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A Steady State Continuous Flow Chamber for the Study of Daytime and Nighttime Chemistry under Atmospherically Relevant NO levels

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Abstract

Experiments performed in laboratory chambers have contributed significantly to the understanding of the fundamental kinetics and mechanisms of the chemical reactions occurring in the atmosphere. Two chemical regimes, classified as 'high-NO' versus 'zero-NO' conditions, have been extensively studied in previous chamber experiments. Results derived from these two chemical scenarios are widely parameterized in chemical transport models to represent key atmospheric processes in urban and pristine environments. As the anthropogenic NO_x emissions in the United States have decreased remarkably in the past few decades, the classic 'high-NO' and 'zero-NO' conditions are no longer applicable to many regions that are constantly impacted by both polluted and background air masses. We present here the development and characterization of the NCAR Atmospheric Simulation Chamber, which is operated in steady state continuous flow mode for the study of atmospheric chemistry under 'intermediate NO' conditions. This particular chemical regime is characterized by constant sub-ppb levels of NO and can be created in the chamber by precise control of the inflow NO concentration and the ratio of chamber mixing to residence timescales. Over the range of conditions achievable in the chamber, the lifetime of peroxy radicals (RO₂), a key intermediate from the atmospheric degradation of volatile organic compounds (VOCs), can be extended to several minutes, and a diverse array of reaction pathways, including unimolecular pathways and bimolecular reactions with NO and HO₂, can thus be explored. Characterization experiments under photolytic and dark conditions were performed and, in conjunction with model predictions, provide a basis for interpretation of prevailing atmospheric processes in environments with intertwined biogenic and anthropogenic activities. We demonstrate the proof of concept of the steady state continuous flow chamber operation through measurements of major first-generation products, methacrolein (MACR) and methyl vinyl ketone (MVK), from OH- and NO₃-initiated oxidation of isoprene.

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1. Introduction

With the discovery of the role of biogenic volatile organic compounds (BVOCs) in urban photochemical smog (Chameides et al., 1988), the interactions of biogenic emissions with manmade pollution and their subsequent impact on the atmosphere's oxidative capacity and aerosol burden have received extensive studies in the ensuing decades (De Gouw et al., 2005; Ng et al., 2007; Goldstein et al., 2009; Surratt et al., 2010; Rollins et al., 2012; Shilling et al., 2013; Xu et al., 2015). A particular research focus has been understanding the influence of nitrogen oxides $(NO_x = NO + NO_2)$ on the atmospheric oxidation cascades of BVOCs, which ultimately generate ozone (O₃) and secondary organic aerosols (SOA). Nitrogen oxides alter the distribution of BVOC oxidation products by primarily modulating the fate of peroxy radicals (RO₂), a key intermediate produced from the atmospheric degradation of VOCs by major oxidants including OH, O₃, and NO₃. In the absence of NO_x, RO₂ reacts predominantly with HO₂ radicals yielding organic peroxides and other products, and to a lesser extent, undergoes self/cross-reactions yielding carbonyls, alcohols, and multifunctional species. In the presence of elevated NO_x, the dominant fate of RO2 is to react with NO leading to ozone production, and also to organic nitrates. During the night, RO₂ also reacts with NO₃ which is produced by the reaction between O₃ and NO₂. In addition, reaction of peroxyacyl radicals (RC(O)O₂) with NO₂ produces peroxyacyl nitrates that constitute a large reservoir of reactive nitrogen and a potentially important SOA precursor (Singh and Hanst, 1981; Nguyen et al., 2015).

Much of our understanding of the extent to which NO_x mediates the oxidation chemistry of BVOC in the atmosphere has been derived from measurements in laboratory chambers, where two extreme experimental conditions, i.e., 'high NO' vs. 'zero-NO', were mostly performed to examine the reaction pathways of RO₂ radicals (Kroll and Seinfeld, 2008; Orlando and Tyndall, 2012; Ziemann and Atkinson, 2012). Results from these two chemical regimes have been widely incorporated into chemical transport models to represent key atmospheric processes in urban and pristing environments, respectively (Kanakidou et al., 2005). In the actual atmosphere, however, the fate of RO₂ radicals is rather more complicated than simply undergoing bimolecular reactions with NO/HO₂ as observed under the two extreme chamber conditions. It has been recently revealed that RO₂ radicals may undergo an internal H-shift followed by sequential O₂ addition, leading to highly oxygenated multifunctional peroxides (Ehn et al., 2014; Jokinen et al., 2015; Kurtén et al., 2015; Kirkby et al., 2016; Zhang et al., 2017). The rate of H-shift largely depends on the thermochemistry of the nascent alkyl radicals and can be reasonably fast, on a time scale of seconds to minutes (Crounse et al., 2013). Further, depending on the stability of the RO₂ precursor (alkyl radicals), RO₂ radicals may lose O₂ in competition with bimolecular reactions with NO, NO₃, RO₂, and HO₂. Recent theoretical and laboratory studies have found that the hydroxy peroxy radical conformers produced from isoprene photooxidation decompose readily to allylic radicals on time scales faster than bimolecular processes under atmospherically relevant NO/HO₂ levels (tens to hundreds of parts per trillion by volume). This highly dynamic system leads to formation of distinctly different products that depend on the concentrations of bimolecular reaction partners from those observed in chamber experiments under 'high-NO' and 'zero-NO' conditions (Teng et al., 2017).

Anthropogenic NO_x emissions in the United States have decreased remarkably in the past few decades (EPA, 2014), resulting in significant changes in the degradation mechanisms of BVOCs, especially in regions impacted by both background and polluted air masses such as the Southeastern United States. However, the ultimate fate of peroxy radicals in environments with

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sub-ppb NO levels is still poorly constrained, in part due to a lack of consistent measurements under well controlled conditions. Experimental environments with a controlled NO production at sub-ppb levels have been recently introduced to examine the various RO₂ fates in the atmosphere. For example, a 'slow chemistry' scenario initiated by photolyzing methyl nitrite (CH₃ONO) under extremely low UV intensities as the OH radical source ($J_{\text{CH3ONO}} \sim 10^{-5} \, \text{s}^{-1}$) was created to study the autoxidation chemistry of peroxy radicals produced from isoprene photooxidation (Crounse et al., 2011; Crounse et al., 2012; Teng et al., 2017). The resulting NO and HO₂ mixing ratios are maintained at \sim ppt (parts per trillion by volume) level (CH₃ONO + O₂ + $hv \rightarrow$ HO₂ + NO + HCHO) over the course of several hours of reaction, and the average OH concentration (OH $\sim 10^5$ molec cm⁻³) is approximately one order magnitude lower than that in the typical daytime ambient atmosphere. Another example relates to a recent method development in the Potential Aerosol Mass (PAM) flow tube reactor where nitrous oxide (N₂O) was used to produce \sim ppb (parts per billion by volume) level of NO (O₃ + $hv \rightarrow$ O₂ + O(1 D); O(1 D) + N₂O \rightarrow 2NO) (Lambe et al., 2017). Timescales for chemical reactions and gas-particle partitioning are ultimately limited to the mean residence time (\sim 80 s) of the PAM reactor.

An alternative experimental platform to the batch-mode chamber and flow tube reactor described above is a well-mixed steady-state chamber with continuous feed of reactants and continuous withdrawal of reactor contents (Shilling et al., 2008). An attribute of the continuous flow steady state chamber is that, by control of the inlet reactant concentrations and the ratio of mixing to residence timescales, it is possible to simulate atmospheric oxidation under stable conditions over a wide range of time periods and chemical scenarios. In this study, we present the development and characterization of the NCAR Atmospheric Simulation Chamber, which is operated in steady state continuous flow mode for simulating atmospheric daytime and nighttime chemistry over chemical regimes not accessible in static chamber experiments. We focus on establishing an 'intermediate NO' regime characterized by a constant steady-state NO level ranging from tens of ppt to a few ppb in the chamber. This particular chemical regime is well suited for the study of atmospheric behavior of RO₂ radicals, as they can survive up to minutes and embrace various reaction possibilities as opposed to reaction with NO, NO₃, HO₂, and RO₂ as their dominant fate observed in most batch-mode chamber experiments. We employ the 'intermediate NO' regimes to reexamine the daytime and nocturnal chemistry of isoprene through the measurements of two first-generation products, methacrolein (MACR) and methyl vinyl ketone (MVK).

2. Experimental

2.1 NCAR Atmospheric Simulation Chamber Facilities

The NCAR Atmospheric Simulation Chamber consists of a 10 m³ FEP Teflon (0.005" thick) bag that is housed in a cubic enclosure with UV reflective surfaces and a bank of 128 wall-mounted blacklight tubes (32W, Type F32T8/BL). To characterize photolytic conditions in the chamber, irradiance spectra were collected in the wavelength range of 180–600 nm at ~0.8 nm resolution by a custom-built spectroradiometer (Petropavlovskikh et al., 2007). Photolysis frequencies were calculated based on the measured downwelling spectral actinic fluxes. The computed photolysis rate of NO₂ (J_{NO_2} ~ 1.27×10⁻³ s⁻¹) agrees within 3% with that measured by photolyzing 18.6 ppb NO₂ in the chamber and monitoring the NO production rate. The chamber is equipped with a standard set of measurements, including an integrated temperature and

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113 humidity probe (Model 50U, VAISALA, CO) and a Magnehelic differential pressure indicating 114 transmitter (Model 605-11, Dwyer Instruments, IN). The chamber temperature is controlled at 115 295 K by the building's air conditioning system and increases to 305–306 K under maximum 116 irradiation conditions. The relative humidity of the chamber air is below 10% under dry 117 conditions and can be varied in the range of $\sim 10-50\%$ by flowing a portion of the purified dry 118 flushing air into the chamber through a temperature-controlled water reservoir. The chamber 119 internal pressure is maintained slightly above the ambient pressure to minimize the enclosure air 120 contamination via penetration through the Teflon film.

Prior to each experiment, the chamber was flushed with purified dry air from a zero air generator (Model 737, Aadco Instruments, OH) for >12 h until ozone and NO_x levels were below 1 ppb. During the operation of the steady state continuous flow mode, the chamber was constantly flushed with purified dry air at 40 L min^{-1} , which gives an average chamber residence time of 4.17 hours. The incoming and outgoing flows were balanced by a feedback control system that maintains a constant internal pressure of $1.2-4.9\times10^{-4}$ atm above the ambient. The characteristic mixing time in the chamber was determined to be ~9 min (~4% of the residence time) by rapid injection of tracer compounds including CO_2 and NO. Under such conditions, the gas/particle-phase composition in the outflow can be assumed identical to that in the well-mixed core of the chamber.

To mimic daytime photochemistry in the continuous flow mode, steady-state OH mixing ratio was created by photolyzing hydrogen peroxide (H₂O₂) vapor that was continuously flowing into the chamber (H₂O₂+hv \rightarrow 2OH, $J_{\text{H}_2\text{O}_2}\sim 3.93\times 10^{-7}~\text{s}^{-1}$). Specifically, a 20 mL syringe (NORM-JECT, Henke-Sass Wolf, MA) held on a syringe pump (Model 100, kdScientific, MA) kept at ~4 °C was used to deliver H₂O₂ solution (1-30 wt%, Sigma Aldrich, MO) into a glass bulb that was gently warmed at ~32 °C. The liquid delivery rate was sufficiently slow (100-300 μL min⁻¹) that all the H₂O₂ vapor was released into the glass bulb through evaporation of a small droplet hanging on the needle tip. An air stream (5 L/min) swept the H₂O₂ vapor into the chamber, resulting in an H₂O₂ mixing ratio in the range of 600 ppb to 16.22 ppm in the injection flow as a function of the concentration of H₂O₂ aqueous solution used. A spreadsheet (Table S2) for calculating the inflow H₂O₂ mixing ratio using the above input method is provided in the Supplement. As H₂O₂-laden air was continuously entering the chamber, it took approximately three turnover times (~12.5 hr) for the desired H₂O₂ vapor mixing ratio to reach steady state in the chamber. The H₂O₂ vapor concentration in the chamber, though not measured, can be estimated from the steady-state OH mixing ratio derived from the observed exponential decay of a given parent hydrocarbon. Constant NO injection flow was achieved by diluting the gas flow from a concentrated NO cylinder (NO = 133.16 ppm, balance N₂) to a desired mixing ratio (0.1–100 ppb) using a set of mass flow controllers (Tylan FC260 and FC262, Mykrolis Corp., MA). Note that for experiments performed in the absence of any VOC precursor, H₂O₂ and NO were the only two species that were continuously input into the chamber for the establishment of a combination of different photochemical conditions as denoted by the O₃ and NO_x measurements. For the isoprene photooxidation experiments, an isoprene standard ($C_5H_8 = 531$ ppm, balance N₂) was constantly injected into the chamber and diluted with the flushing air to achieve an inflow concentration of ~20 ppb.

To mimic the nighttime chemistry in the continuous flow mode, steady-state NO₃ mixing ratio was created by constantly flowing diluted O₃ and NO air into the chamber (NO+O₃

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 \rightarrow NO₂+O₂; NO₂+O₃ \rightarrow NO₃+O₂). The NO source can be replaced by NO₂, although the absolute absence of NO does not necessarily represent the actual atmospheric conditions. O₃ was produced by photolyzing O₂ in air at 185 nm using a mercury "Pen-Ray" lamp (UVP LLC, CA). Ozone concentration in the injection flow can be controlled from 3.5 ppb to 457 ppb automatically by adjusting the mercury lamp duty cycle. To study the RO₂+HO₂ pathway, formaldehyde (CH₂O) was input into the chamber along with NO and O₃ to initiate HO₂ production (NO₃+CH₂O+O₂→HNO₃+HO₂+CO). Formaldehyde agueous solution (37 wt%, Sigma Aldrich, MO) was diluted with ultrapure water (Milli-Q, Merck Millipore, MA) to 0.2–1.0 wt% and continuously input into the chamber using the same method used for H₂O₂ input described above. It is worth noting that the formaldehyde aqueous solution contains 10-15% methanol as stabilizer to prevent polymerization. The presence of methanol in the chamber does not significantly impact the nocturnal chemistry as it consumes OH and NO₃ radicals to generate formaldehyde and additional HO₂ $(CH_3OH+NO_3\rightarrow HNO_3+CH_2O+HO_2)$ CH₃OH+OH→H₂O+CH₂O+HO₂) (Atkinson et al., 2006). The use of formaldehyde as an HO₂ source mimics closely the atmospheric nighttime conditions in forest environments (Schwantes et al., 2015). To study the NO₃-initiated oxidation of isoprene, an injection flow of diluted isoprene (~10 ppb) was achieved using the procedure described above.

2.2 Analytical measurements

A suite of instruments was used to monitor gas-phase concentrations in the chamber outflow. O₃ was monitored by absorption spectroscopy with 0.5 ppb detection limit (Model 49, Thermo Scientific, CO). The O₃ monitor was calibrated using an Ozone Primary Standard in the range of 0 to 200 ppb (Model 49i-PS, Thermo Scientific, CO). The O₃ monitor used for chamber experiments was periodically checked with the primary standard and was shown to be stable over long periods of time (less than 1 ppb drift in over 1 year). NO was monitored by chemiluminescence with 0.5 ppb detection limit (Model CLD 88Y, Eco Physics, MI). Zero-point and span calibrations of the NO_x monitor were performed prior to each experiment by supplying the instrument with pure N₂ gas and diluted NO, respectively. Multi-point calibration was performed on a weekly basis and has shown a good stability and linearity in the NO measurement ranging from 1 ppb to 200 ppb. NO_x (NO+NO₂) measurements were performed using a photolytic converter that selectively converts NO₂ to NO upstream of the photomultiplier tube in the CLD 88Y NO monitor. This converter uses two opposing arrays of UV LEDs shining into a cylindrical quartz mixing tube to achieve approximately 50% conversion of NO₂ to NO per second. The total efficiency for the equipment described here is approximately 70% as determined by measuring calibrated NO₂ standards. The sample path always includes the photolytic converter, and typical experiments cycle the power for the LED lights to switch between measuring NO (lights off) and NO_x (lights on). NO₂ concentrations were then determined by subtracting the NO from the adjacent NO_x measurements.

A customized Proton Transfer Reaction Quadrupole Mass Spectrometer (PTR-Q-MS) was used to measure volatile organic compounds including isoprene (C_5H_8), methacrolein (MACR, C_4H_6O), and methyl vinyl ketone (MVK, C_4H_6O). The instrument was operated at 2.3 mbar drift pressure and 560 V drift voltage. Measurements reported here were obtained at a sampling rate of 10 Hz. In positive-mode operation, a given analyte [M] undergoes proton transfer reaction, producing an ion of the form [M+H]⁺. The instrument background was collected by sampling the chamber air for at least 30 min prior to each experiment. Measured ion intensities for isoprene ($C_5H_9^+$, m/z 69) and MACR and MVK ($C_4H_7O^+$, m/z 71) were calculated as the signal of each ion

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(counts per seconds) normalized to the total ion signal of H_3O^+ . The instrument sensitivities towards isoprene, MACR and MVK were calibrated with a mixture of diluted gas standards. The instrument sensitivity towards MACR is identical to that of MVK, and as a result, the measured $C_4H_7O^+$ signal represents the sum of MACR and MVK in the sampling air. Since artifacts in the measured $C_4H_7O^+$ signal can be produced through thermal decomposition of isoprene oxidation products, such as the peroxides, nitrates, and epoxides, on contact with hot metal surface (Liu et al., 2013; Nguyen et al., 2014; Rivera-Rios et al., 2014), a cold-trap system was used to avoid bias in the interpretation of the PTR-MS data. Specifically, a 1 m section of Teflon tubing was submerged in a low temperature ethanol bath (-40 ± 2 °C) that could trap oxidized products less volatile than the authentic MACR and MVK standards after steady state was established in the chamber. The quantification of the sum of MACR and MVK was then based on the PTR-MS measured $C_4H_7O^+$ (m/z 71) signal downstream of the cold-trap.

3. Kinetic Modeling

Reaction kinetics and mechanisms for the gas-phase photochemistry were extracted from the Master Chemical Mechanism (MCMv3.3.1, accessible at http://mcm.leeds.ac.uk/MCM/). The inorganic reaction scheme includes 21 species and 48 reactions; and the isoprene oxidation system includes 611 species and 1974 reactions. The kinetic schemes were implemented in Matlab (Mathworks) to simulate the temporal profile of a given compound *i* in the chamber operated in the steady state continuous flow mode:

$$\frac{dC_i}{dt} \cdot \tau = C_{i,0} + P_i - C_i - \sum k_i \cdot \tau \cdot C_i$$
 (Eq1)

where C_i (molec cm⁻³) is the gas-phase concentration of compound i in the well-mixed core of the chamber; $C_{i,0}$ (molec cm⁻³) is the initial gas-phase concentration of compound i in the injection flow; k_i (s⁻¹) is the pseudo-1st-order rate coefficient for a chemical reaction that consumes compound i; τ (s) is the chamber mean residence time and can be calculated as the total chamber volume divided by the incoming/outgoing flow rate; and P_i (molec cm⁻³) is the increment in the concentration of compound i through chemical production during one residence time. Note that two terms are neglected in Equation (1), i.e., organic vapor condensation onto particles and deposition on the chamber wall. This is a reasonable simplification here owing to the relatively high volatility ($\geq 10^{-1}$ atm) of compounds studied. Incorporation of these two terms into Equation (1) is feasible given the vapor pressure of compound i, suspended particle size distribution, gas-particle and gas-wall partitioning coefficient, accommodation coefficients of compound i on particles and walls, and the effective absorbing organic masses on the wall (Zhang et al., 2014a; Zhang et al., 2015b; Huang et al., 2016; McVay et al., 2016; Nah et al., 2016).

Model simulations used for comparison with chamber measurements were initialized using experimental conditions summarized in Table S1 in the Supplement. Model input parameters for all simulations include temperature (295 at dark and 306 K under irradiation), local pressure $(8.6 \times 10^4 \text{ Pa})$, relative humidity (8% at dark and 5% under irradiation), light intensity $(J_{\text{NO}_2}=1.27 \times 10^{-3} \text{ s}^{-1})$ under irradiation and 0 at dark), chamber mean residence time (4.17 h), and input mixing ratios of H_2O_2 (0.11–16.2 ppm for photolytic experiments), NO (0.1–100 ppb for photolytic experiments and 10–20 ppb for dark experiments), O₃ (22–225 ppb for dark experiments), HCHO (0–600 ppb for dark experiments), and isoprene (19.9 ppb for photolytic

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experiments and 10.2 ppb for dark experiments). The model was propagated numerically for 25 h duration for each experiment.

4. Results and Discussions

4.1 Optimal operating conditions for daytime photochemistry

Figure 1 shows the model predicted steady-state mixing ratios of OH, HO_2 , NO_3 , NO, NO_2 , and O_3 in the chamber after 20 hours of photochemical reactions as a function of the H_2O_2 and NO concentrations in the continuous injection flow. Six blank chamber experiments were compared with simulations. In general, the model captures the evolution patterns of NO_x and O_3 well. The predicted mixing ratios of NO, NO_2 , and O_3 agree within 69%, 11%, and 33%, respectively, with the measurements (see Table S1 and Figure S1 in the Supplement). The relatively large NO uncertainties originate from the measurements that were performed close to the instrument detection limit (0.5 ppb).

Simulated steady-state mixing ratios of OH radicals ([OH]_{ss}) range from $\sim 5 \times 10^5$ to $\sim 4 \times 10^6$ molec cm⁻³, which over ~ 4 hours chamber residence time would be roughly equivalent to ~ 1 h to ~ 8 h of atmospheric OH exposure (1×10^6 molec cm⁻³). As expected, [OH]_{ss} increases with increasing NO influxes due to the enhanced NO_x/O₃ cycling but decreases with increasing H₂O₂ influxes owing to the overwhelming reaction OH+H₂O₂ \rightarrow H₂O+HO₂. As a consequence, the steady-state mixing ratios of HO₂ radicals ([HO₂]_{ss}) reach up to $\sim 7 \times 10^9$ molec cm⁻³ when 16.2 ppm H₂O₂ is continuously injected into the chamber. If 110 ppb H₂O₂ is used instead, the resulting [HO₂]_{ss} levels fall close to the ambient range ($\sim 10^8$ molec cm⁻³).

Simulated steady-state NO mixing ratios in the chamber range from ~2 ppt to ~0.9 ppb from combinations of 0.1-20 ppb NO and 0.11-16.22 ppm H₂O₂ in the injection flow. The ratio of inflow NO concentration to the steady-state NO concentration in the chamber ranges from 5 to 93, demonstrating the importance of chemical removal in controlling the overall steady-state NO levels. O₃ accumulation is an inevitable consequence under photolytic conditions and, for example, the presence of 10 ppb O_3 leads to the chemical removal term $(k_{O_3+NO} \cdot [O_3] \cdot \tau)$ in Equation (1) that reduces the steady-state NO concentration by a factor of 60. It is worth noting that under all simulated conditions in the continuous flow mode, O₃ (~1-126 ppb) coexists with NO (~0.002-0.9 ppb). This particular chemical scenario, which is impossible to achieve in batch-mode reactors due to prompt conversion of NO to NO₂, could then be used to mimic ambient ozonolysis chemistry, for example, in forest regions that frequently encounter polluted air masses from nearby urban areas. The steady-state mixing ratios of NO₂ ([NO₂]_{ss}) exhibit a strong linear correlation with NO influxes. The use of less than 20 ppb NO in the injection flow results in a few to tens of ppb [NO₂]_{ss} that is higher than the range typically found in the ambient. The potential 'quenching' effect of NO2 on RO2 radicals through reversible termolecular reactions is discussed shortly.

In the so-called 'high- NO_x ' chamber experiments, the NO_3 radical is an unavoidable side-product when black lights are used as a representative of the solar radiation in mimicking the daytime photochemistry in the troposphere. The photolysis of NO_3 , although its primary sink in the atmosphere, proceeds rather slowly $(J_{NO_3} \sim 1.8 \times 10^{-3} \text{ s}^{-1})$ under the present chamber photolytic conditions, thereby leading to a significant accumulation of NO_3 radicals $(7.9 \times 10^4 - 2.8 \times 10^8 \text{ molec cm}^{-3})$ at steady state. The simulated NO_3/OH ratio dictates the extent to

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which the NO_3 (nighttime) chemistry competes with the OH-initiated (daytime) photochemistry. For compounds that are highly reactive towards NO_3 such as isoprene, NO_3 -initiated oxidation accounts for up to ~60% of the overall isoprene degradation pathways at the highest NO_3/OH ratio (~255) simulated. Low concentrations of NO (< 20 ppb) and H_2O_2 (< 2 ppm) in the injection flow are therefore necessary to limit the interferences of NO_3 -initiated chemistry. Again, taking isoprene as an example, the NO_3 oxidation pathway contributes less than 0.1% of the overall isoprene degradation kinetics at the lowest NO_3/OH ratio (~0.13) simulated here.

Also given in Figure 1 is the calculated lifetime (τ_{RO_2}) of an RO₂ radical with respect to reactions with NO and HO₂ at 306 K. In most batch-mode chamber experiments, τ_{RO_2} of only several seconds or less can be achieved, due to the presence of tens to hundreds of ppb levels of NO and HO₂. Here τ_{RO_2} could extend to 60 s or even longer with the continuous input of low mixing ratios of H_2O_2 (≤ 110 ppb) and NO (≤ 0.2 ppb). Note that the presence of tens of ppb NO₂ in the chamber might impose a 'quenching' effect on the steady state RO₂ level through rapid reversible reactions ($RO_2+NO_2+M\leftrightarrow RO_2NO_2+M$). We evaluate this potential 'quenching effect' using ethylperoxy radical (C₂H₅O₂) generated from OH-oxidation of ethane as an example. Simulations shown in Figure S2 in the Supplement reveal that incorporation of the $C_2H_5O_2+NO_2+M\leftrightarrow C_2H_5O_2NO_2+M$ reaction into the mechanism in the presence of ~1–80 ppb NO₂ does not notably change the behavior of C₂H₅O₂ radical. One exception is the peroxyacyl radical, which combines with NO₂ yielding peroxyacyl nitrate. For example, under 0.1–16 ppb [NO₂]_{ss} as displayed in Figure 1, we calculate that the time needed for peroxyacetyl radical $(CH_3C(O)O_2)$ equilibrium with peroxyacetyl reach nitrate $(CH_3C(O)O_2+NO_2+M\leftrightarrow CH_3C(O)O_2NO_2+M)$ ranges from ~1 to ~10 s, suggesting that the lifetime of peroxyacyl radicals is ultimately controlled by NO₂ instead of NO/HO₂ in the reaction system, and consequently, peroxyacyl radicals are not expected to be long-lived in the current chamber configuration.

4.2 Application to OH-initiated oxidation of isoprene

Methacrolein (MACR) and methyl vinyl ketone (MVK) are major first-generation products from the OH-initiated oxidation of isoprene in the presence of NO (Wennberg et al., 2017). They are produced from the decomposition of β-ISOPO alkoxy radicals that are primarily formed from the reaction of β -ISOPOO peroxy radicals (β -1-OH-2-OO and β -4-OH-3-OO) with NO, see mechanisms displayed in Figure 2 (A). Reactions of β-ISOPOO peroxy radicals with HO₂ and RO₂ also partially yield β-ISOPO alkoxy radicals that ultimately lead to MACR and MVK, although these pathways are considered to be minor in the presence of hundreds to thousands of ppt NO in the atmosphere. The molar yields determined from previous studies range from 30–35% for MVK and 20–25% for MACR under high NO conditions (NO > 60 ppb) (Tuazon and Atkinson, 1990; Paulson and Seinfeld, 1992; Miyoshi et al., 1994; Ruppert and Becker, 2000; Galloway et al., 2011). It has been recently shown that the six hydroxyl peroxy radicals (ISOPOO) produced from the initial OH addition to the double bonds of isoprene undergo rapid interconversion by removal/addition of O2 that competes with bimolecular reactions under atmospherically relevant NO levels (Peeters et al., 2014; Teng et al., 2017). As a result, the distribution of ISOPOO radical isomers and their subsequent reaction products varies with their lifetimes with respect to bimolecular reactions. In the presence of hundreds of ppb NO as done by most previous experimental studies, the reaction of ISOPOO radicals with NO dominates over their interconversion, and the production of β-ISOPOO peroxy radical is less favored, leading

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the experiments to underestimate the MACR and MVK yields typically obtained in ambient conditions. Measurements by Liu et al. (2013) conducted at NO concentrations comparable to the urban environment (~1 ppb) found much higher MACR (~31.8%) and MVK (~44.5%) yields than other previous studies.

Here we perform a steady-state continuous-mode experiment to measure the production of MACR and MVK from the OH-initiated oxidation of isoprene in the presence of \sim 0.45 ppb NO. Figure 3 shows the observed and simulated temporal profiles of NO_x, O₃, C₅H₈, and C₄H₆O over 24 hours photooxidation of isoprene. In this experiment, C₅H₈, H₂O₂, and NO were continuously fed into the chamber, with constant inflow concentrations of 19.9 ppb, 600 ppb, and 19 ppb, respectively. An outgoing flow at 40 L min⁻¹ continuously withdrew air from the chamber to balance the pressure. After approaching steady state, the sampling tube was submerged into an ethanol low temperature bath (-40 ± 2 °C) to trap oxidized products that would otherwise undergo thermal decomposition introducing interferences in the C₄H₇O⁺ (m/z 71) signal. The measured concentrations of C₅H₈ and C₄H₆O upon cold-trapping agree within 2.8% and 4.6% uncertainties with the model simulations, see Fig.3 (C) and (D).

To calculate the total molar yield $(Y_{C_4H_6O})$ of MACR and MVK, two reactions are considered:

$$C_5H_8 + OH \xrightarrow{k_1} Y_{C_4H_6O} \cdot C_4H_6O + products$$
 (R1)

$$C_4H_6O + OH \xrightarrow{k_2} products$$
 (R3)

where k_1 is the rate constant for OH reaction with isoprene, and k_2 is taken as the average of rate constants for OH reactions with MACR and MVK. Uncertainties associated with the simplification of k_2 in calculating the MACR and MVK yields will be discussed shortly. Also note that the ozonolysis and NO₃-initiated oxidation in total account for less than 6% of isoprene degradation pathway under current experimental conditions and are neglected in the calculation.

In the continuous-mode operation, two mass conservation equations are satisfied at steady state:

$$\frac{d[C_5H_8]_{ss}}{dt} = [C_5H_8]_0/\tau - [C_5H_8]_{ss}/\tau - k_1 \cdot [OH]_{ss} \cdot [C_5H_8]_{ss} = 0$$
 (Eq2)

$$\frac{d[C_4H_6O]_{ss}}{dt} = Y_{C_4H_6O} \cdot k_1 \cdot [OH]_{ss} \cdot [C_5H_8]_{ss} - k_2 \cdot [OH]_{ss} \cdot [C_4H_6O]_{ss} - [C_4H_6O]_{ss} / \tau = 0$$
 (Eq3)

where $[C_5H_8]_{ss}$ and $[C_4H_6O]_{ss}$ are the PTRMS measured steady-state concentrations of isoprene and the sum of MACR and MVK when using the cold trap, respectively, $[C_5H_8]_0$ is the initial concentration of isoprene, and τ is the chamber mean residence time and can be calculated as the total chamber volume divided by the incoming/outgoing flow rate. The steady state OH radical concentration ($[OH]_{ss}$) can be derived by solving Equation (2). The calculated $[OH]_{ss}$ (3.13×10⁶ molec cm⁻³) is 12% higher than the model prediction (2.74×10⁶ molec cm⁻³). The molar yield of the sum of MACR and MVK from isoprene OH oxidation pathway in the presence of ~0.45 ppb NO is thus given by Equation (4) and calculated as 76.7±5.8%:

$$Y_{C_4H_6O} = \frac{[C_4H_6O]_{ss} + k_2 \cdot [OH]_{ss} \cdot \tau \cdot [C_4H_6O]_{ss}}{k_1 \cdot [OH]_{ss} \cdot \tau \cdot [C_5H_8]_{cs}} \times f_{\beta\text{-ISOPOO+NO}}$$
(Eq4)

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Here a 5.8% uncertainty originates from the assumption that MACR+OH and MVK+OH proceed with equal reaction rate, although the rate constant for MVK+OH is ~31% lower than that of MACR+OH. Another potential uncertainty relates to the accuracy of the simulated steady state HO₂ and RO₂ concentrations and the contribution of β-ISOPOO+HO₂ and β-ISOPOO+RO₂ reaction pathways to the overall β-ISOPOO fate. The fraction of β-ISOPOO radicals that reacts with NO ($f_{\beta-ISOPOO+NO}$) was predicted as 0.88, which was used here to scale the final MACR+MVK yield, see Eq(4).

In summary, the measured yield of the sum of MACR and MVK in this study is close to that reported by Liu et al. (2013), but ~27–52% higher than the majority of previous measurements performed under high NO conditions (NO > 60 ppb). This is consistent with the dynamic nature of the six ISOPOO radical isomers that undergo rapid interconversion by addition/removal of O_2 . In the presence of ~0.45 ppb NO as performed in this study, lifetimes of the β -1-OH-2-OO peroxy radical with respect to reaction with NO and loss of O_2 are estimated as 9.4 s and 0.2 s, respectively, implying that the rapid interconversion between β -ISOPOO and δ -ISOPOO radicals essentially governs their distribution, and under such conditions, the production of thermodynamically more stable β -ISOPOO isomers is favored, leading to higher yields of MACR and MVK. Here the reported MACR and MVK yield from isoprene OH oxidation in the presence of ~0.45 ppb NO represents an illustration of chamber operation at steady state continuous flow mode for the establishment of certain experimental conditions that are not easily accessible from traditional batch-mode chamber experiments. A complete measurement of first-generation oxidation products from isoprene OH reaction under a wide range of NO levels (ISOPOO bimolecular lifetimes) will be forthcoming in a future publication.

4.3 Optimal operating conditions for nighttime chemistry

Figure 4 shows the model simulated steady-state mixing ratios of HO_2 , NO_3 , NO, NO_2 , and O_3 after 16 hours of dark reactions in the chamber as a function of the HCHO concentration and O_3/NO ratio in the continuous chamber inflow. Blank experiments were compared with simulations in five cases (see Table S1 in the Supplement). The model captures the evolution patterns of NO_x and O_3 well. The observed mixing ratios of NO_2 and O_3 agree with the simulations to within 11% and 6%, respectively (Figure S3 in the Supplement).

Compared with the photochemical reaction schemes discussed earlier, the nocturnal chemistry is rather straightforward; that is, the inflow O_3/NO ratio governs the steady-state concentrations of NO_3 , NO_x , and O_3 , while the inflow HCHO concentration ultimately controls the steady-state HO_2 level. Increasing the O_3/NO ratio from 1 to 9 in the continuous inflow leads to increased NO_3 from 2.4×10^5 to 1.1×10^9 molec cm⁻³, but decreased NO_3 from 1.8 ppb to 20 ppt and decreased NO_2 from 18 to 7 ppb. At a fixed inflow O_3/NO ratio, doubling the NO_3 and O_3 concentrations leads to elevated NO_3 , NO_x , and O_3 by a factor of 2.0-3.2, 1.5-2.0, and 1.4-2.0, respectively. The use of HCHO as an effective dark HO_2 source does not significantly impact the steady-state mixing ratios of NO_x and O_3 , but slightly weakens the NO_3 production.

The calculated RO_2 lifetime (τ_{RO_2}) with respect to reactions with NO, NO₃, and HO₂ at 295 K ranges from 3 to 225 s. The highest τ_{RO_2} was achieved in the absence of any HCHO source and corresponds to a chemical regime that can be employed to study the intramolecular isomerization (autoxidation) pathway of RO_2 radicals, if any. Adding a continuous flow of HCHO to the system leads to the production of 10^7 – 10^9 molec cm⁻³ HO₂ radicals that then

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constitute a significant sink of RO₂ radicals and represents prevailing forest environments during nighttime.

4.4 Application to NO₃-initiated oxidation of isoprene

NO₃-initiated oxidation of isoprene proceeds by the NO₃ addition to the carbon double bonds followed by O₂ addition, yielding six distinct nitrooxy peroxy radicals (INOO), including two isomers (β -INOO) with O₂ added on the β -carbon to the nitrate group (see Figure 2B for schematic illustration). The β -INOO radicals react further with NO₃, HO₂, NO, and RO₂, producing nitrooxy alkoxy radicals (β -INO) with molar yields of 1.00, 0.53, 0.97, and 0.40, respectively (Wennberg et al., 2017). The further decomposition of β -INO radicals produces MACR and MVK, together with HCHO and NO₂. Depending on the actual fate of β -INOO radicals, the yields of β -INO radicals can then vary from 0.4 to 1.0, resulting in a distinct distribution of final oxidation products. It is thus important to specify the ultimate fate of INOO radicals during quantification of oxidation products from isoprene reaction with NO₃. As an illustration, we performed one continuous mode experiment that targets on controlling the steady-state fate of INOO radicals to be their reaction with NO and HO₂ (46% and 38% INOO radicals are predicted to react with NO and HO₂, respectively, as shown in Fig.5). Note that by adjusting the concentrations and fractions of inflow reactants (O₃, NO, HCHO, and C₅H₈), different chemical fates and lifetimes of INOO radicals can be achieved.

Figure 5 shows the observed and predicted temporal profiles of NO_x, O₃, C₅H₈, and C₄H₆O over 25 hours of isoprene oxidation by NO₃, with continuous input of 10.2 ppb C₅H₈, 205 ppb O₃, and 59 ppb NO into the chamber and a balancing outgoing flow at 40 L min⁻¹ carrying wellmixed reactants and products. It took >16 hours to reach steady state for all the species displayed. In general, the model captures the trends of O₃ and NO well, while underpredicting the steady state NO₂ by ~26%. After ~18 hours of dark reaction, the PTR-MS sampling tubing was submerged into an ethanol cold bath (- 40±2 °C) to trap artifacts in the PTR-MS measured $C_4H_7O^+$ (m/z 71) signal. The simulated steady-state concentration of isoprene agrees within 9% with the measurements. The derived concentration of the sum of MACR and MVK from the measured $C_4H_7O^+$ ion intensity upon cold-trapping is ~1.1 ppb, which is ~129% higher than the model predictions (~0.48 ppb). This disagreement can be attributed, to a large extent, to the oversimplified representation of the six different INOO radicals as one δ-INOO isomer in the MCMv3.3.1 mechanism. As a result, the production of β-INOO radical, the important precursor of MACR and MVK, from NO₃-initiated oxidation of isoprene is suppressed in the simulations. The measured molar yield of the sum of MACR and MVK is 36.3±12.1%, with uncertainties arising from the fact that 10.5% isoprene is predicted to react with OH as an additional source of MACR and MVK. Using this value, the fraction of β-INOO over the sum of nitrooxy peroxy radicals is estimated as $48.6\pm16.2\%$, which is close to that (~46.3%) reported by Schwantes et al. (2015), although the estimated bimolecular lifetime of INOO radical in that study (~30 s) is lower than that predicted in the present work (~50 s). As discussed above, the hydroxyl peroxy radicals produced from OH-oxidation of isoprene could undergo rapid interconversion through addition/removal of O₂ at atmospherically relevant lifetimes. This interconversion significantly impacts the subsequent chemistry of individual ISOPOO radical isomers in terms of reaction rates and product distributions. It is likely that the INOO radicals follow similar interconversion due to the small R-OO bond dissociation energy, although no experimental evidence exists. A full examination of the INOO chemistry, i.e., their kinetic and thermodynamic properties as well

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as their chemical fate at different lifetimes, will be the focus of future studies using this continuous flow chamber operation method.

5. Conclusions

We report here the development and characterization of the NCAR Atmospheric Simulation Chamber operated at steady state continuous flow mode for simulating daytime and nocturnal chemistry under atmospherically relevant NO levels. The chamber is designed to achieve a well-controlled steady-state environment by continuous inflow of reactants and continuous withdrawal of reactor contents. We use a combination of kinetic modeling and chamber experiments to characterize the 'intermediate-NO' chemical regime (tens of ppt to a few ppb) that can be achieved by precisely controlling the inlet reactant concentrations and the mixing/residence timescales of the chamber.

To mimic daytime photochemistry, continuous input of H_2O_2 and NO gases is required, resulting in steady state OH mixing ratios of $10^5 - 10^6$ molec cm⁻³ under irradiation. Under such conditions, the lifetime of a peroxy radical with respect to reaction with NO and HO_2 can be extended to 60 s or even longer, thus providing a unique environment to study all reaction possibilities of RO_2 radicals including the intramolecular isomerization (autoxidation) pathway. When studying OH-initiated chemistry, care needs to be taken to avoid a range of experimental conditions (e.g., inflow $H_2O_2 > 2$ ppm and NO > 20 ppb) where NO_3 -oxidation might account for a large fraction of the overall degradation pathway of certain parent hydrocarbons such as alkenes.

To mimic nighttime chemistry, continuous input of NO (or NO₂) and O₃ is needed to produce steady state NO₃ radicals in the range of 10⁶–10⁹ molec cm⁻³ in the dark. Under such conditions, an RO₂ radical can live up to 4 min prior to finding a bimolecular reaction partner (e.g., NO, NO₃, and HO₂), which were the dominant fates of RO₂ radicals in most batch-mode chamber experiments. Again, the long lifetime of RO₂ radicals achieved by the steady state continuous mode operation opens an avenue for close examination of RO₂ unimolecular (isomerization) pathways in nocturnal environments.

In simulating both daytime and nighttime chemistry with continuous flow operation method, O_3 accumulation is unavoidable. The extent to which ozonolysis interferes with OH- or NO_3 -initiated oxidation chemistry depends on the steady state O_3 concentration achieved in the chamber and its reactivity towards various parent VOCs. Taking isoprene as an example, ozonolysis accounts for <1% and <0.1% of the overall isoprene degradation kinetics, respectively, under established steady-state photolytic and dark conditions described above.

In atmospheric chemistry, the terms 'zero-NO' versus 'high-NO' have been widely used to classify photooxidation conditions and delineate the gas-phase fate of the peroxy radicals (RO₂) generated from VOCs oxidation (Cappa et al., 2013; Zhang and Seinfeld, 2013; Loza et al., 2014; Schilling Fahnestock et al., 2014; Zhang et al., 2014b; Krechmer et al., 2015; Nguyen et al., 2015; Zhang et al., 2015a; Riva et al., 2016; Schwantes et al., 2017). In the so-called 'high-NO' regime, reaction with NO dominates the fate of RO₂ radicals, whereas in the 'zero-NO' regime, the RO₂ radicals primarily undergo reaction with HO₂ and, perhaps to a much lesser degree, self/cross-combination. The importance of the 'intermediate-NO' regime lies in the fact that at sub-ppb levels of NO, the RO₂+NO and RO₂+HO₂ reactions are expected to co-exist and the RO₂ radical could survive up to several minutes before encountering a partner (NO/HO₂) for

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- 497 bimolecular reactions. Under such conditions, the RO₂ radical isomers may undergo
- 498 interconversion by addition/removal of O₂ and intramolecular isomerization (autoxidation)
- 499 through H-shift. Here we use isoprene as an illustrative VOC to explore the fate of RO₂ radicals
- under sub-ppb NO. Future work will focus on detailed characterization of oxidation products
- from isoprene day- and nighttime chemistry with particular attention given to the controlled RO₂
- fates and lifetimes.

503 Data Availability

Data presented in this manuscript are available upon request to the corresponding author.

505 Competing interests

The authors declare that they have no conflict of interest.

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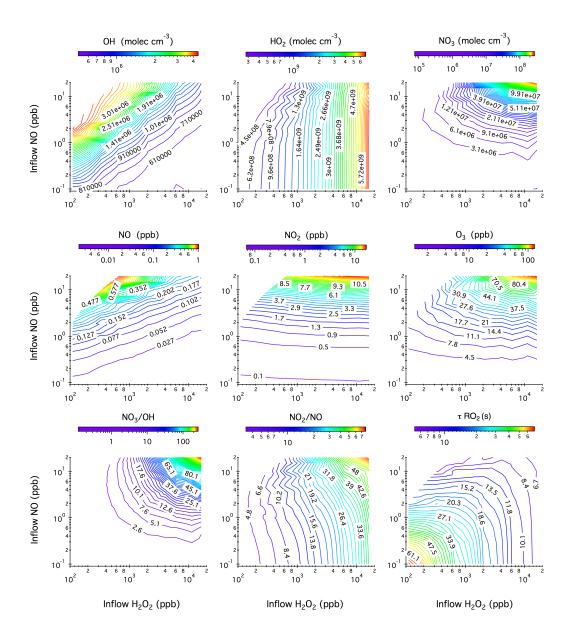


Figure 1. Contour plots showing the model predicted steady-state mixing ratios of OH, HO_2 , NO_3 , NO, NO_2 , and O_3 after 20 hours of photochemical reactions in the chamber as a function of the concentrations of H_2O_2 and NO in the continuous injection flow. Also given here are the simulated NO_3 to OH ratio, NO_2 to NO ratio, and the lifetime of an RO_2 radical (τ_{RO_2}) with respect to reactions with NO and HO_2 . Note that the ripples on the contour lines originate from the limited simulation datasets that are used to generate iso-response values.

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Figure 2. Representative mechanism for (A) OH- and (B) NO_3 -initiated oxidation of isoprene that leads to the formation of MACR and MVK.

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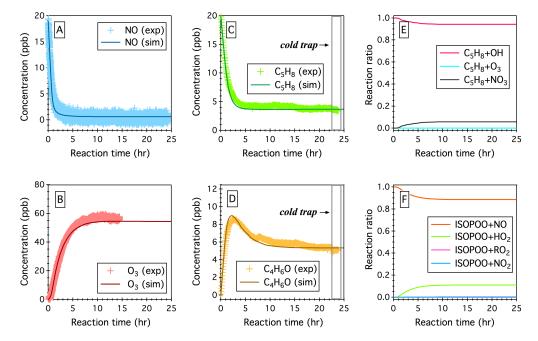


Figure 3. Simulated (sim.) and observed (exp.) temporal profiles of (A) NO, (B) O_3 , (C) isoprene (C_5H_8), and (D) the sum of MACR and MVK (C_4H_6O) over 24 hours OH-initiated oxidation of isoprene in the continuous-flow mode chamber operation. Also displayed here include (E) simulated fractions of OH-oxidation, ozonolysis, and NO₃-oxidation as the removal pathways of isoprene, and (F) simulated fractions of ISOPOO radicals that react with NO, HO₂, RO₂, and NO₃. Time 0 is the point at which the chamber lights are turned on. Initial experimental conditions are 19 ppb NO, 0 ppb NO₂, 0 ppb O₃, 600 ppb H₂O₂, and 19.9 ppb C_5H_8 , with continuous input of 600 ppb H₂O₂, 19 ppb NO, and 19.9 ppb C_5H_8 over the course of 24 hour photochemical reactions.

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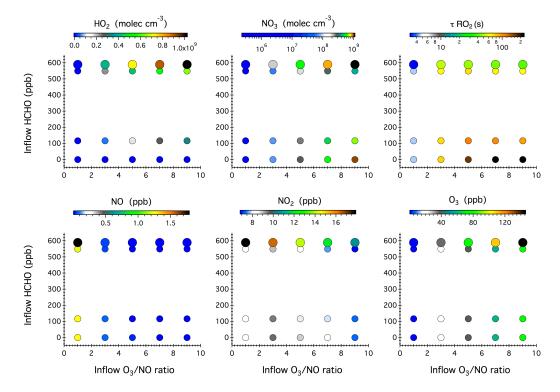


Figure 4. Simulated steady-state mixing ratios of HO_2 , NO_3 , NO, NO_2 , and O_3 after 16 hours of dark reactions in the chamber as a function of the concentrations of NO and O_3 in the continuous injection flow. The symbol size denotes different inflow NO concentrations, i.e., 10 ppb and 20 ppb. Also given here is the calculated lifetime of an RO_2 radical (τ_{RO_2}) with respect to reactions with NO, NO_3 , and HO_2 .

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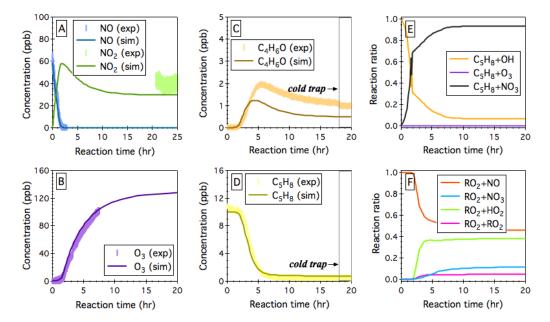


Figure 5. Simulated (sim.) and observed (exp.) evolution patterns of (A) NO_x , (B) O_3 , (C) the sum of MACR and MVK (C_4H_6O), and (D) isoprene (C_5H_8) over 25 hours NO_3 -initiated oxidation of isoprene under continuous-flow mode chamber operation. The fractions of isoprene that react with OH, O_3 , and NO_3 are given in panel (E), and the fractions of INOO radical that undergo bimolecular reactions with NO, NO_3 , HO_2 , and RO_2 are given in panel (F). Initial experimental conditions are 0 ppb O_3 , 59 ppb NO_x , and 10.2 ppb C_5H_8 , with continuous input of 205 ppb O_3 , 59 ppb NO, and 10.2 ppb C_5H_8 over the course of 25 hour dark reactions.