Airborne Lidar Measurements of Aerosol and Ozone Above the Canadian Oil Sands Region

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Abstract. Aircraft based lidar measurements of atmospheric aerosol and ozone were conducted to study air pollution from the oil sands extraction industry in northern Alberta. Significant amounts of aerosol were observed in the polluted air within the surface boundary layer, up to heights of 1 km to 1.6 km above ground. The ozone mixing ratio measured in the polluted boundary layer air directly above the oil sands industry was equal to or less than the background ozone mixing ratio. On one of the flights, the lidar measurements detected a layer of forest fire smoke above the surface boundary layer in which the ozone mixing ratio was substantially greater than the background. Measurements of the linear depolarization ratio in the aerosol backscatter were obtained with a ground based lidar and this aided in the discrimination between the separate emission sources from industry and forest fires. The retrieval of ozone abundance from the lidar measurements required the development of a method to account for the interference from the substantial aerosol content within the polluted boundary layer.

1. Introduction

The oil sands mining and upgrading facilities in northern Alberta are a known source of air pollution (Simpson et al., 2010; Liggio et al., 2016). The Joint Canada-Alberta Implementation Plan for Oil Sands Monitoring (JOSM) was organized by Environment and Climate Change Canada (ECCC) to monitor the impact of oil sands emissions on the quality of air, water, land, and wildlife (Abbatt et al., 2011). This paper concerns the measurement technique and results of airborne lidar measurements of aerosol and ozone that were contributed to the JOSM field campaign during August 2013. A lidar instrument

from York University was installed on a Twin Otter aircraft in order to complement the main research aircraft for the JOSM flight campaign, the Convair-580 from the National Research Council of Canada (Gordon et al., 2015; Liggio et al., 2016).

5   Emissions from the oil sands facility stacks and mining operations include nitrogen oxides (NO and NO_2), sulfur dioxide (SO_2), sulfate (SO_4), methane (CH_4), carbon dioxide (CO_2), carbon monoxide (CO), particulate matter, volatile organic compounds (VOC), and secondary organic aerosol (SOA) (Simpson et al., 2010; Davies, 2012; Howell et al., 2014; Liggio et al., 2016; Li et al., 2017; Baray et al., 2017). Large amounts of NO_x and SO_2 emissions within the oil sands region originate from the
10   upgrading processes and high temperature combustion of oil, gasoline, and coal. The facilities are surrounded by boreal forests which are a natural source of biogenic VOC emissions and also smoke emissions from forest fires. Enhancements in ozone are well known to occur in urban air pollution due to the photochemical reactions involving NO, NO_2, VOCs, and sunlight (Crutzen, 1979, Banta et al., 1998, 2005; Valente, 1998; Langford et al., 2010a; Senff et al., 2010). The exposure to O_3 levels higher
15   than the background can result in damage to biological tissue in crops and living organisms (Haagen-Smit, 1952), and decrease the rate of photosynthesis in plants (Morgan et al., 2003).

       The airborne lidar measurements were carried out to assess whether a substantial amount of ozone was generated from the oil sands industrial emissions. The field campaign with the lidar on board a
20   Twin Otter aircraft consisted of five flights out of Fort McMurray during the period between August 22 and August 26, 2013. The ozone mixing ratio was measured in the unpolluted air upwind, in the polluted air directly above the oil sands operations, and as far as 150 km downwind. The only observed enhancement in ozone occurred in a layer above the polluted boundary layer and air trajectory analysis linked this to forest fire emissions. The measurement technique, analysis methods, results, and
25   interpretation are described in the following sections.

2. Measurement Technique

The differential absorption lidar instrument shown in Figs. 1 and 2 was installed on a Twin Otter aircraft and viewed downward for vertical profile measurements of ozone and aerosol. The lidar transmitter consisted of a Q-switched Nd:YAG laser with second and fourth harmonic generation for emitting pulsed light with wavelengths of 532 nm and 266 nm at a repetition rate of 20Hz. The pulsed light with a wavelength of 266 nm was focused into a cell filled with CO_2, at a pressure of 965 kPa, to generate light at wavelengths of 276.2 nm, 287.2 nm, and 299.1 nm by stimulated Raman scattering (Nakazato et al., 2007). The maximum laser pulse energy was 80 mJ at a wavelength of 266 nm and the Raman conversion efficiency was about 29 % with pulse energies of 10 mJ, 8 mJ at and 5 mJ for the 276 nm, 287 nm and 299 nm wavelengths respectively. The fourth harmonic generation was quite sensitive to temperature and the 266 nm output from the laser was typically in the range of 60 to 80 mJ. The Raman conversion thus varied as well in a nonlinear fashion. The UV wavelengths were directed into the atmosphere along the nadir from the Twin Otter aircraft. The laser light at a wavelength of 532 nm was directed independently into the atmosphere along the nadir.

A 15 cm diameter off axis parabolic mirror with a focal length of 500 mm was used to collect the light that was scattered back from molecules and aerosol particles. Two separate optical fibers were positioned behind field stop apertures with diameters of 0.5 mm and 1.0 mm that determine fields of view of 1.0 mrad for the 532 nm and 2.0 mrad for the UV backscatter signals. The four UV wavelengths (266, 276.2, 287.2, and 299.1 nm) were separated in the receiver using the transmittance and reflectance from interference filters having a bandwidth of 1 nm and tilted at an angle of 7.5 degrees. Photomultiplier tubes (Hamamatsu R9880) were used to detect the backscattered light. Photon counting was used to record the weak signals from distances greater than 1.5 km and analog to digital conversion was used for strong signals in the near range. The vertical range bin was 3.75 m for the 532 nm signal and 7.5 m for the UV signals, while the in-flight temporal averaging was 10 seconds for both the UV and 532 nm signals.

An in-flight visualization tool was used for preliminary real time data analysis and this informed decisions on the flight track. The program provided contour plots of the 532 nm aerosol scattering ratio and the O_3 mixing ratio as measurements were being collected. Line plots of aerosol backscatter and O_3 mixing ratio were displayed at the location the cursor was placed on the contour plot for profile-by-profile analysis during the flight.

3. Analysis of Lidar Measurements

The backscattered optical power as a function of range z is described by the lidar equation as

$$P_\lambda(z) = \frac{C}{z^2}\ \beta(\lambda, z)\ exp\left[-2\int_0^z \left(\sigma_\lambda\, N_{O_3}(z) + \alpha(\lambda, z)\right) dz\right] \tag{1}$$

The constant C includes the emitted pulse energy, sampling interval, telescope area, optical throughput, and detection efficiency. The backscatter coefficient, $\beta(\lambda, z)$, is the fraction of the laser light pulse scattered back to the receiver per unit length through the atmosphere and per unit solid angle. The exponential term represents the round trip transmittance of the laser pulse between the lidar and range z. The extinction coefficient, $\alpha(\lambda, z)$, is the fractional decrease in the laser pulse intensity per unit length in the atmosphere due to scattering. For this experiment, the molecule under investigation is O_3 with an absorption cross section of σ_λ. Temperature-dependent O_3 absorption cross sections were obtained from the HITRAN 2012 database (Rothman et al., 2013). The number density of O_3 molecules in the atmosphere is represented by $N_{O_3}(z)$ in Eq. (1) and the product $\sigma_\lambda\, N_{O_3}(z)$ represents the fractional decrease in the laser pulse intensity per unit length due to the absorption by O_3.

The differential absorption lidar technique was used to determine the mixing ratio of O_3. It is based on the difference between the absorption cross sections of two transmitted wavelengths. The measurement wavelength with larger ozone absorption cross section is referred to as the ON wavelength, λ_{ON}, and the wavelength with smaller absorption cross section as the OFF wavelength, λ_{OFF}. Starting from the ratio of separate lidar equations for the ON and OFF wavelengths, the number density of ozone can be extracted by taking the natural logarithm and differentiating with height

$$\hspace{4em} [A] \hspace{6em} [B] \hspace{6em} [C]$$

$$N_{O_3}(z) = \frac{-1}{2(\sigma_{O_3,ON} - \sigma_{O_3,OFF})} \left[\frac{d}{dz}\left(ln\left(\frac{P_{\lambda_{ON}}(z)}{P_{\lambda_{OFF}}(z)} \right) \right) - \frac{d}{dz}\left(ln\left(\frac{\beta(\lambda_{ON},z)}{\beta(\lambda_{OFF},z)} \right) \right) \right] - \left[\frac{\alpha(\lambda_{ON},z) - \alpha(\lambda_{OFF},z)}{(\sigma_{O_3,ON} - \sigma_{O_3,OFF})} \right] -$$

$$\left[\frac{(\sigma_{SO_2,ON} - \sigma_{SO_2,OFF})}{(\sigma_{O_3,ON} - \sigma_{O_3,OFF})} \right] N_{SO_2}(z) \hspace{12em} (2)$$

$$\hspace{4em} [D]$$

Term A in Eq. (2) represents the O_3 number density calculated directly from the lidar signals. The terms B and C in Eq. (2) are corrections for the wavelength dependence in the backscatter and extinction coefficients and term D is a correction for other gaseous molecules that absorb UV radiation, such as SO_2. The number density of SO_2 molecules in the atmosphere is represented in Eq. (2) by $N_{SO_2}(z)$. The O_3 mixing ratio could be derived from six different ON/OFF wavelength pair combinations from the four UV wavelengths that were transmitted by the lidar. The O_3 absorption coefficients were obtained from the HITRAN database (Rothman et al., 2013).

The recorded signals were smoothed in the vertical with a running (or sliding) boxcar average over 5 points (18.75 m) for the 532 nm signal and 5 points (37.5 m) for the UV signals. In order to reduce the uncertainty in the O_3 measurements, temporal averaging was applied over 1.5 minutes, corresponding to a distance of about 7.5 km along the path of the aircraft. The vertical derivative in term A of Eq. (2) was calculated using a running (or sliding) linear least squares fit over 19 points with the ozone value assigned to the midpoint. The distance between entirely independent ozone values was

then 180 m. Complete overlap between the transmitted laser pulses and the field of view of the telescope occurred at distances greater than 300 m and signals recorded nearer to the aircraft were not used in the analysis. Measurements within clouds have also not been used for retrieving ozone density.

5   Figure 3a shows an example of backscatter signals (after averaging) recorded from below the aircraft at wavelengths of 266, 276, and 299 nm and Fig. 3b shows the corresponding O_3 volume mixing ratio. This was determined by dividing the derived O_3 number density by the total atmospheric molecular number density, which was calculated using temperature and pressure data from radiosondes launched at the City of Edmonton (430 km south of Fort McMurray). For the O_3 measurements

10   presented in this paper, analog (ADC) signal acquisition with the wavelength pair 276/299 nm was used above the top of the boundary layer, while photon counting data acquisition with the wavelength pair 266/299 nm was used within the polluted boundary layer. The height of transition was always a minimum of 300m above the top of the boundary layer. The 266/299 and 276/299 ozone profiles were calculated separately and were within the margin of uncertainty where overlapping in height above the

15   boundary layer (e.g. Fig. 3b). The transition was at a single height.

3.1 Correction for Aerosol Interference in the Lidar Ozone Retrieval

When the amount of aerosol in the atmosphere is insignificant, term B in Eq. (2) is very small and term C is straightforward to calculate since it includes only molecular scattering. When there is a significant amount of aerosol present, terms B and C in Eq. (2) can result in large uncertainties if the aerosol

20   contributions to the backscatter and extinction coefficients are not accounted for. Previously applied methods for correcting the interference of aerosol in the O_3 lidar retrieval were based on the use of a power law wavelength dependence in the extinction and backscatter coefficients with an assumed Angstrom exponent (e.g. Browell et al., 1985; Alvarez et al., 1998), iteration (Alvarez II et al., 2011), or use of three wavelengths (Eisele and Trickl, 2005). For the study reported here, aircraft based in situ

25   measurements of aerosol particles size distribution were available and these data were used to determine the UV backscatter and extinction coefficients for calculating the aerosol correction terms in Eq. (2). There was no need to estimate the wavelength dependence with a power law Angstrom exponent.

The aerosol backscatter and extinction coefficients at the UV wavelengths were derived by making use of the lidar signal at a wavelength of 532 nm and in situ measurements of aerosol size distribution obtained on the NRC Convair-580 aircraft that was operated for ECCC as part of the JOSM program. Particles with diameters in the range 0.03 to 1 μm were sampled with the UHSAS instrument (Cai et al., 2008) and larger particles ranging in diameter from 0.3 to 20 μm were measured with the FSSP-300 instrument (Baumgardner et al., 1992).

The steps involved in accounting for aerosol in the derivation of ozone from the lidar measurements are summarized as follows:

A) Aerosol optical properties derived from the lidar backscatter signal at a wavelength of 532 nm

The profile of extinction and backscatter coefficients was derived from the recorded lidar backscatter signal at the wavelength of 532 nm. The absorption by ozone is not significant at this wavelength so the backscatter and extinction coefficients can be derived from the data independent from the ozone measurement. The method of Fernald (1984) was employed and this required a reference value for the extinction coefficient at a particular height and also the ratio of extinction to backscatter coefficients (the lidar ratio). The reference height was a minimum of 200m above the top of the boundary layer. The aerosol extinction and backscatter coefficients at the reference height were estimated by using in situ measurements of particle size distribution, *N(r)*, during a Convair flight on August 23, 2013 above the boundary layer and integrating over all particle sizes as follows:

$$\alpha_{aerosol}(\lambda_{532}) = \int_0^\infty \pi r^2 \, Q_{ext}(m, r, \lambda_{532}) \, N(r) \, dr \tag{3}$$

$$\beta_{aerosol}(\lambda_{532}) = \int_0^\infty \pi r^2 \, Q_{back}(m, r, \lambda_{532}) \, N(r) \, dr \tag{4}$$

The aerosol extinction and backscatter efficiencies (Q_{ext} and Q_{back}) were determined from the in situ size distribution measurements with calculations based on the theory of Mie scattering for spherical particles (Bohren and Huffman, 1983). A software module was used to evaluate Maxwell's equations for

scattering and absorption of light by homogenous spherical particles. The calculation required a value of the complex refractive index of particles, m, at the measurement wavelength in order to compute the extinction and backscatter efficiencies.

It was assumed that within the boundary layer the particles large enough to contribute significantly to the lidar backscatter signal were mineral dust lofted by mining operations. The particle refractive index corresponding to the mineral kaolinite was used (Table 1). Kaolinite is a clay mineral composed of aluminum silicate. Studies done by Cloutis et al. (1995), Omotoso and Mikula (2004), and Mercier et al. (2008), have found kaolinite to be the prominent clay particle in the oil sands region.

The in situ particle size distribution measurements acquired directly over the oil sands region within the boundary layer, at an altitude of 785 m ASL, were used to calculate the value of the lidar ratio as 31 sr at a wavelength of 532 nm. This was used for the Fernald algorithm to derive the extinction and backscatter coefficient height profiles at a wavelength 532 nm. It was assumed that the lidar ratio was independent of height, which corresponds to an assumption that changes in the optical extinction and backscatter coefficients are attributed to variation in aerosol concentration and not changes in the particle size distribution.

B) Height profile of aerosol UV backscatter and extinction coefficients from combined lidar and in situ measurements.

The lidar 532 nm aerosol extinction coefficient was combined with the in situ measurements of aerosol properties to derive the height profile of aerosol number density as follows:

$$\frac{N_{aerosol}(z)}{N_0} = \frac{\alpha_{aerosol}(\lambda_{532},z)}{\int_0^\infty \pi r^2 \, Q_{ext}(m,r,\lambda_{532}) \, N(r) \, dr} \tag{5}$$

The numerator on the right side of the equation is the extinction coefficient derived from the lidar measurements at the wavelength of 532 nm. The denominator is the extinction coefficient calculated from the in situ measurements on the Convair aircraft at a single height. As before, N(r) is the measured

The backscatter and extinction coefficients as a function of height at the UV wavelengths can be derived as

$$\alpha_{aerosol}(\lambda_{UV}, z) = \frac{N_{aerosol}(z)}{N_0} \int_0^\infty \pi r^2 \, Q_{ext}(m, r, \lambda_{UV}) N(r) \, dr \tag{6}$$

$$\beta_{aerosol}(\lambda_{UV}, z) = \frac{N_{aerosol}(z)}{N_0} \int_0^\infty \pi r^2 \, Q_{back}(m, r, \lambda_{UV}) N(r) \, dr \tag{7}$$

It was assumed that the shape of the aerosol size distribution from the in situ measurement is applicable throughout the boundary layer. The ratio $N_{aerosol}(z)/N_o$ provides a scaling factor that accounts for changes in the total number density.

C) Aerosol correction in the ozone retrieval

The calculated aerosol extinction and backscatter coefficients at the UV wavelengths were substituted into terms B and C in Eq. (2). Figures 4b, 4c, and 4d show the computed values for the first three terms in Eq. (2) for the measurements taken on August 23, 2013, directly over the oil sands industry where significant aerosol was observed within the boundary layer.

indices used for the calculations are provided in Table 1. The red shaded area in Figs. 4c, 4d, and 4e represents the range of aerosol correction values computed with the various particle compositions and size distributions. This represents an estimate of the amount uncertainty due in the aerosol correction.

For the case presented in Figs. 3 and 4 there is significant aerosol loading as indicated with the profile of aerosol optical extinction coefficient (Fig. 4a). Term B in Eq. (2) (Fig. 4c) contributed a maximum correction of -5 to -8 ppbv at a height of 1.1 km where there was gradient in the aerosol content at the top of the boundary layer. At lower heights within the boundary layer where there was a smaller gradient in the amount of aerosol (altitudes below 0.8 km in Fig. 4a) the contribution of term B in Eq. (2) was much less. The aerosol contribution to the differential extinction, term C in Eq. (2), shown in Fig. 4d was proportional to the aerosol extinction coefficient and had a maximum contribution with a range of 1 to 6 ppb near the ground. So in this case the total amount of correction due to aerosol ranged from -5 ppbv to 10 ppbv at the top of the boundary layer and 1 to 6 ppbv near the ground. The uncertainty associated with the aerosol correction within the polluted boundary layer was ± 2.5 ppbv in this case. The relative uncertainty due to statistical variations in photon counting or shot noise in the analog detection is indicated as the grey shading in the uncorrected profile in Figs. 4b and 4e. This reached a maximum of ± 4 ppbv near the ground. The sum of the statistical uncertainty and aerosol correction uncertainty is shown as the shaded region in the profiles in Fig. 3. In cases further downwind from the Oil Sands extraction facilities, the aerosol loading was much smaller, as was the aerosol correction and the associated uncertainty. Examples of profiles with smaller aerosol correction are shown in Fig. 15.

The magnitude of the aerosol correction in the retrieved ozone mixing ratio (Fig. 4) was within the range of what has been reported from previous ozone lidar studies that employ different methods for calculating the aerosol extinction and backscatter coefficients at UV wavelengths (Alvarez et al., 1998; Eisele & Trickl, 2005). As reported in the literature the aerosol correction was small (< 3 ppbv) in regions of low aerosol loading or in regions where the vertical gradient in the backscatter coefficient was small (Sullivan et al., 2014). Greater aerosol corrections of 15 to 35 ppbv have been calculated due

to the presence of large aerosol gradients at the top of the boundary layer (e.g. Alvarez et al., 1998; Eisele and Trickl, 2005).

Forest fire smoke was observed in the lidar measurements for the flight on August 24, 2013 and the results are shown in Sec. 5.2. The correction in the lidar ozone retrieval due to the interference of forest fire aerosol was carried out in a similar manner to that described above. In situ particle size distribution measurements in a layer of forest fire smoke were acquired on the Convair-580 aircraft during an ascent above the boundary layer approximately an hour before the time that the lidar observed the layer of smoke at the same height. The complex refractive index of forest fire aerosol that was used in this correction method is listed in Table 1. The lidar ratio at a wavelength of 532 nm was found to be 65 sr from Mie scattering calculations with the in situ particle size distribution and refractive index for smoke particles. It was found that the correction due to the interference of forest fire aerosol decreased the ozone measurement by a maximum of 7 ppbv. There was some uncertainty since the Convair in situ measurements used in the correction method were taken one hour before the time the lidar observed the layer of forest fire smoke. Different aerosol size distributions from previous studies of biomass burning (Chakrabarty et al., 2006; Pirjola et al., 2015) were also used to assess the uncertainty in the aerosol correction and a maximum correction of -5 ppbv was calculated.

Term D in Eq. (2) represents the interference by SO_2, which absorbs with varying optical cross section within the range of UV wavelengths used for the ozone retrieval. For the measurements presented in this paper, the 266/299 wavelength pair was used to retrieve ozone concentration within the boundary layer since the interference from SO_2 was a minimum in comparison to the other wavelength pairs. The value of the absorption coefficients found in the literature for a given wavelength are different for each reported study. For example, the bias in the derived ozone due to SO_2 for the wavelength pair 266/299 nm is 0.2% of the SO_2 concentration using the values from the HITRAN database (Rothman et al., 2013), 0.6 % using the values from Vandaele et al (2009), and 1.1% using the values reported by Bogumil et al. (2003). In situ SO_2 measurements were acquired on the Convair-580 aircraft and mixing ratios typically ranged between 30 and 150 ppbv within the boundary layer. An SO_2

3.2 Corrections for Detection Nonlinearity and Signal Induced Noise

For weak signals measured with the photomultiplier detectors the photon count rate is proportional to the incident optical power. At high count rates (greater than 10 MHz), the photon counting signal does not respond linearly to the optical power due to overlapping pulses from the detector being counted

10   erroneously as a single pulse. The detection system is unable to count separate individual pulses accurately within a certain time period commonly referred to as dead time t_d (Donovan et al., 1993). A dead time correction was applied to the raw photon counting data by calculating the true count rate N_T, in terms of the measured count rate N_m, as $N_T = N_m/(1 - N_m \times t_d)$. The true count rate was found by using a value of dead time for which the ratio of N_T to the recorded analog signal is constant up to a count rate

15   of 100 MHz. Unique photon counting dead times were determined for each of the five individual photomultiplier detectors and the values ranged from 4.5 to 7.5 nsec. The optimal dead time correction at each wavelength was determined from lidar measurements acquired along one leg of the Twin Otter flight on August 22, 2013 and these dead time corrections were applied to the measurements collected on all subsequent flights. The value of dead time correction at each wavelength was consistent

20   throughout the campaign for each detector.

Another correction was applied to the UV signals in order to remove a residual decaying signal in the far range. Strong UV signals in the near range can introduce a residual decaying signal in the far range, most commonly referred to as the signal induced noise or signal induced background. The cause

25   of this signal induced noise/background is likely UV fluorescence from the detector (Zhao, 1999) and this occurs only in the UV wavelength range. This residual signal had an amplitude that was proportional to the relatively large signal amplitude at near range. It can be modeled by an exponential

function (Sunesson et al., 1994). The residual signal was corrected by fitting an exponential decay function to the signal recorded at distances beyond the ground, where there is no backscatter signal. The exponential fit was then subtracted from the lidar backscatter signal.

4 Air Trajectory Calculations

5   The Hybrid Single Particle Integrated Trajectory (HYSPLIT) model (Stein et al., 2015) was used to predict the trajectory of the emissions released from the oil sands in both the forward and backward directions. Forward air trajectories from the oil sands locations were used for flight planning and backward air trajectory calculations were used in the analysis to reconstruct the past motion of air parcels. The HYSPLIT model was accessed through the NOAA ARL READY website

10   (http://www.arl.noaa.gov/HYSPLIT.php) and the trajectories were computed by using the Global Data Assimilation System (GDAS) meteorological dataset with a resolution of 1 degree. The uncertainty in the trajectory calculation from the HYSPLIT model has been assessed to be less than 20% of the travel distance over a travel time of 48 hours (Baumann & Stohl, 1997). In this paper, air trajectories were used in the interpretation of the lidar measurements. The largest travel time for a backward trajectory

15   used in the analysis was 10 hours. The uncertainty in the air trajectory related to a travel time of 10 hours did not affect the final interpretation or conclusions derived from using these trajectories.

5. Observations

The Twin Otter flight segments were straight and usually oriented either parallel or perpendicular to the wind direction. The goal was to obtain measurements in regions upwind and downwind from the oil

20   sands pollution emission sources. The path of the Twin Otter aircraft for each of the 5 flights during the campaign is shown in Fig. 5. The wind direction used for flight planning was from a forecast, but the wind direction indicated on each map was obtained from the back trajectory analysis (GDAS dataset). The conditions during each flight were clear with occasional fair weather cumulous, ground temperatures not greater than 20° C, and a few showers at the most northern flight legs during the flight

25   on August 24, 2013.

5.1 Industrial Pollution

A typical flight leg from August 23, 2013 that covered areas upwind, above, and downwind from the oil sands industry is shown in Fig. 6. The altitude of the aircraft was 2.95 km above sea level (ASL). The aerosol optical extinction coefficient and the ozone mixing ratio derived from the lidar measurements along this flight leg are shown in Fig. 7. Measurements collected upwind of the industry (within 20 km from the start of the flight leg) in Fig. 7a show small amounts of background aerosol present in this region. Directly above the oil sands industry (distances of 25 to 75 km along the flight track) significant amounts of aerosol were observed to be mixed to heights of up to 1.5 km ASL (about 1 km above ground). Downwind of the industry (distances of 90 to 120 km along the flight leg) the aerosol was dispersed to heights of up to 2.3 km ASL (or 1.6 km above ground). The depth of the boundary layer was apparent from the vertical range over which the aerosol was mixed. A flue-gas desulfurization (FGD) stack was intersected at 57°03' N and 111°39' W in Fig. 6. The vertical plume from the stack is clearly seen in the lidar aerosol measurement in Fig. 7a as the presence of a vertical extension in the depth of the aerosol layer at the distances of 55 to 60 km from the start of the flight leg.

Figure 7b shows the corresponding ozone mixing ratio along the flight segment. Regions of reduced ozone mixing ratio between 17 and 32 ppbv were measured in the polluted boundary layer directly above the oil sands industry (distances from 40 km to 60 km along the flight leg). The ozone mixing ratio upwind and downwind from the industry varied between 27 and 40 ppbv.

A case is presented in Figs. 8 and 9 with a segment of the flight on August 22, 2013 that was oriented transverse to the path of the air that passed over the oil sands industry, approximately 100 km downwind. The flight segment was south along longitude 110° W between positions I and J (Fig. 8), and the corresponding lidar measurements are shown in Fig. 9. The optical extinction coefficient derived from the lidar measurements (Fig. 9a) indicated that the depth over which the aerosol was mixed from the ground ranged from 1.5 to 2 km ASL (1.0 to 1.5 km above ground). The O_3 mixing ratio (Fig. 9b) within the boundary layer varied between 28 and 42 ppbv throughout the flight segment. Ozone mixing ratios greater than the background were not observed.

Backward air trajectories were calculated from locations along all of the Twin Otter flight tracks during the campaign. For each measurement location, the time was determined for the air to travel between the oil sands industry and the position of the lidar measurement from the Twin Otter. Only the trajectories that passed over the oil sands industry were selected for this analysis. Figure 10 shows lidar measurements of the aerosol optical extinction coefficient and O_3 mixing ratio as a function of time taken by the air to travel between the oil sands industry and the measurement point. The measurements were averaged within the height range of 500 m to 800 m ASL. As expected, Fig. 10a shows that larger values of aerosol optical extinction coefficient occur closer to the pollution source area and decrease moving away from the source. The observed O_3 mixing ratios in Fig. 10b showed no trend with time or distance from the industry. There is no evidence of increasing O_3 for up to 10 hours downwind of the oil sands industrial areas. The only deviation from the background were instances of smaller ozone mixing ratios.

5.2 Forest Fire Emissions

A case with air pollution from both natural and industrial sources is described in this section. Airborne lidar measurements to the north of Fort McMurray were made on August 24, 2013 and the corresponding flight path is shown in Fig. 11. In this flight leg, the Twin Otter started at point A, a distance of ~90 km to the east of the oil sands industry and travelled westbound to point B along constant latitude of 57°06' N.

In the contour plot of optical extinction coefficient (Fig. 12a) there was a layer of aerosol in the height range 1.5 to 2.5 km ASL at distances of 0 to 90 km from point B, and this layer was separated from the industrial pollution in the surface boundary layer. The aerosol from the oil sands industrial emissions was confined within the depth of the boundary layer, below a height of 1.2 km ASL at distances of 20 km to 60 km from point B. It was observed visually from the aircraft that the separated aerosol layer above the boundary layer originated from forest fires to the southwest. This was consistent with the approximate locations of forest fires provided from the Alberta Forestry and Emergency

Response Division as indicated in Fig. 11. A backward trajectory is shown in Fig. 11 that was initiated from an altitude of 2.0 km at the time and location of the lidar measurement of the aerosol layer that was observed to be separated above the boundary layer. The air containing the separated aerosol layer had passed over the vicinity of the forest fires southwest of the flight track. This aerosol layer is considered to be forest fire smoke.

The O_3 mixing ratio measured with the lidar along this flight segment is shown in Fig. 12b. The O_3 mixing ratio reached a maximum of 70 ppbv at a height of 2 km, within the separated aerosol layer (distances 15 km to 40 km from point B) that originated from the region of forest fires. In the pollution from the oil sands industry (below the forest fire smoke layer), significant amounts of aerosol were observed in which the O_3 mixing ratio varied between 10 and 33 ppbv. In the eastern half of the flight leg the O_3 mixing ratios were consistent with background values (23 – 32 ppbv).

5.2.1 Ground Based Lidar Polarization Measurements

A ground based lidar was operated by Environment and Climate Change Canada (ECCC) at the location AMS 13, which was approximately 5 km north of the Twin Otter flight track as indicated in Fig. 11. The ECCC lidar observed a distribution of aerosol that was similar to the airborne lidar measurements in Fig. 12a. It detected the same layer of forest fire smoke in the height range of 1.5 to 2.5 km ASL. The ECCC lidar had an additional capability for measuring the polarization in the backscatter signal. The ratio of the perpendicular to parallel components of polarization, relative to the transmitted polarization, in the aerosol backscatter signals (the depolarization ratio), provides an approximate method for discriminating between particles of different sizes and shapes. For example, hexagonal ice crystals can cause a depolarization ratio greater than 0.5, and spherical water droplets result in a small (almost zero) depolarization ratio (Sassen et al., 1991). For this case, the depolarization ratio was used to discriminate between the aerosol from the oil sands operations and forest fire smoke.

The difference in the depolarization ratio between the industrial pollution and forest fire smoke is clearly seen in Fig. 13. The depolarization ratio throughout the forest fire smoke layer (altitudes of 1.5

km to 2.3 km) was measured to be 5-6% and this value is consistent with previous depolarization lidar measurements of forest fire aerosol (Mattis et al., 2004; Murayama et al., 2004; Pereira et al., 2014). The small values of the depolarization ratio measured in the smoke layer reveal a more spherical shape of forest fire particles. The depolarization ratio within the polluted boundary layer at altitudes below 1.2 km ASL had larger values in the range $7 - 10$ % due to the mixture of mineral dust and other emissions from the oil sands facilities. This provides further evidence that the separated layer at heights of 1.5 km to 2.5 km with the enhanced O_3 mixing ratio had originated from forest fires rather than industrial pollution.

5.3 Comparison Between Lidar and In Situ Measurements

The Twin Otter and Convair aircraft were not coordinated to fly along the same flight tracks. The airborne lidar measurements were taken over long and straight flight segments, while the in situ measurements were concentrating on specific emission sources during the period when both aircraft were operating. It was not possible to have a direct comparison between the lidar and in situ measurements with both aircraft simultaneously measuring the same volume of air. There were a few cases when the location where the Convair carried out a spiral ascent or descent could be linked to the location of the Twin Otter lidar measurements since the air trajectory passed through both locations.

Two cases are presented here where vertical profiles of O_3 mixing ratio derived from lidar measurements were compared with the in situ O_3 measurements that were acquired on the Convair-580 aircraft during spiral ascents on August 23, 2013. Locations are indicated in Fig. 14 as A-in situ and B-in situ (designated by a star-shaped symbol) where in situ measurements of the vertical profile of O_3 were collected during two spiral ascents with the Convair-580 aircraft. The Convair spiral ascent at the point labelled as A-in situ in Fig. 14 was carried out in polluted air above the industry. The Twin Otter did not pass directly over this point, but the lidar measurements used for comparison were obtained 2.5 hours later at a location along the Twin Otter flight track where the back trajectory of the air passed over point A-in situ. The in situ and lidar measurements of the vertical profiles of ozone mixing ratio are shown in Fig. 15a. The two separate measurements were within the limits of measurement

uncertainty throughout most of the overlapping height range (0.8 km to 1.2 km), where the O_3 mixing ratio was in the range 20–30 ppbv in the polluted air. At point B-Lidar in Fig. 14, the Twin Otter aircraft collected measurements at a distance of 12 km away from the location of a Convair spiral ascent. The air back trajectories did not pass over any pollution sources in the upwind direction and this is considered to be unpolluted air. The lidar and in situ measured O_3 mixing ratios shown in Fig. 15b were within the limits of uncertainty throughout the overlapping height range.

The statistical distribution of O_3 mixing ratio was also used for comparing the lidar and in situ measurements. Backward trajectories were computed from an altitude of 800 m ASL along all the Twin Otter and Convair flight tracks during the August 22 to August 26 time period. The trajectories were separated into two categories. The air trajectories that did not pass over the oil sands industry were categorized as unpolluted air and the trajectories that passed over the industry were categorized as polluted air. In situ measurements of O_3 were acquired at a single altitude between 550 and 900 m ASL and the lidar measurements were averaged between altitudes of 550 m and 900 m ASL for this analysis. The in situ and lidar measurements were both averaged for 1.5 minutes along the flight tracks. Figure 16a shows the histograms of the O_3 measurements in unpolluted air for both the lidar and in situ measurements collected within the surface boundary layer. The lidar and in situ histograms for the unpolluted air are very similar with a peak occurrence at around 30 ppbv, and with values distributed between 12 and 45 ppbv. For the polluted air, the O_3 measurements were distributed between 10 and 50 ppbv, but the in situ histogram was not as symmetrical, with peaks at about 25 ppbv and 35 ppbv compared to a more normal distribution with a peak at 32 ppbv for the lidar measurements. The in situ measurements were almost always obtained directly above the region of oil sands surface operations, but the lidar polluted air measurements were also obtained down wind to distances of up to 150 km from the oil sands emissions. In both the vertical profile (Fig. 15) and statistical (Fig. 16) comparisons the lidar and in situ measurements were consistent with the general result that the O_3 mixing ratio in the polluted air was smaller than or equal to the background O_3 abundance.

6 Discussion

A general result from the lidar measurements was that the amount of O_3 in the polluted air directly above the oil sands operations was smaller than or equal to the amount in the background unpolluted air. The in situ measurements of NO, NO_2, and O_3 from the Convair-580 aircraft were used to

5   investigate the reason for the cases in which the O_3 abundance was less than the background. A flight segment of the Convair aircraft on August 23, 2013 (between 11:27 and 11:37 AM local time) that travelled eastward at a constant altitude of 650 m ASL while intersecting the oil sands industry is shown in Fig. 17. Figure 18 shows the in situ measurements of O_3, NO, and NO_2 mixing ratio along the Convair flight segment shown in Fig. 17. In regions upwind and further downwind of the oil sands

10   industry, the amount of NO was measured to be less than 2 ppbv while the O_3 mixing ratio ranged between 25 and 30 ppbv. Directly over the oil sands industry (the region in Fig. 18 contained within the dashed lines), the mixing ratio of NO increased to 25 ppbv while the ozone mixing ratio decreased from 30 ppbv to 13 ppbv. The reduction in O_3 over the industry is consistent with NO titration: $NO + O_3 \rightarrow NO_2 + O_2$. The sum of the NO_2 and O_3 mixing ratios in Fig. 18 remained relatively constant, such that

15   the decrease in O_3 was approximately compensated by an increase in NO_2.

Another way to describe this is in terms of odd oxygen, O_x ($O_3 + NO_2$) (Brown et al., 2006). The O_x mixing ratio (shown in Fig. 18) remained relatively constant along the flight track, with a slight increase within the industrialized portion of the track despite the significant decrease in O_3. The

20   decrease in O_3 was slightly more than compensated by the increase in NO_2, which is entirely consistent with a titration of O_3 in a combustion plume where the NO_x composition of the source is mostly NO (e.g., ~90% NO, 10% NO_2), with negligible photochemical formation of O_3 close to the source.

It was observed that O_3 mixing ratios at distances as far as 150 km downwind of the pollution

25   sources, and up to ten hours since emission, were in the range of the regional background levels. There were no observed enhancements in O_3 and this is consistent with previous measurements of O_3 in the Fort McMurray oil sands region (Rudolph, 2004). This result was different from what has normally been observed in polluted air. For example, previous studies of air pollution surrounding the power

plants, refineries, and petrochemical industry near Houston, Texas have observed that O_3 mixing ratios greatly exceeded the regional background (Banta et al. 2005, Senff et al., 2010; Langford et al. 2010b). One obvious difference in comparing the Fort McMurray region to Houston is the temperature. The air temperatures measured from the Convair aircraft over the Fort McMurry oil sands region during late

5 August 2013 were less than 20° C. The surface temperatures in the vicinity of Houston reported by Senff et al. (2010) were in the range of 30° C to 42° C. It is well known and documented that episodes of substantial ozone generation due to pollution occur in hot and stagnant conditions (e.g. Banta et al, 1998; Valente et al., 1998; Jacob et al., 1993, 2009; Lin et al., 2001; Camalier et al., 2007; Coates et al., 2016; Shen et al., 2016).

In addition to the relatively cold temperatures, the conditions could not be characterized as stagnant (Camalier et al., 2007) for most of the flights above the oil sands region. Figure 19 shows the 24 hour back trajectory for each day of the Twin Otter flight campaign at midday. With the exception of August 25th, 2017, the air had travelled at least 200 km in the 12 hours prior to passing over the oil

15 sands region. An increase in the aerosol layer depth downwind of the oil sands emissions (e.g. Fig. 7) provided evidence for vertical mixing. As the pollutants mixed with the clean background air, O_3 mixing ratios downwind of the industry gradually increased to between 25 and 40 ppbv and were consistent with background levels.

20 The absence of enhanced ozone in pollution downwind of the industry is interpreted here as being a result of meteorological conditions that were not favourable for the generation of ozone. These factors include (A) ambient temperatures not greater than 20° C, (B) no regional stagnation of air, and (C) vertical mixing of the polluted air with clean background air.

25 An enhancement in the ozone abundance was detected in the forest fire emissions that were encountered above the boundary layer (Fig. 12b). It has been established previously that forest fire emissions include the precursors for generation of ozone (e.g. Jaffe and Wigder, 2012). In this case the environmental conditions were also more favourable for generation of ozone. The layer remained well

defined and separated from the turbulent boundary layer. It was not subjected to ventilation from the boundary layer convection cells, and the mixing with background air was weak enough that ozone generation could proceed in the middle of the layer.

7 Conclusion

A lidar instrument for measurements of atmospheric aerosol and ozone was developed for field deployment. It was installed on a Twin Otter aircraft for a flight campaign to study the impact of air pollution from the oil sands extraction industry in northern Alberta. A correction for the interference of aerosol was required for the retrieval of ozone concentration from the UV differential absorption lidar measurements in polluted air. An aerosol correction method was developed that made use of in situ measurements of the aerosol size distribution in combination with lidar measurements. It was found that the abundance of ozone in the pollution directly above the oil sands operations was reduced from what was measured in the background air. In situ measurements of NO, NO_2, and O_3 on board the separate NRC Convair-580 aircraft were used to show that the reduction in ozone abundance was consistent with NO titration. It was also found that there was no increase in ozone abundance in the industrial pollution, compared to background levels, as it was transported downwind to distances of 150 km and times of up to 10 hours. The lack of substantial ozone generation was attributed to conditions that were not favourable for the generation of ozone: low temperatures, lack of stagnation, and vertical mixing with clean background air. A layer of forest fire emissions that was separated from the turbulent boundary layer was observed to contain an increase in ozone abundance to 70 ppbv. This was consistent with the conditions being more favourable for ozone generation within the forest fire emissions since there was less turbulent mixing above the boundary layer.

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Composition	Refractive Index UV	Refractive Index Visible	Reference
Kaolinite	1.68 + 0.04i	1.572 + 0.006i	Arakawa et al., 1997
Ammonium Sulphate	1.507 + 0.005i (at λ = 355nm)	1.504 + 0i	Flores et al., 2012
Sulfuric Acid	1.383 + 0i (at λ = 360 nm)	1.366 + 0i (at λ = 556 nm)	Palmer and Williams, 1975
Toluene Secondary Organic Aerosol	1.58 + 0i (at λ = 300 nm)	1.50 + 0i	Nakayama et al., 2013 (Visible) Kozma et al., 2005 (UV)
Diesel Soot	1.62 + 0.55i (at λ = 400 nm)	1.68 + 0.56i (at λ = 550 nm)	Marley et al., 2001
Forest Fire Smoke	1.47 + 0.01i (at 440 nm)	1.61 + 0.06i	Wandinger et al., 2002 (Visible) Dubovik et al., 2001 (UV)
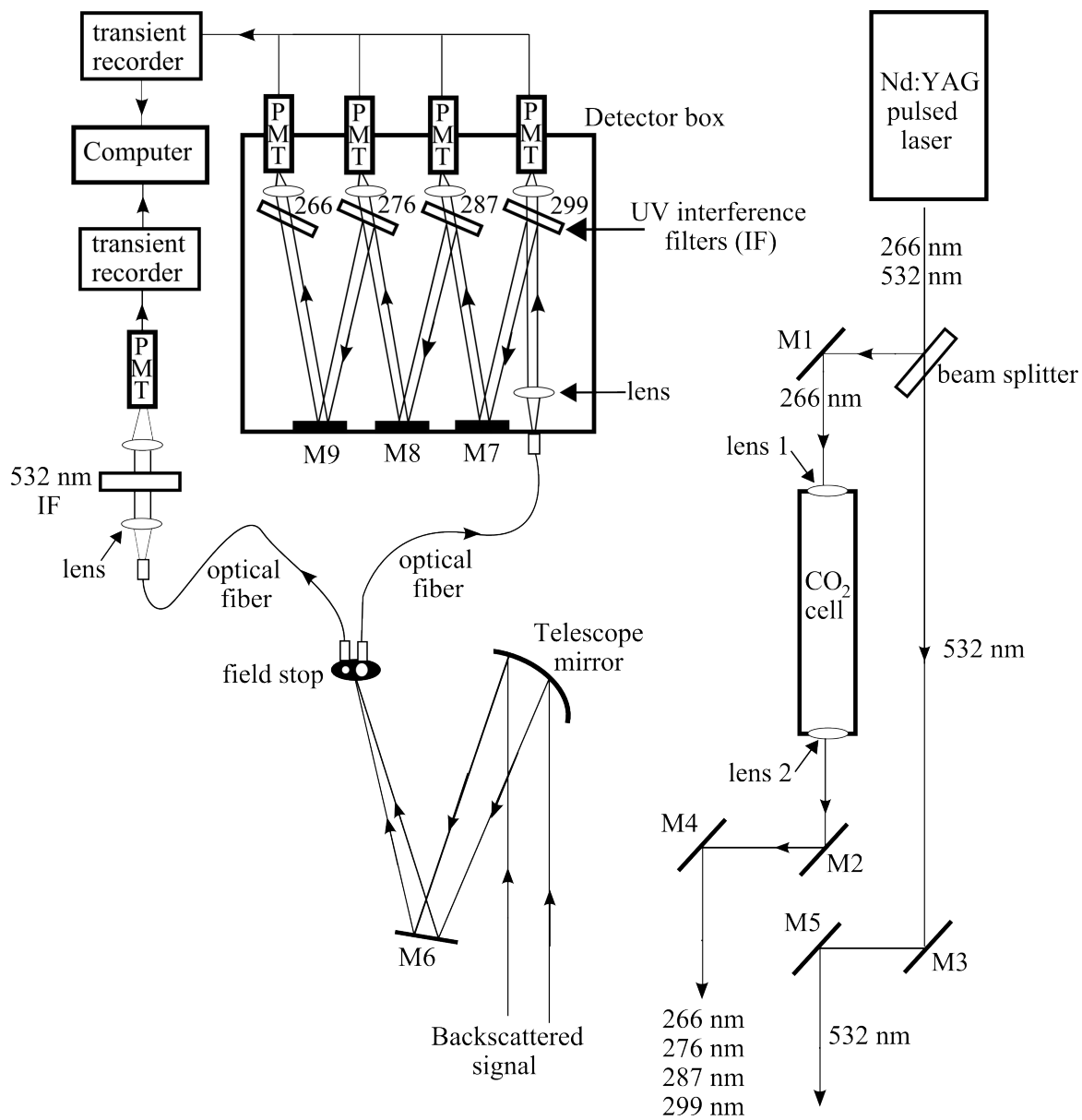
Figure 1: Schematic diagram of the differential absorption lidar system used for measurement of ozone and aerosol during the oil sands field campaign.
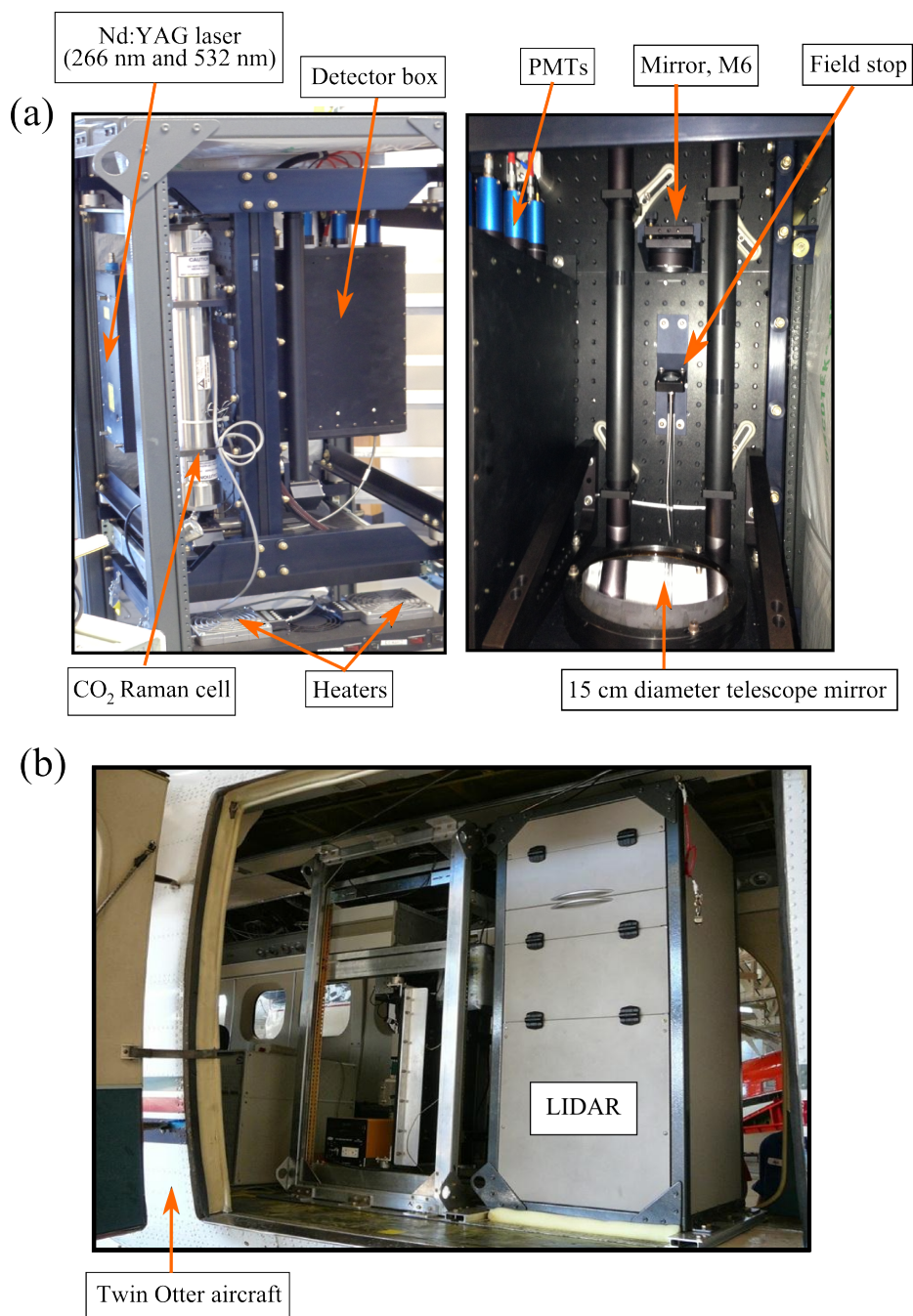
Figure 2: The lidar system installed (a) in the aircraft rack and (b) on the Twin Otter aircraft.
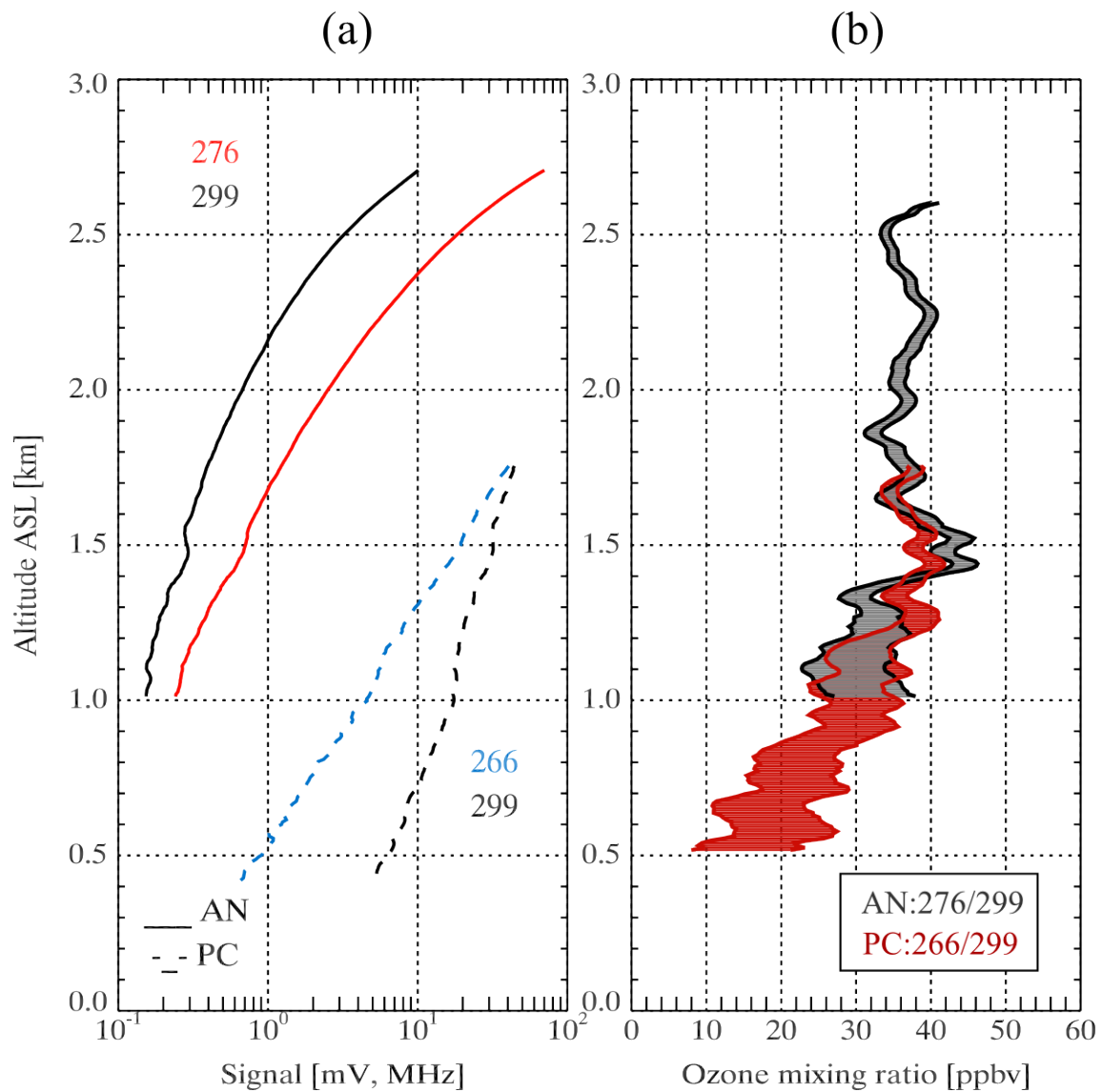
Figure 3: (a) Lidar backscatter signals for the analog (AN) and photon counting (PC) measurements. Altitude is above sea level, ASL. **(b)** The O₃ mixing ratio derived by using the AN:276/299 and PC:266/299 wavelength pairs. The shading represents the sum of the relative statistical uncertainty (from ± one standard deviation in photon counting or shot noise in analog detection) and the possible range in the aerosol correction shown in Fig 4. The measurements shown here were collected on August 23, 2013 at 1:15 PM local time (UTC – 6h) as the Twin Otter flew directly above the oil sands industry.
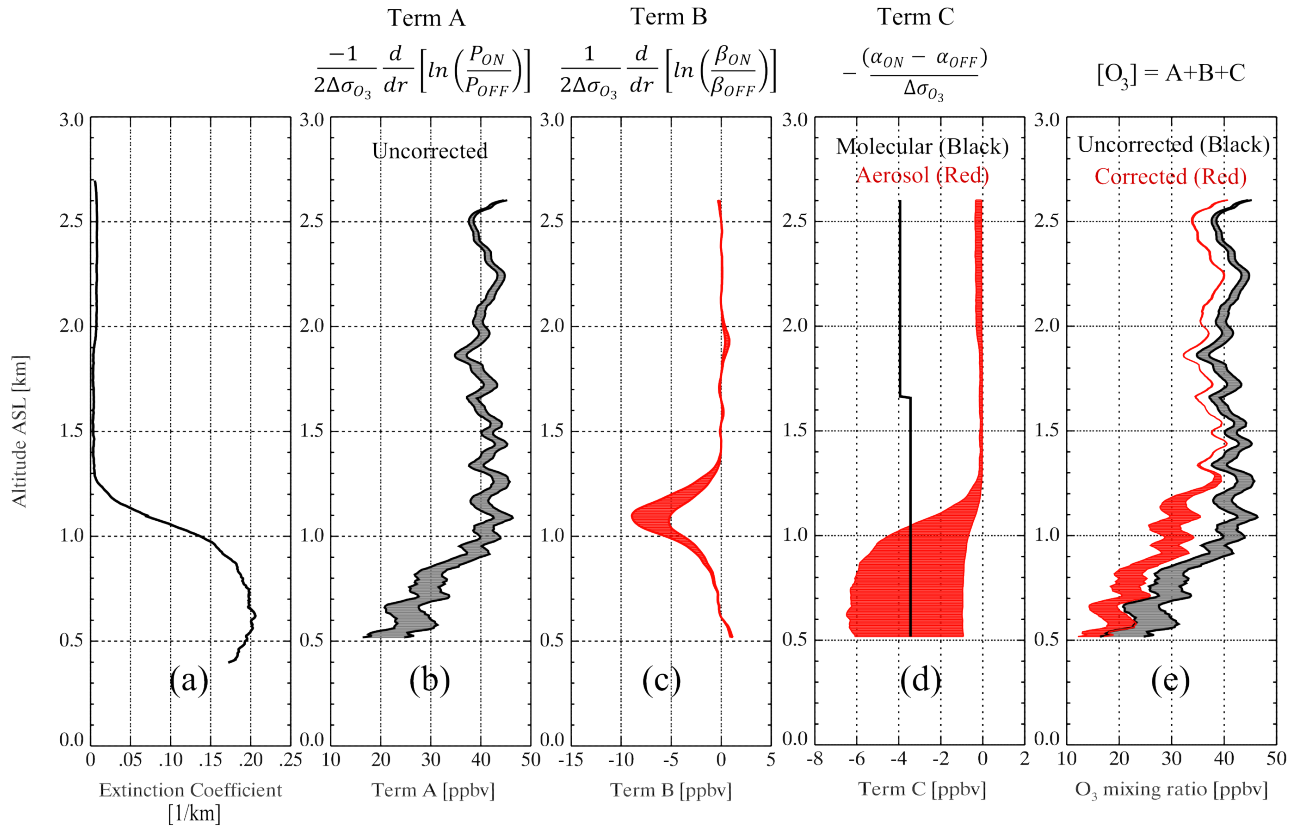
Figure 4: O₃ retrieval and aerosol correction for the AN:276/299 (altitude above 1.65 km) and PC:266/299 (below 1.65 km) wavelength pairs shown in Fig 3. (a) The aerosol optical extinction coefficient derived using the lidar measurement at a wavelength of 532 nm. Calculation of term A (panel b), term B (panel c), term C (panel d) from Eq. (2). (e) The addition of the first three terms in Eq. (2). The shading in red represents the range of O₃ values due to the uncertainty in the aerosol correction method. The grey shading represents the statistical uncertainty in the detection. The measurements shown here were collected on August 23, 2013 at 1:15 PM local time (UTC − 6) as the Twin Otter flew directly above the oil sands industry.

Figure 5: Flight track of the Twin Otter aircraft on (a) August 22, (b) and (c) August 23, (d) August 24, and (e) August 26, 2013. The direction of wind at the start of each flight is represented by the arrow. The oil sands industry is contained within the white box on all of the flight tracks.

Figure 6: The flight segment G-H on August 23, 2013 (1:04 to 1:26 PM local time (UTC – 6h) displayed on GoogleEarth. Point G represents the starting position of the flight leg and point H the ending position. The oil sands industry was contained within the regions outlined in white. The average direction of the wind at height of 800 m ASL on August 23, 2013 at the measurement time is indicated by the arrow. Inset photo shows the area that was flown over, including the flue-gas desulfurization (FGD) stack.
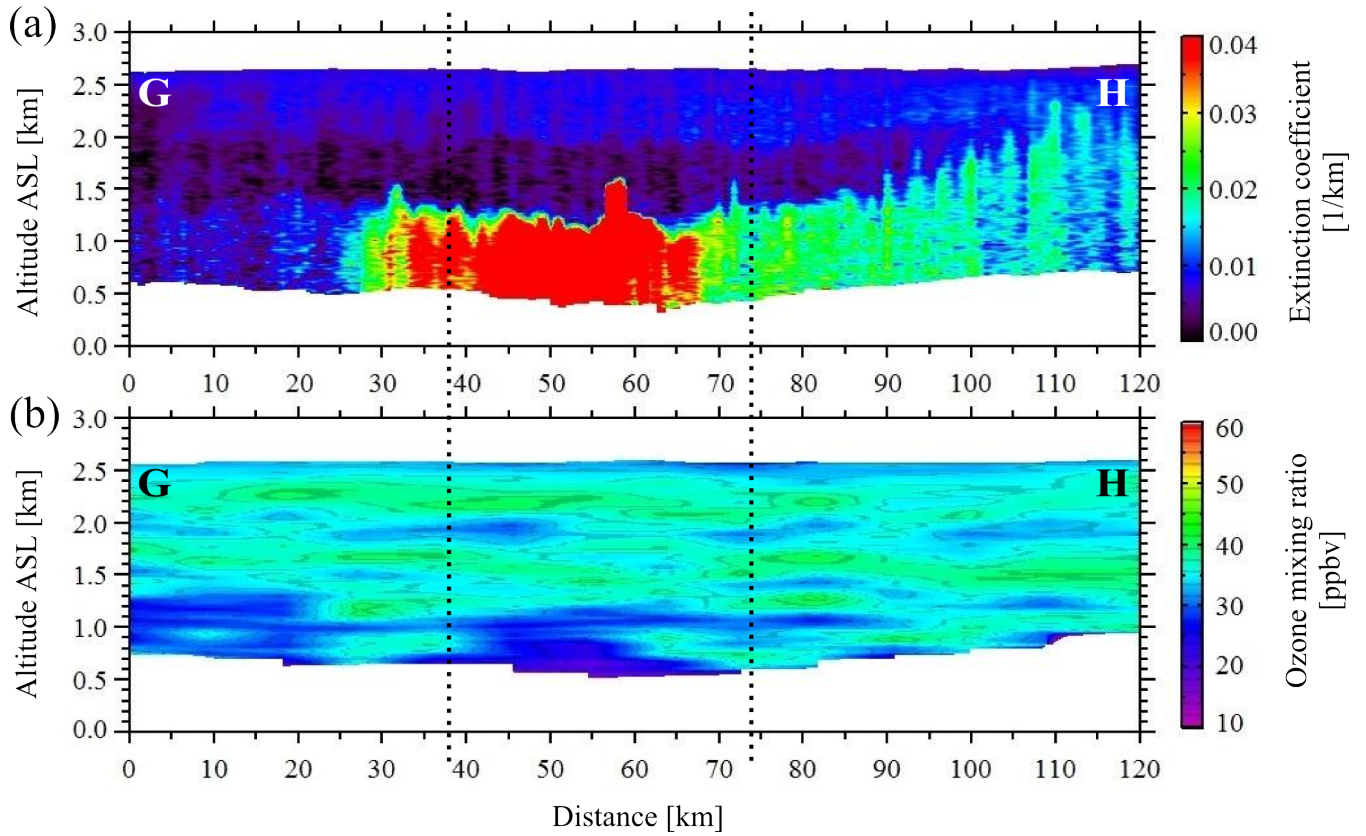
Figure 7: (a) The aerosol optical extinction coefficient derived from the lidar measurements at a wavelength of 532 nm and (b) the ozone mixing ratio derived from the UV lidar measurements for the flight segment G-H on August 23, 2013. The lidar measurements were collected between 1:04 and 1:26 PM local time (UTC – 6h). The height is above sea level (ASL) and the distance is along the flight segment in Fig. 6. The measurements contained within the vertical dashed lines represent the part of the flight segment directly above the oil sands surface operations contained within the regions outlined in white in Fig. 6.
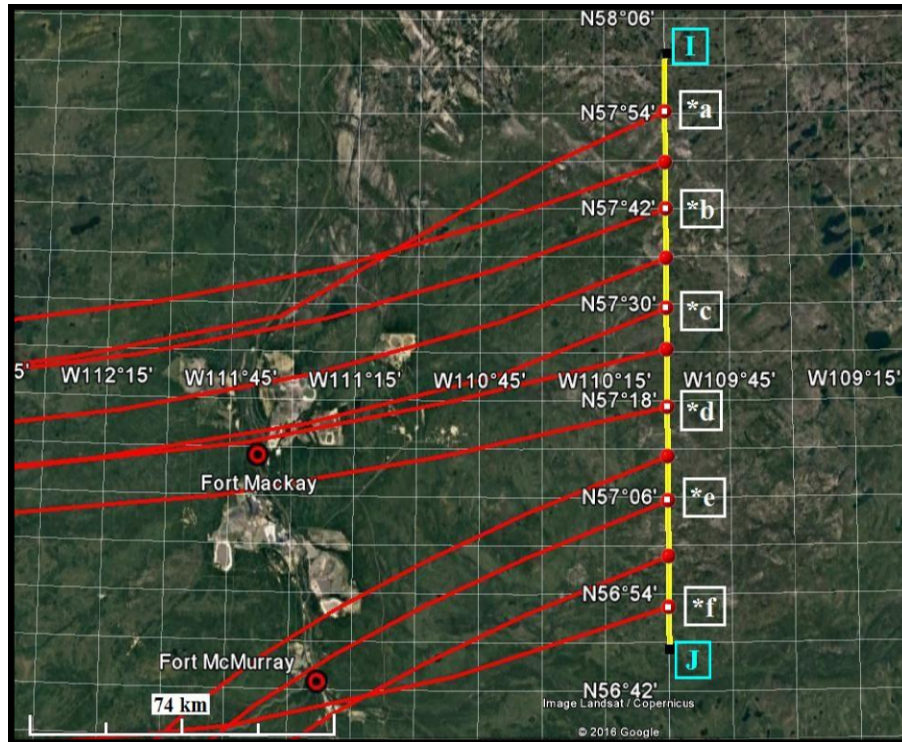
Figure 8: The flight segment I-J on August 22, 2013 is represented by the yellow line. Point "I" represents the starting position of the flight leg and point "J", the ending position. Backward air trajectories initiated from an altitude of 1000 m above sea level on August 22, 2013 at 2:00 PM local time (UTC – 6h) are shown in red and marked by the points *a to *f.
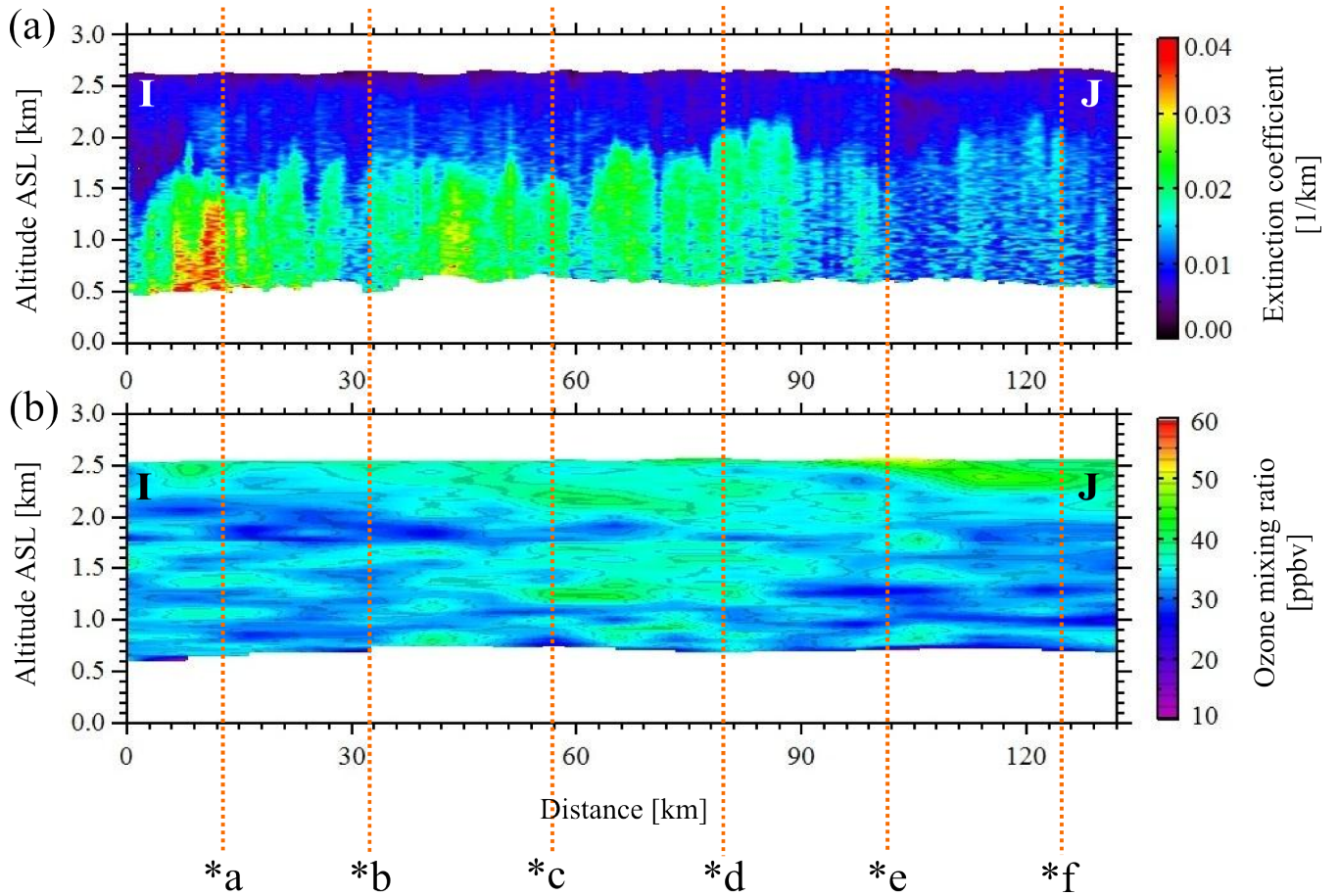
Figure 9: (a) The aerosol optical extinction coefficient measured at a wavelength of 532 nm and (b) the ozone mixing ratio derived from the UV lidar measurements for the flight segment I-J on August 22, 2013. The lidar measurements were collected between 1:52 and 2:20 PM local time (UTC − 6h). Points *a to *f represent the location of backward trajectories along the measurement path and are marked on the flight segment in Fig. 8.
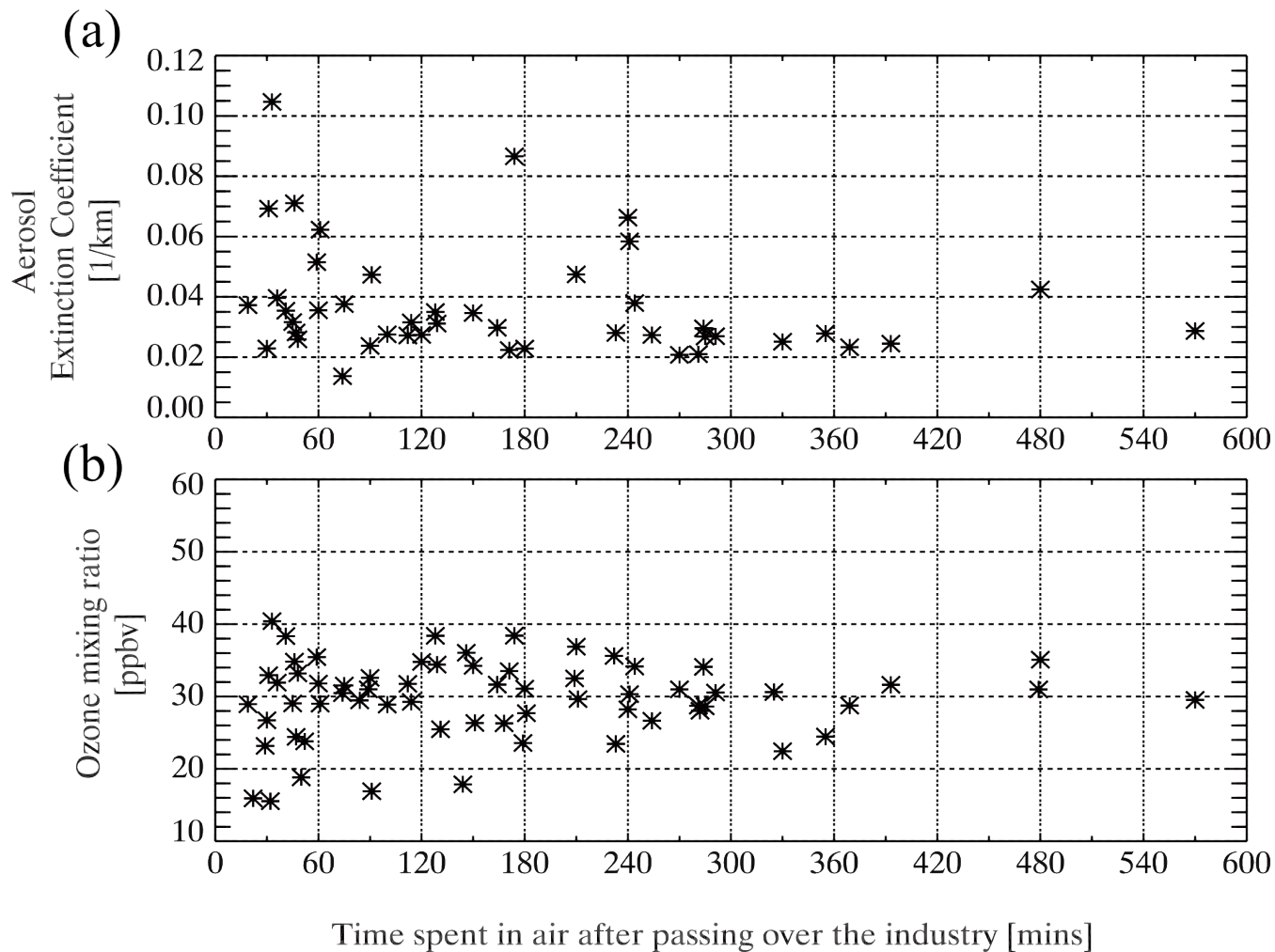
Figure 10: (a) The aerosol optical extinction coefficient and (b) the ozone mixing ratio as a function of time since the air had passed over the industry to reach the measurement point along all Twin Otter flight tracks. The measurements shown here were collected between August 22 and 26, 2013.
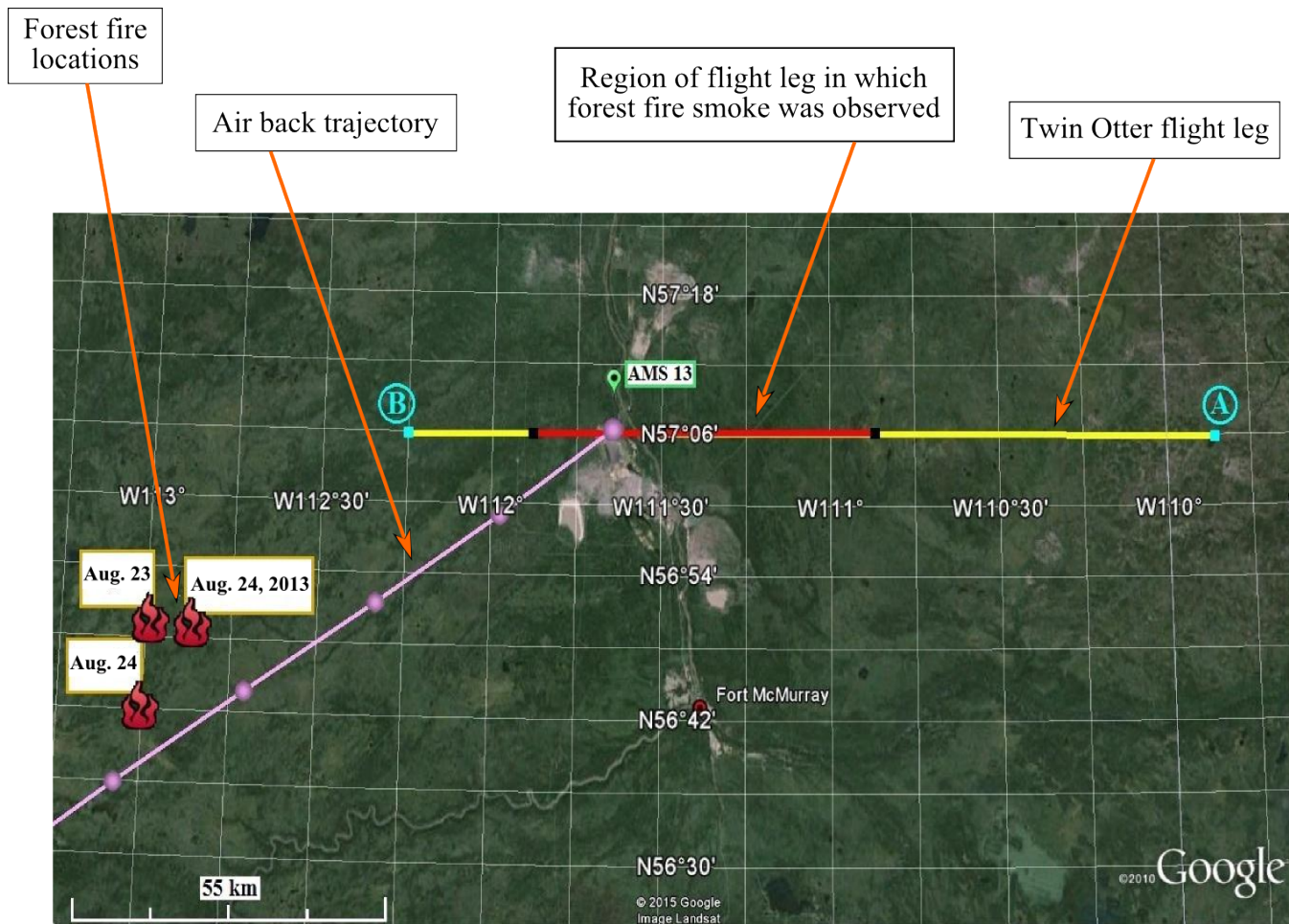
Figure 11: The flight segment A-B on August 24, 2013. The lidar measurements were collected between 2:48 and 3:18 PM local time (UTC – 6h). The red section along A-B represents the region where forest fire smoke was observed. The forest fire locations are depicted by red fire symbols. A backward air trajectory was initiated from an altitude of 2.0 km ASL at a time of 3:00 PM local time on August 24, 2013. The round marks along the trajectory represent a time interval of 1 hour. The location of the ECCC ground based lidar is indicated as AMS 13.
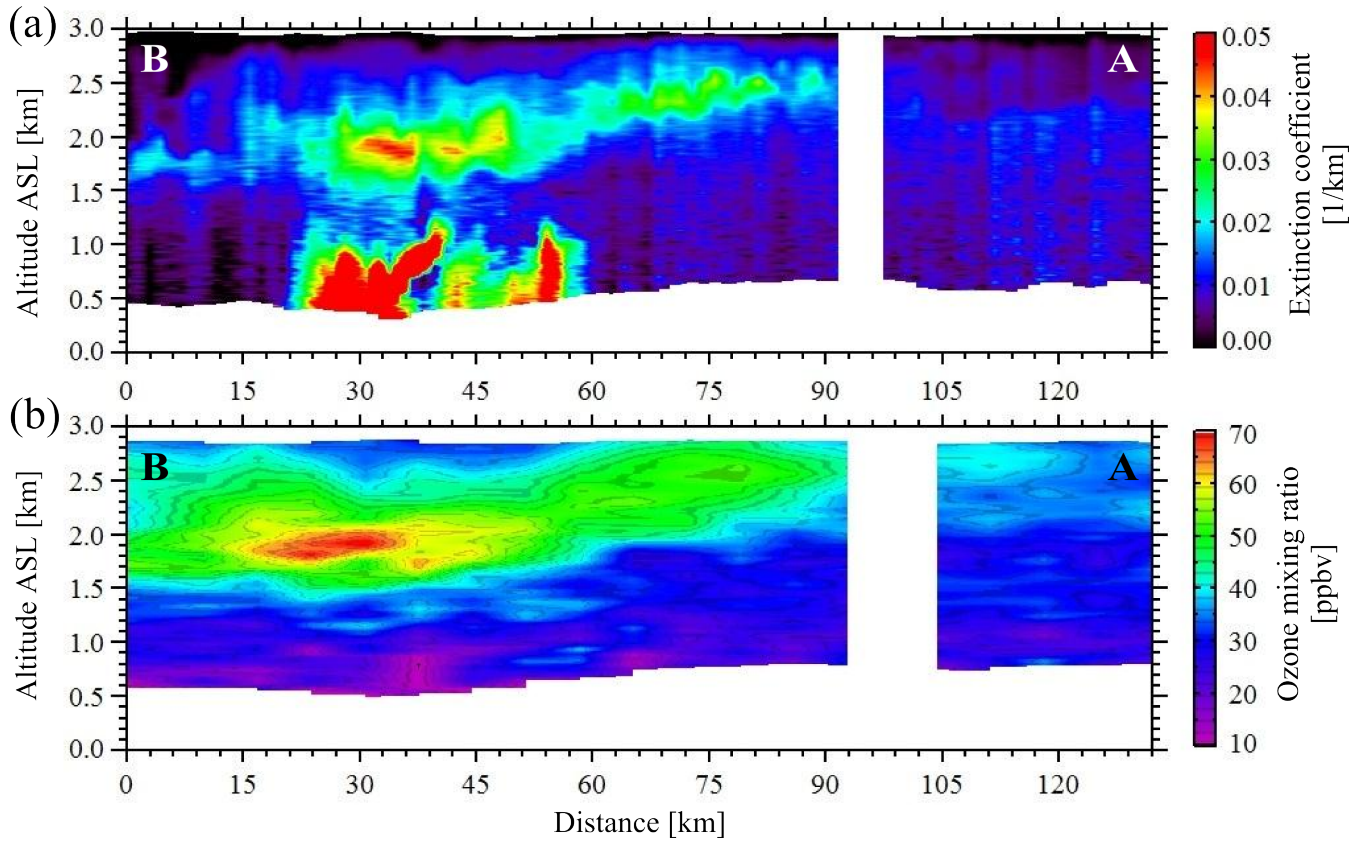
Figure 12: (a) The aerosol extinction coefficient measured at a wavelength of 532 nm and (b) the O₃ mixing ratio derived from the lidar measurements for the flight segment A-B on August 24, 2013. The lidar measurements were collected between 2:48 and 3:18 PM local time (UTC − 6h). The height is above sea level (ASL). Distance is from point B along the flight segment in Fig. 11. The blank section in this figure represents a region where clouds interfered with the lidar measurements.
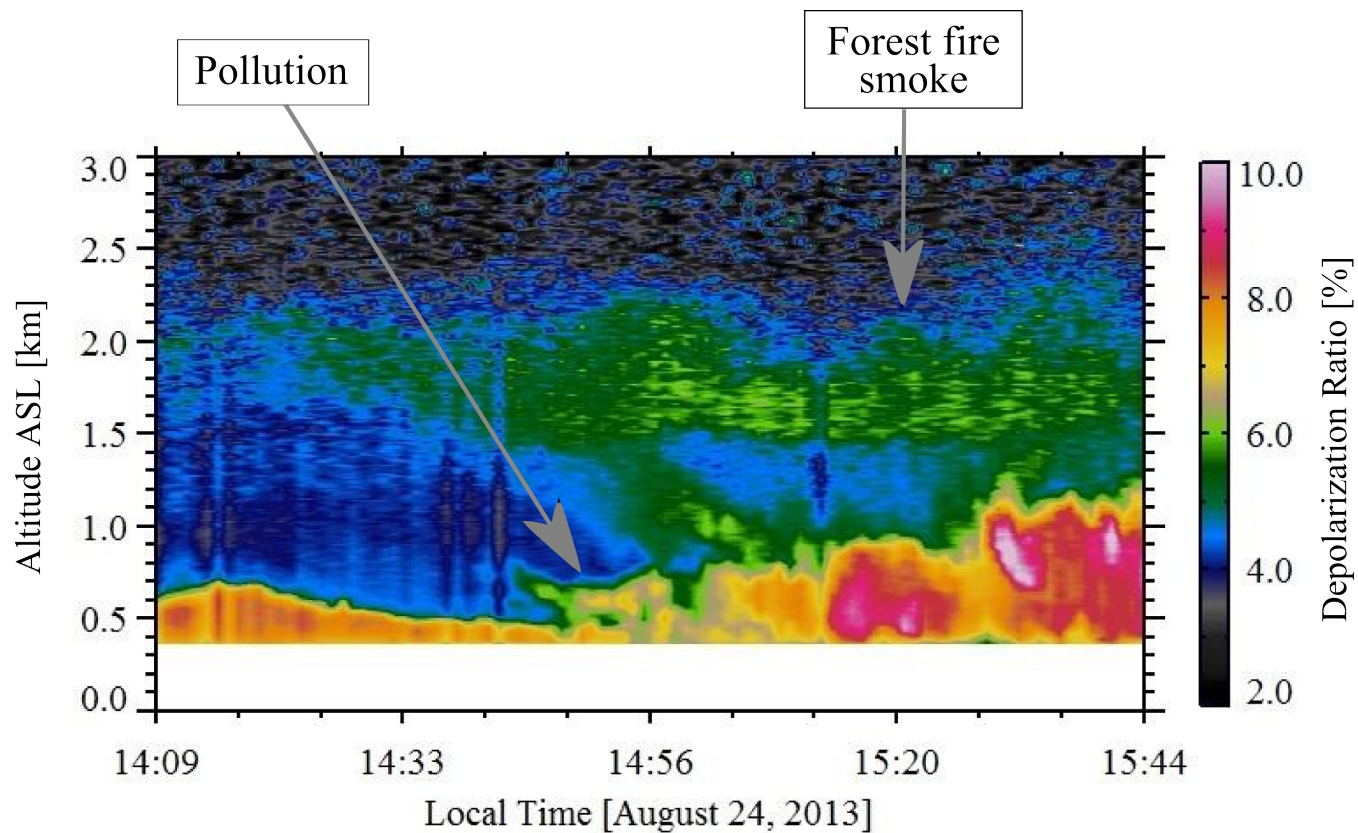
Figure 13: Ground-based lidar depolarization ratio measurements acquired with the ECCC ground based lidar system located at 57.14° N, 111.6° W (AMS 13 in Fig. 11).
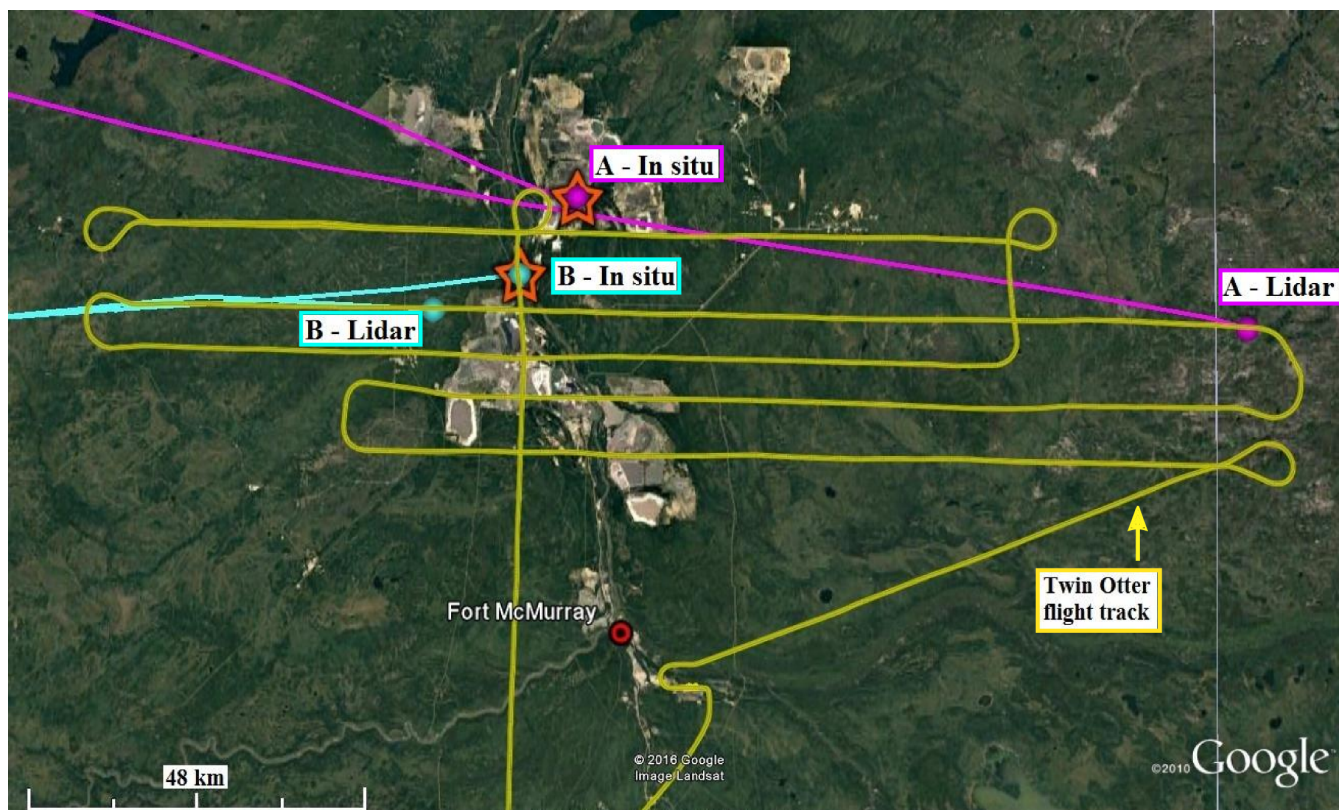
Figure 14: Flight tracks of the Twin Otter aircraft (yellow lines) and locations the Convair-580 aircraft spiral ascents for vertical profiles of in situ measurements (red stars). Backward trajectories coloured in blue and pink show the air coming from unpolluted and polluted areas respectively. Points labelled as A and B correspond to cases (a) and (b) in Fig. 15.
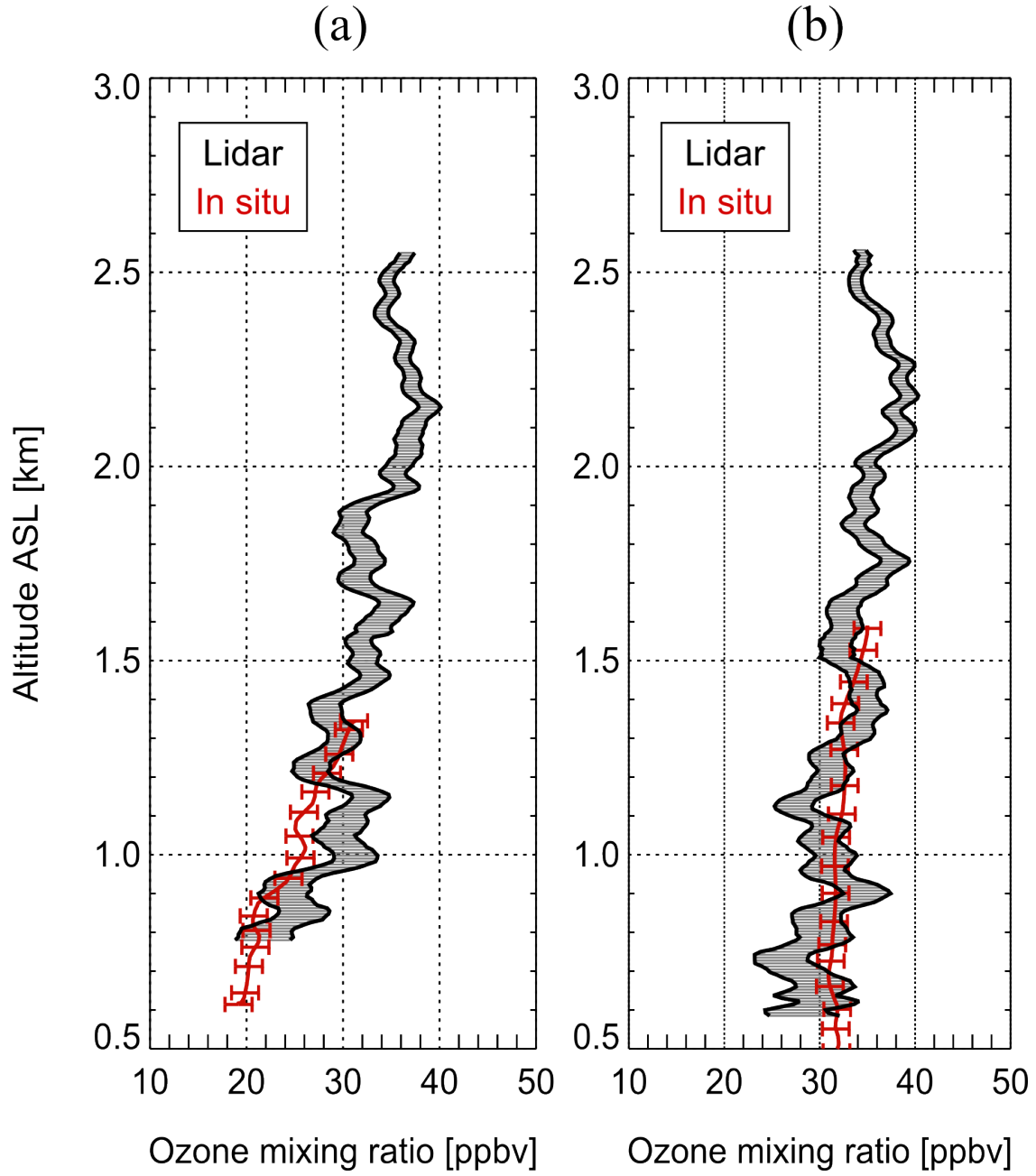
Figure 15: A comparison between the in situ and the lidar derived ozone mixing ratio for the measurements taken in (a) polluted air and (b) unpolluted air. Grey shading represents the sum of the random uncertainty in the lidar signal detection and the range of possible aerosol corrections. The locations of the measurements are indicated in Fig. 14 as points A and B for panels (a) and (b) respectively.
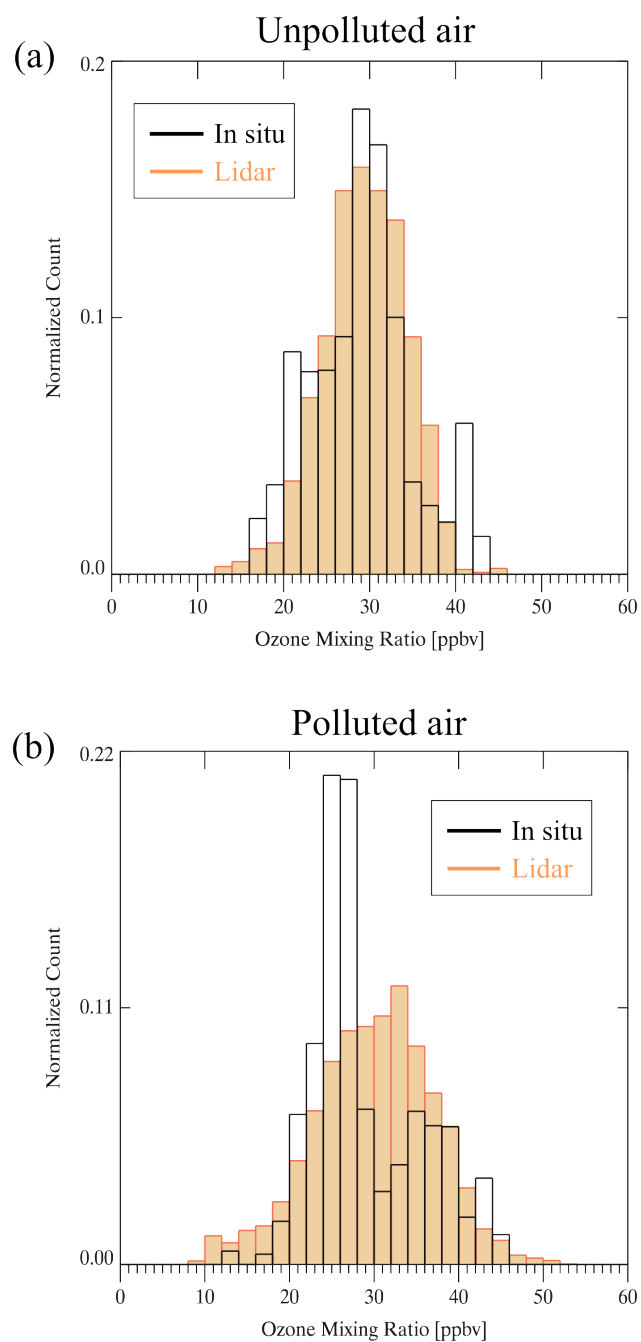
Figure 16: Histograms of in situ and lidar derived ozone mixing ratio for the measurements taken within the boundary layer in (a) unpolluted air and (b) polluted air.
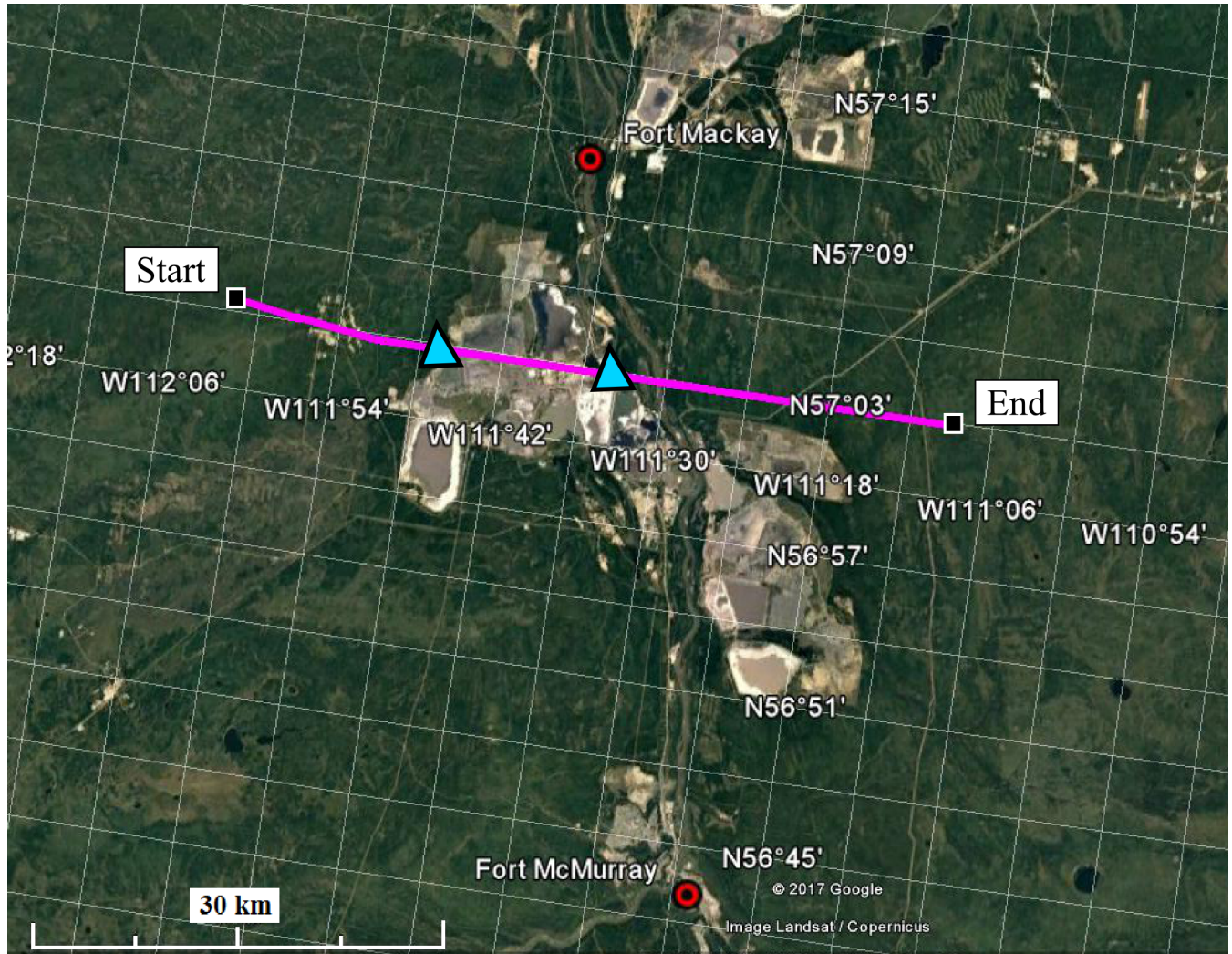
Figure 17: A section of the Convair flight on August 23, 2013 is shown in pink. In situ measurements were collected from west to east between 11:27 and 11:37 AM local time (UTC − 6h) on August 23, 2013. The triangular marks indicate the positions of the dashed lines in Fig. 18.
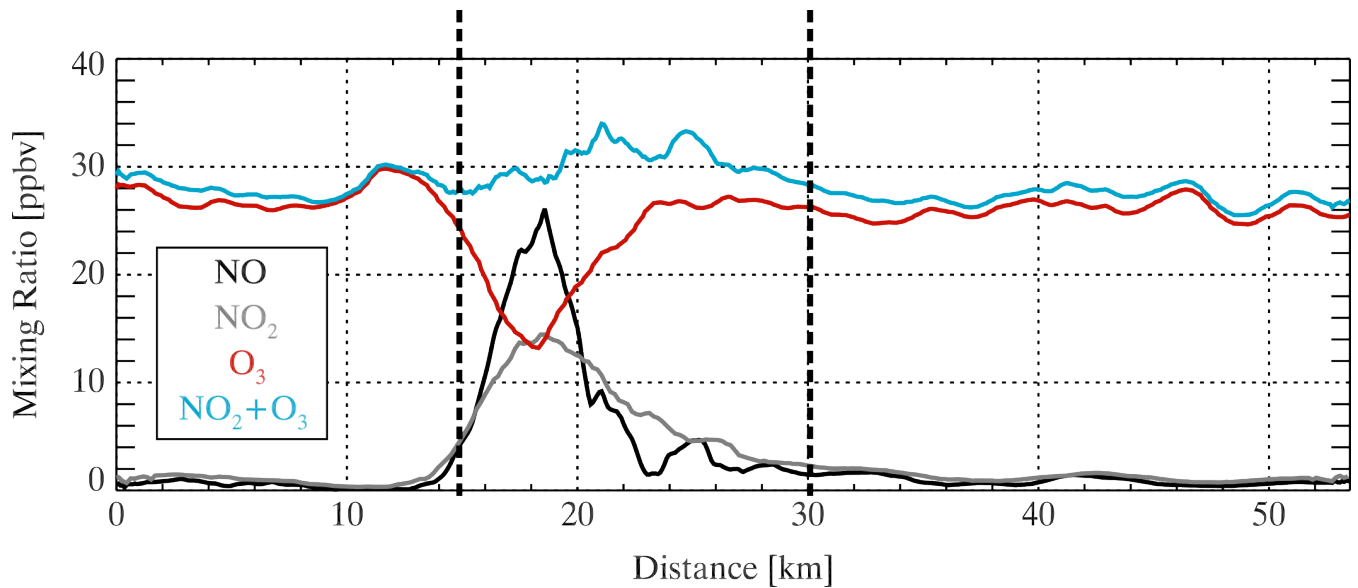
Figure 18: In situ measurements of O₃, NO, and NO₂ taken from a section of the Convair-580 flight on August 23, 2013 along the east-west direction over the oil sands industry and within the surface boundary layer. The in situ measurements were collected between 11:27 and 11:37 AM local time (UTC – 6h). The corresponding flight path is shown in Fig. 17. The dashed lines represent the positions of the blue triangles in Fig. 17.
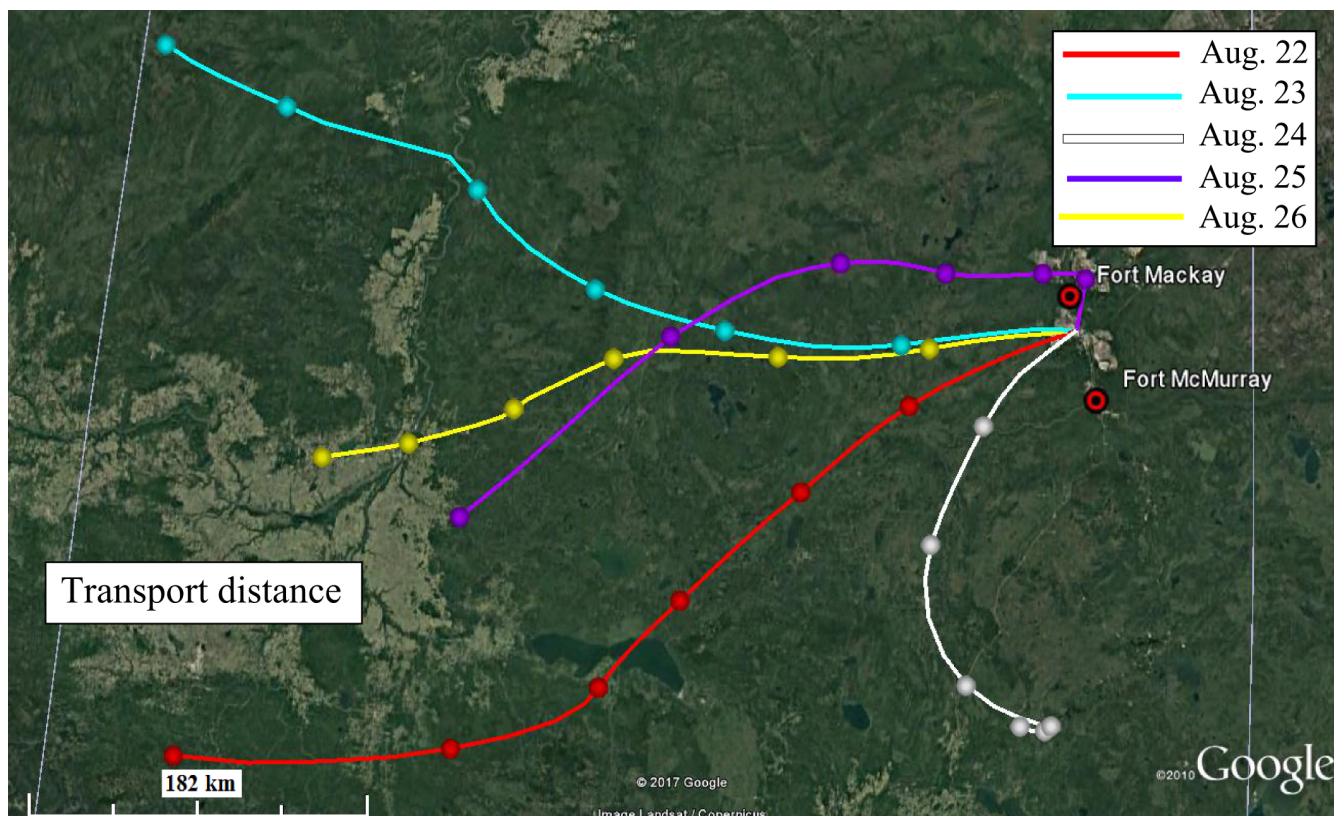
Figure 19: Backward air trajectories initiated from an altitude of 700 m above sea level on August 22 to August 26, 2013 at 1 PM local time (UTC − 6h). The round marks along each trajectory represent the distance travelled over time intervals of 4 hours.