainfall estimates can be improved. In conclusion, considerable potential of X-
38 band radar in high-resolution rainfall estimation can be realized by necessary error



39 corrections.

40 **Keywords:** urban hydrology, X-band radar, quantitative precipitation estimation, error

41 correction, wind drift effect



42 **1. Introduction**

43 Urban flash flooding is one of the most severe hazards in cities (Schmitt et al., 2004;
44 Yang et al., 2015a). Large coverage of impervious surfaces in cities will exaggerate the
45 flooding since heavy rainfall is more likely to transform into runoff instead of
46 infiltrating into the soil. To mitigate its detrimental effects, accurate prediction of runoff
47 at high spatiotemporal resolution is critical for emergency management and warning
48 operations. When conducting the hydrological and/or hydraulic simulations, the
49 spatiotemporal variability of rainfall is known to be the major source of a range of
50 uncertainties (Schellart et al., 2012; Schröter et al., 2015; Rafieeiniasab et al., 2015;
51 Rico-Ramirez et al., 2015), which thus warrants compelling need for high-resolutions
52 rainfall data (Schilling, 1991; Emmanuel, et al, 2012; Eldardiry et al., 2015).

53

54 Weather radars have been worldwide recognized as essential tools to provide high-
55 resolution rainfall measurements (Smith and Krajewski, 1991; Krajewski and Smith,
56 2002; Li et al., 2014; Li et al., 2015). The current operational weather radar systems
57 (e.g., NEXRAD in America, OPERA in Europe) based on C-band and/or S-band radars
58 operating on long-range coverage. However, their spatiotemporal resolutions of 1
59 km/5–10 min are insufficient to support accurate estimations of precipitation variability
60 in urban area (Krajewski et al., 2002; Smith et al., 2007). For instance, recent studies
61 suggest that for urban areas less than 1 ha, rainfall input is required at the spatial
62 resolution of ~100 m; while for urban areas between 1 ha and ~100 ha, the required
63 resolution is relaxed to 500 m (Faures et al., 1995; Berne et al., 2004). Considering the



64 high utility in monitoring rainfall in urban area, X-band radars are being deployed in a
65 number of hydrometeorological applications (Chen and Chandrasekar, 2015).

66

67 Prior to the application of radar-based rainfall product in hydrological simulations,
68 quantitative precipitation estimation (QPE) systems are mandatory to be established,
69 where multiple error sources should be appreciated (e.g. Krajewski and Smith, 2002;
70 Villarini and Krajewski, 2010). One of the error sources is associated with the
71 reflectivity measurement, which can be attributable to mis-calibration, beam blockage,
72 attenuation, non-precipitation clutter, and vertical profile of reflectivity (VPR). These
73 errors may reduce the accuracy of reflectivity measured by weather radar (Germann et
74 al., 2006; Hazenberg et al., 2011a). The variability of Z - R relationship is another
75 important error source. The standard Z - R relationship (Chapon et al., 2008; Hazenberg
76 et al., 2011b) takes the form of $Z = aR^b$ (Marshall and Palmer, 1948), in which the
77 parameters a and b depend on the raindrop size distribution (DSD). Inappropriate
78 determination of a and b will introduce errors into the estimated rainfall. The above
79 errors are termed as **common errors** in this study as they have to be corrected for most
80 operational radars.

81

82 Besides the common errors, the rainfall estimates for X-band radar can be affected by
83 other weather-related dynamic processes. For instance, the falling paths of raindrops
84 are not perfectly vertical due to wind, implying a horizontal displacement may exist
85 between the aloft measurement position and ground falling location of a raindrop, or



86 the “**wind drift**”. The wind drift can lead to inconsistency between the estimated and
87 actual rainfall fields at the ground level (Fabry et al., 1994; Liu and Krajewski, 1996;
88 Sandford., 2015; Seo and Krajewski, 2015). Usually the wind drift is ignored for the S-
89 band and C-band radars due to their relatively coarse spatial resolution. However, this
90 effect can be remarkable for X-band radars given its high spatial resolution of ~100 m,
91 in particular under windy conditions that are common for convective rainfall events
92 (Sandford, 2015; Seo and Krajewski, 2015). As such, errors due to the wind drift should
93 be appreciated in the application of X-band radars in urban hydrometeorology.

94

95 In order to improve the quality of X-band radar based QPE systems in urban
96 hydrometeorological applications, different procedures have been explored to reduce
97 the aforementioned errors. Current research on X-band radar shows that using the
98 differential phase shift can reliably resolve the attenuation which is the primary
99 disadvantage of X-band radar (Anagnostou et al., 2004, 2006a,b; Park et al., 2005;
100 Kalogiros et al. 2014). Specifically, Kalogiros et al. (2014) developed an algorithm to
101 correct the attenuation of horizontal-polarization reflectivity by using an iterative
102 optimal parameterizations of specific differential attenuation and backscattering phase
103 shift. Besides the attenuation, Van de Beek et al. (2010) suggested that the effects of
104 non-precipitation clutter should also be carefully addressed for applications of X-band
105 radars in urban areas. Lo Conti et al. (2015) investigated the effect of calibration in the
106 $Z-R$ relationship of an X-band radar in Palermo (Italy), suggesting the high variability
107 of the $Z-R$ relationships determined for specific events limited its wide applicability.



108 Matrosov et al. (2016) found no bright band rainfall has distinct Z - R relationship from
109 those of other rain types and should be distinguished from stratiform rainfall. For
110 operational applications, Anagnostou et al. (2010) showed that adjusting the Z - R
111 relationship for mean-field bias with the K_{DP} - R estimates as reference is a promising
112 technique for acquiring unbiased high resolution radar-rainfall estimates. Maki et al.
113 (2010) developed one X-band radar QPE system for three major metropolitan areas in
114 Japan, which may still underestimate the rainfall by ~20% compared with the gauge
115 measurement even though the effects due to non-precipitation clutter, beam blockage
116 and attenuation have been accounted for. Chen and Chandrasekar (2015) developed a
117 high-resolution (250 m/1 min) QPE system in Dallas–Fort Worth urban area consisting
118 of polarimetric Weather Surveillance Radar 88 Doppler (WSR-88D) and X-band radars,
119 which demonstrated low overall biases and normalized standard errors in rainfall
120 accumulation products of different temporal scales (5-60 min). Although these studies
121 demonstrate the effectiveness of different measures in improving the X-band-radar-
122 based QPE systems, the relative importance of different error sources contributing to
123 the overall errors remains to be unknown. Furthermore, given the errors of a specific
124 radar QPE system strongly depend on the spatiotemporal characteristics of the local
125 rainfall system, an analysis of long-term rainfall characteristics is expected to enable a
126 better understanding of the potential of X-band-radar-based QPEs in urban
127 hydrometeorological applications.

128

129 In this study, we use a dataset consisting of one-year measurements by an X-band radar



130 in Beijing to explore its potential in high resolution rainfall estimation. The study period
131 extends from July 2014 to September 2015 with 43 rainfall events. Specifically, we aim
132 to answer the following two questions: 1) What is the relative importance of different
133 error sources for the overall accuracy of a QPE in urban area; 2) What are the impacts
134 of wind drift on the ground-level rainfall estimation?

135

136 The paper is organized as follows. Section 2 describes the study area and the dataset.
137 Section 3 details the correction procedures for common error sources and wind drift in
138 X-band-radar-based QPEs. The relative importance of correcting each common error
139 for rainfall estimation is discussed in Section 4, followed by a case study to show the
140 implication of wind drift correction. Finally, the concluding remarks are provided in
141 Section 5.

142

143 **2. Study Area and Data Description**

144 Beijing, the capital city of China with more than 21 million residents, features complex
145 topography, with mountains to its north and west and a highly urbanized area in its
146 eastern part. Beijing is prone to summertime heavy rainfall events that occasionally
147 lead to severe flash floods (Yang et al., 2014b).

148

149 The dataset used in this study consists of one-year measurements by a single-polarized
150 X-band radar (Fig. 1a, hereafter referred as Beijing Radar) in the northwest of Beijing.
151 Technical specifications of the Beijing X-band radar are given in Table 1. A full



152 volumetric scanning by the Beijing Radar is performed every 7 min at 14 elevations
153 (0.5 °, 0.9 °, 1.3 °, 1.8 °, 2.4 °, 3.1 °, 4.0 °, 5.1 °, 6.4 °, 8, 10.0 °, 12.0 °, 15.6 °, and 19.5 °). Each
154 scan has 400 gates along the beam with a gate resolution of 90 m and a maximum range
155 of 36 km.

156
157 An OTT Parsivel disdrometer (Fig. 1b) deployed near the Beijing Radar (within 5 km,
158 cf. Fig. 2) and a gauge network consisting of 8 standard tipping-bucket gauges (Fig. 2)
159 are used to validate the QPE system for Beijing Radar. The disdrometer can archive 32
160 equivalent diameter classes (ranging from 0 to 26 mm with varying diameter increments
161 between 0.125 and 3 mm) and 32 different velocity classes at 1-min resolution. Other
162 specifications of the disdrometer are provided in Table 2.

163
164 In order to avoid the temporal bias among radar, disdrometer and rain gauge
165 measurements, all the measurements are conformed at 1-h resolution for subsequent
166 analysis. We note that the bias correction by assimilating gauge data were not
167 performed in this study due to its shadow effect over the corrections in radar QPE
168 system (Hazenberg et al., 2011a).

169

170 **3. Rainfall estimation algorithm**

171 **3.1 Procedures for common error corrections**

172 The common errors introduced in reflectivity measurement are mostly due to radar
173 miscalibration, non-precipitating echo contamination, signal attenuation, beam



174 blockage and VPR, whereas the errors in Z - R conversion rely on the variability in Z - R
175 relationships for different rainfall types. We note that the errors due to VPR are not
176 considered for two reasons: 1) the lack of required a priori knowledge of vertical profile
177 of rainfall in Beijing and 2) the minimal influence of VPR in this study since the
178 maximum effective measurement height of 2.5 km of Beijing Radar is lower than the
179 melting layer height of ~4 km for the warm-season rainfall (Cao and Qi, 2014).

180

181 3.1.1 Radar calibration

182 Radar calibration is conducted to fix the inappropriate parameter settings. Although the
183 Beijing Radar has been calibrated before installation, post-installation calibration
184 should be conducted to cancel the possible aging and thermal effects (Collier, 1989).
185 Among all the available calibration approaches (Manz et al., 2000), calibration with
186 disdrometer data would be the most straightforward one (Lee and Zawadzki, 2006).
187 With the help of a nearby disdrometer (cf. Fig. 2 for its location), Beijing Radar is
188 calibrated by comparing the radar measurements with disdrometer measurements.

189 The disdrometer-based estimate of Z can be expressed as (Delrieu et al., 1999):

$$Z = \frac{10^6 \lambda^4}{\pi^5 |K|^2} \int_0^{\infty} \sigma_B(D) N(D) dD, \quad (1)$$

190 where λ is the operational wavelength of the radar (3.21 cm in this study), $|K|^2$ a
191 coefficient dependent on the dielectric constant of water. Assuming a raindrop is a
192 sphere of diameter D (cm), DSD spectra $N(D)$ (cm^{-4}) is defined as the raindrop
193 concentration in a given air volume as a function of D and $\sigma_B(D)$ is the backscattering



194 cross-section area (cm^2) as a function of D . Note that the Mie calculation is adopted in
195 this study since the Rayleigh approximation does not satisfy the condition $D \leq \lambda/16$
196 when $\lambda = 3.21$ cm.

197

198 The comparison of the reflectivity measurement between radar and disdrometer
199 demonstrates overall consistency with observed underestimates by radar for reflectivity
200 exceeding 35 dBZ (an example for the comparison of the 1th September 2014 event is
201 shown in Fig. 3). Except for the calibration error, this underestimation may be the joint
202 effect of attenuation and inconsistency between the ground-level point measurements
203 and the aloft volume measurements. Therefore, although there is a calibration drift for
204 the Beijing Radar, it was decided not to apply any correction to the reflectivity
205 measurements for the 43 selected events.

206

207 **3.1.2 Non-precipitating echo removal**

208 Radar echoes may be contaminated by non-precipitating echoes that need to be
209 identified and removed before rainfall estimation. Ground clutters and anomalous
210 propagations are the two main sources of non-precipitating echoes (Steiner and Smith,
211 2002). Ground clutters are caused by scattering in the antenna sidelobes hitting the
212 ground close to the radar site as well as by fixed objects (Villarini and Krajewski, 2010).
213 Anomalous propagations are contamination of radar reflectivity data from echoes
214 normally not seen by the radar. In particular, anomalous propagations remain a serious
215 problem for situations when they are embedded in precipitation echoes (Steiner and



216 Smith, 2002).

217

218 For Beijing Radar, the ground clutter effect is corrected by removing the echoes with
219 radial Doppler velocity close to zero. As the more advanced polarimetric techniques
220 cannot be applied to the measurements by the Beijing Radar, the well-recognized
221 Steiner and Smith (2002) algorithm is used for detecting anomalous propagations (e.g.,
222 Hazenberg et al., 2011a, Hazenberg et al., 2014). This algorithm utilizes the three-
223 dimensional reflectivity structure and builds upon three key parameters: the vertical
224 extent of radar echoes, their spatial variability and vertical gradient of intensity, which
225 are available in the Beijing Radar measurements.

226

227 **3.1.3 Attenuation correction**

228 Radar signals can be attenuated during propagation (Atlas and Banks, 1951), in
229 particular for X-band radars running at short wavelengths. For single-polarized radars,
230 correction algorithms can be categorized into forward and backward algorithms
231 (Delrieu et al., 1999). Among the forward algorithms, the HB algorithm (Hitschfeld
232 and Bordan, 1954) is widely applied and thus adopted in this study for attenuation
233 correction, whose key steps are recapitulated here.

234

235 For a well calibrated radar without blind-range attenuation (e.g. radome attenuation),
236 its measured reflectivity Z_m can be expressed as:

$$Z_m(r) = Z(r) A(r), \quad (2)$$



237 where $Z(r)$ is the true reflectivity at the same range and $A(r) =$
 238 $\exp\left(-\frac{2 \ln(10)}{10} \int_0^r k(s) ds\right)$ is the path-integrated attenuation (PIA) factor with the
 239 specific attenuation $k(s)$ at a distance s being the only unknown to resolve.

240

241 Meanwhile the relationship between the true reflectivity Z and the specific attenuation
 242 k can be given by:

$$Z = ck^d, \quad (3)$$

243 where c and d are the DSD related parameters. Therefore, by canceling k , the
 244 relationship between $Z_m(r)$ and $Z(r)$ can be obtained as follows:

$$Z(r) = \frac{Z_m(r)}{\left(1 - \frac{2 \ln(10)}{10} \int_0^r \left(\frac{Z_m(s)}{c}\right)^{\frac{1}{d}} ds\right)^d}, \quad (4)$$

245 where the parameters c and d can be determined by Z - k regression (Eq.3) with
 246 distrometer measurements. To avoid the numeric instability known in the HB algorithm,
 247 a maximum PIA of 10 dB is specified in this study.

248

249 Also, knowing the DSD, k can be calculated by:

$$k = c_k \int_0^\infty Q_t(D) N(D) dD, \quad (5)$$

250 where D (cm) denotes the raindrop diameter, Q_t (cm²) the Mie total attenuation cross
 251 sections (refer to Delrieu et al. (1999) for the calculation method of Q_t), N (cm⁻⁴) the
 252 raindrop concentration in a given air volume and $c_k = 0.4343 \times 10^6$ a constant.

253

254 By conducting Z - k regression (Eq. 3) with distrometer measurements from July 2014



255 to September 2015 without differentiating rainfall types (Fig. 4), the required
256 parameters for Z_m - Z relationship (Eq.4) are determined as $c = 1.12 \times 10^5$ and $d =$
257 1.1.

258

259 **3.1.4 Beam Integration**

260 Due to the presence of obstructions on the beam path in terrain-complex contexts (e.g.
261 urban, mountainous areas), beam blockage frequently occurs and thus compromise the
262 accuracy of radar QPE. In particular, considering the radar are usually operated at the
263 low elevation angles where more ground clutters exist, removal of beam blockage effect
264 is of great importance for radar QPE systems. As such, beam integration, a technique
265 to avoid the beam blockage by integrating measurements at different elevations for
266 different azimuths, is conducted in this study.

267

268 In this study, the starting integral elevation, or the lowest optimal elevation, for a
269 specific azimuth range is determined as the lowest elevation that at which the beam
270 blockage of all ranges in this azimuth range must be less than 50% (cf. Fig. 2 for the
271 starting integral elevations in this study). For instance, measurements at the elevation
272 of 4.0° for the azimuth between 177° and 181° are used in this study since two tall
273 buildings stand to the south of the Beijing Radar.

274

275 **3.1.5 Convective–stratiform classification**

276 Because of the distinct DSD characteristics between the convective and stratiform



277 rainfall, the Z - R relationships for the two types of rainfall differ significantly. It is thus
 278 necessary to conduct the convective-stratiform classification before the Z - R conversion.
 279 Due to the unavailability of real-time atmospheric temperature profiles that is
 280 commonly used for convective-stratiform classification, a vertically integrated liquid
 281 (VIL; Greene and Clark, 1972) based method (Zhang and Qi, 2010) is adopted in this
 282 study.

283

284 With the volume scan reflectivity measurements, VIL can be obtained by:

$$\text{VIL} = \sum_k \text{VILpar}_k, \quad (6)$$

285 where $\text{VILpar}_k = \text{LW} \cdot \text{DB}$ denotes the VIL within the k^{th} tilt with LW (kg km^{-3}) and
 286 DB (km) being the liquid water content associated with a particular value of reflectivity
 287 and the depth of a radar beam, respectively, given by

$$\text{LW} = 3.44 \times 10^3 Z^{\frac{4}{7}}, \quad (7)$$

$$\text{DB} = \begin{cases} \text{BH}[\theta_{k_{\text{top}}} + 0.5\text{BW}] - \text{BH}[0.5(\theta_{k_{\text{top}}} + \theta_{k_{\text{top}}-1})] & k = k_{\text{top}} \\ \text{BH}[0.5(\theta_{k+1} + \theta_k)] - \text{BH}[0.5(\theta_k + \theta_{k-1})] & 1 < k < k_{\text{top}}, \\ \text{BH}[0.5(\theta_1 + \theta_2)] & k = 1 \end{cases} \quad (8)$$

288

289 where DB (km) is the depth of a radar beam, Z the radar reflectivity within a radar
 290 sample volume, BW the angular width of the radar beam between the half-power points,
 291 BH the beam center height for a given elevation angle and range under the standard
 292 atmospheric refraction conditions and θ_k the elevation angle at the k^{th} tilt.

293

294 Once the knowledge of VIL is obtained, the reflectivity pixels can be categorized into
 295 stratiform with $\text{VIL} < 6.5 \text{ kg m}^{-2}$ and convective with $\text{VIL} \geq 6.5 \text{ kg m}^{-2}$.



296

297 **3.1.6 Derivation of local Z-R relationships**

298 The standard Z-R relationships are $Z = 200 R^{1.6}$ and $Z = 300 R^{1.4}$ for stratiform and
299 convective situations, respectively. However, due to the large variability of Z-R
300 relationship among different locations, localized Z-R relationships are mandatory for
301 building radar QPE systems. As such, we use the DSD measurements collected at the
302 distrometer sites near the Beijing Radar to establish the local Z-R relationships.

303

304 As can be seen in Fig. 5, by conducting Z-R regression without differentiating rainfall
305 types, $Z=428.4 R^{1.2}$ is obtained from non-linear regression. Furthermore, considering
306 the rainfall types (stratiform for $Z \leq 39$ dBZ and convective for $Z > 39$ dBZ; cf.
307 Steiner et al., 1995), Z-R relationships $Z=426.5 R^{1.3}$ and $Z=499.3 R^{1.2}$ are obtained for
308 stratiform and convective event, respectively. It is noteworthy that the Z-R relationships
309 derived by this study distinguish from the standard forms, implying the necessity of
310 locally-derived forms in radar QPE systems. It is also noteworthy the convective events
311 comprise a large portion of the rainfall events, which is consistent with the previous
312 findings that convective events are common in urban areas. (Yang et al., 2014a, Yang
313 et al., 2015b, Yu et al., 2015).

314

315 **3.2 Procedure for wind drift correction**

316 Wind drift means the horizontal displacement between the aloft measurement position
317 and ground falling location of a raindrop. Wind drift correction enables better rainfall



318 estimation at the ground level. The horizontal displacement Δx of a raindrop can be
319 estimated by integrating horizontal wind velocity $u(h)$ over falling duration (Caroline,
320 2015) as follows:

$$\Delta x = \int_0^t u(h) dt = \int_0^{h_b} \frac{u(h)}{w(h)} dh, \quad (9)$$

321 where $w(h)$ is the falling speed at height h and h_b is the height of the radar beam at the
322 measurement location. And $u(h)$ is given by:

$$u(h) = S \cdot h, \quad (10)$$

323 where S is a constant wind shear (Caroline, 2015).

324 By assuming a zero wind speed at the ground level, the wind shear S can be calculated
325 by:

$$S = \frac{u(h_b)}{h_b}. \quad (11)$$

326 Given the constant falling speed of 5 m s^{-1} for raindrops below the melting layer
327 (Caroline 2015), the Eq. (12) thus can be simplified as:

$$\Delta x = \frac{1}{5} \frac{S h_b^2}{2} = \frac{u(h_b) h_b}{10}. \quad (12)$$

328 Furthermore, $u(h_b)$ can be determined by a pixel-based tracking algorithm for short-
329 term quantitative rainfall forecasting (Zahraei et al., 2012). The tracking algorithm can
330 estimate the advection velocity of a rainy pixel (equal to the background wind velocity)
331 by tracking its successive positions between radar images based on the maximum
332 correlation of meshes in consecutive images.

333

334 4. Results and discussion

335 4.1 Importance of different common corrections



336 To assess the relative importance of different common error corrections, a rotation-
 337 based strategy is conducted, which consists of two procedures as follows:

338 1) **Complete-correction (CC) procedure**: all the corrections described in Section 3.1
 339 are applied to the reflectivity measurements to obtain the rainfall field as the best
 340 estimate;

341 2) **Partial-correction (PC) procedure**: all but one of the corrections as in the CC
 342 procedure are used to estimate the rainfall, whereby the corresponding estimate can
 343 be compared with the best estimate of CC procedure to assess the effectiveness of
 344 a specific error correction (i.e., the excluded correction). By rotating the specific
 345 correction in the PC procedure, rainfall estimates without different corrections can
 346 thus be obtained.

347

348 Furthermore, to quantify the correction effectiveness so that get the relative importance
 349 of different error sources contributing to the overall errors, the radar-gauge ratio of daily
 350 accumulated rainfall rd , average radar-gauge ratio of total rainfall ra , the root-mean-
 351 square error RMSE, and the coefficient of determination r^2 are introduced as follows:

$$rd_{i,k} = \sum_n R_{n,i,k} / \sum_n G_{n,i,k}, \quad (13)$$

$$ra = \frac{1}{8} \sum_{k=1}^8 \sum_n R_{n,k} / \sum_n G_{n,k}, \quad (14)$$

$$RMSE = \sqrt{\frac{1}{N} \sum_{n=1}^N (R_n - G_n)^2}, \quad (15)$$

$$r^2 = \frac{(\sum (R_n - \bar{R}_n)(G_n - \bar{G}_n))^2}{(\sum_{n=1}^N (R_n - \bar{R}_n)^2)(\sum_{n=1}^N (G_n - \bar{G}_n)^2)} \quad (16)$$

352 where the subscript i and k denote the date number and gauge number, respectively;
 353 while the radar-based estimates R and gauge measurements G with n and N denoting



354 the n -th hour and total number of hours, respectively. The first two metrics are chosen
355 to describe the systematic bias, while the last two assess the average error magnitude
356 and agreement at hourly scale.

357

358 To reduce the bias in the radar-gauge comparison, 33 events, during which at least three
359 gauges have valid measurements, are chosen and investigated for the correction
360 effectiveness. For the 33 events, the ratio rd based on the CC procedure varies mostly
361 between 0 and 3 with the medians ranging between 0.5 and 1.5 (Fig. 6), suggesting a
362 promising performance of common corrections, though considerable variability can be
363 observed for several events (e.g., events of July 29, 2015). Extending beyond the 33
364 chosen events to all the events in the study period, it is also noted that with the CC
365 procedure performed, the Beijing Radar underestimates the rainfall compared with the
366 gauges (cf. a linear radar-gauge regression slope of 0.69 and coefficient of
367 determination R^2 of 0.76 in Fig. 7) with an averaged underestimate of 24.6% in the total
368 rainfall. This result is comparable with that of the X-band radar at the Delft University
369 (cf. a linear radar-gauge regression slope of 0.65 reported in Van de Beek et al. (2010)).

370

371 The influence of the PC procedure on the rainfall estimates is then examined by
372 comparing the above metrics between the radar-based estimates and gauge
373 measurements during the study period (Table 3 and Fig. 8). Correction for anomalous
374 propagations contributes a minimal improvement in the rainfall estimates (Fig. 8a)
375 because this correction may reduce the estimated reflectivity and thus the rainfall.



376 However, such minimal influence does NOT suggest the non-necessity of anomalous
377 propagation correction since its improvement is largely screened by errors from other
378 sources. The attenuation correction demonstrates improvement in the rainfall estimates
379 in terms of both ra and RMSE (Fig. 8b). As expected, the largest improvement is
380 resulted from the beam integration as indicated by the reduced RMSE (cf. RMSE from
381 3.18 for -BI to 1.95 for CC in Table 3) and by the increased coefficient of determination
382 r^2 for the radar-gauge linear regression (cf. from 0.54 to 0.76 in Fig. 8c). The increased
383 deviation for no beam integration suggests that larger ra (cf. 0.87 for -BI in Table 3) is
384 actually the results of offset of positive and negative deviations.

385

386 Furthermore, significant improvements are observed in the estimated rainfall when the
387 variability in the DSD is taken into account: both the convective–stratiform
388 classification and the local Z - R relationship derivation contribute to increases in ra and
389 decreases in RMSE (Table 3). Such improvements are also demonstrated by the
390 increases in the slope of radar-gauge linear regression (Fig. 8d and e).

391

392 In general, the DSD-related corrections (i.e., convective–stratiform classification and
393 the local Z - R relationship) demonstrates greater improvement in the estimation of
394 rainfall as compared with some of the reflectivity-related corrections (i.e., anomalous
395 propagations removal, attenuation correction), implying the importance of appropriate
396 DSD-related corrections.

397



398 **4.2 Case study: a fast-moving event of 20150904**

399 Although considerable improvements can be observed in the rainfall estimates after the
400 common error corrections, it should be noted the potential for improving the rainfall
401 estimates may be realized by correcting the wind drift errors in radar QPE systems, in
402 particular for X-band radars of high spatial resolutions. To examine the effect on the
403 radar based rainfall estimates of wind drift correction, a long-duration event (~16 h) on
404 4th September 2015 featuring fast-moving storms with complex structures is analyzed
405 here.

406

407 The event originated from low pressure system passing over Beijing from southwest
408 towards northeast, where a high pressure zone resided over the urban area of Beijing.
409 Taking an episode of ~30 min for instance, several convective cells rapidly grew in the
410 southwest of Beijing (Fig. 9a and b), then quickly moved to northeast (Fig. 9c), and
411 developed to a widespread precipitating system afterwards (Fig. 9d).

412

413 The influence of the wind drift correction on the hourly rainfall estimates is then
414 examined by a radar-gauge linear regression (Fig. 10). After the wind drift correction,
415 the slope and coefficient of determination R^2 of the radar-gauge regression increase
416 from 0.46 to 0.58 and from 0.69 to 0.79, respectively, suggesting an evident
417 improvement in the estimates of total rainfall. In addition, the temporal characteristics
418 of rainfall estimates are refined as well. For instance of a gauge close to the radar, the
419 correlation coefficient of the rainfall series between the radar and gauge is increased



420 from 0.79 to 0.86 and the RMSE of rainfall measurements is reduced from 27.4 to 18.8
421 after the wind drift correction (Fig. 11). It is also noteworthy that the wind drift
422 correction leads to an improved temporal consistency in the rainfall time series between
423 the gauge and radar with the more accurate rainfall estimate at the peaking time (i.e.,
424 17:00 shown in Fig. 11).

425

426 **5. Concluding remarks**

427 In this study, we analyzed 43 rainfall events between July 2014 and September 2015
428 based on the measurements gathered by an X-band single-polarized radar, a
429 distormeter and 8 rain gauges in Beijing urban area. These measurements allow us to
430 explore the potential for high-resolution rainfall measurement with X-band radar over
431 complex urban region. The impacts and importance of common corrections (i.e., radar
432 calibration, non-precipitating echo removal, attenuation correction, beam integration,
433 convective–stratiform classification and local Z - R relationships) on the quality of the
434 radar QPE is first studied, followed by an assessment of the effectiveness of wind drift
435 correction. The major findings are summarized as follows:

- 436 1) Although the radar QPE system underestimates the total rainfall accumulations by
437 24.6% as compared with gauges, the common corrections demonstrate promising
438 improvements in the rainfall estimates.
- 439 2) The greatest improvements in the radar based rainfall estimates can be attributed to
440 the beam integration, which significantly outperforms the operation at the single
441 lowest elevation without beam blockage (i.e., 4.0 ° in this study). It is thus highly



442 suggested to conduct volumetric reflectivity measurements with the X-band radar
443 in particular for complex-terrain regions. Minor improvements on the radar rainfall
444 estimation are observed after the anomalous propagations removal as compared to
445 other common error corrections.

446 3) The DSD-related corrections (i.e., convective–stratiform classification and local Z -
447 R relationship) lead to significant improvements in the rainfall estimates. And the
448 local Z - R relationship plays a more crucial role in improving the rainfall estimates
449 compared with the other corrections, which highlights the necessity of deriving the
450 localized Z - R relationships for different types of rainfall.

451 4) The wind drift correction improve both the total accumulation and the temporal
452 characteristics of the estimated rainfall, which suggest the necessity of wind drift
453 correction for X-band radars of high spatial resolutions.

454

455 The possible future improvement relies on the inclusion of vertical profile of reflectivity
456 (VPR) measurements of this region to correct the underestimation in reflectivity (Qi et
457 al., 2013). In addition, polarimetric radars, featuring the ability to capture two-
458 dimensional structure of rainfall, can provide new insight into rainfall microphysics and
459 make further improvements in monitoring urban rainfall.

460

461

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467 providing the rain gauge data.



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620 radar-derived QPE, *J. Hydrometeorol.*, 11, 1157–1171, 2010.

621



622 **Table 1 Main specifications of X-band radar used in this study.**

Parameters	Value
Frequency	9.38 Ghz
Peak transmitted power	25 kw, 38 dB gain
Antenna	1.3 m
Beam width	1.8 °
Platform	44 m above ground level

623

624 **Table 2 Specifications of disdrometer used in this study.**

Parameters	Value
Optical sensor wavelength	780 nm
Particle size range	0.2–5 mm (liquid precipitation), 0.2–25 mm (solid precipitation)
Particle velocity range	0.2–20 m s ⁻¹
Measurement time aggregation interval setting	1 min
Precipitation intensity range	0.001–1200 mm h ⁻¹
Radar reflectivity range	9.9–99 ± 20% dBZ

625

626 **Table 3 Impacts of the correcting different common errors on hourly accumulated**
 627 **rainfall.**

Statistic ¹	CC procedure	PC procedure ²				
		- AP	-Att	-BI	-Seg	-Z-R
<i>ra</i>	0.75	0.77	0.72	0.87	0.57	0.61
RMSE	1.95	1.97	2.02	3.18	2.17	2.34

628

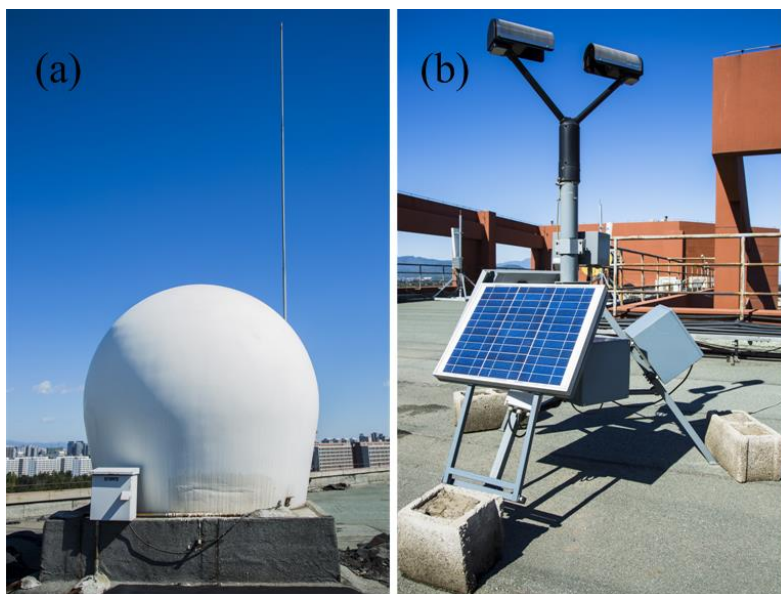
Notes:

- 629 1. The statistics are calculated with hourly rainfall estimates. *ra* is the average radar-gauge
 630 ratio for 8 gauges and $RMSE = \sqrt{\frac{1}{N} \sum_{n=1}^N (R_n - G_n)^2}$ is the root-mean-square error
 631 between the radar-based estimates *R* and gauge measurements *G* with *n* and *N* denoting
 632 the *n*-th hour and total number of hours, respectively.
- 633 2. The minus sign (-) in PC procedure indicates the exclusion of a specific correction. The
 634 correction names are simplified as follows: AP for anomalous propagations correction, Att
 635 for attenuation correction, BI for beam integration, Seg for convective–stratiform rainfall



636 classification, $Z-R$ for local $Z-R$ relationship derivation.

637



638

639 **Figure 1** The site view of (a) the Beijing Radar and (b) the disdrometer used in this

640 study.

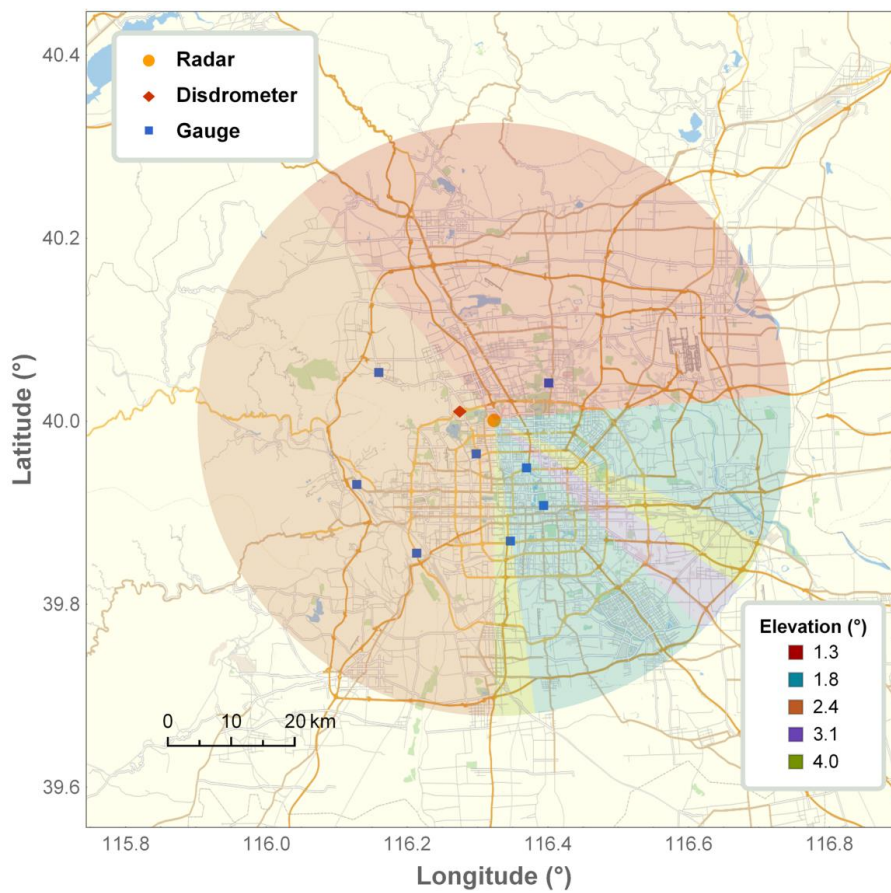
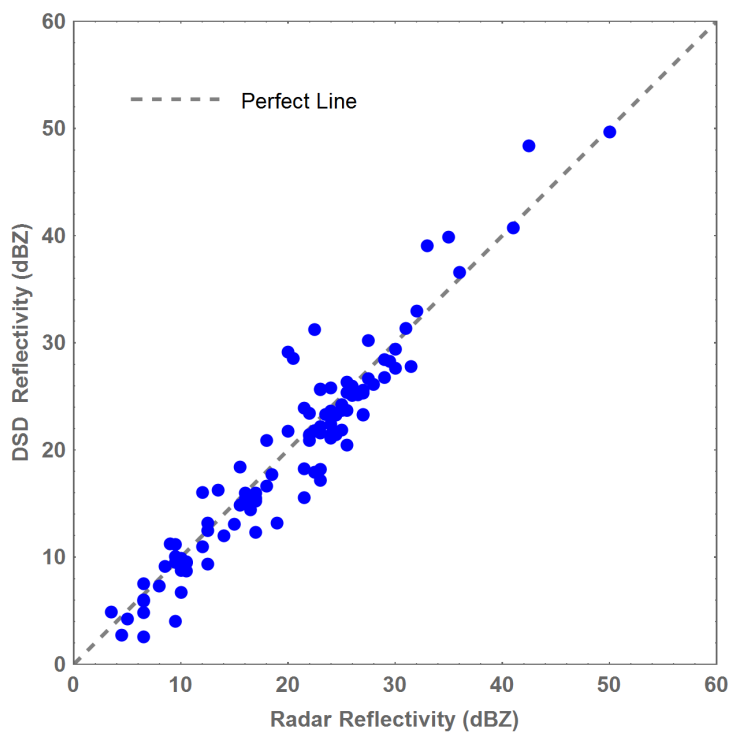


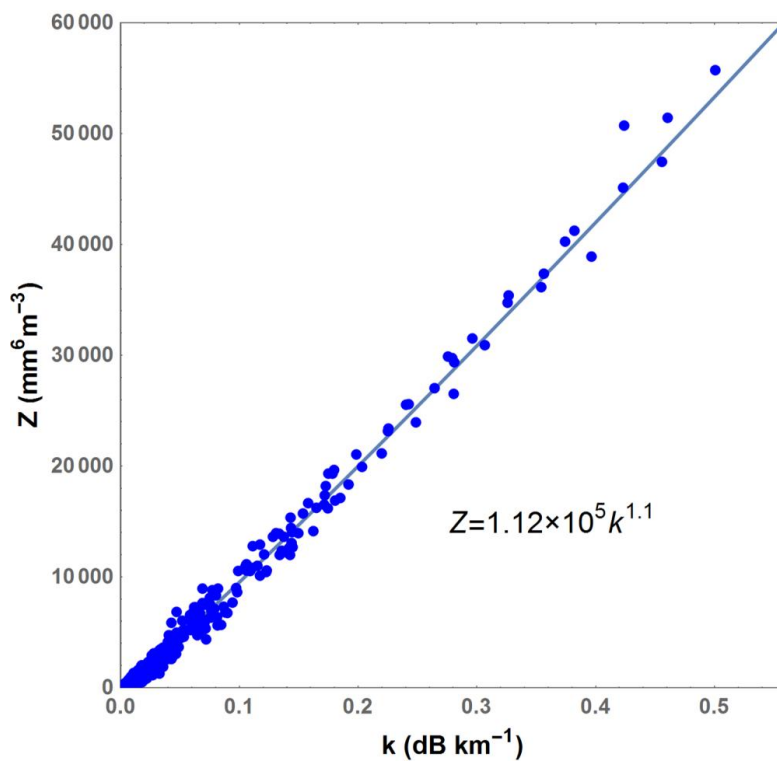
Figure 2 The instrumentation layout of urban rainfall monitoring system of in Beijing.



643

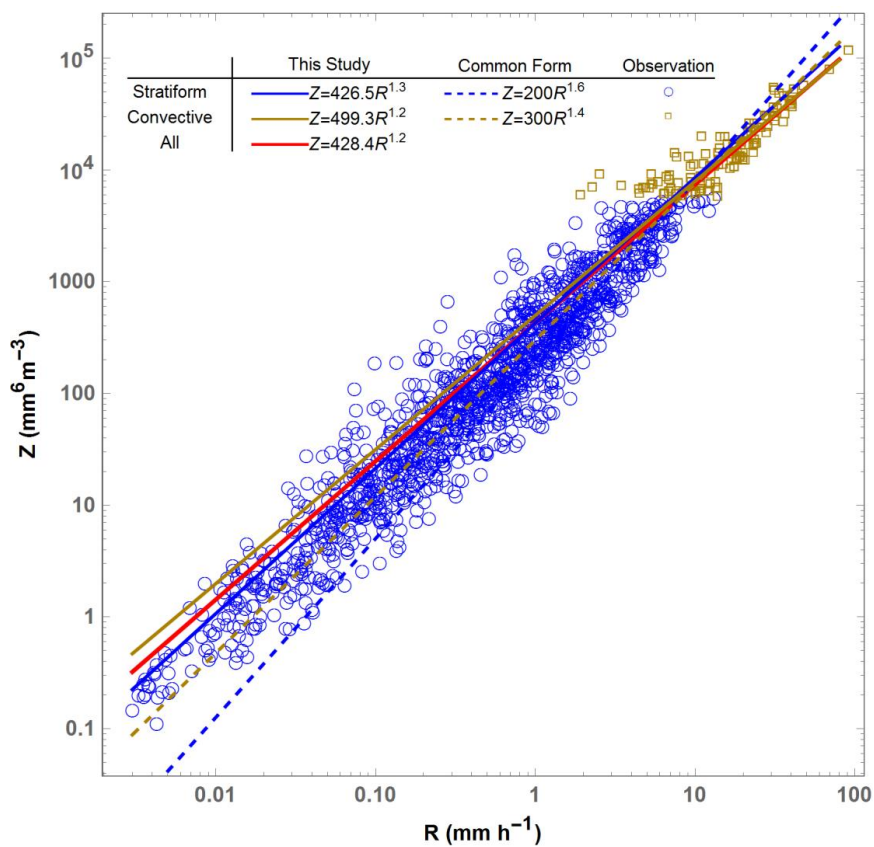
644 **Figure 3** The relationship between radar-measured reflectivity and distrometer-

645 estimated reflectivity.



646

647 **Figure 4** Z - k relationship derived from DSD data using a non-linear power-law fit.



648

649 **Figure 5** Z-R relationships for different rainfall scenarios.

650

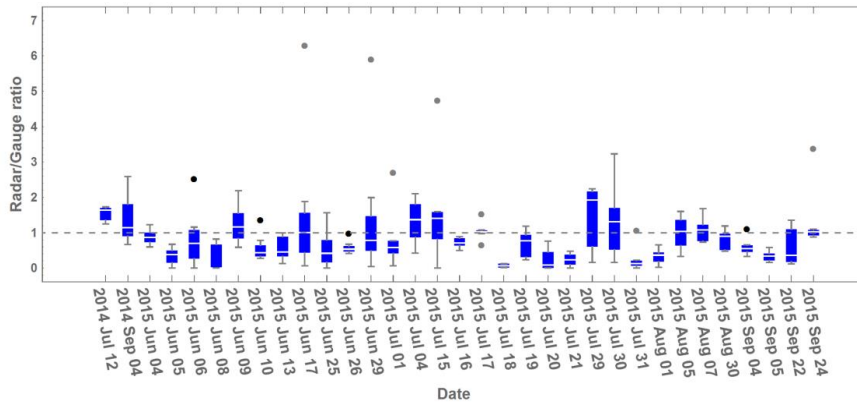
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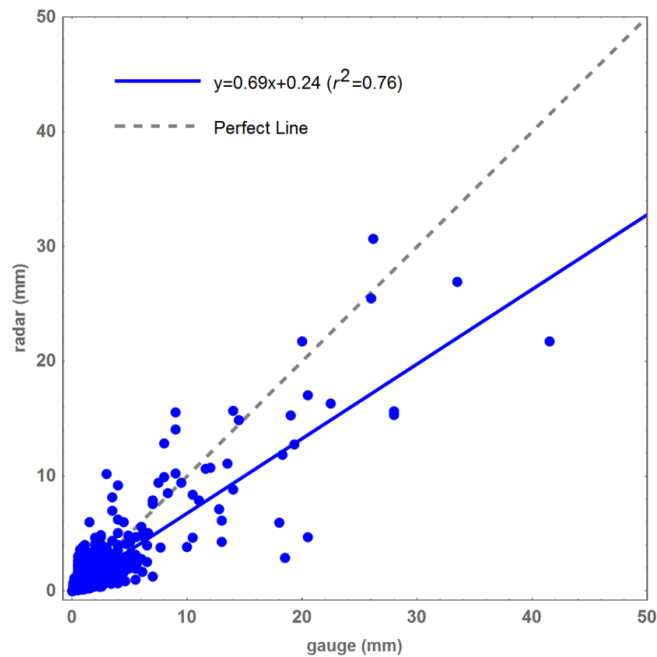
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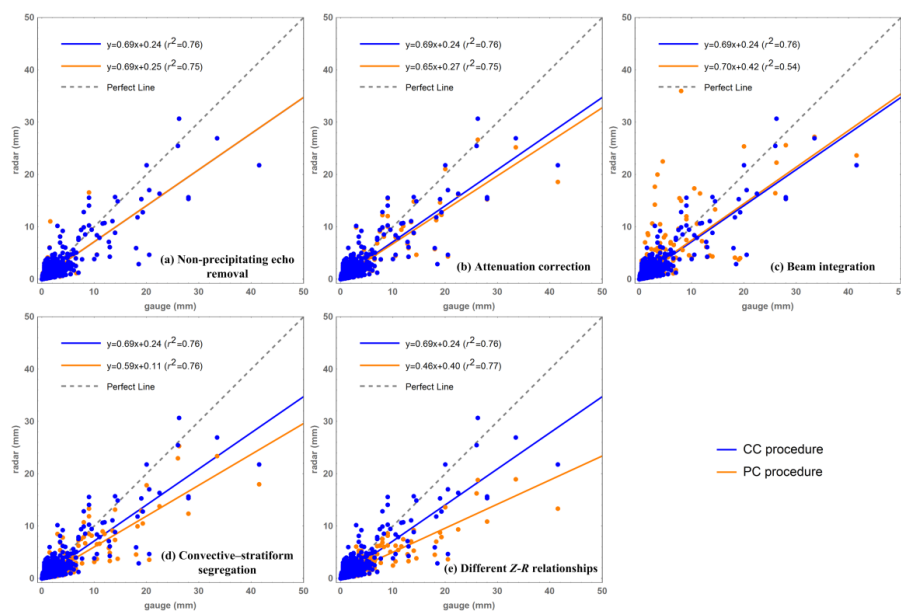
657 **Figure 6** Radar-gauge ratios of the daily accumulated rainfall for events covering at
658 least 3 gauges. The dots denote the outlier values. Each box ranges from the 25th
659 percentile to the 75th percentile with the middle line denoting the median value.

660



661

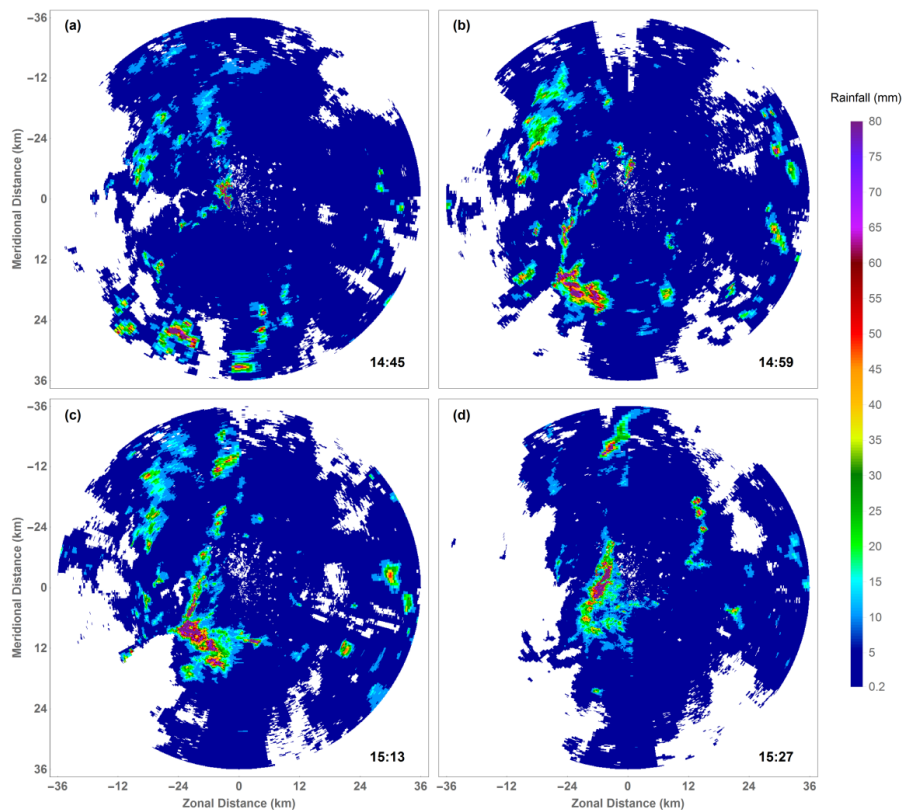
662 **Figure 7** The relationship of hourly rainfall accumulations from 8 rain gauges and the
663 corresponding radar pixels for all the events.



664

665 **Figure 8** Performance in radar-based rainfall estimation of different corrections: (a)
666 non-precipitation echo removal, (b) attenuation correction, (c) beam integration, (d)
667 convective-stratiform segregation, and (e) using different $Z-R$ relationships for
668 converting the reflectivity to rainfall intensity. The blue and orange dots show the
669 results of complete-correction and partial-correction procedures, respectively.

670

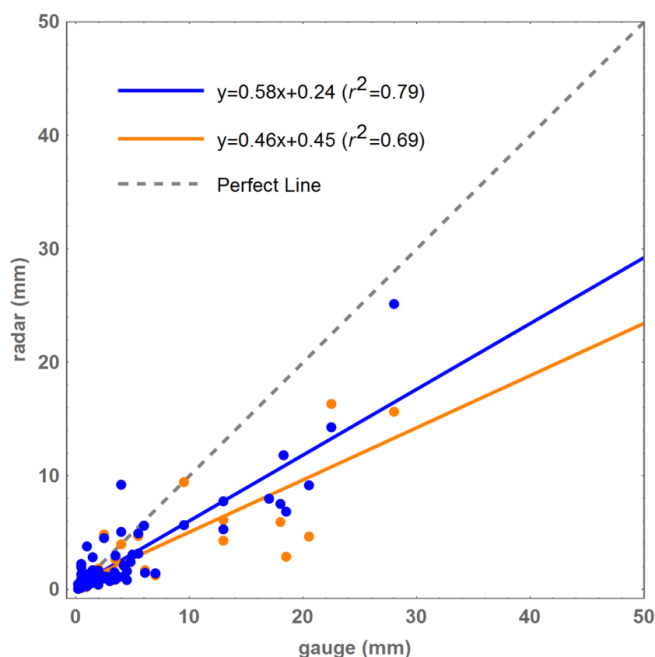


671

672 **Figure 9** Snapshots of the radar-based rainfall fields for the fast-moving rainfall event

673 of 4th September, 2015 at (a) 14:45, (b) 14:59, (c) 15:13 and (d) 15:27.

674



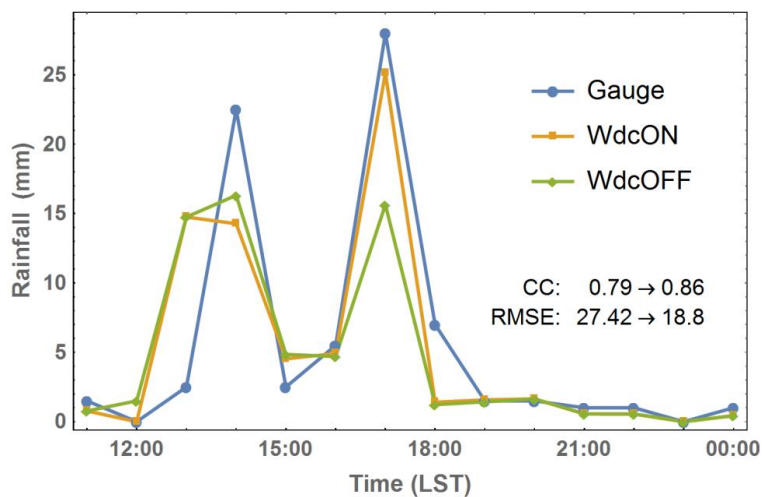
675

676 **Figure 10** Performance in radar-based rainfall estimation of the wind drift correction.

677 The blue and orange dots show the results of complete-correction and partial-correction

678 procedures, respectively.

679



680

681 **Figure 11** Rain gauge, QPE with wind drifting correction and QPE without wind



682 drifting correction rainfall time series for fast-moving event, 4th-5th September 2015
683 at the position of closest gauge to radar.
684