

Interactive comment on “Atmospheric bending effects in GNSS tomography” by Gregor Möller and Daniel Landskron

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We would like to thank referee #1 for his/her detailed comments on our manuscript. In the following, you will find our responses to each specific comment and technical correction addressed. Looking forward to your positive feedback. A revised version of the manuscript will follow.

Specific comment (1): I recommend to rewrite the 'Introduction'. The section 'Introduction' must be more general. In the 'Introduction' there is no need for technical details and formulas. Technical details and formulas must be provided in the following section (see next point). Instead, provide a brief overview on the state of the art in tomography. Provide some relevant references, e.g. Bender et al., 2011, Champollion et al., 2005,

C1

Hirahara, 2000, and their findings. In all the above mentioned works bending effects were ignored. Therefore you should then provide references where bending effects are taken into account. Here you should mention Zus et al (2015) (not cited in the manuscript) and a paper that appeared two years later Aghajany and Amerian (2017) (cited in the manuscript).

Author's response: According to the reviewer's suggestion, we will restructure the first section of the manuscript as follows: The technical details and formulas will be shifted to a new section '3 The principles of GNSS tomography'. A paragraph about achievements in GNSS tomography will be added and all references suggested by the reviewer will be mentioned in the revised version of the manuscript.

Specific comment (2): Section 1 ('Introduction') and 2 ('Atmospheric bending effects in GNSS signal processing') need a complete makeover. I suggest to merge the two sections to one section with the following title 'Atmospheric bending effects and WV tomography'. To my understanding you are concerned with SWDs and not STDs. In short, I recommend the following structure for this section: 2.1 Atmospheric bending effects Here you should at first introduce the basic observable, i.e., STDs. You can either use eq 2 or 10. They are essentially the same. I recommend to use eq 2. Hence, you start as follows: The STD is defined as (Bevis et al. 1992) $STD = \int n ds - g$ n...index of refraction s...arc length of bent ray-path (refer to section 3) g...geometric distance between satellite and station Then, you introduce refractivity N. In essence $n = 10^{(-6)} N + 1$ and therefore $STD = \int 10^{(-6)} N ds + s - g$ Then you introduce the hydrostatic and wet refractivity $N = N_h + N_w$ and therefore $STD = \int 10^{(-6)} N_h ds + s - g + \int 10^{(-6)} N_w ds$ Next, you introduce the following quantities $SHD = \int 10^{(-6)} N_h ds + s - g$ and $SWD = \int 10^{(-6)} N_w ds$ such that $STD = SHD + SWD$ At this point it is again important to mention that the ray-path (and therefore the arclength s) depends on the 'total' refractivity N (refer to section 3). Then you claim that the SWD can be accurately estimated with the GNSS. In essence, you introduce the assembled STD that is used in the GNSS analysis (eq 11) $STD_{GPS} = ZHD_{GPS}$

C2

* $mh(e) + ZWD_GPS * mw(e) + mg(e) (N \cos(a) + E \sin(a))$ and provide the formula that you use to recover the SWD. I can only guess (please provide the details) something like this $SWD_GPS = STD_GPS - ZHD_NWM * mh(e)$ or better yet something like this $SWD_GPS = STD_GPS - ZHD_NWM * mh(e) - mg(e) (N_h_NWM \cos(a) + E_h_NWM \sin(a))$ where ZHD_NWM is ZHD derived from a NWM (or derived from in situ pressure sensor) and N_h_NWM and E_h_NWM are the hydrostatic gradient components derived from a NWM. Here you can mention that the hydrostatic mf (which is derived under the assumption of a spherically layered troposphere) takes into account the geometric bending term. In essence, $mh = (\int 10^{**(-6)} N_h ds + s - g) / ZHD$ With this details you are finished with 2.1 and prepared for 2.2

2.2 WV tomography Since the observable you consider are SWDs, there is no need for eq 3 and 4. You can start directly with the following formula $SWD = \int 10^{**(-6)} N_w ds$ and its numerical approximation $SWD \approx \sum_i 10^{**(-6)} N_{w_i} ds_i$ where you again explicitly mention that, because of ray-path bending, s does not equal g (refer to section 3). Then you can proceed with your eq 6 and 7. It is important that you explain what P and P_c is. I guess (please provide the details) that P_c tells us something about the uncertainty of the observations and P tells us something about the uncertainty of the a-prior (first-guess or background) wet refractivity? With this you are finished with section 2 and proceed with your section 3.

Author's response: Thank you for your detailed suggestions. We agree that a restructure of the first two section can help to improve the understanding of our methods. In consequence, we will replace Eq. 10 by Eq. 2 and will derive the relations between STD, refractivity and bending from this equation in the way suggested by the reviewer. Since the focus of this paper lays on atmospheric bending effects, thereby we will not go into detail on how the SWD is obtained from GNSS signals but will show how and to what extend atmospheric bending is compensated in GNSS signal processing using the concept of mapping function - in particular for VMF1. Instead of section '2.2 WV tomography' the manuscript will be extended by a new section '3 The principles of GNSS

C3

tomography'. This will include the basic equations of tomography, presented in a consistent way to section '2 Atmospheric bending effects in GNSS signal processing'. In addition, we will add a more detailed explanation of the singular value decomposition and weighting method applied, as requested by reviewer 2.

Specific comment (3): I suggest that somewhere in the manuscript you plot the following difference $dSWD = SWD_T - SWD_0$ as a function of the elevation angle for some station. Here SWD_0 is the SWD calculated along the straight line path and SWD_T is the SWD calculated along the ray-path. In essence, $dSWD = \sum_i 10^{**(-6)} N_{w_i} ds_i - \sum_i 10^{**(-6)} N_{w_i} dg_i$ I guess you will find that the following inequality holds true for any elevation angle $SWD_0 > SWD_T$ due to the fact that the ray-path traverses the troposphere at higher altitudes than the straight line path. This would imply that when ray-path bending is not taken into account in tomography the reconstructed troposphere is too dry. To see this you could chose some 'true' wet refractivity field, say N_{w0} , and simply replace in your eq 7 the term $(SWD - A * N_{w0})$ by $dSWD$. I strongly recommend to do this somewhere in the manuscript.

Author's response: In Figure 6 of the manuscript we plotted the additional ray paths caused by straight-line assumption and discussed its impact on the tomography results. As highlighted by the reviewer, it will lead to a drying effect in the reconstructed refractivity field. To provide some numbers, we computed the differences in SWD ($dSWD = SWD_T - SWD_0$) and the corresponding paths lengths within the voxel model as suggested by the reviewer for the 6 GNSS sites mentioned in Table 1. Therefore, we made use of the ALARO model data as 'true refractivity field' and ray-traced all lines-of-sight to the GNSS satellites in view, in total 720 observations distributed over 8 epochs (0, 3, 6 ... UTC) on DoY 121, 2013. The resulting difference ($dSWD$) are always positive and up to 2.2 cm for ~5 degrees elevation angle. In addition, we computed the resulting drying effect in the refractivity field, which follows from the additional ray path: $dN1 = SWD_T[mm] * (ds_0 [km] - ds_T [km])$ In addition, we computed the drying effect, caused by the fact, that the straight-line traverses the troposphere at lower altitudes

C4

(assuming exponential decrease of N_w with height between the model layers) $dN2 = (SWD_T[\text{mm}] - SWD_0[\text{mm}]) * ds_0 [\text{km}]$ Both effects have to be taken into account when computing the drying effect in the reconstructed refractivity field obtained along the signal path if bending is not considered. Author's changes in manuscript: In the revised version of the manuscript we will plot the additional path lengths (Figure 6a) together with $dN1$ and $dN2$ as function of elevation angle (as Figure 6b and 6c) and will add a short description in the text how it was computed.

Technical corrections: Abstract L7: '...Thereby, the ray-tracing approach itself but primarily the quality of the a priori field has a significant impact on the reconstruction quality...' improve the writing.

Author's response: This part of the Abstract will be rewritten as follows: 'Thereby, not only the ray-tracing method but also the quality of the a priori field has a significant impact on the quality of the tomography retrievals.'

Introduction L15: 'GNSS' abbreviation not introduced here.

Author's response: Abbreviation 'GNSS' will be spelled out the first time when it is used in the manuscript as 'Global Navigation Satellite Systems'

Section 3.1 L18: The inner loop you use is to solve the so called 'homing in problem' (you make use of a shooting method). Please state this more clearly here.

Author's response: In the revised manuscript, we will modify section 3.1 L16 ff as follows: 'After setting the initial parameters, the 'true' ray path is reconstructed iteratively by making use of ray-tracing shooting techniques. Therefore, total refractivity derived from an a priori field is read in and pre-processed for ray-tracing. Hereby, the input data is interpolated vertically and horizontally to the vertical plane, spanned by the y- and z-axis. In the ray-tracing loop, for each height layer $h_{[i+1]}$ with $i=1:(t-1)$ where t defines the top layer of the voxel model, the geocentric coordinates and the corresponding angles are computed as follows: [..]

C5

Section 3.1 L24: What is the 'outgoing' elevation angle? Please provide a clear definition here.

Author's response: The outgoing elevation angle is determined through the straight-line geometry between the satellite and entry-point of the signal into the atmosphere. In the revised version of the manuscript, we will call it 'the vacuum elevation angle' with reference to Figure 1.

Section 3.2 L4: '...In consequence, the reconstructed...'. The phrase 'In consequence' can be avoided here and at various other places.

Author's response: The sentence 'In consequence, the reconstructed signal travels significantly apart from the observed signal.' will be removed and the entire manuscript will be revised accordingly.

Section 3.2.2: I suggest to show in Fig 4. directly the difference in SWD[m] and not the difference in the bending angle [arcsec]. Also, I do not find the formula for the bending angle in the manuscript. I guess you mean something like $\arccos(v1, v2)$ where $v1$ is the tangent unit vector of the ray-path at the satellite and $v2$ is the tangent unit vector of the ray-path at the station?

Author's response: The bending angle error in Figure 4 is the difference in elevation angle between full ray-tracing (until ~80 km altitude) and ray-tracing to the upper rim of the tomography model + bending model. Due to the distance of the satellite, it is widely consistent with the bending angle error obtained by analysis of the tangent unit vectors. However, we agree that errors in bending angle are difficult to interpret. Thus, we will convert it into ray path errors and displacement, i.e. how much the ray entry-point differs due to errors in the bending model. We assume that this parameter is more of interest than SWD, since we would like to focus in this paper more on geometrical aspects and its impact on the tomography solution.

Section 4.1: I suggest to add in Fig 8. the difference for the a-priori (first guess or

C6

background) refractivity (ALARO). Is the radiosonde data assimilated into ALARO?

Author's response: This radiosonde data is not assimilated into ALARO. We will add the differences between radiosonde and ALARO to Figure 8 in the revised version of the manuscript.

References: Check all references carefully. For example, Fritsche, M., Dietrich, R., Knofel, C., Rulke, A., and Vey, S.: Impact of higher-order ionospheric terms on GPS estimates, *Geophys. Res. Lett.*, 32, 1–5, 2005. Bender, M., Stosius, R., Zus, F., Dick, G., Wickert, J., Raabe, A. (2011): GNSS water vapour tomography – Expected improvements by combining GPS, GLONASS and Galileo observations. - *Advances in Space Research*, 47, 5, pp. 886–897. DOI:<http://doi.org/10.1016/j.asr.2010.09.011> In the manuscript the correct citation should be e.g. Böhm et al 2006 and not Böhm et al 2006a. Likewise the correct citation should be Hobiger et al 2008 and not Hobiger et al 2008a (there is no b).

Author's response: Thank you. The errors in the references will be corrected and carefully checked again before submission of the revised manuscript.

Additional Reference: Zus, F., Dick, G., Heise, S. and Wickert, J.: A forward operator and its adjoint for GPS slant total delays, *Radio Science*, 50, 393– 405, doi: 10.1002/2014RS005584, 2015.'

Author's response: Will be added to the revised version of the manuscript

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