

1 **Multiple scattering correction factor of quartz filters and the effect of filtering particles**
2 **mixed in water: implications to analyses of light-absorption in snow samples**

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13
14 **Abstract**

15 The deposition of light-absorbing aerosols (LAA) onto snow initiates processes that lead to increased
16 snowmelt. Measurements of LAA, such as black carbon (BC) and mineral dust, have been observed
17 globally to darken snow. Several measurement techniques of LAA in snow collect the particulates on
18 filters for analysis. Here we investigate micro-quartz filters optical response to BC experiments where
19 the particles initially are suspended in air or in a liquid. With particle soot absorption photometers
20 (PSAP) we observed a 20% scattering enhancement for quartz filters compared to the standard PSAP
21 Pallflex filters. The multiple-scattering correction factor (C_{ref}) of the quartz filters for airborne soot
22 aerosol is estimated to ~ 3.4 . In the next stage correction factors were determined for BC particles mixed
23 in water and also for BC particles both mixed in water and further treated in an ultrasonic bath.
24 Comparison of BC collected from airborne particles with BC mixed in water filters indicated
25 approximately a factor of two higher mass absorption cross section for the liquid based filters, probably
26 due to the BC particles penetrating deeper in the filter matrix. The ultrasonic bath increased absorption
27 still further, roughly by a factor of 1.5 compared to only mixing in water. Application of the correction
28 functions to earlier published field data from the Himalaya and Finnish Lapland yielded MAC values
29 of $\sim 7 - 10 \text{ m}^2 \text{ g}^{-1}$ at $\lambda = 550 \text{ nm}$ which is in the range of published MAC of airborne BC aerosol.

30
31 **1 Introduction**

32 Soot refers to carbonaceous particles formed during the incomplete combustion of hydrocarbon fuels,
33 and includes black carbon (BC) and organic carbon (OC), but can also include other elements, such as
34 sulfates. As the most light-absorbing aerosol (LAA) by unit per mass, BC is highly efficient in absorbing
35 solar radiation, and is a vital component in Earth's radiative balance (Bond et al., 2013). Once the

36 particles are scavenged from the atmosphere, possibly far from their emission source, BC can reach a
37 snow surface and decrease the snow reflectivity (Warren and Wiscombe, 1980; Flanner et al., 2007).
38 This will lead to accelerated and increased snowmelt, observed in different snow environments across
39 the globe (see e.g. recent review by Skiles et al., 2018). Perhaps most notably is High Mountain Asia
40 and its extensive cryosphere, where large emission sources of LAA in close proximity is affecting the
41 region's snow and ice (e.g. Xu et al., 2009; Gertler et al., 2016; Zhang et al., 2017).

42

43 There are a variety of methods for measuring BC, which is reflected in BC being operationally defined.
44 A common practice is to measure the change in transmission of a filter collecting aerosol. The measured
45 signal (i.e. optical depth of the filter) is thereafter applied with correction factors to generate
46 atmospheric concentrations of so-called equivalent black carbon (eBC) according to the BC
47 nomenclature (Petzold et al., 2013). The correction factors account for: 1) the loading of aerosol on the
48 filter since the detection signal decreases with increased aerosol content; 2) the multiple scattering of
49 light that is enhanced in the filter substrate; 3) and the enhancement from the deposition of other light
50 scattering aerosol. One instrument used for light absorption measurements is the Particle Soot
51 Absorption Photometer (PSAP), utilizing Pallflex filters. As an alternative for the optical filter analysis
52 of eBC, another approach is to apply the thermal-optical method (TOM), providing organic carbon (OC)
53 and elemental carbon (EC) mass of the aerosol on the filter. With this method, EC refers to the carbon
54 content of carbonaceous matter (Petzold et al., 2013), and can be assumed to be the main light-absorbing
55 element of BC. The technique involves a stepwise heating procedure, therefore creating a need to use
56 micro quartz fiber filters. These filters have been used in numerous studies with filtering snow and ice
57 samples, and thereafter analyzed to determine the EC and OC content of the samples (e.g. Hagler et al.,
58 2007; Forsström et al., 2009; Meinander et al., 2013; Ruppel et al., 2014; Zhang et al., 2017). In
59 Svensson et al. (2018), measurements with TOM were combined with an additional transmittance
60 measurement to further investigate the relative contribution from BC and other LAA particles present
61 in snow samples. The study involved laboratory tests, as well as comparisons to ambient snow samples
62 taken from different environmental settings. One lesson from this study was that the optical properties
63 of absorbing particles on quartz filters must be better understood. In particular when using melted snow
64 samples.

65

66 The overarching goal of this paper is to further investigate micro quartz fiber filters optical behavior
67 when sampling BC particles in a liquid (to simulate snow sampling). An advantage of using these filter
68 is that the sample can be analysed readily using TOM to arrive to an EC concentration on the filter
69 (where MAC values are not needed). The aim is pursued through a series of laboratory studies. Our
70 approach is to compare the use of quartz fibre filter for air and liquid samples to the much better
71 characterized Pallflex type filter used in commercial PSAPs. Hence, we are not intending to determine
72 a universal MAC value, but rather to understand differences in the observations that might be due to

73 the filter substrate or handling of the sample. We do not intend to answer all possible issues with filter
74 sampling, but will concentrate on the difference using the two filter types in air samples, the difference
75 between air and liquid samples with respect to the quartz fibre filter, and finally the potential effect
76 from treating the liquid samples using ultrasound.

77

78 **2 Materials, instruments, and data analyses**

79 **2.1 Soot aerosol production and sampling**

80 A schematic picture of the experiment is presented in Fig. 1, and the methods used in each step are
81 outlined in the subsections (2.1.1 and 2.1.2) below, as well as the instrumentation used (sections under
82 2.2). Section 2.3 explains the data processing. The soot used consisted of particles collected by chimney
83 cleaners in Helsinki, Finland, and this particular soot batch is from small-scale oil-based burning. The
84 same soot has been applied in different experiments previously (Peltoniemi et al., 2015; Svensson et
85 al., 2016; 2018).

86

87 **2.1.1 Airborne sampling**

88 Soot aerosol were sampled onto filters in an airborne phase and as a part of liquid solution. In the
89 airborne aerosol tests, soot was blown into a cylindrical experimental chamber (0.8 m height \times 0.45 m
90 diameter) through a stainless steel tube (25 mm outer diameter) consisting of a y-shaped bend of 130°,
91 creating a size-separation of the aerosol. Essentially a virtual impactor, this set-up allowed the smaller
92 sized particles to continue with the airflow into the chamber, while the larger (and heavier) particles
93 were deposited into a waste pipe through inertial separation (see section 2.2.3 for further description
94 and results in section 3.1.1.). From the experimental chamber a sample inlet (copper, 6 mm outer
95 diameter) simultaneously fed two PSAPs and a portable aerosol spectrometer (Grimm 1.108). One of
96 the PSAPs had quartz fiber filter punches mounted, while the other had standard PSAP filters installed.
97 This set-up was alternated among the PSAPs in between the experimental runs during the experiment,
98 to have both PSAPs assessed with the different filters. In total, 22 different experimental rounds were
99 made with various amounts of aerosol deposited to the substrates.

100

101 **2.1.2 Liquid sampling**

102 In the liquid experiments, the same soot batch and procedure were used as above, but the outlet pipe
103 was submerged into a 20 L container filled with deionized, purified Milli-Q (MQ) water. From this
104 liquid solution, different small amounts (between 10-100 mL) were extracted and mixed with additional
105 MQ water to further dilute the sample (to a typical total volume of 400 mL). This was performed to get
106 a range of filters with different EC concentrations and optical depths. The total number of liquid-

107 generated filters was 35. Some selected liquid samples (n=10) were exposed to an ultrasonic bath (for
108 at least 15 mins) prior to filtration. All of the liquid solutions were filtered onto the same quartz filters
109 used in the airborne test, applying the same filtering principles and analysis procedures as used
110 previously (Svensson et al., 2018). Punches from dried filters had their transmittance first measured
111 using a PSAP, followed by EC concentration measurements (TOM). This procedure was also applied
112 to the quartz filters from the airborne experiment.

113

114 **2.2 Instruments**

115 **2.2.1 Absorption measurements**

116 Absorption was measured with two Radiance Research 3-wavelength PSAPs (S/N 90 and S/N 100) at
117 $\lambda=467$ nm, 530 nm, and 660 nm (Virkkula et al., 2005). One of them was loaded with Pallflex E70-
118 2075W filter that is generally used with the instrument, while the other was loaded with micro quartz
119 fiber filters (Munktell, grade T293). The flows were calibrated with a Gilian Gilibrator bubble flow
120 meter and set to 0.5 LPM. Higher flow rates were not used here since the quartz filter tends to be more
121 fragile and may not withstand higher flows. The sample spot diameters of the PSAPs were measured
122 with an Eschenbach scale loupe with a 0.1 mm graduation ten times each. The average diameters (\pm
123 standard deviation) were 5.04 ± 0.10 mm and 5.05 ± 0.10 mm, giving corresponding spot areas of 19.9
124 ± 1.6 mm² and 20.0 ± 1.6 mm². The aim was to use identical face velocities, i.e. average velocity of
125 aerosol perpendicular to the filter (e.g. Müller et al., 2014) through both filter materials. The essentially
126 identical spot areas meant also that we had tuned the flow rates identical. In addition, to study whether
127 the PSAPs themselves affect the results we used both filter materials alternatingly, as mentioned above,
128 resulting in half of the 22 quartz filter samples being collected on the PSAP S/N 100, and the other half
129 on the PSAP S/N 90. Another custom-built 1-wavelength PSAP ($\lambda=526$ nm; Krecl et al., 2007) used in
130 Svensson et al (2018), was also utilized in for transmittance analysis of all the filters after their
131 production in the airborne- and liquid experiments.

132

133 **2.2.2 EC measurements**

134 Punches (typically with an area of 0.64 cm²) taken from the quartz filters were determined for their OC
135 and EC content with a Sunset Laboratory OCEC-analyzer (Birch and Cary, 1996), using the
136 EUSAAR_2 protocol (Cavalli et al., 2010). The analysis procedure is based on step-wise increases in
137 temperature in a helium atmosphere for the first stage, during which OC is detected with a flame
138 ionization detector. The second phase of the analysis consists of introducing oxygen into the
139 temperature increases and the detection of EC. Pyrolysis of OC during the first phase is monitored by a
140 continuous laser transmittance measurement. Once the transmittance has reached the initial value for
141 the filter in the second phase, a separation split-point between OC and EC is established.

142

143 **2.2.3 Size distribution measurements**

144 During the airborne experiments a Grimm optical particle counter (OPC, 1.108) was used as a portable
145 aerosol spectrometer for particle size distributions. The OPC have been factory-calibrated with PSL
146 spheres that are white. Their scattering cross section is larger than that of BC particles which leads to
147 underestimation of particle diameter. We did not find published Grimm 1.108 calibrations with BC
148 particles in the literature, thus we approximated the effect. By using the cross sections modeled by
149 Rosenberg et al. (2012) we estimate that the diameters presented by the OPC are possibly lower by a
150 factor of 2. In Figure 2 we present both the original size distributions and those calculated by
151 multiplying the diameters by 2.

152

153 **2.3 Data processing**

154 Calculations are presented in a step-by-step procedure below. Loading corrections are routinely applied
155 to filter-based measurements of light absorption by atmospheric aerosol, but, for measurements of
156 absorption by melted and filtered snow samples it is not. In the former, absorption is calculated from
157 the product of a loading correction and the rate of change of transmittance, whereas in the latter the
158 absorption is generally calculated simply from the transmittance of the filter only. We therefore show
159 the equivalence of the two methods and that the loading corrections can and should be applied also to
160 melted and filtered snow samples. First, we present a generally use equation for calculating absorption
161 by aerosols, then how the multiple scattering correction factor C_{ref} appears in the equations, followed
162 by how we determined it for the quartz filters. The numerical values of two published loading
163 corrections are given as clearly as possible to save the reader from looking for constants from the
164 literature. Finally, we show the equivalence of calculating the mass absorption coefficients from
165 airborne aerosol and filtered snow samples.

166

167 A further note on data processing is important. The single-scattering albedo, ω_o , i.e. the ratio of
168 scattering and extinction coefficient, is a measure of the darkness of aerosols: for purely scattering
169 aerosols $\omega_o = 1$. For freshly-generated pure BC, it has been measured to be $\sim 0.2 \pm 0.1$ (Bond et al. 2013).
170 When pure BC particles get coated with some light-scattering material ω_o increases so that far from the
171 sources it is typically larger than 0.9 (e.g., Delene and Ogren, 2002). However, ω_o varies also with
172 particle size even for pure BC, in a way that it increases with increasing particle size as can be shown
173 by the simple Mie calculations in Fig 2b. Both the coating and particle size have consequences for the
174 analysis of BC in snow by filter-based absorption measurements. The coating of BC particles typically
175 consists of some water-soluble material such as sulfates, nitrates and organics. The size of BC particles
176 in snow has been shown to vary in a large range from $\sim 0.1 \mu\text{m}$ to $> 2 \mu\text{m}$ (e.g., Schwarz et al., 2013).

177 On the other hand, the estimation of absorption from filter-based attenuation measurements is affected
 178 also by scattering aerosol and therefore by ω_o (e.g., Arnott et al., 2005; Virkkula et al., 2005; Collaud
 179 Coen et al, 2010). Now, since we do not know the ω_o of the particles and we will apply the algorithm
 180 presented by Virkkula (2010) we will repeat the calculations with four different ω_o values. We use the
 181 size distribution measurements for estimating the size and the Mie modeling for estimating a realistic
 182 range of ω_o for the calculations.

183

184 2.3.1 Calculation of absorption in aerosols

185 The PSAP has been calibrated with the standard filter material Pallflex E70-2075W by Bond et al.
 186 (1999; here referred to as B1999) and Virkkula et al. (2005). Ogren (2010; here O2010) presented an
 187 adjustment to the Bond et al. (1999) calibration, while Virkkula (2010; here V2010) updated the
 188 Virkkula et al. (2005) calibration. In all of these the absorption coefficient is calculated as

$$189 \quad \sigma_{ap} = f(Tr_t) \frac{A}{Q\Delta t} \ln\left(\frac{Tr_{t-\Delta t}}{Tr_t}\right) - s\sigma_{sp} \quad (1)$$

190 where $f(Tr_t)$ is the loading correction function that depends on the transmittance $Tr_t = I_t/I_0$ where I_t is
 191 the light intensity transmitted through the filter at time t, I_0 the light intensity transmitted through a
 192 clean filter at time t = 0, A the spot area, Q the flow rate, and s the fraction of the scattering coefficient
 193 σ_{sp} that gets interpreted as absorption and gets usually called the apparent absorption and should be
 194 subtracted from the uncorrected absorption or be treated as presented by Müller et al. (2014). If apparent
 195 absorption can be considered negligible, equation 1 becomes

$$196 \quad \sigma_{ap} = f(Tr_t) \frac{A}{Q\Delta t} \ln\left(\frac{Tr_{t-\Delta t}}{Tr_t}\right) \quad (2)$$

197 In the present work, this approach was adapted for two reasons: 1) σ_{sp} was not measured during the
 198 calibration experiment and 2) the aerosol used in the experiment was very dark (soot from oil-based
 199 burning), thus the apparent absorption could be considered negligible.

200

201 The loading correction function $f(Tr)$ can be further rewritten as $f(Tr) = g(Tr)/C_{ref}$ where C_{ref} is the
 202 multiple scattering correction factor and $g(Tr)$ at $Tr = 1$ a loading correction function that equals one at
 203 $Tr = 1$ and increases when the filter gets darker, i.e., when $Tr < 1$.

$$204 \quad \sigma_{ap} = \frac{1}{C_{ref}} g(Tr_t) \frac{A}{Q\Delta t} \ln\left(\frac{Tr_{t-\Delta t}}{Tr_t}\right) \quad (3)$$

205 If there is only one time step $t = \Delta t$ and before sampling $Tr = 1$ then $Tr_{t-\Delta t} = Tr_{t=0} = 1$ and

$$206 \quad \sigma_{ap} = \frac{1}{C_{ref}} g(Tr_t) \frac{A}{V_t} \ln\left(\frac{1}{Tr_t}\right) = \frac{1}{C_{ref}} g(Tr_t) \sigma_0 \quad (4)$$

207 where V_t is the air volume drawn through the filter since the start of sampling at time t . The assumption
 208 of only one time step means (4) presents the absorption coefficient since the start of sampling on the
 209 filter. According to the Bouguer-Lambert-Beer law light intensity decreases exponentially as a function
 210 of the optical depth τ

$$211 \quad I_t = I_0 e^{-\tau}$$

$$\Leftrightarrow \tau = \ln\left(\frac{I_0}{I_t}\right) = \ln\left(\frac{1}{Tr_t}\right) \quad (5)$$

212 This is relevant especially in the present study since the purpose is to improve estimation of absorption
 213 in filtered snow samples. In the analysis of a snow sample there is only one "time step": I_0 is the intensity
 214 of light transmitted through a clean filter and I_t the intensity of light transmitted through a filter through
 215 which the melted snow sample has been filtered. Here the airborne data were also treated in a similar
 216 way: for each time step absorption was calculated from (4) since the start of sampling on the filter.

217

218 **2.3.2 Calculation of C_{ref} of quartz filters**

219 If we assume that the difference of the absorption coefficients of the PSAPs using the quartz and Pallflex
 220 filters, $\sigma_{ap}(Q)$ and $\sigma_{ap}(P)$, respectively, is due to the multiple scattering correction factors of the two
 221 materials only we can calculate

$$222 \quad C_{ref,Q} = \frac{\sigma_{ap}(Q)}{\sigma_{ap}(P)} C_{ref,P} \quad (6)$$

223 where $C_{ref,Q}$ and $C_{ref,P}$ are the multiple scattering correction factors of the quartz and Pallflex filters,
 224 respectively. However, this is an approximation only since the difference of $\sigma_{ap}(Q)$ and $\sigma_{ap}(P)$ is also
 225 due to the different transmittances Tr_Q and Tr_P of the two filter materials at each time step and
 226 consequently different values of the loading correction. However, below we will use (6) for the
 227 estimation of $C_{ref,Q}$.

228

229 The $C_{ref,P}$ values for Pallflex E70-2075W filter were calculated here from two published calibration
 230 experiments. The loading correction function of B1999 (with the O2010 adjustment) can be
 231 reformulated as

$$232 \quad f(Tr) = \frac{1}{1.5557 \cdot Tr + 1.0227} \quad (7)$$

233 This can be further rewritten as

$$234 \quad f(Tr) = \frac{1}{C_{ref}} g(Tr) = \frac{1}{2.5784} \frac{1}{0.6034 \cdot Tr + 0.3966} \quad (8)$$

235 where $C_{ref} = 2.5784$. Similarly, the V2010 loading correction can be rewritten as

$$\begin{aligned}
 f(Tr) &= (k_0 + k_1(h_0 + h_1 \omega_0) \ln(Tr)) = k_0 \left(1 + \frac{k_1}{k_0} (h_0 + h_1 \omega_0) \ln(Tr) \right) \\
 &= \frac{1}{C_{ref}} g(Tr) = \frac{1}{C_{ref}} \left(1 + \frac{k_1}{k_0} (h_0 + h_1 \omega_0) \ln(Tr) \right)
 \end{aligned}
 \tag{9}$$

where h_0 , h_1 , k_0 , and k_1 are the constants presented in Table 1 in V2010 and the single-scattering albedo $\omega_0 = \sigma_{sp}/(\sigma_{sp} + \sigma_{ap})$. For the three wavelengths (10) becomes

$$f_{467}(Tr_{467}) = \frac{1}{2.653} (1 - 1.698(1.16 - 0.63 \cdot \omega_0) \ln(Tr_b)) \tag{10}$$

$$f_{530}(Tr_{530}) = \frac{1}{2.793} (1 - 1.788(1.17 - 0.71 \cdot \omega_0) \ln(Tr_g)) \tag{11}$$

$$f_{660}(Tr_{660}) = \frac{1}{2.841} (1 - 1.915(1.14 - 0.72 \cdot \omega_0) \ln(Tr_r)) \tag{12}$$

with $C_{ref,467} = 2.653$, $C_{ref,530} = 2.793$, and $C_{ref,660} = 2.841$.

When C_{ref} has been determined it is assumed that $g(Tr)$ is the same for both filter materials.

2.3.3 Calculation of mass absorption coefficient (MAC)

If m_{EC} is the mass of EC in the filter (corresponding to the spot area) through which the air volume of V_t has flown the average mass concentration of EC in aerosol in the air volume is $c_{EC,aerosol} = m_{EC}/V_t$. If σ_{ap} is the absorption coefficient calculated from (4), the mass absorption coefficient (MAC) can be calculated from

$$\text{MAC} = \frac{\sigma_{ap}}{c_{EC,aerosol}} = \frac{\frac{1}{C_{ref}} g(Tr_t) \frac{A}{V_t} \tau}{\frac{m_{EC}}{V_t}} = \frac{\frac{1}{C_{ref}} g(Tr_t) A \tau}{m_{EC}} = \frac{\frac{1}{C_{ref}} g(Tr_t) \tau}{\frac{m_{EC}}{A}} = \frac{f(Tr_t) \tau}{m_{EC}/A}$$

This applies for aerosol but also for the snow samples since the analysis of EC mass in a filter yields the mass surface density m_{EC}/A in where m_{EC} is the mass of EC in the analyzed filter spot that has the area A . In Svensson et al. (2018) we calculated apparent MAC values of EC in snow samples simply from $\text{MAC} = \tau/(m_{EC})$ without applying additional corrections for filter loading, neither enhanced absorption by the filter medium, nor light scattering particles. Assuming that only loading and filter effects apply in the experiments presented here, the apparent MAC values presented were adjusted by using $f(Tr,Q) = g(Tr)/C_{refQ}(Q)$.

3 Results and discussion

3.1 Airborne aerosol experiment

Through our 22 airborne aerosol samples, we aimed at getting a range of transmittances and EC concentrations in the filters for the regression analysis. The original goal was to control the final transmittances by the length of the sampling time, however, this was not always successful (as noted in

264 Table 1). Without dilution the aerosol concentration in the mixing chamber was very high with
265 attenuation coefficients σ_0 in the range of $\sim 60000 - \sim 90000 \text{ Mm}^{-1}$ (see samples 1 and 2, Table 1).
266 Therefore we added a dilution valve (V1) and a HEPA filter (Fig. 1) after the first couple of experiment
267 runs, and had variations in the sample air to clean filtered air ratio, which lead to lower σ_0 in the range
268 of $\sim 1000 - \sim 30000 \text{ Mm}^{-1}$. The system was not always stable, resulting in different measured
269 concentrations for similar sampling times.

270

271 **3.1.1 Particle size distribution**

272 The average size distribution measured with the Grimm 1.108 OPC shows that most particles larger
273 than $1 \mu\text{m}$ (Fig. 2a) were efficiently removed from the air stream with the pre-separator (Fig. 1). This
274 is uncertain, however, since the OPC has been calibrated with white PSL spheres (as discussed in 2.2.3).
275 Another important point is that the lower limit of the sizes the OPC measured was 300 nm , and is
276 probably even higher due to the above-mentioned calibration error. The particle number size
277 distribution, nevertheless, suggests that there were large numbers of BC particles smaller than the OPC
278 detects since the particle number concentration increases sharply with decreasing particle diameter (Fig.
279 2a).

280

281 The mass absorption and scattering coefficients, MAC and MSC, respectively, and single-scattering
282 albedo ω_0 of single BC particles at $\lambda = 530 \text{ nm}$ were modeled with the Mie code of Barber and Hill
283 (1990) and the complex refractive index of $1.85 - 0.71i$ and a particle density of 1.7 g cm^{-3} . Comparison
284 of single-particle ω_0 size distribution (Fig. 2b) with the particle number size distribution (Fig. 2a)
285 suggests ω_0 varied in the range of $\sim 0.3 - 0.5$. Modeling for the size distribution measured with the OPC
286 yielded $\omega_0 \approx 0.51$ and 0.54 when using the original OPC diameters and the diameters multiplied by 2,
287 respectively. These ω_0 values can be considered as upper estimates considering that a large fraction of
288 small particles were undetected. However, to take the ω_0 uncertainty into account we calculated all
289 V2010-related values by using four ω_0 values: 0.3, 0.4, 0.5, and 0.6.

290

291 **3.1.2 Comparison between custom built and commercial PSAPs**

292 The optical depths presented in Svensson et al. (2018) were measured with the custom-made PSAP of
293 Stockholm University at $\lambda = 526 \text{ nm}$, which is slightly different than the commercial Radiance Research
294 PSAP ($\lambda = 530 \text{ nm}$). Therefore, before applying the corrections (determined in section 3.1.3 below) we
295 examined whether the transmittances measured with these two PSAPs agree. Transmittances of all
296 Pallflex and quartz filters were measured with both instruments. The resulting scatter plot (Fig. 3) shows
297 that the agreement is excellent between the PSAPs, thus we concluded that the corrections established
298 in this paper could be applied to the results presented by Svensson et al. (2018).

299

3.1.3 Estimation of the multiple-scattering correction factor C_{ref} for the quartz filter

Optical depths (τ) for both the Pallflex and quartz filters, $\tau(\text{P})$ and $\tau(\text{Q})$, respectively, were calculated from (5) at a 1-second time resolution. The $\tau(\text{Q})$ -to- $\tau(\text{P})$ ratios – here the τ ratio – got a wide range of values at 1-second time resolution but most of them were > 1 : 99.6 % of $\tau(\text{Q})/\tau(\text{P}) > 1$ and the average and median ratios were 1.21 and 1.16, respectively. To study how the τ ratio depends on filter loading the data were classified into transmittance bins of a 0.025 width in the $\text{Tr}(\text{P})$ range of 0.3 – 1.0 and the averages and medians were calculated for each bin (shown in Fig. 4). The transmittance dependence of the τ ratio of individual samples was often controversial: in some samples it decreased from the beginning, in some samples it increased. We do not have an explanation of this although the high concentrations in the mixing chamber – see the attenuation coefficients σ_0 in Table 1 – are probably largely the factor behind this observation. However, for all data the average and median τ ratio depended on the filter transmittance, so that for a fresh clean filter at $\text{Tr} > 0.9$, it was higher than for heavily-loaded filters at $\text{Tr} < 0.4$ (Fig. 4). In addition to the 1-second data the τ ratio at the end of each sampling period are plotted as a function of transmittance of the Pallflex filter in Fig. 4. For the end values of all samples there was no clear Tr dependence. The most important conclusion in Fig. 4 is that the τ ratio of the two filter materials depends on the filter transmittance. On the average the ratio decreases with increasing loading even though the same amount of BC is collected on both filters. That suggests that the loading corrections to be applied depend on the filter material and that they do not differ just by a constant factor.

319

In sample runs 4, 5, 7, 16, 18, 19, and 20 the decrease of Tr was relatively slow and we considered the bin averages and medians calculated from them to be the most suitable to be used for determining C_{ref} . Sample 17 was also long, taking more than six minutes. Despite the similar settings used for filling the mixing chamber and the diluter, the τ ratio was completely different from the rest of the samples (Fig. 4). This outlier was therefore excluded from the analysis.

325

The two correction algorithms (B1999 and V2010) were next applied to both filter materials and $\sigma_{\text{ap}}(\text{Q})$ and $\sigma_{\text{ap}}(\text{P})$ (at $\lambda = 530$ nm) were calculated from (4) by using the Tr bin averages and median of σ_0 and then the ratio of these two, $\sigma_{\text{ap}}(\text{Q})/\sigma_{\text{ap}}(\text{P})$. When the constants within the correction methods, including the C_{ref} , were the same for both filter materials the ratio is close to 1.2 (Fig. 5). As mentioned previously, V2010 depends also on ω_0 , and due to the fact that we are unsure of the ω_0 of the aerosol, we present four lines ($\omega_0 = 0.3$, $\omega_0 = 0.4$, $\omega_0 = 0.5$, and $\omega_0 = 0.6$) in Fig. 4. The B1999 correction yields a slightly decreasing $\sigma_{\text{ap}}(\text{Q})/\sigma_{\text{ap}}(\text{P})$, suggesting that only adjusting C_{ref} would not be enough. The V2010 correction does not yield a clear Tr dependence of $\sigma_{\text{ap}}(\text{Q})/\sigma_{\text{ap}}(\text{P})$ although it has high $\sigma_{\text{ap}}(\text{Q})/\sigma_{\text{ap}}(\text{P})$

334 values in the $\text{Tr}(\text{P})$ range 0.6 – 0.85. They correspond to the local maxima of the average and median τ
 335 ratio shown in Fig. 4. Nevertheless, there is not enough data in this study to robustly test the correction
 336 algorithms. Therefore, all values are calculated with both of them. We calculated next the multiple-
 337 scattering correction factor C_{ref} from (7) by using the $\text{Tr}(\text{P})$ bin averages of $\sigma_{\text{ap}}(\text{Q})/\sigma_{\text{ap}}(\text{P})$. The averages
 338 and standard deviations over the $\text{Tr}(\text{P},530)$ range of 1 – 0.3 and for averaging of all the four single
 339 scattering albedos $\omega_o = 0.3$, $\omega_o = 0.4$, $\omega_o = 0.5$ and $\omega_o = 0.6$ are presented in Table 2. It is worth noting
 340 that $C_{\text{ref}} \approx 3.4$ at $\lambda = 530$ nm is close with published values for another commonly used absorption
 341 photometer, the Aethalometer, that uses quartz filters backed with supporting cellulose fibers. For
 342 instance, values around 3.5 were reported by Segura et al. (2014), Zanatta et al. (2016), and Backman
 343 et al. (2017).

344

345 **3.2 Comparison of τ vs EC of soot mixed in water with airborne particles**

346 The slopes of the optical depths ($f\tau$) vs. EC concentrations, when applying the transmittance-dependent
 347 loading correction $f(\text{Tr},\text{Q},\text{V2010}, \omega_o = 0.4)$, were different, and depended on how the soot aerosol were
 348 deposited onto the filter (Fig. 7a and b). For the airborne aerosol, the slope is $6.4 \pm 0.2 \text{ m}^2 \text{ g}^{-1}$; while the
 349 particles mixed in water (without the ultrasonic treatment) have a slope that is doubled ($12.6 \pm 0.5 \text{ m}^2$
 350 g^{-1}). Applying $\omega_o = 0.5$ and $\omega_o = 0.6$ loading corrections, the slopes of the airborne particles are $6.1 \pm$
 351 $0.2 \text{ m}^2 \text{ g}^{-1}$ and $5.7 \pm 0.20 \text{ m}^2 \text{ g}^{-1}$, respectively; while the slopes of the particles mixed in water (without
 352 the ultrasonic treatment) are $12.0 \pm 0.4 \text{ m}^2 \text{ g}^{-1}$, and $11.3 \pm 0.4 \text{ m}^2 \text{ g}^{-1}$. The ratios for airborne to liquid
 353 particles are 0.506 ± 0.026 , 0.507 ± 0.026 , and 0.508 ± 0.025 for the three choices of ω_o in the
 354 calculation. The difference in slope between the airborne and liquid particles is likely an effect of
 355 penetration depth of the soot particles into the filter media, with the higher slope for liquid particles
 356 reflecting a deeper penetration. Nevertheless, the ratio is named as the water-mixing factor $f_w \approx 0.51 \pm$
 357 0.03 . In comparison, using $f(\text{Tr},\text{B1999})$ for the airborne and the water-mixed particles the slopes for
 358 optical depth $f\tau$ vs. EC concentration are $4.33 \pm 0.13 \text{ m}^2 \text{ g}^{-1}$ and $8.31 \pm 0.22 \text{ m}^2 \text{ g}^{-1}$, respectively,
 359 providing a ratio of $f_w \approx 0.52 \pm 0.02$, essentially identical to that obtained from the V2010 correction.

360

361 The slope of $f\tau$ vs. EC of the 24 analyzed samples treated in the ultrasonic bath was even higher (Fig.
 362 6a and b), reflecting a probable greater penetration depth of the particles. When $f(\text{Tr},\text{Q},\text{V2010})$ is
 363 calculated with $\omega_o=0.4$, $\omega_o=0.5$ and $\omega_o=0.6$, the slopes of $f\tau$ vs. EC of the particles mixed in water with
 364 the ultrasonic treatment were $18.7 \pm 0.8 \text{ m}^2 \text{ g}^{-1}$, $17.8 \pm 0.8 \text{ m}^2 \text{ g}^{-1}$, and $16.9 \pm 0.7 \text{ m}^2 \text{ g}^{-1}$, respectively.
 365 The average \pm uncertainty of the ratios of the slopes of airborne and water-mixed particles with the
 366 ultrasonic treatment is very stable, 0.34 ± 0.02 . If we consider this value to be a product of a factor f_s
 367 representing the ultrasonic treatment and the above-presented factor f_w we obtain the value $f_s \approx 0.67 \pm$
 368 0.04 . When $f(\text{Tr},\text{B1999})$ is used also for the water-mixed and ultrasonic-bath-treated particles the slope

369 of corrected optical depth $f\tau$ vs. EC concentration is $12.9 \pm 0.4 \text{ m}^2 \text{ g}^{-1}$, with the corresponding $f_s \approx 0.65$
 370 ± 0.03 .

371

372 The factors are used for multiplying $f(\text{Tr}, \text{Q}) = g(\text{Tr})/C_{\text{ref}}(\text{Q})$, and so another way it can be interpreted is
 373 that they affect the multiple scattering correction

374

$$f_s f_w f(\text{Tr}) = \frac{1}{\frac{1}{f_s} \frac{1}{f_w} C_{\text{ref}}} g(\text{Tr})$$

375 In other words, $C_{\text{refSW}}(\text{Q}) = C_{\text{ref}}(\text{Q})/(f_w f_s)$ and $C_{\text{refW}}(\text{Q}) = C_{\text{ref}}(\text{Q})/f_w$ for BC particles mixed in water and
 376 filtered through quartz filters with and without an ultrasonic bath, respectively. The values are presented
 377 in Table 2. The uncertainties of $C_{\text{refW}}(\text{Q})$ and $C_{\text{refSW}}(\text{Q})$ were calculated with a standard error propagation
 378 formula by using the standard deviations of C_{refS} in Table 2 and the above-presented uncertainties of f_w
 379 and f_s .

380

381 To visualize the combined effects of the loading correction functions and the two factors f_w and f_s they
 382 are plotted as a function of τ in Fig. 8. The corresponding transmittances are shown in the secondary x
 383 axis. The range of optical depths of EC in snow presented by Svensson et al. (2018) are also shown in
 384 the figure. It is obvious that the transmittances through those filters were much lower than $\text{Tr} = 0.3$ used
 385 in the PSAP calibration in V2010 and even more lower than the $\text{Tr} = 0.6$ recommended in the World
 386 Meteorological Organization and Global Atmosphere Watch (WMO/GAW, 2011) standard operating
 387 procedures. However, since there is no published calibration for such low transmittances and high
 388 optical depths τ the approach of extrapolating is the best that can be done. Figure 8 also shows how
 389 V2010 and B1999 corrections are close to each other at low τ , but for dark filters at $\tau \approx 2$ there is a
 390 factor of ~ 2 difference between them.

391

392 **3.3 Implications for field samples**

393 Previously published laboratory and ambient τ vs. EC regressions in Svensson et al. (2018), were
 394 updated with the above-developed corrections. Svensson et al. (2018) presented linear regressions of
 395 optical depth τ vs. EC of the same chimney soot we used in the present study, NIST soot (NIST-2975),
 396 and field samples from the Himalaya (India), and Finnish Lapland.

397

398 We multiplied the τ of the laboratory data of Svensson et al. (2018) with $f_s f_w f(\text{Tr}, \text{V2010}, \omega_o=0.4, \text{Q})$
 399 since an ultrasonic bath was used also in those experiments. The slopes of the chimney and NIST soot
 400 decreased from $\sim 40 \text{ m}^2 \text{ g}^{-1}$ and $\sim 35 \text{ m}^2 \text{ g}^{-1}$ to $11.9 \pm 0.9 \text{ m}^2 \text{ g}^{-1}$ and $9.6 \pm 0.6 \text{ m}^2 \text{ g}^{-1}$, respectively (Fig. 9a
 401 and b). In the scatter plot of the chimney soot the two data points with the highest EC concentration of
 402 $\sim 0.04 \text{ g m}^{-2}$ are possible outliers. When they are discarded from the regression the slope becomes $9.8 \pm$

403 $0.5 \text{ m}^2 \text{ g}^{-1}$, which is indicated by the red line in Fig. 9a. This is within the uncertainties and is essentially
404 the same as for the NIST soot.

405

406 These values are now in the order of published MACs, but for chimney and NIST soot still considerably
407 larger than the $6.4 \pm 0.2 \text{ m}^2 \text{ g}^{-1}$ obtained in the present work (section 3.2). The explanation to this
408 difference is not clear. However, the procedures of processing the chimney soot and the NIST soot were
409 not exactly identical to the one we used in the present work. Svensson et al. (2018) mixed both types of
410 soot manually in MQ water, added some ethanol in the solution and mixed samples with variable
411 amounts of MQ water before the ultrasonic mixing. In the present work instead, we blew the aerosol
412 through a virtual impactor into the MQ water, took samples of this solution and diluted the samples
413 before the mixing in the ultrasonic bath. The two major differences are the use of the size separation in
414 the present work and the use of ethanol by Svensson et al. (2018), with the explanation being due to
415 those.

416

417 For the re-evaluation of the field data presented by of Svensson et al. (2018) we multiplied the τ with
418 $f_w f(\text{Tr}, V_{2010}, \omega_o = 0.4, Q)$ since the field snow samples were melted and then filtered through the quartz
419 filters. The slopes of the field samples from the Indian Himalaya and from Finnish Lapland decreased
420 from $17.1 \pm 0.8 \text{ m}^2 \text{ g}^{-1}$ and $21.5 \pm 0.8 \text{ m}^2 \text{ g}^{-1}$ to $7.5 \pm 0.4 \text{ m}^2 \text{ g}^{-1}$ and $9.8 \pm 0.5 \text{ m}^2 \text{ g}^{-1}$, respectively (Fig
421 9c and 9d). All slopes above are in the range of published MAC of BC. For instance, Quinn and Bates
422 (2005) obtained MAC values ranging from 6 to $20 \text{ m}^2 \text{ g}^{-1}$, Bond and Bergstrom (2006) and Bond et al.
423 (2013) reviewed several articles and according to them the MAC of freshly-generated BC is
424 approximately $7.5 \pm 1.2 \text{ m}^2 \text{ g}^{-1}$ at $\lambda = 550 \text{ nm}$.

425

426 **4 Conclusions**

427 Through the airborne laboratory experiments conducted in this study we determined that the multiple
428 scattering effect is enhanced by about 20% with micro quartz filters compared to Pallflex filters. In
429 terms of the multiple-scattering correction factor, C_{ref} , of the quartz filters, we estimate it to be ~ 3.4 for
430 airborne sampled BC. It is worth noting that this is within the range of C_{ref} values published for the
431 Aethalometer, a very commonly used absorption photometer. The results of the airborne experiments
432 have also other implications. Atmospheric aerosols are often collected on quartz filters and analyzed
433 for EC concentration. The same filter samples can also be used for measuring light absorption to derive
434 the MAC. The analysis showed that if this is done the multiple scattering correction and loading
435 correction should be taken into account, just as they are in the data processing of online aerosol
436 absorption photometers.

437

438 Mixing BC particles in water and filtering the solution essentially doubled the attenuation of light
439 compared to airborne generated filters. This is probably explained by the fact that in the liquid phase
440 and the subsequent filtering the soot particles penetrate deeper into the filter media. Deeper in the filter
441 substrate, it is more likely that the light absorption effects are enhanced, and that way accounting for
442 the measured higher optical depth. In the airborne phase the depositional process is most probably
443 different, with the particulates accumulating in the surface layer of the filter.

444

445 When samples were mixed in an ultrasonic bath before filtering through quartz filters the attenuation
446 was further enhanced. The hypothesis for explaining the effect of the ultrasonic bath is that it possibly
447 breaks the chain-like structure of BC particles, resulting in smaller BC particles that are able to move
448 to further depths in the filter matrix. This remains to be confirmed, and can possibly be done with an
449 electron microscopy. More research on the sampling of BC from melted snow and ice onto filter media
450 is much needed.

451

452 All these effects mean that the absorption data obtained from melted snow samples have high
453 uncertainties. However, application of the correction functions to earlier published field data from the
454 Himalaya and Finnish Lapland yielded MAC values of $\sim 7 - 10 \text{ m}^2 \text{ g}^{-1}$ at $\lambda = 550 \text{ nm}$ which is in the
455 range of published MAC of airborne BC aerosol. This gives indirect support for the validity of the PSAP
456 calibration also for darker filters than used as the limit in atmospheric measurements.

457

458 **5 Data availability**

459 All data in this paper are available upon request.

460

461

462 **6 Competing interests**

463 The authors declare that they have no conflict of interest.

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622 Table 1. Main information on aerosol samples taken during the experiment. Sampling time, Tr:
 623 transmittances of Pallflex and quartz filters at $\lambda = 530$ nm at the end of each sample, σ_0 : attenuation
 624 coefficient, calculated without any loading corrections, $\tau(Q)/\tau(P)$: ratio of optical depths of quartz and
 625 Pallflex filters and EC: EC concentration in the quartz filter. The 1-second data from samples denoted
 626 with * were used for deriving C_{ref} of quartz filters. Samples 1 and 2 were taken from the mixing chamber
 627 without any dilution.

Sample number	Sampling time min	Tr		$\sigma_0(P)$	$\sigma_0(Q)$	$\tau(Q)/\tau(P)$	EC g m ⁻²
		Tr(P)	Tr(Q)	Mm ⁻¹	Mm ⁻¹		
1	0.55	0.314	0.279	84245	92840	1.102	0.172
2	0.43	0.493	0.458	65284	72082	1.104	0.113
3	1.82	0.544	0.487	13405	15842	1.182	0.094
4*	6.7	0.543	0.509	3646	4032	1.106	0.056
5*	11.8	0.746	0.702	993	1199	1.207	0.029
6	2.68	0.543	0.505	9103	10184	1.119	0.062
7*	12.13	0.224	0.216	4932	5052	1.024	0.195
8	0.6	0.609	0.592	33062	34950	1.057	0.027
9	0.88	0.823	0.797	8821	10275	1.165	0.014
10	0.67	0.913	0.902	5461	6188	1.133	0.016
11	1.38	0.931	0.923	2067	2317	1.121	0.027
12	0.32	0.915	0.904	11221	12749	1.136	0.012
13	0.57	0.927	0.913	5351	6425	1.201	0.009
14	0.65	0.814	0.781	12664	15211	1.201	0.011
15	2.93	0.704	0.664	4786	5584	1.167	0.032
16*	11.6	0.602	0.555	1750	2030	1.16	0.029
17	6.12	0.5	0.415	4533	5751	1.269	0.080
18*	11.92	0.401	0.354	3067	3486	1.136	0.113
19*	10.47	0.302	0.262	4576	5119	1.119	0.147
20*	6.97	0.402	0.367	5232	5755	1.1	0.113
21	3.6	0.6	0.558	5676	6482	1.142	0.055
22	2.1	0.849	0.833	3118	3480	1.116	0.017

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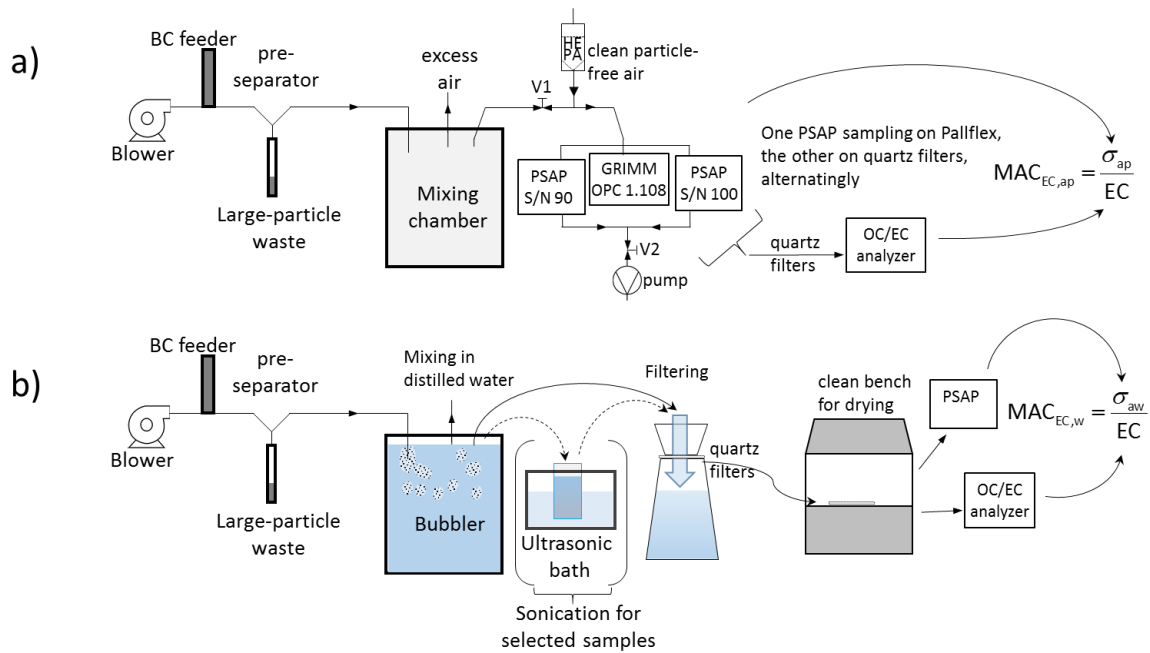
629 Table 2. Multiple-scattering correction factors of quartz filters. $C_{ref}(Q)$: derived here for airborne BC
 630 particles from published Pallflex filter loading corrections V2010 and O2010. $C_{refW}(Q)$: derived here
 631 for BC particles mixed in water and filtered through quartz filters. $C_{refSW}(Q)$: derived here for BC
 632 particles mixed in water and treated in an ultrasonic bath and filtered through quartz filters.

	Derived from V2010			Derived from O2010
	467 nm	530 nm	660 nm	same for all λ
$C_{ref}(Q)$	3.23 ± 0.04	3.41 ± 0.03	3.48 ± 0.09	3.08 ± 0.04
$C_{refW}(Q)$	6.4 ± 0.3	6.7 ± 0.3	6.9 ± 0.4	5.9 ± 0.2
$C_{refSW}(Q)$	9.5 ± 0.7	10.0 ± 0.8	10.2 ± 0.8	9.1 ± 0.6

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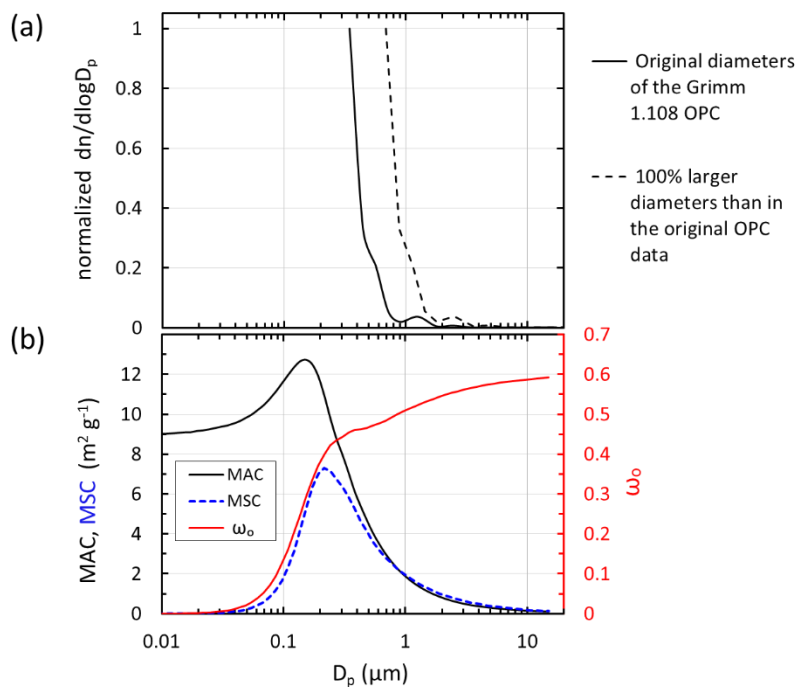
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635 **Figures**



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637 Figure 1. Experimental setup for the airborne (a), and for the liquid (b) procedures.

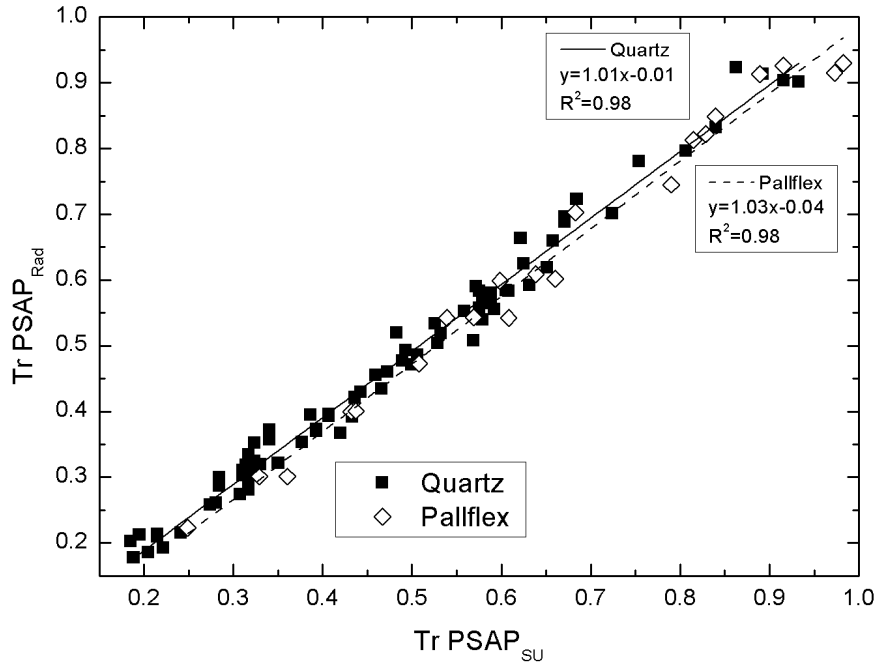


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639 Figure 2. Size-dependent aerosol properties relevant to the experiment. a) Normalized average particle
 640 number size distribution of soot aerosol measurement in the mixing chamber with the Grimm 1.108
 641 OPC. The continuous lines present the size distributions with the original diameters of the OPC and the
 642 dashed lines those assuming that the original diameters were underestimated by a factor of 2. b) Mass
 643 absorption and scattering coefficients, MAC and MSC, respectively, and single-scattering albedo ω_0 of
 644 single BC particles at $\lambda = 530 \text{ nm}$.

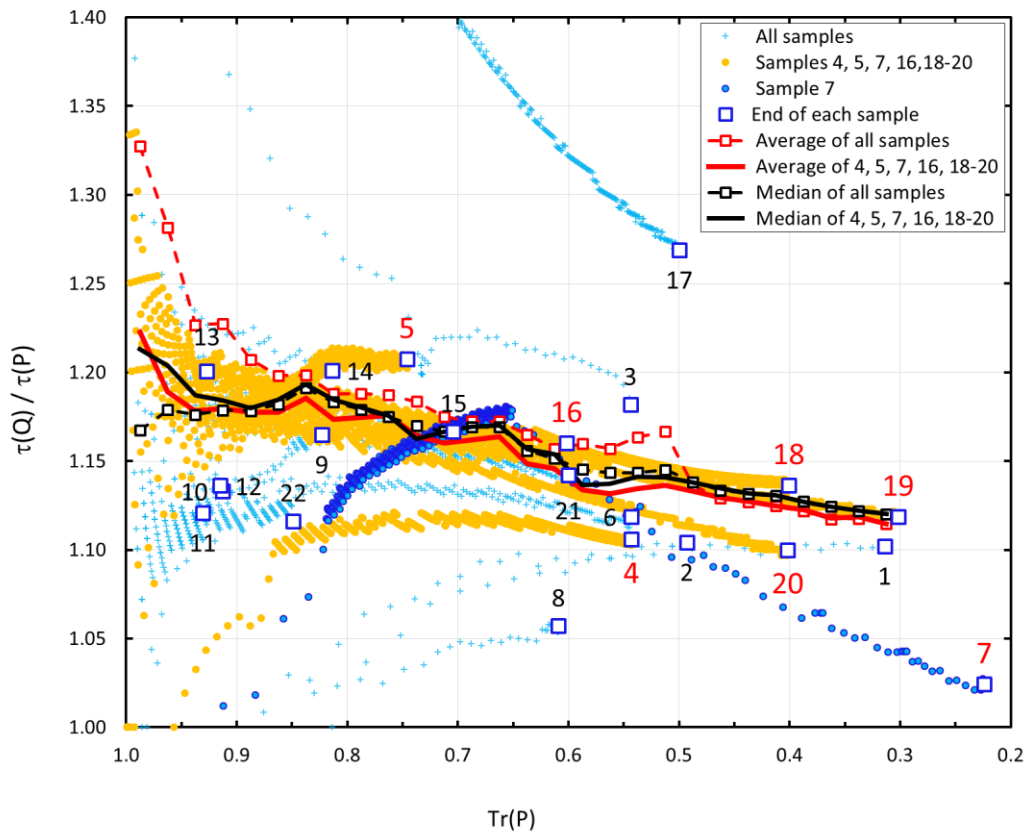
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Quartz filter characterization with soot tests



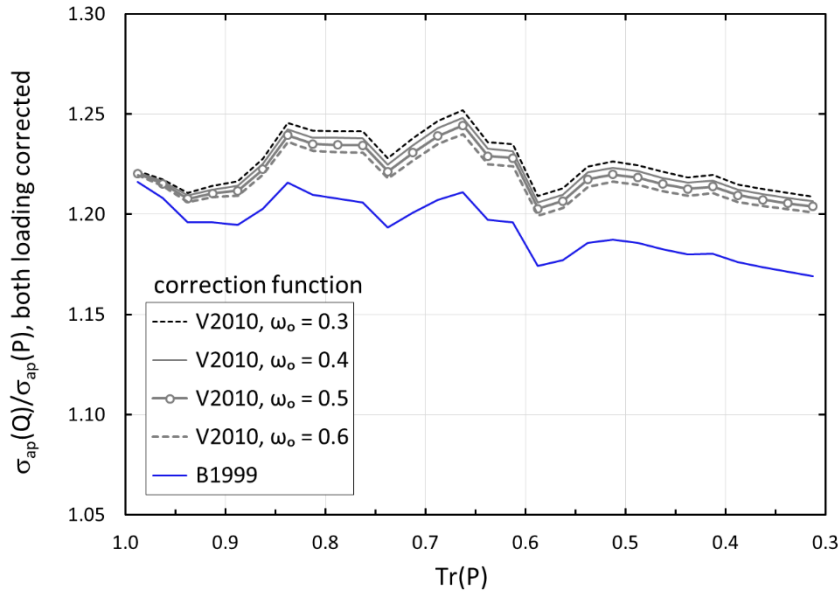
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Figure 3. Transmittance for quartz and Pallflex filters measured with PSAP radiance research and the Stockholm University custom-built PSAP.

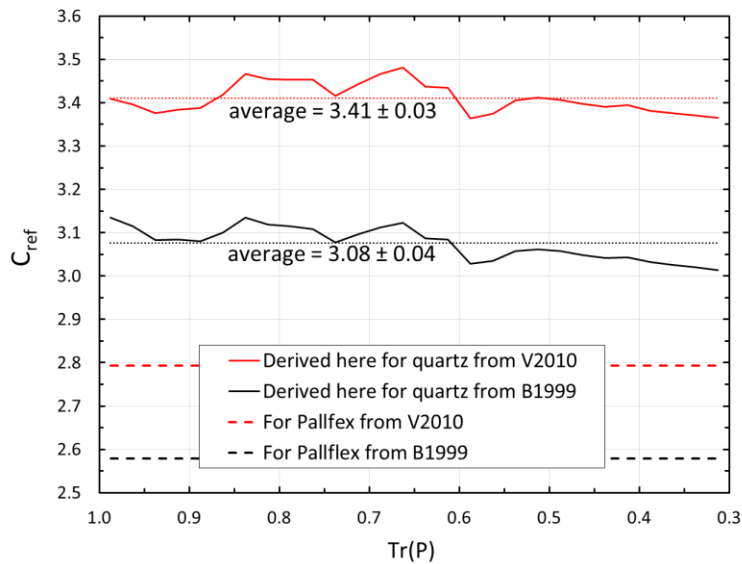


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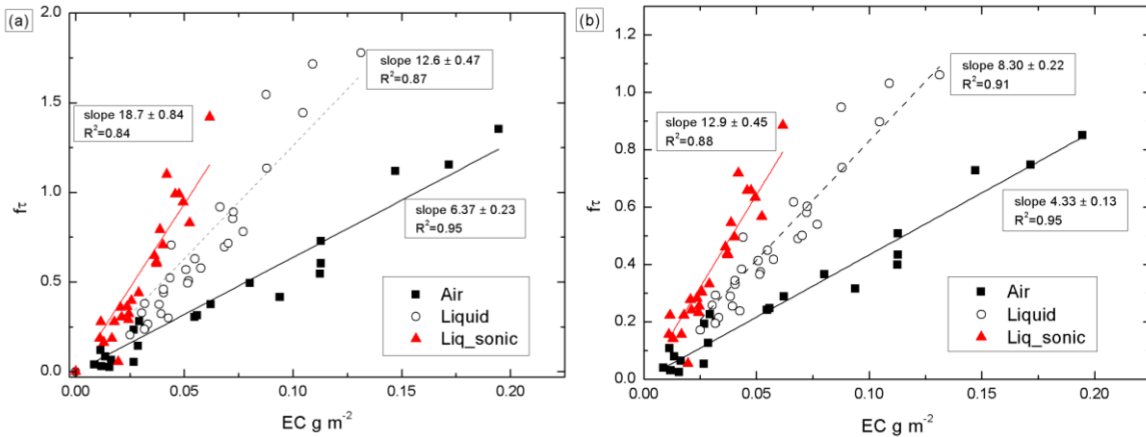
652 Figure 4. Ratio of non-loading-corrected optical depths ($\tau = \ln(1/\text{Tr})$) of quartz and Pallflex filters, $\tau(\text{Q})$
 653 and $\tau(\text{P})$, respectively at $\lambda = 530$ nm at one second time resolution.. The numbers denote the value at
 654 the end of each sample. The red numbers are associated with those samples that were used for deriving
 655 $C_{\text{ref}}(\text{quartz})$ in section 3.1.2



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 657 Figure 5. Average $\sigma_{\text{ap}}(\text{quartz})/\sigma_{\text{ap}}(\text{Pallflex})$ in 0.025 bins of transmittance of Pallflex filter at $\lambda = 530$
 658 nm. Both $\sigma_{\text{ap}}(\text{quartz})$ and $\sigma_{\text{ap}}(\text{Pallflex})$ were corrected both either according to Bond et al. (1999) with
 659 the Ogren (2010) modification (O2010) and Virkkula (2010) (V2010) using four values for the single-
 660 scattering albedo ω_o .

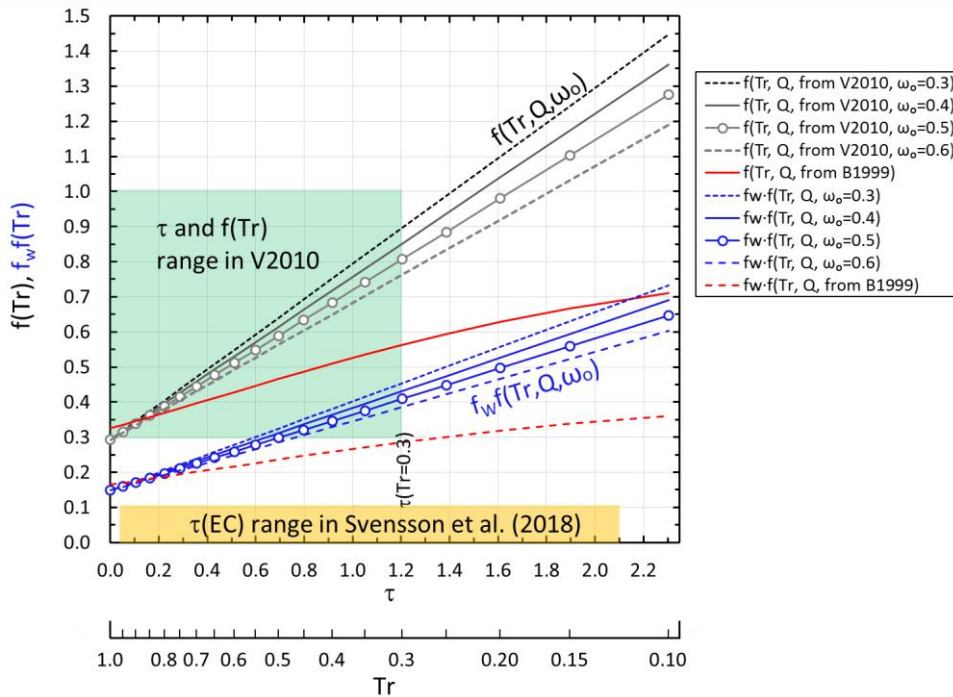


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 662 Figure 6. The multiple-scattering correction factor C_{ref} for quartz and Pallflex filters in 0.025 bins of
 663 transmittance of Pallflex filter at $\lambda = 530$ nm. The straight lines for C_{ref} of O2010 and V2010 are those
 664 shown in Eqs. (9) and (12).
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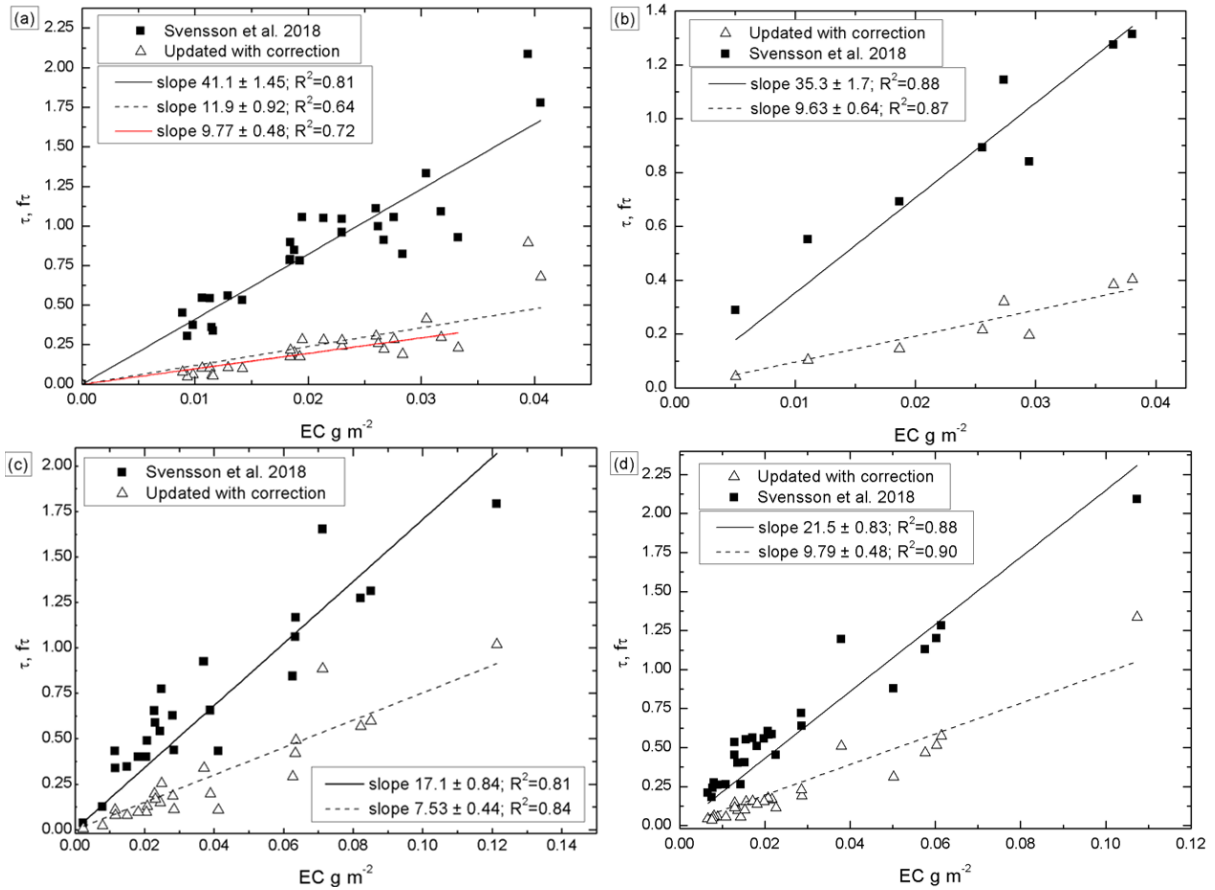
Figure 7. Linear regressions of transmittance-corrected optical depth $f\tau(\lambda = 530 \text{ nm})$ vs. EC of the BC particles blown into the mixing chamber (Air), into water (Liquid) and blown into water and treated in the ultrasonic bath (Liq_sonic). The optical depths were corrected with a) the $f(\text{Tr}, \text{V2010}, \omega_o=0.4)$ and b) $f(\text{Tr}, \text{Q}, \text{O2010})$. The regressions were calculated by forcing offset to 0.



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Figure 8. Loading correction functions derived from V210 and O210 for airborne BC particles collected on quartz filters (grey lines, $f(\text{Tr}, \text{Q}, \omega_o)$) and for BC particles mixed in water and filtered through similar quartz filters (blue lines, $f_w f(\text{Tr}, \text{Q}, \omega_o)$). The green shadowed area shows the range of optical depths and $f(\text{Tr})$ of the V210 Pallflex filter calibration and the yellow shadowed line shows the range of optical depths of EC in snow presented by Svensson et al. (2018).

Quartz filter characterization with soot tests



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682 Figure 9. Reanalysis of linear regressions presented by Svensson et al. (2018). a) chimney soot, with
 683 the red line showing the slope with the two points with the highest EC content are excluded, b) NIST
 684 soot, c) field samples from the Indian Himalaya, d) field samples from Finnish Lapland. On the x axis
 685 there is the EC concentration as g m^{-2} and on the y axis the non-corrected and corrected optical depth,
 686 τ and τ_t , respectively.