

## Temperature correction methodology

The corrected irradiance  $I(\lambda)$  at each wavelength  $\lambda$ , is derived by dividing the measured signal  $I_m(\lambda)$  with the provided correction factor  $cf(\lambda)$ :

$$I(\lambda) = I_m(\lambda) / cf(\lambda) \quad (1)$$

For the three different TRs (TR1, TR2, TR3), different correction factors are used ( $cf_1(\lambda)$ ,  $cf_2(\lambda)$  and  $cf_3(\lambda)$  respectively). Assuming that the limit that separates TR1 from TR2 is  $T_{12}$  and the limit that separates TR2 from TR3 is  $T_{23}$ , that the reference temperature  $T_r$  is above  $T_{12}$  and that the measured temperature is  $T$ , the correction factor for each TR is calculated as follows:

### **If T is in TR3:**

$$cf_3(\lambda) = 1 + c_3(\lambda) \cdot (T - T_r) \quad (2)$$

### **If T is in TR2**

$$cf_2(\lambda) = 1 + c_3(\lambda) \cdot (T_{23} - T_r) + c_2(\lambda) \cdot (T - T_{23}) \quad (3)$$

### **If T is in TR1**

$$cf_1(\lambda) = 1 + c_3(\lambda) \cdot (T_{23} - T_r) + c_2(\lambda) \cdot (T_{12} - T_{23}) + c_1(\lambda) \cdot (T - T_{12}) \quad (4)$$

The factors  $c_i$  represent the slopes of the linear fits that describe the change of the response relative to its mean value at 25°C. For TR1 and TR3 the slopes are considered to be equal, thus  $c_1 = c_3$ . The slopes are calculated using the 2<sup>nd</sup> degree polynomials of the form:

$$c_i = a_0 + a_1 \cdot \lambda + a_2 \cdot \lambda^2 \quad (5)$$

Where  $\lambda$  is in nm.

For each of the eight Brewers the coefficients  $a_i$  are listed in Table 1:

**Table 1:** Polynomial coefficients for the calculation of the factors  $c_i$

	$c_2$			$c_3$		
	$a_0$	$a_1$	$a_2$	$a_0$	$a_1$	$a_2$
B005	$4.7435 \cdot 10^{-6}$	$-2.9025 \cdot 10^{-3}$	$4.4893 \cdot 10^{-1}$	$2.3101 \cdot 10^{-7}$	$-9.5882 \cdot 10^{-5}$	$7.9069 \cdot 10^{-3}$
B030	$1.3444 \cdot 10^{-7}$	$-1.3833 \cdot 10^{-4}$	$3.1543 \cdot 10^{-2}$	$4.0561 \cdot 10^{-6}$	$-2.4422 \cdot 10^{-3}$	$3.6563 \cdot 10^{-1}$
B037	$7.6786 \cdot 10^{-7}$	$-4.3741 \cdot 10^{-4}$	$6.5404 \cdot 10^{-2}$	$-1.0034 \cdot 10^{-6}$	$6.8329 \cdot 10^{-4}$	$-1.1733 \cdot 10^{-1}$
B078	$-1.6146 \cdot 10^{-6}$	$1.0147 \cdot 10^{-3}$	$-1.5890 \cdot 10^{-1}$	$-9.4557 \cdot 10^{-7}$	$6.2536 \cdot 10^{-4}$	$-1.0490 \cdot 10^{-1}$
B086	$2.6727 \cdot 10^{-8}$	$-4.0802 \cdot 10^{-6}$	$5.8431 \cdot 10^{-4}$	$5.4584 \cdot 10^{-7}$	$-3.3678 \cdot 10^{-4}$	$5.0069 \cdot 10^{-2}$
B107	$1.6346 \cdot 10^{-7}$	$-8.3061 \cdot 10^{-5}$	$1.2845 \cdot 10^{-2}$	$2.1427 \cdot 10^{-7}$	$-9.6526 \cdot 10^{-5}$	$8.6595 \cdot 10^{-3}$
B185	$-1.9244 \cdot 10^{-7}$	$1.1939 \cdot 10^{-4}$	$-1.7469 \cdot 10^{-2}$	$-1.9286 \cdot 10^{-7}$	$1.1823 \cdot 10^{-4}$	$-1.8323 \cdot 10^{-2}$
B214	$-1.4453 \cdot 10^{-7}$	$9.4794 \cdot 10^{-5}$	$-1.4689 \cdot 10^{-2}$	$2.9582 \cdot 10^{-7}$	$-1.8451 \cdot 10^{-4}$	$2.7264 \cdot 10^{-2}$