

Dear Editor,

Please find attached the updated version of the amt-2018-233 manuscript, with all the corrections and modifications following the reviewers comments applied

Since the modifications were extensive, and an almost complete revision of the text were suggested by both of the reviewers, the latexdiff output is quite difficult to follow: there are just lots of blocks of text that were replaced.

For what concerns the point by point answer to reviewers comments, this has been already done in the discussion phase: I thought it was already required in that phase so I didn't provide a generic response but a detailed point by point description of the modifications to be added, including figures and data.

Thanks and best regards

G. Bianchini

Interactive comment on “A Fourier transform spectroradiometer for ground-based remote sensing of the atmospheric downwelling long-wave radiance” by Giovanni Bianchini et al.

Giovanni Bianchini et al.

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First of all I would like to thank the reviewer for the thoughtful and in-depth review, which had provided good tools for improving this work.

I'll answer, as much as possible, to each of the single questions posed:

Generally speaking, more references are needed in this paper. Furthermore, the majority of the references (28 out of 34) were by the authors of this paper; are there no other papers written by outsiders that are relevant to this study?

Yes, definitely, I must say that the choice of the references has been biased by the

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attempt of providing information about the specific instrument described in the paper without repeating what was already published, while the use of references to show other relevant works in the field has been quite overlooked. The introductory section has been reorganized in order to add references to previous works that are relevant to the paper topic.

Page1, Line 40: This is true only in clear sky horizontally homogeneous scenes. This approach will generally not work when there are clouds overhead

True, it will be clarified that this consideration, so as other to which a similar remark could apply, are referred to clear sky conditions, since the considerations and problems related to the study of clouds are out of the scope of this work.

Page 3, line 10: “that result critical in the delicate process” is very awkward. Please rephrase

Rephrased in the revision.

Page 3, line 75: Is the spectral calibration procedure similar to that in Knuteson et al. JTECH 2004? What is the spectral region used for this calibration?

The procedure has some similarities, but is not the same: in order to provide a robust algorithm that can operate in all the possible measurement conditions, it has been chosen to use the hot blackbody acquisitions for frequency calibration. This will not to perform an independent frequency calibration of each spectrum, but has the advantage of using the much more reproducible absorption spectrum due to CO₂ on the about 1.5 m optical path inside of the instrument. The calibration operates in two phases, first a rough peak finding algorithm detects the Q band center, then the whole P band in the 635-665 cm⁻¹ spectral region is fitted using the simplified $0.9 \cdot \text{sinc} + 0.1 \cdot \text{sinc}^2$ lineshape (see attached Figure 1).

This two-step process is required due to the fact that the diode laser could in principle have a frequency shift larger than the spacing of the CO₂ lines and this could induce a

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systematic error due to a “skip” of one or more lines. The description of the algorithm, and all the information and figures here provided will be added to the revised paper.

Page 3, line 85: What are the details of this scene mirror? Is it gold plated? What polarization properties?

The folding mirror is bare gold on an aluminum substrate, and has been characterized through laboratory measurement in order to provide the small correction needed for the calibration (correction that is applied using the monitored mirror temperature).

The effect of polarization is estimated as negligible, taking into account the fact that the instrument is not operating in polarization mode and the zenith scene, in clear sky condition (the operating conditions taken as a reference in this paper) is not polarized.

Page 3, line 85: What are the properties of these blackbodies? Emissivity spectra, operating temperatures, etc. How stable are they? What is the shape, arrangement of the thermistors, gradients, etc?

Detailed information on the blackbody sources is available in [Palchetti et al., Infrared Physics Technology 51 (2008)], but in order to improve text readability the main details on the blackbody performances will be added to the text. Specifically, the emissivity is better than 0.999 and the operational temperatures are between 10 and 80 °C. Stability is about same order of the temperature reading uncertainty (0.3 K), while gradients are within 0.5 K.

It should be noted that the calibration procedure compensates for linear temperature drifts of the blackbody temperature (specifically, of the reference blackbody source placed on the second input, which is providing a common reference to all the acquisitions).

Page 5, line 68: How high? What is the IWV amount? What does a LBL radiative transfer model suggest the radiance should be for this condition? Is the small bias shown in the figure due to the small amount of atmospheric emission (which could be

C3

confirmed by a RT model), or is it a real instrument artifact?

The plot was obtained exploiting the full RHUBC-II dataset, acquired from the Cerro Toco site at about 5500 m a.s.l. in the Atacama region. The dataset nevertheless included some acquisitions characterized by 1 mm or more in terms of PWV. This in fact hasn't been a good choice, since the atmospheric residual emission is the main cause of the small offset observed: an improved version of the figure (Figure 3 here attached) has been made using only measurement selected to have a PWV < 0.6 mm, which would give an offset negligible with respect to the instrument estimated accuracy.

*Page 6, line 4 and elsewhere in that paragraph: Should be $mW / (m^{**2} sr cm^{**-1})$.*

Corrected in the revision.

Page 6, line 58: What is this chain? Does it use the Revercomb technique to calibrate in complex radiance? How is non-unity emissivity of the BBs handled?

The level 1 data analysis is described in detail in [Bianchini et al., ACP 8 (2008)], it makes use of the complex calibration [Revercomb et al., Appl. Opt. 27 (1988)], while for the blackbody sources a specific mathematical model has been developed [Palchetti et al., J. Infr. Phys. Tech. 51 (2008)], it will be made an effort to add as much information as possible from the above mentioned references in order to make the paper more readable.

Page 7, line 4: what is “assimilable”? Perhaps you mean “similar” ?

Corrected in the revision in order to avoid the confusion with the most used meaning of “assimilation” in this field...

Figure 8 and in the text: Is the imaginary component of the calibrated spectra zero with some noise? Would be good to see that, esp since fig 8 shows some unbalanced spectra with significant phase signals. What is a typical noise spectrum for a standard radiance measurement?

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A figure (Figure 4 here below) will be added, showing a typical calibrated radiance spectrum (obtained by the real part of the result of the calibration procedure), and the corresponding discarded imaginary part, which contains only the noise, confirming the reliability of the complex calibration procedure.

Page 7, line 28: Are these instrumental parameters (line shape, spectral calibration) not stable with time? If that is true, why is this so?

An analysis of the long-term stability of the instrument calibration will be added, in which it is shown that, in absence of spurious effects, the laser stability allows for a < 30 ppm frequency calibration accuracy over a period of 2 years (dominated by a drift due to laser aging). The instrumental line shape is instead affected by misalignment that can occur in case of large thermal excursions of the instrument (Figure 5 here attached).

This analysis involves a 2-year long period in which no maintenance has been performed on the instrument. The observed effect around the middle of the considered period arises from operations performed on other instrumentation inside of the shelter where REFIR-PAD is installed, operations that caused some level of disturbance due to temperature fluctuations and vibrations.

Page 7, line 32: How were these number of layers determined; e.g., why a 4pt temperature profile? Turner and Löhnert JAMC 2014 using mid-infrared portion of the spectrum suggest that there is 6 pieces of information on temperature (and similar for water vapor when the IWV is small), so I would have assumed that the REFIR-PAD observations would have had at least this number of pieces, unless the noise level is much larger than the AERI used in the T/L paper (which is why the noise spectrum needs to be shown).

The number and altitudes of the fitted levels have been determined by an analysis of Jacobians and a subsequent tuning to avoid oscillations in absence of a-priori constraints, as described in [Bianchini et al., JGR 116 (2011)]. Please note that the noise

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level on REFIR-PAD spectra is actually higher than that on AERI spectra, this is mainly due to the use of uncooled pyroelectric detectors instead of cooled MCT/InSb.

Page 7, line 33: "typical" is misspelled.

Corrected in revision.

Page 7, line 34: Is the entire spectral range of the REFIR-PAD observations used in the retrieval?

Only a subset of the REFIR-PAD spectra between 350 and 850 cm^{-1} is used for the temperature and water vapor profile retrieval. This in general provides consistent results in a wide range of atmospheric conditions. A different subset, between 920 and 1070 cm^{-1} is used for the ozone column retrievals. This will be clarified in the revised text.

Fig 11: The spectral structure of the radiance observations in the 15 m band suggest that there is an inversion in the purple spectrum, and that the lapse rate is markedly different for the dark green vs. light green profiles. But these characteristics don't show up in these retrieved profiles shown in Fig 11 (or at least are not obvious to my eye). Is this due to the low number of vertical layers?

As can be seen in the attached plots (Figures 6-9 here below), showing the fitted spectra in the ν_2 band region, the fitting residuals are well inside of the measurement error, apart for one case in which I noticed that a laser mode jump happened, distorting the averaged spectrum (Figure 6 in this document, corresponding to the light green spectrum in the paper). In this case I removed the spectra showing mode jumps from the average, and as a consequence now the chi-square is better (Figure 7 here, light green spectrum after correction). Anyway, there isn't a relevant change in the resulting temperature profiles, and no significant inversion is present.

Most of the effect seen on the ν_2 band can be attributed to the CO_2 present inside and nearby the instrument enclosure but outside of the calibration path so it doesn't cancel out. This doesn't give significant effects on the retrieval, since the overall contribution

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to the chi square is negligible. In Figure 8 here below (corresponding to the purple spectrum in the paper) the instrument was slightly cooler than the environment, being placed in cool shade on a warm spring day, while in Figure 9 here below (corresponding to the dark green spectrum in the paper) it's the opposite since the instrument was operating outside in February. Please note that I made these plots for example purposes, In my opinion these shouldn't be included in the revised text, unless it is deemed absolutely necessary.

Page 8, line 6: How were these accuracies determined? Are they just the uncertainties from the propagation through the retrieval, or comparison against other obs? If you are going to talk about the retrievals in this paper, then more information needs to be provided so that the reader does not have to search through all of the references to get this information. Please include a discussion on the basic retrieval framework, what assumptions are made, the forward model used, any prior data used to constrain the solution, etc.

Accuracy on the total PWV has been estimated through the error on water vapor column fitting, and validated with a microwave radiometer [Fiorucci et al., JGR 113 (2008)], [Bianchini et al., JGR 116 (2011)]. I understand the fact that repeating some information that is in the cited references could greatly improve readability, but I have been advised (by the other reviewer) not to introduce information that is redundant with other published papers. An effort will be made anyway to add the required information in the revised text.

The retrieval was performed by using the MINUIT routine which is part of the CERNlibs. The subroutine MIGRAD, based on the Davidon-Fletcher-Powell (DFP) algorithm, was used to minimize the chi square cost function given by:

$$\chi^2 = (y - F(X))^T S_y^{-1} (y - F(x)) \quad (1)$$

where y and x are the vector of the measurements and the state of the atmosphere

C7

respectively, F is the forward model (LBLRTM version 12.2 in our case) and S_y is the diagonal VCM for the measurements. The DFP algorithm, on which the MINUIT MIGRAD routine is based, is a quasi-Newton method which does not require the calculation of the jacobians at each iteration but uses an approximated form. This algorithm updates the inverse hessian matrix calculating the derivatives just at the first step and then using the iterative formula shown above. The same fitting approach which was applied in a previous works [Bianchini et al., JGR 116 (2011)], was used in this paper. No a-priori information was assumed as regularly done in a Bayesian approach, such as optimal estimation, and the initial guess is represented by a local monthly climatology, obtained averaging over a set of radiosoundings daily performed at Dome-C. Since no a-priori information was used to constrain the solution and no regularization was introduced, to avoid the oscillation effects due to the ill-conditioning of the problem this approach requires to limit the number of retrieved parameters, hence the number of fitted levels both for water vapor and temperature profiles is equal to the number of degrees of freedom (DOF). The DOF were derived from a preliminary study performed through singular values decomposition of the Hessian matrix which includes Jacobian and the measurements noise.

Page 8, line 29: I don't think that an interferometer like REFIR-PAD can be considered a "relatively simple tool". Even compared with other spectroradiometers this instrument is pretty advanced. Now, perhaps its operating characteristics make it easy to deploy and it can run autonomously, and that is what the authors are referring to here. If so, then there is little information in this paper about the long-term calibration stability and responsivity of the instrument, other than the oblique reference that some instrument parameters need to be retrieved (see above)

I agree that the choice of the term "simple" is at least misleading, if not plainly wrong, the sentence will have to be rephrased in order to stress the simplicity of operation and the ruggedness that allow for minimal need for interventions and maintenance. As stated before, long-term stability of instrument parameters will be described in the

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revised text, so will be the hardware that allow for remote operation and management.

Page 8, line 34: this instrument cannot “resolve all relevant atmospheric processes”. For example, 10-minute resolution is not able to resolve the rapid changes in cloud optical properties as they advect over the sky port of this instrument.

Yes, as stated before, and as will be explicitly described in the revised text, this has to be intended as in clear sky conditions.

Page 8, line 43: The o3, ch4, and n2o retrievals were demonstrated here, and references to papers that show this are few / none.

More details on the procedure to retrieve N₂O and O₃ will be added: in the first case it is an extra parameter that rescales the vertical N₂O profile in the T/WV fitting process, making use of the 589 cm⁻¹ spectral band. In the case of O₃ a separate fitting process is used, operating in the 920-1070 cm⁻¹ spectral region with a total of three fitted levels. In Figure 10 here attached are shown some results obtained in the September 2017 – April 2018 period, in case of ozone the available OMI data are also shown for comparison.

While a noticeable offset in ozone data is present and needs to be investigated further, the temporal variability is in good agreement with the satellite data, and the vertical variability observed in the retrieved 3-points profile shows a noticeable variation in the vertical ozone structure in coincidence with the rapid variations in the columnar amounts (Figure 11 here below). This can be explained with the fact that Dome C is on the edge of the polar vortex region.

Page 8, line 47: As indicated above, you haven’t spoken about the long-term operations at all, and certainly not the ability to remotely control the instrument (this is the first mention of it). What are the “relevant settings” ?

A section of the revised text will describe the infrastructure allowing for remote control and management (remote shell connection, transfer of selected and preprocessed

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data through low-bandwidth connection, auxiliary instrumentation and subsystems as thermal stabilizers)

Page 8, line 55: “aknowledge” is misspelled.

Corrected in the revised text.

Interactive comment on Atmos. Meas. Tech. Discuss., doi:10.5194/amt-2018-233, 2018.

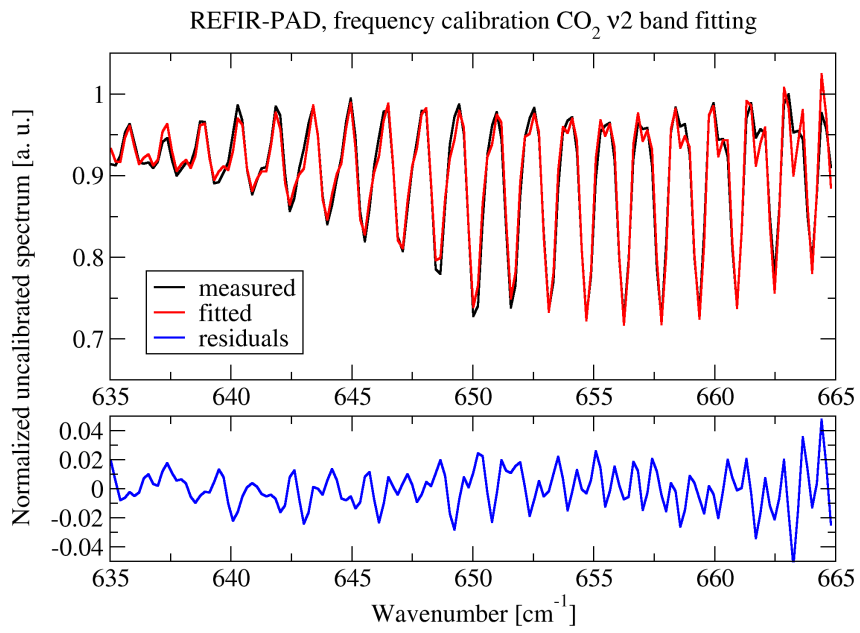


Fig. 1.

C11

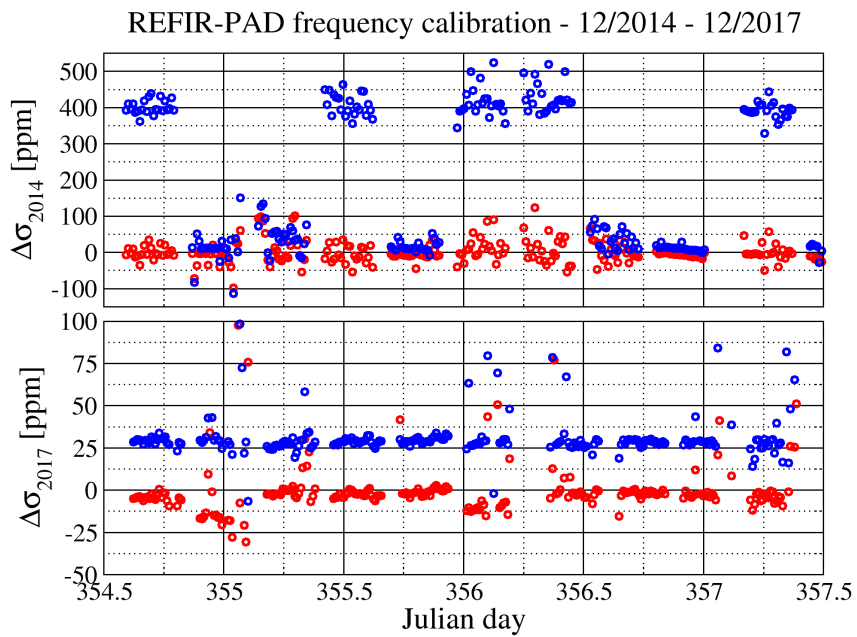


Fig. 2.

C12

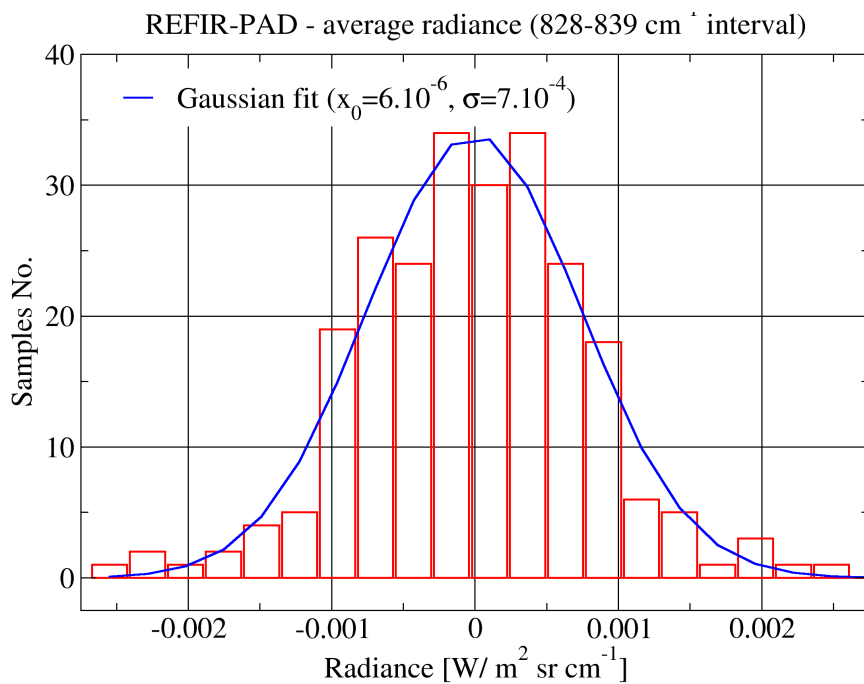


Fig. 3.

C13

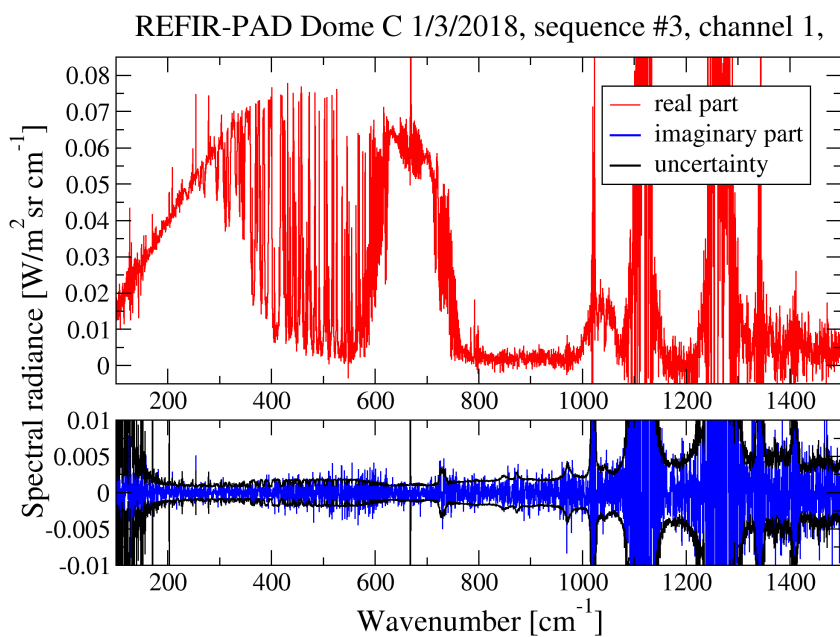


Fig. 4.

C14

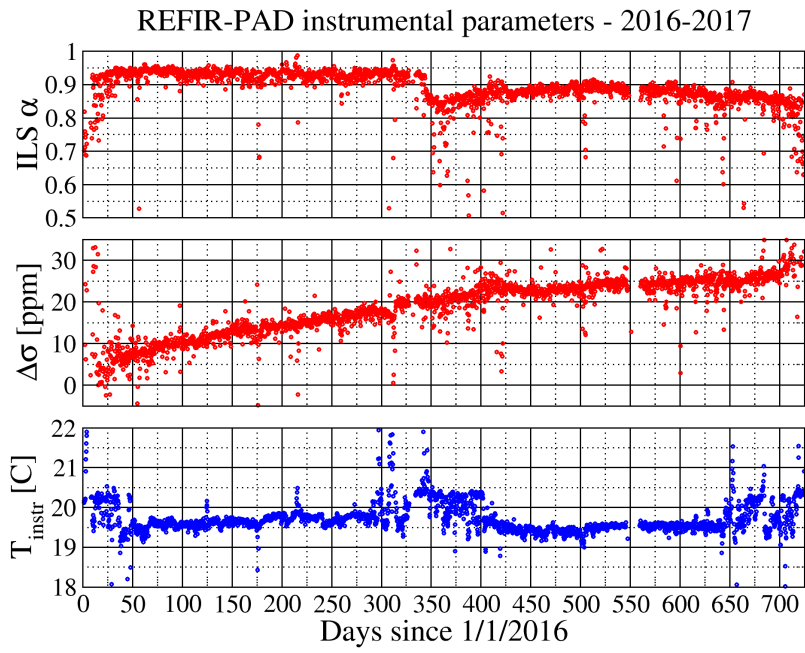


Fig. 5.

C15

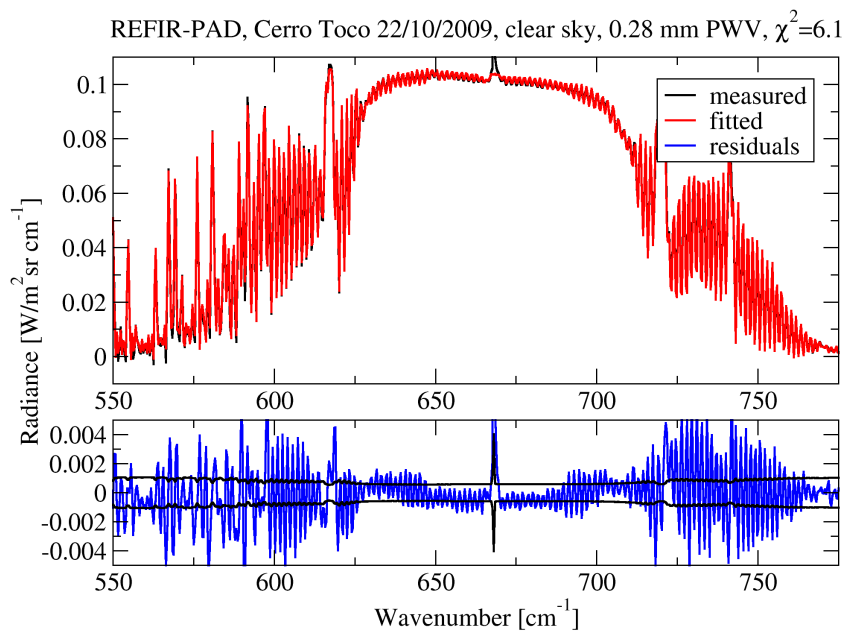


Fig. 6.

C16

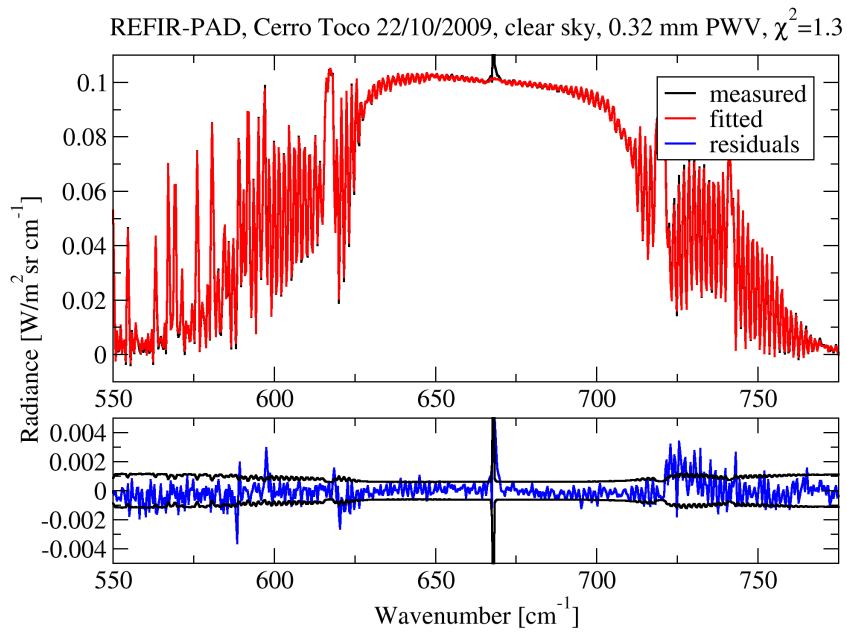


Fig. 7.

C17

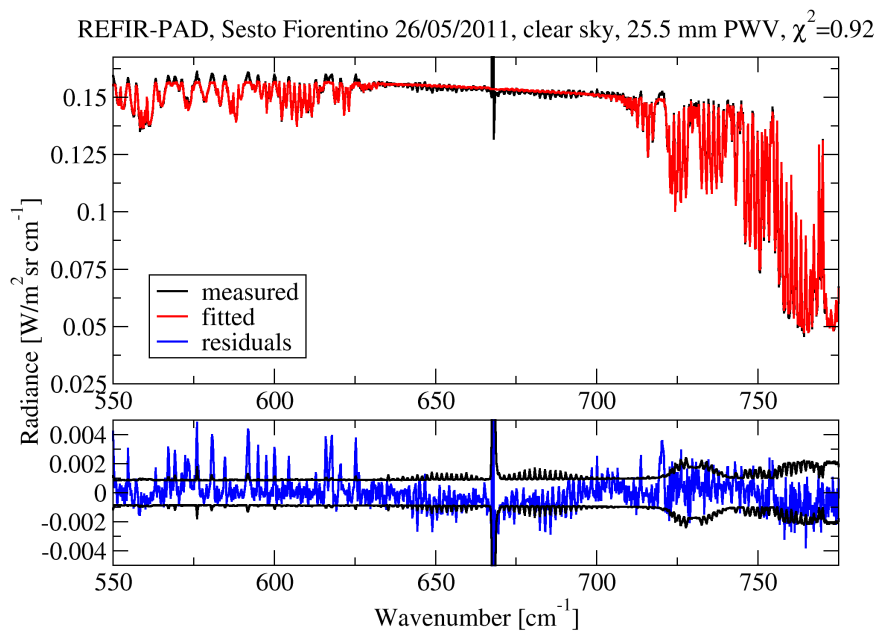


Fig. 8.

C18

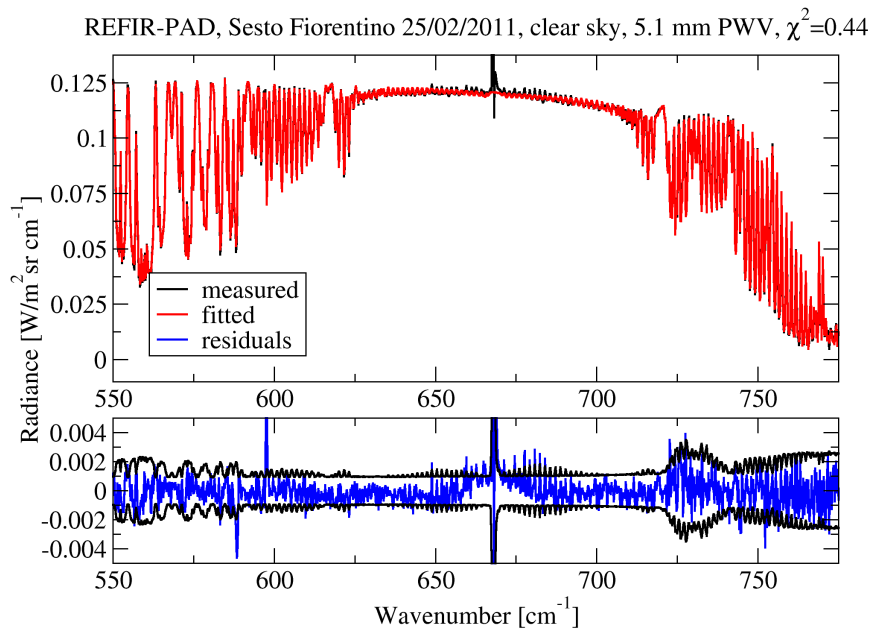


Fig. 9.

C19

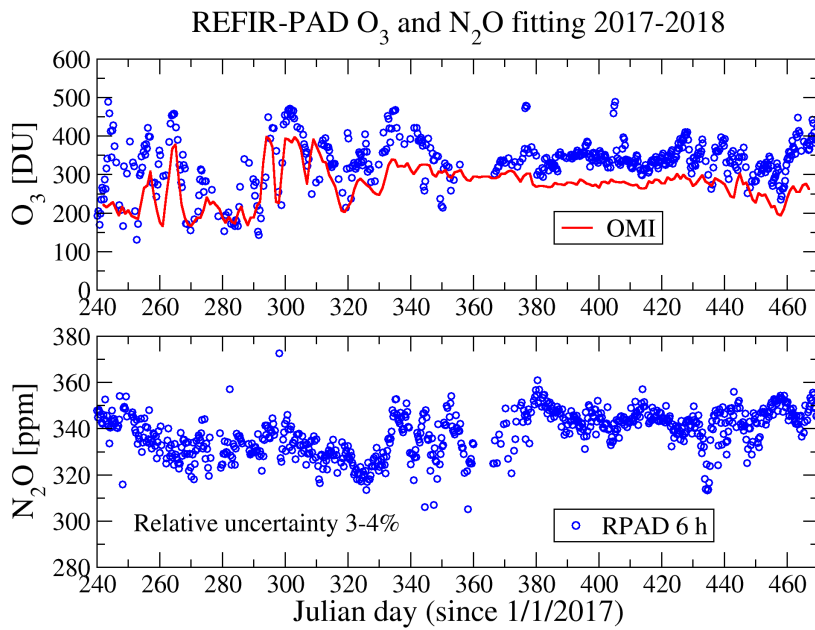


Fig. 10.

C20

REFIR-PAD o3 VMR map

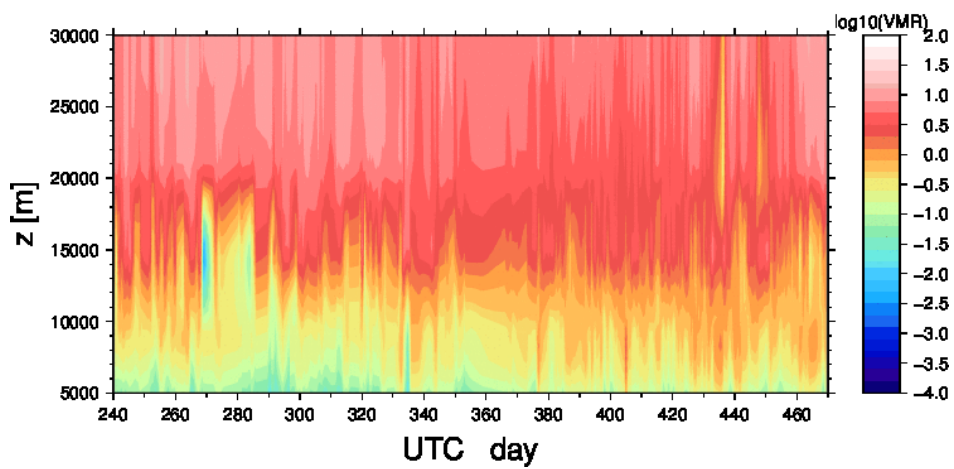


Fig. 11.

Interactive comment on “A Fourier transform spectroradiometer for ground-based remote sensing of the atmospheric downwelling long-wave radiance” by Giovanni Bianchini et al.

Giovanni Bianchini et al.

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Before proceeding, thanks for the time spent in your review, I'll try to answer to all the questions adding the requested information whenever possible, information that will be also included in the reviewed text.

The theme of the article fits well within the scope of AMT and the article is clearly written, but the current scope does not provide enough new information as compared to already existing literature. No substantial new concept or data is presented. Therefore I recommend to publish the article only after major extension/revision. In particular the performance analysis part has to clearly state the new insights gained in comparison to

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earlier papers and the data section needs to present a more comprehensive overview of the Antarctic dataset.

Section 7 has been reorganized and more information has been provided to describe the available dataset and the Antarctic campaign.

Section 3 discusses instrument lineshape. Please highlight the new insights gained relative to the information provided earlier (Fig. 4 of the current paper and Fig. 17 of the Bianchini, 2008b paper seem to be identical).

Yes, actually the instrumental lineshape in the far-infrared region is expected to be quite ideal, by design, so the figure has been changed (see Figure 1 here below) showing the ILS at two different wavenumbers, both in the far-infrared and at the upper limit of the operating spectral band, for two different spectral sampling values (0.5 and 0.25 cm^{-1}). This will integrate the data presented in Figure 5 in the paper, that shows the retrieved lineshape coefficient at different wavenumbers, providing a more complete characterization of the instrumental line shape as a function of spectral sampling and wavenumber.

Section 4 discusses detectors and data acquisition electronics. What is different to the analysis performed in section 2.1 of the abovementioned paper (Figure 6 of the current paper and fig. 3 and 5 of the 2008 paper seem to convey the same information)?

Also in this case, as expected, the instrumental parameters have not changed significantly in time. A choice was made to present some data that is redundant with the published papers: as it has been noted by the other reviewer, in some cases information should be repeated in order to allow readability without having necessarily to keep at hand also all the references. Anyway, the bottom panel of Figure 6 (in the paper) is redundant and will be omitted, while the top panel which corresponds to the last performed characterization involving the current detectors will be kept since it contains new information.

C2

Section 5 discusses radiometric performances. A statistical analysis of offset values in one atmospheric window region is presented. Again the value of this analysis in the context of the existing radiometric performance analysis needs to be stated more clearly. Instrument offset will be wavenumber dependent. An analysis of the radiometric offset in other spectral regions is of interest.

Yes, the observation is correct, but we do not have a similar check that can be performed over the whole spectral range and continuously during a multi-year deployment of the instrument. Thus this kind of estimate, even if related to a narrow spectral range, is relevant. An estimate covering the full spectral range can be obtained through an external reference blackbody placed on the instrument measurement port, but this requires dedicated measurements and cannot be performed during remote operation.

Figure 2 here below shows the results of such a calibration measurement. Even in this case the calibration accuracy is quite constant over the relevant spectral range and well inside of the measurement uncertainties. Below 300 cm^{-1} and in the correspondence of the beam splitter substrate absorption bands the measurement errors are prevalent and it is difficult to quantify the actual calibration accuracy.

Section 6 states to discuss spectroscopic performances. It then describes qualitatively the agreement between an analytical instrument model and laboratory measurements. The model is not detailed and there is no quantitative discussion of the discrepancies between model and measurement. No attempt is made to derive figures of merit and compare them with requirements. The title of the section is misleading and the description of model and results is not sufficing to provide insights. The section should either be omitted or renamed and significantly extended.

I agree that the title "Spectroscopic performances" is without doubt a misnomer, this is my fault because I left the title as it was through various changes of the text, it will be changed in "Instrument mathematical modeling". The scope of the model is to provide a qualitative analysis devoted to the understanding and, if possible, correction,

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of the various instrumental effects. The main scope is to understand the effect of non-ideal beamsplitters and to devise the best way to obtain optical path difference compensation, i.e. minimizing the phase variations across the spectral range.

This is achieved mainly with the correct orientation of the beam splitters, but also small layer thickness differences can give a measurable effect. All this will be better explained in the revised text, along with a more in-depth description of the model used and the corrected title.

Section 7, last sentence: I do not think that one offset measurement at 835 cm^{-1} is sufficient to derive a relative uncertainty for the whole wavenumber region from $200\text{--}667\text{ cm}^{-1}$. The deduction could possibly be made with the help of the instrument model, but then this needs to be demonstrated.

A new figure (number 2 in this document) showing a characterization of the radiometric uncertainty over a wider spectral range will be added to the revised paper. Nevertheless, the results shown in Figure 7 in the paper (which has been updated with a better selection of the analyzed measurements, Figure 3 here below) have their specific purpose in providing a way to check the consistency and stability of the calibration without the need of dedicated measurements. This is of particular importance in case of a remote deployment of the instrument. The sentence will be rephrased to clarify this.

Section 8 shows an exemplary L2 data set. Yet no comprehensive data set is presented (e.g. a time series of measurements), no scientific interpretation is provided and no quality assessment (e.g. validation through other data) is made. There is no supplement with data or information about where the data could be accessed. It is mentioned in section 8 / L2 products that the retrieval of methane requires a hardware modification of the instrument. In the conclusions section, Methane is mentioned as provided data product, though.

For what concerns data validation, this has been performed during previous campaigns, see [Fiorucci et al. JGR 113 (2008)], [Bianchini et al. JGR 116 (2008)], [Turner

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et al. GRL 39 (2012)] in which REFIR-PAD measurements and retrievals have been compared with other instruments, both FTS and microwave radiometers.

The presented level 2 data examples were meant more as a way to show the capability of the instrument/data analysis process to operate across a wide range of atmospheric conditions (in terms of temperature and water vapor content) rather than showing a long-term time series.

While a complete discussion of a long term time series of data would need a complete scientific discussion on its own (and it's possibly out of the scope of this "instrument" paper), however a data set covering a period of about an year will be provided, showing all the level 2 products that are available at the moment (temperature and water vapor profiles, N₂O and O₃ columns, see Figures 4, 5 and 6 here below).

Please note that due to research project constraints, the actual data set cannot be released at the moment, since there is a clause that restricts the access to project participants for the whole project's duration and the following two years.

Unfortunately, for what concerns methane, no data can be provided since the Polypropylene-based beamsplitters even if realized, have not still been used on the field. For what concerns nitrous oxide, it is a secondary output of the temperature and water vapor profile retrieval, it makes use of the 595 cm⁻¹ band and just rescales the initial guess profile (constant in value throughout the troposphere). The values shown in Figure 6 here below are expressed in ppm of VMR at ground due to the nature of the rescaled profile. Ozone fitting is performed separately using the 920-1070 cm⁻¹ spectral range and a 3-point vertical profile, the results shown in Figure 6 are compared with the available OMI data for the Dome C site.

Section 9 (conclusions) reiterates the properties of the instrument without providing real conclusions or an outlook.

The conclusions section will be rewritten in order to cite explicitly the importance and

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uniqueness of the long-term dataset that has been and is still being acquired by the REFIR-PAD instrument. Outlooks for future development of the instrument (like the use of Polypropylene based beamsplitter and the new possibilities opened by this) and for future uses of the acquired dataset will also be presented.

Interactive comment on Atmos. Meas. Tech. Discuss., doi:10.5194/amt-2018-233, 2018.

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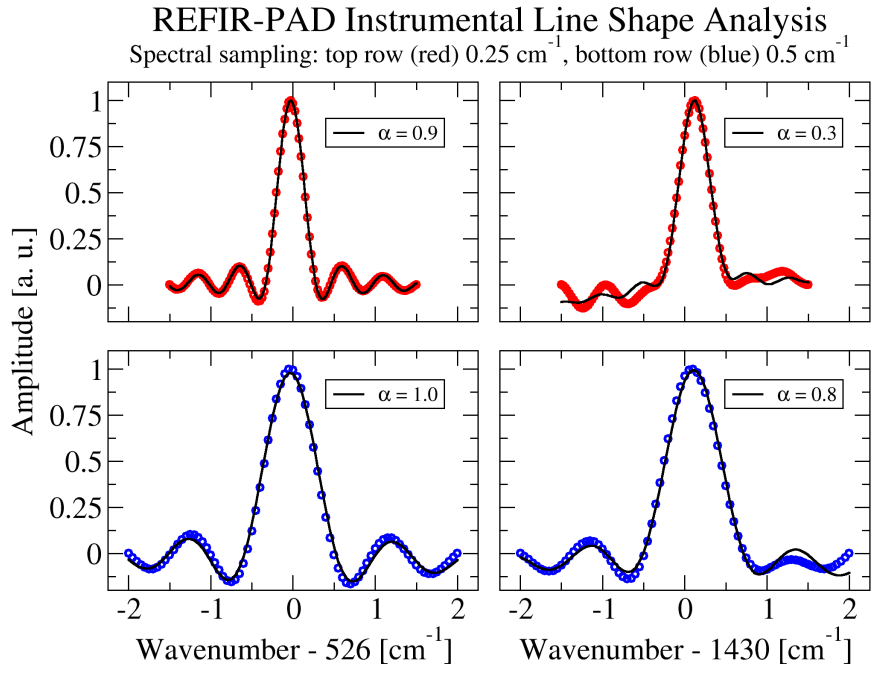


Fig. 1.

C7

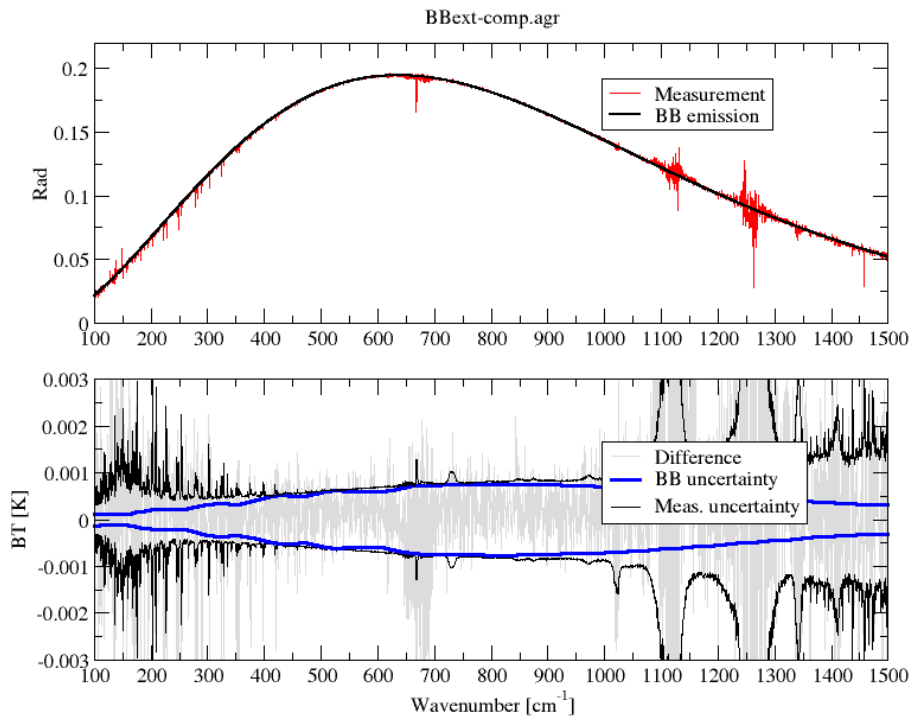


Fig. 2.

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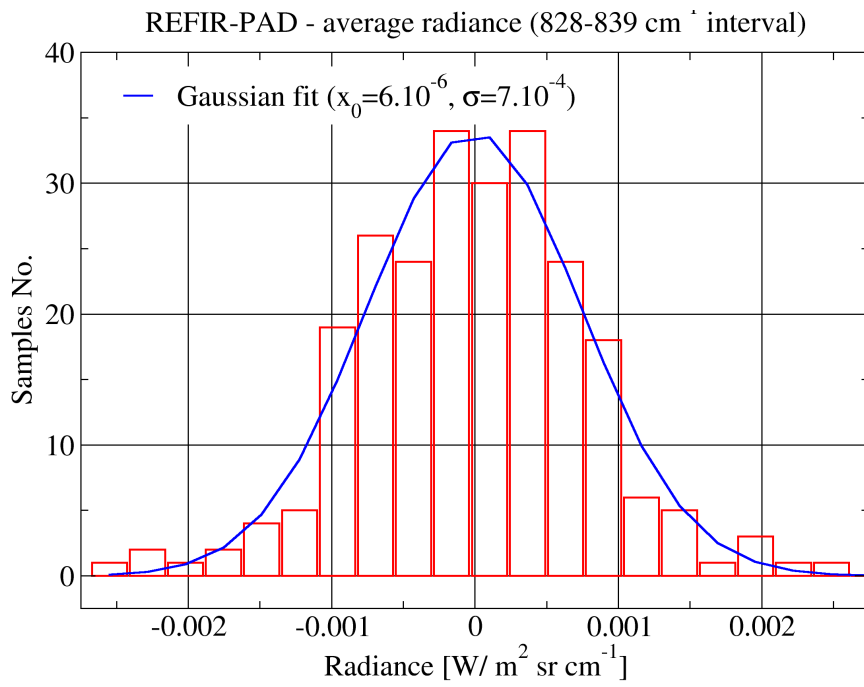


Fig. 3.

C9

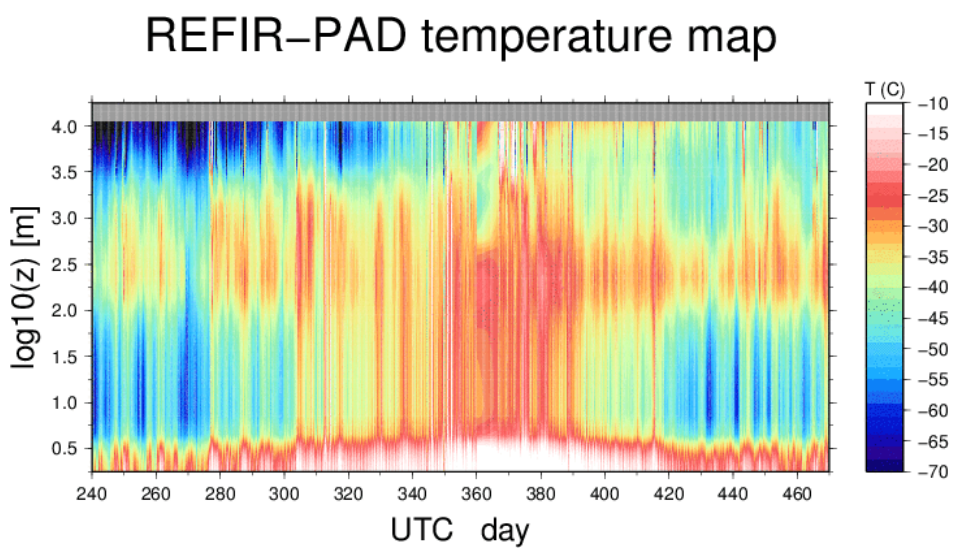


Fig. 4.

C10

REFIR-PAD h2o VMR map

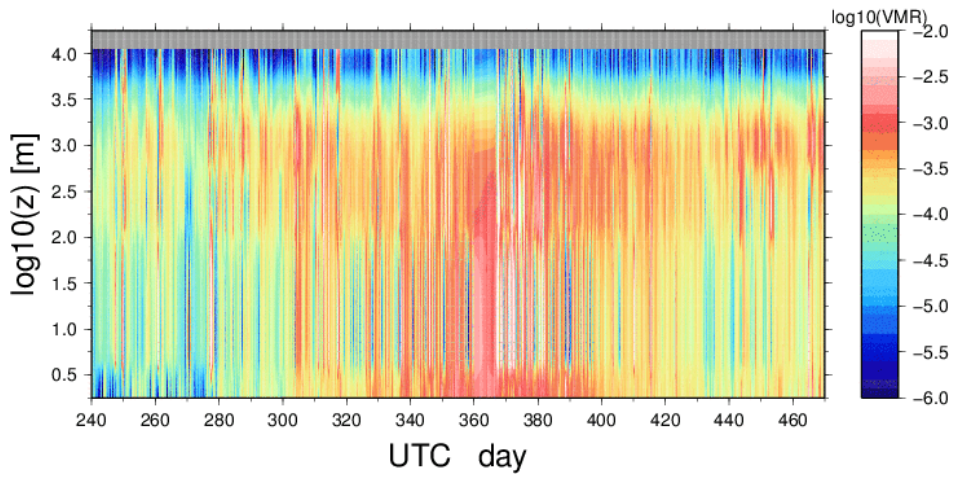


Fig. 5.

C11

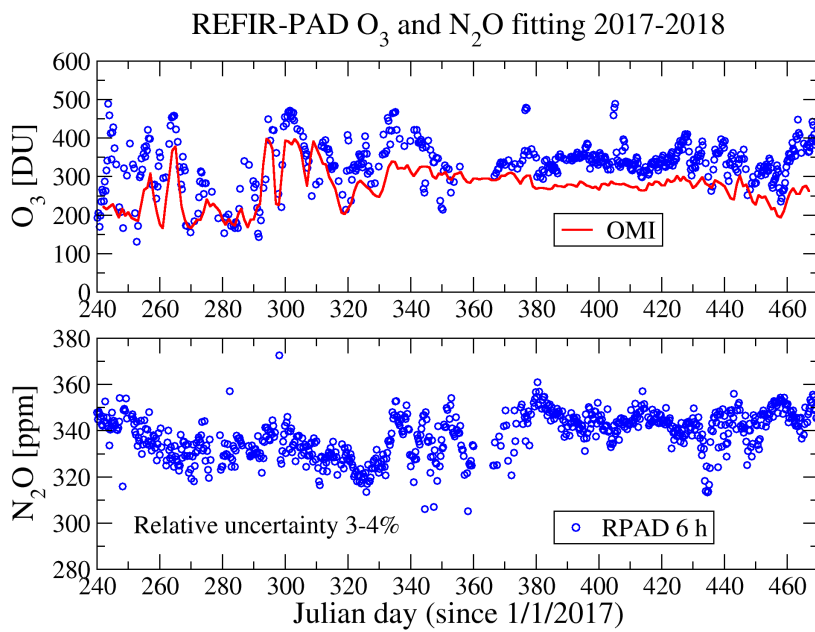


Fig. 6.

C12

A Fourier transform spectroradiometer for ground-based remote sensing of the atmospheric downwelling long-wave radiance

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Abstract. The Radiation Explorer in the Far Infrared - Prototype for Applications and Development (REFIR-PAD) is a Fourier transform spectroradiometer that has been designed to operate both from stratospheric balloon platform and from ground. It has been successfully deployed in a stratospheric balloon flight and several ground based campaigns from high altitude sites, including the current installation in the Concordia Italian-French Antarctic station. The instrument is capable to operate autonomously with only a limited need of remote control and monitoring, and is providing a multi-year dataset of spectrally resolved atmospheric downwelling radiances, measured in the 100-1500 cm^{-1} spectral range with 0.4 cm^{-1} resolution and a radiometric uncertainty better than 0.85 $\text{mW}/(\text{m}^2\text{sr cm}^{-1})$.

1 Introduction

The measurement of the atmospheric downwelling longwave radiance (DLR) is a crucial task in climate and Earth radiation budget studies since it provides the complementary quantity to the top-of-atmosphere outgoing longwave radiance (OLR) measured from space. The knowledge of both these quantities is needed in order to achieve a complete characterization of the Earth radiation budget (ERB) (Wild, 2013).

Unfortunately, for what concerns ground-based measurements, it is very difficult to achieve a global coverage because DLR measurements can be performed only from limited locations above land areas (Ohmura et al., 1998), thus causing large errors in the estimation of the global balance of energy fluxes. This uncertainty limits our ability to identify with sufficient reliability the response (feedback) of the Earth's climate to the variation of different components (forcing) (Stephens et al., 2012).

Nevertheless, some new insights can be obtained by using spectrally resolved measurements (Huang et al., 2007; Huang, 2013). A spectrally resolved measurement of the DLR provides significant advantages with respect to spectrally integrated measurements, allowing for an accurate identification of the radiative forcing and feedback signatures, and thus the contributions to the ERB, of the various atmospheric constituents (Gero and Turner, 2011).

On the other hand, ~~spectrally resolved measurements, in order to observe an homogeneous scene, typically provide compared to standard DLR broadband integrated measurements providing the downwelling irradiance at ground level, as those coming from the Baseline Surface Radiation Network (BSRN) (Ohmura et al., 1998), spectrally resolved measurements typically measure~~ only the radiance for a single line of sight and in a small solid angle. Further calculations, or several measurements made at different angles, are needed to estimate the irradiance.

~~This limitation~~ This limitation is typically present for space measurements where the OLR irradiance is calculated from the observation of few lines of sight from polar orbit, e.g. CERES (Loeb et al., 2005, 2007), or from a single line of sight from geostationary orbit, e.g. GERB (Clerbaux et al., 2003).

This limit can be overcome with the use of a radiative transfer model and the application of an inversion procedure on the measured atmospheric emission spectra to retrieve vertical profiles of relevant variables as water vapor, temperature and minor constituents. ~~These~~, which are relevant for the calculation of DLR. In practice these variables can be used in the forward model to reconstruct radiance in the lines of sight that were not directly measured (Palchetti, 2017) –

~~This kind of analysis also constitutes, in itself, an alternative monitoring method with respect to radiosounding and thus calculating the downwelling irradiance in clear sky conditions.~~ This approach has also been applied to satellite observations to derive CERES fluxes from IASI spectral measurements (Turner et al., 2015).

~~The Radiation Explorer in the Far Infrared – Prototype for Applications and Development (REFIR-PAD) Fourier transform spectroradiometer has been developed with the aim of performing the spectrally resolved measurement of atmospheric emitted radiation, covering the most part of the atmospheric emission spectrum, from 7 to 100 μm , thus including Spectral observations in the thermal infrared have been used to retrieve atmospheric state both from top of atmosphere (TOA), see e.g. Ridolfi et al. (2000) or ground-based observations (Smith et al., 1999), and to perform radiative closure experiments (Turner et al., 2004; Reichert and Sussmann, 2016). However all these observations typically cover only the Mid-IR. A few instruments have been developed to cover the far-infrared (FIR) region, defined as wavelengths greater than 15 μm or, approximately, above the CO_2 ν_2 band, and are operated from ground and airborne platforms for limited timescale campaigns (Mariani et al., 2012; Green et al., 2012; Mlyneczek et al., 2016).~~

While the relevance of the FIR spectral interval for atmospheric studies, and in particular for the study of climate, is a well-established concept (Sinha, 1995; Brindley, 1998; Harries, 2008), FIR still remains a significantly underexplored region, even more if we consider specifically long-term monitoring projects.

The use in the Radiation Explorer in the Far Infrared - Prototype for Applications and Development (REFIR-PAD instrument) Fourier transform spectroradiometer (FTS) has been developed with the aim of performing the spectrally resolved measurement of atmospheric emitted radiation covering the most part of the atmospheric emission spectrum, from 7 to 100 μm , thus including the FIR region.

The use of room-temperature detectors and of highly reliable mechanical solutions derived from space-qualified projects (Rizzi, 2002), makes ~~of it the REFIR-PAD instrument~~ an ideal tool to perform monitoring-mission-ground-based monitoring missions on climatologically relevant timescales. This capability has been tested in 2007 with the ECOWAR campaign (Earth COoling by WAter vapor Radiation) (Bhavar, 2008) and in 2009 with the RHUBC-II campaign (Radiative Heating in the Underexplored Bands Campaign - II) (Turner, 2012). REFIR-PAD measurement capabilities are currently being fully exploited with the installation of the instrument in the Italian-French Antarctic station Concordia, in the Dome C region on the Antarctic Plateau (75° 06' S, 123° 23' E, 3.233 m a. s. l.), where it is operating in continuous acquisition mode since December 2011.

The REFIR-PAD Antarctic campaign is performed in the framework of several research programs financed by the Italian Antarctic Research Program (PNRA - Programma Nazionale di Ricerca in Antartide): PRANA (Proprietà Radiative del va-

pore Acqueo e delle Nubi in Antartide), COMPASS (COncordia Multi-Process Atmospheric StudieS), DOCTOR (DOme C Tropospheric Observer) and FIRCLOUDS (Far Infrared Radiative Closure Experiment For Antarctic Clouds).

5 Previous deployment of a FTS instrument at Dome-C dates back to the austral summer season between 2003 and 2004, when the Polar AERI (PAERI), operating in the 500-3000 cm^{-1} spectral range with 1 cm^{-1} resolution, was used to perform a characterization of the Antarctic DLR (Walden et al., 2005, 2006). Other similar measurements were performed at South Pole (Town et al., 2005) and at Dome A (Shi et al., 2016).

In this paper a review of the main characteristics of the REFIR-PAD spectroradiometer is shown, together with the description of some measurement results obtained in ground-based campaigns in clear sky conditions; considerations and problematics related to the study of clouds are considered out of the scope of this work.

10 2 The REFIR-PAD spectroradiometer

The REFIR-PAD Fourier transform spectroradiometer is based on a Mach-Zehnder interferometer with a folded optical design that allows for a compact instrument while still retaining the moderate resolution and high throughput needed for atmospheric studies. The folding of the optical path and the number of reflections are designed to provide some degree of scanning mirror misalignment compensation (Carli, 1999a; Palchetti, 1999), allowing for a simpler mirror scanning mechanism design
15 (Bianchini, 2006b).

The Mach-Zehnder configuration provides access to both of the two inputs and the two outputs of the interferometer, allowing for the use of a reference ~~source (Reference Black Body, blackbody source (RBB in Figure 1) permanently installed on the second input, a feature that~~. This feature, as we will see later, is critical for the reduction of beam splitter emission effects. Moreover, output separation allows to have two independent output channels.

20 The interferometer has the capability of operating both in a Martin-Puplett (Martin, 1969) polarizing scheme, and in a more simple amplitude-division configuration. In the first case, as shown in Figure 1, top panel, all the four beam splitters are installed, two acting as polarization divider and recombiner, and the other two, the ones nearer to the mirror scanning mechanism (Roof-Top Mirror Unit, RTMU in figure), as proper interferometric beam splitters.

The amplitude-division configuration makes use only of the two interferometric beam splitters, while the two other mounts
25 are left empty. This configuration has shown to be the best choice when aiming for a wide operating spectral range, since with the use of bi-layer dielectric beam splitters the instrumental response can be tuned according to the experimental requirements.

For example, with a 0.85 μm Ge layer on a 2 μm Mylar substrate an interferometric efficiency better than 80% in the 100-1300 cm^{-1} spectral range can be achieved, while with a thinner structure (0.6 μm Ge layer on a 1.5 μm Mylar substrate) the response towards higher wavenumbers can be enhanced, extending the operating range to 1900 cm^{-1} at the cost of a reduction
30 of the efficiency below 200 cm^{-1} (see Figure 2). This does not constitute a problem for ground-based measurements where even in cases of extreme atmospheric transparency, with very low humidity, there is no significant atmospheric signal below 200-250 cm^{-1} .

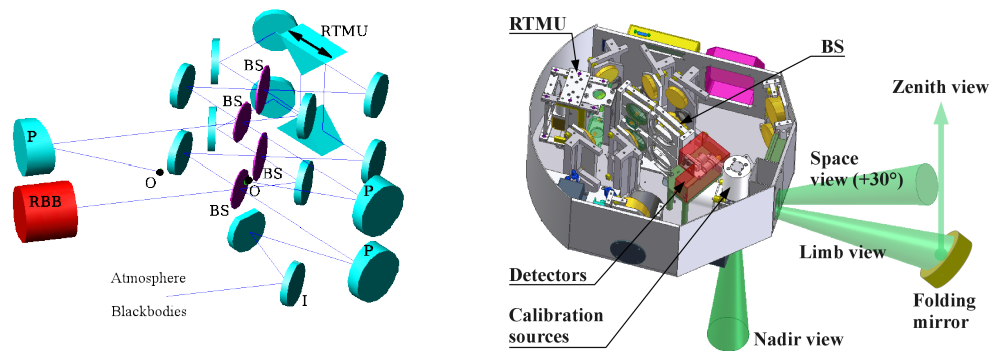


Figure 1. Top panel: REFIR-PAD optical layout. BS: beam splitters, P: off-axis parabolic mirrors, RBB: reference blackbody source, O: outputs (detectors), I: input selection mirror, RTMU: roof-top mirror unit (interferometric scanning mirror). Bottom panel: REFIR-PAD [mechanical](#) layout showing the actual placement of the components in the instrument enclosure [and the optional folding mirror used for zenith view](#).

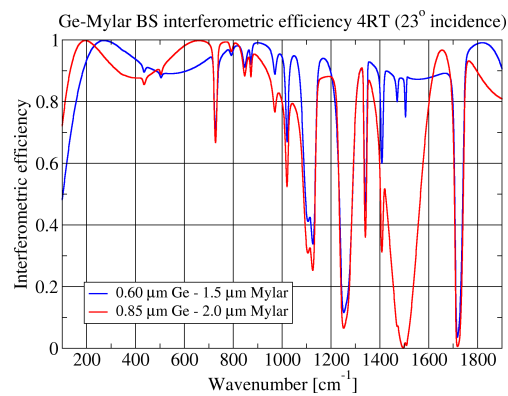


Figure 2. Real part of the interferometric efficiency 4RT calculated with two different configurations of the bi-layer Germanium on Mylar substrate beamsplitters.

In Figure 2 [it](#) is also evident that the substrate itself poses some limitations to the operating spectral range due to its absorption properties. The substrate absorption bands not only reduce the efficiency, possibly “blinding” the instrumental response as in the case of the strong features near 1250 and 1700 cm^{-1} , but also introduce a dephasing that makes an accurate radiometric calibration a challenging task in spectral regions close to the absorption bands (Bianchini, 2008a).

- 5 These problems could be overcome by using a different substrate, like polypropylene, which has fewer and weaker absorption bands in the region of interest, but this comes at the cost of worse optical and mechanical properties [that result critical in, which can critically affect](#) the delicate process of beam splitter assembly and Germanium deposition. So Mylar has been chosen as a trade-off between theoretical efficiency and optical quality.

Problems arising from beam splitter substrate absorption, and in general from non-ideal beam splitters are also mitigated through design choices in the interferometer: the use of a reference source (RBB in Figure 1) operating at the same temperature of the instrument, and thus of the beam splitters, reduces ideally to zero the contribution to the interferogram due to beam splitter emission (Carli, 1999b; Bianchini, 2009). The orientation of the two beam splitters is also chosen in order to symmetrize the optical paths and minimize the out-of-phase contributions to the interferogram (Bianchini, 2009), as it will be discussed in more detail in Section 8. As a matter of fact, the biggest contribution to the interferometer output due to the beam splitters in this configuration comes from the small layer thickness differences between the two beam splitters, differences that are inherent in the manufacturing process (see also Section 8).

A rotating folding mirror is placed at the instrument input port, allowing to select an atmospheric line of sight or one of the two on-board calibration sources. The rotating mirror is in the focus of a 320 mm focal length, 20° off-axis parabolic mirror that collimates input radiation towards the interferometer. The second input do not need collimating optics since its directed towards the large diameter RBB source.

The zenith line of sight that is used in the case of ground based measurements is obtained through the use of an extra folding mirror placed on the limb line of sight (see Figure 1, bottom panel).

Two 170 mm focal length, 30° off-axis parabolic mirrors focus the interferometer output ports on two 10 mm diameter Winston cone concentrators that feed the detectors. The interferometer is placed in the 1.4 m-length collimated optical path between input and output parabolic mirrors. A 22 mm pupil stop is placed in the center of the collimated path, inside the roof-top mirror unit.

The designed beam divergence Ω inside of the interferometer is 0.0027 sr, giving an instrument throughput of 0.011 cm²sr. However in practice there is a limitation that is posed by the concentrator-detector coupling.

The coupling efficiency is limited by the presence of a CsI window that seals the detector case from ambient humidity. Ideally the detector should be placed as near as possible to the concentrator output aperture, but the minimum distance is actually limited by the window thickness and the distance between the window and the detector active surface.

In Figure 3 is shown the variation of the coupling efficiency with the distance between concentrator and detector. The curves corresponding to the two channels differ due to the diameter of the active surface of the two detectors (2 mm for channel 1 and 1.5 mm for channel 2). The dots show the operating condition of the two channels, corresponding to a concentrator-detector distance of 2.7 mm for channel 1 and 2.3 mm for channel 2.

As shown in Figure 3, the limitation in coupling efficiency causes a loss of about 40% in signal, but also acts as a field stop limiting the instrument field of view, reducing the beam divergence to about 0.00087 sr, for a throughput of about 0.0035 cm²sr.

All the mirrors used on the REFIR-PAD instrument are coated in bare gold in order to minimize infrared absorption. Since the zenith looking folding mirror is placed outside the calibration path, its reflectivity has been characterized in laboratory and its temperature is constantly monitored in order to apply a calibration adjustment. The effect of polarization is estimated as negligible, taking into account the fact that the instrument is not operating in polarization mode and the zenith scene, in clear sky conditions, is not polarized.

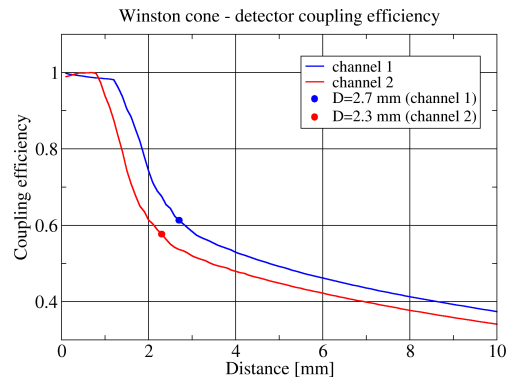


Figure 3. Plot of the concentrator-detector coupling efficiency as a function of their distance for both channels. The solid dots show the actual operating point, corresponding to a concentrator-detector distance of 2.7 mm for channel 1 and 2.3 mm for channel 2.

Interferometric metrology is based on a paraxial laser interferometer with a 780 nm laser source (Bianchini, 2000a) that has been thoroughly tested in high-resolution FTS instruments operating both from ground (Palchetti, 2005) and from stratospheric platforms (Bianchini, 2004, 2006a).

The reference interferometer does not share any of the infrared interferometer optics, simplifying the instrument design and alignment, at the cost of having a possible misalignment between the two optical axes. This doesn't constitute a problem since it induces a linear wavenumber error which is taken care of in the wavenumber calibration procedure. This procedure, [further detailed in Section 7](#), is based on known atmospheric line centers and does not rely on the measurement of the exact laser wavelength.

Along with the reference black body RBB, two other black body sources are used for the radiometric calibration ~~of the REFIR-PAD measurements~~ (Bianchini, 2008a). These sources, Hot Black Body (HBB) and Cold Black Body (CBB), are placed near the instrument measurement port and can be switched into the line of sight through the rotating input [bare gold mirror](#) (see Figure 1, label "Calibration sources"). ~~Acquisition of~~

~~For HBB and CBB can be the emissivity is better than 0.999 and the operating temperature is between 10 and 80 °C. Temperature stability and temperature measurement uncertainty are both about 0.3 K, while gradients are within 0.5 K~~ (Palchetti, 2008a).

~~It should be noted that limited size and good emissivity can be both achieved with these sources due to the relatively small 22 mm aperture of the blackbody which is a consequence of the placement in proximity of the focus of the input parabolic mirror.~~

~~The reference blackbody RBB has a larger diameter (64 mm) due to its placement in a collimated part of the optical path, but its requirements are more relaxed since it is not stabilized in temperature but, instead, left in thermal equilibrium with the instrument.~~

~~Acquisition of HBB and CBB radiance is performed regularly in order to obtain a constant tracking of possible instrumental response function variations. Typically a 10 minutes acquisition sequence includes 4 atmospheric measurements and 4 cal-~~

ibrations, 2 with HBB and 2 with CBB. Radiometric performances of the REFIR-PAD instruments are further described in section 6.

3 Instrumental line shape

5 A good model of the instrumental line shape (ILS) is a necessary requirement to correctly interpret the measured spectra and perform the level 2 data analysis (Section 10). Several effects can contribute to distort the ILS from the theoretical $\text{sinc}(2\pi\sigma z_{\text{max}})$ function, where z_{max} is the maximum optical path difference. Misalignment of the interferometer and scanning mirror deviations (Bianchini, 2000b) can contribute to the ILS, another possible effect is due to the finite solid angle Ω of the radiation propagating inside of the interferometer.

10 The effect of the finite solid angle is to broaden and shift spectral lines by convolving, in the wavenumber domain, the ideal sinc ILS with a box function extending from 0 to $\sigma_0\Omega/2\pi$, where σ_0 is the spectral line center (Vanasse, 1967).

Thus, in the optical path difference domain, the effect gives an additional, wavenumber dependent, apodization term $\text{sinc}(z\sigma_0\Omega/2)$ to be multiplied by the standard boxcar function extending from $-z_{\text{max}}$ to z_{max} . The dependency on wavenumber of the apodization function makes the exact treatment of such an effect a difficult task in the case of a broadband spectrum. A possibility is to consider σ_0 a constant, equal to the central wavenumber of the operating spectral band.

15 Moreover, if $\pi/\sigma_0\Omega \gg z_{\text{max}}$ the solid angle contribution to the ILS is small, and can be approximated with a triangular component in the apodization. The resulting apodization function can thus be treated as a linear combination of a boxcar and a triangle function with α and $1 - \alpha$ coefficients, where $\alpha = \text{sinc}(z_{\text{max}}\sigma_0\Omega/2)$.

20 This is a rough approximation with respect to the exact mathematical treatment of the ILS function, but since in normal instrumental operating conditions the deviations from the “ideal” ILS are very small, the effect of the approximation is negligible, and the calculation of the ILS is much faster since it makes use of the two simplest apodization functions.

REFIR-PAD ILS has been analyzed through hot ~~black-body~~ blackbody calibration measurements in which ~~an~~ isolated water vapor ~~line-lines~~ coming from residual humidity in the instrument ~~has-have~~ been identified. ~~The feature is~~ These features are weak enough to be far from saturation, and ~~has-have~~ a natural linewidth negligible with respect to ILS(~~see~~. In Figure 4, ~~blue line~~) it is shown the result of this analysis for two different lines, one in the FIR region, at 526 cm^{-1} , and one at the edge of the REFIR-PAD operating region, at 1430 cm^{-1} . The top panels in Figure 4 (red lines) correspond to acquisitions performed with a 0.25 cm^{-1} spectral sampling, the bottom panels (blue lines) to a 0.5 cm^{-1} spectral sampling.

The measured lines are fitted with the $\alpha \cdot \text{sinc} + (1 - \alpha) \cdot \text{sinc}^2$ approximated lineshape, corresponding to the combination of a boxcar and a triangular apodization, obtaining the corresponding value for α .

30 The α coefficient ~~can be also retrieved~~ has also been retrieved, as a function of wavenumber ~~through the analysis of wide band spectra in which narrow atmospheric lines can be isolated~~, for several other different spectral lines. The result of this kind of analysis is shown in Figure 5, where average α values are plotted vs. ~~wavenumber for two~~ wavenumber. Two different series of measurements ~~, performed with a nominal resolution of~~ were analyzed: some performed with 0.25 cm^{-1} (red circles) and

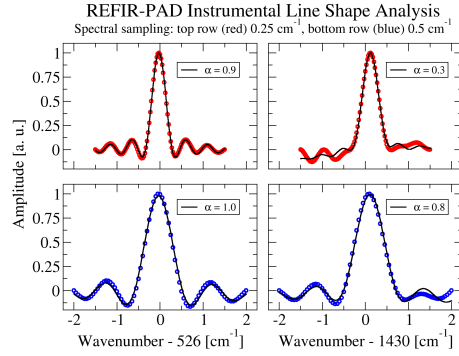


Figure 4. REFIR-PAD instrumental line shape. Blue line shows the isolated atmospheric line used for the analysis, the instrumental line shape is a linear combination of sinc and sinc² components.

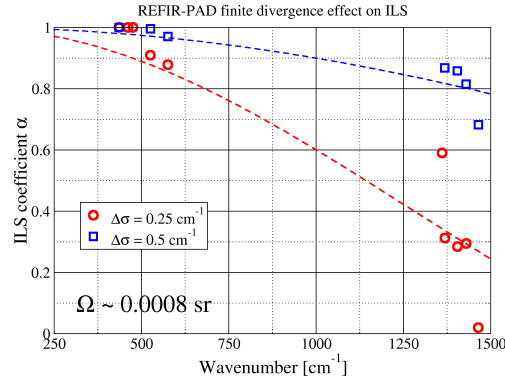


Figure 5. REFIR-PAD instrumental line shape coefficient obtained through analysis of measured spectra for 0.25 and 0.5 cm⁻¹ nominal resolution. Continuous lines show the sinc($z_{\max}\sigma\Omega/2$) theoretical behaviour.

others with 0.5 cm⁻¹ (blue squares) spectral sampling. The theoretical expression, $\alpha = \text{sinc}(z_{\max}\sigma\Omega/2)$ is also plotted, with the Ω value fitted to the experimental data.

Both the datasets provide the same Ω value, as expected, also, the fitted value (0.0008 sr) is smaller than the theoretical beam divergence given by the optical design (about 0.0027 sr), but in good agreement with the actual value of 0.00087 sr calculated taking into account the limitations in coupling efficiency due to the finite distance between Winston cones output aperture and detectors (see Section 2).

It should be noted that at low wavenumbers the solid angle contribution is completely negligible, but even in this case the line fitting gives an α value lower than 1 (typically about 0.95). This can be explained with the fact that there are other contributions to the ILS (residual misalignment, optics planarity, scanning mirror movement irregularities) that can give a residual contribution that is visible when the main-solid angle effect is negligible.

We also observe that, since in case of a small amount of interferometric misalignment the effect on the ILS can be approximated at the first order with an increase of the sinc^2 component, it is possible to treat the interferometric misalignment in level 2 data analysis through fitting the $\text{sinc}/\text{sinc}^2$ ratio as an extra parameter (see Section 10). This is a very useful feature in the case of remote operation in extreme environments, ~~a situation~~ an operating condition in which a slight misalignment is always
5 a possibility.

4 Detectors and data acquisition electronics

One of the defining characteristics of the REFIR-PAD spectroradiometer is the use of room-temperature detectors to cover the ~~far-to-middle-infrared~~ middle to far-infrared spectral range. This result is obtained through the use of high-sensitivity Deuterated L-Alanine doped Triglycine Sulphate pyroelectric detectors provided by BAE-Selex (models P5315 and P5541).
10 Specifications for the P5315 (P5541) at $f = 100$ Hz are: Detectivity $D^* = 5.0 \cdot 10^8 (5.3 \cdot 10^8)$ $\text{cm}\sqrt{\text{Hz}}/\text{W}$, Responsivity 1250 (450) V/W.

The detector active area diameter is 2 mm for P5315 and 1.5 mm for P5541. To enhance the light-gathering ability of the detectors, Winston cone concentrators are mounted in front of them (see Section 2).

The detectors are specified for 10-3000 Hz operating frequency range. In standard operating conditions ($3.3 \cdot 10^{-2}$ cm/s OPD
15 scanning speed, $100\text{-}1500$ cm^{-1} spectral range) the REFIR-PAD instrument operates in the 3.3-49.5 Hz frequency interval. This is partially outside of the low end of the specified operating range, thus an accurate characterization of the detector system is required.

The typical frequency response of a pyroelectric detector is characterized by “crossed” low and high cutoffs resulting in a strongly frequency-dependent amplitude and phase. The presence of a low frequency cutoff is rather an advantage in an
20 intrinsically AC-coupled application like FT spectroscopy, but, on the other side, a frequency-dependent dephasing constitutes a severe problem in a FT spectrometer, and must be solved by the use of a specifically designed preamplifier with a tailored response function in order to obtain a flat response and a very low dephasing across the operating frequency range.

In Figure 6 the ~~main characteristics~~ response of the detector and preamplifier ~~system are shown~~. ~~The response (top panel)~~ is measured in operating conditions, supplying to the detector an optical step function through the use of a laser and a shutter.
25 The resulting response function can be fitted with a mathematical model of the detectors two-pole response multiplied by the preamplifier electronics response in order to obtain an estimate of the actual frequencies of the detector poles. The fitted function is shown in figure as a dotted line, and is in a very good agreement with the measured data.

The values for the low and high frequency cutoffs obtained by the fitting process shown in Figure 6 are used, together with ~~a~~ ~~mathematical simulation~~ the mathematical model of the preamplifier response, to provide an estimate of the residual dephasing
30 to be used in the phase correction algorithm in the processing of level 1 processing of the interferograms (Bianchini, 2008a).

~~In the bottom panel of Figure 6 is also shown the noise spectrum at the output of the preamplifier as measured with a Stanford Research SR780 network analyzer, both with~~

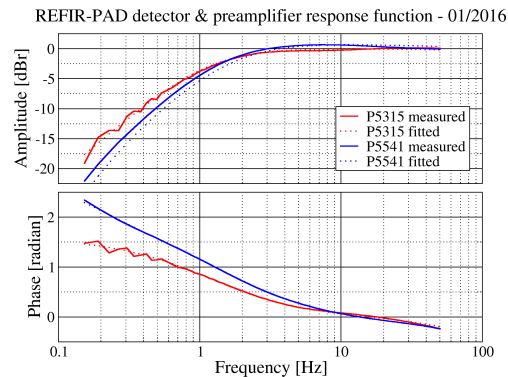


Figure 6. Top panel: REFIR-PAD detector preamplifier response as measured in normal operating conditions, along with a fit of the theoretical model used to measure the detectors characteristic low and high pass frequencies. **Bottom panel: noise characteristics of the detector and preamplifier system.**

5 Control and data storage system

The REFIR-PAD instrument features an on-board control unit that allows for autonomous operation (shown as a purple box in the mechanical layout shown in Figure 1).

The on-board control unit is based on a PC-104 industrial computer with a 486DX2 CPU operating at 100MHz and without connecting the detector, showing how in the operating frequency range of the preamplifier (between 32 MB of RAM. Storage is provided by a 64 GB SSD or, in alternative, a removable CompactFlash card slot (the use of which bypasses the SSD).

The on-board unit runs a streamlined version of Debian GNU/Linux v. 3.0 in which all the non-essential services have been disabled to reduce system disk access and thus increase robustness in case of loss of power. At system boot, after enabling networking, the REFIR-PAD control program is launched, immediately starting the data acquisition sequence.

This setup allows for compactness and robustness, and is ideal for the balloon-borne operation mode and for short ground-based campaigns: the SSD can store up to a month of continuous measurements, while the CompactFlash slot allows to easily retrieve data after a measurement run.

The permanent installation at Concordia station has instead required an upgrade of the control systems surrounding the REFIR-PAD instrument in order to provide continuous, unattended operation capabilities.

At Concordia station the REFIR-PAD instrument is installed indoors, in a shelter near the main base, enclosed in a thermally insulated box that is connected to an opening on the shelter roof by means of an insulated chimney. In this way, even if no window is used to separate the instrument from the outside environment, the shelter inside is kept protected from the outside air. The measurement port on the roof of the shelter can be closed by means of a motorized door when the instrument is not operated (and closes automatically in case of loss of power).

An autonomous microcontroller-based thermal control system is used to keep the instrument at a constant temperature (within ± 0.5 K) through a set of heaters and a fan-driven inlet tube extracting cool air from the bottom of the shelter. The

thermal control system is also provided of an Ethernet connection and can be remotely controlled and configured through a minimal web interface.

5 The REFIR-PAD FTS is remotely operated through a second computer placed in the shelter and connected with a direct point-to-point Ethernet link to the FTS on-board control unit. This control and storage computer can switch on power to the FTS, to the view port door and to the heating system. It does also share, through the NFS protocol, a 2 TB RAID-1 disk array which is mounted at boot by the REFIR-PAD on-board control unit in order to store the acquired data.

The normal operation sequence of this setup consists in the control and storage computer opening the measurement port, turning on REFIR-PAD and waiting for a preset interval (typically configured as about 5-6 h).

10 At the end of the measurement run, it shuts down REFIR-PAD through the network and proceeds to compress and archive the raw data in a time-stamped directory structure and finally to perform level 1 ~~and 100 Hz) the electronics give a contribution more than 20 dB below the detector noise~~ pre-processing.

This pre-processing step is needed in order to send to Italy the calibrated and averaged DLR spectra since the full amount of raw data produced by the FTS is too large for a direct transfer.

After the end of the data pre-processing, a new measurement run is started.

15 Together with REFIR-PAD data, the control and storage computer performs acquisition and storage of several auxiliary parameters ranging from weather parameters outside the shelter measured by a Vaisala WXT520 station to diagnostic temperature values coming from different sensors placed in the shelter and inside of the instrument box.

The control and storage computer is always on and can be accessed remotely, allowing for the complete control of all the acquisition parameters even when REFIR-PAD is not operating, since the configuration files reside on the RAID-1 disk array.

20 Advantages of this architecture are redundancy and fail-safe operation: in case of a malfunction of the control and storage unit the REFIR-PAD instrument can still operate autonomously within the 1 month data storage autonomy provided by the on-board SSD. The control and storage unit can be easily replaced with a pre-configured, identical, spare unit available in the shelter. On the other side, in case of a malfunction of the REFIR-PAD on-board unit, a serial console active at boot time and accessible from the control and storage unit allows for remote troubleshooting including Power-on Self Test monitoring and BIOS configuration.

25 The raw data amount produced by the REFIR-PAD instrument is about 40 GB/day (2 GB/day compressed), the corresponding level 1 preprocessing output is about 50 MB/day (12 MB/day compressed), an amount of data which can be easily transferred even with the low-bandwidth connection provided at Concordia station (512 kb/s maximum).

6 Radiometric performances

30 A direct estimate of the radiometric accuracy of the REFIR-PAD spectra can be obtained through the signal measured in a spectral interval in which complete atmospheric transparency is expected.

In the case of a high-altitude, extremely dry environment, this condition is achieved in the atmospheric window around 800-1000 cm^{-1} . ~~Specifically we selected~~

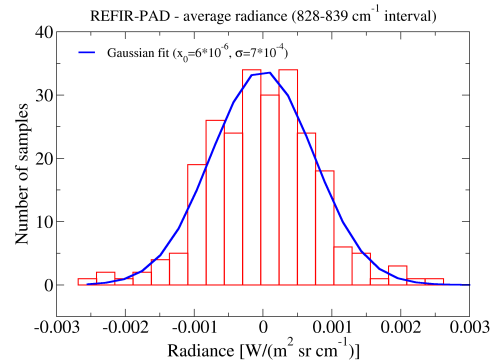


Figure 7. Statistical analysis of the average radiometric signal in a high transparency window (828-839 cm^{-1}) for RHUBC-II measurements. Radiometric bias is closed to zero, while the half width of the Gaussian distribution is 0.7 $\text{mW}/(\text{m}^2 \text{sr cm}^{-1})$.

Specifically we used the dataset acquired from the Cerro Toco site at about 5500 m a.s.l. in the Atacama region, Chile, during the RHUBC-II campaign (Turner, 2012). Of this dataset, we selected only measurements that have a PWV lower than 0.6 mm. In these cases the expected radiance signal in a narrow interval between 828 and 839 cm^{-1} in which interference due to water vapor lines and minor species is completely negligible with respect to the instrument accuracy, so this spectral region can be effectively used to check the instrument radiometric accuracy in the middle of its operating band.

In Figure 7 a statistical analysis of the distribution of the average radiance in the selected interval is presented.

Statistical analysis of the average radiometric signal in a high transparency window (828-839 cm^{-1}). Radiometric bias is estimated in about 0.2 $\text{mW}/\text{m}^2 \text{sr cm}^{-1}$, while the half width of the Gaussian distribution is 0.9 $\text{mW}/\text{m}^2 \text{sr cm}^{-1}$.

The distribution has been fitted with a Gaussian curve, obtaining a bias of about 0.2 $\text{mW}/\text{m}^2 \text{sr cm}^{-1}$ negligible offset and a standard deviation of about 0.9 $\text{mW}/(\text{m}^2 \text{sr cm}^{-1})$. The latter is in a good agreement with the *a-priori* estimate of the radiometric error obtained combining the noise equivalent spectral radiance (NESR) and the calibration error (Bianchini, 2008a): the estimated NESR in the selected spectral band is $<0.6 \text{ mW}/(\text{m}^2 \text{sr cm}^{-1})$ and the calibration uncertainty is $0.6 \text{ mW}/(\text{m}^2 \text{sr cm}^{-1})$, giving a total uncertainty (through root sum of squares) of about $0.85 \text{ mW}/(\text{m}^2 \text{sr cm}^{-1})$.

The much lower value of constant bias show shows that systematic errors in the calibration procedure are negligible with respect to the estimated radiometric uncertainty.

This method for checking the calibration accuracy doesn't provide a characterization through the whole spectral range, but can be continuously performed during a multi-year deployment of the instrument. An estimate of the calibration error covering the full spectral range can instead be obtained only with a dedicated measurement performed using an external reference blackbody (BB) placed on the instrument measurement port. Figure 8 shows the results of such a calibration measurement (red line in the top panel) compared with the reference BB calculated emission (black line in the top panel). In the bottom panel, the difference (gray line) is compared with the estimated measurement uncertainty (black line) and the BB calculated emission uncertainty (blue line).

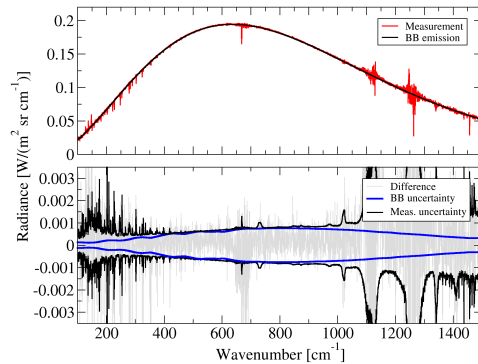


Figure 8. Measurement of a reference calibration blackbody sources at about 324 K.

The results show that the calibration accuracy is quite constant over the 300-1000 cm^{-1} spectral range. Below 300 cm^{-1} , and in correspondence of the beam splitter substrate absorption bands above 1000 cm^{-1} , the measurement errors are prevalent and it is difficult to quantify the actual calibration accuracy.

7 Spectral calibration

- 5 The use of a diode laser as a metrology source for the REFIR-PAD spectroradiometer has allowed for increased ruggedness and compactness of the system, this at the cost of a lower absolute stability of the reference.

The wavelength of a diode laser emission depends strongly on both the diode temperature and drive current. The unit used in REFIR-PAD features a specifically designed control unit providing both temperature stabilization and a high stability, low noise current drive. Besides temperature and drive current, diode lasers typically feature a large device-to-device wavelength variability. For this reason, once the reference source is installed and set up, its wavelength is calibrated and stored as a level 1 analysis software configuration parameter.

The main source of laser frequency error is due to thermal drifts in the temperature and current control and has been evaluated from the electronic component specifications in contributions of about 120 MHz/K (0.31 ppm/K) from laser current and 60 MHz/K (0.16 ppm/K) from laser temperature.

- 15 Assuming a maximum temperature fluctuation of 2 K, a safe estimate considering the performances of the instrument temperature control subsystem (see Section 5), we obtain a laser frequency error better than 1 ppm. This, in normal operation, allows for the use of a single frequency calibration even in case of long term measurements.

The observed laser frequency drift (see Section 11) is about <15 ppm/year, still low enough to allow to perform frequency calibrations monthly or even yearly. Nevertheless, a more robust automatic frequency calibration procedure has been developed to treat specific cases in which the above mentioned frequency stability cannot be reached, e.g. in case of laser mode jumps, or large temperature drifts of the instrument environment.

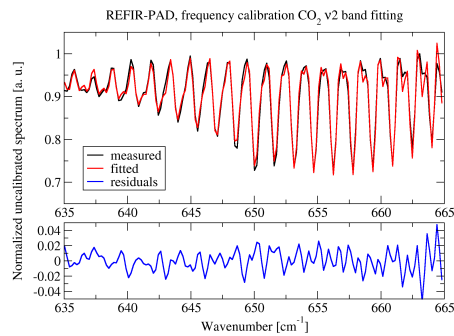


Figure 9. Result of the line fitting process used to perform automatic frequency calibration of the REFIR-PAD measured spectra.

The procedure is based on the line fitting of the residual absorption due to the CO_2 ν_2 band that is observed in the hot blackbody calibration measurements. This approach has been chosen in order to have a reference spectrum that is as independent as possible from the measurement conditions, so the calibration procedure has not to be adjusted according to the observed scene. Also, the absorption spectrum used in the procedure can be simply modeled using line strengths and the $\text{sinc} + \text{sinc}^2$ instrumental line shape (see Section 3). The downside of this approach is that a per-spectrum calibration cannot be performed, since a calibration coefficient is obtained only from the hot blackbody measurements. This does not constitute a limitation as long as the laser frequency drifts are negligible on the timescale of the calibration measurements repetition rate (about 10 minutes). In Figure 9 a sample result of the fitting process is shown.

Since the frequency fluctuation that a diode laser can experience can be quite large, a two step fitting procedure has been developed. First a simple peak finding algorithm is applied on the Q branch of the ν_2 band, then the fitting of the P branch in the $635\text{-}665\text{ cm}^{-1}$ spectral region is performed, as shown in Figure 9. The first stage of the process prevents, in case of a frequency drift that is larger than the P branch line spacing, a systematic error in the second stage due to the periodic structure of the spectrum.

The last step needed to perform the frequency calibration of the atmospheric measurements involves a linear regression in time of the frequency shift coefficients obtained from the hot blackbody measurements, the result of which is used to calculate the frequency drift correction for each of the atmospheric measurement.

In Figure 10 it is shown the effect of the automatic frequency calibration procedure in two different case studies. In both cases the frequency shift retrieved by the level 2 data analysis (see Section 10) is plotted with standard (blue curve) and automatic (red curve) frequency calibration.

During December 2014 (top panel) the reference laser showed bistable operation due to operating parameters being near to a mode jump. This caused the laser to operate on randomly one or the other of the two nearby modes. The separation between modes corresponds to a 400 ppm frequency shift (blue curve). After automatic frequency calibration it can be seen that the frequency shift coefficient variability (red curve) is reduced to the effect of measurement noise on level 2 analysis.

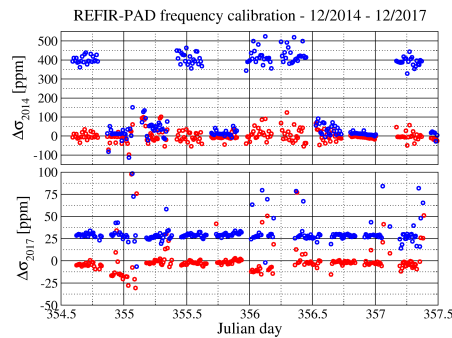


Figure 10. Effect of the automatic frequency calibration procedure. Blue circles represent the frequency correction factor retrieved by the level2 data analysis process with uncorrected data, red circles show the same parameter retrieved from automatically frequency-calibrated spectra.

In bottom panel it is shown the same method applied to a data set from December 2017, at the end of the 2 year period shown in Figure 18. While the overall effect observed is a general reduction of 25 ppm offset, it should be noted that the automatic calibration procedure itself induces fluctuations that can be as large as 10 ppm due to the accuracy of the fitting process.

8 ~~Spectroscopic performances~~ Instrument mathematical modeling

- 5 A simulation software has been developed with the intent of providing a tool to ~~better understand the behavior~~ estimate the expected performances of the REFIR-PAD interferometer. The code is written in MATLAB-compatible language, and takes into account all relevant elements of the instrument geometry and optical design. The main scope of this tool is to assist in the design and test of the beam splitters, and to identify and verify the configuration providing the best optical path compensation.

The simulation assumes a generic Mach-Zehnder design with two independent inputs and two outputs. The beam splitters are modeled as asymmetric multilayers characterized by generally different optical reflectivities for the two sides R_1 , R_2 .

In the simulation the two inputs can be associated to a blackbody source or to a synthetic spectrum provided by an atmospheric forward model, so in both cases a real function. The two sources are split according to the calculated complex transmission and reflection coefficients of the first beam splitter as obtained by the dielectric multilayer theory using the measured complex refraction indexes for the different layers in order to correctly represent bulk material absorption.

- 15 The emission of the first beam splitter, due to its non-null absorption, is also considered as an independent source. Beam splitter absorption is mainly caused by the substrate absorption bands, so it appears as a localized and easily identifiable effect.

The two arms of the interferometer are then recombined on the second beam splitter whose properties are calculated in the same way as for the first.

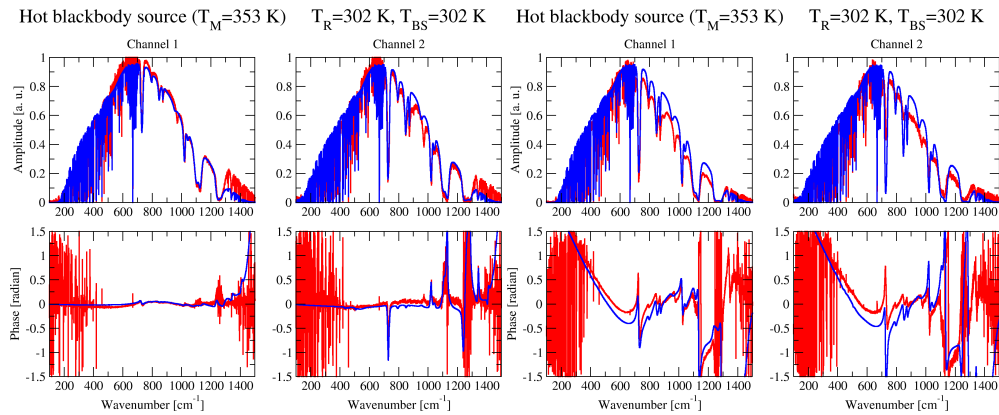


Figure 11. Simulation of the REFIR-PAD instrumental response function for different beamsplitter setups (blue line). Compensated (top 4 panels) and unbalanced (bottom 4 panels) configurations are shown. Laboratory measurements (red line) are compared with simulation outputs for the corresponding configuration.

Effect of the misalignment of interferometric components is calculated in the circular beam approximation using Bessel functions, planarity error is also modeled using simple approximations (spherical or trapezoidal deformation) and integrated on the beam profile.

The resulting complex spectrum is multiplied for a real absorption spectrum simulating the effect of air inside of the instrument (most of the absorption takes place outside of the interferometric path thus it doesn't produce dephasing) and the effect of the detector windows, obtaining the total signal incoming on both detectors. An inverse Fourier transform is applied to this signal to generate the simulated interferogram, which is then processed with the standard level1 data analysis chain used to process the REFIR-PAD measurements and described in detail in Bianchini (2008a).

In Figure 11 a comparison between measurements and simulation of an acquisition of the internal hot blackbody source is shown. ~~All the relevant features of the measured spectrum are well represented in the simulation, including the substrate absorption bands between~~ The four top panels show amplitude and phase of the signals observed on the two output channels in case of a setup in which the beam splitter coated surfaces are facing opposite directions. Red lines correspond to measured spectra and blue line to simulations. The bottom four panels show the same signals obtained in a configuration in which the beam splitter coated surfaces are facing the same way, i.e. the configuration occurring in the case a single, homogeneous, beam splitter surface is used both as beam divider and recombiner in the Mach-Zehnder interferometer. The tests were performed with the 0.85 μm Ge on 2.0 μm Mylar beamsplitter design.

It appears evident that the second configuration does not allow for a good compensation of the optical paths, as can be seen by the large oscillations in the phases. This improves greatly with the use of opposite-facing beamsplitters. It should be noted that, as the model confirms, the residual phase undulations that are still observed in the latter configuration come from small differences, of the order of few tens of nm, in the thickness of the layers composing the two beam splitters.

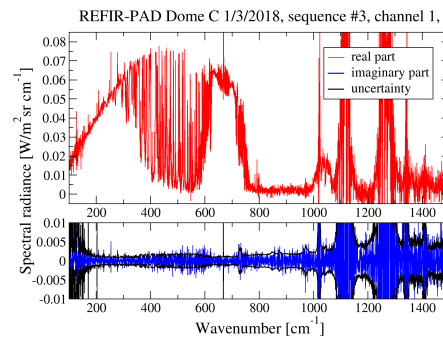


Figure 12. Real (red line), imaginary (blue line) and noise (black) for a typical zenith-looking calibrated spectrum.

On the other side, the sharp peaks observed around 700 and 1400 cm^{-1} and above 1000 cm^{-1} , and they originate from absorption bands in the Mylar substrate and impact both in the amplitude and phase of the measurements.

The minimum in interferometric efficiency near 1500 cm^{-1} that is due to the periodical characteristic of multilayer beam splitters (the tests were performed with the 0.85 μm Ge on 2.0 μm Mylar beamsplitters) is also correctly modeled. Actually the minimum is appears split in two due to the small differences in thickness between the two beam splitters, a behavior that is also correctly modeled, mentioned above.

Simulation of the REFIR-PAD instrumental response function for different beamsplitter setups (blue line). Compensated (top 4 panels) and unbalanced (bottom 4 panels) configurations are shown. Laboratory measurements (red line) are compared with simulation outputs for the corresponding configuration. The opposite-facing beamsplitter configuration, providing the best optical path compensation, is the one used in the REFIR-PAD instrument. This configuration gives, for each interferometer input, an output with almost complete compensation (channel 1 in figure 11) and one with at least partial compensation.

9 Level 1 products

The main data product of the REFIR-PAD spectroradiometer is the calibrated atmospheric emitted radiance integrated in the field of view of the instrument (a cone with an aperture of about 10°) and spectrally resolved with a 0.4 cm^{-1} resolution in the 100-1500 cm^{-1} range. The calibration procedure, described in detail in Bianchini (2008a) follows the complex calibration described by Revercomb et al. (1988). The onboard reference blackbody sources are simulated using a specific mathematical model shown in Palchetti (2008a).

Figure 12 shows a typical calibrated spectrum of the DLR (red line) acquired at Dome-C with an integration time of 5 min. The residual imaginary part of the spectrum, after calibration, is also shown (blue line), which is comparable with the estimated noise (black line) as expected.

The REFIR-PAD spectroradiometer has been operated in several campaigns in different environments (tropical, midlatitude, polar), and at different working altitudes, from about sea level to over 5000 m a.s.l. (Bianchini, 2007; Bhawar, 2008; Turner,

	<u>Date</u>	<u>Duration</u> <u>(UTC)</u>	<u>Int. time</u> <u>(min)</u>	<u>Rep. rate</u> <u>(min)</u>	<u>Spectral range</u> <u>(cm⁻¹)</u>	<u>Resolution</u> <u>(cm⁻¹)</u>
<u>Teresina, Brazil</u>	<u>30 June 2005</u>	<u>8:05–15:48</u>	<u>6.4</u>	<u>10.4</u>	<u>100–1100</u>	<u>0.475</u>
<u>Monte Morello, Italy</u>	<u>6 February 2006</u>	<u>16:26–17:58</u>	<u>5.1</u>	<u>7.7</u>	<u>350–850</u>	<u>0.5</u>
<u>Monte Gomito, Italy</u>	<u>13 – 14 March 2006</u>	<u>16:20–9:30 (+1)</u>	<u>6.1/9.9</u>	<u>9.2/15.7</u>	<u>350–1100</u>	<u>0.5</u>
<u>Testa Grigia, Italy</u>	<u>4 – 13 March 2007</u>	<u>6 days</u>	<u>5.1</u>	<u>11.0</u>	<u>240–1400</u>	<u>0.5</u>
<u>Breuil-Cervinia, Italy</u>	<u>15 March 2007</u>	<u>15:14–23:09</u>	<u>5.1</u>	<u>11.0</u>	<u>350–1400</u>	<u>0.5</u>
<u>Pagosa Springs, USA</u>	<u>22 – 29 April 2009</u>	<u>6 days</u>	<u>5.1</u>	<u>11.0</u>	<u>350–1400</u>	<u>0.5</u>
<u>Cerro Toco, Chile</u>	<u>21 Aug. – 24 Oct. 2009</u>	<u>37 days</u>	<u>5.1</u>	<u>11.0</u>	<u>100–1500</u>	<u>0.5</u>
<u>Testa Grigia, Italy</u>	<u>9 – 11 March 2011</u>	<u>3 days</u>	<u>5.1</u>	<u>11.0</u>	<u>240–1400</u>	<u>0.25</u>
<u>Dome C, Antarctica</u>	<u>since 21 December 2011</u>	<u>permanent</u>	<u>6.4/5.5</u>	<u>14.1/11.9</u>	<u>100–1500</u>	<u>0.4</u>

Table 1. Data available from the measurement campaigns performed by the REFIR-PAD instrument. Integration time corresponds to the actual acquisition time in zenith looking mode used to produce a single spectrum, while the repetition rate accounts for the total duration of the acquisition including calibrations and system overhead.

2012). Table 1 shows a list of the campaigns with some information about the available datasets. Of particular evidence is the dataset acquired at Dome-C, Antarctica (about 3200 m a.s.l), where the instrument has been acquiring spectrally resolved DLR in all-sky conditions since the end of 2011 (Palchetti, 2015).

In Figure 13, top panel, a set of calibrated spectra acquired in different atmospheric conditions is shown. Each spectrum correspond to an average of about 6 h of measurement in clear sky conditions. The measurements span about 2 orders of magnitude in terms of atmospheric total precipitable water vapor (PWV).

The REFIR-PAD instrument has also been operated in nadir-looking observation mode from stratospheric balloon platform (Palchetti, 2006), obtaining atmospheric emission spectra from a 38 km altitude, thus assimilablecomparable, for practical purposes, to the top of atmosphere (TOA) TOA condition. In Figure 13, bottom panel is shown a comparison between the TOA spectrum acquired during the flight and a ground-based zenith-looking measurement performed in similar condition (tropical atmosphere).

The measured spectral range includes almost all of the thermal emission from the Earth’s atmosphere. If we consider the far-infrared region (200-667 cm⁻¹), that is the main scientific target of the REFIR-PAD instrument, using the radiometric accuracy figures provided in Section 6 and the spectra shown in Figure 13, we obtain a relative uncertainty in the measurement of the total radiance which lies between 0.7% and 2%.

10 Level 2 products

The REFIR-PAD level 1 data products can provide plenty of information not only on the radiative properties of the atmosphere, but also on its structure and composition. To perform the retrieval of these variables, a software has been developed (Bianchini,

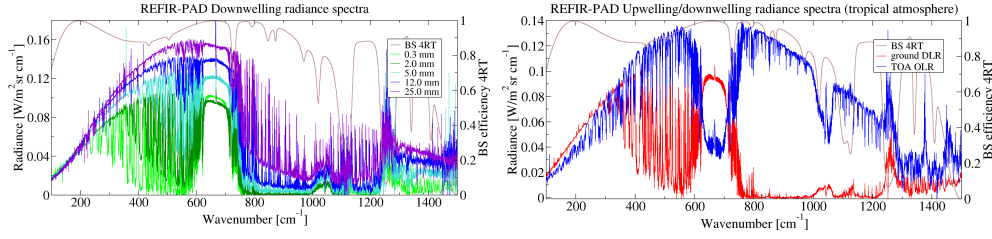


Figure 13. REFIR-PAD level 1 data products. Top panel: average zenith-looking spectra corresponding to about 6 h of data acquisition obtained in different atmospheric humidity conditions, spanning about two order of magnitude in terms of total precipitable water vapor (PWV). Beam splitter efficiency curve is also shown, to explain noise bands. Bottom panel: ground-based zenith-looking spectrum compared with top of atmosphere, nadir-looking measurement performed in tropical regions.

2011) that is based on the Line-By-Line Radiative Transfer Model (LBLRTM) (Clough, 2005) and the MINUIT minimization routines, part of the CERNlibs.

The software allows to retrieve temperature and water vapor content on separate vertical grids, together with extra parameters like columnar amounts of minor species, cloud optical thickness and instrumental parameters (as wavenumber calibration shift, instrumental line shape factor) and line shape coefficient α . The spectral range used in the process is a subset of the full REFIR-PAD spectral range, typically 350-850 cm^{-1} , even if some adjustments to the low-wavenumber end can be made according to the observed PWV ranges.

In detail the retrieval code makes use of the subroutine MIGRAD, which is based on the Davidon-Fletcher-Powell (DFP) algorithm, to minimize the chi square cost function given by:

$$\chi^2 = (\mathbf{y} - \mathbf{F}(\mathbf{x}))^T \mathbf{S}_y^{-1} (\mathbf{y} - \mathbf{F}(\mathbf{x})), \quad (1)$$

where \mathbf{x} and \mathbf{y} are the vector of the measurements and the state of the atmosphere respectively, \mathbf{F} is the forward model (LBLRTM version 12.2 in our case) and \mathbf{S}_y is the diagonal VCM for the measurements. The DFP algorithm is a quasi-Newton method which does not require the calculation of the jacobians at each iteration but uses an approximated form. This algorithm updates the inverse hessian matrix calculating the derivatives just at the first step and then using the iterative formula shown above. The same fitting approach which was applied in a previous works (Bianchini, 2011), was used in this paper. No *a-priori* information was assumed as regularly done in a Bayesian approach, such as optimal estimation, and the initial guess is represented by a local monthly climatology, obtained averaging over a set of radiosoundings daily performed at Dome-C. Since no *a-priori* information was used to constrain the solution and no regularization was introduced, to avoid the oscillation effects due to the ill-conditioning of the problem this approach requires to limit the number of retrieved parameters, hence the number of fitted levels both for water vapor and temperature profiles is equal to the number of degrees of freedom (DOF). The

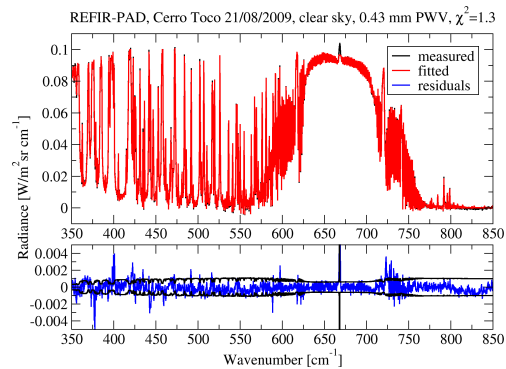


Figure 14. A typical result of the level 2 data analysis process. A single REFIR-PAD measurement is fitted using the LBLRTM forward model and the MINUIT minimization routines. Fitting residuals are compared with the total radiometric uncertainty (black line) in the bottom panel.

DOF were derived from a preliminary study performed through singular values decomposition of the Hessian matrix which includes Jacobian and the measurements noise.

A typical retrieval operates on a 4-point grid for temperature and a 5-point grid for water vapor, with retrieval levels chosen on the base of an analysis of the Jacobians of the selected variables. In Figure 14 the typical result of a fitting process is shown.

5 Even in this case adjustments to the retrieval grid can be made according to the observed atmosphere properties: as an example, in case of Antarctic measurements, the high atmospheric transparency and peculiar vertical structure (coming also from the perturbing effect given by the presence of the shelter in which the instrument is installed) allow for a retrieval of a 5-point profile also for temperature.

10 The vertical profiles of temperature and humidity obtained from the analysis of the set of zenith-looking measurement shown in Figure 13, top panel, are presented in Figure 15. These results show how the process can operate in a very wide range of atmospheric conditions.

15 In order to better reflect the atmospheric modeling performed by LBLRTM the fitted profiles are shown as histograms following the layering structure adopted in the forward model. The logarithmic scale adopted for the representation of the vertical profile reflects the logarithmic spacing used in the layering, which derives from the decrease of vertical resolution with height that is inherent in the zenith-looking vertical sounding geometry.

A better visualization of the products of the retrieval process can be obtained by plotting the profiles vs. time as color maps. In Figure 16 are shown the temperature and water vapor maps obtained for the September – December period in 2017.

20 The profile maps presented in Figure 16 show the transition to Antarctic summer, with the onset of a diurnal cycle for the temperature inversion, cycle that can be correctly resolved and characterized with the 12 minutes repetition rate of REFIR-PAD measurements.

The PWV is also provided as a level 2 data product, the accuracy in the determination of the PWV depends on the atmospheric conditions (total amount of water, presence of clouds) and ranges from 10-20% in the extremely dry conditions found

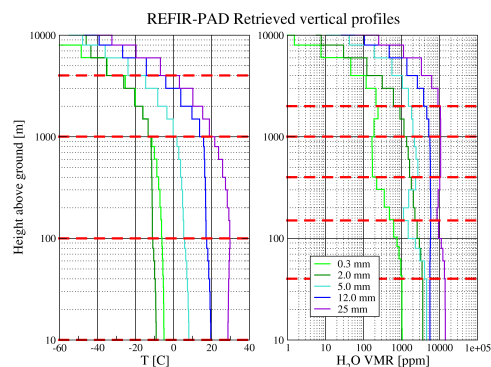


Figure 15. Vertical temperature and water vapor profiles obtained from the spectra in Figure 13, top panel, through the level 2 data analysis process. Red dashed lines show the selected fitting layers for temperature and water vapor.

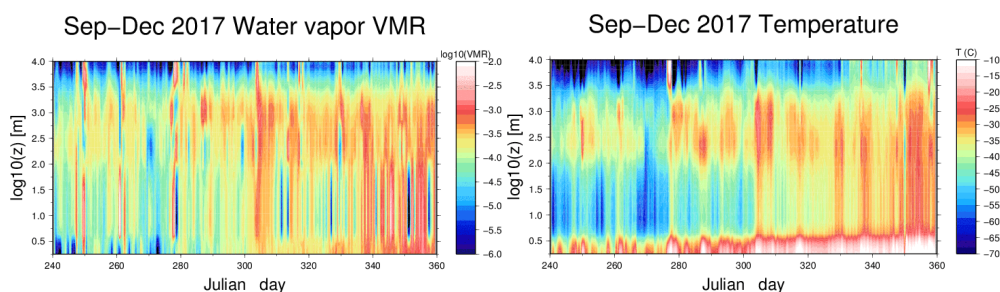


Figure 16. Vertical temperature and water vapor profile maps covering the September – December, 2017 period.

in Antarctica to about 5% in mid-latitude atmosphere. Accuracy on the total PWV has been estimated through the error on water vapor column fitting, and validated with a microwave radiometer (Fiorucci, 2008; Bianchini, 2011).

Columnar amount of other tropospheric minor species with spectral lines in the REFIR-PAD measurement range can also be retrieved, nitrous oxide for example. Methane also could be easily retrieved, but its main feature lies on the absorption band is obtained by adding an extra fit parameter which rescales the vertical N_2O profile in the temperature and water vapor fitting process, making use of the 589 cm^{-1} spectral band. In figure 17, bottom panel, it is shown a sample time series obtained from measurements performed in the September, 2017 – April, 2018 period.

It should be noted that a similar approach could be also applied to methane, provided a suitable spectral window containing methane absorption features is added to the retrieval range (differently from nitrous oxide, methane absorption is not present in the $350\text{-}850\text{ cm}^{-1}$ interval used for standard water vapour and temperature retrieval). Anyway, it must be taken into account that methane main absorption features overlap with the absorption bands of the Mylar beam splitter substrate, so a different beam splitter design (e. g. using based on Polypropylene) would be needed for an efficient methane total column retrieval.

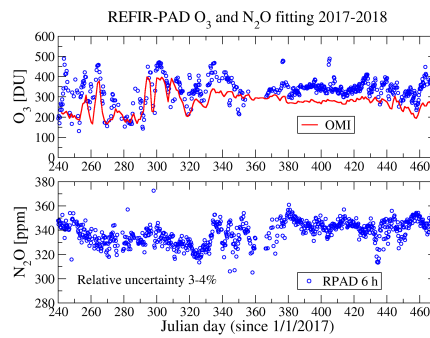


Figure 17. Time series of Ozone and Nitrous Oxide columnar values retrieved from The REFIR-PAD measurements acquired in the September 2017 – April 2018 period. For reference, corresponding Ozone values retrieved from OMI measurements on the Dome C region pixel are also shown.

A different consideration must be made for ozone column retrieval: while a strong ozone emission band is present in the REFIR-PAD operating spectral interval, most of the ozone lies in the stratosphere where the temperature retrieval, mainly relying on the Carbon Dioxide ν_2 band, has no sensitivity. Thus to correctly interpret the emitted radiance due to the ozone band, stratospheric temperatures must be provided as an external input. This can be done through radiosounding ~~, or through~~ or an auxiliary sensor as a stratospheric Raman LIDAR (Bianchini, 2014).

The ozone retrieval process makes use of the $920\text{-}1070\text{ cm}^{-1}$ spectral range. The retrieval grid, obtained through Jacobian analysis as in case of temperature and water vapor retrieval, features 3 fitted levels in the 12-24 km altitude range.

In Figure 17, top panel, are shown ozone columnar amounts obtained in the September 2017 – April 2018 period, together with the available NOAA OMI/OMPS ozone time series data, calculated for the ground pixel corresponding to Concordia station.

While a noticeable offset in ozone data is present and needs to be investigated further, the temporal variability is in good agreement with the satellite data, and the vertical variability observed in the retrieved 3-points profile shows a good correlation with the rapid variations in the columnar amounts. This can be explained with the fact that Dome C lays on the edge of the polar vortex region, so that it can enter and exit the vortex region depending on atmospheric transport.

11 Level 2 auxiliary outputs

The instrumental parameters obtained from the level 2 data analysis process provide also a valuable tool to characterize the quality of the measured spectra and the performance of the instrument. In Figure 18 it is shown the result of the analysis of the instrumental parameters in the 2016-2017 period. During these two years the REFIR-PAD instrument operated continuously without any maintenance operation.

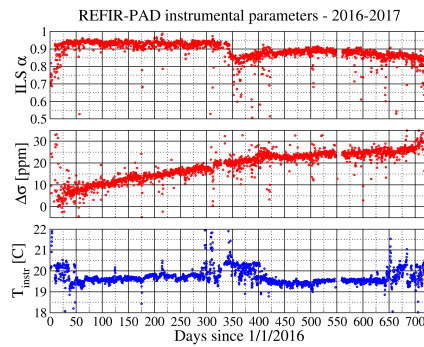


Figure 18. REFIR-PAD instrumental parameters for the 2016-2017 period. Top panel: ILS coefficient α . Center panel: laser frequency error $\Delta\sigma$. Bottom panel: Instrument temperature.

In December 2015 the laser source was replaced due to a malfunction inducing sudden mode jumps, and a laser frequency calibration was performed. Long term frequency stability of the laser source on the following two years can be evaluated from the laser frequency error $\Delta\sigma$, shown in Figure 18, center panel.

Laser frequency appears to be subjected to a slow drift that accumulated a total deviation of about 25-30 ppm since the initial calibration.

This behaviour derives mostly from laser diode aging, since it is not correlated with the instrument temperature (shown in Figure 18, bottom panel) as, instead, would be the effects due to the control electronics. The observed drift is also about an order of magnitude larger than the temperature drifts estimated using the calculated thermal coefficients (see Section 7).

The ILS coefficient α (top panel) also gives useful insights on the instrument performances in the selected period: it can be seen that during the summer season between 2016 and 2017 (the center part of the plot), larger than usual temperature fluctuations are present. This is due to the higher outside temperatures and also due to personnel working inside of the shelters, which is much more frequent during summer.

The temperature fluctuations impact on the ILS coefficient due to thermally induced optical misalignment, which is only partially recovered in the following winter season, so that a yearly optics check and realignment to be performed in summer is desirable even if not mandatory.

12 Conclusions

The REFIR-PAD spectroradiometer has proved to be a reliable and ~~relatively simple versatile~~ tool for the remote sensing of the radiative properties, composition and thermal structure of the troposphere.

The instrument is capable of providing a wealth of information with a measurement repetition rate of the order of 10 minutes, fast enough to resolve all the relevant atmospheric processes. ~~The provided~~, at least for what concerns the clear sky case which is the reference case in this work.

The currently available data products are:

- Atmospheric emitted radiance spectra in the 100-1500 cm^{-1} range with 0.4 cm^{-1} resolution and 0.85 $\text{mW}/(\text{m}^2\text{sr cm}^{-1})$ accuracy.
- Tropospheric water vapor and temperature vertical profiles with up to 5 independently fitted points.
- 5 – Total columnar precipitable water vapor (PWV) with an accuracy ranging from 5% to 20% depending on the total humidity and atmospheric conditions.
- Columnar amounts of minor species as nitrous oxide and ozone.
- Cloud optical thickness in the atmospheric transparency window region (800-1200 cm^{-1}).

The instrument operates at room temperature, is fully autonomous and allows for complete remote control of ~~all-relevant~~
10 ~~settings~~the configuration parameters, thus is perfectly suitable for operation in remote and extreme environment, as demonstrated by more than 6 years of continuous operation in the Antarctic station Concordia.

It should be noted that this specific location provides itself an unique dataset, since no similar instruments are operating continuously in polar regions. Currently the REFIR-PAD instrument is operated in the framework of two different projects funded by the Italian Antarctic Program in the perspective of reaching at least a decade-long measurement time series.

15 Future outlooks include the development and test of new beam splitter designs to overcome the spectral band limitations posed by the use of a Mylar substrate. The development of Polypropylene-based beam splitters is currently in progress, and will allow to fully exploit the 1100-1400 cm^{-1} spectral region to add new products (e.g. methane) to the currently available ones.

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20 (PNRA) for the funding for the following research programs, that have allowed to perform REFIR-PAD measurements since December 2011 at Concordia Station, Antarctica: project PRANA (Proprietà Radiative del vapore Acqueo e delle Nubi in Antartide) 2009/A04.03 2011-2013, project COMPASS (COncordia Multi-Process Atmospheric StudieS) 2013/AC3.01 2013-2016, and the currently active projects DOCTOR (DOme C Tropospheric ObserveR) 2016/AC3.02 and FIRCLOUDS (Far Infrared Radiative Closure Experiment For Antarctic Clouds) 2016/AC3.03.

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