## Response to Reviewer Comments for the manuscript: "Airborne Measurements of CO<sub>2</sub> Column Concentrations made with a Pulsed IPDA Lidar using a Multiple-Wavelength-Locked Laser and HgCdTe APD Detector, " by James B Abshire et al. Manuscript #: AMT 2017-360

February 8, 2018

Response to Reviewer 1:

Thank you for the careful review of the manuscript and for your helpful comments. We have updated the manuscript to address all your comments below. In the attached version of the manuscript for the reviewers, all the changes made are highlighted in yellow. I have briefly addressed each comment below as well.

## Referee #1 comments:

This is a descriptive overview manuscript on the topic of the NASA Goddard CO2 Sounder lidar, the retrieval algorithm, and associated data product examples from two airborne campaigns. These campaigns each consisted of multiple flights and took place in the years 2014 and 2016. The accompanying figures (photos, graphics) are informative. In general it's a well-organized paper that should be of interest to a large segment of the readers. Here are a few comments and questions relating to spots where clarification would be helpful.

1.1 Section 3, line 40: Here reference is made to the optical bandpass filters and accompanying Figure 5. It isn't clear why the 2014 filter was not used in the 2016 flights. The 2016 filter appears to be worse in terms of variability of transmission vs. wavelength.

The text was updated to address question.

1.2 Section 4: Figure 8 is an informative diagram of the retrieval algorithm. It is stated on the figure and on page 5, line 38, that the initial computation assumes a vertically uniform mixing ratio.

No action was requested.

1.3 Later, page 6, line 13, in the paragraph devoted to "clumped fitting", it is stated that clumped fitting "solves for terms like the XCO2 vertical gradient." Please expand on how this is accomplished.

1.4 Section 4: The clumped fitting appears to be an important step, mitigating several potential sources of bias. It would be helpful to expand on this.

Also, can you cite one or more references relevant to the multi-pixel approach used by OCO-2 or AIRS?

Added a subsection on clumped fitting, with the requested additional references.

1.5 Section 6 and Figure 11: Figure 11, cited on page 5, line 46, is difficult to interpret. 1.5 a First, it would help to enlarge it. The figure was enlarged.

1.5b Also, it's not clear from the legend and the plots which is the lidar range and which is the ground elevation. The labels were clarified.

1.5c What is the source of the ground elevation numbers? Is it ground elevation or scattering surface elevation from the altimetry? Since SF1 is over the redwoods, this is a case where the potential capability of the lidar to distinguish the optical scattering surface elevation from the ground elevation should become apparent, provided that accurate measurements can be made over short distance scales.

This was clarified in the text.

1.6 Table 3: This table lists a few numbers from "mean slant range" and "ground elevation" These appear to be averages over each of the fixed altitude segments. As such, they are averages over several km. Correct? What do we learn from these numbers?

The text was updated with the explanation.

## Response to Reviewer Comments for the manuscript: "Airborne Measurements of CO<sub>2</sub> Column Concentrations made with a Pulsed IPDA Lidar using a Multiple-Wavelength-Locked Laser and HgCdTe APD Detector, " by James B Abshire et al. Manuscript #: AMT 2017-360

February 8, 2018

## Response to Reviewer 2:

Thank you for the careful and detailed review of the manuscript and for your many helpful comments. We have updated the manuscript to address all your comments below. We feel they have substantially improved the manuscript. In the attached version of the manuscript for the reviewers, all the changes made are highlighted in yellow. I have briefly addressed each comment below as well.

## Reviewer 2 comments:

This paper successfully details the results of the XCO2 dataset produced by the CO2 Sounder lidar during its 2014 and 2016 ASCENDS flights. It does a nice job of detailing the motivation and science goals of the ASCENDS mission, the CO2 Sounder lidar's role in that mission, the current state of lidar technology, and the CO2 Sounder's performance in the 2014 and 2016 flights. The paper is readable, and flows well, even in more technical sections such as the instrument setup and retrieval algorithm description. The included figures are, overall, very informative and helpful.

2.1a However, I would argue that the paper currently lacks a scientific punch. Providing more context for the instrument performance would help better communicate the scientific and technological impact of the results.

This was added in several different places as recommended in the detailed comments.

2.1b Placing stronger emphasis on past instrument performance, and thus on the improvements in data quality since 2011, would help readers appreciate the instrument's achievements. For example, specific comparisons of 2014/16 noise or in situ bias to 2011 flight legs of similar altitudes; to 2011 spirals.

This was added in several different places as recommended in the detailed comments.

2.1c Repetition of specific precision and accuracy improvements throughout the text can only improve readers' impression of the instrument progress.

These were added in several different places as recommended in the detailed comments.

## General comments:

2.2 While the paper does a good job of giving the broad science background for the instrument, a background on past instrument performance would lend important context to the quality of the results. One way to achieve this would be to include a paragraph on past campaign data in the technical background section (section 2). This could also be its own section between sections 2 and 3.

This was added at the end of Section 2.

2.3 There are several places throughout the text where comparing the 2014 and 2016 data to earlier data would help emphasize the how effective the instrument improvements have been. The abstract, for example, should mention the "five-fold improvement in precision over measurements made in 2011." This is likely the most important take-away message in the entire paper, but is not even given in the abstract. (And, it should be noted, perhaps this number would have be 7.5x better, instead of 5, if not for the "noisy reference voltage"?) This statistic packs a punch, and would draw readers in.

These performance comparisons were added in the abstract, summary and in the campaign discussions. Also I re-examined the comparison of the precisions of 2011 vs 2016 campaigns listed in the tables of the respective papers. These showed found the improvement in precision (for 1 second averaging) for 2016 vs 2011 was actually x9. The numbers in the text were updated correspondingly.

2.4a Remarking on the feasibility of the CO2 Sounder lidar as a future space-based instrument in the abstract, as well, rather than just saying that this study serves as a demonstration of its feasibility, would be a good lead-in for potential readers.

Updates were made to the abstract, discussion and summary.

2.4b How close are you, in some kind of phase space, to technical readiness for a space-based version? Are you there on detectors, or are you a factor of 10 away? Are you there on laser power, or are you a factor of ten away?

These aspects of the discussion section were updated as recommended.

2.5 Throughout the rest of the text, I might recommend pulling numbers from earlier flights' similaraltitude flight legs to compare to those given here for the 2014 and 2016 flights. In the specific comments I list a few places where this can be done – including the summary.

Comparisons were added.

2.6 One other area which might benefit from further detail is the 2016 flight that used 15 wavelengths instead of 30 – the authors could explain that a space-based instrument will likely sample fewer wavelengths, so it is important to test the capabilities of the instrument with that change implemented. This would tie this data, once again, to the larger science goal. Speculation on why that sampling change may or may not make a difference in the results, and whether a change was expected, could also be given. The results of other flights using fewer than 30 wavelengths could also be mentioned – did they show any significant difference? It says later that a space-based instrument would only use 8. Why then are you testing with 15 or 30, and not 8?

Although our early plans for using this technique in space used 8 wavelengths, the number of wavelengths we presently plan to use for space is 16. A sentence on this was added to the discussion section. This is why a similar number (15, which was much easier to change the existing airborne lidar to) was used for the 2016 flights. The discussion of the 2016 flight was also augmented with the rationale for using 15 wavelengths.

2.7 Finally, more discussion of your ability to determine your biases is needed. A low bias is perhaps the most important potential advantage of the lidar over passive measurements. Can you get your biases down to 0.3 ppm? 0.1 ppm? Therefore, doing a good job to quantify the level at which you can determine your biases is a critical aspect to these test flights. It can make or

break a decision to do ASCENDS or not. From this paper, it appears that you cannot see any statistically significant biases in your retrieval (as compared to the in-situ). But what is the current level at which you can determine your biases? I note that while you are often within the standard deviation of the different lidar column measurements at a given altitude, you are virtually never within 1 standard deviation of the mean. If your errors are truly random, the errors should integrate down like the square root of N. Since you often have ~100 measurements per altitude bin, your noise-driven error is on the order 0.05-0.1 ppm on the mean XCO2 in an altitude bin, while your difference to the in-situ is often more like 0.5 ppm. That is a 5-to-10 sigma discrepancy (ie, it looks like a bias!). However, it could be that the in-situ columns are only good to 0.5 ppm, considering the change in the column that determines over the course of the spiral, the native in-situ errors, etc. Therefore, more commentary on and quantification of your biases and bias knowledge is sorely needed.

The reviewer makes some very good points and we agree this is an important topic. A discussion on the differences between the XCO2 calculated from in situ and those from the lidar retrievals was added. This addresses some potential causes of differences and our plans to investigate them further.

### Specific comments:

2.8 Abstract: As stated above, please mention the factor of five improvement in precision in the 2016 flights compared to the 2011 version of the instrument.

This was done and the improvement factor was recalculated and was updated.

2.9 Section 1. Intro - When describing currently operational (passive) space-based instruments and their role in carbon cycle science, it might be informative to comment on their abilities to meet the sub-ppm measurement requirement. It would further tie the statistical results of this study to the larger science goal, which is in part to improve upon passive datasets.

A few sentences were added on GOSAT and OCO-2 passive spectrometer missions and recent assessments of their performance.

2.10 Section 2. Instrument background - Paragraph 3 of this section is the only place where the writing feels a bit disjointed and repetitive, and could be reorganized slightly to convey its message more clearly. It hops back and forth from spectroscopic information to environmental variables and Doppler-shift information a few times; I think that a simple rearrangement would help.

Thank you – this text was rearranged.

2.11 Section 3. 2014/16 Lidar setup - it is not clear in the text why the receiver optical transmission (in Table 1, which is referenced on page 3, line 45) was so low in 2014 (9.2%, as compared to ~50% and 60% in 2011, 2016). The authors should comment on this in this section. What specifically was done to improve it so much from 2014 to 2016 ?

Comments were added addressing the cause of the low transmission in 2014.

2.12 Section 4. Data processing & retrieval – The retrieval summary mentions that "HDO absorption spectrum can bias the retrieved XCO2 value if not taken into account," but it does not give the average value of that bias. The authors should include either that number or a reference to further information on the topic. Also, there seems to be no reference provided for a more detailed description of the retrieval process.

2.13 Finally, what is the posterior uncertainty on your measured HDO column? This could be a side benefit of your technique – knowledge of HDO can be used to study water cycle processes (see e.g. Frankenberg et al, 2013, "Water vapor isotopologue retrievals from high-resolution GOSAT shortwave infrared spectra", AMT).

Two paragraphs were added about the HDO lines, their retrievals, and their potential use for other purposes.

2.14 Also, do you fit for a scale factor to a prior CO2 profile, or do you assume a uniform CO2 profile and solve for that single concentration?

This was clarified in the section on retrievals.

2.15 Finally, and perhaps most importantly, is the short paragraph on the "clumped fitting" approach. This appears to be a novel aspect to this work. Has this approach of yours been described elsewhere in the literature (if so, please give the reference) or is it introduced here? How much does it reduce the errors (and in what way? Ie - is it simply a lowered scatter at a given altitude level?) between L2a and L2b? And how physically does it reduce the errors – what are the mechanisms? This could be an important aspect to this work, but it is downplayed – not mentioned at all in either the abstract or summary. Is is something that none of the passive teams (or other active teams, to my knowledge) currently do – you figured it out, so please make some more noise about it if it is really useful!

Two paragraphs were added with more explanation about clumped fitting.

2.16 Section 5. Campaigns overview – There are a few opportunities here to reference the precision and accuracy of previous campaign data. For example, on page 6, line 35, the authors could state that this <1ppm agreement between lidar and in situ is improved from 2011 comparisons (Abshire et al. 2013b), when this agreement was more along the lines of <1.4ppm.

These were done.

2.17 Also, more should be stated about the "noisy reference voltage". Does this imply that if this were fixed, the precision would be another 33% better? That's significant.

After discussions among our team, we softened this statement to refer to noisy detector electronics. We also did change the electronics before our 2017airborne campaign to eliminate this potential source of noise. We plan to evaluate the change & re-compare to the model as we process our 2017 measurements.

2.18 Section 6. I might contest, on the return leg (bottom of Figure 18), the statement "There is good agreement between E-W gradients measured by lidar and those computed from model", especially in the 5.6km segment. The model predicts something like a 1ppm E-W gradient, whereas the observational gradient might be closer to  $\sim$ 4ppm. Please soften this statement.

Agree and the statement was rephrased and softened.

2.19 SECTION 8. Discussion - Line 2: "Changing from 30 to 15 lines did not significantly change the retrievals, per the 2016 snow flight." It wouldn't hurt to include the numbers on this – how much of a difference did it make? Or was it truly negligible?

A sentence was added that specifies the small differences between 30 and 15 wavelengths on this flight.

2.20 SECTION 9. Summary – to restate what I said above, more quantification of your biases, and at what level you can even determine them with comparisons to in-situ, is needed. On line 28 would be meaningful to state specifically how much smaller the lidar vs. in situ biases are than in 2011, and how this was (missing word – assume "achieved" was intended).

The updates requested above were made to the summary, as well as including more of the previous recommendations.

2.21 Typos/grammar:

Thank you again for such a careful reading. All the issues the reviewer noted below were corrected.

a. Page 2, Line 4 – Cleaner wording – remove "so can" from "[...], and so can cause large retrieval errors."

b. Page 2, Line 22 – Define IPDA acronym once before using it in the rest of the text.

c. Page 2, Line 42 – Missing a period after "et al" in "[...] Abshire et al, 2013b)."

d. Page 5, Line 25 – Typo – "from based on" – remove either "from" or "based on".

e. Figure 7 – This figure appears blurry; update resolution.

*f.* Figure 9 – Change RMS labels to include "initial" and "after fit" for better at-a-glance clarity. Also would recommend, in the caption, describing figures in the order in which they appear - top then bottom.

g. Figure 14 & similar figures – If range and ground elevation are on the same axis (righthand), perhaps clarify this by making them the same color but making one dotted/dashed.

h. Figure 18 - The bottom plot doesn't show any 10.8km data, even though it's included in the legend. Is this a mistake? If so, correct plot; if not, removed 10.8km data from legend.

*i. A secondary legend for observations vs. model would be better than using arrows. j. The statistics in the legends don't seem to be described anywhere; describe in caption. Is the correlation between observations and model?* 

k. Page 8, Line 7 – Reference in wrong format? ("[54]")

# Airborne Measurements of CO<sub>2</sub> Column Concentrations made with a Pulsed IPDA Lidar using a Multiple-Wavelength-Locked Laser and HgCdTe APD Detector

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Abstract. Here we report on measurements made with an improved CO<sub>2</sub> Sounder lidar during the ASCENDS 2014
 and 2016 airborne campaigns. The changes made to the 2011 version of the lidar included incorporating a rapidly wavelength tunable, step-locked seed laser in the transmitter, using a much more sensitive HgCdTe APD detector, and using an analog digitizer with faster readout time in the receiver. We also improved the lidar's calibration approach and the XCO<sub>2</sub> retrieval algorithm. The 2014 and 2016 flights were made over several types of topographic surfaces from 3-12 km aircraft altitudes in the continental US. The results are compared to the XCO<sub>2</sub> values

- 25 computed from an airborne in situ sensor during spiral-down maneuvers. The 2014 results show significantly better performance and include measurement of horizontal gradients in  $XCO_2$  made over the US Midwest that agree with chemistry transport models. The results from the 2016 airborne lidar retrievals show precisions of ~0.7 parts per million (ppm) with 1 second averaging over desert surfaces, which is a ~x8 improvement compared to similar measurements made in 2011. Measurements in 2016 were also made over fresh snow surfaces that have lower
- 30 surface reflectance at the laser wavelengths. The results from both campaigns showed the mean values of XCO<sub>2</sub> retrieved from the lidar consistently agreed with those based on the in situ sensor to within 1 ppm. The improved precision and accuracy demonstrated in the 2014 and 2016 flights should benefit future airborne science campaigns and help advance the technique's readiness for a space-based instrument.

#### 35 **1. Introduction**

Accurate atmospheric CO<sub>2</sub> measurements with full global coverage are critically needed to better understand the Earth's carbon cycle (Schimel et al., 2016). In order to allow atmospheric inversions to reduce uncertainties about carbon sources and sinks, studies show that space-based atmospheric column CO<sub>2</sub> mixing ratio (XCO<sub>2</sub>)

40 measurements need to have sub-ppm precision and biases on regional scales, with areas from 100 deg.<sup>2</sup> (Tans et al, 1990; Fan et al., 1998; ESA A-SCOPE Report, 2008) to 1-25 deg.<sup>2</sup> (NASA ASCENDS Report, 2008). Several groups have analyzed space missions using passive spectrometers (Kuang et al., 2002; O'Brien et al., 2002; Dufour et al., 2003; Kuze et al., 2009), and the GOSAT (Yoshida et al., 2011) and OCO-2 missions (Crisp et al., 2017) are now making global XCO<sub>2</sub> measurements from space using optical spectrometers that view the sun-lit Earth.

However there are limitations to  $XCO_2$  measurements made using passive spectrometers. One inherent error source is optical scattering from aerosols and thin clouds in the illumination or observation paths (Mao and Kawa, 2004; Aben et al., 2007). Even small amounts of optical scattering in either path can modify the optical path length and thus the total CO<sub>2</sub> absorption measured, and can cause large retrieval errors (Aben et al., 2007). For GOSAT an error

5 standard deviations of 1.7 ppm were found versus TCCON measurements with 0.5 - 0.8 ppm of that error irreducible by averaging, implying a bias of that order (Kulawik et al., 2016). For OCO-2 typical land measurements are found to have a precision and accuracy of approximately 0.75 and 0.65 ppm, respectively, based on the small region consistency assumption, which may well underestimate the bias between regions (Worden et al., 2017). A substantial portion of this error is likely related to interferences such as aerosols or surface albedo. Realistic

10 simulations of the ACOS XCO<sub>2</sub> retrieval algorithm, used for both GOSAT and OCO-2, found errors of about 1 ppm in retrieved XCO<sub>2</sub>, but, again, these are found to represent a lower limit on the errors present in retrievals using actual GOSAT observations (O'Dell et al., 2012). With the additional restriction from minimum required solar angles useful XCO<sub>2</sub> measurements from space with passive spectrometers have been restricted to daytime cloud-free scenes within the lower and mid-latitudes.

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To overcome these limitations, the US National Research Council's 2007 Decadal Survey for Earth Science recommended a space-based  $CO_2$  measuring mission called ASCENDS (US National Research Council, 2007) that uses the laser absorption spectroscopy approach. The European Space Agency (ESA) also previously carried out mission definition studies for a similar space mission called A-SCOPE (ESA A-SCOPE Report, 2008; Durand et al.,

- 20 2009), and has supported lidar sensitivity and spectroscopic analyses for it (Ehret et al., 2008, Caron et al., 2009). The ASCENDS mission's goals are to quantify global spatial distribution of atmospheric column  $XCO_2$  with <1 ppm accuracy, and to quantify the global spatial distribution of terrestrial and oceanic sources and sinks of  $CO_2$  with monthly time resolution. The lidar approach directly measures range to the surface along with  $CO_2$  absorption and can provide  $XCO_2$  measurements through thin clouds and aerosols. The measurement is independent of sun angle
- 25 and scattered light has little impact. It provides continuous coverage of land and ocean daytime and nighttime. The ASCENDS mission organizers held an initial workshop in 2008 to better define the science and measurement needs and plans for future work (NASA ASCENDS Report, 2008). In 2015 the study team summarized their results in a white paper (NASA ASCENDS White Paper, 2015) along with plans for future work.
- 30 The Integrated Path Differential Absorption (IPDA) lidar technique is based on laser absorption spectroscopy and has been widely used for open-path measurements of atmospheric gases (Measures, 1992; Weitkamp, 2005). Several groups have developed IPDA lidar for airborne measurements of XCO<sub>2</sub> using different types of laser sources, detection and analysis techniques. Examples of lidar that have targeted measuring a single CO<sub>2</sub> line in the 1570 nm band include two airborne lidar that use intensity-modulated continuous wave (CW) lasers and direct
- 35 detection receivers (Dobler et al., 2013; Lin et al., 2015; Obland et al., 2015). Another is a pulsed airborne IPDA lidar (Amediek et al., 2017) that simultaneously measures the CO<sub>2</sub> absorption near 1572 nm and CH<sub>4</sub> absorption near 1646 nm using a direct detection receiver. Examples of lidar that have targeted the 2051 nm CO<sub>2</sub> line include a two-wavelength laser absorption spectrometer using CW lasers and heterodyne detection (Spiers et al., 2011; Menzies et al., 2014; Spiers et al., 2016) and a pulsed lidar that measures CO<sub>2</sub> absorption with two or three
- 40 wavelengths (Refaat et al., 2015; Yu et al., 2017). Several studies have also investigated the benefits and feasibility of developing a lidar to measure XCO<sub>2</sub> from orbit, and have discussed options for orbits, the laser transmitter, the needed laser power, receiver approaches and have estimated measurement performance (NASA ASCENDS workshop, 2008; Kawa et al., 2010; NASA ASCENDS White paper, 2015; Singh et al., 2017; Han et al., 2017).

### 45 **2.** The Airborne CO<sub>2</sub> Sounder Lidar

The airborne  $CO_2$  Sounder lidar (Riris et al., 2007; Abshire et al., 2010a; Abshire et al., 2010b; Amediek et al., 2012) was developed to demonstrate a pulsed multi-wavelength IPDA approach as a candidate for the ASCENDS mission. Its configuration and performance in the 2011 ASCENDS campaign are described in Abshire et al. (2013a; 2013b). The pulsed transmitter approach allows simultaneous measurement of the absorption of a single  $CO_2$  line in

- 5 the 1570 nm band, and the atmospheric backscatter profile and scattering surface height(s) in the same path. The laser transmitter uses a tunable diode laser followed by a modulator to produce pulses and a series of laser amplifiers. The direct detection receivers measure the time-resolved backscattered laser energy from the atmosphere and the surface. The column average CO<sub>2</sub> concentration is estimated from the pulse energies of the surface returns via a retrieval algorithm. It uses the lidar sampled transmission wavelengths, the aircraft altitude, the measured range
- 10 to the scattering surface, line spectroscopic data and a layered model for atmospheric state to calculate the best-fit XCO<sub>2</sub> value to the lidar signals.

The  $CO_2$  Sounder measurement samples a single  $CO_2$  line in the 1570 nm band (Mao and Kawa, 2004). This vibration-rotation band of  $CO_2$  has an appropriate range of absorption that provides good sensitivity to the surface

- 15 echo signal and to variation in CO<sub>2</sub> in the lower troposphere. The band has minimal interference from other atmospheric species like H<sub>2</sub>O and has several temperature insensitive lines. Although using other lines in this band is also possible, the R16 line at 1572.335 nm has been analyzed and was found attractive for CO<sub>2</sub> measurements (Mao et al., 2007). It has low temperature sensitivity, particularly to changes in the lower atmosphere.
- 20 The CO<sub>2</sub> Sounder approach samples the CO<sub>2</sub> line shape at multiple wavelengths. This provides several benefits including extracting line shape and some information on the vertical CO<sub>2</sub> distribution in the retrievals. It also allows solving for useful spectroscopic information, such as line center wavelengths, line widths and errors in the fits (Ramanathan et al., 2013). This approach also provides information that allows solving for several different measurement environmental variables and instrument parameters, such as Doppler-shift and wavelength offsets,
- 25 baseline tilts, and wavelength-dependent instrument transmission. Our work has found that this information is essential to minimize biases in the XCO<sub>2</sub> retrievals. For airborne and space measurements, performing retrievals in the presence of Doppler shifts expands the instrument capability to allow continuous measurement at off-nadir pointing angles during maneuvers or when pointing at ground targets.
- 30 There were several factors that led to the choice of the pulsed approach, laser pulse rate and pulse width. Using lower pulse energies at a higher pulse rates enables the use of fiber-based technology throughout the laser transmitter. At higher laser pulse rates, there are also a larger number of receiver measurements in a given time, which allows using more averaging to reduce speckle noise. Using pulsed lasers also allows post-detection signal processing to isolate the laser echo signals from the primary scattering surface and to reject backscatter from the
- 35 atmosphere that arrives earlier. Hence it allows isolating the full column measurement from potential bias errors caused by atmospheric scattering (Mao and Kawa, 2004; Aben et al., 2007). It also allows useful XCO<sub>2</sub> measurements to the tops of clouds (Ramanathan et al., 2015; Mao et al., 2017). Isolating the surface relected pulse from the atmosphere backscatter profile also substantially improves the receiver's signal-to-noise ratio (SNR) by limiting the amount of noise from the detector and solar background.
- 40

A previous version of the lidar was used in the 2011 ASCENDS airborne campaign (Abshire 2013b). This previous version had a similar basic design to the one reported here. However its seed laser source was not locked, but rather the center of its pulsed wavelength scan was periodically calibrated by using a reference laser those frequency was monitored with a wavemeter. It also used a much less sensitive photomultiplier (PMT) detector followed by a

45 discriminator and a photon counter in its receiver. After the 2011 campaign a detailed analysis was made on four flights that overflew over a variety of surface and cloud conditions near the US. These included over a stratus cloud deck over the Pacific Ocean, to a dry lake bed surrounded by mountains in Nevada, to a desert area with a coal-fired power plant, from the Rocky Mountains to Iowa, and over cloud land with both cumulus and cirrus clouds. Most flights had 5–6 altitude steps to >12 km. Analyses of the 2011 measurements showed the retrievals of lidar range,  $CO_2$  column absorption, and  $CO_2$  mixing ratio worked well when measuring over topography with rapidly changing height and reflectivity, through thin clouds, between cumulus clouds, and to stratus cloud tops (Mao et al., 2018).

- 5 The measurement precision of the 2011 version of the lidar was limited by the linear dynamic range of the PMT detector and by the signal photon count of the laser wavelengths on the CO<sub>2</sub> absorption line. For 10 s averaging, the scatter in the 2011 retrievals was typically 2-3 ppm. The analysis showed the differences between the mean lidar retrieved values, based on the DC-8 measured atmosphere, and the *in situ* measured  $CO_2$  column concentrations to be < 1.4 ppm for all four flights at altitudes > 6 km.
- 10

## 3. CO<sub>2</sub> Sounder lidar used in 2014 and 2016 campaigns

Photographs of the lidar are shown in Figure 1. For these campaigns the lidar's transmitter/telescope unit was mounted above the NASA DC-8's (NASA DC-8 Fact Sheet, 2017) aft-most nadir window (Port 9). The window 15 assembly used separate wedged and anti-reflection coated optical windows for the transmitter and receiver. The laser transmitted pulses at a 10 kHz rate while the wavelengths of the laser pulses are sequentially stepped across the  $1572.33 \text{ nm} (6360 \text{ cm}^{-1}) \text{ CO}_2$  absorption line. Although the number of laser wavelength steps is programmable, all airborne campaigns to date have used either 30 or 15 steps. The receiver telescope collects the backscatter, focuses it onto the receiver detector. The detector's analog output is amplified, digitized, and the data is synchronously

20 averaged and recorded.

> After the 2011 flight campaign, our team made a set of improvements to that version of the CO<sub>2</sub> Sounder lidar (Abshire et al, 2013b). The parameters for the 2011, 2014 and the 2016 versions are summarized in Table 1. For the 2014 flights, we replaced the previous wavelength-swept seed laser source with a rapidly tunable step-locked seed

- 25 laser (Numata et al., 2012). Figure 2 shows a block diagram of the lidar configuration used in the 2014 and 2016 airborne campaigns. For these campaigns the wavelength settings of the seed laser were locked and better optimized for measuring the CO<sub>2</sub> absorption lineshape. In the lidar receiver, we increased the receiver's optical transmission and replaced the photomultiplier (PMT)-based photon-counting receiver with a much more sensitive 16-element HgCdTe avalanche photodiode (APD) detector whose analog output was recorded by an analog digitizer. This
- 30 change also increased the lidar receiver's linear dynamic range and readout rate from 1 to 10 Hz. In 2016 we also increased the laser's divergence and the receiver field of view (FOV) to reduce speckle noise. Finally we improved the retrieval algorithms and models that solve for range, for parameters that can cause offsets in the measurements and for XCO<sub>2</sub>. Together all these changes considerably improved the lidar's measurement precision, stability and dynamic range, and reduced measurement bias.
- 35

Figure 3 shows more detail on the design of the  $CO_2$  seed laser subsystem used in the 2014 and 2016 campaigns (Numata et al, 2012). The master laser (a single frequency DFB laser diode) was continuously locked to the peak of the 1572.335 nm line of CO<sub>2</sub> in the Herriott absorption cell via the Pound-Drever-Hall technique (Numata et al, 2011). The cell pressure was 40 mb and optical path length was 18m. A single-frequency slave laser (a DS-DBR

- 40 laser diode) was dynamically offset-frequency-locked to the master laser using a rapidly tunable step-locked phaselocked loop technique (Numata et al., 2012). The offset frequencies were supplied by the FPGA. The resulting frequency-stepped CW output from the slave laser was modulated into a 10 kHz pulse train by an electro-optic modulator, amplified by a commercial erbium doped fiber amplifier (EDFA), and was collimated and transmitted.
- 45 The receiver's Cassegrain telescope viewed nadir through the receiver window and collected the laser backscatter. An antireflection-coated multimode optical fiber was used to couple the signal from the telescope focal plane to the receiver optics. After passing through an optical bandpass filter, the signal was focused onto a 3x3 pixel area of the

4x4 pixel HgCdTe APD detector. The electrical outputs from the 3x3 pixels were amplified, summed together, passed through a low-pass filter and digitized at a 100 MHz rate. The start time of the digitizer recording sweep was synchronized with the trigger for start of the laser wavelength sampling sequence. The receiver electronics averaged the signal for 32 wavelength sampling sequences (64 when using 15 samples), storing them in the memory, resetting

5 itself, and start recording again at the beginning of the next 100 ms. The laser trigger and the data acquisition were synchronized to timing markers from the GPS receiver and data was stored every 0.1 second. The computer also recorded other signals, including the GPS position and time. Due to the computer time needed to store data, not all received profiles could be recorded, and the duty cycles for the stored data were 80% and 90% for the 2014 and 2016 campaigns respectively. The DC-8 data system also recorded many other parameters, including aircraft

10 position, altitude and pitch and roll angles that were later used in data analysis and XCO<sub>2</sub> retrievals.

Figure 4 shows the wavelength sampling of the  $CO_2$  line shape used in the 2011, 2014 and 2016 campaigns. It shows that wavelength samples in 2014 and 2016 were more widely distributed in wavelength and were also more uniformly distributed in optical depth. Both changes improved the retrieval results. In the 2016 flights we also made

15 some measurements using the 15 wavelength samples shown in the figure. The receiver optics had some variability in spectral transmission that impacted the lidar measurements. Plots of the optical transmission vs wavelength for the optical bandpass filters used to reduce solar background in the lidar receiver are shown in Figure 5. The insets show expanded views with the red dots indicating the lidar measurement wavelengths. Since the transmission is not uniform with wavelength for the CO<sub>2</sub> measurement region near the peak of filter's transmission, the bandpass filter

20 slightly distorts the measured CO<sub>2</sub> lineshape. This distortion in transmission is solved for as part of the lidar retrieval algorithm.

Figure 6 shows the 16-element HgCdTe APD lidar detector (Sun et al., 2017) used in the 2014 and 2016 flights. The detector and preamplifier chip were cooled to 77 K and were housed in a commercial integrated-Dewar-cooler

25 assembly. A multimode fiber optical cable coupled the optical signal from the telescope to the detector assembly and the signal was focused onto the detector array through an optical window. For the 2014 campaign an extra fiber optics assembly was used between the telescope and the detector. This was later found to introduce excessive losses and so reduced the receiver's optical transmission for that campaign. This assembly was removed and the receiver's optical transmission was re-optimized for the 2016 campaign.

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For unbiased XCO<sub>2</sub> measurements the lidar detector's output voltage must respond to optical power in a highly linear fashion. Figure 7 shows the results from evaluating the dynamic range and the linearity of the HgCdTe APD detector for the 2014 flights, before the optical illumination of the pixels was optimized. The detector response was linear until 500 detected photons and the non-linearity slowly grows to 1% at 2000 detected photons. This correction factor was also solved for as part of the 2014 retrieval algorithm. For the 2016 flights, the receiver's optical focus was better optimized so that the detector pixels were illuminated much more uniformly. Also during the 2016 flights the laser transmitter energy was reduced for the lower altitude measurements. These changes greatly reduced the

peak powers on some pixels, so that a detector non-linearity correction was not required for the 2016 campaign.

#### 40 **4.** Data processing and XCO<sub>2</sub> retrievals

The retrieval algorithm approach is shown in Figure 8. First, the receiver backscatter at 10 Hz is further averaged over 1-s and then searched for pulse echoes with significant energy, such as those reflected from cloud tops or from the ground. The averaged pulse echo energies at each wavelength are then corrected for variation in transmission of

45 the receiver's optical band-pass filter and for any detector nonlinearity. The calibrated pulse echoes are then normalized by the transmitted laser energy and divided by the square of the range to yield the product of transmission and surface reflectance at all 30 wavelengths. This yields a first estimate of the lidar-sampled CO<sub>2</sub> transmission line shape. The 1-s averaged transmittances across the  $CO_2$  absorption line are then converted into optical depth (OD), which is linearly proportional to number density of  $CO_2$ .

Flight calibrations are constructed from a segment during the Engineering Flight that had known atmospheric
conditions and a vertical profile of CO<sub>2</sub> mixing ratio measured by the in situ sensor during the flight's spiral down maneuver. Radiative transfer calculations are used to predict the CO<sub>2</sub> transmission line shapes at different altitudes based on the in situ CO<sub>2</sub> measurements. This allows solving for and applying any further corrections needed to compensate for instrument changes seen in flight, such as for detector nonlinearities and for any changes in the wavelength dependence of the receiver optics. These final calibrations are then applied to all retrievals for the

10 science flights.

*Line shape and fit:* The retrievals utilize a CO<sub>2</sub> absorption line shape based on atmospheric state information (pressure, temperature and water vapor profiles) from the near real-time forward processing data of the Goddard Earth Observing System Model, Version 5 (GEOS-5) (Rieneker et al., 2011). Data on the full model grid (0.25 deg.

- 15 latitude x 0.3125 deg. longitude x72 vertical layers, every 3 hours) are interpolated to flight ground track position and time. The aircraft altitude, measurement path angle and altitudes of the significant scattering surfaces are determined using the aircraft GPS altitude, pitch and roll angles and the lidar-measured range. For the CO<sub>2</sub> line shape calculation, the algorithm used the spectroscopy database HITRAN 2008 (Rothman et al., 2009; Lamouroux et al., 2010) and the Line-By-Line Radiative Transfer Model (LBLRTM; Clough et al., 1992; Clough et al., 1995)
- 20 V12.1 to calculate CO<sub>2</sub> optical depth and create Look-Up-Tables (LUT). These are initially computed for a vertically uniform 400-ppm mixing ratio.

The algorithm then retrieves the best-fit  $XCO_2$  by comparing the line shapes calculated based on the vertically uniform mixing ratio to the lidar measured line shape samples. The algorithm performs the line shape fitting in

- 25 optical transmission using an unconstrained minimum variance fit. At each measurement wavelength, the fitting residual is weighted by the square of estimated SNR at that wavelength based on the average received signal and the instrument model. The retrieval algorithm then solves for Doppler shift, baseline offset, slope, surface reflectance and XCO<sub>2</sub> simultaneously by using a best fit of the lineshape function to the data. The Level 2a products are created at this step are shown in Figure 8. An example of the transmission line shape and the results of the line fitting
- 30 process are shown in Figure 9.

*Weak Water Vapor Lines*: There is also a weak (OD ~ 0.01 to 0.05) isotopic water vapor (HDO) absorption line on the short wavelength shoulder of the 1572.335 nm CO<sub>2</sub> line currently measured by the lidar, as well as one about 4 times weaker near 1572.389 nm. When measuring this CO<sub>2</sub> line, the HDO absorption spectrum can bias the

- 35 retrieved XCO<sub>2</sub> value by up to 2 ppm if not taken into account. Our laser transmitter wavelength assigned 1 or 2 wavelengths on the short wavelength HDO line to allow solving for column water vapor concentration (XHDO). The XHDO retrievals are used iteratively to reduce the uncertainty of the water vapor content in the forward calculations and then to improve the XCO<sub>2</sub> retrievals.
- 40 However the interfering HDO lines are weak and do not have other properties, such as temperature insensitivity, favorable to accurately retrieving column HDO. We estimate the precision of our retrievals of the HDO column (assuming only random noise), based on our posterior uncertainties to be around 1%. Hence the accuracy of the HDO column is likely worse, especially considering the variability in the water vapor profile. To date the HDO retrievals have been useful for pointing toward errors in the model water vapor columns. Further study may yield
- 45 opportunities for using the HDO retrievals in comparison to meteorological models or to study water cycle processes.

*Clumped Fitting*: Retrievals of  $XCO_2$  with high (~ parts per thousand) precision require line fits with very small residual errors. This requires the retrieval algorithm to solve for several potential sources of systematic error. Some of these, like the receiver wavelength response and detector intensity response, can be carefully calibrated. Other sources, like changes in the water vapor column, the Doppler shift or slow instrument drifts in the receiver

- 5 wavelength response are time-varying and so cannot be addressed using calibrations. Still other sources of systematic error, such as the Doppler shift or changes in the receiver's wavelength response, have impacts on the line fits that are orthogonal to changes in XCO<sub>2</sub>. This allows them to solved for in the line fitting process without impacting the XCO<sub>2</sub> retrieval. The remaining systematic errors have some overlap with the CO<sub>2</sub> line shape, and so fitting for them in each line fit can cause an increase in the XCO<sub>2</sub> uncertaint. One example of this is the Level 2a
- 10 fitting removes potential bias from the HDO line by fitting for the water vapor. If this is performed for each fit, this comes at the cost of a 30% increase in the standard deviation of  $XCO_2$ .

We addressed these systematic errors by using clumped fitting. Clumped fitting takes advantage of temporal correlations of some systematic errors and attempts to minimize their effect on the line fit without substantially

- 15 impacting the XCO2 posterior uncertainty or averaging kernel. Clumped fitting works similarly to the multi-pixel retrievals used by AIRS (Susskind et al, 1998 and 2003; Langmore et al., 2013) and post-retrieval processing used by TCCON (Wunch et al., 2011) and GOSAT/OCO-2 (O'Dell et al., 2012) to lower biases and reduce scatter. However, rather than assuming varying degrees of correlation between different soundings, our algorithm uses a single, averaged value for the entire clump. A typical case for the 2016 flights were XCO<sub>2</sub> retrievals to data with 30
- 20 wavelength samples averaged over 1 second. In this step, 20-s clumps of 1-s retrievals (20 lineshapes) are simultaneously fit for the parameters of the above-mentioned systematic effects being held fixed for the entire clump, while the remaining parameters, including XCO<sub>2</sub>, are allowed to vary on a 1-s scale. This gives a state-vector size (fitting parameters) of 4x20 individual terms + 3 clumped terms = 83 total terms. The measurement basis for the clumped fit is 30 wavelengths x 20 lineshapes = 600 samples. In contrast, the level-2a fitting terms had 30
- 25 wavelength samples and 5 fitting terms for each of the 20 lineshapes.

In implementing clumped fitting, we found it is important to exclude the Level 2a line fits that had high residual errors (for example, from very high signals from specular reflections from smooth water surfaces). Our analysis of clumped fitting showed it was able to remove small biases from the systematic effects mentioned above, with little change to the uncertainty in the retrieved XCO<sub>2</sub> or its averaging kernel. The averaged values of 1-s XCO<sub>2</sub> retrievals from Level 2a processing are then adjusted for these terms. After this processing, the retrievals, now called Level 2b

products, had smaller errors than those from Level 2a.

## 35 5. Overview of Airborne Campaigns

Table 2 summarizes the flight locations, focus of measurements, flight altitudes and number of lidar measurements for the 2014 and 2016 flights reported here. All flights were based out of NASA Armstrong Flight Facility in Palmdale CA. As in previous ASCENDS campaigns, for each flight we compared lidar measurements of  $XCO_2$ 

- 40 made during spiral down maneuvers to the surface with those computed from the AVOCET in situ sensor (Choi et al., 2008; Vay et al., 2003). Lidar measurements were made over low mountains covered by tall trees, desert areas with atmospheric haze, areas with growing crops, a transition area between high plateau and cropland, fresh cold snow and clear sky over desert. Spiral down maneuvers were made over most types of areas, allowing the lidar retrievals of XCO<sub>2</sub> to be compared to the column average from in situ sensors.
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The retrieval results, described subsequently, show the lidar worked well during both campaigns, although the 2016 airborne results were best due to the higher receiver optical transmission and the reduced speckle noise. The

retrievals from the 2016 measurements made over desert surfaces from a 10 km altitude with 1 second averaging time consistently had a standard deviation of ~ 0.8 ppm, while those with 10-s averaging time had precision of 0.3 ppm. This is a five-fold improvement in precision over measurements made in 2011 (Abshire et al., 2013b), where the agreement between the lidar and in situ values of XCO<sub>2</sub> were < 1.4 ppm. The higher precision in 2016 also

5 allows a more careful comparison of differences in lidar measured XCO<sub>2</sub> values to those computed from the column averaged in situ sensor. In most cases, the agreement of average XCO<sub>2</sub> computed from the lidar to that computed from the in situ sensor was better than 1 ppm.

### 6. 2014 Airborne Campaign

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2014 SF1: The focus of the 2014 Science Flight 1 was to make measurements over a forested region with tall trees and targeted the northern California coast. The ground track for the flight is shown in Figure 10. Most of the ground track was covered by coastal forest of tall trees covering hills and low (few km high) coastal mountains. The figure also shows a plot of the time tagged location and altitude. A time series of the measurement results is shown in

- 15 Figure 11. It shows the aircraft and ground elevations computed from range versus time as well as the lidar measured differential optical depths (DODs, measured from the peak to offline shoulder) and the retrieved values of XCO<sub>2</sub>. In this and in similar figures, the scattering surface elevation is computed from the aircraft altitude, the off nadir beam angle, and the lidar measured slant range to the scattering surface. All measurements plotted are for 10-s averages. Figure 12 shows a photograph of a typical surface measured from the aircraft and a summary of the lidar
- 20 retrieval statistics versus altitude for the indicated area in Figure 11. The corresponding measurements from the AVOCET in situ sensor in the spiral are shown as blue line and as blue dots for the column average from that altitude to the surface.

2014 SF2: The 2014 Science Flight 2 targeted measurements over a desert region. The location chosen was western edge of the Mohave Desert in California. The ground track and the time-tagged altitude plot are shown in Figure 13 and show approach and spiral down over Edwards Air Force Base. This flight occurred during a period of widespread atmospheric haze at lower altitudes caused by smoke spreading from a wildfire in the nearby Sierra Nevada Mountains. A time series segment of lidar measurements from this flight is shown in Figure 14. This segment contains a spiral down maneuver. The height-resolved backscatter profile is shown in Figure 15. It shows a

- 30 layer of haze from ~ 4km to the surface caused by smoke from the wildfire. The altitude summary of the lidar measurements is also shown, along with measurements from the in situ sensor. The results show there is very good agreement between the  $XCO_2$  retrieved from the lidar and that computed from the in situ sensor, despite the significant optical scattering from the thick haze layer.
- 35 2014 SF3: The 2014 Science Flight 3 was a flight to and from Iowa made in the afternoon and evening, respectively. There were also segments during the transit from California to and from Iowa that allowed assessing the lidar's capability to measure horizontal (east-west) gradients in XCO<sub>2</sub>. Figure 16 shows the ground track of the 2014SF3G1 segment in Colorado and Nebraska, which was during the west-to east-leg of the flight toward Iowa. Figure 17 shows the ground track of the segment 2014SF3G2, in Iowa, Nebraska and Colorado, which was during the return
- 40 (east-to-west) flight leg toward California.

The time series of the lidar retrievals of  $XCO_2$  during these flights legs are shown in Figure 18. The outbound (west-to-east) leg flew at only one aircraft altitude, but the return leg flew 3 altitudes. The data points plotted are for lidar retrievals based on 50-s (~12 km alongtrack) averaging. Both segments clearly show the gradual decrease of  $XCO_2$ 

45 caused by increasing growing crop density (and CO<sub>2</sub> uptake) toward the eastern end of the flight legs in the Midwest US, even for the return segment that used three different aircraft altitudes. The solid lines show the XCO<sub>2</sub> values computed from the NASA Parameterized Chemistry Transport Model (PCTM) (Kawa et al., 2004) for these tracks

and times. Although there are offsets in the average values, there is good agreement between the E-W gradients measured by the lidar on the outbound (SF3G1) flight segment and those computed from the model, as well as for the 6.3 km altitude leg of the return segment (SF3G2).

- 5 2014 SF5: The 2014 Science Flight 5 targeted XCO<sub>2</sub> over growing corn cropland in Iowa in early morning. Figure 19 shows the ground track of the segment of SF5 made over Iowa along with the time-tagged altitude plot. The spiral-down location was centered near West Branch Iowa. This flight used a 3-box pattern flown from lowest to highest altitude, then a spiral down maneuver made to near the West Branch Tower. Figure 20 shows the time history of the segment of the flight just west of the Rocky Mountains to the box pattern in Iowa. The elevation of the
- 10 eastern most Rocky Mountains and the longer ranges from the turns in the corners of the box patterns are noticeable in the history. Figure 21 shows a photograph of the Iowa landscape for one leg of the lower box. It also shows the altitude summary for the XCO<sub>2</sub> retrievals from the lidar measurements between the dashed lines in Figure 20. The XCO<sub>2</sub> retrievals from the lidar measurements closely follow those from in situ except at the lowest altitude and the gradually increasing values with altitude agree with those computed from the in situ sensor. In the 7-10 km altitude
- 15 range the retrieved XCO<sub>2</sub> for the 2011 flight segment over Iowa had standard deviations of  $\sim$ 1.8 ppm over Iowa, while in the 2014 flights they were  $\sim$ 1.2 ppm.

#### 7. 2016 Airborne Campaign

- 20 The 2016 campaign was a short (two flight) campaign flown during the local wintertime. The campaign objective was to assess the performance of the 2016 version of the  $CO_2$  Sounder lidar, to assess its measurements made using fewer wavelength samples and with additional laser power to characterize the measurements made at low sun angles over fresh cold snow. The changes in the instrument from the 2014 version are summarized in Table 1.
- 25 2016 Desert: The 2016 Desert Flight was made again over the Mohave Desert and Edwards Air Force Base CA, which was used for the spiral down location. Figure 22 shows a plot of the ground track and the time-tagged altitude plot for the flight. Figure 23 shows the altitude summary of the lidar measurements for the spiral down and their comparison to the in situ measurements. The plot format is the same as for Figure 13, except that these measurements have 1-s averaging time. The smallest standard deviations for the 1-sec measurements were ~ 0.7
- 30 ppm for altitudes between 7-10 km, which is a factor of ~8 smaller than corresponding lidar measurements made in 2011. The standard deviation of the lidar 1-second retrievals vs altitude is also shown in the figure, along with those computed from a statistical model of the lidar (Sun et al., 2017a). The altitude dependence of both plots is quite similar, with the standard deviations increasing at lower altitudes due to decreasing optical depth of the  $CO_2$  line, and at upper altitudes due to the  $R^{-2}$  dependence of the lidar signal and the increased attenuation of the stronger  $CO_2$
- 35 absorption. The plot also shows the standard deviations of the retrievals are about a factor of 1.5 higher than the lidar model. After the campaign, investigations found that the detector electronics may have contributed some additional noise. Improvements in the detector electronics were made for the 2017 ASCENDS airborne campaign and the impact on the lidar retrievals will be assessed as part of the data analysis.
- 40 2016 Snow: The 2016 Snow Flight targeted a long series of measurements over fresh cold snow. Snow had recently fallen in northeast Nevada and the surface temperatures had stayed below 0 C, so the flight repeated a north-south route just south of Elko NV. The Elko NV airport was the nearest location available for the spiral down maneuvers. The flight altitudes of the north-south legs of this flight were between 6.6 and 9.5 km. Figure 24 shows a plot of the flights ground track and a photograph of the snow-covered desert surface made from the airplane. The altitude
- 45 summary of the lidar measurements for this flight is shown in Figure 25. To investigate measurement approaches planned for space we also used 3 different laser configurations for this flight. Those were 30 sample wavelengths and one laser amplifier, 15 sample wavelengths and one laser amplifier, and 15 wavelengths and two laser

amplifiers. The second amplifier almost doubled the transmit power to 50 uJ/pulse. As expected the 30 and 15 wavelength samples with one laser amplifier (same average power) gave similar results. The standard deviations for two-amplifier lidar setting were also smaller than for one amplifier, due to the larger received signal and hence higher SNR. Also, as expected from the snow surface's low (~4%) reflectivity, the measurement standard deviations over the snow were about 3 times higher than those over the desert.

#### 8. Discussion

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The flights and height-resolved measurement statistics from the 2014 and 2016 airborne campaigns are summarized in Tables 3 and 4 in the Appendix. All column entries in these tables, except counts and standard deviations (s.d.), are the average values for the measurements binned by altitude. The 2014 altitude bins typically averaged 30 of the 10-s measurements, which at a nominal 200 m/s aircraft speed meant ~60 km along track averaging. The 2016 altitude bins typically averaged 150 of the 1-s measurements, resulting in ~30 km along track averaging. Plots of the differences between the lidar-measured XCO<sub>2</sub> and those computed from the in situ sensor are shown in Figure 26,

15 along with the number of measurements for the data set and error bars. In the Tables, the measurement DOD is computed from the fitted retrieval from the line peak to the line shoulder. The lidar offline total signal column is for detected photons per wavelength, summed over the averaging time.

The results show that in 2014, typical standard deviations in retrievals based on 10-s averaging were  $\sim$  1ppm, with 20 lowest standard deviations over desert and slightly higher values over forest. The lidar changes made for the 2016 reduced the speckle noise and the signal shot noise in the measurements and improved the performance. For the 2016 flights,  $\sim$  0.7 ppm standard deviations were achieved over desert with 1 second averaging time, with 2.5 ppm standard deviations measured over snow surfaces. As was seen in the 2011 airborne measurements (Abshire et al., 2013b) the standard deviations of the XCO<sub>2</sub> retrievals vary with altitude. At lower altitudes the optical depth of the

25 line is smaller, which magnifies the lidar measurement error, and since the received signal varies as  $R^{-2}$ , at higher altitudes the lower signal levels limit the measurement resolution. As a result there is an altitude with smallest standard deviation, which for the 2016 flights was ~ 8 km. In all cases the agreement between the lidar measured XCO<sub>2</sub> and that computed from the in situ sensor and MERRA atmospheric model was < 1ppm.

30 Two experiments using slightly different lidar transmitter configurations were conducted during the 2016 Snow flight. The results show that reducing the number of laser measurement wavelengths from 30 to 15 using the same average laser power had only a minor impact (changed mean  $XCO_2 \sim 0.5$  ppm, increased standard deviation to  $\sim 0.4$ ppm) on the retrieval results. They also show that adding an additional fiber amplifier to the transmitter to double the laser energy increased the received signal and reduced the measurement standard deviation, as expected.

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Since  $CO_2$  fluxes make only small changes in the column average, it is important to understand the causes of the differences between  $XCO_2$  values calculated from the in situ sensor measurements and those from the lidar retrievals. The laser's wavelength locking was quite good, as was the ranging accuracy, so residual errors from those potential sources are likely small. There are several other potential sources for ppm-level differences. Any

- 40 small slowly moving changes in the lidar's response versus wavelength or other factors that are not modeled in the retrieval algorithm will cause biases. Previous work (Abshire 2013b) also showed that the mean retrieved XCO<sub>2</sub> values were sensitive, at the few ppm level, to the source of the reference atmosphere (for example, MERRA or that from the DC-8) used for the retrieval's look-up-tables. If the atmosphere is not in steady state, then the actual CO<sub>2</sub> concentrations in the column may be slowly drifting versus time before, during and after the spiral maneuvers used
- 45 for comparison. All these potential sources of difference and bias need to be investigated in future work. The recently completed ASCENDS 2017 airborne campaign (Abshire 2017) has provided a new and extensive data set

that can be used for this purpose. It carried out a robust calibration flight that had 10 spiral maneuvers along with 7 additional flights made under a wide variety of conditions.

Work has been ongoing at NASA Goddard Space Flight Center for several years to extend the airborne CO2

5 Sounder lidar's measurement capability to orbit for a space mission like ASCENDS (NASA ASCENDS White Paper, 2015). The key capabilities needed are a performance model that allows accurately scaling the characteristics of the airborne measurements to space, and the laser and detectors with the needed performance in the space environment. The present plans for a space-based version of this lidar use 16 laser wavelengths. Recent summaries are available on the modeling the space-based lidar measurement performance and on determining the needed laser

10 power (Sun et al., 2017a), on developing the rugged higher power laser (Stephen et al., 2017; Nicholson et al., 2016; Stephen et al., 2018) and on developing the HgCdTe APD detector needed in the lidar receiver (Sun et al., 2017b) for a space mission. An engineering model of the receiver's HgCdTe APD detector/cooler assembly has passed space qualification and radiation testing and has the sensitivity needed for a space mission. An engineering model of the space laser's key electro-optic assemblies is undergoing space environmental testing during spring 2018.

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#### 9. Summary

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Since its use in the 2011 campaign (Abshire et al., 2013b), our team made several improvements to the  $CO_2$  Sounder airborne lidar. These included incorporating a rapidly wavelength tuneable step-locked seed laser in the lidar transmitter, using a much more sensitive HgCdTe APD detector, and using a digitizer with higher measurement rate in the receiver. We also improved the lidar calibration approach, the  $XCO_2$  retrieval algorithm and the approach used to minimize the impact from a nearby isotopic water vapor (HDO) line. In 2016 we used a larger laser divergence angle and improved the transmission of the receiver optics and the uniformity of the illumination pattern on the detector pixels. All these changes considerably improved the lidar's precision, stability and accuracy.

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The improved  $CO_2$  Sounder lidar was used to make measurements during the ASCENDS 2014 and 2016 airborne campaigns. These were made over several types of surfaces from 3-12 km aircraft altitudes. The results are compared to the  $XCO_2$  values computed from an airborne in situ sensor during spiral-down maneuvers. The 2014 results also show measurement of horizontal gradients in  $XCO_2$  made over the US Midwest on two flight segments

30 that were consistent with those computed from a chemistry transport model. Analysis show the 2014 and 2016 measurements have consistent agreements within 1 ppm for mean value of XCO<sub>2</sub> compared to that computed from the in situ sensor, which is better than those for 2011 version.

Retrievals for the 2016 airborne lidar measurements made over desert surfaces show precision of 0.8 ppm with 1

35 second averaging, which is ~8 times smaller than similar measurements made in 2011. In 2016 measurements were also made over fresh snow surfaces, which are important for high latitude studies, but which are dark at CO<sub>2</sub> measurement wavelengths. As expected, the standard deviations of lidar measured XCO<sub>2</sub> were about 3 times larger over snow surfaces. Over snow the agreements of the mean values of lidar retrievals with XCO<sub>2</sub> computed from the in situ sensor were also within 1 ppm. The 2016 lidar's precision and consistent sub-ppm agreement with the XCO<sub>2</sub>

40 calculated from in situ sensors are expected to benefit future airborne carbon science campaigns. They also help advance the technique's readiness for a future space-based instrument.

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#### 11. Conflicts of Interest

The authors declare no conflict of interest.

## 10 **12. Appendix**

Tables 3 and 4 summarize the measurement statistics for 5 flights made during the 2014 and 2016 campaigns.

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Parameter	2011 flights	2014 flights	2016 flights
CO <sub>2</sub> Line used	R16, 6359.96 cm <sup>-1</sup>	same	same
CO <sub>2</sub> line center wavelength	1572.335 nm	same	same
Laser min wavelength	1572.228 nm	1572.235 nm	same
Laser max wavelength	1572.39 nm	1572.440 nm	same
Laser pulse rate	10 kHz	same	same
# of wavelength samples on line	30	same	30 or 15
Laser scan rate of $CO_2$ line	300 Hz	same	300 or 600 Hz
Seed laser wavelength adj.	linear sweep	step locked	same
Wavelength change/ laser step	~ 3.8 pm	varied via program	same
$CO_2$ reference cell conditions	0.8 m path, ~200	18 m path, 40 mbar	same
	Torr pressure	pressure	
Laser peak power, pulse width	25 watts, 1 µsec	same	same
Primary Laser pulse energy	25 μJ	same	same
Optional Laser pulse energy*			50 µJ
Laser divergence angle	100 µrad	100 µrad	430 µrad
Laser linewidth	~15 MHz	<4 MHz = 0.032 pm	same
Receiver Telescope type	Cassegrain, f/10	same	same
Telescope diameter	20 cm	same	same
Receiver FOV diameter	200 µrad	200 µrad	500 µrad
Receiver Optical Transmission	~ 50%	9.2%	60%
Detector type	Hamamatsu	DRS HgCdTe APD	
	H10330A-75		same
Detector effective QE	4%	70%	70%
Detector APD gain settings	$\sim 10^{5}$	600	300
Receiver signal processing	Photon Counting &	Analog detection &	
approach	histogramming	averaging	same
Receiver time bin width or ADC			
sample time bin width	8 nsec	10 nsec	same
Receiver electronic bandwidth	10 MHz	7 MHz	same
Data recording rate	1 Hz	10 Hz	same
Data recording duty cycle	80%	80%	90%

Table 1 – CO<sub>2</sub> Sounder Lidar Parameters for the 2011, 2014 and 2016 airborne campaigns

\*- used 2 laser amplifiers

	Table 2 – Summary	y of 2014 and 2016	campaign flights	and regions studied
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Flight				Aircraft Altitude	Ave. time per	Number of Lidar
Designation	Date	Location (in US)	Focus of measurements	Range (km)	measurement (sec)	measurements
2014 SF1	20-Aug-14	North CA Coastal forests	Forests on low mountains	2.89 - 11.19	10	712
2014 SF2	22-Aug-14	Near Edwards AFB, CA	Desert through haze	3.50 - 11.25	10	446
2014 SF5	3-Sep-14	Eastern Iowa	XCO2 over cropland	2.62 - 11.16	10	1010
2014 SF3G1	25-Aug-14	Colorado to Iowa (outbound)	East-West XCO2 gradients	11.2	50	43
2014 SF3G2	25-Aug-14	Iowa to Colorado (return)	East-West XCO2 gradients	5.6, 6.3, 10.8	50	67
2016 Desert	10-Feb-16	Edwards AFB, CA	Desert	3.59 - 12.60	1	1281
2016 Snow	11-Feb-16	Eastern Nevada	Recent cold snow	6.68 - 9.52	1	5893

Lidar &	Aircraft	Ground	Mean Slant	# of	Lidar	Lidar Offline	Lidar	Lidar	AVOCET	XCO2 Difference:
Measurement	Altitude	Elevation	Range	meas .in	DOD	Tot. Signal	XCO2	XCO2	XCO2	(Mean Lidar -
Conditions	(km)	(km)	(km)	alt bin		(Kcounts)	mean (ppm)	S.D. (ppm)	(ppm)	AVOCET) (ppm)
SF1	3.518	0.752	2.861	25	0.384	5590	394.32	2.2	394.78	-0.45
Forests	4.469	0.814	3.773	26	0.516	3474.4	393.85	1.99	394.58	-0.73
30 wavelengths	5.224	0.756	4.489	286	0.623	1993	394.32	1.85	394.88	-0.56
1 amplifier	6.467	0.799	5.822	20	0.826	1222.6	394.22	1.39	394.82	-0.6
10 sec average	7.498	0.722	6.988	23	1.008	802.2	394.85	1.28	394.93	-0.08
	8.468	0.596	8.361	22	1.222	624.7	394.93	1.26	395.02	-0.08
	9.5	0.865	8.934	19	1.333	531.1	395.08	1.47	395.1	-0.01
	10.502	0.644	10.23	30	1.543	313.6	395.23	1.26	395.22	0.01
	11.193	0.757	10.582	254	1.613	395	395.57	1.4	395.27	0.3
	3.498	0.747	2.929	26	0.392	13304	397.4	2.23	397.62	-0.22
SF2	4.692	0.842	4.125	55	0.565	6156.1	396.22	1.62	396.17	0.04
Desert	5.454	0.859	4.74	168	0.658	3837.1	396.37	1.71	396.15	0.21
30 wavelengths	6.473	0.914	5.925	19	0.839	2506.4	396.02	0.83	396.12	-0.11
1 amplifier	7.438	0.824	7.236	12	1.038	1759.2	395.59	0.96	396.06	-0.46
10 sec average	8.484	0.842	8.393	11	1.227	1299.1	395.29	1.12	395.98	-0.68
	9.51	0.843	9.513	12	1.415	937.2	396.03	0.96	395.95	0.07
	10.497	0.815	10.539	11	1.592	824.1	396.4	0.79	395.94	0.46
	11.246	0.78	10.604	132	1.614	663.2	395.99	0.83	395.93	0.06
SF5	3.489	0.228	3.425	29	0.453	4713.1	391.4	1.94	391.03	0.37
Cropland	4.504	0.22	4.455	24	0.604	2763.4	392.35	1.86	391.61	0.74
30 wavelengths	5.112	0.219	4.96	384	0.682	2038.9	391.45	1.48	391.95	-0.49
1 amplifier	6.507	0.225	6.533	33	0.922	1043	391.52	1.26	392.5	-0.98
10 sec average	7.92	0.22	7.834	259	1.134	741.2	393.04	1.13	392.87	0.17
	8.499	0.224	8.554	30	1.249	582.3	392.77	1.33	393.04	-0.27
	9.513	0.227	9.51	35	1.409	423.4	392.44	1.28	393.34	-0.9
	10.529	0.238	10.569	34	1.59	293	392.72	1.13	393.56	-0.83
	11.158	0.218	10.974	166	1.665	136.9	393.48	2.03	393.67	-0.19

Table 3 – Summary of results for three of the 2014 flights

## Table 4- Summary of results for the 2016 flights

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Lidar &	Aircraft	Ground	Mean Slant	# of	Lidar	Lidar Offline	Lidar	Lidar	AVOCET	XCO2 Difference
Measurement	Altitude	Elevation	Range	meas .in	DOD	Tot. Signal	XCO2	XCO2	XCO2	(Mean Lidar
Conditions	(km)	(km)	(km)	alt bin		(Kcounts)	mean (ppm)	S.D. (ppm)	(ppm)	- AVOCET) (ppm)
Enginering	3.589	0.734	2.997	90	0.424	2690	404.96	2.43	404.36	0.6
Desert	4.503	0.726	3.965	114	0.572	1731.5	405.16	1.52	404.18	0.98
30 wavelengths	5.464	0.715	4.968	99	0.73	1726.8	404.95	1.21	404.08	0.87
1 amplifier	6.496	0.76	6.005	115	0.902	2729.4	404.75	0.85	404.02	0.73
1 sec average	7.501	0.724	7.078	117	1.082	2031.8	404.91	0.68	403.98	0.93
	8.49	0.714	8.154	119	1.267	1605.3	404.46	0.65	403.95	0.51
	9.495	0.799	9.092	114	1.437	1268	404.19	0.72	403.91	0.28
	10.519	0.798	9.843	128	1.58	1122.4	403.87	0.75	403.86	0.01
	11.497	0.816	11.304	137	1.845	876.9	403.95	0.86	403.84	0.11
	12.601	0.795	12.227	248	2.022	710.5	403.34	1	403.74	-0.4
Snow										
30 wavelengths	7.914	1.848	6.081	883	0.945	394.2	403.85	2.37	404.32	-0.47
1 amplifier										
1 sec average										
Snow										
15 wavelengths	6.682	1.907	4.805	2414	0.73	1255.6	404.49	2.89	404.45	0.05
1 amplifier	7.841	1.875	6.008	1271	0.932	827.3	403.62	2.56	404.32	-0.7
1 sec average										
Snow										
15 wavelengths	7.912	1.902	6.026	985	0.94	1185.5	404.65	2.35	404.28	0.37
2 amplifiers	8.506	1.64	7.166	158	1.128	1066.5	405.18	1.89	404.52	0.65
1 sec average	9.525	1.454	8.19	182	1.307	632.9	405.24	1.92	404.64	0.59



Figure  $1 - CO_2$  Sounder instrument photographs. *a*) The aircraft rack with the new seed laser subsystem. *b*) The aircraft racks containing the laser power amplifiers and the lidar's detector subsystem. *c*) The lidar's transmitter and receiver telescope assembly, which is positioned over the nadir window assembly in the aircraft fuselage. The optical pulses from the fiber amplifiers, and the received optical signals are coupled via fiber optics. *d*) The instrument operator's console, with the control computer screens folded away.



Figure 2- Instrument block diagram for the 2014 and 2016 versions of the  $CO_2$  Sounder lidar described here. The inset shows the transmitted pulse train sequence that is repetitively stepped in wavelength across the  $CO_2$  line.



- 5 Figure 3 Block diagram of the CO<sub>2</sub> seed laser subsystem that is used to produce the wavelength-stepped pulse train transmitted by the lidar. The wavelength of the master laser (a DFB laser diode) is frequency locked to the center of the CO<sub>2</sub> absorption line. The slave laser is offset-frequency-locked to the master via an optical phase locked loop. The frequency offset is changed during the 99-us between laser pulses based on the wavelength settings stored in a table in the seed laser's FPGA. The slave laser's output is carved into 1-us wide pulses by the modulator (MZM) and
- 10 is used as the input for the transmitter's fiber amplifiers (EDFAs) that produce the laser pulse train that is transmitted. Here PM denotes phase modulator; PFD, phase frequency detector; FPGA, field programmable gate array; DDS, direct digital synthesizer; MZM, Mach-Zehnder modulator; and EDFA, erbium doped fiber amplifier.



Figure 4 - Plots of the  $CO_2$  line sampling laser wavelengths (blue dots) used for the airborne campaigns in 2011, 2014 and 2016. The 2016 campaign used both 30 and 15 laser sampling wavelengths. The  $CO_2$  absorption lineshapes (black lines) are shown for a two-way path for airborne lidar measurement conditions from a flight

lineshapes (black lines) are shown for a two-way path for airborne lidar measurement conditions from a flight altitude of 13 km to a surface elevation of 220m. These conditions occurred during the September 3, 2014 flight over Iowa.



Figure 5 – Plots of transmission vs wavelength for the optical bandpass filters (BPF) used in the lidar receiver. *a*) Filter used for the 2014 flights, and *b*) Filter used for the 2016 flights. The insets show expanded views of the peak filter transmissions at the lidar measurement wavelengths (red dots). The 2016 filter was purchased in an attempt (which was unsuccessful) to flatten the response at the lidar measurement wavelengths. The lidar retrieval algorithm solves for the variability in instrument transmission at the measurement wavelengths introduced by the filters.



Figure 6 – The HgCdTe APD detector used in the lidar receiver. *a*) A diagram showing the locations of the 4x4 APD detector array and the CMOS preamplifier and readout integrated circuit (ROIC). *b*) Photograph of the same elements mounted on the detector's leadless chip carrier (LCC). *c*) Top view of the detector's cryo-cooler assembly used to keep the LCC at ~80K. The cooler's compressor is on the left, the cooled section is on the right, and the fiber optic cable used to couple the optical signal from the telescope through the cryo-cooler's optical window assembly onto the 4x4 detector array is at the bottom. The conditioning and control electronic box is at the top of the photograph.



Figure 7 – The results from calibrating the linearity of the lidar's HgCdTe detector for the 2014 lidar configuration. *(Top)* Measurement of the detector output vs optical input. *(Bottom)*Deviation from linear response in the detector response, showing a deviation starting at 600 photons with a maximum deviation of 1%. For the 2016 flights, the receiver optics were improved so that the optical signal was more uniformly distributed across the detector array elements, and an additional electronic preamplifier stage was used. Together these reduced the non-linearity effect so that its effect was negligible for the 2016 flights.



Figure 8 – Processing diagram for retrieval algorithm used to estimate  $XCO_2$ , range and other parameters from the lidar measurements as well as from other information from the aircraft. The results shown in this paper are labeled as Level 2a and Level 2b products in the algorithm.



Figure 9 – *(Upper plot)* Example of the CO<sub>2</sub> transmission line shape measured by the lidar from an altitude of 7.6 km. The line shape samples from the lidar are the red dots. The line shape computed from the retrieval is shown as the black line. *(Lower plot)* The ratio of the retrieved line shape and lidar retrievals with the red dots being the initial trial XCO<sub>2</sub> value of 400 ppm and the black dots and line being the final best fit retrieved XCO<sub>2</sub> value of 404 ppm.



Figure 10 - (Left) Map of the 2014 SF1 flight track over the northern California coast on 20 Aug 2014. (*Right*) Time tagged location and altitude plot for the same flight.



Figure 11- Lidar measurement and retrieval results from 2014 SF1 flight over the north coast of CA on August 20, 2014. *(Bottom)* time resolved results showing the lidar measured differential optical depth in red, the range to the surface in blue, and the computed elevation of the scattering surface in dark green. The upward spikes in the DOD and range are from the slant paths during the banking of the aircraft during the corners of the box pattern. *(Top)* The retrieved XCO<sub>2</sub> values from the lidar measurements, with each dot made using 10 second averaging time. The measurements between the dashed lines are summarized in Figure 19.



Figure 12 - (Left) Photo of northern CA coastal redwood forests taken from the aircraft on 2014 SF1. (*Right*) Summary plot of the in situ (blue) and retrievals from lidar measurements (red) versus altitude. The lidar results are for XCO<sub>2</sub> retrievals based on 10-s average from the altitude where the results are plotted, and the error bars are for 1 standard deviation. The XCO<sub>2</sub> computed from the in situ sensor from the plotted altitude to the ground are shown as the blue dots.



Figure 13 –(*Left*) Map of the track of the spiral down over Edwards AFB California on 2014 SF2 on 22 August 2014. (*Right*) Time tagged location and altitude plot for that flight segment.



Figure 14- Lidar measurement and retrieval results from 2014 SF2 flight over Edwards AFB CA on August 22, 2014. From the  $\sim$  11 km altitude, the aircraft flew a spiral down pattern to near the Edwards Dry Lake Bed *(Bottom)* time resolved results showing the lidar measured differential optical depth, the range to the surface, and the computed surface elevation. The lidar-measured range to the scattering surface and the scattering surface "ground" elevation are plotted against the right hand axis. The upward spikes in the DOD and range are from the slant paths during the banking of the aircraft during the corners of the box pattern. *(Top)* The retrieved XCO<sub>2</sub> values from the lidar measurements, with each dot made using 10 second averaging time.



- Figure 15 (Left) Time history of the range resolved backscatter for the off-line wavelengths recorded on 2014 SF2 before the spiral down maneuver. The plot shows enhanced scattering from haze in the boundary layer. The aircraft altitude is the thin red line at the top of the plot. Each vertical profile is R<sup>2</sup> corrected and used 1-s averaging. (*Right*) Summary of the in situ (blue) CO<sub>2</sub> measurements and the XCO<sub>2</sub> retrievals from lidar measurement (red) versus altitude for the segment in Figure 15. The lidar results are for XCO<sub>2</sub> retrievals based on 10-s average from the
- 10 altitude where the results are plotted to the surface, and the error bars are for 1 standard deviation. The XCO<sub>2</sub> values computed from the in situ sensor from the plotted altitude to the ground are shown as the blue dots.



Figure 16 – Map of the segment of the west-to east flight track analyzed for 2014 SF3 on 25 Aug 2014.made approaching Iowa.



Figure 17 – Map of the segment of the east-to-west flight track analyzed during 2014 SF3 on 25 August 2014 when leaving Iowa approaching Colorado.



Figure 18 – Retrieved XCO<sub>2</sub> from lidar measurements vs longitude for the transit flights to/from Colorado to Iowa on 2014 SF3. *(Top)* Outbound leg (West to East flight direction, SF3G1, measured from 11.2 km altitude) and *(Bottom)* Return flight leg (East to West flight direction, SF3G2, with dark blue points measured from 5.6 km altitude and light blue points from 6.3 km altitude). The measurements shown are for retrievals using 50-s data averages, and the flight altitudes are indicated. The solid lines show the XCO<sub>2</sub> values computed from the PCTM atmospheric model for that location and these times.



Figure 19 - (Left) Map of the flight track from Lincoln Nebraska west-to-east, then a box pattern made over Iowa at dawn on the 2014 SF5 flight on September 3, 2014. (*Right*) Plot of the time tagged location and altitude for 3-altitude box pattern during the same flight.



Figure 20- Lidar measurement and retrieval results from 2014 SF5 flight over Iowa on September 3, 2014. This flew a square flight pattern near the NOAA West Branch Iowa tower at 3 different altitudes. *(Bottom)* time resolved results showing the lidar measured differential optical depth, the range to the surface, and the computed surface elevation. The lidar-measured range to the scattering surface and the scattering surface "ground" elevation are plotted against the right hand axis. The upward spikes in the DOD and range are from the slant paths during the banking of the aircraft during the corners of the box pattern. *(Top)* The retrieved XCO<sub>2</sub> values from the lidar measurements, with each dot made using 10 second averaging time. The measurements between the dashed lines are summarized in Figure 21.



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Figure 21 - (Left) Photo of the Iowa topography and the West Branch tower taken from the aircraft on 2014 SF5. (*Right*) Summary of the in situ (blue) and the retrievals from the lidar measurement (red) versus altitude. The lidar results are for retrievals based on 10-s average from the altitude where the results are plotted, and the error bars are for 1 standard deviation. The XCO<sub>2</sub> computed from the in situ sensor from the plotted altitude to the ground are shown as the blue dots. The in situ sensor shows the drawdown in CO<sub>2</sub> concentrations at lower altitudes caused by cropland, and that general trend is seen in the XCO<sub>2</sub> values computed from in situ and in lidar retrievals.



Figure 22 – (*Left*) Flight track for February 10, 2016 flight over Edwards AFB California. (*Right*) Time tagged location and altitude plot for the spiral down maneuver over Edwards AFB for the same flight.

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Figure 23 - (Left) Plot of the measurements made during the spiral down segment of the 2016 desert flight over the Rogers dry Lake bed near Edwards AFB CA. The XCO<sub>2</sub> retrievals from the lidar measurements are shown (in red) from the plotted altitude to the surface, the in situ CO<sub>2</sub> concentration measurements (blue line) and the XCO<sub>2</sub>

20 computed from the in situ CO<sub>2</sub> readings from the plotted altitude to the surface (blue dots). (Right) Plot of the standard deviation of the XCO<sub>2</sub> retrievals from the lidar measurements (red) using 1-s integration time, showing best resolution near 8 km altitude. The solid black line is for the standard deviations computed from a statistical model of the lidar measurement.



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Figure 24 - (Left) Map of the ground track for the 2016 Snow flight made over northeastern Nevada. The spiral down location was centered on the airport at Elko NV and all subsequent measurements were made during the north-south tracks south of Elko. (Right) Photograph of the snow covered hills and desert floor made during the 2016 Snow flight.



Figure 25 - Lidar results from the 2016 snow flight. (*Left*) Plot of the XCO<sub>2</sub> measurements from the lidar (in red) from the plotted altitude to the surface, the in situ CO<sub>2</sub> concentration measurements (blue line) and the XCO<sub>2</sub> computed from the in situ CO<sub>2</sub> readings (blue dots) from the plotted altitude to the surface (blue dots). Here the lidar measurements were made using made using 30 laser wavelength samples across the CO2 line. (*Middle*) Results over the same snow area, but with lidar measurements were made using 15 wavelength samples across the

20 CO2 line. (*Right*) Results over the same snow area, but with lidar measurements made using 15 wavelengths and using two EDFA laser amplifiers in parallel.



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Figure 26 -Summary of results from the 2014 and 2016 flights, plotted from the values summarized in Tables 3 and 4. The dots are the mean value of the XCO<sub>2</sub> from the lidar minus that computed from the in situ sensor. They are plotted at the altitude from which they were measured, and the average ground elevations are also shown. The 2014 statistics are from data using 10-s averaging and the 2016 measurements used 1-s averaging. The error bars are those of the lidar data set, and the numbers shown are the number of lidar observations in that set. There were three

different settings used in the lidar for the 2016 snow flight, and their results are plotted in different colors.