# Martin Burgdorf



Meteorologisches Institut • Bundesstraβe 55 • 20146 Hamburg• Phone: +49 40 42838-8121 • Fax: +49 40 42838-5452 E-Mail: martin.burgdorf@uni-hamburg.de

Web: https://www.mi.uni-hamburg.de/arbeitsgruppen/strahlung-und-fernerkundung/personen/burgdorf-martin-joerg.html

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Natascha Töpfer Editorial Support Copernicus Publications editorial@copernicus.org

Dear Natascha:

Please give the referees again my sincere gratitude for their well-considered and helpful comments on our manuscript. In addition to my previous replies I want to make the following statements:

Dr. Yang

1. in section 2.2.1, the author checked pointing error in both cross scan and along scan direction. For ATMS 1.1 deg beam width channels, the lunar can only appear in one of the 4 FOVs at most of the time. How many cases can you find in AMSU-B and MHS lunar intrusion events that all 4 DSV been illuminated ? For cross scan pointing error assessment, if the smear effect was included in your study ?

Further investigation has shown that there are indeed some periods during which the Moon appears most of the time in only one FOV, namely the one closest to nadir. The frequency of the Moon appearing in a certain FOV depends on the relative positions of Earth, Moon, and Sun and hence changes slowly with time. An alignment, in which the Moon appears in all four DSVs is very rare, and the signal in DSVs zero and three is in this case very small. We have added a short description of this situation in Sect. 2.2.1.

2. section 2.2.2. The author take the maximum fitting counts in along track direction as the lunar radiation signal. But actually for each single DSV, the receiver output counts when lunar intrusion happens are weighted sum of radiation from Moon's disk, cold space background radiation, earth radiation entered from side lobe, as well as the instrument noise. When calculate the rations between different channels, the impact of other radiation sources should be evaluated

The varying Earth radiation in the side lobes was included with the noise in the overall random uncertainty that we calculated from the scatter of the signal ratios for each Moon intrusion. This way we could judge whether these ratios changed significantly with time or not. We have included this aspect in the first bullet of the list of conclusions in Sect. 3.

3. section 2.3. Ratio of brightness temperature should be square of of frequency ratio instead of two times of frequency ratio

This section has been completely revised; the reasoning takes now also the seventh comment of the referee into account.

4. section 2.4. the noise level of MHS 183 channel is different, which should be considered in this study when check the calibration consistency of G band. For example, the +-1 channel has larger noise than +-7 channel.



As stated in our response to the second comment, we consider the overall random uncertainty sufficient to judge the significance of the calibration consistency. Besides, we averaged the values from channels 18 and 19 in order to reduce the noise (see Sect. 2.2.2).

5. section 2.4.2. As mentioned before, the smear effect should be considered for across track pointing error assessment.

It is true that the smear effect causes a systematic difference between the average pointing position of the measurement and the pointing position recorded in the level 1b data. But this effect is not only present when observing the Moon, but also when observing the Earth. A paragraph explaining this was added to section 2.4.2.

6. The nonlinearity of Moon brightness temperature is much smaller than polar region due to the fact that after convolution with antenna pattern, the effective temperature of the moon is below 30K for 1.1 deg beam width channel. therefore it is not appropriate using lunar radiation check the nonlinearity bias.

Further investigations carried out after our preliminary reply from 2/11 have shown that a full Moon at perigee gives a brightness temperature of 45K, but that this is still closer to the temperature of the Cosmic Microwave Background than polar regions are to the temperature of the blackbody. So it is true that the nonlinearity is better characterized with simultaneous nadir overpasses (SNOs) at polar latitudes than with the Moon. The Moon is still useful, however, in cases where there are no SNOs with another, suitable instrument. We have made clear in Sect. 2.5.1 that observations of polar regions are better suited to determine the non-linearity than the Moon.

7. section 2.5.4, the impact of the center frequency shift is scene dependent: it is much more sensitive for earth scene than for The moon disk. I don't think the moon observations can be used to evaluate the center frequency shift.

This is true and we have completely revised section 2.5.4 (now 2.5.5). The center frequency shift can only be estimated from observations of the Earth. The point is here that in order to explain the bias in channel 20 one needs a large frequency shift. Because of the common local oscillator, channel 18 would then have the same shift and produce absurd values for the strength of the water line.

8. The author attribute the bias in channel 20 to RFI but provide no solid evidence. It is better to present some more details about RFI in 183 channels. For example, what is the interference source of the RFI for G band ? This may important because for RFI study, the previous research works only focused on frequencies lower than V band. If there is solid evidence to show the RFI in G band, the user should be noted.

Our attempts to prove the existence of RFI with AMSU-B on NOAA-16 did not produce quite convincing results yet. This is mainly because two transmitters are always switched on, so without dedicated procedures in flight one can never know for sure whether an instrument is affected by RFI or not. We refer to the second bullet in Sect. 3, where we state that our finding needs confirmation, and we are quite prepared to change other statements about RFI, if the referees find them too strong.

9. in section 3, the author concluded that "Any frequency shift of channel 20 must be smaller than  $0.003 \cdot 183$  Ghz = 500 MHz, else channel 20 would not agree with the other sounding channels". As mentioned before, moon surface is not sensitive to center frequency shift, therefore it may not being able to identify significant center frequency shift.

See seventh comment, the key argument mentioned in our reply on 2/11 is actually not valid.



# 10. Table.2, The dynamic range from cold to warm counts is only 1000 counts. Please double check the raw data. Is this due to instrument gain degradation ?

The values were re-calculated from the raw data and small modifications were applied to Table~2. Fact is, however, that the dynamic range is exceptionally small because of the instrument gain degradation. This aspect has been added to Sect. 2.5.1.

# Dr. Berg

The referee doubts that RFI is the reason for the large bias values that built up with channel 20 of AMSU-B on NOAA-16 in the course of the mission. We have therefore expanded Sect. 2.5.5 (now 2.5.6) by describing the results from the characterization of the RFI on ground in more detail. It is true that the RFI does not impact all three 183 GHz channels in the same way: We assume that it mainly affects channel 20 with Earth scenes and none of the channels with the deep space view. Similar, large variations of the interference effects among channels and scan positions have been found with AMSU-B on NOAA-15. The mitigation of RFI applied to the instruments on NOAA-16 and -17 became ineffective with the former because of the drastic gain reduction. Nevertheless the data processing in AAPP corrects for RFI in case of NOAA-17, but not with NOAA-16 – hence it seems likely that RFI has not been completely eliminated in this satellite.

The alternative explanation of the bias in channel 20 suggested by the referee brings the emissive reflector into play. It may well be that it shows a significant frequency dependence, but one must bear in mind that, unlike MHS, the sounding channels of AMSU-B are all equipped with double-sideband amplifiers with the sidebands being located symmetrically around 183 GHz. This means that in first approximation the frequency dependence disappears in the average of the sidebands. We have added Sect. 2.5.4 to state these facts. We admit, however, that without a proper characterization of the RFI, which is probably impossible now, i. e. after the end of the mission, our explanation for the bias is not fully proven. If the referees insist on changing our choice of words in this matter, we are quite prepared do that, see item eight above.

Sincerely,

Dr. Martin Burgdorf Fiduceo Postdoc Manuscript prepared for Atmos. Meas. Tech. with version 2015/11/06 7.99 Copernicus papers of the  $\[Mathbb{E}T_{E}X\]$  class copernicus.cls. Date: 25 April 2018

# Inter-channel uniformity of a microwave sounder in space

Martin Burgdorf<sup>1</sup>, Imke Hans<sup>1</sup>, Marc Prange<sup>1</sup>, Theresa Lang<sup>1</sup>, and Stefan A. Buehler<sup>1</sup>

<sup>1</sup>Universität Hamburg, Faculty of Mathematics, Informatics and Natural Sciences, Department of Earth Sciences, Meteorological Institute, Bundesstraße 55, 20146 Hamburg, Germany

Correspondence to: Martin Burgdorf (martin.burgdorf@uni-hamburg.de)

#### Abstract.

We analyzed intrusions of the Moon in the deep space view of the Advanced Microwave Sounding Unit-B on the NOAA-16 satellite and found no significant discrepancies in the signals from the different sounding channels between 2001 and 2008. Earlier investigations, however, had detected

- 5 biases of up to 10 K by using simultaneous nadir overpasses of NOAA-16 with other satellites. These discrepancies in the observations of Earth scenes cannot be due to non-linearity of the receiver or contamination of the deep space view without affecting the signal from the Moon as well. As major anomalies of the on-board calibration target and frequency shifts of or the local oscillator were not present, either, the most obvious reason for the degrading photometric stability is we consider radio
- 10 frequency interference in combination with a strongly decreasing gain the most obvious reason for the degrading photometric stability. By means of the chosen example we demonstrate the usefulness of the Moon for investigations of the performance of microwave sounders in flight.

#### 1 Introduction

Photometric stability of the measurement devices is an indispensable prerequisite for a reliable characterization of global change in atmospheric properties. This basic rule is particularly valid for spacebased instruments, because they cannot be checked in the laboratory again once the operational phase
has begun. Microwave sounders take therefore advantage of an on-board calibration target (OBCT)
for updating the flux calibration in intervals of a few seconds. Nevertheless systematic errors can
creep in from slowly changing instrumental properties that cannot be detected with the generally

- 20 employed two-point calibration, for example non-linearity. In order to first characterize and then reduce these errors in the case of AMSU-A (Advanced Microwave Sounding Unit-A), Zou and Wang (2011) determined time-dependent calibration offsets and nonlinear coefficients from simultaneous nadir overpass (SNO) regressions, which resulted in more consistent multi-satellite radiance observations for all respective channels. SNOs and other inter-calibration methods, however, that rely
- 25 exclusively on the comparison of two space instruments without a third source of information about

the Earth scenes, can, as a matter of principle, never remove all spurious trends in the data, because they cannot identify the relative contributions of either instrument to offsets and drifts.

At first sight it seems impossible to transfer the method developed by Zou and Wang (2011) to the sounding channels of AMSU-B (channels 18-20), because their departure from linearity was proven to be smaller than 0.1 K and basically independent of instrument temperature in ground tests (Saunders et al. , 1995b). As a consequence the nonlinear coefficient for the sounding channels was supposed to be insignificant and set to zero in the calibration files used by AAPP (ATOVS [Advanced TIROS-N {Television and InfraRed Observation Satellite} Operational Vertical Sounder] and AVHRR [Advanced Very High Resolution Radiometer] Pre-processing Package) for AMSU-B on all platforms. Nevertheless there were considerable biases between the sounding channels of AMSU-B on NOAA-16 and those on other satellites, especially towards the end of its lifetime (John et al. , 2012; Hanlon and Ingram , 2015) and particularly pronounced with channel 20. In this work we investigate why the flux calibration of the different channels seemed to diverge with time by

40 using the radiation from the Moon when entering the deep space view (DSV) as a third reference flux, in addition to the Cosmic Microwave Background (CMB) and the OBCT. We concentrate on the three sounding channels, because they are the scientifically most important ones, characterizing the 183.3 GHz line of water vapor, and at the same time apparently the worst with respect to stability.

- 45 As the Moon fills only a fraction of the beam, it is particularly well suited to detect effects, whose impact grows with decreasing scene flux. On top of that its microwave spectrum differs considerably from Earth's, for it is featureless and varies little with wavelength (Mangum , 1993). This means that all channels with the same central frequency, i. e. the three sounding channels, must produce the same brightness temperature when observing the Moon<sup>1</sup>. With this approach it seemed therefore
- 50 feasible to throw additional light on the origin of the biases of AMSU-B on NOAA-16, which have defied explanation until now.

## 2 Observations and methods

#### 2.1 Selection of Moon intrusions

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As the different sounding channels of AMSU-B observe at the same time with the same center frequency and in the same direction, there is no need to know the brightness temperature of the Moon for studies of the inter-channel uniformity, for every channel gets the same flux. It is advantageous, however, to select those intrusions, where the Moon comes closest to the center of the beam. This is not only because one gets the strongest signal with this alignment, but also because the "light curve", i. e. the measured brightness temperature as a function of time, resembles most closely a Gaussian

<sup>&</sup>lt;sup>1</sup>Apart from a very small band correction

- 60 in this case, making it easy to determine its maximum value without introducing systematic errors from the fit. The minimum distance between the pointing direction of each DSV and the Moon can be calculated for each orbit with AAPP, providing the information needed to identify candidates for further investigation. We concentrated our search on the years 2001, 2004, 2006, and 2007, thus increasing the density of observations at the start of the mission and the period of the emerging
- bias pattern. Beginning with the year 2007, the decreasing signal-to-noise ratio started to affect the accuracy of the photometric measurements (Hans et al. , 2017).

#### 2.2 Analysis

We fit the light curves of the Moon, which are sampled once per scan, with a Gaussian. The fit is achieved by optimizing three parameters: the maximum number of counts *a*, the centroid (location)
μ, and the peak width σ. Each of these parameters provides information about a different property of the instrument: gain, pointing direction in the along-track direction, and beam size in the along-track direction. If the Moon appears in three DSVs at the same time, it is possible to fit a Gaussian through the maximum signal of each of them and thus to obtain information about the beam pattern in the across-track direction as well, see Fig. 1. Obviously the Moon produces a signal in all frequency

rto-noise ratio varies considerably among the different channels.

For an investigation of photometric stability and uniformity the value of a and the minimum distance of the Moon to the pointing direction of the DSVs need to be known. This is because a is a function of this distance and the beam pattern.

#### 80 2.2.1 Position of the beam

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AAPP calculates the lunar angles for each scan and all four DSVs and writes part of this information in the level 1b file. It is therefore possible to identify the smallest lunar angle for each DSV. Unfortunately the calculation with AAPP is subject of several uncertainties:

- The error in the moon calculation is at worst 0.3° (MHS L1 PGS, 2013). This value has been confirmed by the analysis of Moon intrusions in Burgdorf et al. (2016). It is caused by incomplete knowledge of the alignment of the satellite; the position of the Moon is known with very high accuracy.
- Misalignment of the quasi-optics or feedhorns would be likely to produce effects on Channels 18, 19, and 20 which share the path to the receiver (McLellan, 1998). Such a misalignment could have been caused by vibrations during launch and is difficult to detect during flight, since Ground Control Points cannot be used with the sounding channels. So for the utilization period of AMSU-B on NOAA-16, no geolocation correction is performed on data from MW instruments aboard the NOAA satellites (Moradi et al., 2011).

- The position of the warmest spot on the lunar surface varies with phase and is therefore in general not in the center. Given the fact that the Moon can only appear with phases  $\pm 60^{\circ}$   $\pm 75^{\circ}_{\circ}$  around full Moon in the DSV (Burgdorf et al., 2016), its temperature maximum cannot be off centre by more than half of the Moon's apparent radius, i. e.  $\approx 0.1^{\circ}$  (Coates , 1961).

For these reasons one cannot rely on the calculation with AAPP to determine the lunar angles of the different Moon intrusions. Instead the point of maximum signal was first identified in the along-track

- 100 direction from the light curve in each DSV (Fig. 1). Then we determined the point of maximum signal in the across-track direction, i. e. in the scan plane, by fitting a Gaussian to the maximum signal  $a_i$  from each DSV,  $1 \le i \le 4$ . This procedure requires a detection of the Moon with a good signalto-noise ratio in three DSVs, as shown in Fig. 1, since the fitting procedure uses three independent parameters. The value for  $\mu$  obtained this way was multiplied by the difference in  $\theta$  between two
- 105 neighbouring DSVs, which is 1.1° with AMSU-B and MHS, and then compared to the value calculated with AAPP in Table 1. These new lunar angles formed the basis for the final selection of intrusion events from the provisional shortlist based on the lunar angles less accurate values calculated with AAPP (see Sect. 2.1). If the lunar angle is close to zero for a certain DSV, the adjacent DSVs produce light curves with a good signal-to-noise ratio as well, because they are only one beam
- 110 diameter away. In cases, however, where the Moon falls exactly in between two DSVs, the Moon is barely detectable in the other DSVs. Such intrusions happen only a few times per year and satellite and are less useful for our purpose, because the Moon gives less signal when off center of the FOV.
- Given the fact that both the satellite and the reflector are constantly in motion, the image of the
  Moon is actually smeared over a certain region of the field of view. As a result the signal is somewhat altered compared to the case where the Moon would remain at the same spot. As this "smear effect", however, is the same for all channels, it does not affect the ratio of the signal in different channels. The identification of the smallest lunar angles relies on the ratio of signals in different DSVs and is therefore independent of the smear effect as well. Hence we did not characterize its size or impact
  on each signal.

#### 2.2.2 Brightness temperatures

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The value for a from the second Gauss fit gives now the number of counts the Moon would have provided, if it had been in the center of the DSV, and it was used, after division by the gain, to calculate the ratios of the brightness temperatures in channels 18/19 and 20 (last column in Table 1).

125 The values from channels 18 and 19 were averaged in order to reduce the noise in the reference, to which channel 20, the one with the highest bias (see Sect. 1), is compared. In cases where the Moon could only be detected in two DSVs, we used the brightness temperatures as measured in the DSV that came closest to the Moon. This method was only applied, when we could conclude from the relative strengths of the signals in the two DSVs, where the Moon appeared, that the lunar angle

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130 must have been very small ( $< 0.2^{\circ}$ ) in one of them. This way the impact of pointing uncertainties on the signal from the Moon is kept as small as possible. Our values, however, do not represent the actual temperature of the Moon, because we did not correct for the fact that it does not fill the beam.

This calculation ignores the cold space correction factors, i. e. the correction for Earth and platform radiation entering through the side lobes, but they should be the same for each sounding channel, because they use the same quasi-optic feed, and therefore cancel out in the ratios of the signals that we consider here. The same is true for the warm load correction factors, which according to AAPP differ among the sounding channels only for AMSU-B on NOAA-17. The effect of the band correction that allows for the fact that the sounding channels receive slightly different fluxes because

140 of their side bands being at different distances from 183.311 GHz was ignored, because it amounts to less than two per mill and does not change with time.

#### 2.2.3 Beam pattern

An important characteristic of the beam, namely its full width at half maximum, follows immediately from the peak width of the Gauss fit, which is related to the full width half maximum via

- 145  $\sigma = FWHM / \sqrt{8 \cdot ln2}$ . In the across-track direction , where the Moon can only be detected in three DSVs with sufficient signal-to-noise ratio, it is and the smear effect alters the measured beam shape. It is therefore less accurate than the one measured in the along-track direction, where the FWHM of the beam can be determined from light curves with dozens of points representing an almost perfect Gaussian. Random samples showed no significant deviations from the nominal value
- 150 of  $1.1^{\circ}$  for the FWHM of the beam.

#### 2.3 Inter-band calibration (18 - 20)

As the brightness temperature of the disk-integrated Moon as seen by the microwave sounders is always more than 200 K (Eq. (5) in Yang and Weng , 2016), the Rayleigh-Jeans approximation of Planck's law is applicable<sup>2</sup>, and its spectral radiance is proportional to the product of temperature and frequency squared. This means that the maximum signal from a Moon intrusion in counts, divided by the gain, should be in good approximation the same for all sounding channels. Differences can might be caused, however, by the following two effects:

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- Incorrect gain values: The uncertainty associated with the gain has been calculated for the time of each Moon intrusion and is included in Table 1. The gain value assigned to the time of the Moon intrusion was obtained from interpolating the mean values a short time before and after the intrusion. The uncertainty of this gain value was then estimated from the variation of the

<sup>&</sup>lt;sup>2</sup>The difference between the spectral radiances at 200 K and 183 GHz according to Planck and Rayleigh-Jeans amounts to  $\frac{2\%2\%}{3}$ .

gain values before and after the intrusion. We note that any error in the temperature of DSV and OBCT that was used in determining the gain cancels out in the following calculations, because we consider only ratios between the channels.

- Imperfect co-registration of the channels: The Moon comes closer to the pointing direction of one channel than the pointing direction of another. This is unlikely, however, because all sounding channels share the path to the receiver (see Sect. 2.2.1). The difference in signal between a lunar angle of 0.05° and one of 0.15° - more than what was found for uncorrelated channels by Bonsignori (2017) - is only 1%, assuming a Gaussian light curve and a FWHM of the beam of 1.1°. We consider therefore this effect negligible.

A common misalignment of all-channels is irrelevant for our analysis, because it affects them all all signals in the same way , and any reasonable and therefore cancels out in their ratios. For the same reason an error in frequency should be negligible: Its temperature coefficient is typically 1 MHz/K

(?)would be negligible, because the brightness temperature of the Moon changes very little with frequency, and the local oscillator is the same for all sounding channels (Saunders, 1995a). Hence it is should be possible to verify the stability of the gain ratio between different sounding channels, i. e. their inter-band calibration, with an accuracy that is essentially limited by the uncertainties of the gain and the parameters of the Gaussian fit.

#### 180 2.4 Results

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#### 2.4.1 Uniformity of flux calibration

The average ratio between the signals obtained in channels 18/19 and 20 is 1.001 ± 0.006 for all observations in Table 1 combined. It is 0.993 ± 0.008 for the twelve values from the years 2001 and 2004 and 1.007 ± 0.008 for the later Moon intrusions. Within the error margins calculated
uncertainties these figures are in agreement with the values derived by John et al. (2012) and Hanlon and Ingram (2015) from simultaneous nadir overpasses. The uncertainties were determined from the distribution of the measured values, i. e. they include contributions from the noise in each sounding channel.

#### 2.4.2 Across-track pointing accuracy

- 190 For a comparison of the pointing directions of DSVs two and three in the across-track direction as calculated with AAPP (min moon angle) and with the aid of a Gauss fit (see Sect. 2.2.1), we consider now only the years 2001 and 2004, because the noise was lowest in the beginning of the mission. We find a difference of -0.113° ± 0.019°, i. e. the DSV direction determined with the Gauss fit leads the one calculated with AAPP by about 0.1° in the scan direction. The systematic error in the
- absolute pointing direction of the sounding channels of AMSU-B on NOAA-16 lies well below the upper limit of the overall, i.e. across- and along-track, pointing error of  $0.2^{\circ}$  for channel 16 that was

given by Atkinson (2000b).

The above mentioned smear effect can cause a pointing error, because the Moon moves a short
 distance through the field of view during the finite duration of the measurement. The same effect, however, is present with observations of Earth scenes, hence the pointing positions derived from the intrusions of the Moon in the DSV are more relevant than those calculated with AAPP.

## 2.5 Discussion

In the following we identify the reason rule out possible reasons for the trends found by John et al. (2012) and others in the sounding channels of AMSU-B on NOAA-16 with the aid of the results obtained from our analysis of the Moon intrusions. We start with the measurement equation for microwave sounders Eq. (1), as it is usually found in the literature, (e. g. Labrot et al., 2011; MHS L1 PGS, 2013; Weng and Yang, 2016).-:

$$R_{\rm s} = R_{\rm w} + (C_{\rm s} - \overline{C}_{\rm w}) \cdot \frac{R_{\rm w} - R_{\rm c}}{\overline{C}_{\rm w} - \overline{C}_{\rm c}} + Q + \Delta R \tag{1}$$

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$$Q = u \cdot (R_{\rm w} - R_{\rm c})^2 \cdot \frac{(C_{\rm s} - \overline{C}_{\rm w}) \cdot (C_{\rm s} - \overline{C}_{\rm c})}{(\overline{C}_{\rm w} - \overline{C}_{\rm c})^2}$$
(2)

$$\underline{\Delta R} = \alpha \cdot (R_{\rm w} - R_{\rm s}) \cdot (\cos(2 \cdot \theta_{\rm s}) - \cos(2 \cdot \theta_{\rm c})) / 2 \tag{3}$$

 $R_s$  = Earth scene radiance

 $R_w$  = warm calibration target radiance

- $R_c = \text{cold space radiance}$
- 215  $C_s$  = Earth scene counts

 $\overline{C}_{w}$  = warm target calibration measurement counts, averaged over four values pixels and seven scans

 $\overline{C}_{c}$  = cold space calibration measurement counts, averaged over four values pixels and seven scans

- Q =non-linear term
- 220 u =non-linearity coefficient

 $\Delta R$  = correction due to non-unity antenna reflectivity

$$\alpha = 1 - \frac{790}{2}$$

 $r_{90^\circ}$  = reflectivity of antenna for electric field parallel to the plane of incidence

- $r_{0^\circ}$  = reflectivity of antenna for electric field perpendicular to the plane of incidence
- 225  $\theta_s$  = position of antenna for Earth scene relative to nadir  $\theta_c$  = position of antenna for cold space relative to nadir

In the following we discuss the uncertainties belonging to each term in the measurement equation and decide which ones could have caused the bias trends on the basis of the complete picture of the

230 behavior of the instrument in flight. To simplify matters we assume that a difference of flux density

expressed in K is proportional to the corresponding difference in W cm<sup>-2</sup> s<sup>-1</sup>, i. e. the Rayleigh-Jeans approximation is applicable (see Sect. 2.3).

#### 2.5.1 Non-linearity

- The non-linearity correction coefficient is zero for all sounding channels of all AMSU-B flight models at all reference temperatures in the file of AMSU-B calibration parameters (amsub\_clparams.dat, version 25) used by AAPP. In order to investigate whether a non-linearity developed during the mission we consider how the corresponding bias would change as a function of scene temperature, bearing in mind that  $Q \propto (C_s - \overline{C}_w) \cdot (C_s - \overline{C}_c)$ . John et al. (2013a) find for Channel 20 they call it Channel 5 - of AMSU-B on NOAA-16 a bias of about 3 K in the year 2008 relative to
- AMSU-B on NOAA-15, which is mainly due to an anomalous decreasing trend of unknown origin for N16. This bias is independent of the natural target chosen for the Earth scene, Antarctica or tropical oceans. Similar phenomena with AMSU-A were corrected by postulating a modified, time dependent *u* (Zou and Wang , 2011). The values in Table 2, however, demonstrate that the bias should be ten eleven times larger in observations of polar regions or and almost eight times larger in
- 245 <u>observations of the Moon than when derived from data collected over warm bodies of water, if it was</u> due to non-linearity with AMSU-B as well. The reason is that the effect of the non-linearity on the calculated radiance becomes very small for scene temperatures close to those of the blackbody or the Cosmic Microwave Background. The brightness temperature of the atmosphere in Channel 20 is of course subject to variations, but and the difference between the counts from black body and deep
- 250 space is rather small because of the instrument gain degradation. But even when we allow an uncertainty of a factor two in its difference to the temperature of the blackbody, the spread of values of Qfor the different scenes in Table 2 is incompatible with the observation that the biases depend very little on radiance. Non-linearity can therefore be ruled out as an explanation for the inter-channel trends.

#### 255 2.5.2 Cold space temperature bias correction

The cold space temperature bias correction  $\delta T_{c,ch}$  is for a given DSV the same for all sounding channels of AMSU-B on NOAA-16 in the file of calibration parameters (version 25) used by AAPP. It varies between 1.09 and 1.26 K Atkinson (2000b)(Atkinson, 2000b) among the four possible DSV directions. In order to investigate whether the cold space temperature bias changed during the

260 mission we consider how its impact varies with scene temperature, bearing in mind that in first approximation, i. e. neglecting the non-linearity term,  $\delta T_{c,ch} \propto \frac{C_{\rm s} - \overline{C}_{\rm w}}{\overline{C}_{\rm w} - \overline{C}_{\rm c}}$ . We make use of the same reasoning as in Sect. 2.5.1 by constructing a contradiction between expected and observed variation of the bias with scene brightness.

- The values in Table 3 demonstrate that the bias should be <u>39.60</u> times larger in observations of the Moon than when derived from data collected over warm bodies of water. The reason is that the effect of the cold space temperature bias on the calculated radiance is largest for scene temperatures close to those of the Cosmic Microwave Background. Even when the bias in Channel 20 were only 1 K, a lower limit in view of the variations reported by John et al. (2013a), it would amount to an
- error of  $\approx 39 \approx 60$  K in the combined signal from Moon and CMB in the DSV. The actual error is at least an order of magnitude smaller (Burgdorf et al. , 2016), hence cold space temperature bias can be ruled out as an explanation for the inter-channel trends as well.

#### 2.5.3 Warm target bias correction

The warm target bias correction  $\delta T_{bb,ch}$  is zero for all sounding channels of all AMSU-B flight models at all reference temperatures in the file of AMSU-B calibration parameters (version 25) used by AAPP, except for channel 20 on FM3, where it is -0.16 K. Here the situation is just the opposite of the previous case inasmuch as the warm target bias affects the measurements less for lower scene temperatures. This is intuitively clear and follows from the fact that the second term of the sum on the right side of the measurement equation is negative for  $C_s \leq \overline{C}_w$ . The Moon

- 280 intrusions do therefore not help to characterize effects originating in the blackbody. A warm target bias correction for channel 20 about ten times as large as the biggest value used by AAPP for any flight model would be needed. On top of that the correction for the other sounding channels, where the bias is different or not existent, would have to have opposite sign or be zero. While this possibility cannot be ruled out completely, it seems highly unlikely, especially given the fact that the Platinum
- 285 Resistance Thermometers (PRTs) on the blackbody of the instrument in question gave no hint at dramatic alterations to the temperature pattern of the blackbody, see Fig. 2 and for a discussion of temperature drifts Hans et al. (2017).

### 2.5.4 Non-unity antenna reflectivity

Another effect that cannot be characterized with Moon intrusions is the emission of the main reflector and the variation of its contribution to the antenna temperatures as it rotates during a scan. According to Eq. (3) a correction to the measured radiance is required that is proportional to trigonometric functions of the distance of the rotating reflector from nadir position and  $\alpha$ . Its value for Earth scenes is quite different than the one for observations of the Moon, because of the different position of the reflector in either case. In first approximation, however, it must be the same for all sounding

295 channels, because they all operate at the same center frequency of 183 GHz and should therefore have very similar values for  $\alpha$ . The values found in the relevant calibration file from AAPP for MHS are  $|\alpha| = 0.0022$  at 183 GHz and  $|\alpha| = 0.0021$  at 190 GHz. The sign must be the same for all channels of AMSU-B, because they have the same polarization. Hence the maximum difference the non-unity antenna reflectivity can make among the sounding channels is  $10^{-4} \cdot (R_w - R_s)$  - a 300 negligible amount.

#### 2.5.5 Shift of channel center frequencies

Having discussed the main sources of error in the flux calibration we turn our attention to drifts of channel frequencies as a possible explanation of the bias that channel 20 exhibits when observing Earth scenes. (A change of center frequency would make no difference to the Moon observations, and Sect. 2.2) An accurate value of  $P(x_1 + x_2)$  is a the impact of a change in fractment on the

- 305 see Sect. 2.3). An accurate value of  $B(\nu + \delta \nu)$ , i. e. the impact of a change in frequency on the measured flux, is difficult to calculate for channels 18 and 19, because the exact shape of the water vapor absorption line depends on the state of the atmosphere. It is possible, however, to give at least an estimate of the shift in frequency required to change the measured radiance by 0.4%, i. e. causing an error of about 1 K, for channel 20, because this one probes the well-characterized wings of the
- 310 line profile (Bobryshev et al., 2017). It amounts to 3.5 GHz. This value is 50 times larger than the specification for frequency stability (Atkinson, 2001). As all sounding channels use the same local oscillator<del>(Saunders, 1995a)</del>, the same frequency shift would apply to channel 18 with ten times the effect on radiance. Such an enormous bias, however, is not observed.

#### 2.5.6 Radio-frequency interference on NOAA-16

- 315 As we found no fault with the calibration of AMSU-B on NOAA-16, we searched for instrumental effects that could alter the counts used as input of the calibration process. Malfunction of the processing electronics can be ruled out, because the data from all channels are clocked into the same AMSU instrument processor. There is, however, another phenomenon with the potential to strongly affect the counts, namely radio-frequency interference (RFI). The bias it causes can be positive or
- 320 negative and depends on channel, scan angle, and the transmitter in use. It was demonstrated in ground tests that AMSU-B on NOAA-16 was susceptible in all channels to radiation of the space-craft transmitters. The strongest effects were observed with channel 19 at the SARR (Search And Rescue Repeater) frequency, with channel 16 at the SARR frequency, and with channel 17 at the STX-1 (S-Band Transmitter # 1, 1698MHz) frequency (Ricketts and Atkinson , 1999). Modifica-
- tions of the instrument, e. g. wrapping cables with electrically conductive aluminum tape, were carried out as a consequence of the problems encountered with AMSU-B on NOAA-15 and reduced this susceptibility by 1-2 orders of magnitude. From the NOAA-16 post launch orbital verification tests it was estimated that the remaining Earth-view Earth view biases, though difficult to quantify, are were within  $\pm 0.5$  K when the transmitter is active (Atkinson , 2000a). During the Channel 17,
- 330 however, produced even after launch a bias of 1.2K for the space view due to interference with the STX-2 omni-directional antenna. What is more, during the lifetime of the satellite , however, the gain of the sounding channels decreased tremendously (see Table 1 and Hans et al. (2017)). A reduced gain produces a reduced signal, which means that interference becomes relatively more important,

as described by John et al. (2013b). The overall reduction of signal during the mission lifetime due

- 335 to gain degradation a factor six for channel 19 between 2001 and 2010 is of the same magnitude as the could boost a bias of 0.5 K pre-launch reduction of interference, which came from about 6 K down to a little less than 1 K. Channel 19 is the channel that was most affected by RFI during tests on ground (Ricketts and Atkinson, 1999) up to 3 K and more during flight. We therefore conjecture that individual interference events caused a bigger and bigger bias over the years, but at the same
- 340 time the noise equivalent difference in temperature (NE $\Delta$ T) increased, making them still difficult to detect. We know from the experience with NOAA-15 that interference effects can be very quite different for Earth and space views, hence RFI could be absent in the observations of the Moon while still affecting  $C_s$ .

#### 3 Conclusions

- 345 We have demonstrated that intrusions of the Moon in the DSV can be used to obtain otherwise inaccessible information about the characteristics of microwave sounders in flight. This is because the Moon provides a third flux reference, in addition to the CMB and the OBCT, with a spectrum that closely resembles a blackbody. This property makes it particularly suited for checks of the uniformity of sounding channels, where vicarious calibration is not an option. Another characteristic of the
- 350 Moon is that it fills only a fraction of the beams of past and present microwave sounders and therefore provides a flux level much lower than Earth scene and OBCT (see Fig. 3). As a consequence the Moon becomes a unique diagnostic tool for checking the cold space temperature bias correction and, in case of insufficient or missing SNOs, non-linearity. Such characterisation characterization of instrumental effects is essential for calculating uncertainties and harmonization coefficients of fun-
- 355 damental climate data records, as undertaken for example by the FIDUCEO project (FIDelity and Uncertainty of Climate data records from Earth Observations<sup>3</sup>).

In case of AMSU-B on NOAA-16 we found that the Moon signal from channel 20 agrees within 0.6% with the average signal of channels 18 and 19. It follows that

The co-registration of the sounding channels is very good, and the beam solid angle of channel 20 is within 0.3% the same as the average beam solid angle of channels 18 and 19, else they could not have given the same value for a source much smaller than OBCT and DSV. This result was to be expected because of the common quasi-optic feed of all sounding channels with AMSU-B. The agreement among the sounding channels, however, proves in addition that the Earth radiation entering the DSV pixels through the side lobes do not significantly alter the overall signal, because this radiation corresponds to different brightness temperatures in each

<sup>&</sup>lt;sup>3</sup>www.fiduceo.eu

channel. The scatter of the measured signal ratio can be fully explained by the uncertainties of the gain and the Gaussian fit.

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We attribute the bias in the sounding channels of AMSU-B on NOAA-16 to a simple and well-known effect, namely radio frequency interference, by eliminating all other possible causes. Although this finding needs confirmation by a careful investigation of the interference in flight, we recommend to exclude periods of active transmitters when calculating inter-calibration coefficients (Ferraro , 2015).

- One type of bias identified by Zou and Wang (2011) with AMSU-A, namely inaccurate calibration non-linearity, was ruled out in our investigation of AMSU-B. This finding provides evidence that the approach taken in the FIDUCEO project of harmonizing AMSU-B and MHS with the help of simultaneous nadir overpasses is sound, because the calculation of time-dependent nonlinear coefficients in flight, which would render that method impractical, is unnecessary.
- 380 Our characterization of sounding channels in flight demonstrates the potential of using intrusions of the Moon in the DSV as diagnostic tool for AMSU-B. Even Still higher accuracy is possible with MHS because of its lower NEΔT. As MHS is equipped with a sounding channel at 190.3 GHz with its own quasi-optic feed and local oscillator, the co-registration, bias correction, etc. will be less uniform among the channels, making their characterization even more important. In order to include also the window channels in the kind of analysis we presented, the differences of the brightness tem-
- perature of the Moon between the different radio wavebands must be known. A model describing them with the required accuracy is not available and remains therefore a worthwhile task for the future.
- 390 We conclude with a description of the potential of the Moon for in-orbit verification of future microwave imagers like MWI (MicroWave Imager). Because of its smaller beam For the channels with a smaller beam that are planned for these facilities, the method we described in this paper cannot be applied the same way, since the light curve will no longer have the shape of a Gaussian. This is because the finite size of the Moon and the asymmetric temperature distribution of its surface will
- 395 cause deviations from the case of disk-integrated measurementsbecome more relevant. A specially defined scan profile in the ideal case a two-dimensional raster map with a step size of 0.1° as proposed by Bonsignori (2017) will then be advantageous. It will enable measurements of the Moon's flux with much better signal-to-noise ratio, because it will fill the whole a larger part of the beam, and it will provide several additional reference flux levels, because one can point at regions of the
- 400 Moon with quite different temperatures. This way the non-linearity, to give just one example, can be characterised over a large flux range.

Author contributions I. Hans investigated the gain and noise changes, M. Prange investigated the stability of the OBCT and calculated, together with T. Lang, the values in Table 1. S. Buehler contributed to the text

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5 and helped with the interpretation and presentation of the results. M. Burgdorf prepared the manuscript with contributions from all co-authors.

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**Table 1.** Results from Gaussian fits to the light curves of Moon intrusions in DSVs of AMSU-B on NOAA-16. Columns 1 and 2: date and time of occurence of smallest lunar angle, columns 3-5: gain in counts/K, column 6: number of DSV pixel closest to the Moon, column 7: minimum lunar angle as calculated with AAPP, column 8: minimum lunar angle as calculated from maximum signal in each DSV, column 9: ratio of brightness temperatures in channels 18/19 (averaged) and channel 20.

Date	Time	Gain 18	Gain 19	Gain 20	DSV	Pos. (AAPP)	Pos. (Gauss)	$T_{18/19}/T_{20}$
1/4, 2001	16:14	$21.05\pm0.07$	$16.71\pm0.05$	$10.87\pm0.04$	4	$-0.02^{\circ}$		0.9944
1/6, 2001	2:58	$21.03\pm0.09$	$16.71\pm0.06$	$10.87\pm0.05$	2	$-0.09^{\circ}$	$+0.12^{\circ}$	0.9523
1/6, 2001	4:40	$21.03\pm0.07$	$16.70\pm0.06$	$10.85\pm0.05$	1	$+0.11^{\circ}$		0.9947
2/3, 2001	9:34	$21.11\pm0.09$	$16.83\pm0.07$	$10.91\pm0.05$	1	$+0.02^{\circ}$		0.9751
2/3, 2001	23:23	$21.10\pm0.10$	$16.83\pm0.06$	$10.90\pm0.04$	1	$+0.02^{\circ}$		1.0073
1/1, 2004	14:02	$17.34\pm0.07$	$13.83\pm0.05$	$9.34\pm0.04$	2	$-0.12^{\circ}$	$-0.04^{\circ}$	0.9982
1/3, 2004	2:13	$17.29\pm0.08$	$13.81\pm0.06$	$9.31\pm0.04$	2		$-0.03^{\circ}$	0.9897
4/29, 2004	11:41	$16.54\pm0.07$	$13.29\pm0.05$	$8.98\pm0.04$	2	$-0.22^{\circ}$	$-0.13^{\circ}$	1.0127
5/29, 2004	7:14	$16.47\pm0.07$	$13.23\pm0.06$	$8.92\pm0.04$	2	$-0.21^{\circ}$	$-0.10^{\circ}$	0.9929
5/29, 2004	22:19	$16.49\pm0.07$	$13.26\pm0.05$	$8.95\pm0.03$	2	$-0.25^{\circ}$	$-0.11^{\circ}$	0.9520
11/23, 2004	9:36	$15.54\pm0.06$	$12.58\pm0.04$	$8.84\pm0.03$	2	$-0.22^{\circ}$	$-0.12^{\circ}$	1.0606
12/21, 2004	6:46	$15.25\pm0.06$	$12.39\pm0.04$	$8.35\pm0.04$	3	$-0.07^{\circ}$	$-0.01^{\circ}$	0.9914
4/8, 2006	19:58	$10.86\pm0.06$	$9.33\pm0.04$	$6.08\pm0.04$	4	$-0.36^{\circ}$		0.9529
5/8, 2006	17:07	$10.47\pm0.05$	$9.01\pm0.05$	$5.84\pm0.04$	2	$+0.08^{\circ}$	$+0.15^{\circ}$	1.0024
11/2, 2006	12:36	$8.37\pm0.06$	$7.47\pm0.04$	$4.71\pm0.04$	1	$+0.02^{\circ}$		1.0457
11/2, 2006	14:17	$8.34\pm0.05$	$7.46\pm0.05$	$4.69\pm0.05$	2	$-0.04^{\circ}$	$-0.12^{\circ}$	0.9692
12/2, 2006	5:28	$7.98\pm0.08$	$7.19\pm0.05$	$4.48\pm0.04$	4	$+0.03^{\circ}$		1.0643
12/2, 2006	14:07	$7.96\pm0.08$	$7.18\pm0.05$	$4.47\pm0.05$	4	$+0.03^{\circ}$		0.9906
3/29, 2007	12:55	$7.22\pm0.06$	$6.61\pm0.05$	$4.07\pm0.04$	2	$-0.12^{\circ}$	$+0.06^{\circ}$	0.9819
3/31, 2007	9:51	$7.12\pm0.05$	$6.54\pm0.05$	$4.01\pm0.04$	2	$-0.03^{\circ}$	$+0.03^{\circ}$	1.0012
11/22, 2007	15:03	$4.96\pm0.05$	$4.80\pm0.04$	$2.81\pm0.03$	2	$-0.11^{\circ}$	$-0.20^{\circ}$	1.0465
11/22, 2007	21:57	$5.02\pm0.05$	$4.85\pm0.04$	$2.84\pm0.03$	3	$-0.06^{\circ}$	$-0.03^{\circ}$	1.0237
11/22, 2007	23:41	$4.99\pm0.06$	$4.83\pm0.04$	$2.83\pm0.04$	3	$-0.08^{\circ}$	$+0.02^{\circ}$	0.9810
11/23, 2007	1:25	$4.95\pm0.06$	$4.79\pm0.05$	$2.81\pm0.04$	3	$-0.15^{\circ}$	$-0.07^{\circ}$	0.9812
11/23, 2007	6:35	$4.90\pm0.08$	$4.75\pm0.05$	$2.78\pm0.04$	2	$0.00^{\circ}$	$+0.05^{\circ}$	1.0358
2/19, 2008	6:09	$3.68\pm0.08$	$3.73\pm0.07$	$2.09\pm0.05$	1	$-0.03^{\circ}$		1.0291
10/13, 2008	9:23	$4.11\pm0.07$	$4.53\pm0.04$	$2.45\pm0.03$	3	$-0.22^{\circ}$	$-0.10^{\circ}$	0.9928

Scene	Counts	$Q \ / \ Q_0$
Tropical Ocean	15,200	1
Polar Regions	15, <del>100-075</del>	11
Moon	14, <del>635-615</del>	<del>9</del> - <u>7.5</u>
Black Body	15, <del>215-210</del>	0
Deep Space	14, <del>540-530</del>	0

**Table 2.** The relative value of the non-linearity term Q in the measurement equation for different scenes. The counts are from channel 20 in the orbit of the last Moon intrusion listed in Table 1, i. e. measured in October 2008.  $Q_0$  is the non-linearity correction for observations over tropical ocean.

**Table 3.** Relative value of the cold space bias correction  $\delta T$  in the measurement equation for different scenes - the counts are from channel 20 in the orbit of the last Moon intrusion listed in Table 2, i. e. measured in October 2008.  $\delta T$  is the change in the calculated scene temperature due to the cold space temperature bias correction, where the subscript 0 indicates the value for observations over tropical ocean.

Counts	$\frac{\delta T}{\delta T_0}$	
15,200	1	
15, <del>100-075</del>	<del>8-14</del>	
14, <del>635-615</del>	<del>39.60</del>	
15, <del>215</del> -2 <u>10</u>	0	
14, <del>540-530</del>	4 <u>5.68</u>	
	Counts 15,200 15, <del>100-075</del> 14, <del>635-615</del> 15, <del>215-210</del> 14, <del>540-530</del>	



**Figure 1.** Left: Light curves of the Moon obtained from the four AMSU-B deep space views (pixels) on 11/2, 2006. Right: Observing geometry projected to the sky: The axis of the orbit of the satellite is marked with a plus sign.  $\theta = 9.5^{\circ}$  is its angular distance from DSV 4, shown as a filled, green circle. The pointing direction of the instrument describes a great circle in the sky during one scan, which covers all four deep space views and then continues along the large, red arrow. From one scan to the next, all DSVs move by a small amount along the large circles in the orientation of the small red arrow. The yellow arrow gives an example of the trajectory of the Moon. DSV 2 came closest and gave therefore the highest signal in its light curve. DSV 4 was too far away from the Moon to be affected by its presence. From the ratio of the maximum signals in DSV 1 and DSV 3 one can caluclate how far the Moon is away from DSV 2. This distance is zero if and only if the counts from DSV 1 and DSV 3 are the same. The completion of the circles that each DSV desribes in the sky takes 100 min, the duration of the orbit of the satellite. This is fast compared to the movement of the Moon (synodic month 29.5 days) and the movement of the orbit axis of the satellite with a period of one year (blue arrow).



**Figure 2.** Temperature measured by seven PRTs of the blackbody of AMSU-B on board NOAA-16 during two orbits ten years apart: 2/12, 2001 (top) and 7/30, 2011 (bottom)



**Figure 3.** Schematic representation of the signal range in counts and brightness temperature covered by deep space, Moon scenes, Earth scenes, and internal calibration target for channel 20 of AMSU-B on NOAA-16 in 2006. October 2008. A gain of 52.5 counts/K was assumed. The Moon gives a much lower signal than the Earth, because it fills only a fraction of the beam.