

1 **Comparison of slant open-path flux gradient and static closed chamber techniques to**  
2 **measure soil N<sub>2</sub>O emissions**

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9  
10 **Abstract**

11 Improving ~~the~~ direct field measurement techniques to quantify gases emissions from ~~the large~~  
12 ~~agriculture farm~~cropped agricultural fields is challenging. We compared nitrous oxide (N<sub>2</sub>O)  
13 emissions measured with static closed chambers to those from a newly developed  
14 ~~micrometeorological~~aerodynamic flux gradient (FG) approach. Measurements were made at a  
15 vegetable farm following chicken manure application. The FG calculations were made with a  
16 single open-path Fourier transform infrared (OP-FTIR) spectrometer (height of 1.45 m)  
17 deployed in a slant-path configuration: sequentially aimed at retro reflectors at heights of 0.8  
18 and 1.8 m above ground. Hourly emissions were measured with the FG technique, but once a  
19 day between 10:00 and 13:00 with chambers. We compared the concurrent emission ratios  
20 (FG/Chambers) between these two techniques, and found N<sub>2</sub>O emission rates from celery crop  
21 farm measured at mid-day by FG were statistically higher (1.422–1.40 times) than those from  
22 the chambers measured at the same time. Our results suggest the OP-FTIR slant-path FG  
23 configuration worked well in this study: it was sufficiently sensitive to detect the N<sub>2</sub>O gradients  
24 over our site, giving high temporal resolution N<sub>2</sub>O emissions corresponding to a large  
25 measurement footprint.

27 **Keywords:** chamber techniques, chicken manure, flux gradient, N<sub>2</sub>O emission, OP-FTIR  
28 spectroscopy

29

30 **Abbreviations:** FG, flux gradient; OP-FTIR, open-path Fourier transform infrared  
31 spectroscopy

32

### 33 **1 Introduction**

34 The accurate measurement of soil nitrous oxide (N<sub>2</sub>O) emissions from agricultural land is  
35 challenging. Chambers are commonly used for these measurements (Hutchinson and Mosier,  
36 1981), and chamber based observations are widely used to calculate greenhouse gas inventories  
37 (Dalal et al., 2008). The principle behind the most common type of chamber measurement  
38 (static, or non-steady state) is to create a sealed control volume over the soil surface, such that  
39 by monitoring the gas concentration change during the chamber deployment, one can calculate  
40 the surface emission rate (Denmead, 2008). One of the advantages of chambers is that they can  
41 be employed at relatively low cost, with simplicity and easy field operation (de Klein et al.,  
42 2001). However, chambers have a fundamental limitation – the control volume inevitably  
43 perturbs the soil-atmosphere interface (e.g., temperature, pressure), which has the potential to  
44 modify the ambient soil emission rate (Denmead, 1979). Moreover, manually operated static  
45 chambers are not well-suited to measure temporal variations in emissions (Denmead et al.,  
46 2008; Jones et al., 2011). ~~These weaknesses~~ The temporal variation issue can be addressed by  
47 alternative approaches, e.g. a dynamic measurement with automated-chamber opening and  
48 closing by pneumatic actuators (Yao et al., 2009) and can be run for many months. However,  
49 in many situations the most important disadvantage of chambers is their small surface  
50 measurement footprint. With a surface enclosure typically less than 1 m<sup>2</sup>, and the likelihood  
51 that soil emissions vary dramatically at length scales greater than 1 m (Denmead, 2008; Griffith

52 and Galle, 2000; Turner et al., 2008), many replications are needed to adequately quantify the  
53 emissions from an agricultural field (Christensen et al., 1996; Denmead, 1995).

54

55 Micrometeorological measurements avoid some of the problems associated with chamber  
56 methods (Christensen et al., 1996; Denmead et al., 2010; Li et al., 2008; Pattey et al., 2006).

57 These techniques are based on concentration and windflow measurements made in the free air  
58 above the surface, and they do not perturb the surface environment. They also measure

59 emissions over footprints much larger than those from chambers (Hargreaves et al., 1996). The

60 aerodynamic flux gradient (FG) technique is a well-used micrometeorological method, where

61 the vertical flux of gas is inferred from a height gradient in concentration (multiplied by an

62 estimate of the gasturbulent diffusivity). When measured above a large and homogeneous

63 surface, this atmospheric flux is assumed equal to the underlying surface emission or

64 absorption rate. In this study we used a recently developed modification of the technique.

65 Rather than vertically separated point concentrations, we used a slant-path configuration based

66 on vertically separated long line-averaged measurements (Flesch et al., 2016; Wilson and

67 Flesch, 2016). A single open-path Fourier transform infrared (OP-FTIR) concentration sensor

68 with motorized aiming gives the gas concentrations along the two paths, from which we can

69 calculate the surface emission/deposition rate.

70

71 In this study we conducted a set of N<sub>2</sub>O emission measurements from a vegetable farm

72 following manure application. Measurements were made with both static chambers and the

73 slant-path FG approach. Our objective was to 1) demonstrate the newly developed slant-path

74 FG method at a vegetable farm; and 2) compare the emission rates measured by the static

75 chamber and FG techniques.

76

## 77 **2 Materials and methods**

### 78 **2.1 Experimental site**

79 This study was conducted at an intensive vegetable farm in Clyde, Victoria, Australia (38.1°  
80 S, 145.3° E). The site consisted of two adjacent fields of 5.4 ha (Site 1) and 3.1 ha (Site 2).  
81 These sites differ only in the addition of a fertilizer amendment at Site 2. A celery crop at the  
82 4-5 leaf stage was transplanted to these two sites on 27 February 2014 (Fig. 1). Chicken manure  
83 (4.3% N,  $\text{NH}_4^+\text{-N}$ : 4633 mg  $\text{kg}^{-1}$ ,  $\text{NO}_3\text{-N}$ : 313 mg  $\text{kg}^{-1}$ ) was applied at rate of 8.2 tonne  $\text{ha}^{-1}$  at  
84 both sites on 28 March. Fertiliser Cal-Gran (a blend of calcium ammonium nitrate and  
85 ammonium sulphate, total 23.9% N) was also applied at both sites at rate of 200 kg  $\text{ha}^{-1}$  on 15  
86 April. Emission measurements began just prior to manure application and ended on 6 May  
87 2014. The terrain was open and flat with sandy loam topsoils. Prevailing winds were southeast  
88 or northwest during this period. The average daily minimum and maximum temperature  
89 waswere 6 and 33°C, respectively. The total precipitation (including rainfall and irrigation)  
90 during the measurement period was 186 mm.

91 Figure 1

92

### 93 **2.2 Methodologies**

#### 94 **2.2.1 Static chamber**

95 Four static chambers (50 × 50 × 25 cm) were located at each site (Fig. 1). The metal base for  
96 each chamber was placed into the soil to a depth of 8 cm prior to the experiment, and remained  
97 in place through the study. The chamber was made of plexiglass with a built in ventilation  
98 system. Reflective aluminium foil was attached inside the lid to minimize changes in ambient  
99 pressure and temperature after the chamber was placed onto the base. A thermocouple Tinytag  
100 Transit 2 (TG-4080 temperature loggers, West Sussex, UK) was placed on the soil surface  
101 inside the chamber to monitor the headspace air temperature. Gas samples (20 mL) were

102 collected into evacuated 12 mL vials (Exetainer®, Labco Ltd., Ceredigion, UK) at 0, 30 and  
 103 60 minutes after chamber placement and analysed at an off-site laboratory by gas  
 104 chromatography (GC) (Agilent 7890A, Wilmington, USA). The sensitivity of GC for N<sub>2</sub>O  
 105 concentration was 0.01 ppm. Gas samples were collected daily between 10:00 and 13:00 from  
 106 29 March to 7 April and on 9, 11 and 16 April. The N<sub>2</sub>O flux was calculated as (Ruser et al.,  
 107 1998) (Eq. 1):

$$108 \quad Q_{chamber} = \kappa K_{N_2O} (273/T) (V/A) dC/dt \quad (1)$$

109 where  $Q_{chamber}$  is the gas flux ( $\mu\text{g N}_2\text{O-N m}^{-2} \text{h}^{-1}$ );  $\kappa$ ;  $K_{N_2O}$  is a density factor for N<sub>2</sub>O gas, 1.25  
 110 ( $\mu\text{g N } \mu\text{L}^{-1}$ ); according to the ideal gas law, where  $K_{N_2O} = P m/R T_0$ , and  $P$  is air pressure (at  
 111 1 atm),  $m$  is molecular mass ( $28 \text{ g mol}^{-1}$ ),  $R$  is gas constant ( $0.0821 \text{ L atm K}^{-1} \text{ mol}^{-1}$ ), and  $T_0$  is  
 112 273 K;  $T$  is the air temperature within the chamber (K);  $V$  is the total volume of headspace  
 113 (L);  $A$  is a surface area inside the chamber ( $\text{m}^2$ ); and  $dC/dt$  is the rate of change in  
 114 concentration mole fraction of N<sub>2</sub>O in the chamber ( $\mu\text{L L}^{-1} \text{h}^{-1}$ ). determined by linear  
 115 regression model. The N<sub>2</sub>O mole fraction is provide by GC, in ppm.

116

### 117 2.2.2 Flux gradient

118 The basic principle of the FG method has been well-described (Judd et al., 1999; Laubach and  
 119 Kelliher, 2004; Webb et al., 1980). We followed a modification described in Flesch et al.  
 120 (2016), in which an open-path sensor was used to measure the concentration difference ( $\Delta C_L$ )  
 121 between two vertically offset slant-paths. The open-path sensor measures gas concentration  
 122 between the sensor and a distant retro reflector. The concentration difference  $\Delta C_L$  is calculated  
 123 by sequentially aiming the sensor at high and low retro reflectors (Eqs. 2, 3). Flesch et al.  
 124 (2016) showed that the conventional FG equation can be transformed into Eqs. 2, 3:

$$125 \quad Q_{FG} = (k_v \rho_a u^*/S_c)(M_s/M_a) * \kappa * \Delta C_L \quad (2)$$

126  $\kappa = l_{PATH} / \int_{x1}^{x2} [\ln(z_{p2}/z_{p1}) - \phi(z_{p2}/L) + \phi(z_{p1}/L)] dx$  (3)

127 where  $Q_{FG}$  is the gas flux ( $\text{g m}^{-2} \text{s}^{-1}$ ),  $k_v$  is von Karman's constant (0.4),  $\rho_a$  is dry air density ( $\text{g}$   
 128  $\text{m}^{-3}$ ),  $u^*$  is friction velocity ( $\text{m s}^{-1}$ ),  $S_c$  is the turbulent Schmidt number (0.64),  $M_s$  and  $M_a$  are  
 129 the molar mass of  $\text{N}_2\text{O}$  ( $44 \text{ g mol}^{-1}$ ) and dry air ( $29 \text{ g mol}^{-1}$ ), respectively,  $\Delta C_L$  (ppb) is the  
 130 difference in the line-average volumetric mixing ratio of the gas (relative to dry air) from the  
 131 lower ( $z_{p1}$ ) and upper ( $z_{p2}$ ) paths (m, relative to celery beds surface),  $\kappa$  is proportional to the  
 132 height integral of the gas diffusivity along the FTIR path pair,  $l_{PATH}$  is the sensor-retro reflector  
 133 path length (m, equal for the two paths),  $L$  is atmospheric Obukhov stability length (m). Path  
 134 heights ( $z_{p1}$  and  $z_{p2}$ ) along the path length are given by a 5th-order polynomial fit of height vs.  
 135 distance from the OP-FTIR spectrometer (path heights were measured in the field at 5 m  
 136 intervals). We used the stability correction factor  $\phi$  from Flesch et al. (2016).

137  
 138 An estimate of the uncertainty in  $Q_{FG}$  ( $\delta Q_{FG}$ ) was calculated as the sum in quadrature of the  
 139 relative uncertainties in  $S_c$ ,  $\Delta C_L$  and  $\kappa$  according to the formula described in Flesch et al. (2016).  
 140  $Q_{FG}$  values were not calculated when  $u^* < 0.05 \text{ m s}^{-1}$ .

141  
 142 The FG calculations relied on open-path concentrations measured with a robust Bruker OP-  
 143 FTIR spectrometer (Matrix-M IRcube, Bruker Optics, Ettlingen, Germany) and two retro  
 144 reflectors located 80 m from the spectrometer (PLX Industries, New York, USA). Briefly, the  
 145 OP-FTIR system measures multiple gas concentrations ( $\text{N}_2\text{O}$ ,  $\text{CH}_4$ ,  $\text{NH}_3$ ,  $\text{CO}_2$ ,  $\text{CO}$  and water  
 146 vapour) with high precision ( $\text{N}_2\text{O} < 0.3 \text{ ppb}$ ,  $\text{CH}_4 < 2 \text{ ppb}$ ,  $\text{NH}_3$ ,  $0.4 \text{ ppb}$ ,  $\text{CO}_2$ ,  $1 \text{ ppm}$ ,  $\text{CO}$ ,  $0.1$   
 147  $\text{ppb}$ , and water vapour  $< 5\%$ ) (Griffith, 1996; Griffith et al., 2008; Griffith et al., 2012). More  
 148 details on the OP-FTIR system can be found in Bai (2010). The spectrometer was mounted at  
 149 a height of 1.45 m above ground. A motorized mounting head sequentially aimed the

150 spectrometer to the retro reflectors at 0.8 and 1.8 m above ground. Line-averaged N<sub>2</sub>O  
151 concentrations with an averaging time of 2.5-min were measured. Background N<sub>2</sub>O  
152 concentrations were measured prior to manure application in order to assess measurement  
153 precision. A sequence of observations were averaged, the standard deviation of the mean was  
154 retrieved and the precision of N<sub>2</sub>O concentration measurements (less than 0.3 ppb) was  
155 determined according to Bai (2010). The OP-FTIR measurements were made continuously  
156 from 25 March until 16 April, and thereafter measurements were made for three days  
157 (continuously) per week until 6 May.

158

159 A weather station coupled with a three-dimensional sonic anemometer (CSAT3, Campbell  
160 Scientific, Logan, UT, USA) was established at a height of 3.0 m above ground, 50 m east of  
161 Site 2. Fifteen-min average climatic data including ambient temperature, pressure and wind  
162 statistics were recorded by a data logger (CR23X, Campbell Scientific, Logan, UT, USA) at a  
163 frequency of 10 Hz. Atmospheric stability parameters of friction velocity ( $u^*$ ), surface  
164 roughness ( $z_0$ ) and Obukhov stability length ( $L$ ) were calculated from the ultrasonic  
165 anemometer data. We used a data filtering procedure to remove error-prone observations in the  
166 FG calculation according to Flesch et al. (2014).

167 ~~Fe~~

168 The FG flux measurements correspond to surface emissions within a flux “footprint”. The  
169 footprint generally extends upwind of the concentration sensors, but its spatial size varies with  
170 wind conditions. A concern of this study is that the FG footprint extends beyond our plots, and  
171 the calculated emission rates are “contaminated” by emissions occurring outside the plot. This  
172 possibility was investigated by modelling the FG footprint for our smaller Site 2, where the  
173 contamination concerns are greater. The WindTrax dispersion software  
174 (thunderbeachscientific.com) was used to simulate the OP-FTIR slant-path setup, and calculate

175 the fraction of the FG measured flux occurring within the Site 2 plot. We looked at the wind  
176 direction that results in a short fetch (NE), and looked at different atmospheric stability  
177 conditions and roughness lengths. The results for  $z_0 = 0.1$  m (representative of the plot) are  
178 shown in Figure 2. We concluded that during stable night-time conditions the FG emission  
179 calculations for Site 2 maybe contaminated by up to 40% by outside fluxes. This may result in  
180 either over- or under-estimation of Site 2 emissions depending on the emission rate outside the  
181 plot. In unstable daytime conditions the contamination potential falls to 0–10%. Contamination  
182 at Site 1 will not be as serious due to the larger fetches.

183  
184 The main objective of our study is to compare ~~the two measurement techniques we~~ chamber  
185 and FG emission estimates. We looked at periods with concurrent measurements from ~~FG and~~  
186 ~~the chamber~~ two techniques, and hourly flux ratios of  $Q_{FG}/Q_{chamber}$  measured between 10:00  
187 and 13:00 are compared. Because the comparison took place during the day when conditions  
188 were generally unstable, the FG contamination potential is low (and will be ignored). The  
189 contamination potential does highlight a concern with micrometeorological measurements, that  
190 a large measurement footprint may extend outside the study area and result in measurement  
191 errors.

192 Figure 2

### 194 **3 Results and discussion**

#### 195 **3.1 Daily N<sub>2</sub>O flux**

196 The FG measurements gave high temporal resolution of fluxes and this provides an opportunity  
197 to study the pattern of N<sub>2</sub>O emissions in detail. Here we only describe the temporal flux  
198 measurements from Site 1.

### 200 3.1.1 The **FG flux gradient fluxes**

201 Hourly N<sub>2</sub>O fluxes showed large temporal variation during the experimental period in response  
202 to fertilisation. There was a rapid increase in N<sub>2</sub>O emission from a background level of 0.6 mg  
203 N<sub>2</sub>O–N m<sup>-2</sup> h<sup>-1</sup> before manure application to a peak of 158.0 mg N<sub>2</sub>O–N m<sup>-2</sup> h<sup>-1</sup> within 24 h  
204 after application, which could be attributed to both nitrification and denitrification. After the  
205 peak, several spikes between 16–17 April were also observed associated with fertilizer  
206 application, followed by a decline in emissions to an average of 2.5 mg N<sub>2</sub>O–N m<sup>-2</sup> h<sup>-1</sup> (Fig.  
207 [2A3A](#)). One of the conclusions we draw from Figure [2B3B](#) is that the slant path FG system is  
208 sensitive enough to measure the N<sub>2</sub>O fluxes that accompanied fertilisation at our site, i.e., the  
209 measurement uncertainty as represented by 1-σ is generally well below the flux magnitude.

210

211 In addition to the long-term pattern of decreasing emissions after manure application, we  
212 observed a diurnal pattern where maximum emission tended to occur in the late afternoon  
213 (16:00) (Fig. [2B3B](#)). We believe this is related to the time of maximum soil surface  
214 temperature, which occurs after the peak air temperature (Christensen et al., 1996; Wang et al.,  
215 2013). A strong diurnal emission pattern implies that once-a-day snapshot emission  
216 measurements (e.g., chambers) would almost certainly give a biased estimate of the daily  
217 average emission rate. We also noticed occasional high emissions at night, which was closely  
218 related to precipitation events. Negative N<sub>2</sub>O fluxes calculated from the FG measurements most  
219 likely represent instrument noise, as the flux magnitudes were below the detectable limit of our  
220 OP-FTIR system, i.e.g., the uncertainty represented by the 1-σ error bars in Fig. [23](#) span zero.

221 Figure [23](#)

222

### 223 3.1.2 Chamber fluxes

224 Nitrous oxide fluxes from the static chambers (once-a-day snapshots) were in general  
225 agreement with the FG measurements in terms of the long-term patternbackground exchange  
226 patterns (Fig. 23): hourly fluxes rose from a background level of 1.12 mg N<sub>2</sub>O–N m<sup>-2</sup> h<sup>-1</sup>  
227 (before manure application, data is not shown), reached a spike of 3.48 mg N<sub>2</sub>O–N m<sup>-2</sup> h<sup>-1</sup> 48  
228 hours after manure application, then dropped to a minimum of 1.02 mg N<sub>2</sub>O–N m<sup>-2</sup> h<sup>-1</sup> on 5  
229 April. A maximum emission peak of 3.55 mg N<sub>2</sub>O–N m<sup>-2</sup> h<sup>-1</sup> was measured on 16 April and  
230 was most likely related to fertilizer application.

231

### 232 3.2 Comparison of the two emissionmeasurement techniques

233 We selected the concurrent measurements from FG and the chambers and a total of 23  
234 comparison pairs were obtained during the study period (note that each chamber observation  
235 is an average from four replicate chambers). We calculated the ratio  $Q_{FG}/Q_{chamber}$  of these  
236 concurrent pairs.

237

238 The  $Q_{FG}/Q_{chamber}$  ratio showed large variation, with values ranging between 0.4 and 4.9. The  
239  $Q_{FG}/Q_{chamber}$  data follows a non-normal distribution. To better interpret these data we log-  
240 transformed the ratios (Abdi et al., 2015). The average of the natural logarithm of the ratio,  
241 converted back to the ratio units, gives the geometric mean (the process was duplicated to  
242 calculate the confidence interval  $\alpha = 0.9$ ). The geometric mean of  $Q_{FG}/Q_{chamber}$  was 1.40, with  
243 a confidence interval ranging from 1.15 to 1.69. This means that on average the FG measured  
244 fluxes were 40% higher than those from the chambers, and this difference was statistically  
245 significant.

246

247 Differences between chamber and micrometeorological measurements have been previously  
248 noted. Some studies have reported that micrometeorological techniques gave emission rates

249 that were 50–60% of those from chambers (Christensen et al., 1996; Neftel et al., 2010). In  
250 contrast, Wang et al. (2013) reported N<sub>2</sub>O emissions measured by chambers were 17–20%  
251 lower than from the eddy covariance micrometeorological technique, and Norman et al. (1997)  
252 reported that chamber measurements were 30% lower than micrometeorological  
253 measurements. Sommer et al. (2004) found static vented chambers underestimated N<sub>2</sub>O  
254 emissions from manure piles by 12–22% compared to mass balance measurements.

255

256 Discrepancies between FG and chamber fluxes could be due to very different measurement  
257 footprints. Large spatial variability is a characteristic of soil N<sub>2</sub>O emissions. For example,  
258 Turner et al. (2008) reported N<sub>2</sub>O emissions varied from 30 to 800 ng N<sub>2</sub>O–N m<sup>-2</sup> s<sup>-1</sup> over an  
259 irrigated dairy pasture (8,100 m<sup>2</sup>). This high variability, together with the substantial difference  
260 in measurement footprint size (chambers < 1 m<sup>2</sup> vs FG > 1000 m<sup>2</sup>) will likely result in  
261 differences between the two techniques because the chambers are not capable of accounting  
262 for this variability, unless many chambers are used, whilst the FG method can. If this explains  
263 the difference between the two techniques, then discrepancies between chambers and  
264 micrometeorological techniques should be site dependent, i.e., dependent on the degree of  
265 spatial variability in emissions at each site.

266

267 Several researchers have reported that chamber flux calculation procedures introduced large  
268 uncertainty in N<sub>2</sub>O emissions (Levy et al., 2011; Venterea et al., 2010). In particular, using  
269 linear regression to determine the rate of change  $dC/dt$  in Eq. (1) can lead to an underestimate  
270 of emissions (Anthony et al., 1995; Matthias et al., 1978). Venterea (2013) concluded that the  
271 typical calculations used for non-steady state chambers underestimated N<sub>2</sub>O emissions by  
272 20–50%. ~~Our results are in line with this conclusion.~~ To examine the potential bias in N<sub>2</sub>O  
273 emissions when  $dC/dt$  is estimated with a linear regression model, we also calculated the results

274 using a non-linear monomolecular model (Bolker, 2007). The monomolecular model is one of  
275 the simplest saturating functions and follows (Eq. 4):

$$276 \quad C_{N_2O} = a_0 + a_1 (1 - \exp(-a_2/a_1 * t)) \quad (4)$$

277 where  $C_{N_2O}$  is the mole fraction of  $N_2O$ ,  $a_0$  is the intercept corresponding to the  $N_2O$  mole  
278 fraction at time  $t = 0$ ,  $a_1$  is the horizontal asymptote at  $t = +\infty$ ,  $a_2$  is the slope ( $dC/dt$ ) at  $t = 0$ ,  
279 and  $t$  is time after chamber placement (h).

280  
281 Chamber fluxes calculated using the non-linear  $dC/dt$  ( $Q_{\text{chamber-non-linear}}$ ) were 1.15 times higher  
282 than  $Q_{\text{chamber}}$  estimated using linear regression. Comparing the concurrent fluxes of  $Q_{\text{FG}}$  and  
283  $Q_{\text{chamber-non-linear}}$ , we found the geometric mean of  $Q_{\text{FG}}/Q_{\text{chamber-non-linear}}$  to be 1.22 (confidence  
284 interval of 0.99 to 1.49). Using 10,000 bootstrap re-samples (Efron and Tibshirani, 1994), we  
285 computed 10,000 potential mean fluxes from the non-linear model, of which 9540 of the means  
286 were greater than 1, and 460 were lower than 1. This result suggests the use of the non-linear  
287  $dC/dt$  calculation has resulted in better agreement with the FG estimates.

288

289 While there is a long and successful history of FG applications, there are still questions about  
290 its implementation. The value of the turbulent Schmidt number ( $Sc$ ) in Eq. (2) is debated (Flesch  
291 et al., 2002). ~~In addition, concerns about FG arise if the fetch (upwind distance from the~~  
292 ~~concentration measurement to the source edge) is not large. In our case the ratio of  $z_d$  (the~~  
293 ~~maximum height of the OP-FTIR measurement path, 1.8 m) to the upwind fetch (minimum of~~  
294 ~~90–68 m for Sites 1 and 2, respectively) was  $< 1:35$ . This is considered to be sufficient in most~~  
295 ~~conditions, but during stable night-time conditions the fetch may not have been large enough~~  
296 ~~to satisfy the FG assumption of a constant flux layer (Flesch et al., 2016). In this case the FG~~  
297 ~~measurements would have been contaminated by emissions occurring upwind of our sites.~~

298 There is also a concern regarding the accuracy of FG during light winds. In our study the light

299 wind data ( $0.05\text{--}0.15\text{ m s}^{-1}$ ) accounted for 24% of the measurement periods. We found the FG  
300 uncertainty ( $\delta_{Q_{FG}}/Q_{FG}$ ) increased from 0.41 to 1.25 when the friction velocity ( $u^*$ ) dropped from  
301  $0.15$  to  $0.05\text{ m s}^{-1}$ . However, we note that in this study the periods in which we compared FG  
302 and chamber measurements were not light wind periods.

303

#### 304 **4 Conclusions**

305 Our results showed that ~~FG and static chamber measurements of~~ soil  $\text{N}_2\text{O}$  emissions measured  
306 by FG and static chambers (linear  $dC/dt$ ) were statistically different, with fluxes from FG being  
307 on average 40% higher. Using a non-linear calculation of  $dC/dt$  in the chambers decreased the  
308 disagreement to 22%. Given the likelihood of large spatial variability in  $\text{N}_2\text{O}$  emissions, and  
309 the vastly different measurement footprints of the two methods, it is not surprising the two  
310 techniques give different results. It is difficult to conclude that one technique or the other is  
311 biased based on this experiment alone. However, the relationship we observed, together with  
312 other reports on the biases created by chamber calculation procedures, supports an  
313 interpretation that our FG emission calculations were accurate and in this instance the chamber  
314 measurements were biased too low.

315

316 The OP-FTIR flux gradient system used here showed the capability for real-time emission  
317 measurements over a large spatial footprint with no surface interference. Furthermore, being  
318 free from pumps and tubing, the open-path FG system would be particularly advantageous for  
319 measuring multiple gas emissions including “sticky” gases like  $\text{NH}_3$ .

320

#### 321 **5 Author contribution**

322 DC, HS, SKL, MB and TF designed the experiments and MB and SKL carried them out. TF  
323 and MB developed the techniques. MB prepared the manuscript with contributions from all  
324 co-authors.

325

## 326 **6 Competing interests**

327 The authors declare that they have no conflict of interest.

328

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338

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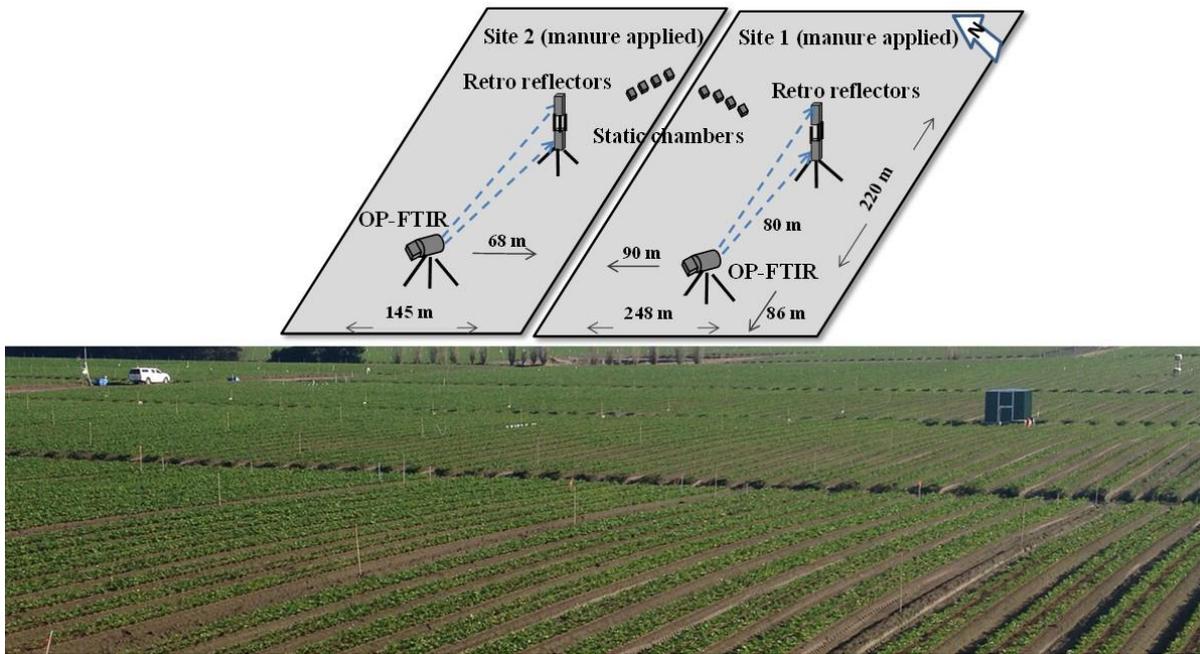
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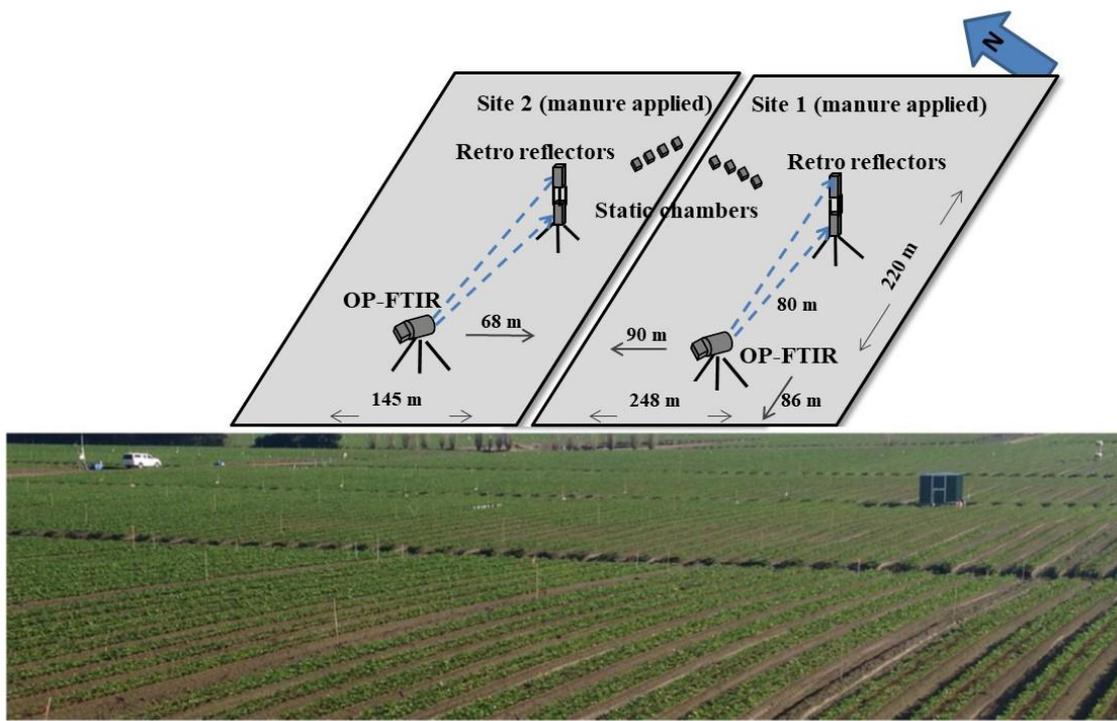
## 449 **Figures**

450 Figure 1

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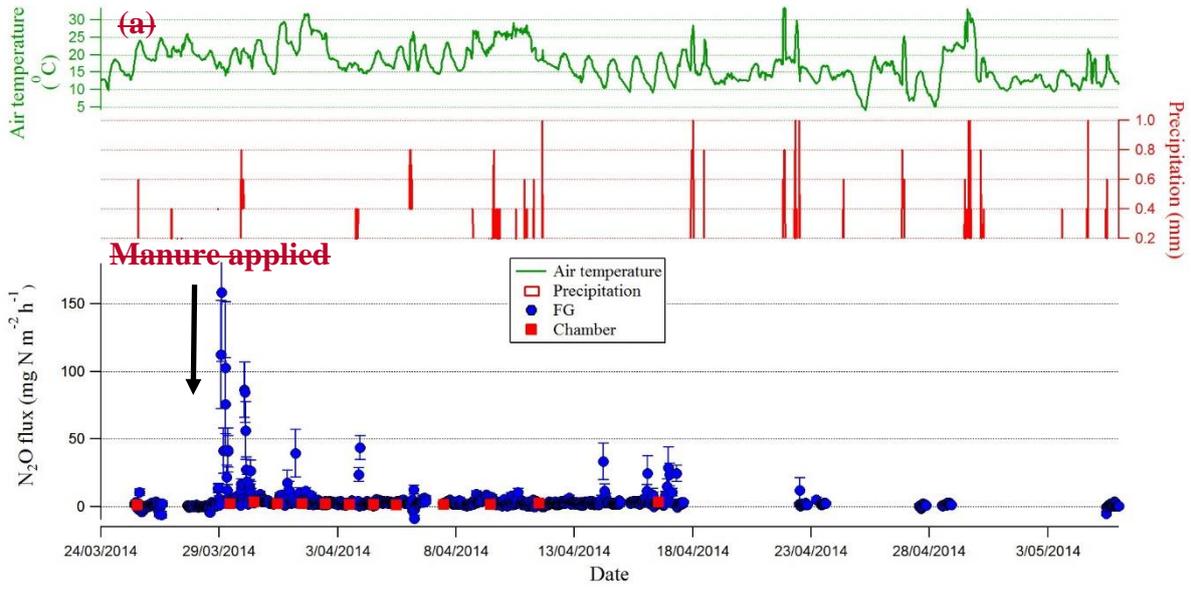


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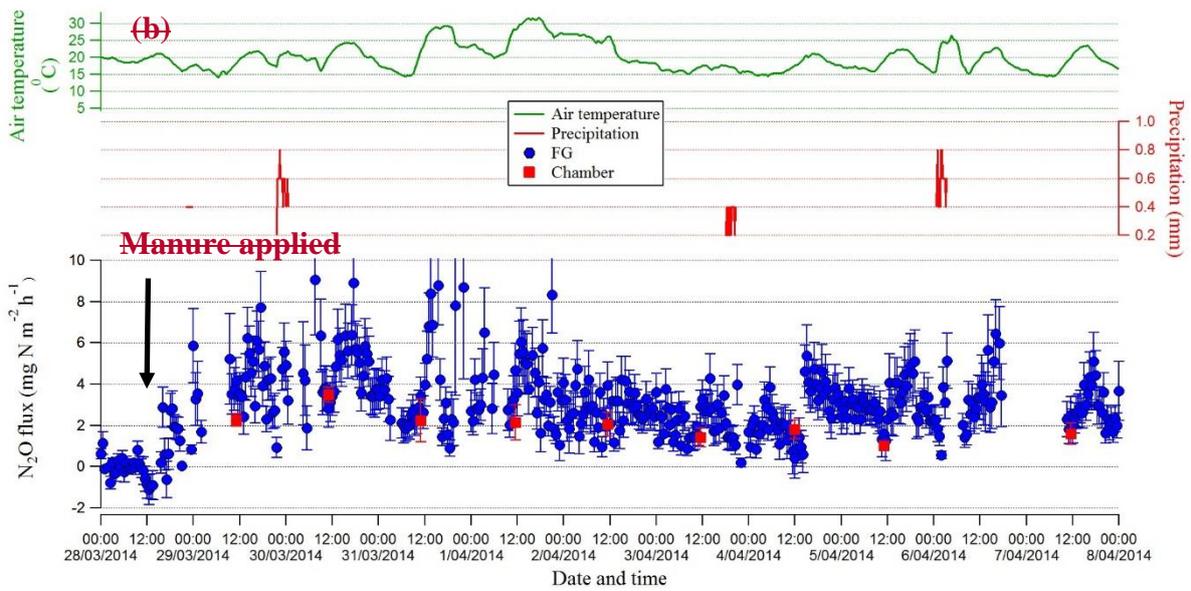
454 **Figure 1** The design of the study (upper panel) and photo of experimental site with OP-FTIR  
 455 set up (lower panel). Emission measurements were conducted with static chambers (four per  
 456 site) and FG using the OP-FTIR spectroscopy system with retro reflectors at 0.8 and 1.8 m  
 457 above ground. The figure is not in scale.

458

459 Figure 2



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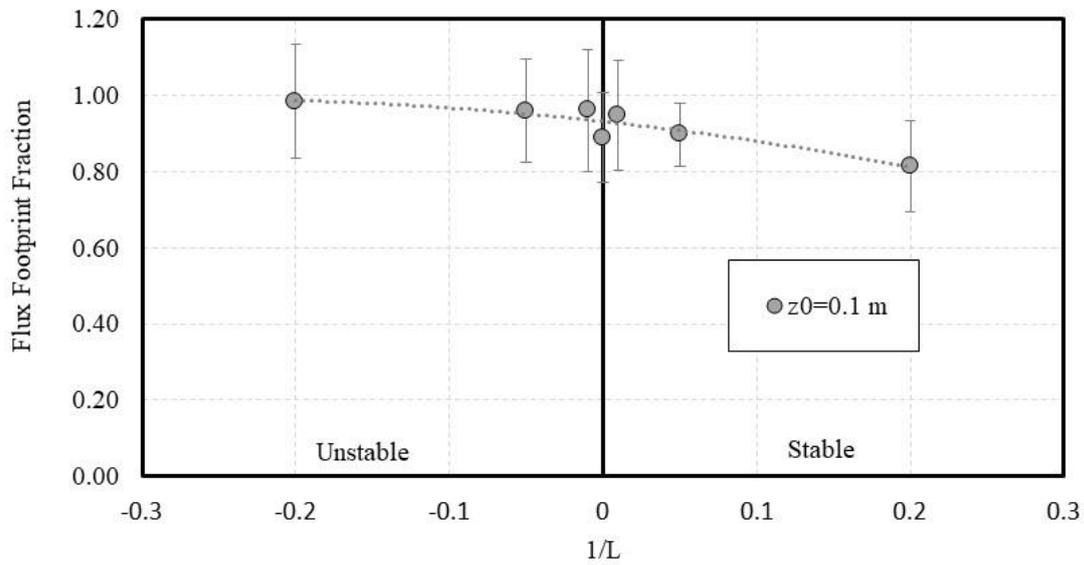


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Figure

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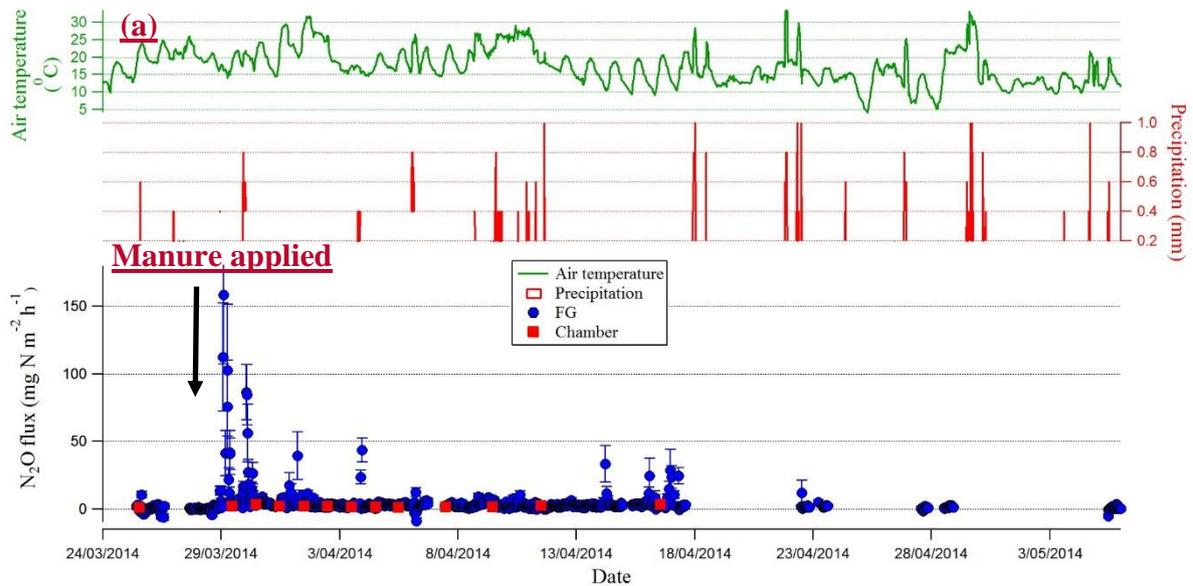


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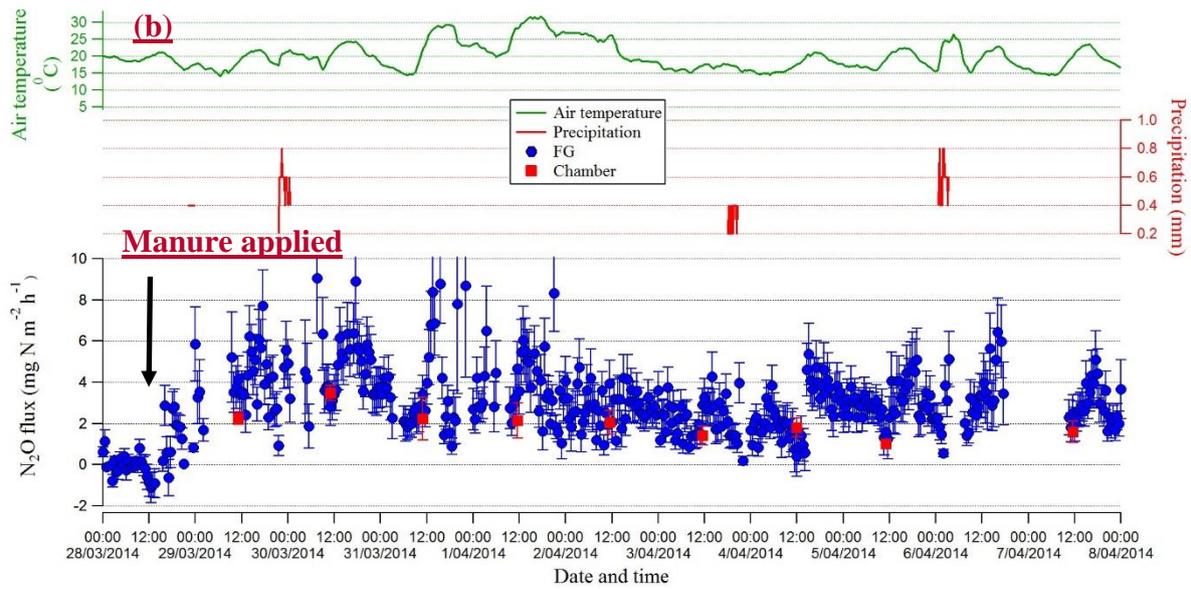
464 **Figure 2** Estimated flux footprint fraction at Site 2, plotted versus atmospheric stability (the  
465 reciprocal of the Obukhov length  $L$ ). The model results are for a roughness length  $z_0 = 0.1$  m.

466

467 **Figure 3**



468



469

470 **Figure 3** (a) Hourly N<sub>2</sub>O fluxes measured by FG and static chambers from 25 March to 6 May.

471 Air temperature and precipitation are plotted during the same period; and (b) subset of N<sub>2</sub>O

472 fluxes from 28 March to 8 April. Error bars (both upper and lower panels) represent 1- $\sigma$

473 estimate of measurement uncertainty ( $\delta_{Q_{FG}}$ ) for the FG measurements and standard error for

474 chambers. Manure was applied on 28 March 2014.

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487 Anonymous refere#1

488 Re: Revision of manuscript Number: AMT-2018-90, Title: **Comparison of flux gradient and**  
489 **chamber techniques to measure soil N<sub>2</sub>O emissions**

490

491

492 We thank the positive feedback on the manuscript.

493 Reviewer is aware of the difference in N<sub>2</sub>O fluxes between these two techniques that is mainly because  
494 that the static chamber measurements were obtained periodically (no measurements during night-  
495 time or morning). Reviewer suggested to compare the cumulative flux over the first 10 days after N  
496 fertilizer was applied.

497 we agree, and the chamber vs. FG comparison was only evaluated during periods of concurrent  
498 measurements. In the revised manuscript, we have summarised our footprint analysis on FG fluxes  
499 and the investigation of the bias of chamber measurements using linear  $dC/dt$ .

500 The cumulative flux is often estimated by summing the mean daily flux over a period of time. Ideally,  
501 a continuous real time series (or regular measurements during the day) should be used as emissions  
502 can vary throughout the day. As we used chambers measurements only from 11 am to noon each day,  
503 calculating cumulative fluxes using the chamber data would result in a biased  
504 estimation. Furthermore, a cumulative flux ratio between the two measurement methods would only  
505 provide one data point, which would preclude inference.

506

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519 Refere #2

520 Dear Dr. Flechard,

521 Re: Revision of manuscript Number: AMT-2018-90, Title: **Comparison of flux gradient and**  
522 **chamber techniques to measure soil N<sub>2</sub>O emissions**

523  
524

525 We thank the positive feedback on the manuscript. We have addressed the comments thoroughly,  
526 our response to every issue raised is given point by point in **blue text** below.

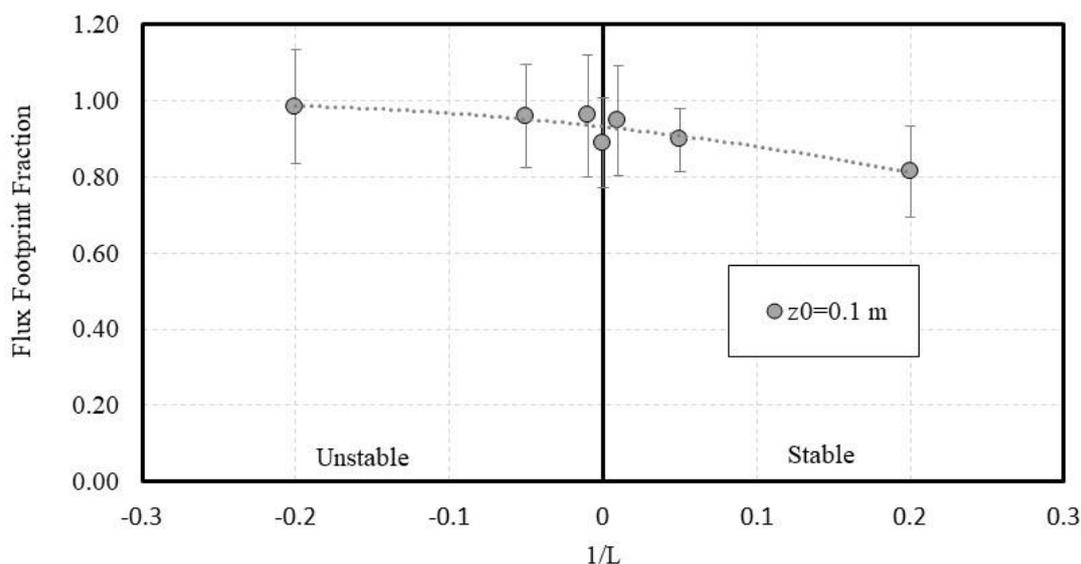
527  
528

529 The reviewer is aware of the conclusions that should count two aspects: 1) quantitative footprint  
530 analysis, 2) recalculate the chamber fluxes using non-linear algorithms.

531

532 **Authors agree with the reviewer.**

533 **We conducted a footprint analysis using the Windtrax dispersion model to examine the contribution**  
534 **of area outside our plot to the slant-path FG fluxes. We examined Site 2 (the smaller plot) and**  
535 **considered a wind direction which would be the worst-case scenario for a footprint (wind from**  
536 **NE). We also considered the atmospheric stability ( $1/L$ ) and surface roughness ( $z_0$ ). We estimated the**  
537 **footprint of the slant-path configuration, and what fraction of the surface flux occurred within the plot**  
538 **boundary. Figure A shows the Estimated flux footprint fraction at Site 2 increased from stable to**  
539 **unstable conditions at  $z_0 = 0.1$  m.**



540

541 **Fig. A** Estimated flux footprint fraction at Site 2, plotted versus atmospheric stability (the reciprocal of

542 the Obukhov length  $L$ ). The model results are for a roughness length  $z_0 = 0.1$  m.

543 This result suggests the OP-FTIR flux estimates at night-time could be contaminated by emissions  
544 outside the plot (up to 40% contaminated). However, the contamination decreases to < 10% during  
545 the day time.

546

547 The results are summarised in the revised manuscript, see on page 7-8, Line 166-188 and Figure 2.

548 *“The FG flux measurements correspond to surface emissions within a flux “footprint”. The footprint*  
549 *generally extends upwind of the concentration sensors, but its spatial size varies with wind*  
550 *conditions. A concern of this study is that the FG footprint extends beyond our plots, and the calculated*  
551 *emission rates are “contaminated” by emissions occurring outside the plot. This possibility was*  
552 *investigated by modelling the FG footprint for our smaller Site 2, where the contamination concerns*  
553 *are greater. The WindTrax dispersion software (thunderbeachscientific.com) was used to simulate the*  
554 *OP-FTIR slant-path setup, and calculate the fraction of the FG measured flux occurring within the Site*  
555 *2 plot. We looked at the wind direction that results in a short fetch (NE), and looked at different*  
556 *atmospheric stability conditions and roughness lengths. The results for  $z_0 = 0.1$  m (representative of*  
557 *the plot) are shown in Figure 2. We concluded that during stable night-time conditions the FG emission*  
558 *calculations for Site 2 maybe contaminated by up to 40% by outside fluxes. This may result in either*  
559 *over- or under-estimation of Site 2 emissions depending on the emission rate outside the plot. In*  
560 *unstable daytime conditions the contamination potential falls to 0 – 10%. Contamination at Site 1 will*  
561 *not be as serious due to the larger fetches.*

562 *The main objective of our study is to compare chamber and FG emission estimates. We looked at*  
563 *periods with concurrent measurements from the two techniques, and hourly flux ratios of  $Q_{FG}/Q_{chamber}$*   
564 *measured between 10:00 and 13:00 are compared. Because the comparison took place during the day*  
565 *when conditions were generally unstable, the FG contamination potential is low (and will be*  
566 *ignored). The contamination potential does highlight a concern with micrometeorological*  
567 *measurements, that a large measurement footprint may extend outside the study area and result in*  
568 *measurement errors.”*

569

570 2) For our chamber analysis we added an alternative estimation of the rate of  $dC/dt$ , using a non-linear  
571 monomolecular model (Bolker, 2007). This follows the equation:  $C_{N_2O} = a_0 + a_1 (1 - \exp(-a_2/a_1 * t))$ ,  
572 where  $C_{N_2O}$  is the mole fraction of  $N_2O$ ,  $a_0$  is the intercept corresponding to  $N_2O$  mole fraction at time  
573  $t = 0$ ,  $a_1$  is the horizontal asymptote at  $t = +\infty$ ,  $a_2$  is the slope ( $dC/dt$ ) at  $t = 0$ , and  $t$  is time after the  
574 chamber is chamber placement time (h).

575 We plotted  $dC/dt$  estimated from both the original linear regression and non-linear monomolecular  
576 model in Figs. B, C. The chamber fluxes using the non-linear  $dC/dt$  estimate is 1.15 times higher than  
577 that using linear  $dC/dt$  estimate. This improved the geometric mean  $Q_{FG}/Q_{chamber\_non-linear}$  to 1.22  
578 (confidence interval of 0.99 to 1.49). We still concluded that chamber measurements are  
579 underestimating the flux, but the use of a non-linear calculation of  $dC/dt$  decreases the disagreement  
580 to 22% compared to that of 40% using linear regression model.

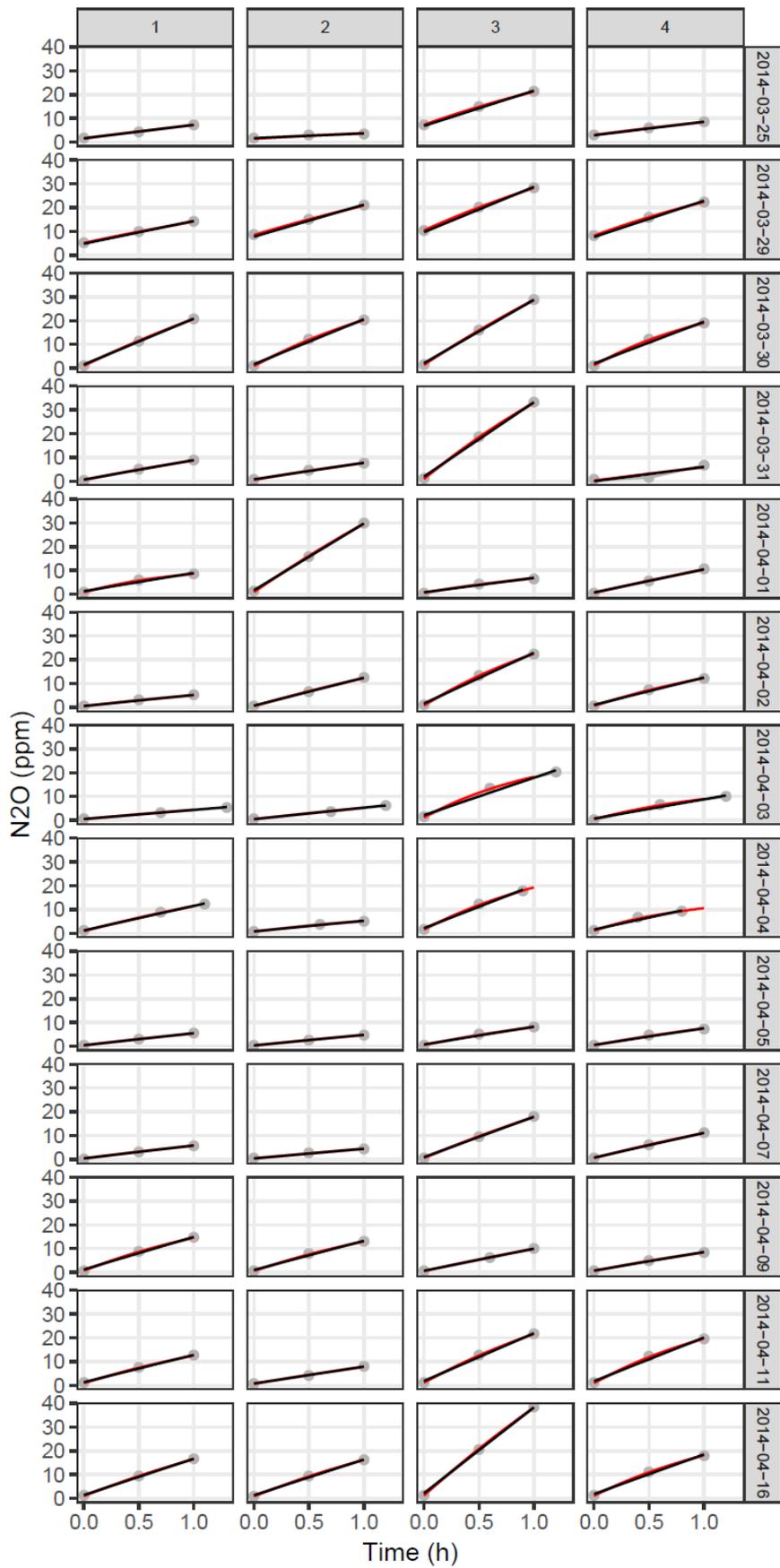
581 We also added this discussion in the revised manuscript, see page 11-12, Line 269-284.

582 *“To examine the potential bias in  $N_2O$  emissions when  $dC/dt$  is estimated with a linear regression*  
583 *model, we also calculated the results using a non-linear monomolecular model (Bolker, 2007). The*  
584 *monomolecular model is one of the simplest saturating functions and follows (Eq. 4):*

$$585 \quad C_{N_2O} = a_0 + a_1 (1 - \exp(-a_2/a_1 * t)) \quad (4)$$

586 *where  $C_{N_2O}$  is the mole fraction of  $N_2O$ ,  $a_0$  is the intercept corresponding to the  $N_2O$  mole fraction at*  
587 *time  $t = 0$ ,  $a_1$  is the horizontal asymptote at  $t = +\infty$ ,  $a_2$  is the slope ( $dC/dt$ ) at  $t = 0$ , and  $t$  is time after*  
588 *chamber placement (h).*

589  
590 *Chamber fluxes calculated using the non-linear  $dC/dt$  ( $Q_{chamber-non-linear}$ ) were 1.15 times higher than*  
591  *$Q_{chamber}$  estimated using linear regression. Comparing the concurrent fluxes of  $Q_{FG}$  and  $Q_{chamber-non-linear}$ ,*  
592 *we found the geometric mean of  $Q_{FG}/Q_{chamber-non-linear}$  to be 1.22 (confidence interval of 0.99 to 1.49).*  
593 *Using 10,000 bootstrap re-samples (Efron and Tibshirani, 1994), we computed 10,000 potential mean*  
594 *fluxes from the non-linear model, of which 9540 of the means were greater than 1, and 460 were lower*  
595 *than 1. This result suggests the use of the non-linear  $dC/dt$  calculation has resulted in better agreement*  
596 *with the FG estimates.”*



598 **Fig. B.** the N<sub>2</sub>O concentration (ppm) changes with time (hour). The slope of the regression ( $dC/dt$ )  
599 using linear regression (black) and non-linear monomolecular model (red).

600

601 **Special comments**

602 Title. Agree with the reviewer, and the title has been changed.

603 P5, L109. We calculated the rate of  $dC/dt$  using a simple linear regression model. Following the  
604 reviewer's suggestion, we calculated the  $dC/dt$  using a non-linear monomolecular model.

605 We added couple of paragraphs in the revised manuscript, see page 11-12, Line 269-284. Refer to  
606 above text.

607 And Conclusions on page 12, Line 295-297.

608 " Our results showed that soil N<sub>2</sub>O emissions measured by FG and static chambers (linear  $dC/dt$ ) were  
609 statistically different, with fluxes from FG being on average 40% higher. Using a non-linear calculation  
610 of  $dC/dt$  in the chambers decreased the disagreement to 22%."

611

612 P6, L140. We have provided the precisions on page 6, Line 144-145. "OP-FTIR system measures  
613 multiple gas concentrations (N<sub>2</sub>O, CH<sub>4</sub>, NH<sub>3</sub>, CO<sub>2</sub>, CO and water vapour) with high precision (N<sub>2</sub>O < 0.3  
614 ppb, CH<sub>4</sub> < 2 ppb, NH<sub>3</sub>, 0.4ppb, CO<sub>2</sub>, 1 ppm, CO, 0.1 ppb, and water vapour < 5%)."

615 P7, Line 170-171 and Fig.2. The background N<sub>2</sub>O flux is about 0.6 mg N<sub>2</sub>O-N m<sup>-2</sup> h<sup>-1</sup> prior to manure  
616 application. In this study, the topsoil (0–15 cm) had high N contents: 52 mg NH<sub>4</sub><sup>+</sup>-N kg<sup>-1</sup> and 118 mg  
617 NO<sub>3</sub><sup>-</sup>-N kg<sup>-1</sup> before manure application. Therefore, the high background N<sub>2</sub>O flux is reasonable.

618 P8, Line 192-193. We agree with the reviewer. We made the changes to be "agreement with the FG  
619 measurements in terms of the long-term background exchange patterns...". See page 9, Line 222.

620 P10. Line 237. As suggested, we calculated the chamber fluxes using the rate of  $dC/dt$  estimated  
621 using non-linear monomolecular model. The changes can be seen on page 11-12, Line 269-284, and  
622 Conclusions, Line 295-297.

623 P10, Line 247-248. We agree with the reviewer. As mentioned previously, we conducted a footprint  
624 analysis using Windtrax dispersion model, and added the results at page 7-8, Line 166-188 and  
625 Figure 2. We also removed the statement "In addition, concerns about FG arise if the  
626 fetch...occurring upwind of our sites." The changes can be seen on page 12, Line 286-288.

627 P 11, Line 249-250. The reviewer is correct. We have addressed this comment and added the footprint  
628 analysis results on page 7-8, Line 166-188. Refer to the above text.

629

630 P11. Conclusion, Line 263-265. In the Conclusions, we added a sentence “*Our results showed that soil*  
631 *N<sub>2</sub>O emissions measured by FG and static chambers (linear dC/dt) were statistically different, with*  
632 *fluxes from FG being on average 40% higher. Using a non-linear calculation of dC/dt in the chambers*  
633 *decreased the disagreement to 22%.” see page 12, Line 295-297.*

634 Our study supports the statement that chamber measurements underestimate the fluxes. See page  
635 13, Line 301-303.

636 “*However, the relationship we observed, together with other reports on the biases created by chamber*  
637 *calculation procedures, supports an interpretation that our FG emission calculations were accurate*  
638 *and in this instance the chamber measurements were biased too low.”*

639

#### 640 **Technical Corrections**

641 P1. Abstract. Agree with the reviewer, the changes have been made.

642 P1, Line 12. Agree. Have added “aerodynamic” and removed “micrometeorological”. See page 1, Line  
643 13, and P3, Line 59.

644 P2, Line 42. Agree. “manually operated” has been added to “static chambers”, see page 2, Line 43.

645 P2, Line 44. Agree. Change has been made to be “The temporal variation issue can be addressed by...”,  
646 see page 2, Line 45.

647 P3, Line 59-60. We agree with the reviewer. Change has been made to be “an estimate of the turbulent  
648 diffusivity”, see page 3, Line 61.

649 P4, Line 86. Agree with the reviewer. The sentence has been changed to be “The average daily  
650 minimum and maximum temperature were 6 and 33°C, respectively.” See page 4, Line 87.

651 P5, Eq. 1. Agree. We have modified the equation, see page 5, Line 107-113.

652

653 
$$Q_{chamber} = K_{N_2O} (273/T) (V/A) dC/dt \quad (1)$$

654 where  $Q_{chamber}$  is the gas flux ( $\mu\text{g N}_2\text{O-N m}^{-2} \text{ h}^{-1}$ );  $K_{N_2O}$  is  $1.25 (\mu\text{g N } \mu\text{L}^{-1})$  according to the ideal gas law,  
655 where  $K_{N_2O} = P m/R T_0$ , and  $P$  is air pressure (at 1 atm),  $m$  is molecular mass ( $28 \text{ g mol}^{-1}$ ),  $R$  is gas  
656 constant ( $0.0821 \text{ L atm K}^{-1} \text{ mol}^{-1}$ ), and  $T_0$  is 273 K;  $T$  is the air temperature within the chamber (K);  $V$  is

657 *the total volume of headspace (L); A is a surface area inside the chamber (m<sup>2</sup>); and dC/dt is the rate of*  
658 *change in mole fraction of N<sub>2</sub>O in the chamber (μL L<sup>-1</sup> h<sup>-1</sup>) determined by linear regression model. The*  
659 *N<sub>2</sub>O mole fraction is provide by GC, in ppm.”*

660 P6, Line 126. Because the path height is a function of x, when “kappa” is integrated with x, there is an  
661 implicit integration with z. Therefore, there is no error in the formula and the statement.

662 P7, Line 153-154. Agree. The sentence has been modified as “...at a frequency of 10 Hz.” See page 7,  
663 Line 160.

664 P7, Line 155. Agree. The sentence has been changed to be “Atmospheric stability parameters of  
665 friction velocity ( $u^*$ ), surface roughness ( $z_0$ ) and Obukhov stability length ( $L$ ) were calculated from the  
666 ultrasonic anemometer data.” See page 7, Line 162-163.

667 P7, Line 168. We agree with the reviewer. The subtitle has been changed to be “The flux gradient  
668 fluxes”. See page 8, Line 197.

669 P9, Line 200. We agree with the reviewer. The subtitle has been changed to “Comparison of the two  
670 measurement techniques”. See page 10, Line 229.

671 P10, Line 235. We agree with the reviewer. The sentence has been changed to be “Several researchers  
672 have reported that chamber flux calculation procedures introduced large uncertainty in N<sub>2</sub>O  
673 emissions.”, see page 11, Line 264.

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