

*Supplement of*

**Measurements of Delays of Gas-Phase Compounds in a Wide Variety of Tubing Materials due to Gas-Wall Interactions**

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## Calculation of tubing delays

The depassivation time traces for the instrument only and combined instrument plus absorbent tubing  
30 were fitted to exponential decays using Eq. (S1):

$$\frac{S}{S_0} = e^{-\frac{t}{\tau}} \quad (\text{S1})$$

where  $S$  is the measured signal at time  $t$ ,  $S_0$  is the signal before depassivation, and  $\tau$  is the fitted timescale. Calculating the time at which the measured signal decays to 90% of its final value is equivalent to determining the point at which  $\frac{S}{S_0}$  equals 0.1, which yields Eq. (S2):

$$35 \quad t = \tau \ln(10) \quad (\text{S2})$$

We then define the tubing delay for absorbent materials as the difference between the instrument only delay and the instrument plus tubing delay, giving Eq. (S3):

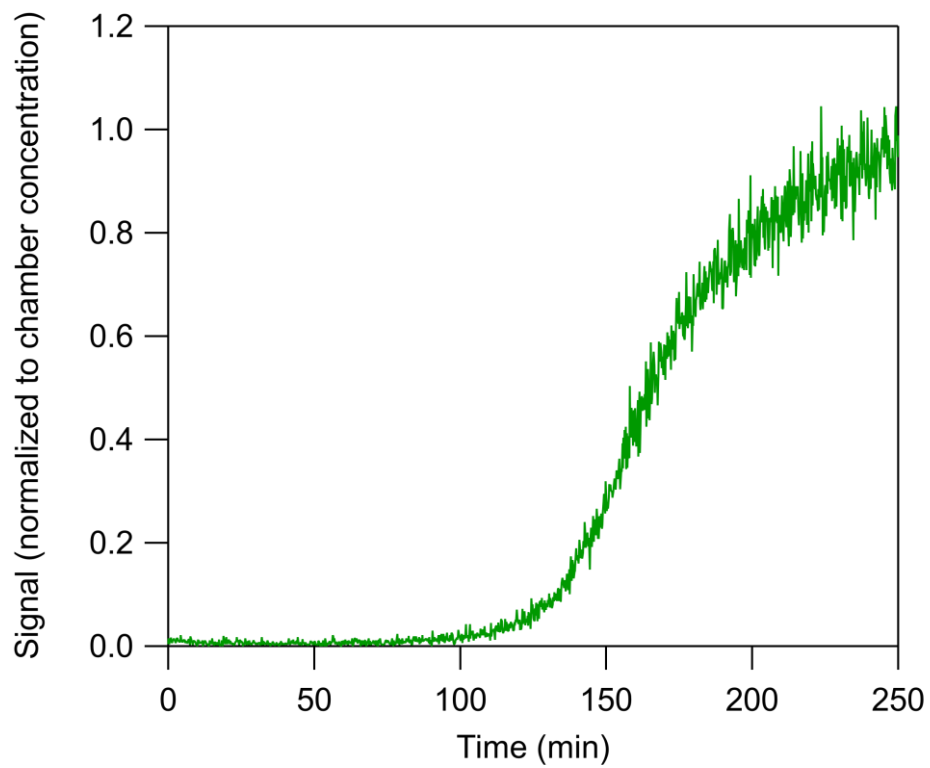
$$t_{tubing,abs} = \ln(10) (\tau_{total,abs} - \tau_{instrument}) \quad (\text{S3})$$

where  $t_{tubing,abs}$  is the tubing delay for absorbent materials,  $\tau_{instrument}$  is the instrument delay timescale, and  
40  $\tau_{total,abs}$  is the timescale for depassivation of the instrument plus tubing.

The tubing delay for adsorbent materials is defined slightly differently. Namely,  $t_{total,ads}$  is not determined from an exponential fit (due to the sigmoidal shape of the time series), but by calculating the point at which the signal reaches 50% of its maximum on passivation. An example time series is presented in Fig. S1. The calculated value of  $t_{total,ads}$  is corrected by the measured instrument delay to give Eq. (S4):

$$45 \quad t_{tubing,ads} = t_{total,ads} - \ln(10) \tau_{instrument} \quad (\text{S4})$$

where  $t_{tubing,ads}$  is the adsorbent tubing delay time,  $t_{total,ads}$  is the measured delay to 50% as described above, and  $\tau_{instrument}$  is the instrument delay timescale.



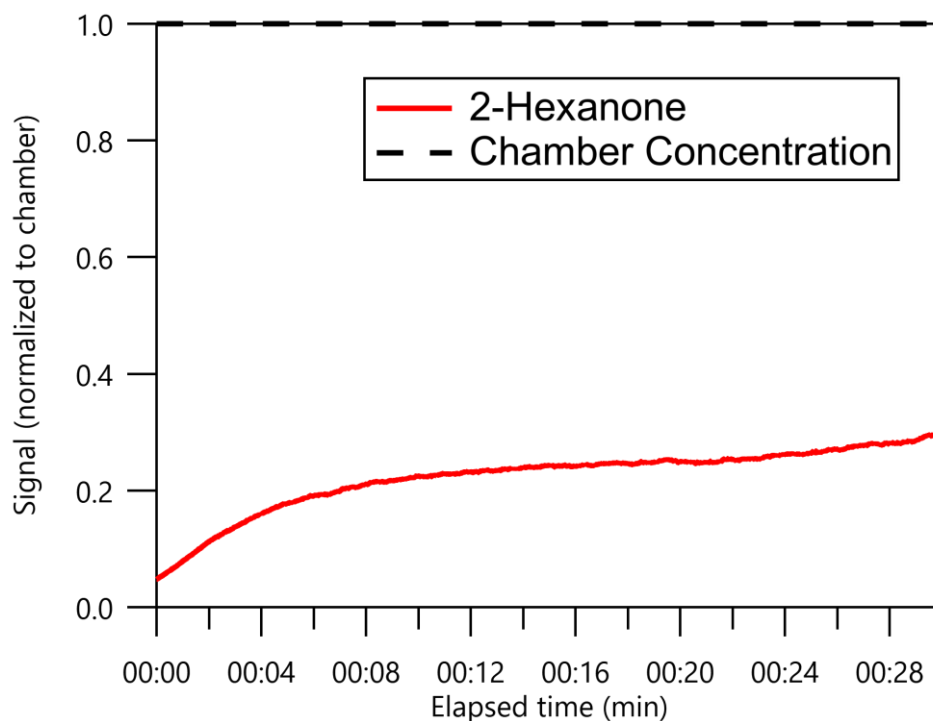
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Figure S1. Time series of the delay of 20 ppb of 2-decanone through approximately 0.6 m of aluminum tubing at RH = 0%. This is a typical tubing delay measurement for adsorbent tubing.

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## Sampling through Nafion tubing



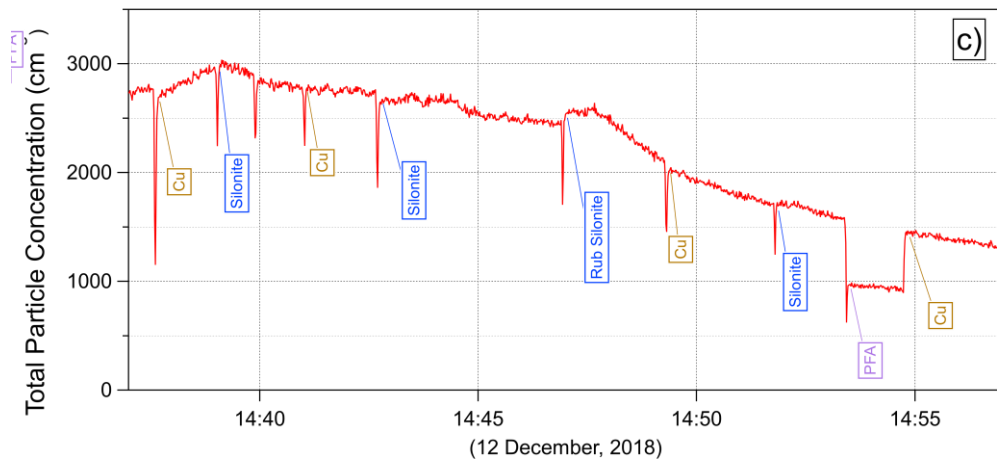
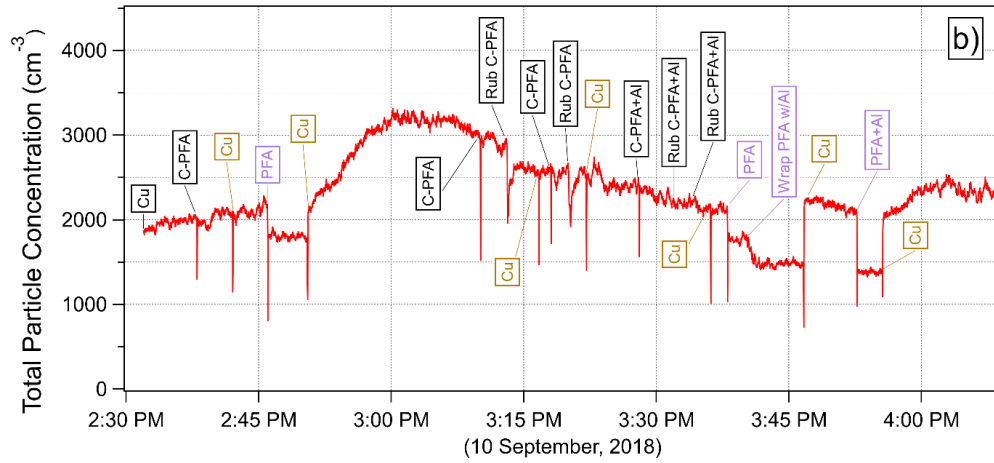
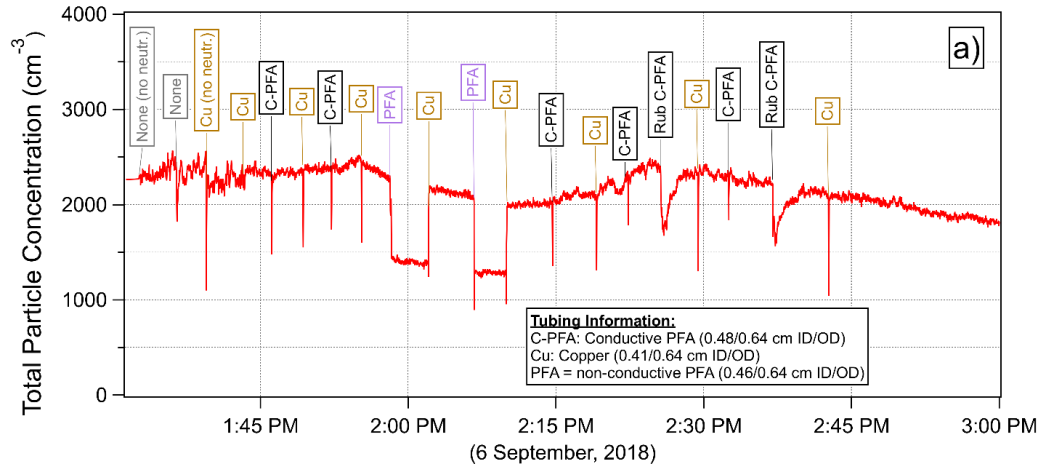
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Figure S2. Time series of signal from 2-hexanone sampled through 0.6 m of Nafion tubing. No counter flow was passed over the Nafion, and signals from the other sampled 2-ketones were negligible over this time period.

## 70 Losses of charged particles during transport through copper, PFA, and conductive PFA tubing

Fig. S3a shows no detectable particle losses in conductive PFA tubing compared to copper tubing. In contrast, non-conductive PFA tubing showed a consistent loss of ~35–40% of particles, possibly due to complete loss of particles of one charge polarity. Upon briefly (10s) rubbing the conductive PFA tubing with bare hands, however, an additional immediate loss of ~30% was observed followed by full recovery within ~1 min. During this measurement period the particle number distribution had a geometric mean  $\pm$  standard deviation of  $76 \pm 1.8$  nm. Fig. S3b shows a similar response to rubbing the conductive PFA; however, after wrapping it in aluminum foil ("+Al") no particle loss was observed upon rubbing as compared to sampling through copper tubing. One other observation is that when non-

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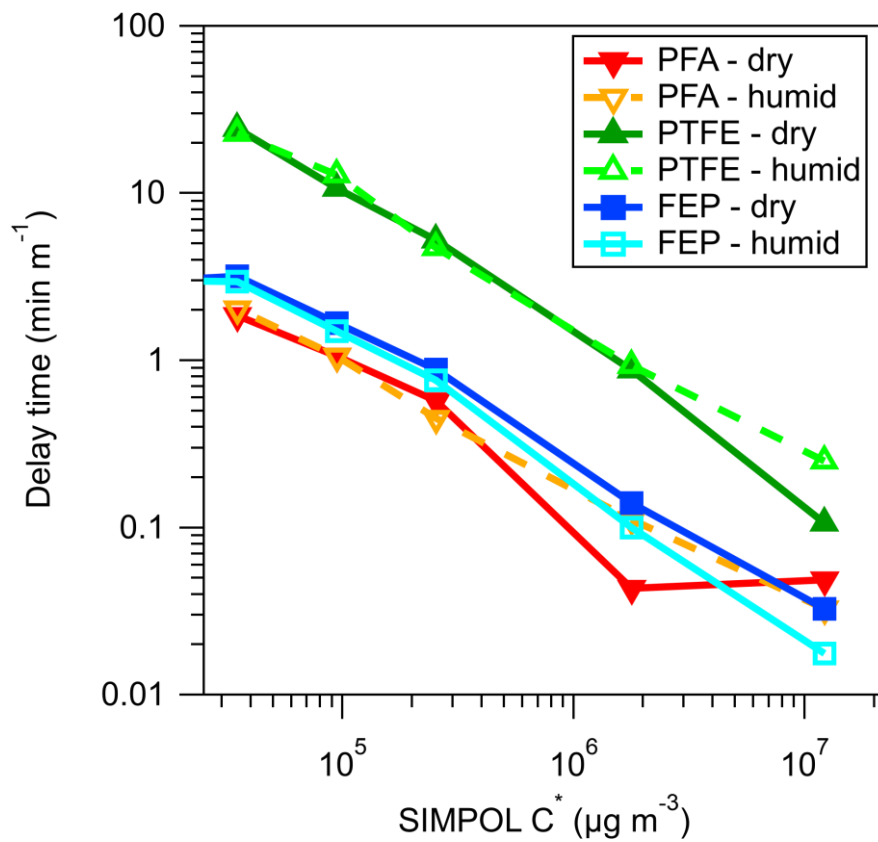
85 Figure S3. Time series of total particle number concentration (TSI CPC 3775, 1 LPM) while sampling  
laboratory (room) air. Measurements were alternated every few minutes by sampling through different  
tubing materials, while sampling through copper tubing between changes. All tubing was 1.5 meters long  
and nominally ¼" outer diameter (dimensions in legend). Tags indicating tubing material or activity are  
placed at the time when valves were switched or activity was initiated. All sampling was conducted  
90 through a TSI 3077 aerosol neutralizer unless otherwise indicated ("no neutr."). Sharp, brief (1-3 s) dips  
are from sampling particle-depleted air upon initial valve switching to tube that did not have flow for  
several minutes. Data shown are 1-s points. Residence time in the tubing was 8–11 s.

conductive PFA tubing was retested it showed a smaller loss than the ~20% shown in Fig S3a, whereas  
upon wrapping with aluminum foil the loss was more comparable to the ~35% seen before. This may be  
95 because the non-conductive tubing had not been touched for several days, and handling it while wrapping  
the foil caused it to build additional charge. During this measurement period the particle number  
distribution had a geometric mean  $\pm$  standard deviation of  $62 \pm 2.0$  nm. Fig S3c shows no losses of  
particles through Silonite tubing, even after rubbing with bare hands. The particle number distribution  
had a geometric mean  $\pm$  standard deviation of  $70 \pm 1.7$  nm over this time.

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### **RH dependence of tubing delays for polymeric materials**

A diagnostic used to label tubing materials as either absorbent or adsorbent was the humidity dependence  
of the measured tubing delay times. Tubing delays measured for a series of polymeric materials under  
both dry (<0.5% RH) and humid (45% RH) conditions are shown in Fig. S4. The similarity between the  
105 curves demonstrates a lack of humidity dependence and verifies that these delays are controlled by  
compound saturation vapor concentration  $C^*$ .



110 Figure S4. Comparison of tubing delay times measured under dry conditions (<0.5% RH, solid lines, darker colors) and humid conditions (45%RH, dashed lines, lighter colors).