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We thank Professor Genthon for reviewing the manuscript.

This paper demonstrates that an original algorithm used in the Total Precipitation sensor TPS-3100 also called “hotplate” to derive quantities of precipitation has some errors that can be corrected, and has shortcomings that can be reduced. This is based on both theoretical and experimental approaches. The Hotplate concept uses an original method to quantify precipitation: the differential energy needed to keep 2 overlaid hotplates at constant temperature, one facing up and the other facing down, includes the contribution (latent heat) needed to evaporate any condensed water falling on the upper plate (but obviously not affecting the lower plate facing down). There are many other terms to account for though. Both plates lose sensible energy and the loss rate is related to wind speed and ambient temperature.

However the 2 plates are equally affected so the differential is 0. On the other hand, the radiation balance of the 2 plates is not necessarily the same and the differential must be accounted for. The issue of the catch efficiency of the instrument is also raised, particularly for solid particles.

The hotplate concept is very attractive for a number of reasons listed in the paper, including the fact that it is immune to frost deposition and snow/frost clogging, thus particularly appropriate in cold regions. Yet, although the instrument is not new (marketed by YES since the early 2000’s), it does not seem to be so widely used (the paper mentions that “70 Yankee Environmental Systems (YES) hotplate precipitation gauges have been purchased by researchers and operational meteorologists” which is not a lot). This may (or may not, price is also an issue of course) sign some dissatisfaction with the results obtained, and an improvement of the algorithm may contribute to popularize the instrument.

If the approach and methods appear sound, there is one potential major shortfall with the paper: it is not obvious if and how the revised algorithm can be implemented in an existing unit. This is admittedly a technical issue but this is “atmospheric measurement techniques” so one expects technical issues to be addressed.

33           The paper mentions that the hotplate outputs data in 2 files, one (UHP)  
34 which “is provided to all YES customers” and the other (SHP) with no indication  
35 how it can be accessed. Of course the later has the data needed to design and use a  
36 new algorithm but there is no reference to the second file in the YES Hotplate  
37 documentation as of 2011.

38           We asked Roy Rasmussen at the National Center for Atmospheric Research  
39 (NCAR) for access to the SHP data and were granted access after signing a legal  
40 agreement that protects the real time processor from piracy. We have presented  
41 analyses of SHP data in two theses, and now, in this manuscript in AMTD.

42           Here is how we will revise section 2.1:

### 43           2.1 - Hotplate Data Files

44           The hotplate outputs data to two files. The previously discussed  $Q_{top}$  and  $Q_{bot}$  are  
45 two of several recorded variables and both of these are essential for the analysis  
46 described here. One of the files is known as the UHP or “user” hotplate file. The  
47 UHP file is provided to all YES customers. The second file is the SHP or “sensor”  
48 file. The SHP file is proprietary but we were granted access to it by the National  
49 Center for Atmospheric Research (NCAR; Boulder, CO). Table 1 has the list of all  
50 recorded variables and how some of these are symbolized. A complete list of  
51 variables (measured and computed), and constants, is provided in the Appendix.  
52 With the exception of Unix time, all variables in Table 1 are provided as 60-s  
53 running averages, sampled at 1 Hz (YES, 2011).

54           YES no longer markets the instrument and no longer provides any  
55 information on its web site. In such a paper, one should not have to bet on  
56 obtaining “private communication” from a manufacturer which has terminated  
57 production, to learn how to access the data needed to implement the improved  
58 algorithm.

59           As we understand it, termination of production/marketing is temporary and occurred  
60 because of a legal argument between UCAR and YES. Currently, YES is servicing  
61 our hotplate.

62

63 I believe that the paper has very limited significance and is not acceptable  
64 for publication in its current form unless this information, and all information  
65 necessary to implement the new algorithm, is clearly provided.

66 We want to probe your comment in the last sentence. Are you saying that more  
67 information about the UW Algorithm is needed? It is our opinion that we provided  
68 enough for a user to implement the UW algorithm, provided they have access to the  
69 SHP data. Also, please see our previous statement that we will revise section 2.1 to  
70 include discussion of how the SHP data was accessed.

71

72 On the other hand, it definitively ranks publication status if the information  
73 is given so that the reader can implemented the new algorithm, and provided the  
74 various issues bellow are addressed, some of which are fairly serious though.

75 1) The introduction (lines 33 – 37) states that 2 types of instrumentations to  
76 measure precipitation have been developed: the capture and optical gauges. This  
77 ignores radars which are powerful tools to measure and even profile precipitation.  
78 Because of ground clutter and vertical resolution, radars do admittedly not  
79 measure precipitation right at the very surface but because they can profile  
80 vertically it may be checked whether precipitation rates vary or not as it reaches  
81 closer to the surface. Radars do not “obstruct the wind and deflects falling particles  
82 in the measurement zone” (line 38). There is no “clogging with snow” with radars  
83 (line 47).

84 In the US National Weather Service (NWS) network, a radar-derived snow amount  
85 is dependent on gauge measurements made simultaneous with the radar  
86 measurements. A published example of this is the NWS gauge-radar network data  
87 analyzed by Martinaitis et al. (2015). In that network, and presumably others, the  
88 gauge-calibrated radar-derived estimates of snow can be significantly biased.  
89 Factors contributing to this are gauge clogging by snowfall, postevent thaw of snow,  
90 and underestimation of snow because wind speed is either not used to correct for  
91 gauge undercatch or it is unavailable. Martinaitis et al. (2015) state that “..The  
92 accuracy of hourly radar-derived QPE values of winter precipitation is unknown..”.  
93 Given this caveat, the dependence of radar precipitation estimates on gauge  
94 measurements, and the factors you mention (vertical structure, Earth curvature, ray  
95 ducting, ground clutter, and etc.), we have opted to not mention that radars can be  
96 used to derive snowfall amounts.

97  
98 Martinaitis, S.M., S.B.Cocks, Y.Qi, B.T.Kaney, J.Zhang, and K.Howard, Understanding  
99 winter precipitation impacts on automated gauge observations within a real-time  
100 system, J. Hydrometeor., 16, 2345-2363, [https://doi.org/10.1175/JHM-D-15-](https://doi.org/10.1175/JHM-D-15-0020.1)  
101 [0020.1](https://doi.org/10.1175/JHM-D-15-0020.1), 2015  
102

103 Equation (3) (lines 113 – 120) describes the improvement of the algorithm  
104 by the authors by taking into account the solar and thermal radiation contributions  
105 the heat balance of the upper plate. Except for the latent heat term, one would  
106 expect a similar expression for the lower plate but this is not explicit. Because the  
107 hotplate is immune from snow and frost related problems that affect other  
108 sensors, it is expected particularly useful in cold snowy regions but then comes in  
109 the short wave power input reflected by the surface. If the sensor only measures  
110 the downwelling solar radiation, how is the reflected part factored in the lower  
111 plate energy balance?

112 Rasmussen et al. (2011) factored bottom plate power and ambient temperature, both  
113 measured at 2 m AGL, into a function that was regressed against wind speeds  
114 measured at 10 m AGL. This is evident in section 3a of their paper. Because the  
115 bottom plate power is affected by wind, snow-reflected solar, and longwave  
116 exchange, they have accounted for (implicitly) the effect you are referring to.

117

118 We hope that Professor Rasmussen and Mark Beaubien at YES can comment more  
119 on this.

120

121           Line 103: the sensible term is a function of U and T. Figure 1 shows that the  
122 temperature sensor is very poorly shaded from solar radiation reflected by the  
123 surface. Over a snow covered surface this is a likely major problem. The authors  
124 should evaluate the impact on precipitation estimation over snow, possibly bring in  
125 an empirical correction?

126   In Table R-1 we estimate this error for nonprecipitating conditions. Here the type-1  
127 accumulations are evaluated using the UW algorithm and the type-2 accumulations  
128 are evaluated by substituting into the UW algorithm coincident temperature  
129 measurements made within a shielded temperature sensor (Vaisala WXT520).  
130 Results are presented for four days. The reported liquid equivalent accumulations  
131 are derived by integrating liquid equivalent rates from 16 to 20 UTC (10 to 14 LT).  
132 The table shows that positive bias in type-1, relative to type-2, is no larger than 1.4  
133 liquid equivalent mm in four hours. Further, it needs to be acknowledged that solar  
134 is attenuated when precipitation is occurring, and thus the effect of sensor heating on  
135 precipitation measurements is smaller than demonstrated in Table R-1. In our  
136 opinion, more analysis is needed to explain and quantify this effect for both  
137 precipitating and nonprecipitating periods. Thus, we feel that the reviewer's  
138 recommendation is beyond the scope of the manuscript.

139

140 Table R-1 - Accumulations derived for nonprecipitating four-hour daytime cases; 16 to  
141 20 Universal Coordinated Time (10 to 14 LT). Measurements are from the UW hotplate  
142 operated at the Medicine Bow Mountain Site described in Zelasko (2017).

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UTC Year Month Day	20170128	20170129	20170130	20170131
Type-1 <sup>a</sup> Accumulation, mm <sup>c</sup>	1.7	1.7	1.8	1.4
Type-2 <sup>b</sup> Accumulation, mm <sup>c</sup>	0.5	0.7	0.4	0.1

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152 <sup>a</sup> Type-1 are liquid-equivalent four-hour accumulations derived from UW hotplate  
153 measurements using the UW processing algorithm

154

155 <sup>b</sup> Type-2 are liquid-equivalent four-hour accumulations derived from UW hotplate measurements  
156 using the UW processing algorithm with Vaisala WXT520 temperatures substituted for  
157 YES temperatures

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159 <sup>c</sup> The accumulation unit is liquid-equivalent depth over four hours (16 to 20 UTC)

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163 Zelasko, N., Orographic Precipitation in Southeastern Wyoming, MS Thesis,  
164 Department of Atmospheric Science, University of Wyoming, 2017

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168           Then, according to line 202, the upwelling IR is also estimated from this  
169 temperature supposed to be the ambient air temperature, but probably largely  
170 overestimated over snow.

171   The term is overestimated by sensor heating (Wolfe and Snider, 2012, their section  
172 2c), however, the term contributes is less than 3 % to the power budget. This is  
173 demonstrated below (Figure R-1) for the same nonprecipitating daytime cases as in  
174 Table R-1. Furthermore, during precipitation the solar is attenuated, and thus the  
175 magnitude of the error is less than that for these nonprecipitating cases.

176

177   Wolfe, J.P., and J.R.Snider, A Relationship between Reflectivity and Snow Rate for  
178           a High-Altitude S-Band Radar, J. Appl. Meteor. Climatol., 51, 1111–1128,  
179           2012

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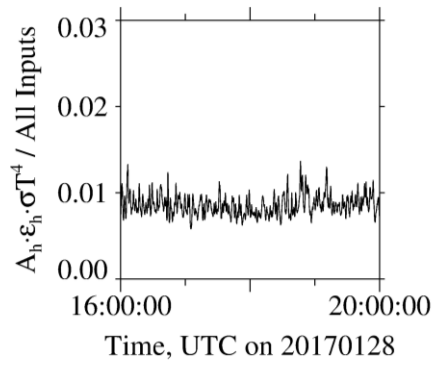
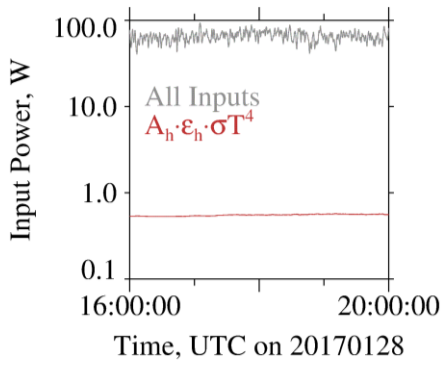
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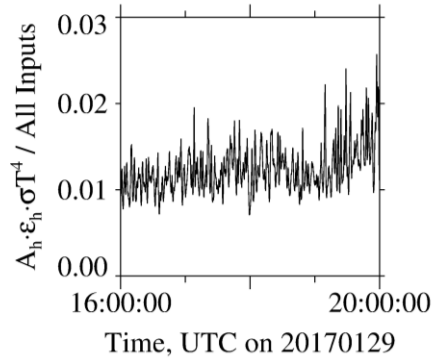
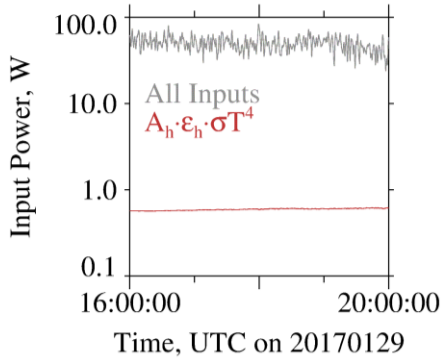
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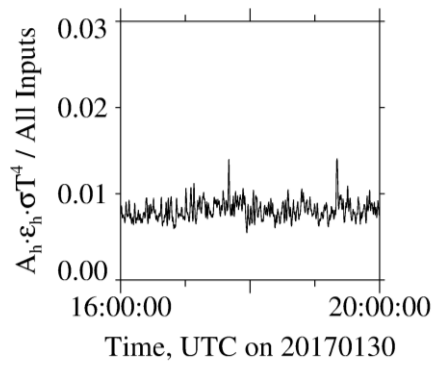
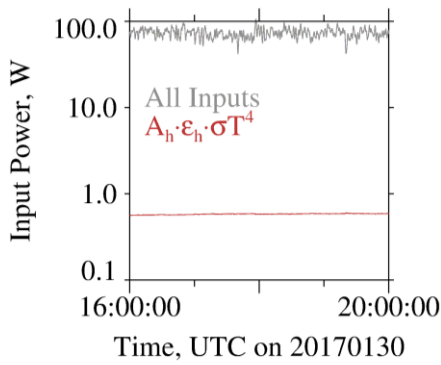
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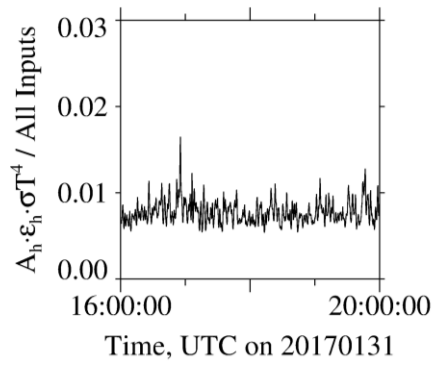
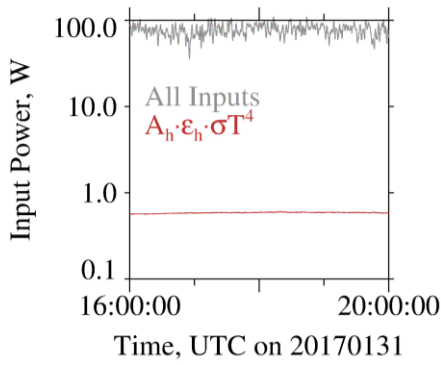
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Figure R-1 – Left) Time sequence of  $A_h \cdot \epsilon_h \cdot \sigma T^4$ . Also plotted is the sum of all input terms in the power budget. Right) Ratio  $A_h \cdot \epsilon_h \cdot \sigma T^4$  divided by all inputs. Results are for the nonprecipitating daytime cases. The field site is described in (Zelasko, 2017).

206 Line 3176: Define AGL (presumably Above Ground Level)

207 **In the revision, we will define AGL.**

208 Line 376: How would a “violation of the steady state assumption” could  
209 explain the delay? Would this have to do with thermal inertia?

210 **We do not see a “delay”, rather a “slowed response”. Two things are contributing to this.**  
211 **1) Each 1-s sample is a 60 s running average (see L131 and L977 in the manuscript), and**  
212 **2) thermal inertia. Better understanding of the thermal inertia will require power**  
213 **measurements that are not 60-s averaged. We have asked YES for this.**

214 Lines 422 – 423: This is not clear: the authors use data derived for a flow  
215 perpendicular to the plates to determine parameters for a flow parallel to the  
216 plates? Does this make sense? Can you clarify?

217 **Hansen and Webb (1992) is the only publication, we are aware of, that reports**  
218 **experimentally-derived values of  $\alpha$  and  $\beta$  for a circular plate with concentric rings.**  
219 **And yes, the airflow in Hansen and Webb (1992) was perpendicular (normal to) the**  
220 **plate surface. We did *not* mean to imply that the values of  $\alpha$  and  $\beta$  determined by**  
221 **Hansen and Webb (1992) were used in our analysis.**

222 **Here are revisions that should clarify the sentence on L420:**

223 **This result is based on UW hotplate measurements, acquired at the GLE site, and**  
224 **formulas developed in section 3.6.**

225 **Revision for L227 to L229.**

226 **In this section, we develop a relationship between  $Nu$  and  $Re$  based on**  
227 **measurements recorded in the field when precipitation was not occurring; in a later**  
228 **section we show how that relationship is applied in the new algorithm.**

229

230 Table 1: "Hotplate data files". This table is misleading has long as access to  
231 SHP data is not explicit.

232 We apologize for not stating how we acquired the SHP data. As discussed above,  
233 we plan to revise section 2.1 so this is clear.

234 Lines 527-530: A synthesis table describing the various algorithms  
235 referenced in the paper could be useful. Only here does one clearly realize that  
236 none of the above algo discussion applies to the commercial (YES) one. The  
237 average hotplate user, presumably a target reader, probably got his/her  
238 instrument from YES and expects he/she will be able to improve his/her instrument  
239 with the new algo. It is not necessarily obvious from the beginning that R11 is not  
240 YES algo and that the authors describe an algo which objectively improve over R11  
241 but not necessarily over the commercial units. Improvement over the commercial  
242 algo is verified only in the end. This should be clearly stated from the very  
243 beginning.

244 On L268-L274, near the beginning of the manuscript, we stated that we **assumed**  
245 that the YES algorithm has incorporated R11's surface area and R11's distinction  
246 between the theoretical and actual conversion factors. At present, we do not know if  
247 these effects are actually incorporated into the YES algorithm.

248

249 We do not think that a synthesis table is necessary. If the reviewer is insistent, we  
250 think it should go toward the end of the manuscript.