

23 January 2019

Dear Dr. Abbatt,

Thank you again for the opportunity to revise our manuscript for further consideration by Atmospheric Measurement Techniques. The suggestions made by the reviewer were fair and have further improved our manuscript. Below are the original reviewer comments and suggestions (in italics) and our responses. Accompanying this letter are the: 1) manuscript with edits tracked for easier review, 2) manuscript with all edits incorporated and not tracked, and 3) revised supporting information. Again, thank you for the opportunity to submit our revised manuscript to AMT and we look forward to further feedback.

Sincerely,

Sarra M. Dunham-Cheatham, Postdoctoral Scholar
Mae Sexauer Gustin, Professor
Matthieu B. Miller

Reviewer 1:

GENERAL COMMENTS:

I believe the supplementary experiments that tested the pyrolyzer up to 1000 °C are of great benefit to this manuscript as it provide the necessary evidence that it is likely the responsible party for the higher recoveries. While a safe and operational 1000 °C pyrolyzer would have been ideal for all the experiments I can understand concerns if it was not entirely stable or safe for on-going operation.

I will now accept the manuscript for publication if the following minor corrections and updates are made:

SPECIFIC COMMENTS:

Line 29: Please write the actual value (127%) and not >100%

We have added the actual value to this sentence.

Lines 30-32: Please rephrase this sentence to:

"The low HgBr₂ breakthrough on the downstream CEMs (<1%), suggest that the elevated recoveries are more likely related to sub-optimal pyrolyzer conditions or inefficient collection on the Tekran 2537 gold trap."

The low breakthrough is what suggests the pyrolyzer likely being responsible for the elevated recoveries, not the elevated recoveries suggesting poor pyrolyzer conditions.

We have reworded this sentence using the reviewer's suggested sentence.

Lines 38-39: The authors have now removed any and all discussion on the concerns of using the more general terminology RM, which was my concern in the original round of reviews "More

caution should be used in the definition of the term reactive mercury (RM)."

The "Often" (or perhaps sometimes) use of RM is by one or maybe two research groups. This does not qualify as often.

Since the authors are struggling for a descriptive terminology due to their own interchanging use of GOM and RM in their literature I suggest the following simple and clear addition:

"While the term RM does dilute some specific information in regard to the state of oxidized Hg in the atmosphere it does remove some of uncertainty as whether or not PBM contributes to the Hg collected by the CEMs."

This qualifying statement has been added.

Lines 117-118: Should be "We attempted to explain..."

The error has been corrected.

Lines 200-202: Please do not use "pretty" in a scientific paper. It is a colloquial and very unspecific term. Can the authors be more quantitative here? Use the data from SI Figure 4. What was the collection efficiency compared to 1000 °C? State this. This doesn't mean this value describes the exact inefficiency of the existing system (which should be mentioned), but it does a better job than "pretty".

A more quantitative discussion of the pyrolyzer efficiency has been added.

Lines 276-280: Linearity of the first filters remains poorly addressed. Fit both a linear and exponential curve to the data with equations and r^2 values (as suggested below). The authors say in their response:

"There are only five data points, so we feel any assertion about this relationship being linear or exponential is not robust."

The authors seems to be using this as some form excuse as to why this should not be discussed, but on the contrary why did this again not sound some alarm bells and why was this set-up not re-tested? This goes specifically with the sentiments of myself and one other reviewer that experiments were rushed and less conclusive than they should have been. The authors are happy to conclude the linearity of the relationship based on limited data, but seem to not want to make conclusions if they pose a problem. This is and has been a concern of mine because if it is a exponential relationship then it would pose a problem for lower concentrations. Some form of description or discussion on this point IS necessary.

Linear and exponential models equations and r^2 values have been added to SI Figure 5 for both sets of membranes, and more discussion has been added to the end of section 3.1.

Line 369-371: This sentence should be changed to:

"Although further work is required to more definitively determine detection and quantification limits of the various CEM methodologies, based on the mean total Hg mass of 50 ± 20 pg observed in this study, the artifact of GEM uptake to the CEMs would be below the detection limit observed here."

This sentence finally provides an (albeit subtle) mention that work is still required on defining

detection and quantification limits of the CEM methodologies that I have suggested in all rounds of review.

The requested revision has been made.

Line 406: Please add the following after the sentence concluding on line 406:

“Evidence for this conclusion can be seen in by the XX % increase in Hg collection by the pyrolyzer at 1000 °C (see SI Figure 4) in supplementary experiments.”

The sentence has been added.

SUPPLEMENTAL

In the current supplemental information that caption to SI Figure 5 has a caption. This caption should obviously be removed for publication.

BUT, it makes a perfect point. Add both linear and exponential curves with their appropriate equations and r² values. This is something I have been inquiring about throughout the reviews and even co-authors have asked for its inclusion.

The linear and exponential curve equations and r² values have been added to the Figure, and the mentioned comment on the figure caption has been removed.

1 **Evaluation of cation exchange membrane performance under exposure to high Hg⁰ and**
2 **HgBr₂ concentrations**

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13 **Abstract**

14 Reactive mercury (RM), the sum of both gaseous oxidized Hg and particulate bound Hg, is an
15 important component of the global atmospheric mercury cycle, but measurement currently
16 depends on un-calibrated operationally-defined methods with large uncertainty and demonstrated
17 interferences and artifacts. Cation exchange membranes (CEM) provide a promising alternative
18 methodology for quantification of RM, but method validation and improvements are ongoing.
19 For the CEM material to be reliable, uptake of gaseous elemental mercury (GEM) must be
20 negligible under all conditions, and RM compounds must be captured and retained with high
21 efficiency. In this study, the performance of CEM material under exposure to high
22 concentrations of GEM (1.43×10^6 to 1.85×10^6 pg m⁻³) and reactive gaseous mercury bromide
23 (HgBr₂ ~ 5000 pg m⁻³) was explored, using a custom-built mercury vapor permeation system.
24 Quantification of total permeated Hg was measured via pyrolysis at 600 °C and detection using a
25 Tekran[®] 2537A. Permeation tests were conducted for 24 to 72 hours in clean laboratory air, with
26 absolute humidity levels ranging from 0.1 to 10 g m⁻³ water vapor. GEM uptake by the CEM
27 material averaged no more than 0.004% of total exposure for all test conditions, which equates to
28 a non-detectable GEM artifact for typical ambient air sample concentrations. Recovery of HgBr₂

29 on CEM filters was ~~>100~~on average 127-% compared to calculated total permeated HgBr₂ based
30 on the downstream Tekran[®] 2537A data. The low HgBr₂ breakthrough on the downstream CEMs
31 (<1%) suggest that the elevated recoveries are more likely related to sub-optimal pyrolyzer
32 conditions or inefficient collection on the Tekran[®] 2537A gold traps.~~These results suggest~~
33 ~~incomplete thermal decomposition due to the pyrolyzer or the gold trap in the Tekran 2537, as~~
34 ~~the CEM demonstrated a high collection efficiency for HgBr₂, as indicated by less than 1%~~
35 ~~downstream breakthrough on average.~~

36

37 **1 Introduction**

38 Mercury (Hg) is a persistent environmental contaminant with a significant atmospheric life time,
39 and the form and chemistry of Hg is an important determinant of its biogeochemical cycling.
40 Mercury in the atmosphere is found in three forms: gaseous elemental mercury (GEM), gaseous
41 oxidized mercury (GOM), and particulate bound mercury (PBM). PBM and GOM are often
42 quantified together as reactive mercury (RM = GOM + PBM); while the term RM dilutes some
43 specific information regarding the state of GOM in the atmosphere, it removes some uncertainty
44 as to whether or not PBM contributes to the Hg collected by the CEMs. Atmospheric GEM, at an
45 average global background concentration of 1 to 2 ng m⁻³, can be reliably measured with
46 calibrated analytical instruments (Gustin et al., 2015; Slemr et al., 2015). The measurement of
47 GOM and PBM requires detection at part per quadrillion (pg m⁻³) concentrations, and depends
48 currently on un-calibrated operationally defined methods with demonstrated interferences and
49 artifacts, and concomitant large uncertainty (Maruszczak et al., 2017; Jaffe et al. 2014; McClure et
50 al. 2014; Gustin et al. 2013; Lyman et al. 2010). Recent reviews (Zhang et al., 2017; Gustin et

51 al., 2015) detail the shortcomings, difficulties, developments, and ongoing improvements [needed](#)
52 for atmospheric RM measurements.

53 One alternative methodology that may provide improved measurement of ambient RM involves
54 use of cation exchange membranes (CEM). CEM materials have been used to selectively
55 measure GOM concentrations in ambient air in previous studies (Huang et al., 2017; Maruszczak
56 et al., 2017; Pierce and Gustin, 2017; Huang and Gustin, 2015a; Huang et al., 2013; Sheu and
57 Mason, 2001; Ebinghaus et al., 1999; Mason et al., 1997; Bloom et al., 1996). Use of CEM type
58 filters (then manufactured by Gelman Sciences and referred to as “ion exchange membranes”)
59 for this purpose was first documented in the literature in a conference presentation (Bloom et al.,
60 1996), though these had also been deployed in an earlier field-based international comparative
61 study of RM measurement techniques in September, 1995 (Ebinghaus et al., 1999). In the
62 comparative study, one participating lab deployed a series of ion exchange membranes (for
63 GOM) behind a quartz fiber filter (for PBM) at a sample flow rate of 9 to 10 Lpm, for 24 h
64 measurements (filter pore sizes were not reported). Results for PBM and GOM were in similar
65 ranges of 4.5 to 26 pg m^{-3} and 13 to 23 pg m^{-3} , respectively (Ebinghaus et al., 1999).

66 The ion exchange membrane method was also applied in a 1995-96 field campaign for
67 determining the speciation of atmospheric Hg in the Chesapeake Bay area (Mason et al., 1997).
68 This study used a 5-stage Teflon filter pack system that included one up front quartz fiber filter
69 (0.8 μm pore size) to remove particles, and four downstream Gelman ion exchange membranes
70 (pore size not reported) to 1) capture GOM, 2) capture GOM breakthrough, 3) serve as
71 deployment blanks, and 4) isolate the filter train on the downstream side (Mason et al., 1997).
72 Concentrations of GOM were reported to be 5-10 pg m^{-3} , essentially at or below the method
73 detection limit and it was speculated that even this small amount may have been an artifact from

74 fine particulate Hg passing through the 0.8 μm quartz fiber filter (Mason et al., 1997). These low
75 concentrations are likely due to GOM being degraded on the quartz fiber filter or inefficient
76 uptake by the Gelman filter (see Supplemental Information Gustin et al. 2013). The 3rd-in-series
77 ion exchange membrane blanks were reported to be not significantly different in Hg
78 concentration from unused membrane material, indicating that breakthrough was not a
79 phenomenon that extended past the second ion exchange filter position.

80 The particulate Hg artifact problem was subsequently elaborated on in a further comparative
81 study focusing exclusively on RM measurement techniques (Sheu and Mason, 2001). Specific
82 concerns included physical particle breakthrough, re-evolution of gas-phase Hg^{2+} from PBM
83 captured on the upstream particulate filters passing downstream to the ion exchange membranes,
84 possible adsorption of GOM compounds to the particulate filters, or a GEM collection artifact on
85 the ion exchange membranes. None of these concerns were proven or disproven conclusively.

86 Recent CEM based sampling systems typically deploy a pair of CEM disc filters without a pre-
87 particulate filter, in replicates of 2 to 3 at a flow rate of 1.0 Lpm (Gustin et al., 2016). Each pair
88 of filters constitutes one sample, the first filter serving as the primary RM collection surface, and
89 the second filter capturing breakthrough. Filters are deployed for 1 to 2 weeks and then collected
90 for analysis (Huang et al., 2017). The CEM material consists of a negatively charged
91 polyethersulfone coated matrix (Pall Corporation), and at least one manufacturing evolution has
92 occurred (Huang and Gustin, 2015b). Prior CEM material versions (I.C.E. 450) had a pore size
93 of 0.45 μm , while the current CEM material (Mustang[®] S) has a manufacturer reported pore size
94 of 0.8 μm .

95 Previous work with the I.C.E 450 material indicated it does not adsorb significant quantities of
96 GEM in passive exposures, but selectively uptakes gas-phase Hg^{2+} species (Lyman et al., 2007).
97 The CEM material was subsequently adapted for use in active sample flow systems, with the
98 presumption of continued inertness to GEM and selectivity for GOM (Huang and Gustin, 2015a;
99 Huang et al., 2013). These studies and others (Lyman et al., 2016) have shown better GOM
100 recovery on CEM material compared to potassium chloride (KCl) coated denuder methods.

101 Despite these tests, the transparency of the CEM material to GEM uptake has not been
102 conclusively demonstrated for active sampling flow rates, nor for high GEM concentrations,
103 though limited data using low concentration manual Hg^0 injections through CEM filters suggests
104 little or no GEM uptake (Lyman et al., 2016). However, even small rates of GEM uptake by the
105 CEM material could result in a significant measurement artifact (e.g. a modest 1 to 2% GEM
106 uptake could easily overwhelm detection of typical ambient GOM concentrations). It is therefore
107 important that a GEM artifact be ruled out if the CEM material is to be successfully deployed for
108 ambient RM measurements.

109 Additionally, previous studies observed significant amounts of “breakthrough” GOM on the
110 secondary filter. The amount of breakthrough is not consistent, neither as a constant mass, with
111 total Hg ranging from zero to as high as 400 pg (Huang et al., 2017), nor as a percentage of Hg
112 collected on the primary filter, ranging from 0 to 40% (Pierce and Gustin, 2017). Similar variable
113 breakthrough issues were observed in the earliest field-based CEM measurements as well
114 (Mason et al., 1997). In contrast to ambient measurements, previous laboratory experiments have
115 reported only minor (0 to 16%) or no breakthrough (Huang and Gustin, 2015a; Huang et al.,
116 2013). Limited experimental work with flow rates of 1.0 and 16.7 Lpm in ambient air could not
117 provide an explanation for differing breakthrough rates (Pierce and Gustin, 2017).

118 In this research we investigated the potential for GEM uptake on CEM material using a custom-
119 built permeation system. Tests were done to investigate the ability of a pyrolyzer to convert
120 GEM to GOM. In addition, the ability of the CEM material to capture and retain a
121 representative GOM compound (mercury(II) bromide, HgBr_2) was explored, and the collection
122 efficiency for this compound was estimated. W~~we~~ attempted to explain or rule out possible
123 mechanisms of RM breakthrough for both dry and humid conditions.

124

125 2 Methods

126 2.1 System for sampling configuration

127 A Tekran[®] 2537A ambient mercury analyzer was integrated with a custom-built permeation
128 system designed to enable controlled exposures of GEM and GOM to CEM filters (Fig. 1). The
129 2537A analyzer was calibrated at the beginning and periodically throughout the study and
130 checked for accuracy by manual Hg^0 injections (mean recovery $101.1\% \pm 4.3$, $n = 10$, SI Fig. 1).
131 The entire system was checked for Hg contamination in clean air prior to permeation tests, and
132 periodically during sampling (SI Fig. ~~1~~2). See SI for additional information on Tekran quality
133 control. All tubing and connections used in the permeation system were polytetrafluoroethylene
134 (PTFE), except for the quartz glass pyrolyzer tube and perfluoroalkoxy (PFA) filter holders.
135 Given its reactive nature, some GOM inevitably adsorbs to internal line surfaces, but the capacity
136 of these materials to sorb and retain GOM is not infinite and a steady state of
137 adsorption/desorption is expected after 5-6 hours of exposure to a stable concentration (Xiao et
138 al., 1997; Gustin et al., 2013).

139 Sample flow through the system was alternated between two PTFE sample lines (designated
140 Line 0 and Line 1) using a Tekran[®] Automated Dual Switching (TADS) unit. Sample air was
141 constantly pulled through each line at 1.0 Lpm by the internal pump and mass flow controller
142 (MFC) in the 2537A, or by an external flush pump (KNF Laboport[®] N86 KNP) and MFC (Sierra
143 Smart-Trak[®] 2). Laboratory air was pulled through a single inlet at the combined rate of 2.0
144 Lpm, passing through a 0.2 µm PTFE particulate filter and an activated charcoal scrubber
145 (granular activated carbon 6-12 mesh, FisherChemical[®]) to produce clean sample air.
146 Additionally, for dry air permeations sample air was pulled through a Tekran[®] 1102 Air Dryer
147 installed upstream of the particulate filter, and for elevated humidity permeations sample air was
148 pulled through the headspace of a distilled water bath (DIW, < 0.2 ng L⁻¹ total Hg) that was
149 located upstream from the charcoal scrubber to eliminate the DIW being a potential Hg source to
150 the system. Temperature and relative humidity (RH) were measured in-line (Campbell Scientific
151 CS215) and used for calculation of absolute humidity.

152 Pure liquid Hg⁰ and crystalline HgBr₂ (purity > 99.998% Sigma-Aldrich[®]) were used as Hg
153 vapor sources. The elemental Hg⁰ bead was contained in a PTFE vial. Solid HgBr₂ crystals were
154 packed in thin-walled PTFE heat-shrink tubing (O.D. 0.635 cm) with solid Teflon plugs in both
155 ends to create a permeation tube with an active permeation length of 2 mm (Huang et al., 2013).
156 The HgBr₂ permeation tube was also placed in the bottom of a PTFE vial, and the permeation
157 vials were submerged in a temperature-controlled laboratory chiller (0.06 ± 0.13 °C, Cole Parmer
158 Polystat[®]). A low source temperature was favored, because higher temperatures would have
159 produced unacceptably high concentrations, and there is evidence that at higher temperatures a
160 small amount of Hg⁰ can be evolved from Hg²⁺ compounds (Xiao et al., 1997).

161 An ultra-high purity nitrogen (N₂) carrier gas was passed through the permeation vials at 0.2
162 Lpm to carry the target Hg vapor into the main sample line through a PTFE T-junction. The main
163 sample line was split into Line 0 and Line 1 immediately downstream from the permeation flow
164 junction, with flow on each line controlled by MFC. Line 0 proceeded directly to the 2537A
165 without modification during GEM permeations (Fig. 1A), but housed CEM filters during the
166 HgBr₂ permeations (Fig. 1B, 1C). Line 1 contained an in-line pyrolyzer unit. The goal of the
167 pyrolyzer was to convert all Hg to GEM for detection on the Tekran[®] 2537A.

168 **2.2 Pyrolyzer**

169 The pyrolyzer used in the study (SI Fig. 3) consisted of a 25.4 cm long quartz glass tube of 0.625
170 cm diameter (custom, URG Corporation). A loosely packed 3 cm section of quartz wool was
171 lodged in the mid-section of the tube, and this 3 cm section was wrapped with 22 gauge
172 Nichrome wire (18 loops). The quartz tube was closely contained within 2.5 cm thick quartz
173 fiber insulation within a 1.6 mm aluminum casing, except for an enclosed air space around the
174 heated Nichrome coil section. The coil wire was connected to 16 AWG stranded copper wire
175 with all metal disconnects that were buried within the quartz fiber insulation to reduce thermal
176 fatigue on the connections. The copper wire insulation was stripped and replaced with higher
177 temperature heat-shrink insulation where the wiring passed through the pyrolyzer case to the
178 external power supply. The tip of a 150 mm long K-type thermocouple (Auber WRNK-191) was
179 inserted through the insulation into the heated air space next to the coil to provide a temperature
180 feedback for a PID controller (Auber SYL-1512A). Power to the Nichrome coil was supplied by
181 a 12 VDC transformer through a solid-state relay (Auber MGR-1D4825) switched by the PID
182 controller. It was found that the position of the feedback thermocouple in the airspace outside of
183 the heating coil caused a large discrepancy between nominal temperature setpoint and actual

184 temperature inside the heated section of pyrolyzer tube. In general, much higher temperatures are
185 achieved inside the coil than outside. To compensate for this, actual temperature at the heated
186 coil section was verified to 600°C by external IR sensor and internal thermocouple probe.

187 To test if higher pyrolyzer temperatures converted more GOM to GEM for detection by the
188 Tekran 2537, the pyrolyzer temperature was increased to 650, 800, and 1,000°C (SI Fig. 4).

189 Pyrolyzer temperatures were measured by placing a thermocouple inside the pyrolyzer. GOM
190 concentrations measured as GEM by the Tekran 2537A increased at 600 and 800°C relative to
191 375°C. There was no significant difference between the amount of mercury concentrations in the
192 downstream Tekran 2537A when the pyrolyzer was at 600 and 800°C C (*t-test, p = 0.08*),
193 indicating that the increased pyrolyzer temperature did not convert more GOM to GEM.

194 However, when the pyrolyzer temperature was increased to 1000 °C, significantly more mercury
195 was measured by the downstream Tekran 2537A relative to when the pyrolyzer was at 650°C (*t-*
196 *test, p = 0.00*), indicating that the higher temperature was more efficient at converting GOM to
197 GEM; however, the pyrolyzer design could not sustain the 1000 °C temperature and was deemed
198 unsafe to use in the experimental permeation system. Thus, all experiments were performed with
199 a pyrolyzer temperature of 600°C.

200 The residence time in the pyrolyzer tube was approximately 1.5 seconds. Quartz wool was added
201 to increase the amount of surface area available to facilitate reactions and maximize the amount
202 of GOM converted to GEM in the pyrolyzer. Based on supplemental experiments, the
203 downstream Tekran® 2537A Hg measurements when the pyrolyzer was at 650 °C was 75%
204 compared to the measurements when the pyrolyzer was at 1000 °C (SI Fig. 4), indicating a
205 higher GOM to GEM conversion efficiency with higher pyrolyzer temperatures. Though this
206 conversion efficiency value does not describe the exact inefficiency of the experimental system

207 in this study, it provides an estimate for the efficiency of the pyrolyzer design in this study.

208 ~~Because of the conversion rate (discussed below), this is a pretty efficient method for converting~~

209 ~~GOM to GEM.~~ Having an efficient pyrolyzer provides us with a means of constraining

210 permeation tube permeation rates.

211 **2.3 Sample deployment**

212 CEM filters were deployed in 2-stage, 47 mm disc PFA filter holders (Savillex[®]). The primary

213 “A” filter in the 2-stage holder is the first to be exposed to the permeated Hg, with the secondary

214 “B” filter mounted immediately behind the A filter (A to B distance ~ 3mm) to measure potential

215 breakthrough. For GEM permeations, three 2-stage filter holders were placed in-series on Line 1

216 behind the pyrolyzer unit (Fig. 1A), while total Hg coming through the system was measured on

217 Line 0 with no filters in place. This allowed simultaneous exposure of 6 CEM filters in one GEM

218 sample exposure. The first CEM filter in-line served to scrub any small residual RM passing

219 through the system and pyrolyzer, and these first in-line filters were removed for the calculations

220 of mean GEM uptake rate, (SI. 5 and discussion). A controlled experiment was also performed to

221 ensure that both Lines 0 and 1 were conducting comparable concentrations of mercury under the

222 experimental conditions. Two-stage filter packs were deployed with CEM filters in each line at

223 equal distances from the permeation tube. The membranes were deployed for the same amount

224 of time in triplicate and analyzed to quantify the amount of total mercury sorbed to the

225 membranes. The average % deviation between lines was 2.9%, with a maximum deviation of

226 5.4%. These results indicated that though there may be some difference in the amount of

227 mercury passing through Lines 0 and 1, the difference was relatively small.

228 For determining the potential for GOM breakthrough, two system configurations were used. In

229 the first configuration (Fig. 1B), the total Hg concentration of air that passed through the

230 pyrolyzer on Line 1 was measured without any filters, while Line 0 held one 2-stage CEM filter
231 pair for HgBr₂ loading. This configuration allowed for 10 min interval quantification of the
232 HgBr₂ permeation concentration through Line 1 using the 2537A, and comparison with total Hg
233 loading on the CEM filters on Line 0.

234 In the second configuration, replicate filters were concurrently loaded with HgBr₂ by placing 2-
235 stage CEM filter holders on both Line 0 and Line 1 (upstream of the pyrolyzer, Fig. 1C). In all
236 HgBr₂ exposures, the filter holders were placed as close to the permeation vial as possible, with a
237 total distance from vial to filter surface of approximately 20 cm. Mercury bromide permeation
238 was conducted in dry air and elevated humidity air. The difference between one line being fully
239 open to the HgBr₂ permeation flow (configuration Fig. 1B) and then closed by deployment of the
240 CEM filters (configuration Fig. 1C) enabled a rough determination of the amount of HgBr₂ line-
241 loss within the system.

242 **2.4 Analyses of cation exchange membranes**

243 After permeation, CEM filters were collected into clean, sterile polypropylene vials and analyzed
244 for total Hg by digestion in an oxidizing acid solution, reduction to Hg⁰, gold amalgamation, and
245 final quantification by cold vapor atomic fluorescence spectrometry (CVAFS, EPA Method
246 1631, Rev. E) using a Tekran[®] 2600 system. The system background Hg signal was determined
247 for every analytical run by analyzing pure reagent solution in the same vials and at the same
248 volume as used for actual filter samples. Total Hg standards (5 to 100 ppb) were analyzed before
249 and after each batch of 10 filter samples to check precision and recovery, and the mean recovery
250 for all Hg standards was 97.2 ± 5.0 % (n = 37). Analysis for total Hg on the CEM filters
251 provided for comparison of total Hg filter loading, and verification of in-line results. A to B filter

252 breakthrough was calculated by comparison of total Hg recoveries on the primary and secondary
253 CEM filters, using Eq. (1):

$$254 \quad \% \text{ Breakthrough} = 100 * CEM_{2nd} / (CEM_{1st} + CEM_{2nd}) \quad (1)$$

255 Blank CEM filters were collected and analyzed in the same manner with every set of sample
256 filters deployed on the permeation system, and the overall mean filter blank value was subtracted
257 from all total Hg values to calculate the final blank-corrected Hg values used for data analysis.
258 All data were analyzed in Microsoft[®] Excel (version 16.12) and RStudio[®] (version 3.2.2).

259

260 **3 Results**

261 **3.1 Elemental Mercury Uptake on CEM Filters**

262 Elemental Hg uptake on CEM material was negligible for permeated Hg⁰ vapor concentrations
263 ranging from 1.43×10⁶ to 1.85×10⁶ pg m⁻³ (Fig. 2). High GEM concentrations were employed in
264 this study under the logic that if no GEM uptake was observed at high concentrations, a similar
265 lack of GEM uptake can be expected for lower concentrations.

266 The mean Hg mass on blank CEM filters was 50 ± 20 pg (n = 28). For permeations into dry
267 sample air of 0.5 ± 0.1 g m⁻³ water vapor (WV), total mean Hg⁰ permeation exposures of 2.7×10⁶
268 pg (24 h) and 7.3×10⁶ pg (72 h) resulted in total (blank-corrected) Hg recoveries on the CEM
269 filters of 100 ± 40 pg (n = 10) and 280 ± 110 pg (n = 5), respectively. These quantities of total
270 recovered Hg equate to a mean GEM uptake rate on the CEM filters of 0.004 ± 0.002% (0.006 ±
271 0.006% including first in-line filter). For GEM permeations into ambient humidity sample air (2
272 to 4 g m⁻³ WV), at a slightly lower total mean permeated Hg⁰ 24 h exposure of 2.1×10⁶ pg, total

273 (blank-corrected) Hg recoveries on the CEM filters were 55 ± 30 pg ($n = 10$), equating to a GEM
274 uptake rate of $0.003 \pm 0.001\%$ ($0.005 \pm 0.005\%$ including first in-line filter).

275 The first CEM filter in-line during the GEM permeations always showed more total Hg than the
276 following 5 downstream filters, ~~which that~~ were not significantly different from each other (SI
277 Fig. 5). It is unlikely that the Hg observed on the first CEM filters resulted from GEM uptake.
278 Even at the highest GEM permeation rate, the first filter captured only ~ 1700 pg of Hg, out of a
279 total permeated amount of over 7.3 million pg (a 0.02% uptake rate). This means that the
280 downstream CEM filters were still exposed to about 7.2985 million pg of GEM but captured less
281 total Hg. As we cannot entirely rule out the possibility of some small rate of *in-situ* oxidation of
282 GEM in the system, at the surface of the Hg^0 bead or in the vapor phase, the first in-line filters
283 were not included in the calculation of GEM uptake rates because of suspicion that some
284 component of the Hg captured on the first filter was GOM. ~~Inclusion or removal of the first in-~~
285 ~~line filters did not significantly alter calculations.~~

286 The overall GEM uptake rate was linear ($r^2 = 0.9769$, $p = 0.0004$; SI Fig. 5) for the range of
287 concentrations used in this study, indicating a similar low uptake rate can be expected down to
288 lower GEM concentrations. GEM uptake by first in-line filters was also linear ($r^2 = 0.92$, $p =$
289 0.00), though these results are based on 5 data points. Exponential models poorly fit the
290 experimental data for both the overall GEM uptake and uptake by first in-line filters (SI Fig. 5).

291 3.2 Mercury Bromide Uptake on CEM Filters

292 Breakthrough of HgBr_2 vapor from the primary (A) to secondary (B) CEM filters was low for all
293 conditions tested in this study (Table 1). These conditions included HgBr_2 permeated into clean
294 dry laboratory air with < 0.5 g m^{-3} WV, clean air at ambient room humidity (4 to 5 g m^{-3} WV),

295 and clean air at elevated humidity (10 to 11 g m⁻³ WV), at line temperatures between 17 to 19
296 °C. Overall, the mean A to B filter breakthrough ranged from 0 to 0.5%, and averaged 0.2 ± 0.2
297 % (n = 17), with no statistical difference observed in mean breakthrough rates for the three levels
298 of humidity (ANOVA, p = 0.124).

299 The first HgBr₂ permeation in clean dry (< 0.5 g m⁻³ WV) laboratory air was over a 96 h period,
300 using the system configuration in Fig. 1B to establish an approximate permeation rate (Fig. 3).
301 Total Hg reaching the 2537A through the pyrolyzer on Line 1 (red line, Fig. 3) indicated an
302 average HgBr₂ exposure concentration of 4540 pg m⁻³, or about 4.5 pg min⁻¹ from the permeation
303 tube. This permeated concentration of HgBr₂ was deliberately much higher than ambient in order
304 to test retention and break through at high levels. It should be noted that these concentrations are
305 50 – 1000 times above background ambient concentrations and the performance of the CEM
306 filters at low concentrations could be slightly different. After this permeation, total blank-
307 corrected HgBr₂ loading on the primary CEM filter on Line 0 was 49400 pg, but only 50 pg on
308 the secondary CEM filter, indicating a breakthrough rate of approximately 0.1%. Total Hg
309 reaching the 2537A through the CEM filters on Line 0 (black line, Fig. 3) over this time period
310 was 15 pg, mostly at the beginning of the deployment when some ambient Hg entered the
311 opened system. The low concentrations of Hg measured downstream in Line 0 on the 2537A
312 corroborates that breakthrough of HgBr₂ was low. These data also demonstrate that the CEM
313 material did not saturate with a HgBr₂ loading of ~ 50000 pg, a loading far higher than could be
314 expected in ambient conditions.

315 Subsequent replicate 24 h HgBr₂ permeations in clean dry air resulted in consistent total Hg
316 loading on CEM filters placed on both lines concurrently (8560 ± 320 pg, n = 6, Samples 2-7
317 Table 1), and mean total Hg on the secondary CEM filters was 20 ± 10 pg (average

318 breakthrough of 0.3%). On Line 0 (black line, Fig.3), which was never open to HgBr₂ vapor
319 downstream from the CEM filters at any point in the study, Hg measured at the 2537A was zero
320 for all three 24 h permeations, indicating no breakthrough (Samples 2, 4, & 6, Table 1).

321 However, on Line 1, ~~which that~~ had been exposed to the full HgBr₂ vapor concentration of 4540
322 pg m⁻³ over the duration of the 96 h permeation test, 1155 pg of Hg were measured downstream
323 in the first 24 h sample (Sample 3, Table 1). The amount of downstream Hg dropped to 10 pg in
324 the second 24 h, and 6 pg in the third 24 h (Samples 5 & 7, Table 1). This downstream Hg in
325 Line 1 (compared to the zero Hg simultaneously observed on Line 0) is attributed to
326 volatilization of HgBr₂ that had adsorbed to the line material during the open permeation flow.
327 At the moment CEM filters were deployed on Line 1 (red-to-blue transition, Fig. 3), a rapid
328 asymptotic decline in the Hg signal began. This decay curve supports drawdown and depletion of
329 a Hg reservoir on the interior line surfaces behind the CEM filters, and not a continuous source
330 such as breakthrough from the permeation tube that was still supplying HgBr₂ to both sample
331 lines. The total mass of Hg volatilized from the interior line surfaces (1155 pg) represents 4 to 5%
332 of the total HgBr₂ that had passed through Line 1 (~25000 pg based on 2537A measurement).
333 Eventually, Hg reaching the 2537A through Line 1 decreased to zero during the same 24 h filter
334 deployment, indicating the majority of HgBr₂ line contamination in a high-concentration
335 permeation system can be expected to flush out within ~12 h. However, we caution that
336 materials used in high-concentration permeation systems, despite being flushed out, should not
337 be used for background ambient air work without at least a very thorough acid cleaning.

338 Additional HgBr₂ permeations were made at two levels of in-line humidity. At ambient room
339 humidity (4 to 5 g m⁻³ WV), mean total Hg measured on the CEM filters was 7910 ± 520 pg (n =
340 4; Samples H2-5, Table 1), with an average breakthrough to the secondary filters of 0.3%. When

341 normalized for sample volume, the mean HgBr₂ loading on CEM filters during ambient humidity
342 (5968 ± 125 pg) and dry air (5995 ± 188 pg) permeations was not statistically significantly
343 different (t-test $p = 0.790$). HgBr₂ breakthrough rates were also the same (0.3%) as during the
344 dry air permeations, indicating that the permeation system was operating similarly at the two
345 humidity levels, and suggesting that absolute humidity concentrations of 4 to 5 g m⁻³ WV had
346 insignificant effects on collection of HgBr₂ in clean laboratory air by the CEM material.

347 An increase in humidity resulted in an initial large increase in Hg measured at the 2537A
348 downstream of the CEM filters on Line 0 (Sample H1, Table 1), concurrently with an open
349 HgBr₂ permeation flow through Line 1 while both lines were subjected to increased RH. This
350 downstream Hg on Line 0 dropped substantially to zero in ~10 h in the first 24 h deployment
351 (Sample H2, Table 1), and was zero for the duration of the second 24 h deployment (Sample H4,
352 Table 1). Hg rapidly declined to zero, due to off-gassing from the tubing induced by the
353 increased humidity, which facilitated a heterogeneous surface reduction of HgBr₂ to GEM in the
354 short section of line between the permeation source and CEM filters. This phenomenon was also
355 observed during the Reno Atmospheric Mercury Intercomparison eXperiment (RAMIX; Gustin
356 et al., 2013). Reduced HgBr₂ then then passed through to the 2537A as GEM. As the
357 breakthrough rate and the mean HgBr₂ loading on the CEM filters did not change between the
358 dry air and ambient humidity permeations, the downstream Hg observed at the 2537A during the
359 ambient humidity permeations cannot be attributed to a loss of Hg from the CEM filters and is
360 more likely due to a process in the sample lines.

361 As a further test of possible humidity effects, two replicate 24 h CEM filter deployments were
362 conducted in elevated humidity conditions (10 to 11 g m⁻³ WV) created by an in-line water bath.
363 Mean total Hg loading on the primary CEM filters was higher compared to the previous

364 permeations (11700 ± 720 pg, $n = 4$, Samples H9-12, Table 1), indicating an increase in the
365 effective HgBr₂ permeation rate, possibly due to the perturbation caused by a poor filter seal and
366 small leak in the preceding deployment (Sample H7-8, Table 1). However, mean total Hg on the
367 secondary CEM filters was 20 ± 20 pg, indicating an average breakthrough of 0.1%, less than the
368 breakthrough observed for the lower humidity permeations.

369

370 4 Conclusions

371 GEM uptake on the CEM material was negligible under the laboratory conditions and high GEM
372 loading rates (3 orders of magnitude above ambient) tested in this study, with an overall linear
373 uptake rate of 0.004% (SI Fig. 5). This uptake rate would be insignificant at typical ambient
374 atmospheric Hg concentrations (1 to 2 ng m⁻³). As a hypothetical example, a CEM filter
375 sampling ambient air at an average GEM concentration of 2 ng m⁻³ for a typical 2-week sample
376 period would have a total Hg⁰ exposure of ~ 40000 pg. At the calculated uptake rate of 0.004%, a
377 maximum 1.6 pg of Hg observed on the sample filter could be attributed to GEM artifact. ~~Given~~
378 ~~that blank filters have a mean total Hg mass of 50 ± 20 pg, this amount would be below the~~
379 ~~detection limit~~ Although further work is required to more definitively determine detection and
380 quantification limits of the various CEM methodologies, based on the mean total Hg mass of 50
381 ± 20 pg observed in this study, the artifact of GEM uptake ~~to~~by the CEMs would be below the
382 detection limit observed here. This corroborates the lack of GEM uptake seen by Lyman et al.
383 (2016) for manual Hg⁰ injections on CEM filters at lower total mass loadings of 300 to 6000 pg.

384 Mean HgBr₂ breakthrough from primary to secondary CEM filters averaged $0.2 \pm 0.2\%$ over all
385 test conditions. A to B filter breakthrough was derived from a comparison between the large

386 amount of HgBr₂ permeated onto the primary CEM filters, to the small amount of HgBr₂ that
387 collected on the secondary CEM filters, 3 mm immediately downstream. The measurement of
388 1000s of pg of Hg on the primary filter, and only 10s of pg on the secondary filter, leads to the
389 conclusion that the primary filter removed the majority of HgBr₂ from the sample air stream
390 under laboratory conditions applied in this study. In addition, low breakthrough was corroborated
391 by downstream measurement of the air stream passing through the CEM filters, using the
392 Tekran[®] 2537A. The average breakthrough to the 2537A was 0 pg for 24 h permeations in dry
393 air, and 0 to 40 pg in humid air, for filter deployments at steady-state (> 24 h without large
394 perturbations).

395 While the permeation system was not specifically optimized for a quantitative mass balance
396 between permeated HgBr₂ and HgBr₂ recovered on the CEM filters, a rough estimation of the
397 CEM collection efficiency is possible. Using the HgBr₂ permeations conducted in clean dry air
398 (mean loading 8560 pg) and comparing this to the mean Hg concentration measured at the
399 2537A analyzer during the last 24 h of the 96 h permeation measurement (4680 pg m⁻³ or 6739
400 pg per 24 h), HgBr₂ recovery on the CEM filters averaged 127%. Adjusting the expected
401 permeated HgBr₂ mass for our estimated line-loss (~4-5%) changed the recoveries to ~123%.
402 Still, HgBr₂ loading on the CEM filters was ~23% higher than expected based on the pyrolyzed
403 total measurement on the 2537A, indicating not all HgBr₂ was converted to GEM. This can be
404 explained by the pyrolyzer design used in this study not being 100% efficient at thermally
405 reducing HgBr₂ to Hg⁰, based on the higher total Hg recoveries on the CEM filters versus total
406 Hg measured through the pyrolyzer on the Tekran 2537.

407 The technique of gold amalgamation in general, and specifically including the Tekran[®] 2537A
408 analyzer, is widely considered to provide a quantitative total gaseous Hg measurement, at or very

409 near 100% collection efficiency for Hg⁰ and Hg compounds (Temme et al., 2003; Landis et al.,
410 2002; Schroeder et al, 1995; Dumarey et al., 1985; Schroeder and Jackson, 1985). However, to
411 our knowledge collection and desorption efficiencies on gold traps have not been demonstrated
412 for HgBr₂. The stated desorption temperature of the Tekran[®] 2537A gold traps is 500 °C, but
413 temperatures as low as 375 °C have been reported (Gustin et al., 2013). This would cause
414 reduced thermal decomposition efficiency for all captured GOM compounds, including HgBr₂.
415 We speculate that a combination of incomplete thermal decomposition to Hg⁰ at both the 600 °C
416 pyrolyzer and during the best-case 500 °C desorption of the 2537A gold traps contributed to the
417 ~20% non-detection of total permeated HgBr₂ as it passed through the CVAFS optical path.
418 Evidence for this conclusion can be seen in the 134% increase in Hg collection by the Tekran[®]
419 2537A when the pyrolyzer was at 1000 °C, as compared to at 650 °C (SI Fig. 4), in
420 supplementary experiments.

421 While our results validated some basic performance metrics for the CEM material, they did not
422 provide data that could fully explain the higher levels of breakthrough observed for CEM filters
423 deployed in ambient air over the 1-to-2 week sample periods in previous studies. Increasing
424 humidity by itself did not affect observed HgBr₂ breakthrough. A HgBr₂ loading of ~50000 pg
425 also did not lead to increased breakthrough, indicating there is no saturation effect on CEM filter
426 capacity at a GOM loading far greater than expected from ambient concentrations. It remains
427 unclear, though, whether breakthrough results from different collection efficiencies for GOM
428 compounds other than HgBr₂, or whether breakthrough results from a degradation of GOM
429 retention capacity in the CEM material when exposed to ambient air chemistries not simulated in
430 this study. Also, our experiments were conducted in particulate-free air, which leaves open the
431 possibility that breakthrough is related to capture (or lack thereof) of PBM by the CEM material.

432 Further testing and refinements are necessary, beginning with optimization of the pyrolyzer
433 parameters (e.g., temperature, volume) to allow for a more accurate quantitative comparisons
434 between the CEM and Tekran[®] 2537A results. Permeation rates of HgBr₂ were variable and need
435 to be more precisely controlled, a standardized and stable GOM permeation system being needed
436 in general. This study was undertaken using controlled laboratory conditions, but CEM
437 performance needs to be further validated in ambient air. Specifically, the reasons for RM
438 breaking through CEM filters deployed in ambient air still need to be determined.

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446

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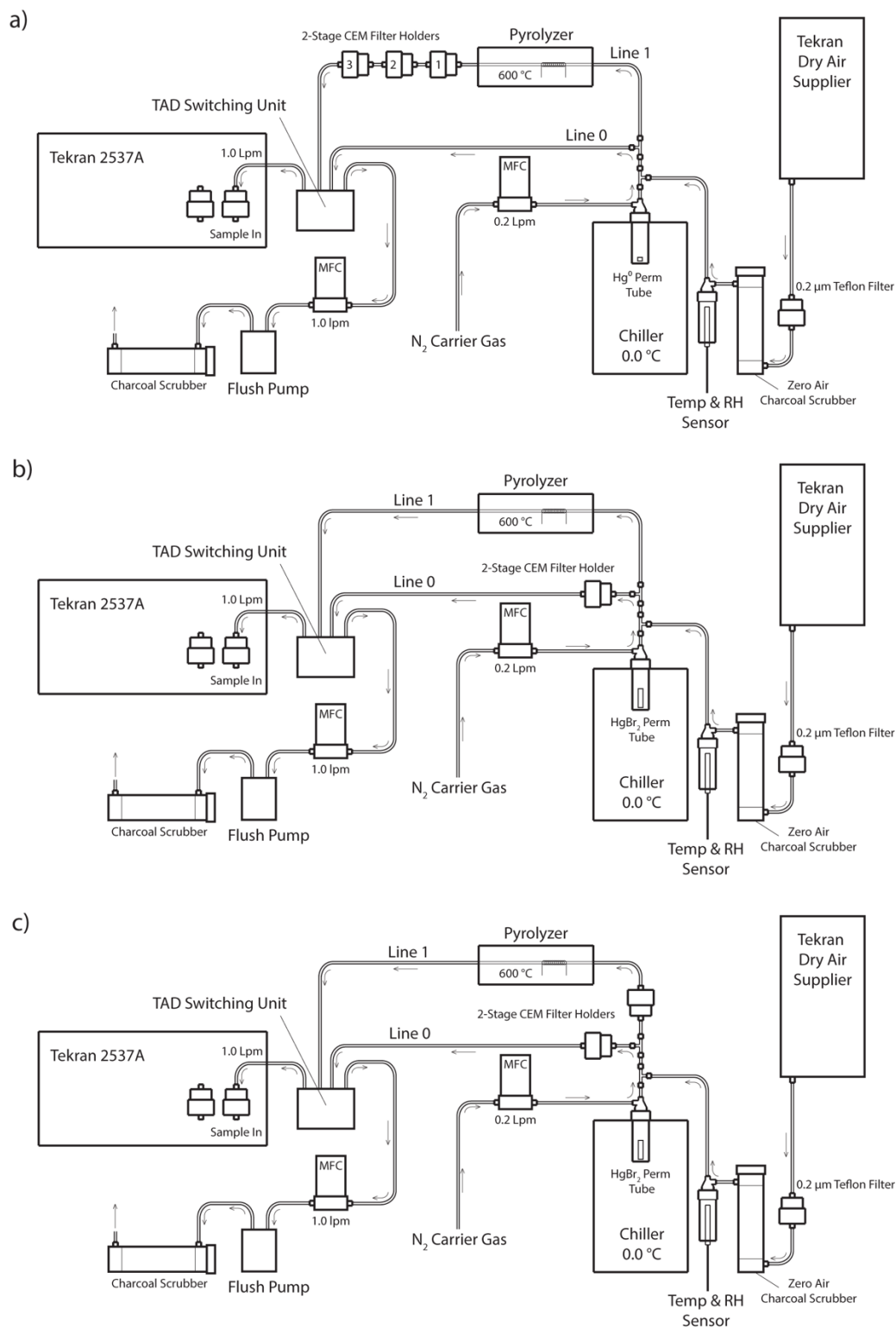
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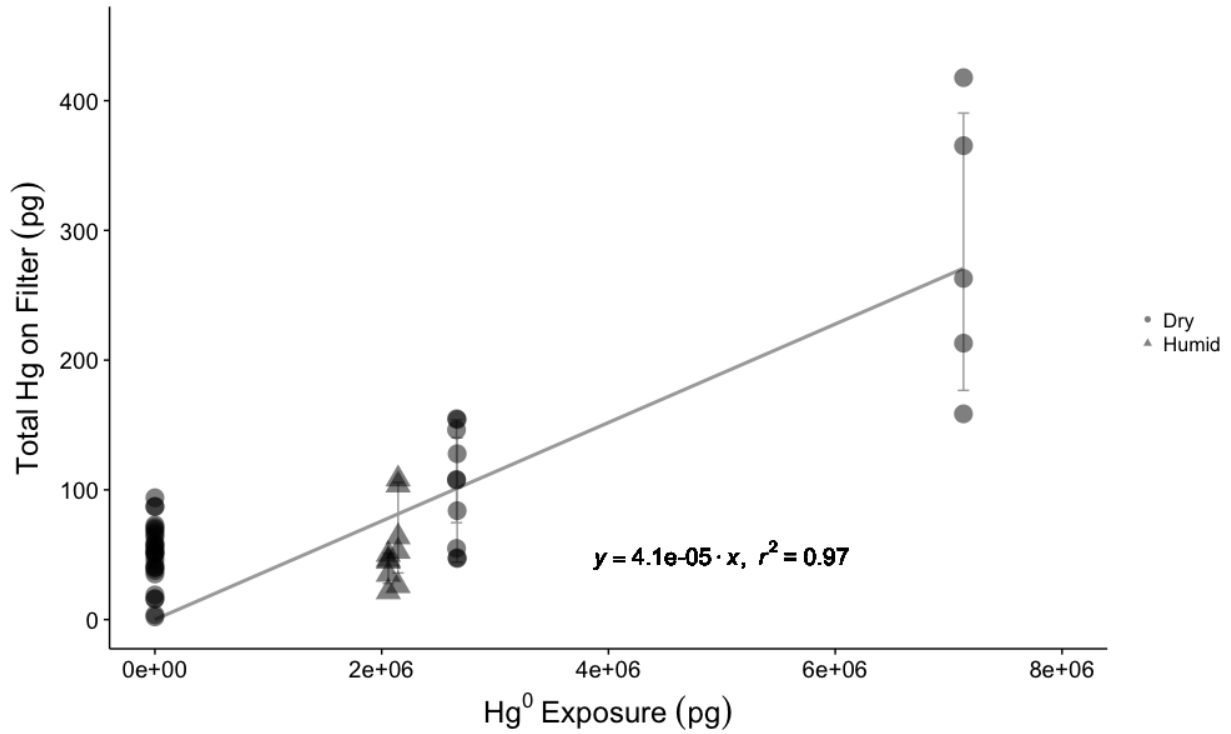
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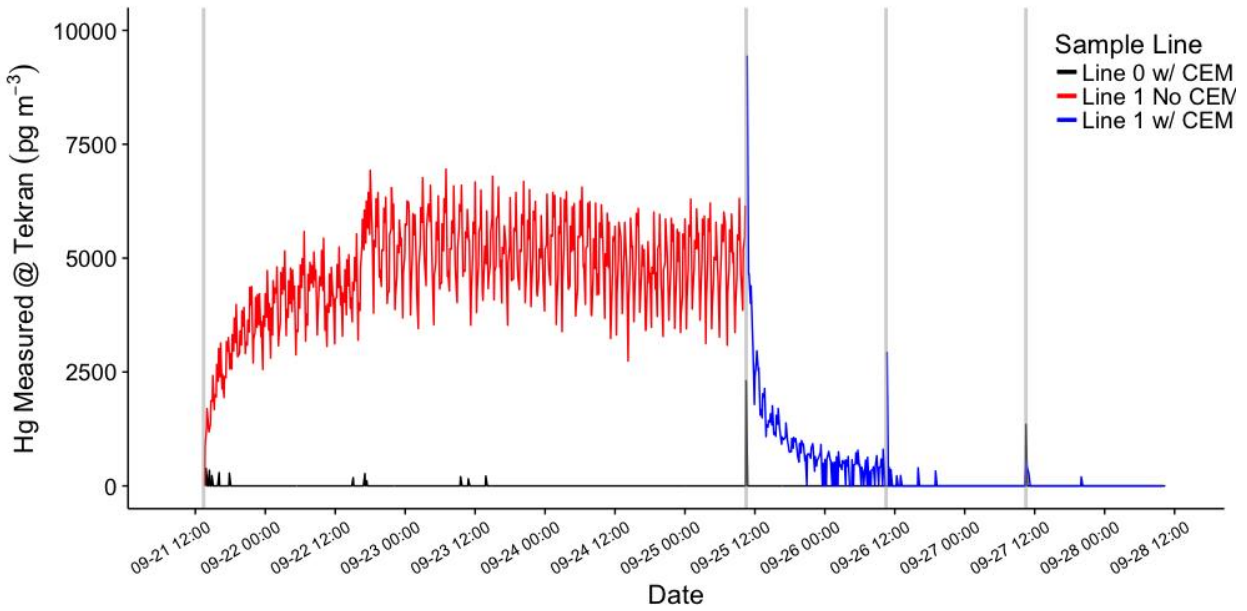
542 **Figure 1.** Schematic of the Hg vapor permeation system configurations for: a) GEM permeations b) HgBr₂
 543 permeations c) Simultaneous HgBr₂ loading on two sample lines. Note dry air supplier disconnected for ambient and
 544 elevated humidity HgBr₂ permeations, with sample path starting at 0.2 μm Teflon particulate filter and water bath
 545 inserted immediately in front of the charcoal scrubber. All tubing is PTFE, except for the quartz glass pyrolyzer tube
 546 and PFA filter holders.



547

548 **Figure 2.** Total Hg recovered on CEM material for blank filters (Hg exposure = 0 pg) and different Hg⁰ vapor
 549 permeations in dry ($0.5 \pm 0.1 \text{ g m}^{-3} \text{ WV}$) and humid air ($2\text{-}4 \text{ g m}^{-3} \text{ WV}$). Circles represent dry air permeations,
 550 triangles represent humid air exposures, and all permeation exposures were blank-corrected. The regression line
 551 shows the relationship between total Hg⁰ exposure and blank-correct mean total Hg recovered on CEM filters (error
 552 bars \pm one standard deviation), with a slope of 4.1×10^{-5} indicating a linear uptake rate of 0.004%.

553



554
 555 **Figure 3.** HgBr₂ permeations in clean dry lab air using the configuration in Figure 1B (red line) and Figure 1C (blue
 556 line). The red line indicates total Hg released from permeation tube and passing through pyrolyzer on Line 1 before
 557 being measured by Tekran 2537A, black line indicates Hg reaching 2537A through CEM filters on Line 0. Vertical
 558 grey lines indicate open system during filter deployments.

559

Table 1.

Sample	Start	End	Sample Time (min)	Sample Flow (lpm)	Sample Volume (m ³)	Total Hg on CEM (pg)	Blank Correct (pg)	Total Hg @ Tekran (pg)	A to B Filter Brkthru (%)
Mean CEM Filter Blank							54		
Clean Dry Air (0.3 ± 0.05 g m⁻³ wv)									
<i>HgBr 1P</i>	9/21/17 13:25	9/25/17 10:25	5580	1.00	5.580	<i>na</i>	<i>na</i>	25181	<i>na</i>
HgBr 1A	9/21/17 13:25	9/25/17 10:25	5580	1.00	5.580	49478	49424	15	0.10
HgBr 1B						101	47		
HgBr 2A	9/25/17 10:30	9/26/17 10:30	1440	1.00	1.440	8901	8847	0	0.20
HgBr 2B						71	17		
<i>HgBr 3A</i>	9/25/17 10:30	9/26/17 10:30	1440	1.00	1.440	9125	9072	1155	0.36
<i>HgBr 3B</i>						86	33		
HgBr 4A	9/26/17 10:40	9/27/17 10:25	1425	1.00	1.425	8494	8440	0	0.28
HgBr 4B						77	24		
<i>HgBr 5A</i>	9/26/17 10:40	9/27/17 10:25	1425	1.00	1.425	8306	8253	10	0.36
<i>HgBr 5B</i>						83	29		
HgBr 6A	9/27/17 10:35	9/28/17 10:25	1430	1.00	1.430	8496	8442	0	0.22
HgBr 6B						72	19		
<i>HgBr 7A</i>	9/27/17 10:35	9/28/17 10:05	1410	1.00	1.410	8386	8333	6	0.15
<i>HgBr 7B</i>						66	13		
Clean Humid Air (4.4 ± .2 g m⁻³ wv)									
<i>HgBr H1P</i>	10/2/17 16:10	10/3/17 15:20	1390	1.00	1.390	<i>na</i>	<i>na</i>	5888	<i>na</i>
HgBr H1A	10/2/17 16:10	10/3/17 15:20	1390	1.00	1.390	10498	10444	1700	0.25
HgBr H1B						80	27		
HgBr H2A	10/3/17 15:30	10/4/17 14:40	1390	1.00	1.390	8589	8535	164	0.13
HgBr H2B						65	11		
<i>HgBr H3A</i>	10/3/17 15:30	10/4/17 14:40	1390	1.00	1.390	8182	8129	420	0.54
<i>HgBr H3B</i>						98	44		
HgBr H4A	10/4/17 14:50	10/5/17 11:50	1260	1.00	1.260	7504	7451	0	0.31
HgBr H4B						76	23		
<i>HgBr H5A</i>	10/4/17 14:50	10/5/17 11:50	1260	1.00	1.260	7576	7522	25	0.25
<i>HgBr H5B</i>						73	19		
<i>HgBr H6P</i>	10/5/17 12:05	10/9/17 10:25	5660	1.00	5.660	<i>na</i>	<i>na</i>	11889	<i>na</i>
HgBr H7A	10/9/17 10:40	10/10/17 10:45	1445	1.00	1.445	9024	8970	105	<i>na</i>
HgBr H7B						2672*	2618*		
<i>HgBr H8A</i>	10/9/17 10:40	10/10/17 10:45	1445	1.00	1.445	12359	12305	397	<i>na</i>
<i>HgBr H8B</i>						75	21		
Clean High Humidity Air (10.9 ± 1.7 g m⁻³ wv)									
HgBr H9A	10/10/17 10:50	10/11/17 9:30	1360	1.00	1.360	10920	10866	181	0.22
HgBr H9B						78	24		
<i>HgBr H10A</i>	10/10/17 10:50	10/11/17 9:30	1360	1.00	1.360	11413	11359	308	0.00
<i>HgBr H10B</i>						53	0		
HgBr H11A	10/11/17 9:35	10/12/17 9:35	1440	1.00	1.440	12001	11947	5	0.00
HgBr H11B						52	0		
<i>HgBr H12A</i>	10/11/17 9:35	10/12/17 9:35	1440	1.00	1.440	12579	12525	40	0.29
<i>HgBr H12B</i>						90	36		
<i>HgBr H13P</i>	10/12/17 9:40	10/13/17 9:40	1440	1.00	1.440	<i>na</i>	<i>na</i>	1430	<i>na</i>
HgBr H13A	10/12/17 9:40	10/13/17 9:40	1440	1.00	1.440	13152	13099	4	0.12
HgBr H13B						69	16		

560

561 **Table 1.** Summary of CEM filter loading and breakthrough during HgBr₂ permeations. Samples denoted P indicate
562 approximate permeation rate check through Line 1 via pyrolyzer and Tekran 2537A, italicized text indicates filter
563 deployments on Line 1, and * indicates high values due to leak around first filter seal.