amt-2018-87-RC1 comments response

Overall comments

The comments from the referee were minor annotations/changes to be implemented in the article. All were considered and fixed accordingly.

amt-2018-87-RC2 comments response

All changes implemented are marked in red in the revised article.

Overall comments

Comment #1: The referee pointed out the lack of quantitative conclusion on the photocurrent estimation.

Response : The method was refined by allowing the model to adjust the photoelectric yield and the altitude of the molecular absorption and a much better fit was obtained on the measurements from Robertson et al. (2014). The residual showed a sinusoidal pattern versus height, with +/- 300 pA amplitude. This was set as the limit for which the method can be applied. Similar results are seen in the flight data from April 2018 (to be published separately).

Comment #2: The referee mentioned that the photoelectric yield is greatly dependent on the material preparation (surface, oxidation, alloy, contamination, etc..) and ask if these conditions were known for both the aluminium plate from Robertson et al. (2014) and the materials reported by Feuerbacher and Fitton (1972).

Response: We fully agree with the comment, and agreed that such information was missing in our article. More information on how the material was prepared by Feuerbacher and Fitton (1972) was included, although some information is still missing (type of alloy, surface roughness). As for Robertson et al. (2014), no information could be found in their article. Overall, we tried to emphasis the importance of these properties and stress the lack of detailed knowledge about them.

Comment #3: The referee asked for some guidelines based on our results for building future instruments.

Response: We added a part in the conclusion section suggesting pathways for instrument design and testing based on our results.

Minor comments

Abstract, line 18: As opposed to the abbreviation MSPD, the abbreviation MSP has not been defined.

→ Added

Page 2, line 2: add "to" after "referred"

→ Added

Page 2, line 4: "subject to" instead of "subject of"

→ Corrected

Page3, line 4, and several other places in the manuscript: The authors refer to upcoming sounding rocket campaign PMWE during Spring 2018. By now, this campaign has taken place. I therefore recommend to update these text passages in the manuscript. (However, I would not ask the author to refer to any results from that campaign.)

→ More information added, stating the two flight from April 2018 and the two upcoming flights scheduled for 2019.

Page5, line 8: The authors state that molecular oxygen densities can vary by a factor 2 in the atmosphere. They should specify what altitudes they refer to.

→ This was a mistake (at least below 150 km, which is our region of interest). The molecular oxygen density between 60 and 100 km varies by +/- 20% between the low and high solar and geomagnetic activities cases. This was corrected for in the text, and illustrated by a new figure as well.

Page 5, line 26: It is unclear what is meant by "the height of the corresponding atmospheric column...". The sentence becomes more correct by simply removing the words "the height".

→ Corrected

Page 6: The authors argue that atmospheric (molecular Rayleigh) scattering is not important for their study.

This is correct. However, simply referring to the absorption and scattering cross section in figure 3 is not sufficient when making this argument. In principle, large amounts of (upwelling) scattered radiation from lower atmospheric altitudes (where the product of scattering cross section and number density is large) could contribute to producing the photocurrent. However, absorption by O2 (< 200nm) and O3 (> 200 nm) at lower altitudes prevents these contributions from becoming important.
→ We agree with this comment, and we thought our explanation in the text was clear enough to reflect this idea. We added more explanation by writting "absorption by O2 should dominate below 120 km, thus making the contribution from photons scattered below this altitude negligible".

page 8, line 8: It is confusing that the authors talk about transmission when it comes to solid surfaces. I recommend to replace transmission by absorption. Hence Absorption = 1 - Reflectance, rather than Transmission = 1 - Reflectance.
→ Changed accordingly

page 9, line 1: Define "quartic equation".
→ Added

page 9, Section 2.4: Is reflection of radiation from the grid wires included in the simulation? This should be explicitly stated. In that case, how important is reflection from the grid wires? If it is not important, this would be an important message to other instrument modelers: in that case only the shadowing effect of the grids would be important to consider in the radiative transfer.
→ We clarified this. The reflected rays are not considered, mainly because they are unlikely in this design of the detector. Only rays hitting the inner side of the grids could be reflected towards the electrode, but the inner side of the grids is partially shadowed by the grids themselves.

page 13: In the absence of the contamination issue, the spectral flux of photons to the MSPD would be well defined based on the absolutely calibrated light source and the known transmission curve of the filter. There would be no need for the photodiode. Hence, the reason for using the photodiode is the contamination issue. Do I understand that correctly? This should be clarified in the text.
→ More explanation added. The photodiode was mainly here to monitor change of the light source intensity over time (e.g. due to temperature). It is true that if the light-source is perfectly calibration there is no need for a photodiode. However, it is always useful to monitor the flux, and was even more due to the contamination problem.

page 13, line 21: I would not call the wavelength responses as "empirical", rather "assumed" or "estimated".
→ Changed

figure 12: Define "PEEK" in the caption.
→ Added

page 16, line 9: the authors refer to "two orders of magnitude". Figure 13a only shows a factor 3. Also: The relative decline in photocurrent and photodiode signal is very different in Figure 13 and Figure 14. This does not seem to be consistent. More explanations are necessary.
→ This was a mistake. Factor of three is correct. The difference in decrease rate between the electrode photocurrent and the photodiode current was also clarified. Basically, the photocurrent is more sensitive to shorter wavelengths (due to the shape of the yield), whereas the photodiode current is more sensitive to longer wavelengths (due to its sensitivity response). The contamination on the filter was most likely affecting shortest wavelengths more, hence reducing the photocurrent more compared to the photodiode current.

Table 2: The notation "estimated electrode photocurrent" is confusing. Please clarify.
→ Change to Calculated photocurrent based on the model.

page 19, line 10: The authors ask for "modern and reliable" measurements of material properties. I do not

like the implicit connection of these two words. 40 year old measurements are certainly not unreliable just because they are old. (And modern measurements made in 2017 or 2018 are not necessarily reliable.) Please change the wording.

→ We agree that this statement was not properly formulated. The "modern and reliable" was more referring to "open-access" or database compared to published curve without error bars. We changed it to "open-access accurate measurements".

Photocurrent modelling and experimental confirmation for Meteoric Smoke Particle Detectors onboard atmospheric sounding rockets.

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Abstract. Characterizing the photoelectron current induced by the Sun's UV radiation is crucial to ensure accurate day-light measurements from particle detectors. This article lays out the methodology used to address this problem in the case of the Meteoric Smoke Particle Detectors (MSPDs), developed by the Leibniz Institute of Atmospheric Physics in Kühlungsborn (IAP) and flown onboard the PMWE (Polar Meosphere Winter Echoes) sounding rockets in April of 2018. The methodology focuses
5 on two complementary aspects: modelling and experimental measurements. A detailed model of the MSPD photocurrent was created based on the expected solar UV flux, the atmospheric UV absorption as a function of height by molecular oxygen and ozone, the photoelectric yield of the material coating the MSPD as a function of wavelength, the index of refraction of these materials as a function of wavelength and the angle of incidence of the illumination onto the MSPD. Due to its complex structure composed of a central electrode shielded by two concentric grids, extensive ray tracing calculations were conducted
10 to obtain the incidence angles of the illumination on the central electrode, and this for various orientations of the MSPD with respect to the Sun. Results of the modelled photocurrent at different heights and for different materials, as well as for different orientation of the detector, are presented. As a pre-flight confirmation, the model was used to reproduce the experimental measurements conducted by Robertson et al. (2014) and agrees within an order of magnitude. An experimental setup for the calibration of the MSPD photocurrent is also presented. The photocurrent induced by the Lyman-alpha line from a deuterium
15 lamp was recorded inside a vacuum chamber using a narrow-band filter, while an UV-sensitive photodiode was used to monitor the UV flux. These measurements were compared with the model prediction, and also matched within an order of magnitude. Although precisely modelling the photocurrent is a challenging task, this article quantitatively improved the understanding of the photocurrent on the MSPD and discusses possible strategies to untangle the Meteoric Smoke Particles (MSP) current from the photocurrent recorded in-flight.

20 *Copyright statement.*

1 Introduction

Meteoric smoke particles (MSP, sometimes also referred to as meteor smoke particles) play an important role in the mesosphere/lower thermosphere (MLT) region. They interact with the D- and E-region ionosphere forming the dusty plasma which properties are currently subject to active research. MSPs originate from incoming meteor influx and the estimates of their input to the Earth's atmosphere ranges from several to hundreds of tons per day (Hughes, 1978; Love and Brownlee, 1993; Ceplecha et al., 1998; Cziczo et al., 2001; Wasson and Kyte, 1987; Mathews et al., 2001; Plane, 2004; Gabrielli et al., 2004; Plane, 2012). Since work of Rosinski and Snow (1961) the term MSP refers to solid state particles which are recondensed from evaporated meteoric material (see *e.g.*, Hunten et al., 1980, for more details). Both these processes (evaporation and recondensation) take place in the height range 70 to 120 km (*e.g.*, Hunten et al., 1980; Love and Brownlee, 1991; McNeil et al., 1998; Kalashnikova et al., 2000; Vondrak et al., 2008; Plane, 2004). The solid particles can further sediment and are even found in the Arctic ice (Gabrielli et al., 2004). The MSPs are also a subject to atmospheric advection and, therefore are influenced by neutral dynamics of the MLT region (see *e.g.*, Megner et al., 2006). It is commonly believed that MSPs could serve as nuclei for heterogeneous nucleation of mesospheric ice particles which cause the strong radar returns known as Polar Mesospheric Summer Echoes (PMSE) (see *e.g.*, review by Rapp and Thomas, 2006). There are a number of works suggesting that MSPs play a key role in formation of the Polar Mesospheric Winter Echoes (PMWE) similar to the mechanism including ice particles in summer for PMSE-formation (*e.g.*, Chen and Scales, 2005; Kavanagh et al., 2006; Belova et al., 2008; Kero et al., 2008; La Hoz and Havnes, 2008; Havnes and Kassa, 2009; Havnes et al., 2011; Mahmoudian et al., 2017). This hypothesis is supported by indirect measurements (*e.g.*, Belova et al., 2008; Kero et al., 2008; La Hoz and Havnes, 2008; Havnes and Kassa, 2009; Havnes et al., 2011), however a verification by direct in-situ measurements is still needed.

Considerable effort was put in the last decades to study the MSP properties (see *e.g.*, reviews by Baumann et al., 2013; Plane et al., 2014). First detected by ion mass spectrometer on board sounding rockets (Arnold and Viggiano, 1982; Arnold et al., 1982; Schulte and Arnold, 1992), their existence was later confirmed by other measurement techniques (Strelnikova et al., 2007; Fentzke et al., 2009; Rapp et al., 2010, 2012; Robertson et al., 2014). Remote sensing techniques as well as modelling rely on some assumptions on MSP's properties, which are poorly known. Thus, there are many open questions regarding the MSPs, like their size distribution, composition, shape, charge state, work function, photoelectric yield, etc. Microphysical properties of MSPs are difficult to measure because their size varies from tens of nanometers to less than a nanometer. It is known that physical properties of such tiny particles can significantly differ from those, of say μm-size (*e.g.*, Duft et al., 2015).

The most direct measurement technique to study MSPs are the so-called Faraday cup detectors carried by sounding rockets (*e.g.*, Havnes et al., 1996; Rapp and Strelnikova, 2009). These instruments, however are drastically affected by aerodynamics of the rocket flight, prohibiting detection of the smallest particles, normally below 1 nm-size (see *e.g.*, Horányi et al., 1999; Hedin et al., 2005, 2007; Strelnikova et al., 2009; Asmus et al., 2017). To circumvent this limitation, a new rocket-borne MSP-detector (MSPD) was developed at the Leibniz Institute of Atmospheric Physics (IAP) in Kühlungsborn, Germany (Staszak et al., 2017). Its design was inspired by the successful results obtained with the CONE instrument, which was designed as an aerodynamically improved TOTAL instrument (Giebeler et al., 1993; Strelnikov et al., 2013). The MSPD, shown in Figure 1,

consists of a central spherical electrode collecting current from the electrically charged MSPs, shielded by two electrically biased concentric grids (*e.g.* +6 V and −6 V) repelling the ambient ions and electrons. The geometry was optimized to reduce aerodynamic and bow-shock effects, as these effects directly determine the minimum mass required for the MSPs to reach the central electrode, therefore affecting the estimation of the MSP density. These MSP detectors will be part of a sounding rocket

5   campaign aiming at investigating PMWE, with the two first launches conducted in April 2018 from Andøya, Norway, and two additional flights scheduled for 2019.

    The photocurrent is another possible limitation of the detector: PMWE are predominantly observed during day-time, so that the measurements need to be conducted under direct sunlight. The photocurrent induced by solar UV radiation on vehicles in the Near-Earth environment is of the order of few nA/cm^2 (Feuerbacher and Fitton, 1972), which can be few orders of

10   magnitude larger than the current collected from MSPs. The characterization of the expected MSPD photocurrent prior to flight is therefore a crucial aspect of the instrument development, and is presented in detail in this article. The final goal is to provide strategies for interpreting the expected flight measurements, as the recorded current will be the sum of both the MSPs current of interest and the unwanted photocurrent. This endeavour was conducted by means of two distinct, yet complementary, ways: modelling and experimental measurements. An overview of a photocurrent model is presented in Section 2, which includes

15   an atmospheric absorption model for estimating the UV light intensity at various heights, the material properties for various possible surface coating of the detector, and a detailed ray-tracing simulation to quantify the complex illumination on the central electrode depending on the MSPD orientation. The experimental aspect is described in Section 3, where the experimental setup for measuring the MSPD photocurrent is presented. The setup includes a vacuum chamber, a deuterium UV light-source with calibrated spectrum from 115 to 170 nm, a narrow-band filter to select the UV range around Lyman-alpha (121.56 nm) and a

20   UV-sensitive photodiode for monitoring the UV flux. Finally, Section 4 gives a summary of both aspects and discusses ways to utilise them in the prospect of untangling the MSP current from the photocurrent recorded during the flight.

Figure 1. Meteoric Smoke Particle Detector with its central spherical electrode (26 mm radius) shielded by two electrically biased concentric grids (35 mm and 45 mm radius).

2   Modeling the photocurrent

The photocurrent is the result of the photoelectric effect (Einstein, 1905): high-energy photons at wavelengths from the ultra-violet and below are able to eject electrons from a material when absorbed, as the energy transferred from the photon to the electron is larger than the material work function, giving the excess as kinetic energy to the ejected electron. The photocurrent,

5   *i.e.* the number of photoelectrons ejected per second, depends on the spectral flux of photon illuminating the material, as well as on the material properties which determine its interaction with the photons.

2.1   Ultraviolet spectral flux as a function of altitude

The first step for estimating the MSPD photocurrent during flight is to determine the spectral flux illuminating the detector as a function of altitude. All photons considered are originating from the Sun, and its UV spectrum is well characterized by space-

10   borne instruments. The major feature of the solar UV spectrum is the Lyman-alpha line at 121.56 nm, with its spectral intensity being more than two orders of magnitude larger than the UV continuum. The continuum decreases drastically for wavelengths below Lyman-alpha, and as the photocurrent induced by near-UV photons is negligible for most materials, only the spectral region from 115 to 300 nm is considered to be relevant for modelling the MSPD photocurrent. The reference solar UV flux considered for the modelling was taken from the SOLSTICE instrument onboard the SOlar Radiation and Climate Experiment

15   (SORCE) spacecraft (Rottman et al., 2005). This measurement was taken on July 30th 2006, approximatively one solar cycle ago to roughly represent a similar solar activity as expected during the forthcoming launch. For each height, the number of each spectral photons is reduced by atmospheric absorption depending on the atmospheric column along the photon trajectory.
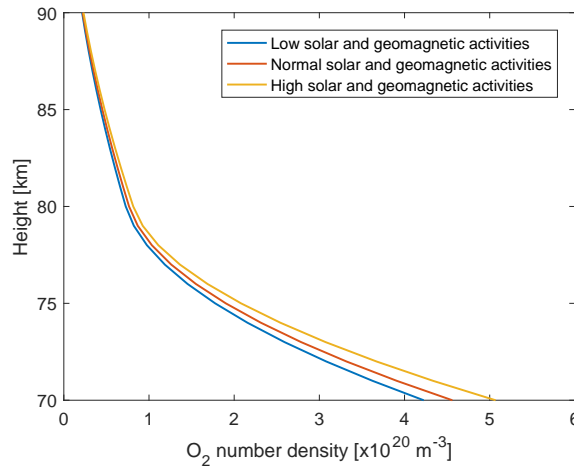
Figure 2. Comparison of O_2 number density between 70 and 90 km altitude, based on the NRLMSISE-00 atmospheric model.

Atmospheric absorption in the UV is mainly the result of molecular oxygen O_2 at heights below 150 km and for wavelength below 200 nm, and of ozone O_3 in the whole UV range becoming significant at heights below 70 km. The spectral absorption as a function of height can be estimated knowing the density (as a function of the height) and the absorption cross-section (as a function of the wavelength) for each of these two molecules.

5   The NRLMSISE-00 atmospheric model (Picone et al., 2002) was used to obtain the atmospheric density of molecular oxygen, following the parameters suggested by the COSPAR international reference atmosphere (CIRA-2012). Although the atmospheric density of molecular oxygen can vary by up to $\pm 20\%$ below 150 km altitude depending on the solar and geomagnetic activities as shown in Figure 2, calculations for both low and high activity scenarios did not show a significant difference in term of the resulting amount of photocurrent. The main absorption layer of the UV light by O_2 molecules, occuring at altitudes between 70 and 90 km (see Figure 8 in Section 2.4), was however shifted by up to few kilometers due to difference in the O_2 profiles. The low solar and gemagnetic activities scenario was therefore used as a baseline for the model, while the altitude was left as an optional adjustable parameter within few kilometers to accomodate for the solar and geomagnetic uncertainty. The atmospheric density of O_3 was taken from Bodeker and Hassler (2012), at the latitude of the Andøya rocket launch site in Norway (69.1144°N). Note that the variation of the ozone concentration due to the solar activity was not considered in Bodeker and Hassler (2012) but is not expected to impact significantly the photocurrent estimation in the presented case since ozone absorption mainly occurs below the altitude of interest for MSP measurements. The absorption cross section for O_2 was taken from Blake et al. (1966); Huffman (1985) and from Molina and Molina (1986); Huffman (1985) for O_3. It is important to notice that a proper treatment of the Lyman-alpha absorption is crucial for the modelling. For this reason, the precise absorption cross section of O_2 at the Lyman-alpha wavelength was taken from Ogawa (1968) and used to the two spectral bins (121 and 122 nm) in which all photons were considered to be from the Lyman-alpha line. This last point is a reasonable assumption, as the UV continuum in this wavelength range is orders of magnitude lower than the Lyman-alpha emission.

Using the atmospheric density $\rho(h)$ and absorption cross-section $\sigma(\lambda)$ of a given species, one can derive the amount of absorption at a given height by first calculating the absorption coefficient β at each height

$$\beta(h, \lambda) = \rho(h) \times \sigma(\lambda) \tag{1}$$

The total absorption coefficient β is obtained as the sum of all species considered, in the presented case β_{O_2} and β_{O_3}.

The solar zenith angle θ_z is also an important parameter, as it determines the atmospheric column above a given height. The Earth's curvature was considered when calculating the atmospheric column, which mostly affects high solar zenith angle condition by reducing the corresponding atmospheric column compared to a classical plan-parallel calculation of the atmosphere. To simulate a realistic atmosphere, the β coefficient representing the absorption is derived considering the atmospheric column along the line of sight, which depends on the solar zenith angle θ_z and the curvature of the Earth. The full geometry of the realistic atmosphere considered is shown in Appendix A.

The absorption optical depth τ is calculated by integrating the absorption coefficient β along the line-of-sight from each given height to the top of the atmosphere h_{top} (here considered to be 240 km) as shown in Equation (2).

$$\tau(h, \lambda) = \int_{h}^{h_{top}} \beta(h, \lambda) \mathrm{d}h \tag{2}$$

Finally, the number of photons at a given height is derived using the absorption equation

$$F(h, \lambda) = F(h_{top}, \lambda) \times e^{-\tau(h, \lambda)} \tag{3}$$

where $F(h_{top}, \lambda)$ is the solar UV flux at the top of the atmosphere.

Figure 3 shows the computed solar UV flux for various heights and for a solar zenith angle θ_z of 75° (around the expected solar zenith angle around mid-day and during spring at the launch site of Andøya). The resulting spectral distributions of photons at various heights are comparable with the ones presented by Huffman (1985).

Note that the contribution from scattered photons was not considered in the calculation. In this part of the atmosphere, the main scattering mechanism is Rayleigh scattering by air molecules (N_2 and O_2) which approximatively scales as λ^{-4}. Although one might expect it to be significant for VUV wavelengths, a comparison between the absorption and scattering cross-sections (Bucholtz, 1995) of the major contributors to both effects shows the opposite. Figure 4 shows that the Rayleigh scattering cross-section of air molecules is several orders of magnitude smaller than the absorption cross-section of both O_2 and O_3. Hence, absorption by O_2 should dominate below 120 km, thus making the contribution from photons scattered below this altitude negligible. Scattering from above this altitude can also be neglected due to the low density of molecules.

2.2 Material properties

The properties of the material are the second important aspect to be considered when estimating the photocurrent, as each material interacts differently with the incoming energetic photons. For any material, knowledge of two properties are required:
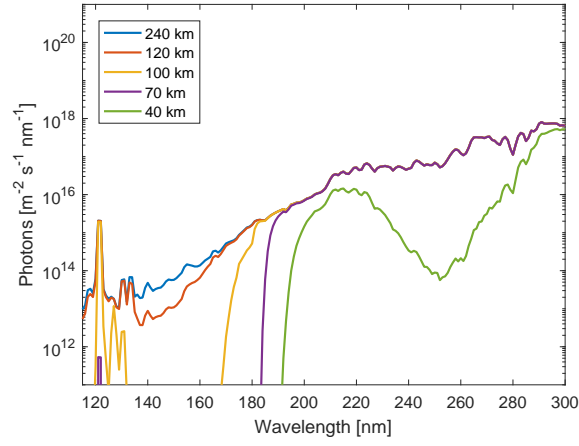
Figure 3. Spectral photon flux from 115 to 300 nm for various altitudes, for a solar zenith angle θ_z of $75°$.
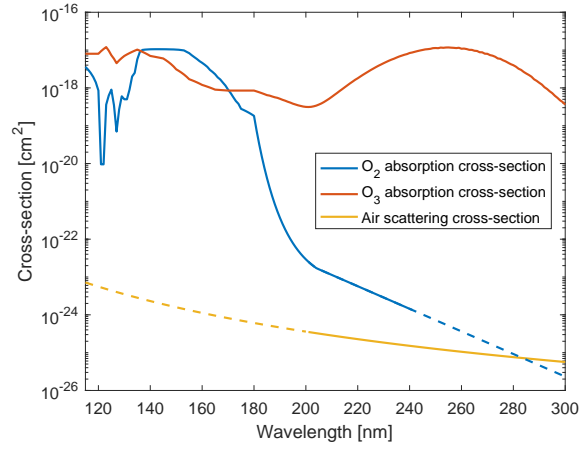
Figure 4. Comparison between the absorption cross-section of O_2 and O_3 with the scattering cross-section of air. Dash lines show the interpolated data.
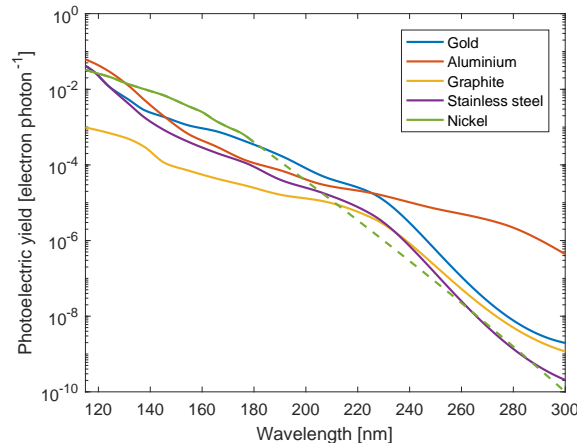
Figure 5. Photoelectric yield as a function of wavelength for the five different materials: gold, aluminium, stainless steel, graphite and nickel. Dash part of the nickel curve shows the interpolated data.

their photoelectric yield and their reflectance. The photoelectric yield is the probability for a photon with a given energy to eject an electron from the material. Indeed, although all absorbed photons transfer their energy to the electrons inside the material, most of the electrons are only excited inside the material and therefore do not contribute to the photocurrent. The reflectance gives the probability for a photon to be reflected from the material, depending on its angle of incidence θ_i. Reflected photons do not contribute to the photocurrent: only absorbed photons can transfer their energy to the material electrons.

Photoelectric yields for gold, aluminium, stainless steel and graphite are taken from Feuerbacher and Fitton (1972), and values for nickel up to 180 nm were obtained from Hinteregger and Watanabe (1952). The values used for these five materials are shown in Figure 5. It is important to notice that the photoelectric yield drops by almost two orders of magnitude from 121.5 nm to 250 nm. Hence, even if the solar spectral flux is higher in the near-UV compared to the Lyman-alpha line (see Figure 3), the contribution to the photocurrent from these near-UV photons is expected to be much lower than the contribution from the more energetic Lyman-alpha photons. In addition, material composition (*e.g.* alloys), preparation (*e.g.* freshly cut aluminium compared to oxide aluminium surface), intrinsic structure (*e.g.* lattice structure for crystalline materials) and surface roughness can have a large impact on the photoelectric yield. Gold and aluminium measurements presented by Feuerbacher and Fitton (1972) were evaporated film on glass substrate, exposed to ambient atmosphere for several days. The stainless steel surface was a clean polished one, and graphite was prepared as an atomically clean surface. No information about the alloy used for aluminium and stainless steel was given. Results for nickel from Hinteregger and Watanabe (1952) were obtained using a cathode but no additional information was given.
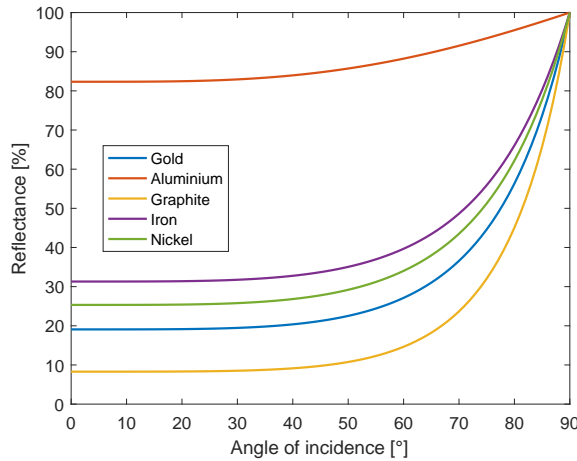
Figure 6. Reflectance at the wavelength of Lyman-alpha (121 nm) as a function of angle of incidence, for each of the five materials.

The total reflectance $R(\lambda, \theta_i)$ for these materials is the average of the two $R_s(\lambda, \theta_i)$ and $R_p(\lambda, \theta_i)$ reflectances for s and p polarization, respectively, which can be obtained from the Fresnel equations

$$R_s(\lambda, \theta_i) = \left| \frac{\cos\theta_i - n(\lambda)\sqrt{1 - n(\lambda)^{-2}\sin^2\theta_i}}{\cos\theta_i + n(\lambda)\sqrt{1 - n(\lambda)^{-2}\sin^2\theta_i}} \right|^2$$

$$R_p(\lambda, \theta_i) = \left| \frac{\sqrt{1 - n(\lambda)^{-2}\sin^2\theta_i} - n(\lambda)\cos\theta_i}{\sqrt{1 - n(\lambda)^{-2}\sin^2\theta_i} + n(\lambda)\cos\theta_i} \right|^2$$

(4)

where $n(\lambda)$ is the refractive index of each material as a function of wavelengths. Measurements of $n(\lambda)$ for gold, aluminium, graphite and nickel were taken from Hagemann et al. (1975), McPeak et al. (2015), Djurisic and Li. (1999) and Werner et al. (2009), respectively. Proper measurements of the index of refraction for stainless steel in the UV were not found in the literature, and values for iron measured by Werner et al. (2009) were used instead.

The absorption is obtained as $1 - R(\lambda, \theta_i)$. Figure 6 shows a comparison of the reflectance at Lyman-alpha for the five difference materials.

2.3 Illumination on the detector

A proper knowledge of the illumination's angle of incidence θ_i onto the MSPD is required for estimating the photocurrent. Ray-tracing simulations can provide a quantitative estimation of illumination across the detector surface given that a high enough spatial resolution for the grid is used. However, due to its complex geometry, modelling the instrument in a standard ray-tracing software was not possible and a custom routine was created instead. The central electrode was modelled as a sphere, and each wire composing the two concentric grids (hereafter referred as grid-wire) was modelled as a torus (98 in total). The ray-tracing calculations aimed at finding the intersection between a given ray (*i.e.* a vector) and each of the instrument surfaces

by solving a quartic equation (*i.e.* equation of the fourth degree) for each torus, and one quadratic equation for the central sphere. The resolution of the simulated grid of rays was 0.1 mm, which is small enough compared to the radius of the grid-wire radius (0.5 mm). In addition, only half of the MSPD was simulated thanks to symmetry, *i.e.* X-axis from 0 to +45 mm, and Z-axis from −45 to +45 mm. Although the MSPD is symmetric along two of its axes, a change in inclination (*i.e.* rotation of the detector around one of the two axes of symmetry) can result in a different illumination of the central electrode. This was investigated by performing calculation for seven different inclinations, from 0° to 90°. Such simulations are quite computationally-intensive: each run at a given inclination was composed of approximatively 320,000 rays and required about a week of computation on a 24-CPU node from the KTH PDC post-processing server. Figure 7 shows the resulting illumination for three different inclinations: 0°, 45° and 90°. Rays interacting with the central electrode are shown in red in Figure 7, and their angle of incidence with respect to the sphere can easily be obtained using the output from the ray-tracing simulation. Note that rays reflected by the grids towards the central electrode were not considered here. In this design of the detector, such rays are unlikely to have a significant impact as only the inner side of both grids could reflect photons back onto the electrode, and the inner sides are shadowed by the grids themselves.

2.4 Resulting photocurrent

The MSPD photocurrent can be obtained by combining how the UV photons at each height (Section 2.1) fall on the detector (Section 2.3) and interacts with its material (Section 2.2). The resulting photocurrent as a function of height is shown in Figure 8 for the five different materials at a 0° inclination. As expected from its photoelectric yield, a carbon coating produces the lowest photocurrent at heights above 80 km. Aluminium, nickel and stainless steel produce relatively similar photocurrent below 60 km, as most of the Lyman-alpha photons are absorbed by the atmosphere and their photoelectric yields in the near-UV are relatively similar.

Figure 9 shows the expected photocurrent of a stainless steel electrode (*i.e.* the base material of the MSPD) at an altitude of 85 km and for various inclination of the detector. As expected from its asymmetric design, the change of the photocurrent as a function of inclination is not straightforward due to the complex shadowing of the central electrode by the two concentric grids. In addition, the photocurrent can be seen to be much larger for the case at 90° compared to the other cases. This is most likely due to a perfect alignment of the two grids for this particular case, reducing the shadowing on the central electrode, and is expected to be less significant on the real detectors as both concentric grids are not as perfectly aligned together. Nevertheless, this is an important result as it confirmed the relationship between the recorded photocurrent and the instrument attitude, which could be used as an additional parameter to constrain the photocurrent from the MSP current during the analysis of the flight measurement.
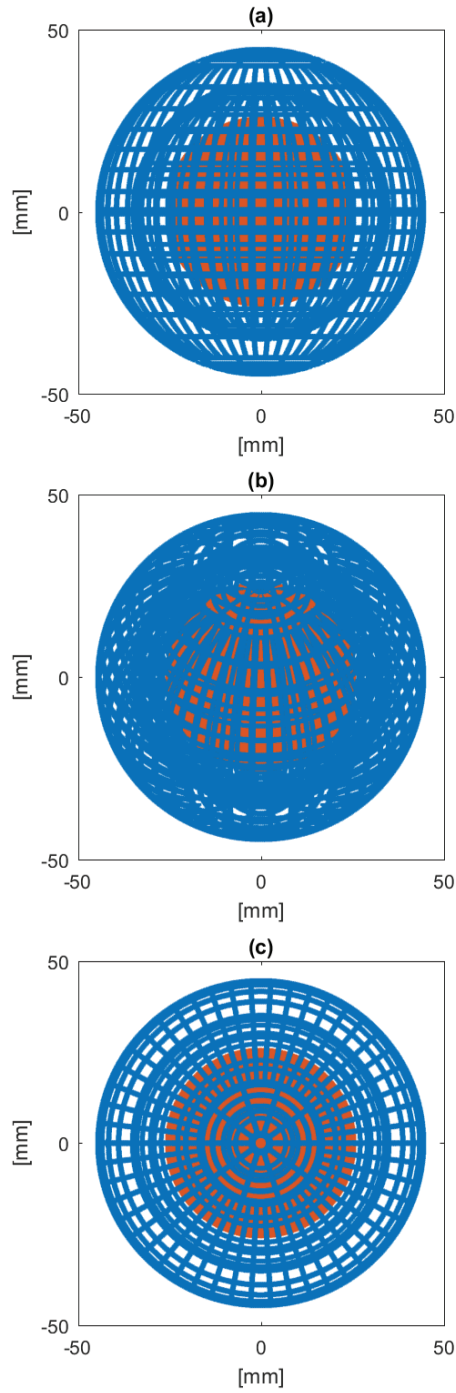
Figure 7. Illumination on the MSPD for an inclination angle of (a) $0°$, (b) $45°$ and (c) $90°$. Red shows the rays hitting the central electrode and blue the rays hitting the grids.
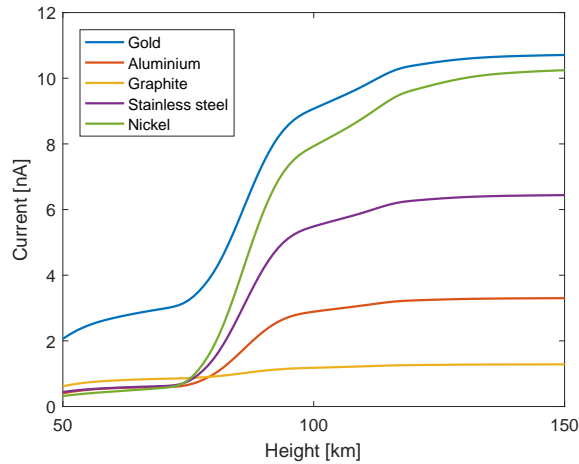
Figure 8. MSPD photocurrent at various heights for the five different materials, for an inclination angle of $0°$ and a solar zenith angle of $75°$.
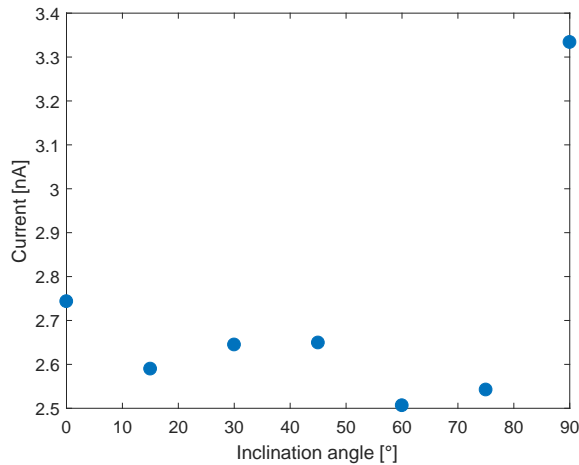
Figure 9. Photocurrent as a function of inclination of the MSPD detector at a 85 km altitude, for the seven different inclination angle simulated. The material considered is stainless steel and the solar zenith angle is $75°$.

2.5 Comparison photocurrent measurements from a sounding rocket flight

Robertson et al. (2014) presented photocurrent measurements recorded by a 20 mm diameter aluminium plate onboard the CHAMPS sounding rocket. The rocket was launched from Andøya on October 13th 2011 at 13:50 UT. The model was used to estimate the photocurrent emitted by such aluminium plate, using the solar spectral irradiance recorded by the SOL-
STICE/SORCE instrument on this particular day and assuming an almost normal angle of incidence on the plate (*i.e.* differences in angle of incidence from $0°$ to $30°$ can be considered negligible). Information about how the aluminium plate was prepared was not provided by Robertson et al. (2014), although one can probably assume a polished surface with oxidation from the ambient atmosphere. Figure 10 shows the results of the calculation, compared to the measurements from Robertson

et al. (2014) (see Figure 13 therein, here taken as the average of both the up-leg and down-leg measurements). Note that measurements below 700 nA/m^2 and above 96 km were not provided by Robertson et al. (2014). One can see that in the region of interest where MSP are expected, *i.e.* from 75 to 95 km, the decrease in photocurrent due to the Lyman-alpha absorption by molecular oxygen is reproduced by the base model (*i.e.* using an unshifted altitude range for the O$_2$ and O$_3$ profiles and

5   using the photoelectric yield of aluminium from Feuerbacher and Fitton (1972)), although the scaling is quite different. The base model underestimates the photocurrent above 90 km by a factor of five while slightly overestimating it below 80 km. The reason behind these differences is most likely due to the uncertainty of the photoelectric yield, as well as a small influence by the unknown true density profile of O$_2$ at these heights. These two parameters were left are free parameters in order to fit the photocurrent measured by the plate. Since the plate photoelectric yield was unknown, the measurement for aluminium was

10   taken for the overall shape of the yield and a power law scaling (*i.e.* linear trend in the log-scale curve) was used to adjust its slope. The resulting photocurrent profile is shown in Figure 10 whereas the adjusted photoelectic yield is shown in Figure 11 along side the yield of other metals from Feuerbacher and Fitton (1972). One can see that the model can provide a much better fit to the measurements with only a small +1.2 km offset of the model altitude, combined with an adjusted photoelectric yield about five times larger at Lyman-alpha, where most of the O$_2$ absorption occurs. Notice that the adjusted yield is comparable to

15   the measurements of other metals. Although these results are empirical, the altitude offset and adjusted yield are not completely unrealistic. As previously mentioned, the difference in the photoelectric yield might be due to contaminating material on the plate surface, as well as the purity and the surface roughness of the aluminium used. The residual between the fitted model and the measurements has a sinusoidal shape with a ± 300 pA amplitude and is shown in Figure 12. Such pattern in the residual is an artefact from the model not perfectly reproducing the photocurrent.

20   Considering the number of possible uncertainties, the base model was still able to reproduce the photocurrent within the same order of magnitude and with a similar absorption behaviour with respect to height. In addition, adjustment to the photoelectric yield and the height of the atmospheric density profiles allowed the model to fit the measurement with a ± 300 pA amplitude residual. Although this method is not perfect (*i.e.* one would ideally want to have a precise measurement of the detector photoelectric yield), such fitting of the model should still be able to detect MSP layers inducing current larger than 300 pA in

25   the 70 to 100 km altitude region in the case of the MSPD.

3   Experimental measurement of the photocurrent

3.1   Overview of the experiment and apparatus

The experiment aims at using a known UV spectral flux to illuminate the detector and monitor the resulting photocurrent on the MSPD. Ideally, a calibrated UV light-source in a monochromator setup can provide a precise wavelength selection of

30   the UV flux and allow for a detailed breakdown of the photocurrent as a function of the incident wavelength. However such configuration was not readily available and, for the purpose of keeping the cost low, narrow-band filters were used to select various UV wavelength-bands instead. Figure 13 shows the layout of the experiment. The experiment was conducted inside a 300 mm radius and 600 mm long vacuum chamber, to avoid absorption of the VUV light by the atmosphere.
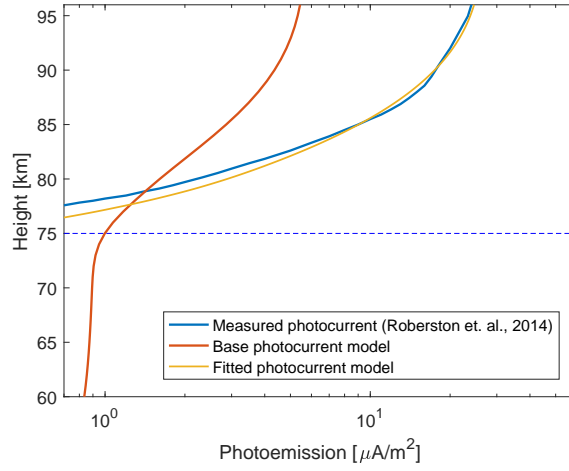
Figure 10. Photocurrent measurents from a 20 mm diameter aluminium plate taken from Robertson et al. (2014) (blue curve), compared to the computed photocurrent by the base model (red curve) and the model with adjusted yield and $+1.2$ km shift in altitude (yellow curve). Horizontal dash line shows the lower height limit for the expected MSP layer. The solar zenith angle considered for the calculation is 75°.
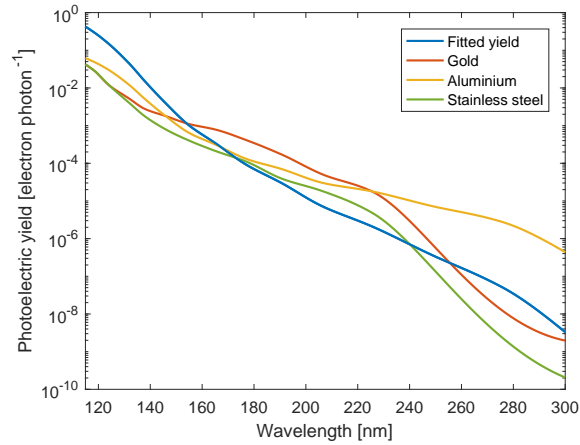
Figure 11. Fitted photoelectric yield compared to other metals from Feuerbacher and Fitton (1972).
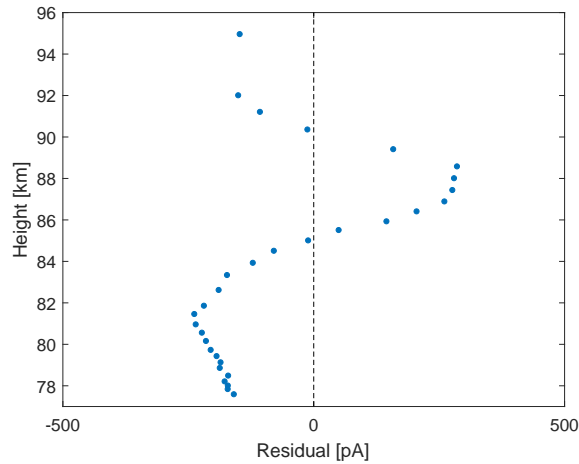
Figure 12. Residual between the photocurrent measurements from Robertson et al. (2014) and the fitted photocurrent model.
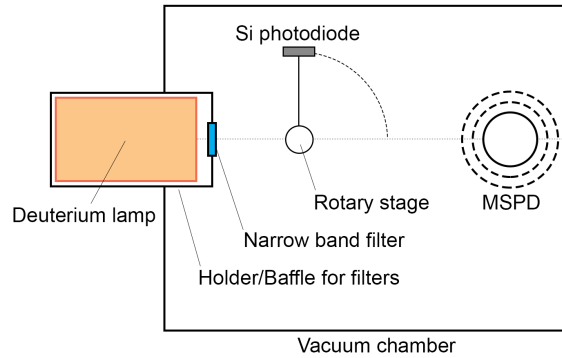
Figure 13. Layout of the experiment in the vacuum chamber.

The light-source used was an Heracles V01 Deuterium lamp which was calibrated by PTB (Physikalisch-Technische Bundesanstalt, the German national institute of metrology) back in 2011 for a previous calibration experiment (Ernst et al., 2011). Its normalized emission spectrum is shown in Figure 14a. Although the initial plan was to use four different filters centred around 121.5, 160, 200 and 250 nm to obtain the photocurrent in various passbands, no significant photocurrent was recorded when using the three latest filters. This was not due to lack of photons from the light-source in these spectral ranges but rather to the photoelectric yield of the material decreasing rapidly as the wavelength increases (see Figure 5), making the resulting photocurrent below the detection limit ($\sim$10 pA). Hence, only the Lyman-alpha filter was used during the experiment and its transmission curve is shown in Figure 14b. Finally, the VUV flux from the light-source was monitored using a silicon photodiode mounted on a rotary stage in order to move it either in front or away from the light-source beam. Monitoring the light-source flux was needed to estimate possible temperature related variation of the intensity as well as measuring the light-source stability, but also for estimating possible decrease in the flux due to contamination. Knowing the spectral response from

the photodiode and the incident spectrum via the light-source spectrum and the filter transmittance, it is possible to estimate the photon flux emitted by the light-source from the photodiode current. However, the manufacturer only provided the spectral response of the diode down to 148 nm, and the response for lower wavelengths was unknown. Figure 14c shows the spectral response down to 148 nm, as well as two empirical response for wavelengths down to 115 nm. The first case represents a monotonic decrease of the spectral response as a function of wavelength whereas the second case represents an insensitivity of the photodiode to lower wavelengths. Pictures of the experimental setup are shown in Figure 15.

3.2 Experimental measurements

Measurements were conducted for three different inclination angles of the MSPD: $0°$, $45°$ and $90°$. The initial plan was to record the photocurrent for additional inclination of the detector. However, large variations between multiple measurements taken at the same inclination were observed. These large variations were due to contamination on the Lyman-alpha filter, most likely caused by outgasing from the deuterium lamp socket, greatly degraded the VUV throughput over time as the light-source was operated under vacuum. An example is shown in Figure 16. One can notice the much larger decrease in the electrode current compared to the photodiode current. This suggests a larger absorption of the shorter wavelengths which are a larger contributor to the photocurrent but for which the photodiode is less sensitive. Note that a positive sign is adopted as convention for the electrode photocurrent, to be consistent with the calculation presented in Section 2.

To mitigate this issue, a rigorous cleaning of the filter using methanol was performed in between each measurement sequence taken at a given MSPD inclination. This effectively removed the contaminating material from its surface. The lamp MgF_2 window and the MSPD detector (inside an ultrasonic bath of ethanol) were also cleaned in between measurement sequences. The duration of each measurement sequence was kept below 15 minutes to minimize the time spent under vacuum and therefore limit the built-up of the contamination. Each measurement sequence was performed as follows: the light-source was switched on after reaching a pressure of 10^{-3} mbar and five minutes were allocated for its output light and current levels to stabilize. Then, a first recording of the electrode photocurrent was performed (each individual measurement consisted of 500 points recorded in about 1 min at a fixed bias using a Keithley 6430 sub-femtoamp remote sourcemeter). The photodiode was then placed in front of the beam and a recording of its current was performed. After that, a second measurement of the electrode photocurrent was performed, followed by a photocurrent measurement on each of the two grids, a second photodiode measurement, a third electrode photocurrent measurement and a final third photodiode measurement before switching off the light-source. Dark current measurements for the electrode, the two grids and the photodiode were also recorded with the light-source off and was around 10 pA for all surfaces. The biases used on the detector were the same as for one of the supposed flight configurations: central electrode grounded (in this case, to the chamber walls), inner grid at $+6$ V and outer grid at -6 V. Note that reaching a higher vacuum was not required for the purpose of the experiment, as the threshold for significant decrease in the photocurrent due to absorption was observed to be around 10^{-2} mbar. Figure 17 shows the results for the 15 measurement sequences taken during the experiment in chronological order, five for each of the three orientations tested. The degradation of the throughput over time due to contamination is seen between the three measurements of the electrode photocurrent recorded on each sequence, even though the time spent under vacuum was less than 15 minutes. This added a large measurement un-
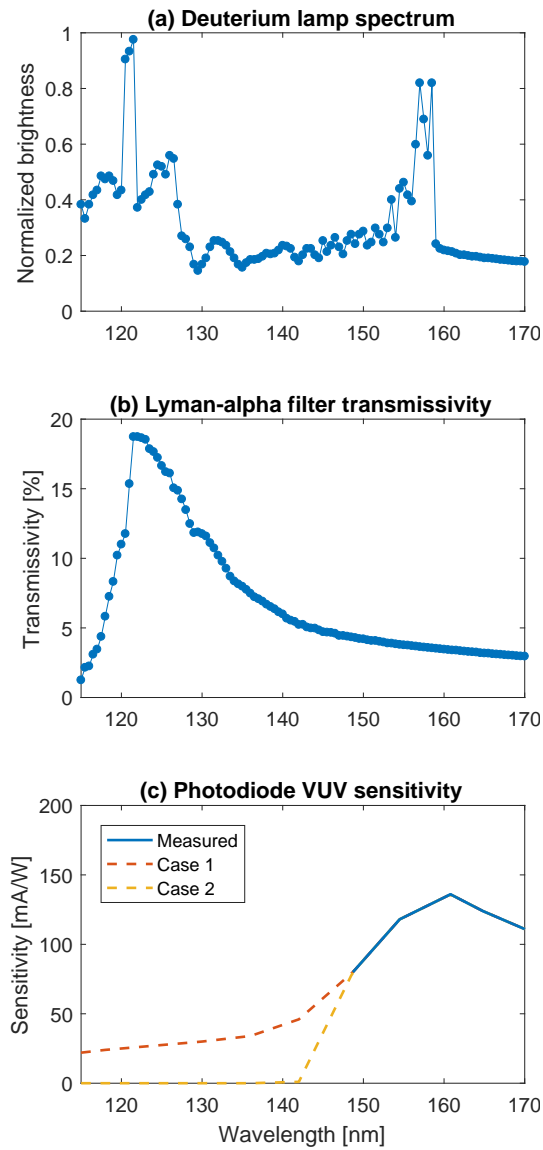
Figure 14. (a) Deuterium lamp spectrum measured by PTB. (b) Transmission curve of the Lyman-alpha filter. (c) Sensitivity of the photodiode, with the two different assumed cases below 148 nm.
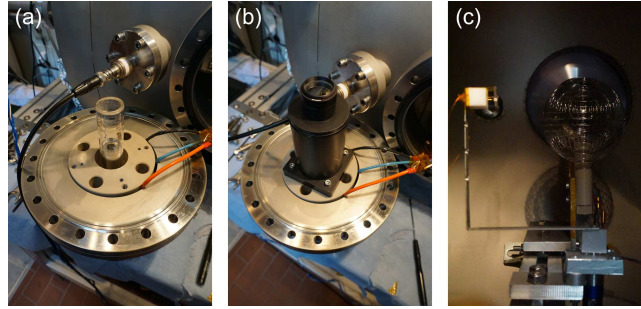
Figure 15. (a) Deuterium lamp spectrum inside its Polyether Ether Ketone (PEEK) holder. (b) Deuterium lamp covered with baffle and filter holder. (c) Setup inside the vacuum chamber, with MSPD in the background (0° inclination) and the photodiode on its rotating arm on the left.
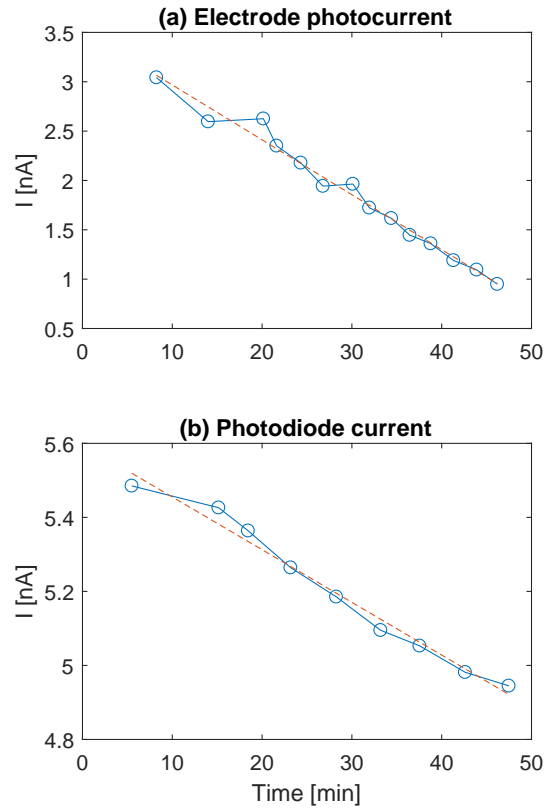
Figure 16. Decrease of (a) the electrode photocurrent and (b) the photodiode current over time suggesting a degradation of the UV throughput due to contamination on the Lyman-alpha filter. Time starts at the start-up of the light-source. Red dash line shows a linear fitting.
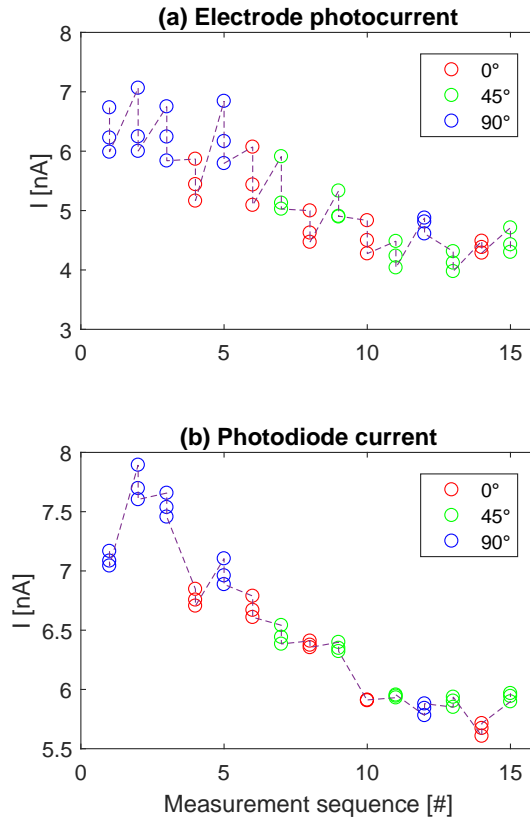
Figure 17. Results from the measurement sequences in chronological order for (a) the electrode photocurrent and (b) the photodiode current, for the three different inclinations.

certainty and for this reason, multiple measurement sequences were conducted for the same three inclination angles instead of measuring additional inclination angles. Moreover, a linear decrease on both the electrode photocurrent and the photodiode current can be seen between the different measurement sequences. This was interpreted as a residual contamination building up over time onto the filter surface, which could not be removed entirely by the methanol cleaning. Still, the cleaning was

5 very effective as Figure 16 showed that the throughput would otherwise be decreased by a factor of three after only 50 min of operation. Note that the current collected by the photodiode only decreased by about 10% compared to the much larger decrease of the electrode photocurrent. This can be interpreted as the shortest wavelengths (*i.e.* around Lyman-alpha) are more affected by the contamination compared to longer wavelengths which are also transmitted by the filter (see Figure 14b). These shorter wavelengths contribute more to the photocurrent whereas the photodiode is, by design, more sensitive to the longer

10 ones, hence the smaller decrease rate of the photodiode current compared to the electrode photocurrent.

An estimation of the uncontaminated signal was made by removing the linear trend from the degradation. Table 1 shows the averaged corrected electrode photocurrent and corrected photodiode current for each of the three inclinations, with their corresponding 1-σ errors calculated as the standard deviation of all fifteen measurements taken at a given inclination.

Table 1. Average electrode photocurrent and photodiode current for each inclination.

MSPD inclination	Photodiode current	Electrode photocurrent
0°	7.27 ± 0.12 nA	6.17 ± 0.39 nA
45°	7.45 ± 0.21 nA	6.34 ± 0.39 nA
90°	7.52 ± 0.32 nA	6.62 ± 0.42 nA

3.3 Comparison with modelling

The photodiode currents from Table 1 can be used to determine the VUV flux from the light-source. This current is the result of the integral of the light-source spectrum multiplied by the filter spectral transmittance and the photodiode spectral sensitivity. By normalizing the light-source spectrum, one can use the recorded photodiode current to scale the light-source spectrum and determine the number of photons emitted by the light-source at each wavelength (assuming the light-source spectrum is constant and not a function of other parameters such as the temperature). As previously mentioned, an uncertainty remained on the photodiode sensitivity for wavelengths below 148 nm, and two empirical cases were considered: a monotonic decrease of the spectral response as a function of wavelength and an insensitivity to lower wavelengths (see Figure 14c). The resulting spectral flux of photons from the light-source can then be input into the photocurrent model from Section 2 to estimate the expected photocurrent. Table 2 shows the expected photocurrent determined from the above described calculation, compared to the measured photocurrent from Table 1. One can see that, depending on the case for the photodiode sensitivity, the estimated photocurrent is between three to eight times smaller than the measured one. This is comparable to the photocurrent modelled by the base model for the aluminium plate as discussed in Section 2.5, which also underestimated the photocurrent by a factor from one to five. In addition, one can see that the predicted differences in photocurrent for the various inclinations is roughly similar to the error on the measured photocurrent, meaning that distinguishing between the different inclinations was unfortunately not possible based on the experimental measurements.

Table 2. Calculated electrode photocurrent based on the photodiode current from Table 1 and the ase model from Section 2, compared to the experimentally measured electrode photocurrent, for each of the three inclination angles tested.

	Calculated electrode photocurrent (case 1)	Calculated electrode photocurrent (case 2)	Measured electrode photocurrent
0°	0.81 ± 0.01 nA	1.85 ± 0.03 nA	6.17 ± 0.39 nA
45°	0.80 ± 0.02 nA	1.83 ± 0.05 nA	6.34 ± 0.39 nA
90°	1.00 ± 0.04 nA	2.32 ± 0.10 nA	6.62 ± 0.42 nA

4 Conclusion

The characterisation of the photocurrent induced by solar UV radiation is a crucial aspect of any plasma probe launched during day-time. A dual and complementary approach to the problem was presented by means of both modelling and experimental measurements in the particular case of a rocket-borne Meteoric Smoke Particle Detector (MSPD) currently developed at the IAP.

The details of the photocurrent simulation were presented, including 1) an atmospheric absorption model providing the spectral flux of photons from 115 to 300 nm at any given height, 2) the material properties (photoelectic yield and reflectance) for various possible material and surface coatings of the detector, and 3) a detailed ray-tracing simulation providing a complete picture of the solar illumination onto the detector. The resulting photocurrent as a function of height was presented for the different material coatings of the MSPD. The model was also used to estimate the photocurrent on a circular aluminium plate and compared to actual photocurrent measurements by a similar plate made by Robertson et al. (2014), revealing an underestimation of the photocurrent by a factor one to five in the 75 to 95 km region. A much better fit was obtained by allowing the model to adjust the photoelectric yield with a power law scaling, as well as shifting the height of the O_2 and O_3 atmospheric number densities by few kilometers. Adjusting the yield can be justified by the fact that the plate photoelectric yield was unknown and could largely differ from the measurement by Feuerbacher and Fitton (1972) due to surface effects (*e.g.* oxidation, contamination, roughness and/or composition). Similarly, absolute knowledge of the O_2 number density at these heights was lacking, which can be accounted for by slightly shifting the model altitude. The residual between the measurements and the adjusted model was within ± 300 pA in the 70 to 95 km altitude range, suggesting that MSP signal larger than 300 pA hidden in the photocurrent might be detectable using this method in the case of the MSPD.

The MSPD photocurrent was also measured experimentally: a deuterium lamp was used to provide VUV light and a known passband was selected around the Lyman-alpha wavelength using a narrow-band filter. The light-source flux was monitored using a silicon photodiode and, knowing the light-source spectrum, the filter transmissivity and the photodiode sensitivity, an

estimation of the spectral flux illuminating the detector could be made. Although the experiment had some issues, namely the contamination of the filter reducing which reduced transmissivity and the uncalibrated spectral response of the photodiode below 148 nm, some practical solutions were presented and an improved experiment could provide better results in the future. Based on the measured photon flux, the model was used to estimated the resulting photocurrent, which was then compared to the experimentally measured one. The base model again underestimated the photocurrent by a factor from three to eight, depending on the photodiode sensitivity considered.

Precisely estimating the photocurrent is very challenging but the presented work revealed some pathways for building and preparing future rocket-borne instruments. First of all, knowledge of the material properties is crucial when attempting any estimation of the photocurrent. From a material standpoint, a graphite coating seems to be the best choice for minimizing the photocurrent. However, a proper experimental characterization of the reflectivity and, most importantly, of the photoelectric yield is required. This could be done simultaneously by measuring the wavelength dependence of the photocurrent response for the entire instrument as attempted in Section 3. However, a monochromator setup would be required for precise measurements, as well as a very bright UV light especially in the wavelength range above 200 nm where the photoelectric yield drastically decreases. Another possibility could be to characterizing material samples of the detector at a synchrotron facilities with a monochromator setup at the beamline. The high intensity of the beam would allow for a precise characterization of the material photocurrent response. On this topic, it is worth pointing out the lack of open-access accurate measurements of material properties, in particular for the photoelectric yield, as all measurements used in this article could only be retrieved from the published curves. Secondly, simultaneous measurements of the O_2 number density along the rocket path is needed in order to constrain the deep-UV absorption at heights between 70 to 95 km. Monitoring the UV flux from the Sun, especially the Lyman-alpha line, during the flight could also provide a useful input to further constrain the photocurrent. Finally but not least, placing the detector in the shadow of the rocket would directly solve all photocurrent related issues. This can however be complicated as the rocket spins and in particular if the detectors are installed on deployable booms such as the MSPDs. Nonetheless, one could for example envision an umbrella-like deployable shade installed on the boom which could increase the time spent by the detector in shadow.

In the particular case of the MSPD, three important aspects derived from the presented work will be utilised to untangle the MSPD photocurrent from the actual MSP current. First, the photocurrent is affected by the detector inclination due to its asymetric design, indicating a possible relation between the recorded photocurrent and the rocket attitude. Second, in-flight measurements of the O_2 density will be provided by the CONE instrument also flying onboard the PMWE sounding rockets. This will serve to better estimate the O_2 absorption in the 75 to 95 km region of interest. Finally, the photoelectric yield will be adjusted to best fit the photocurrent recorded during flight, as demonstrated in Section 2.5, in order to constrain MSP signal larger than ±300 pA.

Appendix A: Realistic atmospheric curvature

The geometry of the atmosphere used in the model is shown in Figure A1, where h is the height of a given point of interest P, R is Earth radius, θ_z is the solar zenith angle, x is the distance between P and a given point P' along the line-of-sight (LOS) and h' is the corresponding heigh of the point P'. Using the law of cosine, one can express h' as function of the distance x in a polynomial equation of order two. The path along the line-of-sight x is discretized with one kilometre steps, and the corresponding h' are calculated by solving the polynomial equation. The final light-path is obtained by considering values of h' between h and 240 km, the top of the atmosphere considered in the model.
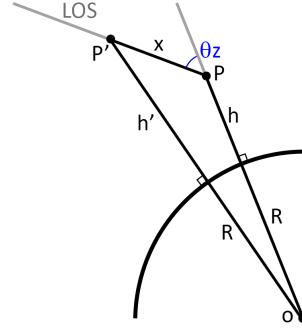
Figure A1. Geometry of the atmospheric curvature.

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