

1 **Comparison of slant open-path flux gradient and static closed chamber techniques to**  
2 **measure soil N<sub>2</sub>O emissions**

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9

10 **Abstract**

11 Improving direct field measurement techniques to quantify gases emissions from cropped  
12 agricultural fields is challenging. We compared nitrous oxide (N<sub>2</sub>O) emissions measured with  
13 static closed chambers to those from a newly developed aerodynamic flux gradient (FG)  
14 approach. Measurements were made at a vegetable farm following chicken manure application.  
15 The FG calculations were made with a single open-path Fourier transform infrared (OP-FTIR)  
16 spectrometer (height of 1.45 m) deployed in a slant-path configuration: sequentially aimed at  
17 retro reflectors at heights of 0.8 and 1.8 m above ground. Hourly emissions were measured  
18 with the FG technique, but once a day between 10:00 and 13:00 with chambers. We compared  
19 the concurrent emission ratios (FG/Chambers) between these two techniques, and found N<sub>2</sub>O  
20 emission rates from celery crop farm measured at mid-day by FG were statistically higher  
21 (1.22–1.40 times) than those from the chambers measured at the same time. Our results suggest  
22 the OP-FTIR slant-path FG configuration worked well in this study: it was sufficiently sensitive  
23 to detect the N<sub>2</sub>O gradients over our site, giving high temporal resolution N<sub>2</sub>O emissions  
24 corresponding to a large measurement footprint.

25

26 **Keywords:** chamber techniques, chicken manure, flux gradient, N<sub>2</sub>O emission, OP-FTIR  
27 spectroscopy

28

29 **Abbreviations:** FG, flux gradient; OP-FTIR, open-path Fourier transform infrared  
30 spectroscopy

31

## 32 **1 Introduction**

33 The accurate measurement of soil nitrous oxide (N<sub>2</sub>O) emissions from agricultural land is  
34 challenging. Chambers are commonly used for these measurements (Hutchinson and Mosier,  
35 1981), and chamber based observations are widely used to calculate greenhouse gas inventories  
36 (Dalal et al., 2008). The principle behind the most common type of chamber measurement  
37 (static, or non-steady state) is to create a sealed control volume over the soil surface, such that  
38 by monitoring the gas concentration change during the chamber deployment, one can calculate  
39 the surface emission rate (Denmead, 2008). One of the advantages of chambers is that they can  
40 be employed at relatively low cost, with simplicity and easy field operation (de Klein et al.,  
41 2001). However, chambers have a fundamental limitation – the control volume inevitably  
42 perturbs the soil-atmosphere interface (e.g., temperature, pressure), which has the potential to  
43 modify the ambient soil emission rate (Denmead, 1979). Moreover, manually operated static  
44 chambers are not well-suited to measure temporal variations in emissions (Denmead et al.,  
45 2008; Jones et al., 2011). The temporal variation issue can be addressed by alternative  
46 approaches, e.g. a dynamic measurement with automated-chamber opening and closing by  
47 pneumatic actuators (Yao et al., 2009) and can be run for many months. However, in many  
48 situations the most important disadvantage of chambers is their small surface measurement  
49 footprint. With a surface enclosure typically less than 1 m<sup>2</sup>, and the likelihood that soil  
50 emissions vary dramatically at length scales greater than 1 m (Denmead, 2008; Griffith and

51 Galle, 2000; Turner et al., 2008), many replications are needed to adequately quantify the  
52 emissions from an agricultural field (Christensen et al., 1996; Denmead, 1995).

53

54 Micrometeorological measurements avoid some of the problems associated with chamber  
55 methods (Christensen et al., 1996; Denmead et al., 2010; Li et al., 2008; Pattey et al., 2006).

56 These techniques are based on concentration and windflow measurements made in the free air  
57 above the surface, and they do not perturb the surface environment. They also measure  
58 emissions over footprints much larger than those from chambers (Hargreaves et al., 1996). The  
59 aerodynamic flux gradient (FG) technique is a well-used micrometeorological method, where  
60 the vertical flux of gas is inferred from a height gradient in concentration (multiplied by an  
61 estimate of the turbulent diffusivity). When measured above a large and homogeneous surface,  
62 this atmospheric flux is assumed equal to the underlying surface emission or absorption rate.

63 In this study we used a recently developed modification of the technique. Rather than vertically  
64 separated point concentrations, we used a slant-path configuration based on vertically separated  
65 long line-averaged measurements (Flesch et al., 2016; Wilson and Flesch, 2016). A single  
66 open-path Fourier transform infrared (OP-FTIR) concentration sensor with motorized aiming  
67 gives the gas concentrations along the two paths, from which we can calculate the surface  
68 emission/deposition rate.

69

70 In this study we conducted a set of N<sub>2</sub>O emission measurements from a vegetable farm  
71 following manure application. Measurements were made with both static chambers and the  
72 slant-path FG approach. Our objective was to 1) demonstrate the newly developed slant-path  
73 FG method at a vegetable farm; and 2) compare the emission rates measured by the static  
74 chamber and FG techniques.

75

## 76 **2 Materials and methods**

### 77 **2.1 Experimental site**

78 This study was conducted at an intensive vegetable farm in Clyde, Victoria, Australia (38.1°  
79 S, 145.3° E). The site consisted of two adjacent fields of 5.4 ha (Site 1) and 3.1 ha (Site 2).  
80 These sites differ only in the addition of a fertilizer amendment at Site 2. A celery crop at the  
81 4-5 leaf stage was transplanted to these two sites on 27 February 2014 (Fig. 1). Chicken manure  
82 (4.3% N,  $\text{NH}_4^+\text{-N}$ : 4633 mg kg<sup>-1</sup>,  $\text{NO}_3\text{-N}$ : 313 mg kg<sup>-1</sup>) was applied at rate of 8.2 tonne ha<sup>-1</sup> at  
83 both sites on 28 March. Fertiliser Cal-Gran (a blend of calcium ammonium nitrate and  
84 ammonium sulphate, total 23.9% N) was also applied at both sites at rate of 200 kg ha<sup>-1</sup> on 15  
85 April. Emission measurements began just prior to manure application and ended on 6 May  
86 2014. The terrain was open and flat with sandy loam topsoils. Prevailing winds were southeast  
87 or northwest during this period. The average daily minimum and maximum temperature were  
88 6 and 33°C, respectively. The total precipitation (including rainfall and irrigation) during the  
89 measurement period was 186 mm.

90 Figure 1

91

### 92 **2.2 Methodologies**

#### 93 **2.2.1 Static chamber**

94 Four static chambers (50 × 50 × 25 cm) were located at each site (Fig. 1). The metal base for  
95 each chamber was placed into the soil to a depth of 8 cm prior to the experiment, and remained  
96 in place through the study. The chamber was made of plexiglass with a built in ventilation  
97 system. Reflective aluminium foil was attached inside the lid to minimize changes in ambient  
98 pressure and temperature after the chamber was placed onto the base. A thermocouple Tinytag  
99 Transit 2 (TG-4080 temperature loggers, West Sussex, UK) was placed on the soil surface  
100 inside the chamber to monitor the headspace air temperature. Gas samples (20 mL) were

101 collected into evacuated 12 mL vials (Exetainer®, Labco Ltd., Ceredigion, UK) at 0, 30 and  
 102 60 minutes after chamber placement and analysed at an off-site laboratory by gas  
 103 chromatography (GC) (Agilent 7890A, Wilmington, USA). The sensitivity of GC for N<sub>2</sub>O  
 104 concentration was 0.01 ppm. Gas samples were collected daily between 10:00 and 13:00 from  
 105 29 March to 7 April and on 9, 11 and 16 April. The N<sub>2</sub>O flux was calculated as (Ruser et al.,  
 106 1998) (Eq. 1):

$$107 \quad Q_{chamber} = K_{N_2O} (273/T) (V/A) dC/dt \quad (1)$$

108 where  $Q_{chamber}$  is the gas flux ( $\mu\text{g N}_2\text{O-N m}^{-2} \text{ h}^{-1}$ );  $K_{N_2O}$  is 1.25 ( $\mu\text{g N } \mu\text{L}^{-1}$ ) according to the  
 109 ideal gas law, where  $K_{N_2O} = P m/R T_0$ , and  $P$  is air pressure (at 1 atm),  $m$  is molecular mass (28  
 110  $\text{g mol}^{-1}$ ),  $R$  is gas constant ( $0.0821 \text{ L atm K}^{-1} \text{ mol}^{-1}$ ), and  $T_0$  is 273 K;  $T$  is the air temperature  
 111 within the chamber (K);  $V$  is the total volume of headspace (L);  $A$  is a surface area inside the  
 112 chamber ( $\text{m}^2$ ); and  $dC/dt$  is the rate of change in mole fraction of N<sub>2</sub>O in the chamber ( $\mu\text{L L}^{-1}$   
 113  $\text{h}^{-1}$ ) determined by linear regression model. The N<sub>2</sub>O mole fraction is provide by GC, in ppm.  
 114

### 115 **2.2.2 Flux gradient**

116 The basic principle of the FG method has been well-described (Judd et al., 1999; Laubach and  
 117 Kelliher, 2004; Webb et al., 1980). We followed a modification described in Flesch et al.  
 118 (2016), in which an open-path sensor was used to measure the concentration difference ( $\Delta C_L$ )  
 119 between two vertically offset slant-paths. The open-path sensor measures gas concentration  
 120 between the sensor and a distant retro reflector. The concentration difference  $\Delta C_L$  is calculated  
 121 by sequentially aiming the sensor at high and low retro reflectors. Flesch et al. (2016) showed  
 122 that the conventional FG equation can be transformed into Eqs. 2, 3:

$$123 \quad Q_{FG} = (k_v \rho_a u^*/S_c)(M_s/M_a) * \kappa * \Delta C_L \quad (2)$$

$$124 \quad \kappa = l_{PATH} / \int_{x1}^{x2} [\ln(z_{p2}/ z_{p1}) - \phi(z_{p2}/L) + \phi(z_{p1}/L)] dx \quad (3)$$

125 where  $Q_{FG}$  is the gas flux ( $\text{g m}^{-2} \text{s}^{-1}$ ),  $k_v$  is von Karman's constant (0.4),  $\rho_a$  is dry air density ( $\text{g}$   
126  $\text{m}^{-3}$ ),  $u^*$  is friction velocity ( $\text{m s}^{-1}$ ),  $S_c$  is the turbulent Schmidt number (0.64),  $M_s$  and  $M_a$  are  
127 the molar mass of  $\text{N}_2\text{O}$  ( $44 \text{ g mol}^{-1}$ ) and dry air ( $29 \text{ g mol}^{-1}$ ), respectively,  $\Delta C_L$  (ppb) is the  
128 difference in the line-average volumetric mixing ratio of the gas (relative to dry air) from the  
129 lower ( $z_{p1}$ ) and upper ( $z_{p2}$ ) paths (m, relative to celery beds surface),  $\kappa$  is proportional to the  
130 height integral of the gas diffusivity along the FTIR path pair,  $l_{PATH}$  is the sensor-retro reflector  
131 path length (m, equal for the two paths),  $L$  is atmospheric Obukhov stability length (m). Path  
132 heights ( $z_{p1}$  and  $z_{p2}$ ) along the path length are given by a 5th-order polynomial fit of height vs.  
133 distance from the OP-FTIR spectrometer (path heights were measured in the field at 5 m  
134 intervals). We used the stability correction factor  $\varphi$  from Flesch et al. (2016).

135

136 An estimate of the uncertainty in  $Q_{FG}$  ( $\delta Q_{FG}$ ) was calculated as the sum in quadrature of the  
137 relative uncertainties in  $S_c$ ,  $\Delta C_L$  and  $\kappa$  according to the formula described in Flesch et al. (2016).  
138  $Q_{FG}$  values were not calculated when  $u^* < 0.05 \text{ m s}^{-1}$ .

139

140 The FG calculations relied on open-path concentrations measured with a robust Bruker OP-  
141 FTIR spectrometer (Matrix-M IRcube, Bruker Optics, Ettlingen, Germany) and two retro  
142 reflectors located 80 m from the spectrometer (PLX Industries, New York, USA). Briefly, the  
143 OP-FTIR system measures multiple gas concentrations ( $\text{N}_2\text{O}$ ,  $\text{CH}_4$ ,  $\text{NH}_3$ ,  $\text{CO}_2$ ,  $\text{CO}$  and water  
144 vapour) with high precision ( $\text{N}_2\text{O} < 0.3 \text{ ppb}$ ,  $\text{CH}_4 < 2 \text{ ppb}$ ,  $\text{NH}_3$ ,  $0.4 \text{ ppb}$ ,  $\text{CO}_2$ ,  $1 \text{ ppm}$ ,  $\text{CO}$ ,  $0.1$   
145  $\text{ppb}$ , and water vapour  $< 5\%$ ) (Griffith, 1996; Griffith et al., 2008; Griffith et al., 2012). More  
146 details on the OP-FTIR system can be found in Bai (2010). The spectrometer was mounted at  
147 a height of 1.45 m above ground. A motorized mounting head sequentially aimed the  
148 spectrometer to the retro reflectors at 0.8 and 1.8 m above ground. Line-averaged  $\text{N}_2\text{O}$   
149 concentrations with an averaging time of 2.5-min were measured. Background  $\text{N}_2\text{O}$

150 concentrations were measured prior to manure application in order to assess measurement  
151 precision. A sequence of observations were averaged, the standard deviation of the mean was  
152 retrieved and the precision of N<sub>2</sub>O concentration measurements (less than 0.3 ppb) was  
153 determined according to Bai (2010). The OP-FTIR measurements were made continuously  
154 from 25 March until 16 April, and thereafter measurements were made for three days  
155 (continuously) per week until 6 May.

156

157 A weather station coupled with a three-dimensional sonic anemometer (CSAT3, Campbell  
158 Scientific, Logan, UT, USA) was established at a height of 3.0 m above ground, 50 m east of  
159 Site 2. Fifteen-min average climatic data including ambient temperature, pressure and wind  
160 statistics were recorded by a data logger (CR23X, Campbell Scientific, Logan, UT, USA) at a  
161 frequency of 10 Hz. Atmospheric stability parameters of friction velocity ( $u^*$ ), surface  
162 roughness ( $z_0$ ) and Obukhov stability length ( $L$ ) were calculated from the ultrasonic  
163 anemometer data. We used a data filtering procedure to remove error-prone observations in the  
164 FG calculation according to Flesch et al. (2014).

165

166 The FG flux measurements correspond to surface emissions within a flux “footprint”. The  
167 footprint generally extends upwind of the concentration sensors, but its spatial size varies with  
168 wind conditions. A concern of this study is that the FG footprint extends beyond our plots, and  
169 the calculated emission rates are “contaminated” by emissions occurring outside the plot. This  
170 possibility was investigated by modelling the FG footprint for our smaller Site 2, where the  
171 contamination concerns are greater. The WindTrax dispersion software  
172 ([thunderbeachscientific.com](http://thunderbeachscientific.com)) was used to simulate the OP-FTIR slant-path setup, and calculate  
173 the fraction of the FG measured flux occurring within the Site 2 plot. We looked at the wind  
174 direction that results in a short fetch (NE), and looked at different atmospheric stability

175 conditions and roughness lengths. The results for  $z_0 = 0.1$  m (representative of the plot) are  
176 shown in Figure 2. We concluded that during stable night-time conditions the FG emission  
177 calculations for Site 2 maybe contaminated by up to 40% by outside fluxes. This may result in  
178 either over- or under-estimation of Site 2 emissions depending on the emission rate outside the  
179 plot. In unstable daytime conditions the contamination potential falls to 0–10%. Contamination  
180 at Site 1 will not be as serious due to the larger fetches.

181

182 The main objective of our study is to compare chamber and FG emission estimates. We looked  
183 at periods with concurrent measurements from the two techniques, and hourly flux ratios of  
184  $Q_{FG}/Q_{chamber}$  measured between 10:00 and 13:00 are compared. Because the comparison took  
185 place during the day when conditions were generally unstable, the FG contamination potential  
186 is low (and will be ignored). The contamination potential does highlight a concern with  
187 micrometeorological measurements, that a large measurement footprint may extend outside the  
188 study area and result in measurement errors.

189 Figure 2

190

## 191 **3 Results and discussion**

### 192 **3.1 Daily N<sub>2</sub>O flux**

193 The FG measurements gave high temporal resolution of fluxes and this provides an opportunity  
194 to study the pattern of N<sub>2</sub>O emissions in detail. Here we only describe the temporal flux  
195 measurements from Site 1.

196

#### 197 **3.1.1 The flux gradient fluxes**

198 Hourly N<sub>2</sub>O fluxes showed large temporal variation during the experimental period in response  
199 to fertilisation. There was a rapid increase in N<sub>2</sub>O emission from a background level of 0.6 mg

200  $\text{N}_2\text{O-N m}^{-2} \text{ h}^{-1}$  before manure application to a peak of  $158.0 \text{ mg N}_2\text{O-N m}^{-2} \text{ h}^{-1}$  within 24 h  
201 after application, which could be attributed to both nitrification and denitrification. After the  
202 peak, several spikes between 16–17 April were also observed associated with fertilizer  
203 application, followed by a decline in emissions to an average of  $2.5 \text{ mg N}_2\text{O-N m}^{-2} \text{ h}^{-1}$  (Fig.  
204 3A). One of the conclusions we draw from Figure 3B is that the slant path FG system is  
205 sensitive enough to measure the  $\text{N}_2\text{O}$  fluxes that accompanied fertilisation at our site, i.e., the  
206 measurement uncertainty as represented by  $1-\sigma$  is generally well below the flux magnitude.

207

208 In addition to the long-term pattern of decreasing emissions after manure application, we  
209 observed a diurnal pattern where maximum emission tended to occur in the late afternoon  
210 (16:00) (Fig. 3B). We believe this is related to the time of maximum soil surface temperature,  
211 which occurs after the peak air temperature (Christensen et al., 1996; Wang et al., 2013). A  
212 strong diurnal emission pattern implies that once-a-day snapshot emission measurements (e.g.,  
213 chambers) would almost certainly give a biased estimate of the daily average emission rate.  
214 We also noticed occasional high emissions at night, which was closely related to precipitation  
215 events. Negative  $\text{N}_2\text{O}$  fluxes calculated from the FG measurements most likely represent  
216 instrument noise, as the flux magnitudes were below the detectable limit of our OP-FTIR  
217 system, i.e., the uncertainty represented by the  $1-\sigma$  error bars in Fig. 3 span zero.

218 Figure 3

219

### 220 **3.1.2 Chamber fluxes**

221 Nitrous oxide fluxes from the static chambers (once-a-day snapshots) were in general  
222 agreement with the FG measurements in terms of the long-term background exchange patterns  
223 (Fig. 3): hourly fluxes rose from a background level of  $1.12 \text{ mg N}_2\text{O-N m}^{-2} \text{ h}^{-1}$  (before manure  
224 application, data is not shown), reached a spike of  $3.48 \text{ mg N}_2\text{O-N m}^{-2} \text{ h}^{-1}$  48 hours after

225 manure application, then dropped to a minimum of 1.02 mg N<sub>2</sub>O–N m<sup>-2</sup> h<sup>-1</sup> on 5 April. A  
226 maximum emission peak of 3.55 mg N<sub>2</sub>O–N m<sup>-2</sup> h<sup>-1</sup> was measured on 16 April and was most  
227 likely related to fertilizer application.

228

### 229 **3.2 Comparison of the two measurement techniques**

230 We selected the concurrent measurements from FG and the chambers and a total of 23  
231 comparison pairs were obtained during the study period (note that each chamber observation  
232 is an average from four replicate chambers). We calculated the ratio  $Q_{FG}/Q_{chamber}$  of these  
233 concurrent pairs.

234

235 The  $Q_{FG}/Q_{chamber}$  ratio showed large variation, with values ranging between 0.4 and 4.9. The  
236  $Q_{FG}/Q_{chamber}$  data follows a non-normal distribution. To better interpret these data we log-  
237 transformed the ratios (Abdi et al., 2015). The average of the natural logarithm of the ratio,  
238 converted back to the ratio units, gives the geometric mean (the process was duplicated to  
239 calculate the confidence interval  $\alpha = 0.9$ ). The geometric mean of  $Q_{FG}/Q_{chamber}$  was 1.40, with  
240 a confidence interval ranging from 1.15 to 1.69. This means that on average the FG measured  
241 fluxes were 40% higher than those from the chambers, and this difference was statistically  
242 significant.

243

244 Differences between chamber and micrometeorological measurements have been previously  
245 noted. Some studies have reported that micrometeorological techniques gave emission rates  
246 that were 50–60% of those from chambers (Christensen et al., 1996; Neftel et al., 2010). In  
247 contrast, Wang et al. (2013) reported N<sub>2</sub>O emissions measured by chambers were 17–20%  
248 lower than from the eddy covariance micrometeorological technique, and Norman et al. (1997)  
249 reported that chamber measurements were 30% lower than micrometeorological

250 measurements. Sommer et al. (2004) found static vented chambers underestimated N<sub>2</sub>O  
251 emissions from manure piles by 12–22% compared to mass balance measurements.

252

253 Discrepancies between FG and chamber fluxes could be due to very different measurement  
254 footprints. Large spatial variability is a characteristic of soil N<sub>2</sub>O emissions. For example,  
255 Turner et al. (2008) reported N<sub>2</sub>O emissions varied from 30 to 800 ng N<sub>2</sub>O–N m<sup>-2</sup> s<sup>-1</sup> over an  
256 irrigated dairy pasture (8,100 m<sup>2</sup>). This high variability, together with the substantial difference  
257 in measurement footprint size (chambers < 1 m<sup>2</sup> vs FG > 1000 m<sup>2</sup>) will likely result in  
258 differences between the two techniques because the chambers are not capable of accounting  
259 for this variability, unless many chambers are used, whilst the FG method can. If this explains  
260 the difference between the two techniques, then discrepancies between chambers and  
261 micrometeorological techniques should be site dependent, i.e., dependent on the degree of  
262 spatial variability in emissions at each site.

263

264 Several researchers have reported that chamber flux calculation procedures introduced large  
265 uncertainty in N<sub>2</sub>O emissions (Levy et al., 2011; Venterea et al., 2010). In particular, using  
266 linear regression to determine the rate of change  $dC/dt$  in Eq. (1) can lead to an underestimate  
267 of emissions (Anthony et al., 1995; Matthias et al., 1978). Venterea (2013) concluded that the  
268 typical calculations used for non-steady state chambers underestimated N<sub>2</sub>O emissions by  
269 20–50%. To examine the potential bias in N<sub>2</sub>O emissions when  $dC/dt$  is estimated with a linear  
270 regression model, we also calculated the results using a non-linear monomolecular model  
271 (Bolker, 2007). The monomolecular model is one of the simplest saturating functions and  
272 follows (Eq. 4):

$$273 \quad C_{N_2O} = a_0 + a_1 (1 - \exp(-a_2/a_1 * t)) \quad (4)$$

274 where  $C_{N_2O}$  is the mole fraction of  $N_2O$ ,  $a_0$  is the intercept corresponding to the  $N_2O$  mole  
275 fraction at time  $t = 0$ ,  $a_1$  is the horizontal asymptote at  $t = +\infty$ ,  $a_2$  is the slope ( $dC/dt$ ) at  $t = 0$ ,  
276 and  $t$  is time after chamber placement (h).

277

278 Chamber fluxes calculated using the non-linear  $dC/dt$  ( $Q_{\text{chamber-non-linear}}$ ) were 1.15 times higher  
279 than  $Q_{\text{chamber}}$  estimated using linear regression. Comparing the concurrent fluxes of  $Q_{\text{FG}}$  and  
280  $Q_{\text{chamber-non-linear}}$ , we found the geometric mean of  $Q_{\text{FG}}/Q_{\text{chamber-non-linear}}$  to be 1.22 (confidence  
281 interval of 0.99 to 1.49). Using 10,000 bootstrap re-samples (Efron and Tibshirani, 1994), we  
282 computed 10,000 potential mean fluxes from the non-linear model, of which 9540 of the means  
283 were greater than 1, and 460 were lower than 1. This result suggests the use of the non-linear  
284  $dC/dt$  calculation has resulted in better agreement with the FG estimates.

285

286 While there is a long and successful history of FG applications, there are still questions about  
287 its implementation. The value of the turbulent Schmidt number ( $Sc$ ) in Eq. (2) is debated (Flesch  
288 et al., 2002). There is also a concern regarding the accuracy of FG during light winds. In our  
289 study the light wind data ( $0.05\text{--}0.15\text{ m s}^{-1}$ ) accounted for 24% of the measurement periods. We  
290 found the FG uncertainty ( $\delta_{Q_{\text{FG}}}/Q_{\text{FG}}$ ) increased from 0.41 to 1.25 when the friction velocity ( $u^*$ )  
291 dropped from  $0.15$  to  $0.05\text{ m s}^{-1}$ . However, we note that in this study the periods in which we  
292 compared FG and chamber measurements were not light wind periods.

293

#### 294 **4 Conclusions**

295 Our results showed that soil  $N_2O$  emissions measured by FG and static chambers (linear  $dC/dt$ )  
296 were statistically different, with fluxes from FG being on average 40% higher. Using a non-  
297 linear calculation of  $dC/dt$  in the chambers decreased the disagreement to 22%. Given the  
298 likelihood of large spatial variability in  $N_2O$  emissions, and the vastly different measurement

299 footprints of the two methods, it is not surprising the two techniques give different results. It is  
300 difficult to conclude that one technique or the other is biased based on this experiment alone.  
301 However, the relationship we observed, together with other reports on the biases created by  
302 chamber calculation procedures, supports an interpretation that our FG emission calculations  
303 were accurate and in this instance the chamber measurements were biased too low.

304

305 The OP-FTIR flux gradient system used here showed the capability for real-time emission  
306 measurements over a large spatial footprint with no surface interference. Furthermore, being  
307 free from pumps and tubing, the open-path FG system would be particularly advantageous for  
308 measuring multiple gas emissions including “sticky” gases like  $\text{NH}_3$ .

309

## 310 **5 Author contribution**

311 DC, HS, SKL, MB and TF designed the experiments and MB and SKL carried them out. TF  
312 and MB developed the techniques. MB prepared the manuscript with contributions from all  
313 co-authors.

314

## 315 **6 Competing interests**

316 The authors declare that they have no conflict of interest.

317

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327

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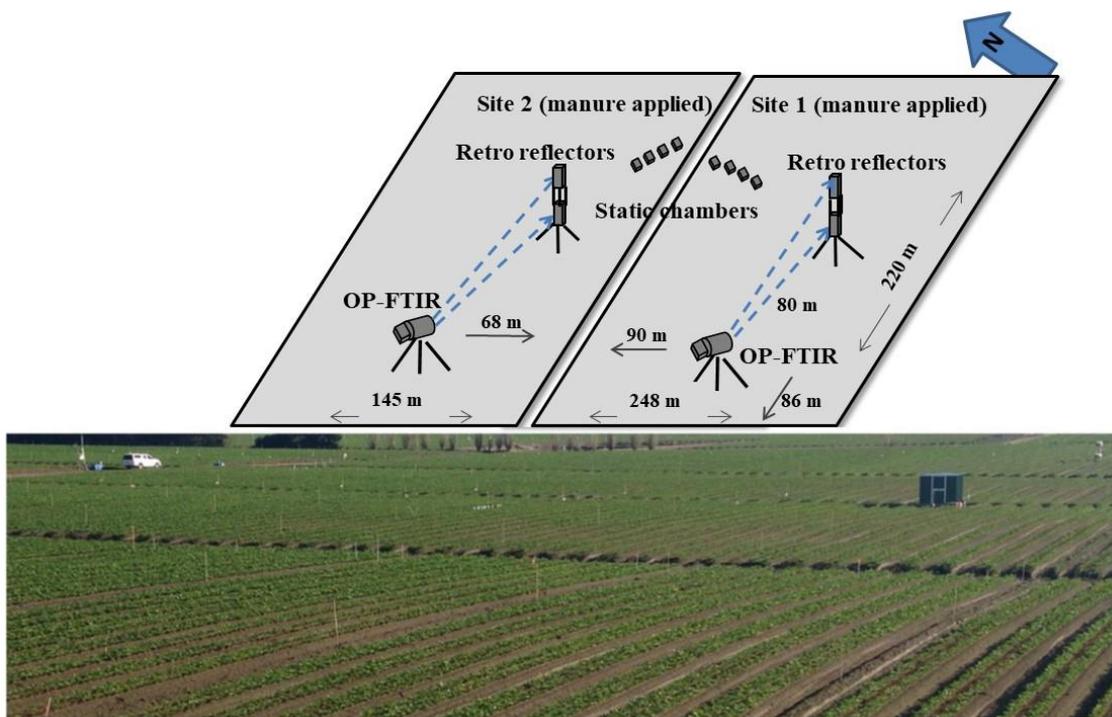
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437

## 438 Figures

439 Figure 1

440

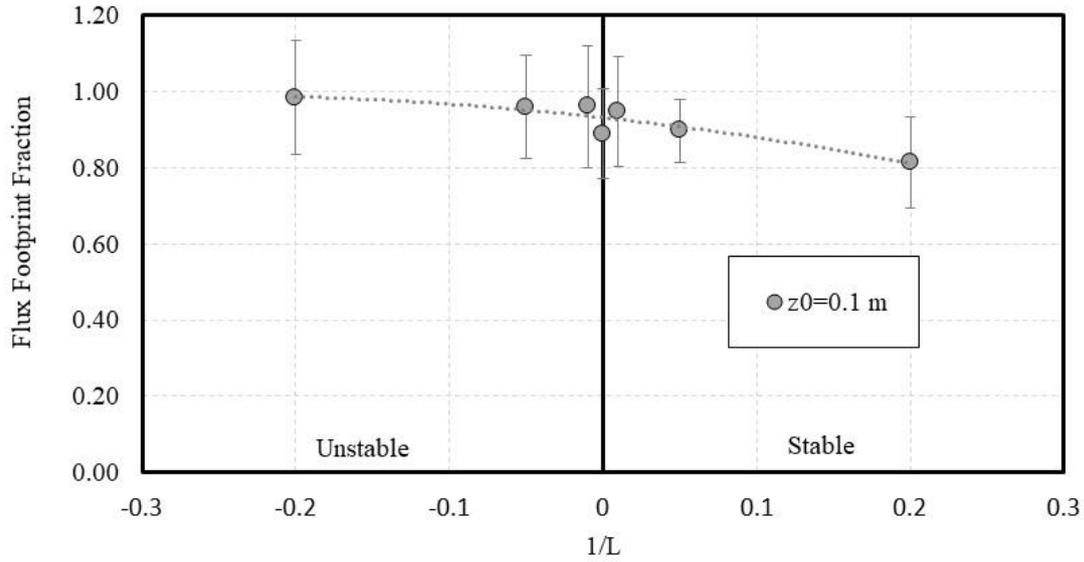


441

442 **Figure 1** The design of the study (upper panel) and photo of experimental site with OP-FTIR  
443 set up (lower panel). Emission measurements were conducted with static chambers (four per  
444 site) and FG using the OP-FTIR spectroscopy system with retro reflectors at 0.8 and 1.8 m  
445 above ground. The figure is not in scale.

446

447 Figure 2

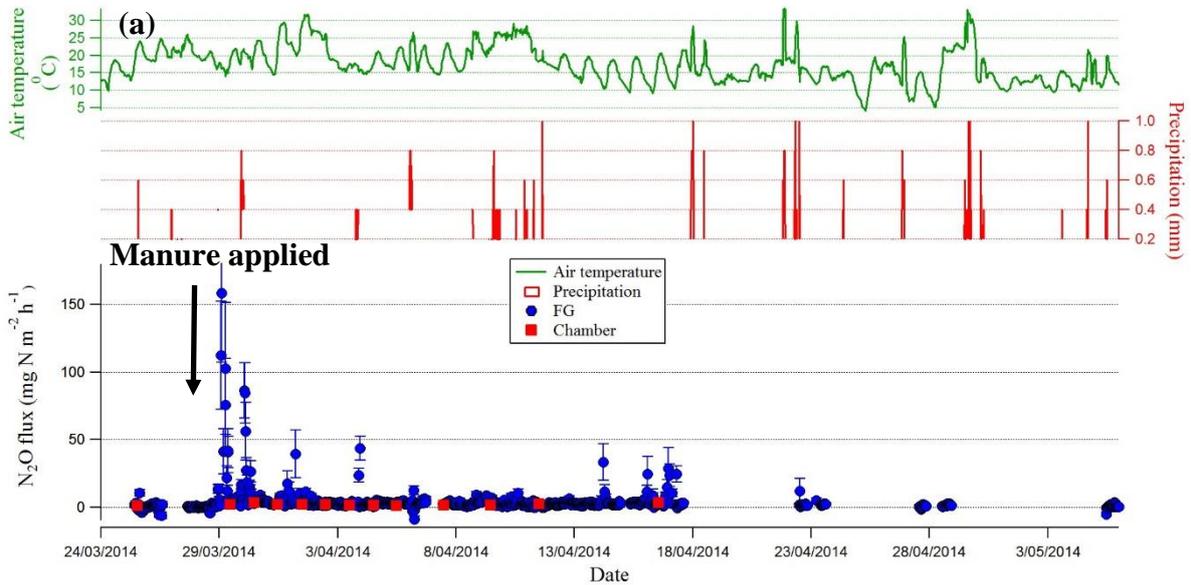


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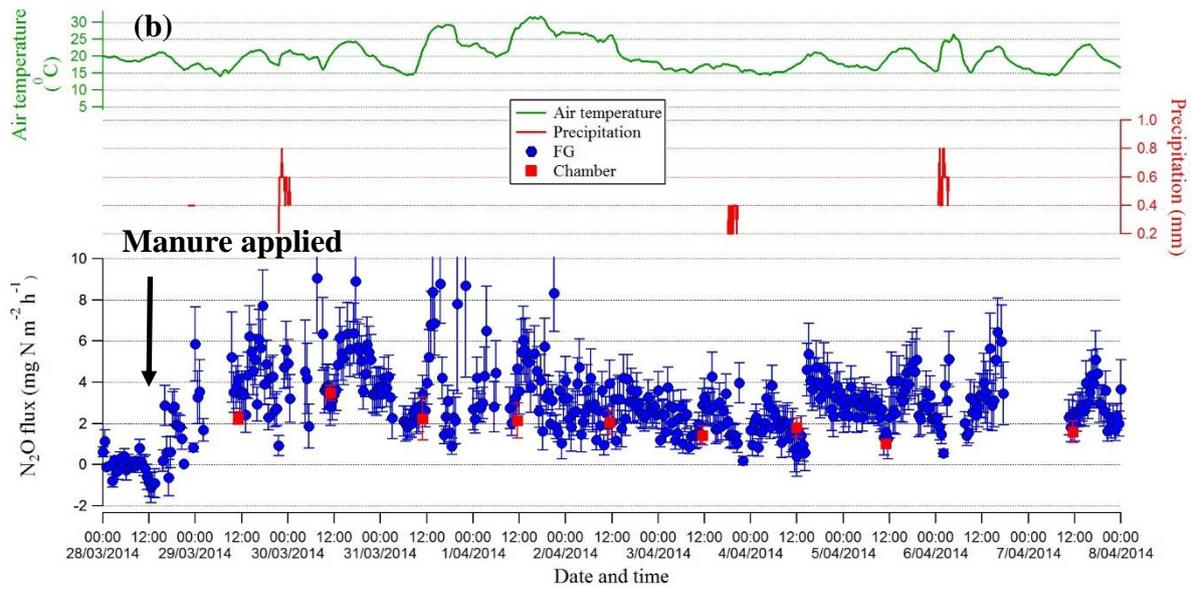
449 **Figure 2** Estimated flux footprint fraction at Site 2, plotted versus atmospheric stability (the  
 450 reciprocal of the Obukhov length  $L$ ). The model results are for a roughness length  $z_0 = 0.1$  m.

451

452 **Figure 3**



453



454

455 **Figure 3** (a) Hourly  $\text{N}_2\text{O}$  fluxes measured by FG and static chambers from 25 March to 6 May.

456 Air temperature and precipitation are plotted during the same period; and (b) subset of  $\text{N}_2\text{O}$

457 fluxes from 28 March to 8 April. Error bars (both upper and lower panels) represent  $1-\sigma$

458 estimate of measurement uncertainty ( $\delta_{\text{QFG}}$ ) for the FG measurements and standard error for

459 chambers. Manure was applied on 28 March 2014.