

## Supplementary Materials

### S1. Analyzer Calibration

#### *S1.1 TDLAS Calibration*

The TDLAS were calibrated at installation and each time the reference gas cylinder was replaced, per the procedure outlined in the user manual. That procedure is summarized below, with notes added specific to the present study.

The dominant sources of error in the TDLAS concentration measurement are the offset error caused by Fabry-Perot interference, and span errors caused by errors in reference gas analysis or by different pressure or temperature in the reference and sample cells. For eddy covariance measurements the mean concentration is subtracted; therefore the offset error cancels out and only the span errors are significant. The calibration process adjusts the span of the TDLAS.

The TDLAS span calibration requires the measurement of two calibration gases (details are given below). A five-way valve (Swagelok B-43ZF2) was used to switch between zero and span cylinders and filtered ambient air (to idle during setup). Flows and pressure regulators were adjusted to calibrate at the nominal sample cell pressure. The TDLAS parameter Reference gas concentration (ppm) was adjusted to correct the error in the measured concentration difference using:

$$C_{New} = C_{Orig} \left( \frac{T_S - T_Z}{M_S - M_Z} \right) \quad [S1]$$

where  $C_{\text{new}}$  is the corrected reference gas concentration parameter,  $C_{\text{orig}}$  is the original reference gas concentration parameter,  $T_s$  and  $T_z$  and the true span and zero concentration, and  $M_s$  and  $M_z$  are the measured span and zero concentrations.

The initial TDLAS calibration was performed 24 June 2015 using a span cylinder containing  $\text{CO}_2$  and  $\text{N}_2\text{O}$  in nitrogen rather than air, which can give rise to measurement error in IRGAs (Bischoff, 1974; Pearman and Garratt, 1975), and has also been shown to affect TDLAS (Bowling, et al. 2003). This cylinder was replaced with a cylinder of  $\text{CO}_2$  and  $\text{N}_2\text{O}$  in air for the subsequent calibrations on 23 February 2016 and 18 April 2016. A cylinder of nitrogen was used as zero gas throughout the experiment.

Measurements that infer total  $\text{CO}_2$  based on a single isotopologue can be affected by the isotope ratio, particularly when a minor isotope is measured (Tans, et al., 2017). Tans et al. (2017) derived a correction for  $^{12}\text{CO}_2$  analyzers used to quantify total  $\text{CO}_2$  when the sample has different isotopic content than the calibration gases. Adapting this approach to an analyzer that measures  $^{13}\text{CO}_2$ , and ignoring the relatively small effect of oxygen isotopes gives a simple approximate correction:

$$\frac{X_{\text{Cor}}}{X_{\text{Meas}}} = 1 + (\delta^{13}C_{st} - \delta^{13}C_{air})/1000 \quad [\text{S2}]$$

Sample bags (1 L Supel inert foil gas sampling bags with screw cap valve, Sigma-Aldrich, Bellefonte, PA) were filled from the zero and span cylinders used in the field experiment and analyzed at Campbell Scientific, Logan, UT. The samples in the bags were measured simultaneously by two TGA200As, one configured for  $\text{N}_2\text{O}$  and  $\text{CO}_2$  ( $^{13}\text{CO}_2$ ) and the other configured for isotopic  $\text{CO}_2$  ( $^{12}\text{CO}_2$ ,  $^{13}\text{CO}_2$ , and  $^{12}\text{C}^{18}\text{O}^{16}\text{O}$ ) measurements. During this test the TDLAS were calibrated using the two-point calibration method described in Bowling (2003).

A custom valve manifold (Campbell Scientific) switched between a sample bag, a cylinder of zero air (Airgas Ultra Zero grade), and a reference cylinder of unmodified natural air obtained from the WMO/GAW Central Calibration Laboratories (CCL) located at the NOAA Global Monitoring Division (GMD). This reference cylinder (serial number CB11313) was calibrated for N<sub>2</sub>O (WMO-N2O-X2006A mole fraction scale), CO<sub>2</sub> (WMO-CO2-X2007), and stable isotopes of CO<sub>2</sub> (VPDB scale, determined by IRMS by the Stable Isotope Laboratory, Institute of Arctic and Alpine Research, University of Colorado, Boulder (INSTAAR) (Trolier et al., 1996). Each gas was selected for 60 s, with 30 s of data omitted after valve switching for equilibration. Four cycles were recorded for each sample bag. A tee at the outlet of the manifold split the flow between the two TDLAS (100 ml min<sup>-1</sup> to each). The data were processed to give a mean for each sample bag. The resulting means and ranges for the samples of span gas and nitrogen are given in Table S1.

Table S1.. Mean and (range) of two sample bags for each cylinder. Values are also given for the reference cylinder used to calibrate the analyzers.

	CO <sub>2</sub> isotope TDLAS			$X_{Cor}/X_{Meas}$	N <sub>2</sub> O/CO <sub>2</sub> TDLAS	
	CO <sub>2</sub> (ppm)	$\delta^{13}C$ (‰)	$\delta^{18}O$ (‰)		CO <sub>2</sub> (ppm)	N <sub>2</sub> O (ppb)
Reference (CB11313)	400.38	-8.442	-3.194		-	328.81
Span in air	399.39 (0.42)	-37.00 (0.12)	-31.91 (0.02)	0.975	399.0 (0.6)	1001 (4)
Zero air (N <sub>2</sub> )	9.98 (0.32)	-206.0 (1.8)	-27.8 (4.7)		11.8 (0.4)	8 (1)

Ambient CO<sub>2</sub> has a  $\delta^{13}C$  of approximately -8 ‰, (Tans, et al., 2017) but it is the isotope ratio of the CO<sub>2</sub> flux that is of interest in the present study. Photosynthesis discriminates against the heavier isotopologue (<sup>13</sup>CO<sub>2</sub>) in favor of the lighter <sup>12</sup>CO<sub>2</sub>, and this discrimination depends on photosynthetic pathway (Farquhar, et al. 1989). O’Leary (1988) compiled results of

approximately 1000 measurements of plant material  $\delta^{13}\text{C}$ , showing that C4 plants generally range from -11 to -15 ‰ and C3 plants generally range from -23 to -31 ‰. Dercon et al. (2006) measured isotope ratios in corn plants grown over various water regimes and nitrogen availability, with ratios from -10.8 to -12.4 ‰. Griffis et al. (2005) directly measured the isotope ratio of daytime net flux (-11.6 ‰) and nighttime respiration (-12.5 ‰) during the growing season over corn in a corn/soybean rotation. We assume an isotope ratio of -12 ‰ for the  $\text{CO}_2$  fluxes in the present study. The correction factor  $X_{Cor}/X_{Meas}$  is given in table S1. for the span cylinder. Fluxes are multiplied by this factor in post-processing to account for this isotopic difference between the span cylinder and the fluxes.

### *S1.2 IRGA Calibration*

This CPEC200 system was equipped with the manufacturer's optional valve module and scrub module, and the CPEC200 program parameters were set to automatically run a zero and  $\text{CO}_2$  span sequence daily at 0:59 AM. This zero/span sequence is illustrated in Fig. S1, which shows the  $\text{CO}_2$  and  $\text{H}_2\text{O}$  concentrations measured by the EC155.

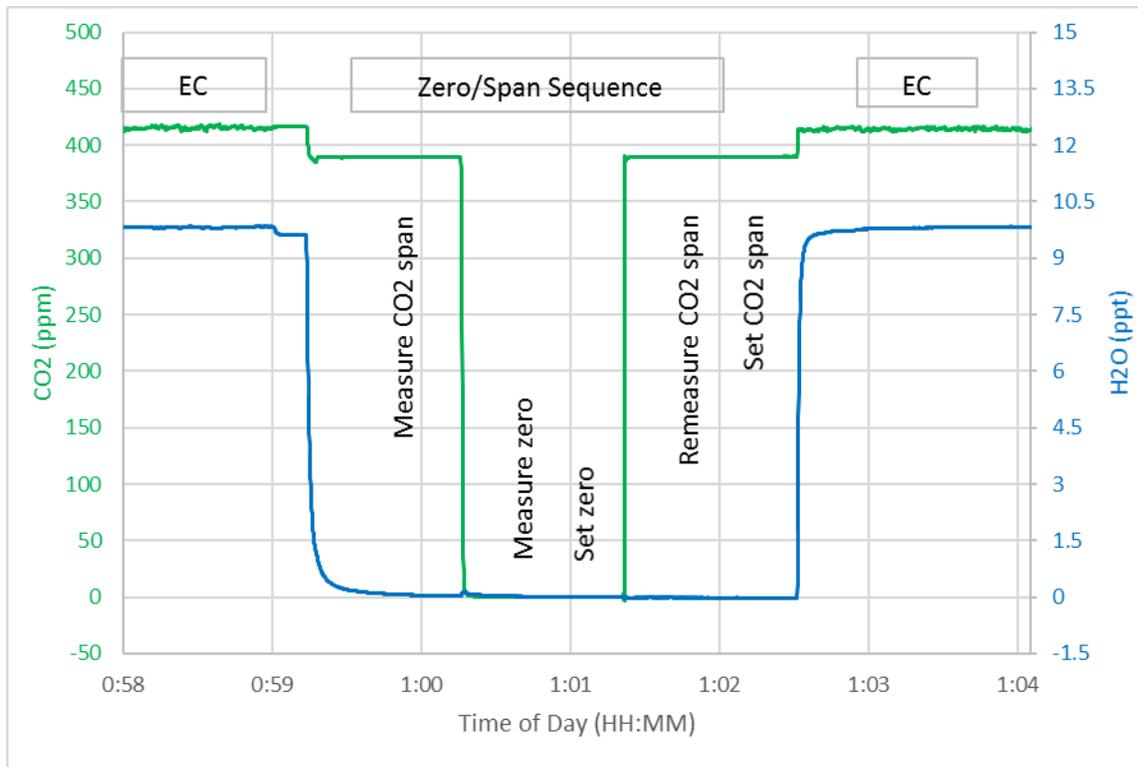


Figure S1. Example EC155 automated zero/span sequence.

The zero air for the IRGA calibration was supplied from a scrub module (part number 27423, Campbell Scientific, Inc., Logan UT) that includes a small diaphragm pump and a 3-stage scrubber using molecular sieve (CSI pn 27450, molecular sieve 13X, 1.6 – 2.5 mm beads, 250 g or VWR pn AAB21109-30). The scrub module removes CO<sub>2</sub> and H<sub>2</sub>O from ambient air and pushes it to the EC155 at approximately 1.5 L min<sup>-1</sup>. At beginning of the experiment the scrub module was refilled with a fresh molecular sieve. The scrub module received no maintenance over the entire campaign (1.5 years), although replacement of the molecular sieve is recommended annually. At the end of the experiment the scrub module was tested by setting the zero and span of the EC155 using ultrazero grade air, reference cylinder CB11313 (Table S2), and a dewpoint generator (LI-610, LI-COR). A zero-air generator (pn 31022, Campbell Scientific, Inc.) was compared to the cylinder of zero air. The CO<sub>2</sub> agreed within 0.01 ppm and

the H<sub>2</sub>O agreed within 0.03 ppt, giving high confidence in the quality of the cylinder of zero air. The EC155 was then used to measure the output from each of the three stages of molecular sieve in the scrub module. The results are given in Table S2. The first stage allowed approximately half of ambient CO<sub>2</sub> to pass through, indicating the need to replace its molecular sieve. The second stage removed nearly all the remaining CO<sub>2</sub>, but the final stage actually increased the CO<sub>2</sub>, to 2.45 ppm. This was likely due to the outlet of the scrub module being uncapped for 2 months after the field campaign and before testing. After standard maintenance (replacing molecular sieve in the first bottle and rotating this to become the final stage), the scrub module removed all the CO<sub>2</sub>. Molecular sieve has a higher capacity for removing H<sub>2</sub>O than CO<sub>2</sub>. Residual H<sub>2</sub>O was very low in every case.

Table S2. CO<sub>2</sub> and H<sub>2</sub>O in the air from the scrub module.

	CO <sub>2</sub> (ppm)	H <sub>2</sub> O (ppt)
First stage	251.7	0.085
Second stage	0.95	0.051
Third stage	2.45	0.044
After service	-0.05	0.035

The EC155 CO<sub>2</sub> span cylinder was CO<sub>2</sub> balanced in nitrogen. The effect of an N<sub>2</sub>-balanced cylinder as opposed to the recommended air-balance (Zhao, et al., 1997), as well as isotopic differences between the span and sample gases (Tans et al., 2017) on the calibration values was tested after completion of the field experiment.

Samples of this span cylinder were sent to CSI, Logan UT, for analysis. The EC155 was zeroed using ultrazero air and the CO<sub>2</sub> span was set using a cylinder of natural air (CB11313, see Table S1). The sample of the CO<sub>2</sub> span cylinder was measured and found to be 401.98 ppm.

During the field experiment the CO<sub>2</sub> span parameter in the CPEC200 software was set to a preliminary value of 390 ppm. In postprocessing, fluxes measured by the EC155 were multiplied by a correction factor:  $401.98/390 = 1.0307$ . This corrected any errors due to carrier gas or isotope ratios.

### *SI.3 References*

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