Replies to the comments by the Referee Professor Giuseppe Petrucci:

First of all, we would like to thank Professor Giuseppe Petrucci from the University of Vermont for reviewing our manuscript and for his helpful comments to improve it. In the following we will comment on the individual points. The referee's comments are shown in black and our answers in blue. The referee's comments refer to the version of the manuscript submitted for review and our answers refer to the revised version of the manuscript.

Comments and Replies:

This is a well written manuscript describing thorough experimental results for a significantly improved method of measuring INPs.

1) Fig. 10: I don't understand why there are two distinct branches for aerosol generation.

The two separate branches for aerosol generation are required for the INP measurement of the externally mixed Snomax and NaCl particles (as described in Sect. 4.1.1 and Sect. 5). Referee#2 has also pointed out that the reference to Fig. 10 in Sect. 4.1.3 is missing. The corresponding reference to Fig. 10 has now been added in Sect. 4.1.3 (pg. 15, line 329).

2) Please elaborate How robust are the fits to equations 4 and 5? There are so many adjustable parameters in each, I wonder whether similarly good fits could be obtained with diverse sets of fitted parameters? In other words, is the fit a true global minimum in error or could there possibly be several local minima?

The fit according to Eq. 4 is well constrained, since the parameters are quite independent. To describe a scan we need to specify the position and background (z_0 or y_0 for detection laser 1 or detection laser 2 and b_g) values. These are quite trivial to determine in a complete scan. Further we use only two parameters to represent the width and the height of the signal, since there is no reason why the width of the particle beam (σ_p) should be dependent on the width of the laser beam (r_{DL}) and vice versa. Additionally, these two parameters represent real physical parameters, which help to choose reasonable initial values and to judge the results. We tried out randomly different meaningful initial values, and we always ended up at the same result. Further, we randomly set either the fit parameters for the effective laser width or the particle beam width as constant. However, by these tests no similarly good fits could be obtained.

In contrast, the fit according to Eq. 5 requires further conditions for the determination of the fitted parameters (Sect. 4.4), since the effective detection width at the ablation spot $(r_{DL(AL)})$ and the effective width of the ablation laser (r_{AL}) cannot be considered independently of each other. To avoid this problem, the parameters for the particle beam width (σ_p) , effective width of the detection (r_{DL}) and the y_0 -position for the distribution of the detection efficiency (y_0) were first determined at the second detection laser using Eq. 4 before the application of Eq. 5. Subsequently, the resulting particle beam width and effective detection width could be scaled up

to the distance to the ablation laser, resulting in $r_{DL(AL)}$ and $\sigma_{p(AL)}$. Together with y_0 (included in $y_{\overline{DA}}$, which is the difference between the center position of the detection y_0 and the center position of the hit rate $y_{0(AL)}$), the values of the three parameters were kept constant during the fits using Eq. 5. Thus, the fit again uses only independent parameters: 1) the effective width of the ablation laser, 2) the position of the ablation spot and 3) a background value.

Because the values of the fit parameters in Eq. 4 and Eq. 5 are real physical parameters, they are confined to certain boundaries. Within the confined parameter space, different combinations for initial values were tested. To the best of our knowledge, the given set of parameters are the global minima in this confined parameter space. In Sect. 4.2.2 (pg 20, line 411-414) and Sect. 4.4 (pg 28, line 598-605) we have added further explanations to the parameters of Eq. 4 and Eq. 5.

3) Some of the figures don't use symbols (lines are different colors) or use the same symbol (but, again, lines of different colors) to distinguish between experiments. This may be problematic for someone who is visually impaired or doesn't have access to a color version of the manuscript. I would suggest using different symbols for each experiment to facilitate understanding the figures.

Many thanks for the hint. We modified Fig. 13, Fig. 19 and Fig. 22 such that the different measurement series can be better recognized by the symbols.

4) I found the use of "coincidences" terminology to be confusing. In my experience with this field, "coincidence" is typically reserved for when a second particle enters the timing region before the first particle has passed through second detection laser for estimating particle aerodynamic diameter. In other words, I have always seen this word used to describe a possible experimental complication or error.

To avoid irritation, we decided to use the term "sized particles" as an alternative term to "coincidence" and replaced $d_{50(coinc)}$ by $d_{50(SizedP)}$. The terms were exchanged in the text of the new manuscript:

- in Sect.2, pg 5 line 100-101
- in Sect.4.2.1, pg 17 line 348
- in Sect.4.3.1, pg 21 line 439, 447-454
- in Sect.4.3.1, pg 22 Fig. 13 caption
- in Sect.4.3.1, pg 22 line 461-464
- in Sect.4.3.1, pg 23 line 478-480
- in Sect.4.3.2, pg 25 line 527
- in Sect.4.4, pg 29 line 612, 613
- in Sect.4.5.6, pg 36 line 767-768
- in Sect.6, pg 40 line 837, 838

In the Supplement:

- in Sect.S5, pg 6 line 91-95
- in Sect.S6, pg 6-7 line 103-110
- in Sect.S9, pg 8 line 129-135
- in Sect.S9, Fig S7 caption
- in Sect.S9, pg 9 line 138-145
- in Sect.S15.1, pg 15 line 263
- 5) Sec. 4.2.1 is unclear to me, although I am not familiar with these types of counting instruments. Why sum OPC size channels from 0.65 to 3.0 μ m to represent a smaller range of particle sizes (1.8 to 2.6 μ m)? Similarly, for particles greater than 2.6 μ m?

We agree that Sect. 4.2.1 "Definition of particle detection efficiency" was a bit misleading. Also for Referee #2 the background of the size selection in the OPC was not clearly visible from the text. Basically the summation over several size channels in the OPC was only performed for PSL particles with known size, because despite monodisperse PSL particles a size mode over several size channels could be observed in the OPC. First of all, a selection of size channels is not necessary as long as a DMA was used. With increasing size of the supermicron-particles it becomes more difficult to use our DMA in a suitable way. For monodisperse particles the applicable size range of the DMA can be extended, but not to all particle sizes we used. Therefore, the large particle sizes were measured without DMA. Without DMA, however, we have the effect that in the OPC a second size mode was observed in the smallest size channels. We attribute this second mode to small droplets or substances dissolved in the PSL suspension. To avoid that these unwanted small particles have an influence on our measurements, we removed this mode by selecting the size channels in the OPC and corrected the particle concentration measured with the OPC accordingly. The use of the size selection in the OPC is now described in more detail in Sect. 4.2.1 (pg.17, line: 357-364).

6) The authors refer several times to a size-dependent particle beam shift. Why is that? If particles are focused onto the ALS central axis, what causes beam pointing differences for different diameters?

It can be observed from the measurements that the particle beam focus shifts slightly depending on size. The main reason for this is probably production-related imperfections in real lenses. Similar observations were made by other groups, e.g. Huffman et al. (2005; Sect. 3.4.; page: 1152; DOI: 10.1080/02786820500423782). The reference to Huffman et al. (2005) was added in Sect. 4.5.2, pg 31, line 662.

Replies to the comments by Anonymous Referee #2:

First of all, we would like to thank Referee #2 for reviewing our manuscript and for her/his helpful comments to improve it. In the following we will comment on the individual points. The referee's

comments are shown in black and our answers in blue. The referee's comments refer to the version

of the manuscript submitted for review and our answers refer to the revised version of the

manuscript.

Comments and Replies:

General comments:

This is a well-written and extremely thorough paper about improvements to the ALABAMA laser

ablation aerosol mass spectrometer that greatly improve the detectable size range and the detection

efficiency. Bravo

Specific minor comments:

1) The CPI is discussed first, so the CPI should be Figure 3 and the air diffusor and lens should be

Figure 4.

We agree that it is better to swap Fig. 3 and Fig. 4. It is now changed.

2) For the angle of the air diffuser, the text says 5.6 degrees, but the figure says 6 degrees. Maybe

use the same value in both places.

Thank you very much for the hint, we use now uniformly six degrees as indication for the

opening angle.

Changed:

Sect. 3.1.1, pg:7, line: 152

3) Pg 8, lines 165-6: What does the acronym ODD stand for? Outer diameter diffuser, maybe? I

think it would make more sense to mention the ID at the end of the diffuser which looks like

31.2 mm.

ODD is really not the best choice in this case. ODD is actually the inner diameter of the air

diffusor. Instead of ODD we now use the term maximum inner diameter of the air diffusor

(ID_{Di(max)}) in the paper. ID_{Di(max)} is 39 mm at its maximum extension directly before the 45° tapper.

Changed:

Sect. 3.1.1, pg:8, line: 167-169

4) Pg 9, line 182-186: What you are calling outer diameter lens (ODL) is not an outer diameter. It is the inner diameter of the lens. I think it would be better to use subscripts to distinguish between the ID of the lens and the ID of the orifice, rather than calling one an OD.

Yes indeed, this could lead to confusion for the reader, we now use subscripts for a clearer distinction between the inner diameter of the aerodynamic lens (ID_{Le}) and inner diameter of the orifices (ID_{Or}) or inner diameter of the first orifice ($ID_{Or(1)}$).

Changed:

Sect. 3.1.1, pg:8, line: 168-169 Sect. 3.1.2, pg:8, line: 189-193

5) Figure 7: I'm confused by the timing. The DIE trigger is shown 50 ns after the Q-switch out. Then it takes 50 + 5 ns for the voltages to turn on. Wouldn't the voltages be on 35 ns after the laser pulse, not 70 ns as indicated in the figure? Shouldn't the expected DIE (line 272) be 35 ns? What DIE did you determine from the high voltage signals? The 70 ns time is mentioned again on page 35, line 725.

We understand that our wording suggested that the HTS specific delay times (50 ns + 5 ns) are directly related to the time to switch on the ion extraction voltages. However, it must be mentioned that the box with the HTS's inside is installed between the mass spectrometer housing and the high voltage modules and is connected to the mass spectrometer by high voltage cables, which means that a further delay of the switch-on times for the ion extraction voltages can be expected. The DIE was measured at the connections of the high voltage cables on the mass spectrometer housing by observing the triggered high voltage signals using an oscilloscope. At this point, a time delay of 140 ns \pm 10 ns between the Q-Switch out signal and the high voltage signals was measured. Taking into account the time period of 70 ns between Q-Switch out and the laser pulse as determined by Brands et al. (2009), a DIE of about 70 ns can be expected for the measurements performed in this study.

The determination of DIE is now described in more detail in Sect. 3.2.2:

pg. 12, line 263-265 pg. 13, line 279-282

6) You should refer to Figure 10 in Section 4.1.3 about the INP measurements. There is currently no reference to Figure 10 in the text.

Thanks for the hint, the reference to Fig. 10 was added in Sect. 4.1.3 (pg. 15, line 329).

7) Pg 17, lines 353 – 361: Is this section about PSLs for which the size is known? If not, it is not clear how summing over large size ranges in the OPC will give you the correct concentration to compare with the number detected. Please clarify.

We agree that Sect. 4.2.1 "Definition of particle detection efficiency" was a bit misleading. Also for Referee #1 the background of the size selection in the OPC was not clearly visible from the text. Basically the summation over several size channels in the OPC was only performed for PSL particles with known size. First of all, a selection of size channels is not necessary as long as a DMA was used. With increasing size of the supermicron-particles it becomes more difficult to use our DMA in a suitable way. For monodisperse particles the applicable size range of the DMA can be extended, but not to all particle sizes we used. Therefore the large particle sizes were measured without DMA. Without DMA, however, we have the effect that in the OPC a second size mode was observed in the smallest size channels. We attribute this second mode to small droplets or substances dissolved in the PSL suspension. To avoid an influence of these unwanted small particles on our measurements, we have removed this mode by selecting the size channels in the OPC and corrected the particle concentration measured with the OPC accordingly. The use of the size selection in the OPC is now described in more detail in Sect. 4.2.1 (pg.17, line: 357-364).

8) Figure 12: I would add a legend with the results from the fit for sigma_p and r_DL.

The legend was added in Fig. 12.

9) Pg 21, lines 455 –6: I don't understand the source of this statement. The results in Kollner (2020) show DE at 2.5 hPa for lab experiments and DE at 3.2 hPa for field measurements which are actually higher, though the size is not indicated. Pg 22, lines 457-8: Please summarize the reasons for the much lower DE in Kollner (2020) vs Brands et al. (2011) for 200 to 600 nm particles. A PhD Thesis is not the easiest source to find this information.

Pg21: In Köllner (2020), Figure A.4 shows the experimental results of the detection efficiency against the lens pressure (laboratory measurements with PSL particles). It is shown that especially the measured particle sizes 1680 nm and 1890 nm show a decreasing detection efficiency for a lens pressure deviating from 2.5 hPa. The corresponding reference to Figure A.4 in Köllner (2020) was added in Sect. 4.3.1, pg 22, line 465.

Pg22: A possible cause for the lower measured detection efficiencies in Köllner (2020) compared to those of Brands et al. (2011) is clogging of the O-ring or non-optimal lens alignment. Furthermore, Köllner (2020) points out that possibly also the device modifications made to the ALABAMA in the meantime may have led to a reduction of the detection efficiency in the size range between 200 and 600 nm. For example, the results shown in Brands et al. (2011) were obtained using a diode-pumped continuous-wave laser with a wavelength of $\lambda = 532$ nm. However, the exact cause of the different results could not be found out.

The summary of the points was included in Sect. 4.3.1, pg 22-23, line 466-475.

10) Figure 13 caption: I think you mean the detection efficiency is "relative to", not "related to"

11) Figure 14: What is the physical distance between the exit of the lens and the first detection laser? A particle beam width < 20 um seems really small. Is this consistent with your CFD calculations?

The particle beam widths shown in Fig.14 are the widths related to one sigma according to Eq. 4. The particle beam widths calculated with the aerosol lens calculator (Fig.S2) were originally given as widths in diameter and comprising 90% of all particles (Wang and McMurry, 2006). In order to compare the particle beam widths calculated with the aerosol lens calculator with our experimentally determined widths, the theoretical values are now converted into widths of one sigma. For the conversion of the theoretical values it was assumed that the particle beam diameters originally resulting from the aerosol lens calculator describe a 2-dimensional circular Gaussian distribution. A comparison of the experimentally determined particle beam widths with the values of the aerosol lens calculator shown in the Supplement Fig.S2 now shows a good agreement. In Fig.S2 an additional column with the experimentally determined values is now added and described in the text of Sect. S2. Furthermore, in the captions of Fig.14 and Fig.16 there is now the addition that the particle beam widths presented there refer to one sigma. In the caption of Fig.21, the particle beam width is given as diameter in four sigma.

Further additions:

Sect. 4.2.2, pg 19, line: 408

Sect. 4.2.2, Fig.12 in the legend

Sect. 4.2.2, pg 20, line: 419

Sect. 4.2.2, pg 21, line: 427

Sect. 4.3.3, pg 26, line: 552

Sect. 6, pg 40, line: 833

12) Figure 17: I understand why you ordered the x-axis in Figure 17b the way you did, but it makes it very hard to compare with 17a. I would use the same order for the x-axis in both 17a and 17b. You can draw the same conclusions in the text.

Ok, thanks for the hint, Fig. 17 was changed according to your suggestion.

13) pg 31, lines 646-7. What does the statement that "a voltage of 1100 was assumed" mean? Was the voltage not actually set to 1100V? Or you think the effective voltage at the electrode is different than the setting?

Actually, the voltage was set to 1100 V. However, small drifts in the high voltage supplies may lead to a slightly different real value. We changed to "A calculation of the particle deflection within the electric field after Eq. 1, using 1100 V for both electrodes, resulted in a shift of roughly $90 \mu m$ for 300 nm PSL particles" (see Sect. 4.5.3, pg 32, line 673-674).

The asymmetric curves of the fits shown in Fig. 19 result from the assumptions made in Sect. 4.4, which may lead to a slight distortion of the edges of the hit rate distributions. Furthermore, the measurements showed a slight offset between the beam center position of the second detection laser and the beam center position of the ablation laser, which also contributes to an asymmetry. In Sect. 4.5.3, which belongs to Fig. 19, an additional reference to the assumptions of Sect. 4.4 and the existing offset was added.

New (Sect. 4.5.3, pg 33, line 684-687):" The asymmetric curves for 308 nm PSL particles using the DIE(on) setup result from the assumptions made in Sect. 4.4, which lead to a slight distortion of the edges of the hit rate distributions. Furthermore, the measurements revealed a slight offset between the beam center position of the second detection laser and the beam center position of the ablation laser, which also contributes to an asymmetry."

15) Pg 35, lines 703-4. It's not clear what "the offset between the two curves" is referring to. The difference between cation and anion curves, which anticorrelate? Or the difference between the DIE(on) and DIE(off+) curves which are slightly offset.

This refers to the offset between the DIE(on) and DIE(off+) curve. It is now described in Sect. 4.5.5, pg 35, line: 733-734.

Supplement

16) Figures in the Supplement should be called S1, S2, etc. Same with the equations. And sections. This will make it less confusing when you refer to something in the main paper.

We agree. All sections, figures and equations in the supplement have been renamed accordingly.

17) Figure S2. The calculated particle beam diameters are orders of magnitude larger than the measured particle beam widths in Figure 14 in the paper. Do you have an explanation?

Motivated by your comment 11), there is now an additional column in the table (Fig. S2) with the experimentally determined particle beam widths, given in one sigma. All particle beam widths given in this study refer to the one sigma width of the particle beam unless otherwise stated. Comparisons of the experimentally determined particle beam widths with those calculated with the aerosol lens calculator are now directly comparable and show good agreement. In the caption of Fig. S2 the used width definition is now given, and further explanations in Sect. S2 are added (pg. 2-3, line: 28-37).

18) Figure S8 and S9: It is hard to compare these figures to Figure 21 in the main paper because the panels are in a different order. Please put the cations in Figure S8 and the anions in Figure S9. Also put the sum in the top panel and the number in the bottom panel.

Fig. S8 and Fig. S9 have been changed according to your suggestion. The text in Sect. S12 was adapted to the changed arrangement of Fig. S8 and Fig. S9 (see pg. 10-11, line: 177-187).

19) Pg 13, lines 203-4: Superscripts with m/z's seem like an odd notation for these ions. Normally, the superscript would be charge. Or, in the case of isotopes, the superscript would precede the symbol. Maybe put the sign and the m/z in parentheses instead.

We now use the label according to your suggestion with sign and m/z in parentheses (see Sect. S14, pg. 13, line: 215-216).

Technical corrections:

Pg 1, line 14: insert "than" before "500" Added

Pg 1, line 19: "ALABMA" misspelled Corrected

Pg 1, line 19-20: use "an" before "up" in two places Done

Pg 2, line 41: use "an" before SPMS

Done

Pg 5, line 96: "a sufficiently light scattering signal" is missing the word "large" Thanks, it was added

Pg 10, Figure 5 caption: should be "Schematic" not "Schematical" Thanks, it is corrected

Pg 16, line 337: Please group the minus sign with the temperature value. Done

Pg 21, line438: should be "a detectable" not "an detectable" Changed

Pg 21, line 454: word missing between "this" and "not" "is" was added

Figure 13 caption: I think you mean the detection efficiency is "relative to", not "related to" Changed, see reply to comment 10

Pg 24, line 502: word missing between "likely" and "to"

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Thanks, "due" was added
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Pg 30, line 624: should be "a reduced" not "an reduced"

Changed

Pg 31, line 655: "new installed DIE result" should be "newly installed DIE results"

Done

Pg 33, line676: "mass spectra" should be "mass spectrum"

Corrected in Sect. 4.5.5, pg 33 line: 706, pg 34, line: 716, pg 35, line: 724

Figure 21 caption: "Dependence of mass spectral information on particle beam position. . ." is better English than "Mass spectral information in dependence of. . ."

Modified according to recommendation

Pg 34, line 692: "switched" instead of "dwitched" and "a reduced" instead of "an reduced" Done

Pg 34, line 694: "significantly" instead of "significant"

Changed

Pg 40, line 838: Presumably, something should go here besides "TEXT"

Removed

Supplement

Pg 1, line 2: Presumably, something should go here besides "TEXT"

Removed

Pg 9, line 140: delete "can"

Removed

Pg 10, 161: "cumulated" is not commonly used in English. Maybe used "summed" instead.

Changed

Pg 13, line 195: "randomly" instead of "random"

Done

Pg 13, line 196: "spectrum" instead of "spectra"

Changed

Optimizing the detection, ablation and ion extraction efficiency of a single particle laser ablation mass spectrometer for application in environments with low aerosol particle concentrations

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Abstract. The aim of this study is to show how a newly developed aerodynamic lens system (ALS), a delayed ion extraction (DIE) and better electric shielding improve the efficiency of the Aircraft-based Laser ABlation Aerosol MAss spectrometer (ALABAMA). These improvements are applicable to single particle laser ablation mass spectrometers in general. To characterize the modifications extensive size-resolved measurements with spherical polystyrene latex particles (PSL; 150 – 6000 nm) and cubic sodium chloride particles (NaCl; 400 - 1700 nm) were performed. Measurements at a fixed ALS position show an improved detectable particle size range of the new ALS compared to the previously used Liu-type ALS, especially for supermicron particles. At a lens pressure of 2.4 hPa, the new ALS achieves a PSL particle size range from 230 nm to 3240 nm with 50 % detection efficiency and between 350 nm and 2000 nm with 95 % detection efficiency. The particle beam divergence was determined by measuring the detection efficiency at variable ALS positions along the laser cross sections and found to be minimal for PSL at about 800 nm. Compared to measurements of SPMS instruments using Liu-type ALSs, the minimum particle beam divergence is shifted towards larger particle sizes. However, there are no disadvantages compared to the Liu-type lenses for particle sizes down to 200 nm. Improvements achieved by using the DIE and an additional electric shielding could be evaluated by size-resolved measurements of the hit rate, which is the ratio of laser pulses yielding a detectable amount of ions to the total number of emitted laser pulses. In particular, the hit rate for multiply charged particles smaller than 500 nm is significantly improved by preventing an undesired deflection of these particles in the ion extraction field. Moreover, it was found that by using the DIE the ion yield of the ablation, ionization and ion extraction process could be increased, resulting in up to seven times higher signal intensities of the cation spectra. The enhanced ion yield results in a larger effective width of the ablation laser beam, which in turn leads to a hit rate of almost 100 % for PSL particles in the size range from 350 nm to 2000 nm. Regarding cubic NaCl particles the modifications of the ALABAMA result in an up to two times increased detection efficiency and an up to five times increased hit rate. The need for such instrument modifications arises in particular for measurements of particles that are present in low number concentrations such as ice nucleation particles (INP) in general,

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but also aerosol particles at high altitudes or in pristine environments. Especially for these low particle number concentrations improved efficiencies help to overcome statistical limitations of single particle mass spectrometer measurements. As an example laboratory INP measurements carried out in this study show that the application of the DIE alone increases the number of INP mass spectra per time unit by a factor of two to three for the sampled substances. Overall, the combination of instrument modifications presented here resulted in an increased measurement efficiency of the ALABAMA for different particle types, particles shapes and for highly charged particles.

1 Introduction

Single particle mass spectrometry (SPMS) is an in-situ method to analyze the chemical composition of single aerosol particles. Measurements of particle chemical composition improve our knowledge of particle sources and atmospheric processing. This knowledge is necessary for a better understanding of aerosol-radiation and aerosol-cloud interactions and thus the contribution of aerosol particles to the radiative forcing (Haywood and Boucher, 2000; Boucher et al., 2013; Stocker et al., 2013). However, due to a large number of poorly constrained parameters the estimates of aerosol forcing are still subject to large uncertainties (e.g., Boucher et al., 2013; Stocker et al., 2013; IPCC, 2014; Prospero et al., 2010). In particular, the contribution of ice nucleating particles (INPs) to aerosol-cloud interactions can only be estimated under various assumptions due to their partly unknown chemical composition, different possible freezing processes and the limited number of suitable aircraft-based measurements (Boucher et al., 2013; Cziczo et al., 2017; Kanji et al., 2017; Heymsfield and Willis, 2014; DeMott et al., 2011; Gettelman et al., 2012).

One method to analyze the chemical composition of INPs is a combination of an ice nucleation chamber, a pumped counterflow virtual impactor (PCVI; Boulter et al., 2006; Kulkarni et al., 2011a) and an SPMS instrument as described in Hiranuma et al. (2016); Schenk et al. (2014); Corbin et al. (2012); Baustian et al. (2012), and Cziczo et al. (2003). In short, the ice chamber serves to initiate heterogeneous ice nucleation, which is triggered by INPs. After a defined residence and growth time in the ice chamber, the ice crystals are separated from the background aerosol particles as well as from activated droplets using the PCVI. After the separation of the ice crystals, their water content is sublimated or evaporated such that the ice residuals can be chemically analyzed with the SPMS instrument. However, several difficulties arise when using this combination of devices as described in Schenk et al. (2014). Together with the typically low atmospheric INP number concentration between about 10⁻⁶ stdL⁻¹ and 10⁴ stdL⁻¹ (Kanji et al., 2017; Cziczo et al., 2017), the statistical limitation became a decisive problem in these measurements. This requires a high measurement efficiency of instruments analyzing the particle chemical composition. In the past, SPMS instruments showed low lens transmission, particle detection and/or ablation/ionization efficiencies. For example, in Cziczo et al. (2003) a particle transmission efficiency of about 10 % is given for the inlet of the particle analysis by laser mass spectrometry (PALMS) instrument. As described in Corbin et al. (2012), the Aerosol Time-Of-Flight Mass Spectrometer (ATOFMS) typically achieved a detection efficiency of less than 10 %, which in turn was one of the reasons why only 196 INP mass spectra were recorded with the ATOFMS within 35 hours in their study. As a consequence, the authors stated that it was not possible to quantify the importance of the measured potential INPs due to the statistical limitations (Corbin et al.,

55 2012). It should also be mentioned that in general the duration of an experiment that can be run with an ice nucleation chamber is limited, such that the statistical limitations cannot be simply overcome by increasing the measurement time. Particularly, the Aircraft-based Laser ABlation Aerosol MAss spectrometer (ALABAMA) in connection with an ice nucleation chamber and PCVI had issues with the particle counting statistics and the hit rate of the INPs. Atmospheric INP measurements showed a significant decrease in hit rate compared to the measurement of the atmospheric aerosol particles without prior ice activation and separation. Thus the hit rate decreased from typical values by 10 – 20% (Köllner, 2020; Schneider et al., 2020) to 0 – 2%.

Transmission efficiencies, detection efficiencies and hit rates of well below 100 % indicate the challenges and optimization potential for single particle mass spectrometers. Several instrument sections of the SPMS are particularly decisive for low efficiencies. First: The inlet system consisting of a critical nozzle and an aerodynamic lens is characterized by the particle transmission efficiency. Second, the particle detection efficiency is dependent on the focusing width of the particle beam and the sensitivity of the detection units. Third, the hit rate is determined not only by the absorption efficiency and the ionization efficiency of the particle components, but also by other factors, such as electrostatic forces within the mass spectrometer as well as the time interval between particle ablation/ionization and ion extraction, as presented in this paper.

In this paper, we report on a modified inlet system for the ALABAMA, also known as an aerodynamic lens system. In this context, we have analyzed the dependencies of the detection efficiency and particle beam properties on particle size and lens pressure associated with the new aerodynamic lens system. Additionally, we report how the application of a delayed ion extraction and shielding of the electric field created by the ion optics affects the hit rate. The results are compared to results obtained using two configurations without a delayed ion extraction. In this context, we discuss the particle size-dependent influence of particle charges and the influence of ion extraction efficiency on the hit rate.

75 2 General description of the ALABAMA single particle aerosol mass spectrometer

Figure 1 shows a schematic of the bipolar single particle laser ablation mass spectrometer ALABAMA. The setup can be subdivided into three different sections based on the respective modes of operation.

In the first section, the aerosol particles are focused into a narrow particle beam and are separated from the surrounding air as efficiently as possible. To achieve this, the particles in the sample flow (1.06–2.1 cm³ s⁻¹ at lens pressure of 1.5–2.6 hPa) are first passed through an aerodynamic lens system (ALS) consisting of a constant pressure inlet (CPI), an air diffusor and an aerodynamic lens. The actual focusing of the particles takes place in the aerodynamic lens. In short, a series of orifices with different diameters initially reduce the cross section of the air flow. Due to the reduced cross section, the streamlines of the air are radially shifted and thus the particle trajectories are also shifted in the direction of the centerline of the aerodynamic lens. This causes the particles to move away from the streamlines of the air at different distances depending on their inertia. After passing through the single orifices, the air expands back to the original cross section. However, the particles can only partially follow the streamlines of the air. As a result, the particle radial position behind the single orifices usually deviates from the corresponding air streamline radial position, which is described by the particle stream contraction factor (Liu et al., 1995a).

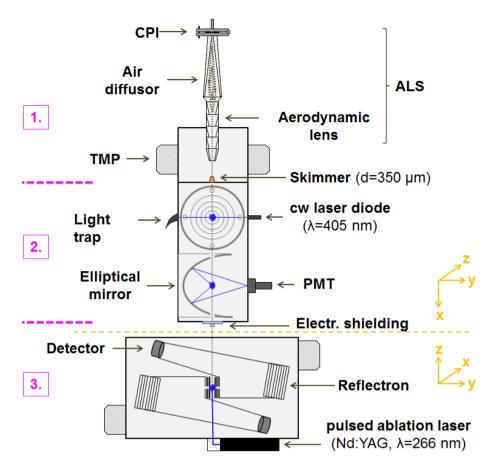


Figure 1. Schematic of the ALABAMA (modified according to Brands et al., 2011), with subdivision of three sections according to their functional principles. The grey dotted line indicates the flight path of the aerosol particles from the inlet to the ablation spot. Abbreviations: ALS - aerodynamic lens system, CPI - constant pressure inlet, TMP - turbomolecular pump, PMT - photomultiplier tube, cw - continuous wave.

Ideally, at the exit of the ALS, the vast majority of particles are focused on a line on the axis of rotation of the aerodynamic lens. After leaving the ALS, a large portion of the air expands into the first pump stage ($\sim 10^{-2}$ hPa) and is removed. To reduce the amount of air reaching the detection stage (section 2), a skimmer with a diameter of 350 μ m is installed between the first and second section. Assuming optimal focusing, the particles are not influenced by the expanding air and can therefore continue to fly unhindered through the skimmer.

In the second section, the particles are detected and their velocity is measured. The particle velocity is determined using the flight time of the particles between two continuous wave detection laser beams ($\lambda = 405 \, \text{nm}$, referred to as detection lasers herein). To achieve this, the particles have to pass through the detection lasers in such a way that a sufficiently large light scattering signal is detected by the photomultiplier tube (PMT) at each detection unit. Elliptical mirrors and signal amplifiers are used to detect even weak scattering signals from small particles (down to 100 nm) or at the edges of the detection lasers

(for further details see Brands et al., 2011, although in the original ALABAMA version a wavelength of 532 nm was used). All particles that produce two detectable light scattering signals within a defined time interval ($\sim 0.3-1.3$ ms) are referred to as coincidences sized particles in the following. Only for such coincident particle signals the particle size can be determined. , since only for such particles a vacuum aerodynamic diameter (d_{va}) can be determined. Size determination (referring to vacuum aerodynamic diameter d_{va}) is performed by converting the flight time of the particles (DeCarlo et al., 2004) using a size calibration performed with particle size standards (see Supplement Sect. S1). The determined particle velocities are also required to trigger the pulsed ablation laser ($\lambda = 266$ nm, max. repetition rate 20 Hz, Nd:YAG laser; Quantel Laser, 2019).

The evaporation of the particles and the ionization of their molecular fragments by the ablation laser pulse take place in the third section, the mass spectrometer (Z-shaped bipolar ToF-MS; TOFWERK AG, Thun Switzerland). As soon as a particle is hit by an intense laser pulse, a part of the available energy can be absorbed by the matter. The absorption of photons leads to an electronic excitation, which can return back to the ground state via a transition in the vibrational energy levels of molecules within the particles. The laser pulse duration of a few nanoseconds is significantly longer than the time required for transferring energy from the electrons to the atomic lattice. This enables the conversion of a large portion of the energy into heat, which in turn leads to a complete or at least a partial ablation of the particles (Klimach, 2012; Drewnick, 2000; Miller, 1994). Whether a particle is ablated completely, partially, or not at all depends, among other things, on the power density of the laser pulse. At power densities of the laser above $\sim 10^8$ W cm⁻², the ablation of the sample material is accompanied by the formation of ions or the formation of a plasma within the ablation plume in which atoms and molecules can partially be ionized (Amoruso et al., 1998; Drewnick, 2000; Miller, 1994; Conzemius and Capellen, 1980). The formation of ions is essentially limited to the duration of the laser pulse (Van Breemen et al., 1983).

After the ion formation process, the positive and negative ions are extracted in opposite directions from the ablation/ionization spot by means of the electric field formed between the first positive (nEx1) and the first negative (pEx1) electrode (see Fig. 2). Within the electric field, the ions are accelerated and thereby separated depending on their inertia during their further flight path (\sim 610 mm, Brands et al., 2011) up to the detectors (consisting of a multi channel plate + scintillator + PMT). The time dependent signals can be converted to a mass spectrum as a function of the mass-to-charge ratio (m/z) of the ions. By means of a reflectron (see Fig. 2), the different initial conditions of the ions caused by the ablation and ion formation process such as location, time and flight direction are reduced and thus a higher mass resolution is achieved (Cornett et al., 1992; Mamyrin et al., 1973).

3 Modifications within the ALABAMA setup

3.1 Aerodynamic lens system (ALS)

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The new ALS consists of the CPI (Fig. 3), the air diffusor and the aerodynamic lens. As part of this study, the ALS was mounted on a new alignment holder, which is shown in Fig. 4 together with the air diffusor and the aerodynamic lens.

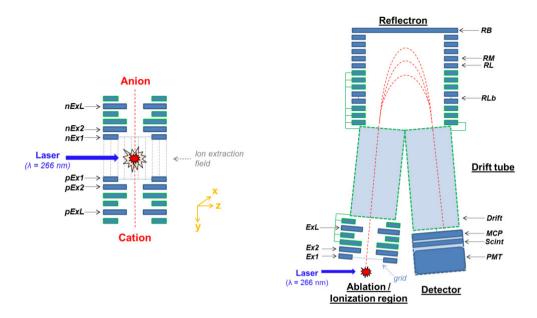


Figure 2. Cross sectional view of the ion optics within the mass spectrometer. Left figure: ion extraction components, consisting of several consecutive ring electrodes (Ex1, Ex2 and ExL for both polarities respectively). Furthermore the ablation spot, the ion extraction field between the electrodes nEx1 and pEx1 and the trajectories of the extracted ions are shown. Right figure: Fictitious ion trajectory (red dashed lines) from the ablation spot to the detectors, shown for one polarity. The ion optics are only shown in cross section, so the ring shape of the electrodes is not visible. The labeling of the electrodes corresponds to their names. Abbreviations: MCP - micro-channel plate, Scint - scintillator, PMT - photomultiplier tube

3.1.1 Constant pressure inlet and air diffusor

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In the ALABAMA, the CPI is used instead of a fixed critical orifice that frequently is adopted for stationary measurements. A schematic of the CPI is shown in Fig. 3. A detailed description of the CPI that is similar to the one used in the ALABAMA is presented by Molleker et al. (2020). Since ALABAMA has been developed particularly for aircraft-based measurements (Schneider et al., 2020; Wendisch et al., 2019; Köllner et al., 2017; Brands et al., 2011), an inlet is required that can quickly adapt to changing atmospheric pressure conditions while still allowing sufficient particle transmission. With the CPI, it is possible to keep the mass flow into the instrument and thus also the pressure within the aerodynamic lens constant.

The principle of the CPI is as follows. The lever with an integrated opening (d = 1 mm, with a 45° conical inlet in front of it) can be pulled by means of a motor against the fixed base part with the appropriate opening (d = 2 mm at the beginning and opening conically downstream at an angle of about 6°). Between the lever and the base part, there is a in-house manufactured O-ring with an inner opening diameter of 0.5 mm (Molleker et al., 2020) that encompasses the openings and is squeezed when the lever is pulled down. This allows the O-ring to act as a critical orifice. The squeezing is controlled by a pressure sensor such that the lens pressure can be kept constant for different ambient pressures by changing the O-ring opening. A comparison measurement between a fixed critical orifice and a CPI with the new O-ring type at ground level shows comparable

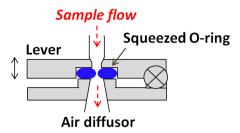


Figure 3. Schematic drawing of the constant pressure inlet (CPI) used in the ALABAMA. The double arrow on the lever indicates the possible directions of movement for squeezing the O-ring. The desired position of the lever is reached by means of a motor, which operates in dependency of the set lens pressure and the ambient sample air pressure.

particle size-dependent transmission behavior for polystyrene latex (PSL) particles (Molleker et al., 2020). In particular, the new in-house manufactured O-ring type has led to a significantly better transmission of particles compared to previously used commercially available O-rings (Molleker et al., 2020). In addition, compared to a previous version of the CPI (Köllner, 2020), the new design allows a more uniform squeezing of the O-ring such that the circular shape of the opening's cross section is better maintained irrespective of the applied squeezing. Furthermore, compared to the previous version, the new CPI has a reduced inner diameter of the tube on the inlet side (in Fig. 3, from 6.35 mm to 3.18 mm), which in turn should have a positive effect on particle transmission (Molleker et al., 2020).

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The air diffusor is located between the CPI and the aerodynamic lens. This device is used to smoothly expand the air behind the critical orifice at an angle of 5.6° six degrees, reducing radial flow velocities due to jet expansion (Hwang et al., 2015). This can in turn reduce particle impaction on the walls behind the critical orifice and diffusion losses of small particles due to recirculation in a developing downstream vortex (Hwang et al., 2015; Chen et al., 2007). As shown in Hwang et al. (2015), the downstream vortex in the area of the critical nozzle can be suppressed by reducing the opening angle. However, diffusion losses in the ALS are expected only for particle sizes below 100 nm (Hwang et al., 2015; Chen et al., 2007) and can therefore currently be neglected for the ALABAMA. Much more important is the ability of the air diffusor to increase the transmission of large particles (Hwang et al., 2015; Cahill et al., 2014; Williams et al., 2013). For the transmission of super-micron particles, the inner diameter and length of the air diffusor in relation to the particle velocities are decisive. First, the inner diameter should be larger than the maximum radial stopping distance of the particles. Second, the length of the air diffusor should be larger than the longest axial distance to the bending point of the particle trajectories (Hwang et al., 2015). The stopping distance and the position of the bending point depend on the size, velocity, mass, exit position, and exit angle of the particles with respect to the critical orifice. The diffusor presented in Hwang et al. (2015) is designed for particle sizes up to $10 \, \mu m \, (d_{va})$. The resulting length (up to 60 cm) of the diffusor is not suitable for the ALABAMA. Also, it is not necessary to aim for 10 µm particles due to the very low number concentration of such particles at higher altitudes. Thus, we altered the dimension of the air diffusor presented by Hwang et al. (2015). Additionally, a 45° taper was implemented at the transition point from the air diffusor to the aerodynamic lens (see Fig. 4), to optimize the transmission of large particles. This in turn reduces the inner diameter of the ALS from a maximum of 39 mm at the end of the diffusor ($ODD ID_{Di(max)}$) to 7.8 mm at the first single orifice ($ID_{Or(1)}$). With a comparatively small ratio of 0.2 ($(ID/ODD) ID_{Or(1)}/ID_{Di(max)}$) it can be assumed that the transmission at the upper end of the particle size range drops quite sharply, according to numerical calculations by Zhang et al. (2002). Since no particle focusing has occurred in this section of the ALS, the highest probability of impaction of large particles within the ALS is suspected in the transition from the air diffusor to the aerodynamic lens.

3.1.2 Aerodynamic lens

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The concept behind the new aerodynamic lens design is to optimize the particle beam (focusing) properties within the detectable particle size range of the ALABAMA in comparison to the design of the previously installed Liu-type lens (Köllner, 2020; Brands et al., 2011; Kamphus et al., 2008). In addition, the new geometry should reduce impaction losses of large particles. The physical dimensions of the new aerodynamic lens are mainly based on calculations using the aerosol lens calculator (Wang and McMurry, 2006). In particular, the diameter of the individual orifices as well as the lens diameter were determined with the help of this tool. In order to obtain an optimized particle beam focusing in the detectable particle size range of the ALABAMA, the required lens dimensions were empirically tested with the aerosol lens calculator. A comparison of the resulting calculations for the old previous and the new aerodynamic lens design is presented in the Supplement Sect. S2. The main focus of this comparison was the size-resolved particle beam width. The particle sizes marked in green (500 nm – 2000 nm) are those which theoretically lead to improved particle focusing with the new lens design. However, the calculations with the aerosol lens calculator are based on the assumption that the individual orifices correspond to thin cylindrical discs. This is a major reason why the calculations show that particle transmissions with the new lens design become worse with increasing particle size than with the old previous lens design (not shown). To counteract this problem, conical shaped single orifices were used instead of the cylindrical discs. The cone angels were adapted to the lens geometry obtained with the aerosol lens calculator. In the following, the influence of the conical orifice shapes used here is discussed.

The calculations resulted in a significantly larger outer inner diameter of the lens (ID_{Le}) of 31.2 mm compared to the previously used Liu-type lens (9.5 mm). Due to the larger diameter of the new lens and the enlarged openings of the single orifices (ID_{Or}), we expect a shift in the maximal focusing diameter towards larger particle sizes (Zhang et al., 2002). Compared to the previously used aerodynamic lens, the new design has a different ratio of the ID_{Or} to the ID_{Le} , since the openings of the single orifices have not increased to the same extent. A smaller ID_{Or}/ID_{Le} results on the one hand in a sharper drop at the upper end of the particle size range and on the other hand in an enhanced particle beam contraction at a single orifice (Zhang et al., 2002). In this case, the enhanced particle beam contraction would rather lead to an overfocusing of the particles. However, particle overfocusing is compensated due to the conical shape of the single orifices (Zhang et al., 2002). Further advantages of conical orifices are a reduced particle impaction and thus a better transmission of large particles (Zhang et al., 2002; Chen and Pui, 1995). In addition, the conical shape is intended to reduce the number of edges within the aerodynamic lens and associated recirculation of the airflow. Similarly, the exit nozzle was manufactured in conical shape, which should further lead to an improved transmission of large particles. Based on the results of the aerosol lens calculator, the diameter of the exit

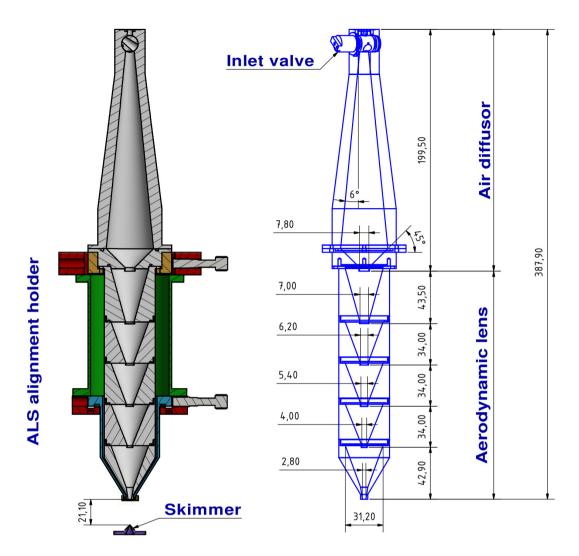


Figure 4. Schematic of the new aerodynamic lens, the air diffusor (including a conical shaped valve) and the ALS alignment holder, as well as the corresponding dimensions in millimeters. On the left side, the cross-section of the ALS alignment holder in the xz-plane is presented, which is why only one upper and one lower adjusting screw is shown, whereas the adjusting screws perpendicular to them (in y-direction) are not shown. The two lower screws precision align the pivot point of the ALS (O-ring center close to the lens exit) centrally above the skimmer, the upper screws tilt the ALS around the pivot point, aligning the aerodynamic particle path to the geometrical detection system axis (see also Supplement Sect. S7). The two upper screws have now been replaced by motors (as described in Sect. 3.1.3). A spring mechanism is used for the required restoring force on the opposite side of the adjusting screws/motors.

nozzle was reduced from 3.0 mm to 2.8 mm in order to focus small particle sizes more effectively. With the reduced nozzle opening, the new lens can be operated at a maximum lens pressure of 2.6 hPa. A higher lens pressure is suitable to improve the transmission of supermicron particles and is accompanied by a higher sample flow into the instrument. With a lower lens

pressure, however, a lower beam divergence can be achieved for small submicron particles (Zhang et al., 2002). In summary, the new aerodynamic lens system aims to improve transmission and particle beam properties of sub- and super-micron particles.

3.1.3 Alignment holder for the aerodynamic lens system

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Compared to the previous version of the ALS alignment holder used in the ALABAMA, the new version (see Fig. 4) has several improvements. The new alignment holder provides two additional degrees of freedom, which allow the aerodynamic lens and thus also the particle beam to be shifted in y- and z-direction by means of the lower adjusting screws. Due to the shift, design inaccuracies in the manufacturing can be compensated. The maximum displacement is limited to \pm 0.5 mm. Tilting of the ALS is possible by means of the upper screws, but was limited to a maximum of \pm 1°, which means a maximum displacement of the particle beam of \pm 4 mm at the ablation spot (under consideration of the skimmer orifice diameter). Tilting is controlled by two DC motors (Motor Mike - 18012 series; ORIEL INSTRUMENTS, 1991). This has the advantage that positions are reproducible and that an automated scan of the ALS can be conducted, as described below.

215 3.2 Delayed ion extraction and electric shielding

This section presents modifications that significantly influenced the ALABAMA hit rate (incl. ablation/ionization/ion extraction efficiency). As already described in Sect. 2, the particles must be hit by the ablation laser beam to be ablated and to ionize the molecules. For the extraction of the ions an electric field is required that accelerates the cations and anions into the corresponding directions towards the detectors. In addition to the ions, however, the particles themselves can be charged and thus may be deflected on their way through the ion extraction field to the ablation spot, as illustrated in Fig. 5. If charged particles are deflected too far from their original flight direction, they will miss the ablation laser beam.

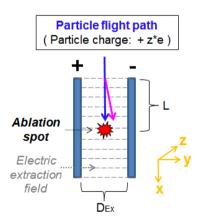


Figure 5. Schematic illustration of charge-dependent particle deflections using a constant electric ion extraction field within the mass spectrometer. The blue arrow shows the particle flight path that is not influenced by the electric field, while the pink arrow indicates the charge-dependent deflection.

In order to prevent such undesired interactions, the ion extraction field can be switched on after the particles have reached the ablation spot. For this, the extraction field is triggered by the detection unit. This procedure is commonly termed delayed ion extraction (Vera et al., 2005; Van Breemen et al., 1983; Wiley and McLaren, 1955).

3.2.1 Particle deflection in the ion extraction field

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In order to assess the influence of the constant ion extraction field on charged particles, their deflection in y-direction is first determined theoretically (see Eq. 1). According to the derivation shown in Supplement Sect. S3, the following equation results for the deflection of the particles at the ablation spot:

$$y(t) = \frac{1}{2} \cdot \frac{z \cdot e \cdot U_y \cdot L^2}{\rho_p \cdot (\frac{4}{3} \cdot \pi \cdot r_p^3) \cdot d_{Ex} \cdot v^2}$$

$$\tag{1}$$

where z is the charge number, e is the elementary-charge constant, U_y is the voltage difference between the positive and the negative electrode, L is the flight distance in the electric field (in x-direction), ρ_p is the particle density, r_p is the particle radius, d_{Ex} is the distance between the two electrodes and v is the particle velocity in x-direction.

Using the extraction voltages applied in the ALABAMA (pEx1 = $-1100 \,\text{V}$, nEx1 = $+1100 \,\text{V}$) and the measured particle velocities, we can calculate the deflections of particles from their undisturbed flight path. The flight distance L in the electric field is assumed to be half the length of the first electrodes in x-direction. The results for different particle diameters, charges and densities are presented in Fig. 6.

The diameter of the laser beam at the ablation spot in the ALABAMA is in the range of several hundred micrometers (in this study, Roth, 2014, and Brands et al. 2011). However, it is shown below that the effective width of the ablation laser beam in the ALABAMA is size-dependent and decreases towards small particle sizes. Thus, a considerable influence on the ablation efficiency can be expected, especially for particles with diameters of a few hundred nanometer if they carry a sufficient number of charges.

In clouds considerably higher charge numbers can occur than those assumed in Fig. 6. Especially in mixed-phase clouds different processes can occur that result in the presence of charged cloud particles and contribute to thunderstorm electrification (Saunders, 2008). Hallett and Saunders (1979) for example investigated the ice splinter charging during the Hallet-Mossop ice multiplication process and found out that an ejected ice fragment had a negative charge of order -10^{-16} C, which would correspond to a charge number z of about 600. Even though the Hallett-Mossop mechanism is an important source of ice particles in clouds, especially at temperatures between -3° C and -8° C (Saunders, 2008), the aforementioned charge number can only serve as a rough orientation for ice crystals containing an ice nuclei. Determining the charge numbers of ice particle residuals is hardly possible due to the difficulty of measuring them and their low concentrations. Aircraft-based investigations of cloud droplet residuals from convective clouds (only water phase) resulted in charge numbers in the range of z = -150 to z = +100 (personal communication S. Mertes). As a conclusion, preventing the deflection of charged particles in the ion extraction field should be of particular importance for measurements of cloud residuals.

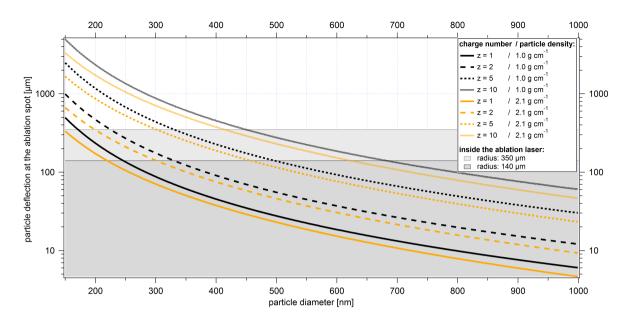


Figure 6. Calculated particle deflection from the undisturbed flight path of the particles through the center of the ablation laser beam, for different particle diameters (corresponding to particle velocities), particle charge numbers, and particle densities. Charge numbers and particle densities are represented by different styles or colours of the lines, respectively. The gray colored areas show the size range of half the ablation laser beam width (simplified assumption of an effective width of the ablation laser beam of either 280 μ m or 700 μ m as used in Brands et al., 2011, neglecting particle size and particle type). Particles outside the colored background are likely to miss the ablation laser beam. The particle densities used correspond approximately to those of PSL with $\rho = 1.05$ g cm⁻³ and sodium chloride with $\rho = 2.17$ g cm⁻³.

3.2.2 Delayed ion extraction

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Delayed ion extraction (DIE) is basically not a new method, but has already been introduced to improve mass resolution (Hinz et al., 2011; Brands, 2009; Vera et al., 2005). The focus of this work is on the influence of the DIE on the hit rate (incl. ablation/ionization and ion extraction efficiency). DIE is a method to control the electric ion extraction field between both the first negative and first positive electrode (in this case pEx1 and nEx1, Fig. 2). This means that the high voltages applied to the electrodes can precisely be turned on and off, such that in the ideal case the ion extraction field is only generated when the particles have already been hit by the ablation laser beam. Compared to the previously used permanent electric field, the DIE can generate an almost field-free space for the flightpath of the particles to the ablation spot.

Here, the DIE is realized by fast high voltage transistor switches (HTS 50; Behlke Power Electronics GmbH, 2019) to trigger the high voltages within the ALABAMA mass spectrometer. The HTS are installed in an external box between the high voltage generating modules and the connections of the electrodes within on the mass spectrometer and connected to both by high voltage cables. Only the electrodes pEx1 and nEx1 are controlled by the DIE, since the electric field in the extraction region is predominantly influenced by their voltages. The following electrodes, nEx2 and pEx2, have only a minor influence on the

extraction region between nEx1 and pEx1, because they are shielded by thin grids wrapped around nEx1 and pEx1. The HTS trigger signals are generated by the ALABAMA control electronics. Taking into account the particle velocities, the control electronics trigger the flash lamp and the Q-Switch in the ablation laser as well as the signal for the HTS (DIE trigger) in a precise chronological sequence as shown in Fig. 7. Thus, the laser pulse and the time of switching on the ion extraction field can be synchronized.

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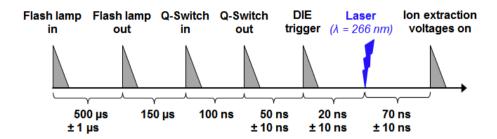


Figure 7. Time diagram of the trigger signals of the ablation laser, the laser pulse and the time-controlled switching process of the high voltages at the first electrodes (modified after Brands, 2009). Flash lamp in: trigger signal for the flash lamp in the laser; Flash lamp out: actual triggering of the flash lamp; Q-Switch in: trigger signal for the Q-Switch of the laser; Q-Switch out: actual triggering of the Q-Switch; DIE trigger: trigger signal for the HTS. The triangles shown in the figure were only used for better visualization and do not represent the decay times of the signals. The uncertainty values correspond to the reading accuracy at the oscilloscope.

The time intervals between Flash lamp in and Flash lamp out, O-Switch in and O-Switch out, as well as O-Switch out and the laser pulse have been determined experimentally previously in our group (Brands et al., 2011; Brands, 2009). The DIE trigger signal can be varied between 2 µs before and 150 ns after the Q-Switch out trigger signal, which also shifts the time of switching on the ion extraction field. This allows the HTS turn-on delay time of 50 ns and the HTS turn-on rise time of about 5 ns to be taken into account. The optimal time for the DIE trigger signal and the associated switching on of the ion extraction field was empirically determined by observing the width and height of the potassium ion signals at m/z 39 and m/z 41. Subsequently, the DIE related time intervals were determined with respect to the Q-Switch out signal using an oscilloscope. The DIE was measured at the connections of the high voltage cables on the mass spectrometer housing by observing the triggered high voltage signals using an oscilloscope. At this point, a time delay of $140 \text{ ns} \pm 10 \text{ ns}$ between the Q-Switch out signal and the high voltage signals was measured. Taking into account the time period of 70 ns between O-Switch out and the laser pulse as determined by Brands (2009), a DIE of about 70 ns can be expected for the measurements performed in this study. However, there may be an additional delay until the electric field has actually built up at the ion extraction region. Since, after the HTS was switched and the high voltage supply of pEx1 and nEx1 started, the high voltage signals of pEx1 and nEx1 at the mass spectrometer connections were used as an indicator to determine the DIE. Nevertheless, after a turn-on time of the HTS of 1 µs the high voltage supply to pEx1 and nEx1 is interrupted again, after a further 6 µs a decrease in the voltage signals at pEx1 and nEx1 was observed. The total decay time of the high voltages are in the order of hundreds of microseconds and thus several orders of magnitude below the firing sequence of the ablation laser (max. 20 Hz). Considering the known particle velocities, no influence on charged particles due to the decaying electric field is expected.

3.2.3 Electric shielding

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An additional electric shielding was installed in front of the electrodes (Fig. 8a) to shield an electric field generated by the remaining electrodes. The influence of such an electric field on the particles could be determined by the fact that despite the use of the DIE, the hit rate of highly charged particles was lower than with an additional upstream neutralizer (see section 4.5.1). Although the electric field strength in front of the electrodes can be assumed to be significantly weaker than in the space between the electrodes, it must be taken into account that the traveled path in the electric field is included quadratically in Eq. 1. The electric shielding was designed with openings to avoid pressure gradients (Fig. 8b). It was placed inside the instrument such that it is in contact with the housing of the mass spectrometer, which is used as the chassis ground.

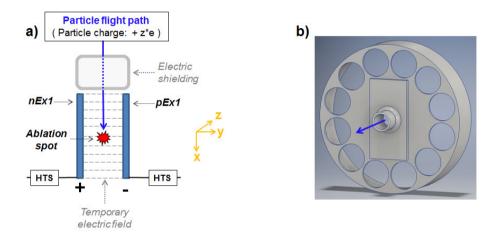


Figure 8. Figure a): The blue arrow shows the flight path of charged particles when using an electric shielding and fast high voltage transistor switches (see text for details). The electric shielding is installed upstream of the extraction electrodes. Figure b): 3-D scheme of the electric shielding

4 Experimental characterization of the modified components

4.1 Experimental setup

4.1.1 Test particles

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The majority of the measurements were performed using particle standards. During laboratory measurements at the Max Planck Institute, spherical PSL particles ($\rho = 1.05 \,\mathrm{g\,cm^{-3}}$; Duke Scientific Corporation and Polyscience Inc.) were used for size-, shape- and charge-dependent measurements. Sodium chloride particles (NaCl, $\rho = 2.17 \,\mathrm{g\,cm^{-3}}$; Carl Roth GmbH + Co. KG)

were used as widespread reference for particles of aspherical shape (Brands et al., 2011; Huffman et al., 2005). A comparison of our results with results from Zelenyuk et al. (2006) shows that the shape of the NaCl particles formed from the atomized saline water solution must be almost cubic under conditions measured by us (see Supplement Sect. S4 and Sect. 4.1.2). Thus, a spherical particle type that can be focused quite well with an aerodynamic lens can be compared to a cubic particle type that is rather difficult to focus (Brands et al., 2011). Mineral dust particles and ambient aerosol from the laboratory room air were used as other test particles in order to demonstrate the need for an electric shielding. In addition, INP measurements with: a) Birch pollen washing water containing ice active macromolecules (see Augustin et al., 2013, and von Blohn et al. 2005 for details), referred to as Birch pollen herein, b) externally mixed Snomax and NaCl particles, and c) a mixture consisting of Na and K-feldspar particles (see Augustin-Bauditz et al., 2014, for details) were conducted under laboratory conditions at the Leibniz Institute for Tropospheric Research.

315 4.1.2 Laboratory setup for characterization measurements

Figure 9 gives an overview of the laboratory setup used for size-, shape- and charge-dependent measurements of PSL and NaCl particles at the Max Planck Institute. The particle flow direction is marked by red arrows, starting from the atomizer following downstream the individual measurement instruments. Before the Differential Mobility Analyzer (DMA), the particle flow is routed via one of the three flow paths. 1) Monodisperse PSL particles were generally passed through the DMA because the atomization of PSL particles generates small water droplets whose residuals can be removed by the DMA. 2) PSL particles larger than 3.5 µm were bypassed, since the DMA is not able to size select them. 3) If polydisperse particles such as NaCl are used, larger and multiply charged particles may also pass through the DMA when they have the same mobility diameter as the smaller singly charged particles. To avoid this, an additional impactor was used in front of the DMA to remove the larger multiply charged particles.

The particle-free flow was installed to control the flow through the DMA using the valves. The transition from 1/4" to 1/8" to 1/2" was installed between the two ports of the particle-free flow downstream of the DMA for more effective mixing of the particle flow with the particle-free flow. If not mentioned otherwise, results were obtained using the above presented setup.

4.1.3 Laboratory setup for INP measurements

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The setup for the INP measurements at the Leibniz Institute for Tropospheric Research, shown in Fig. 10, was similar to that presented in Schenk et al. (2014). The INP counter FINCH (Frankfurt Ice Nucleus CHamber; Frank, 2017) was used to activate INPs at $-24.1^{\circ}\text{C} \pm 1.1^{\circ}\text{C}$ under ice-supersaturated conditions. Along their flightpath through FINCH, the activated particles grow to super-micrometer ice crystals, but also supercooled droplets can form in FINCH when water-supersaturated conditions are applied. At the exit of FINCH a pumped counterflow virtual impactor (PCVI; Schenk et al., 2014; Boulter et al., 2006; Cziczo et al., 2003) was used to separate the grown ice crystals from water droplets and non-activated aerosol particles. After passing the counterflow ice crystals are evaporated by heating and drying the sample air such that only the ice crystal residuals are left over. These residuals were guided to the ALABAMA. Since the separation of ice crystals from supercooled droplets

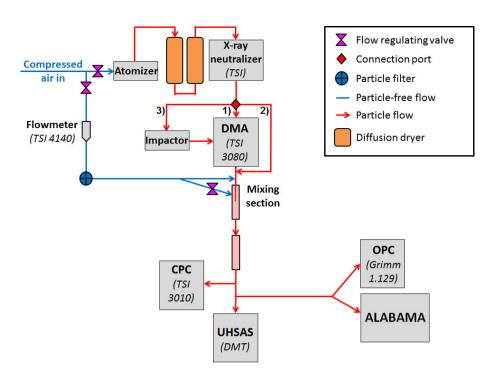


Figure 9. Laboratory setup for the characterization measurements. Particles are produced by means of an atomizer. The particles are subsequently dried, charged and size selected by means of two diffusion dryers, an X-ray neutralizer and a DMA, respectively. Downstream the particle flow is diluted and mixed with a particle-free flow prior to detection and measurement by the CPC, OPC, the UHSAS, and the ALABAMA. The detectable (50%) particle size ranges specified by the manufacturer are between about 0.01 μm and 3 μm for the CPC, between 0.25 μm and 32 μm for the OPC and between 0.055 μm and 1.0 μm for the UHSAS.

relies only on particle size, it cannot fully be excluded that supercooled droplet residuals were occasionally sampled also.

As an alternative to FINCH, the SPectrometer for Ice Nuclei (SPIN) was also used for ice nucleation (see e.g. Garimella et al., 2016, for details). For ice nucleation in SPIN, the temperature was controlled to $-25.5^{\circ}\text{C} \pm 0.2^{\circ}\text{C}$ (Birch pollen) or $-35.8^{\circ}\text{C} \pm 0.5^{\circ}\text{C}$ (Feldspar) under water-supersaturated conditions. The PCVI was alternated between the two INP counters, either FINCH or SPIN.

4.2 Methods for characterization of the aerodynamic lens system (ALS)

4.2.1 Definition of particle detection efficiency

345 The particle detection efficiency (DE) in this paper is defined as the ratio of the particle concentration measured by the AL-ABAMA detection units (further details in Supplement Sect. S5) to the particle concentration simultaneously measured with a reference instrument. For the detection efficiency, both the number of particles detected at the first or second detection unit can

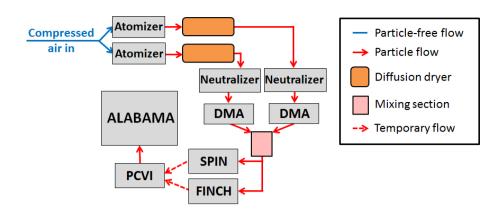


Figure 10. Laboratory setup for the INP measurements presented in Sect. 5. Particles are produced by means of an atomizer. The particles are subsequently dried, charged and size selected by means of a dryer, a neutralizer and a DMA, respectively. Since externally mixed particles were also investigated during the measurements, two branches of particle generation were required. The FINCH/SPIN and the PCVI were either used in the described ice activation mode for the analysis of INPs or in the no ice activation mode for direct measurement of the particles without prior INP activation and separation. Temporary flow means that only one INP counter, either FINCH or SPIN, was coupled to the PCVI.

be taken into account. In addition, the detection efficiency can also be determined by using the coincidences sized particles, which means only those particles are taken into account, that have been detected by both detection units within a defined time interval and for which a vacuum aerodynamic diameter can thus be determined. The reference instruments used are as follows:

- For particle sizes smaller than 250 nm in mobility diameter (d_{mob}), a TSI Condensation Particle Counter (CPC; model 3010, Mertes et al., 1995) was used as the reference instrument.
- In the range from 260 nm to 1700 nm (d_{mob}), the results of the CPC were averaged with those of a Grimm Optical Particle Counter (OPC; model 1.129, Bundke et al., 2015) and used as a reference. The average value from OPC and CPC was taken to compensate for minor variations between the two devices.
- For particle sizes larger than $1700 \,\mathrm{nm}\,(d_{mob})$, the OPC was used as the only reference instrument.

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In addition, for measurements performed with PSL particles larger than 1800 nm and without the DMA a size channel selection was applied: 1) For the ALABAMA, the time interval for recording the detection signals was adjusted and fixed such that only particles with the corresponding flight time ($\sim d_{va}$) were detected at both detection units. 2a) For the OPC, the size channels from 0.65 µm to 3.0 µm were summed up for particle sizes between 1.8 µm and 2.6 µm. 2b) For particle sizes greater than 2.6 µm, the size channels 1.3 µm to 32 µm were added up. In principle, a size selection was not necessary as long as a DMA was used, although this was not possible for all particle sizes (see Sect. 4.1.2). Without DMA, however, a second size mode was observed in the smallest size channels of the OPC. To avoid an influence of these unwanted small particles on our measurements, they were removed by selecting the appropriate size channels in the OPC.

The measurement procedure with the same settings was repeated up to four times. Data from the ALABAMA and the reference

instruments were each averaged to obtain better counting statistics. The measurement time for the determination of detection efficiencies shown in Fig. 13 was typically between three and six minutes per particle size and lens pressure, but was extended to about 30 minutes for particle concentrations below 1 particle cm⁻³.

Measurements with NaCl particles between 380 nm and 550 nm (d_{va}) were corrected by parallel Ultra High Sensitivity Aerosol Spectrometer (UHSAS) measurements (see Supplement Sect. S10), because below 550 nm (d_{va}) a small percentage of multiply charged particles passed through the DMA, forming a second size mode. For particles larger than 550 nm, the multiply charged particles could be separated very efficiently with an impactor upstream of the DMA, such that no second size mode was visible.

4.2.2 Particle beam scan through the detection lasers using the lens scan method

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Measurements of the detection efficiency as a function of particle beam position along the laser cross sections allow to optimize the alignment of the ALS and to determine the particle beam width and particle beam divergence. The method used here to characterize the properties of the particle and laser beams is to tilt the ALS stepwise in the y- and z-direction so that the particle beam is scanned orthogonally through the respective detection laser (Klimach, 2012), in the following also called lens scan. At each position, a measurement series of a few seconds with a time resolution of one second was generated (parallel to the external reference instruments). Using the DC motors, automated 2D scans with a motor step size of 50–75 μm were performed. Calculations from the intercept geometry were used to convert the step size between two motor positions into the step size between two particle beam positions at the location of the respective laser (see Supplement Sect. S7). For the measurements presented here, the particle beam was scanned through the cross section of each laser on seven adjacent paths at a distance of 50 μm to 75 μm from each other, as shown in Fig. 11.

The starting particle beam positions for the paths were chosen so that they are located around the laser beam center position of the respective, orthogonally aligned detection laser. It must be taken into account that due to a size-dependent particle beam shift when changing particle sizes, new start positions of both motors had to be set. After a lens scan was performed, the particle counts per second of each of the seven adjacent particle beam positions were averaged, converted into concentrations (see Supplement Sect. S5) and normalized with the reference instruments. As an example, Fig. 12 shows the averaged and normalized measurement data for $400 \, 460 \, \text{nm} \, (d_{va}) \, \text{PSL}$ particles. It can be seen that the detection efficiency increases from 0 % outside of the laser beam to a maximum around the laser beam center point. The detection efficiency as a function of particle beam position follows a 2-D Gaussian distribution (Klimach, 2012; Huffman et al., 2005) by having the following three assumptions. First, the particle beam has a radial Gaussian profile. Second, all particles reach the detection region. Third, the scattered light of the laser can be measured within its effective width. In this study, the 1-D case was used (further details in Klimach, 2012; Huffman et al., 2005). Accordingly, the probability density of a particle at location z (respectively y for 2nd detection laser) is described by the following function:

$$p_{1D}(z) = \frac{1}{\sigma\sqrt{2\pi}} \exp\left(\frac{(z-z_0)^2}{2\sigma^2}\right) \tag{2}$$

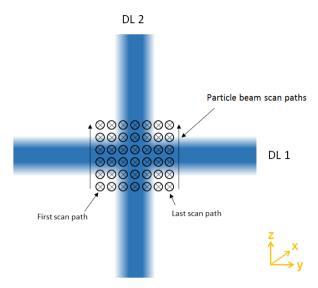


Figure 11. Schematic representation of the seven particle beam paths used for the scan through the first detection laser (DL1), viewed from the ALS perspective. According to Fig. 1 the flight direction of the particles is in x-direction. Six measurement positions per scan path were chosen for illustration purposes only, but represent significantly fewer measurement positions than were actually used in the lens scans (see Fig. 12). For a scan of the particle beam through the second detection laser (DL2), the particle beam paths would be correspondingly oriented in the y-direction. During regular measurements, the ALS should ideally be aligned in a way that the particles fly through the center of the overlapping area of the two lasers.

with σ being the standard deviation of the Gaussian distribution. If Eq. 2 is integrated within the effective laser width $(\pm r_{DL})$ 400 in which particles generate a detectable scatter signal, a function for position-dependent detection efficiencies $DE(z_p)$ can be deduced.

$$DE(z_p) = \int_{z_p - r_{DL}}^{z_p + r_{DL}} p_{1D}(z) dz$$
(3)

The cumulative distribution function of the Gaussian distribution can be represented with the error function (erf), which results in the position-dependent function of the detection efficiency as follows (Klimach, 2012):

$$DE(z_p) = \frac{1}{2} \operatorname{erf}\left(\frac{z_p + r_{DL} - z_0}{\sqrt{2}\sigma_p}\right) - \frac{1}{2} \operatorname{erf}\left(\frac{z_p - r_{DL} - z_0}{\sqrt{2}\sigma_p}\right) + b_g \tag{4}$$

with σ_P being the particle beam width (as radius, corresponds to one σ) (as radius in terms of one σ), z_0 the center position of

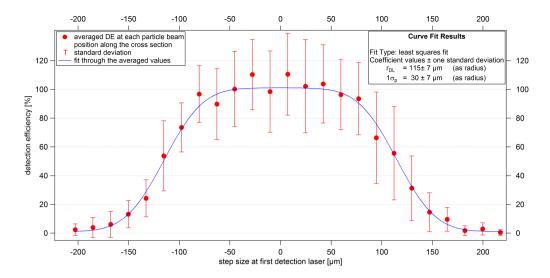


Figure 12. Lens scan along the cross section of the first detection laser using the example of $400 \, 460 \, \text{nm}$ (d_{va}) PSL particles. The averaged values of the DE, as well as the associated standard deviations (given as the uncertainties), result from a measurement time of about 5-10 seconds per particle beam position and from seven adjacent paths. The zero position on the x-axis corresponds to the laser beam center point in z-direction.

the distribution, r_{DL} the effective width of the detection laser (as radius) and a value for the background (bg), which indicates the difference between the baseline of the fit and the zero line. Thus, the distribution of the detection efficiency is fitted using Eq. 4 with σ_P , r_{DL} , z_0 , and bg as fit parameters. According to Eq. 4, only two parameters are needed to determine the width and height of the distribution, since there is no reason why the particle beam width (σ_P) and the effective width of the detection laser (r_{DL}) should be interdependent. Furthermore, these two parameters represent real physical parameters which help to provide reasonable output values and to evaluate the results. In order to find the parameter values of Eq. 4 that best fits the measured data, the Levenberg-Marquardt least-squares method was selected as the method for fitting in the program IGOR Pro (Version 6.37; WaveMetrics, 2015). The coefficients and sigma values resulting from the fitting are estimates of what would result if the fitting were performed infinitely many times with the same data but with different noise, and then calculated the mean and standard deviation for each coefficient (see IGOR Pro manual, WaveMetrics, 2015, for more details). For example, in Fig. 12 the fit function is shown by the blue line, resulting in a particle beam width (one σ_P) of 30 μ m \pm 7 μ m and an effective detection laser width (as diameter) of 230 μ m \pm 14 μ m. The plateau around the maximum is formed due to the fact that the particle beam is narrower than the effective laser beam width. In conclusion, with the lens scan it is possible to perform particle size dependent analyses of particle beam widths at both detection units.

Additionally, the lens scan method can be used to determine the particle beam divergence. The particle beam divergence is defined as the particle beam width normalized to the distance to a reference point. The location of the reference point depends on whether the particle beam width was measured at one position only or at different positions, so as shown in Sect. 4.3.4, the exit of the ALS or the first of two detection lasers can be used as the reference point. The particle beam divergence determined

for the ALABAMA is calculated from the particle beam widths (one σ_P) at both detection units and their distance from each other. In addition to the particle beam width, the particle beam divergence serves as a further characterization feature for evaluating the particle beam focusing of an aerodynamic lens system.

430 4.3 Results of the aerodynamic lens system characterization

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The characterization of the new aerodynamic lens system was carried out indirectly by measuring the size-resolved detection efficiency of the ALABAMA and directly by investigating the size-dependent properties of the formed particle beam. Particle beam width as well as particle beam divergence were determined by using the lens scan method (see Sect. 4.2.2). The size-resolved detection efficiency, however, was determined at a fixed ALS position. The fixed ALS position was set to maximum detection efficiency and hit rate. The optimum ALS position was found as a compromise from three lens scans with PSL particles of the sizes $150 \, \text{nm}$, $200 \, \text{nm}$ and $400 \, \text{nm}$ (d_{mob}).

4.3.1 Size-resolved detection efficiencies at the optimum, fixed ALS position

The size-resolved detection efficiency for PSL and NaCl particles are shown in Fig. 13. In this case, the detection efficiency was calculated using the coincidences sized particles. The results achieved with the new ALS are shown for different lens pressures between 1.5 hPa and 2.6 hPa. The figure further includes earlier ALABAMA measurements taken with the previously used Liu-type aerodynamic lens and without the air diffusor (Köllner, 2020; Brands et al., 2011). Since Brands et al. (2011) several improvements have been made to the ALABAMA (Köllner, 2020; Roth, 2014). The ALABAMA setup used by Köllner (2020) is identical to the one used here except for the ALS, but already contained a similar CPI with the same O-ring type, whereas Brands et al. (2011) worked with a fixed critical orifice. Investigations on the differences between the use of a critical orifice and a squeezed O-ring are presented in Molleker et al. (2020).

As can be seen from the PSL measurements in Fig. 13, particles between 350 nm and 1800 nm were detected with 90–100 % efficiency at 2.1 hPa lens pressure. Furthermore, by using the 50 % cut off diameter in efficiency $d_{50(coinc)}$ $d_{50(sizedP)}$, we obtain a detectable $d_{50(coinc)}$ $d_{50(sizedP)}$ particle size range between 230 nm to 3000 nm (d_{va}) for 2.1 hPa and 230 nm to 3240 nm (d_{va}) for 2.4 hPa. The lower $d_{50(coinc)}$ $d_{50(sizedP)}$ are nearly identical for all lens pressures and do not show the expected shift to smaller particles for lower pressures (Zhang et al., 2002). Thus, it can be assumed that the limiting factor of the lower $d_{50(coinc)}$ $d_{50(sizedP)}$ is not only the performance of the ALS, but also the scattered light intensity, which strongly decreases with decreasing particle diameter. As shown in Fig. 15, the decreasing scattered light intensity results in a significantly reduced effective width of the detection lasers. The upper $d_{50(coinc)}$ $d_{50(sizedP)}$ shows a clear correlation with lens pressure. The upper $d_{50(coinc)}$ $d_{50(sizedP)}$ increases from 1900 nm to 3500 nm by an increase of the lens pressure from 1.5 hPa to 2.6 hPa, respectively. This result is supported by numerical simulations of the transmission efficiency for a single thin orifice (Zhang et al., 2002). However, the detection efficiency between 2 μ m and 4 μ m decreases sharply. An explanation for this could be the low value of the ratio between the diameter of the first single orifice to the diameter of the air diffusor directly in front of the orifice (as described in Sect. 3.1.1). The numerical calculations presented by Zhang et al. (2002) and the discussion in Sect. 3.1.1 suggest that the transmission drop should be rather steep for such a small ratio of 0.2.

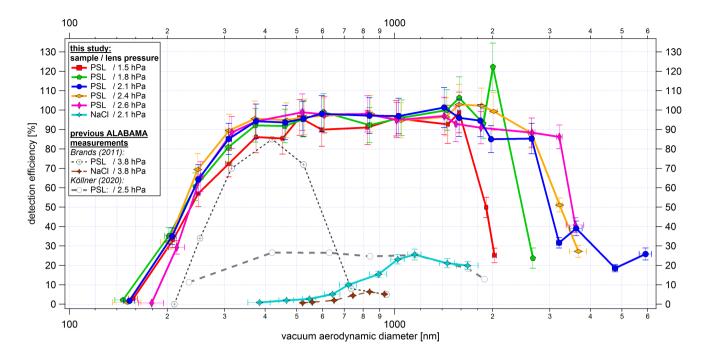


Figure 13. Size-resolved detection efficiency of PSL and NaCl particles. The detection efficiency is relative to particles that led to eoincidences sized particles. The results achieved with the new ALS are shown with solid lines. The colors represent the different lens pressures from 1.5 hPa to $2.6 \, \text{hPa}$ and the markers distinguish between PSL and NaCl particles. ALABAMA measurements taken with the previously used Liu-type aerodynamic lens (Kamphus et al., 2008) and without the air diffusor are shown as dashed lines. The y-uncertainty bars refer to the uncertainties of the components used (see Supplement Sect. S15.1 and S15.2) and the x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with the ALABAMA, converted into d_{va} according to Eq. S1 (Supplement).

The new ALS achieves an improved detectable particle size range especially for super-micron particles compared to the ALS previously used in the ALABAMA. For example, in Fig. 13 a clear shift of the upper \$\delta_{50(coinc)}\$ d_{50(sizedP)}\$ towards large particle sizes can be observed compared to measurements with the previous ALS. In Brands et al. (2011) the interpolated PSL \$\delta_{50(coinc)}\$ d_{50(sizedP)}\$ range was between 270 nm and 620 nm. The lens pressure of 3.8 hPa used in Brands et al. (2011) was higher than the pressure used in the new ALS. In principle, the upper \$\delta_{50(coinc)}\$ d_{50(sizedP)}\$ should benefit from a higher lens pressure (Zhang et al., 2002), but this is not the case here. The measurements by Köllner (2020, Figure A.4) have shown that when using the Liu-type lens with the CPI, the detection efficiency of super-micron PSL particles decreased for lens pressures > 2.5 hPa. Nevertheless, the measurements of Köllner (2020) indicate an improved detection efficiency for super-micron particles compared to Brands et al. (2011), resulting in an interpolated PSL \$d_{50(sizedP)}\$ range from 260 nm to 1880 nm at a lens pressure of 2.5 hPa. On the other hand, the measurements of Köllner (2020) result in a significantly lower maximum detection efficiency in the PSL size range between 200 nm and 600 nm compared to Brands et al. (2011). Köllner (2020) considers clogging of the

O-ring or non-optimal ALS alignment as possible reasons for the lower maximum detection efficiency compared to Brands et al. (2011). In addition, Köllner (2020) points out that possibly also the device modifications made to the ALABAMA in the meantime may have led to a reduction of the detection efficiency in the PSL size range between 200 nm and 600 nm. For example, the results shown in Brands et al. (2011) were obtained by using a diode-pumped continuous wave laser with a wavelength of 532 nm. However, the exact cause for the different results could not be found out. The possible reasons for the different detection efficiencies between both of them are discussed in Köllner (2020). In Köllner (2020) the interpolated PSL $d_{50(sizedP)}$ range was between 260 nm and 1880 nm at a lens pressure of 2.5 hPa.

To summarize, by comparing the $d_{50(coinc)}$ $d_{50(sizedP)}$ range of the new ALS with the previously used one (Brands et al., 2011; Köllner, 2020), the new ALS facilitates an increase of the upper $d_{50(coinc)}$ $d_{50(sizedP)}$ by more than 1300 nm. In addition to an improved upper $d_{50(coinc)}$ $d_{50(sizedP)}$, the new ALS achieves a shift of the lower $d_{50(coinc)}$ $d_{50(sizedP)}$ towards smaller particle sizes. However, the effect is rather small and is probably limited by the decreasing scattered light intensity with decreasing particle sizes.

Figure 13 further shows measurements with NaCl particles which, with a maximum of 25.5% around $1150\,\mathrm{nm}$ (d_{va}), have a significantly lower detection efficiency than the spherical PSL particles. One reason for this could be that the scattered light intensity and distribution not only depends on the size, but also on shape and refractive index of the particles (Kulkarni et al., 2011b). In addition, for non-spherical particles, aerodynamic forces during the expansion of the air at the nozzle exit of the ALS lead to a defocusing of the particle beam (Huffman et al., 2005; Liu et al., 1995a). Nevertheless, a higher detection efficiency for the cubically shaped NaCl particles can be achieved with the new ALS than with the ALABAMA setup used by Brands et al. (2011).

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The detection efficiency of other SPMS instruments have been reported in literature: Gemayel et al. (2016) present a maximum detection efficiency for the laser ablation aerosol particle time-of-flight mass spectrometer (LAAP-ToF-MS) of about 2.5 % for PSL particles with a particle diameter of about 450 nm. In Shen et al. (2018), measurements with PSL particles resulted in detection efficiencies between 1 % and 5 % for the LAAP-ToF-MS in the size range between 400 nm and 1000 nm (d_{mob}) , while for NaCl particles the detection efficiencies were below 5 % in the size range between 300 nm and 1000 nm (d_{mob}) . A modified version of the LAAP-ToF-MS achieved up to 17 % detection efficiency at the second detection laser for 800 nm PSL particles (Marsden et al., 2016). Another modified version of the LAAP-ToF-MS increases the detection efficiency to a maximum of about 4 % for 700 nm PSL particles, but achieves a larger detectable particle size range compared to measurements of Gemayel et al. (2016) due to an improved light collection technique (Zawadowicz et al., 2020). For the single particle laser ablation mass spectrometer (SPLAM) the maximum detection efficiency is about 65 % for 300 nm (d_{va}) PSL particles (Gaie-Levrel et al., 2012). The single particle laser ablation time-of-flight mass spectrometer (SPLAT) achieves a maximum detection efficiency of about 73 % for approximately 350 nm (d_{va}) particles (Zelenyuk and Imre, 2005). The successor models SPLAT II and miniSPLAT achieve detection efficiencies of 100 % for spherical particles in the size range between 125 nm and 600 nm (Zelenyuk et al., 2015). Differences between the individual devices are diverse. This is partly due to the different geometries of the instruments but also due to the application of different detection methods. Further, the definition of

the detection is not uniform and instruments use different aerodynamic lens systems.

However, when measuring in environments with low particle concentrations, a higher particle detection rate may be required despite improved detection efficiency. In this case an additional particle enrichment per time unit can be achieved by increasing the sample flow into the instrument. An increase of the lens pressure from 1.5 hPa to 2.6 hPa corresponds to a doubling of the standard volume flow rate from 1.05 cm³ s⁻¹ to about 2.1 cm³ s⁻¹. As can be seen in Fig. 13, increasing the lens pressure to 2.6 hPa does not result in a decrease in detection efficiency for PSL particles larger than 200 nm. However, the current ALABAMA design limits the lens pressure to 2.6 hPa due to the vacuum requirements for the high voltages. An overview of the particle detection rate as a function of lens pressure is given in Supplement Sect. S8.

4.3.2 Size-resolved particle beam width using the lens scan method

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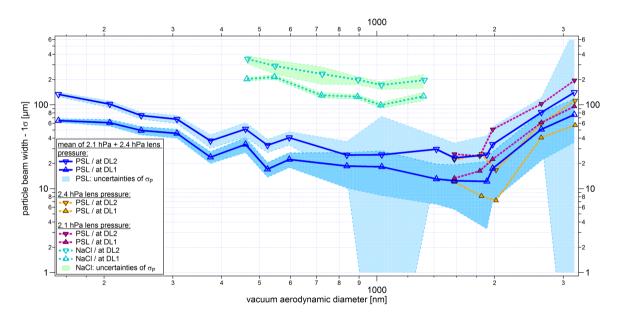


Figure 14. Size-resolved particle beam widths (PBWs) (one σ_P), as defined in Eq. 4, at the two detection stages (DL1 and DL2) for PSL and NaCl particles. Below 1600 nm, the beam widths are averaged for 2.1 hPa and 2.4 hPa lens pressure (PSL only). The PBWs are given as one σ as defined in Eq. 4. The y-uncertainty range is given by the uncertainty of the fit of each scan (see Sect. 4.2.2). The x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with the ALABAMA, converted into d_{va} according to Eq. S1 (Supplement).

Figure 14 shows the particle beam width for PSL particles (150 nm to 3200 nm, d_{va}) and for NaCl particles (460 nm to 1320 nm, d_{va}). The particle beam width generally depends on particle size and particle types. For both particle types (PSL and NaCl), the curves show a comparable size dependence of the particle beam widths. The minimum particle beam width is observed around 1000 nm for NaCl and around 1600 nm for PSL particles. The particle beam width increases with decreasing

particle size due to the fast expansion of the air at the exit of the ALS. The increase in particle beam width with increasing size and inertia of the particles is likely due to a poorer focusing of these particles within the ALS. These poorly focused particles are in turn accelerated more strongly in the y- and z-direction at the exit of the ALS, which can lead to larger particle beam divergence. The trend of the PSL curves in Fig. 14 resembles the particle beam contraction ratio, which was numerically determined for a single thin orifice lens (Zhang et al., 2002), assuming spherical particles and unit density. Below 1600 nm the PSL beam widths for 2.1 and 2.4 hPa lens pressure are similar, and therefore were averaged in Fig. 14. Above 1600 nm there is a spread in the curves for 2.1 hPa and 2.4 hPa. This finding fits quite well with the results of the different upper $d_{50(coinc)}$ $d_{50(sizedP)}$ of 2.1 hPa and 2.4 hPa (see Fig. 13). Figure 14 further shows that the particle beam for NaCl particles is about one order of magnitude broader compared to the PSL particles. As already mentioned in Sect. 4.3.1, this is explained by the aerodynamic lift forces on non-spherical particles (Huffman et al., 2005; Liu et al., 1995a).

Particle beam widths measured with the previously used ALS are not available because there was no automated lens scan for this ALABAMA setup. However, a qualitative comparison of the new and previous ALS shows improved particle beam characteristics for the overall size range with the new ALS (see Supplement Sect. S9).

4.3.3 Size-resolved effective width of the detection lasers using the lens scan method

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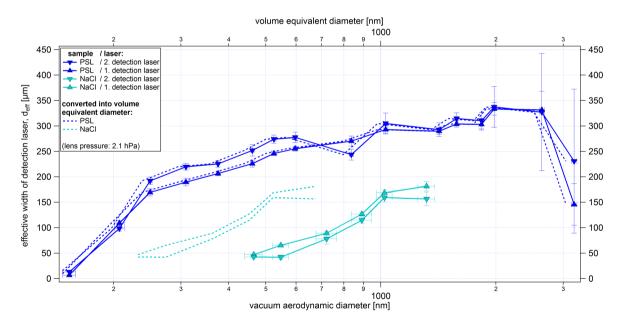


Figure 15. Size-resolved effective widths of the first and second detection laser (λ = 405 nm), for PSL particles and NaCl particles as a result of lens scans. In addition to ALABAMA sizing in d_{va} , the effective laser widths are also displayed as a function of the volume equivalent diameter (dashed lines). The y-uncertainty range is given by the uncertainty of the fit of each scan (see Sect. 4.2.2). The x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with the ALABAMA, converted into d_{va} according to Eq. S1 (Supplement).

The effective width of the detection lasers (as defined in Eq. 4) is important for an assessment of the detection efficiency. For maximum detection efficiency, the particle beam needs to have a width smaller than the effective width of the detection laser. As expected, the effective laser width displayed in Fig. 15 tends to increase with increasing particle size. However, there is a significant change in the slope of the curves for sizes larger than 250 nm. As a result, smaller particles need to move more centrally through the laser beam than larger particles in order to generate sufficient scattered light for detection. This ultimately determines the lower detection limits of the ALABAMA. Whether there is a connection between Mie scattering and the partially inverse trends of the effective laser widths could not be finally clarified.

The effective laser width also seems to be dependent on particle shape and/or refractive index effects. The cubic NaCl particles result in similar curves as the PSL particles, but are shifted to larger sizes (solid lines). This is due to the fact that for the vacuum aerodynamic diameter the particle density and the shape factor must be taken into account (Hinds, 1999). Nevertheless, even after conversion of the vacuum aerodynamic diameter into volume equivalent diameter, smaller effective laser widths for the NaCl particles (dashed lines) are obtained than for PSL particles. Since both PSL and NaCl show a non-absorbing behavior at the wavelength of 405 nm (He et al., 2018; Querry, 1987), the smaller effective widths can be explained mainly by the cubic shape of the NaCl particles and the shape-dependent distribution of the scattered light intensity (Kulkarni et al., 2011b). Thus, the smaller effective width of the detection laser, which result from the lower scattered light intensity of cubic particles, further contribute to a lower detection efficiency of NaCl particles as evident from Fig. 13.

The comparison between the effective laser width, the particle beam width, and the detection efficiency (see Fig. 15, 14, and 13, respectively) provides the following consistent picture. As an example, the 461 nm (d_{va}) PSL particles at the second detection laser have a 4σ beam width (as diameter) of about 200 μ m. With an effective width of the second detection laser of about 240 μ m at this size almost all particles should be detected and this is indeed confirmed by the results in Fig. 13.

4.3.4 Comparison of the particle beam divergences generated by different ALS

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To compare the performance of the new ALS from the ALABAMA with the ALS of other mass spectrometers, the particle beam divergence is used as described in Sect. 4.2.2. In Huffman et al. (2005) and Su et al. (2004), results of particle beam width measurements using Liu-type aerodynamic lenses (Liu et al., 2007) are presented. The aerodynamic lens type characterized by Liu et al. (2007) also corresponds to the aerodynamic lens previously used in the ALABAMA and is based on the design by Liu et al. (1995a, b). In Hünig (in prep.) and Molleker et al. (2020) results of the characterization measurements of ERICA are based on those used in the ALABAMA. Furthermore, the approach for determining particle beam widths (see Eq. 4) is similar to that used in Hünig (in prep.), except for a "transmission term" introduced there was not applied here. Nevertheless, the particle beam divergence determined in our study and by Hünig (in prep.) can be compared in the size range from about 240 nm to 2600 nm, since the maximum detection efficiency achieved in this size range were about 100 % in our study at 2.1 hPa lens pressure. In contrast to the ALABAMA, ERICA is equipped with the aerodynamic lens model IPL-013 (Aerodyne Inc.; Peck et al., 2016; Xu et al., 2017).

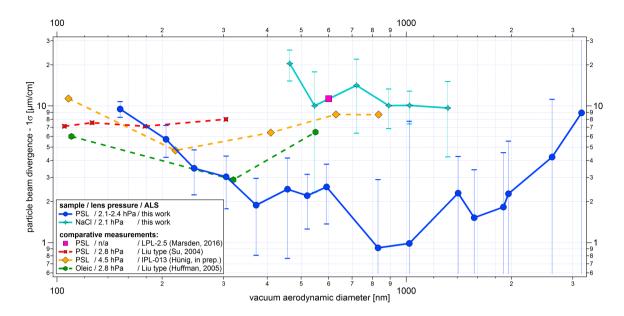


Figure 16. Comparison of size-resolved particle beam divergences for different ALS. The particle beam divergence for the ALABAMA was calculated from the particle beam width (one σ_P) at both detection units and their distance from each other. The same approach was used in Hünig (in prep.) and Marsden et al. (2016). For Huffman et al. (2005) and Su et al. (2004) the distance from the exit of the ALS to the vaporizer was used to determine the particle beam divergence, assuming that the particle beam has no broadening at the center point of the exit of the ALS. However, there is a finite radius of the particle beam at the exit of the ALS, as mentioned in Cziczo et al. (2006) and confirmed by our study. Sphericity is assumed for PSL and oleic acid particles, and a cubic shape for NaCl particles. The results of Su et al. (2004) are shown considering a particle density for PSL of 1.05 g cm⁻³. The y-uncertainty range is given by the uncertainty of the fit of each scan (see Sect. 4.2.2) and Gaussian error propagation. The x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with the ALABAMA, converted into d_{va} according to Eq. S1 (Supplement).

Figure 16 shows that the minimum particle beam divergence achievable with the new ALS is shifted towards larger particle sizes compared to measurements with the Liu-type and IPL-013 lenses. For spherical particles between 200 nm and 350 nm (d_{va}) values of divergences are comparable with each other. For particles larger than 350 nm, a contrary behavior can be observed. With the new ALS, the divergence of the particle beam decreases further with a minimum value for 800 nm particle size, in contrast to the reference measurements. For spherical particles below 200 nm, the new ALS seems to be less efficient in particle focusing compared to the Liu aerodynamic lens type, which is particularly suitable for spherical particles below 400 nm (Liu et al., 2007). But in principle, the size-resolved PSL curve of the particle beam divergence from this work is similar to the curve determined from numerical calculations for a cylindrical nozzle (Zhang et al., 2002).

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The measurements of NaCl particles show a particle beam divergence that is about one order of magnitude larger than that of PSL particles. Possible reasons for this difference have been discussed in Sect. 4.3.2. Similar to spherical particles, the beam

divergence increases with decreasing particle size for cubic particles. An increase of the divergence of the NaCl particle beam towards larger particles cannot be demonstrated in this work.

4.4 Methods for characterizing the DIE and electric shielding

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This section introduces the following three methods that have been used to characterize the DIE in connection with the electric shielding: the hit rate, the lens scan through the cross section of the ablation laser's beam path, and the settings for the analysis of charging effects. The hit rate is defined as the ratio of laser pulses yielding detectable mass spectra to the total number of emitted laser pulses per time unit. To obtain particle mass spectra, a sufficient amount of ions have to be detected, at least for one mass to charge ratio, to pass a predefined threshold. This threshold was set using background signals produced by laser shots on a particle free air beam.

As described in Sect. 4.2.2, the lens scan method can also be used to scan the particle beam through the beam path of the ablation laser. The characteristic of the ablation laser beam is determined by means of the hit rate. However, the hit rate depends on the particle detection, because the laser pulses on particles are only triggered if the particles have prior also triggered a signal at both detection units. Accordingly, a modified approach must be applied to find a suitable fit function. The fit function must represent the distribution of the hit rate along the cross section of the ablation laser beam. As an approach for such a hit rate imaging function, the portion of particles passing the ablation laser beam was set in relation to the portion of particles passing simultaneously the detection spot scaled up to the level of the ablation laser beam (according to Supplement Sect. S7):

$$HR(y_p) = \frac{\frac{1}{2}\operatorname{erf}\left(\frac{y_p + r_{AL} - y_{0(AL)}}{\sqrt{2}\sigma_{p(AL)}}\right) - \frac{1}{2}\operatorname{erf}\left(\frac{y_p - r_{AL} - y_{0(AL)}}{\sqrt{2}\sigma_{p(AL)}}\right)}{\frac{1}{2}\operatorname{erf}\left(\frac{y_p + r_{DL(AL)} - y_{\overline{DA}}}{\sqrt{2}\sigma_{p(AL)}}\right) - \frac{1}{2}\operatorname{erf}\left(\frac{y_p - r_{DL(AL)} - y_{\overline{DA}}}{\sqrt{2}\sigma_{p(AL)}}\right) + b_g}$$

$$(5)$$

where r_{AL} is the effective width of the ablation laser beam (as radius), $y_{0(AL)}$ is the y-position of the maximum of the hit rate distribution, $r_{DL(AL)}$ is the effective detection width at the ablation laser beam level (as radius), $\sigma_{p(AL)}$ is the particle beam width at the ablation laser beam level (as radius), $y_{\overline{DA}}$ describes a possible shift offset of the center position of the ablation $(y_{0(AL)})$ to that of the detection spot (y_0) determined at the second detection laser using Eq. 4 and bg is a value for the background. However, the effective detection width at the ablation spot $(r_{DL(AL)})$ and the effective width of the ablation laser beam (r_{AL}) depend on each other. To avoid this problem, the parameters for the particle beam width (σ_p) , the effective detection width (r_{DL}) , and the center position of the detection spot (y_0) were each determined first at the second detection laser using Eq. 4 before applying Eq. 5. Subsequently, the resulting particle beam width and the effective detection width were scaled up to the distance to the ablation laser in analogy to Sect. S7, resulting in $r_{DL(AL)}$ and $\sigma_{p(AL)}$. Finally, the values of y_0 , $\sigma_{p(AL)}$ and $r_{DL(AL)}$ were kept constant during the fit using Eq. 5. Therefore, only independent parameters were used for the fit. The values $\sigma_{p(AL)}$ and $r_{DL(AL)}$ were set as constant, because they were determined from the respective simultaneous scan at the

second detection laser and scaled up to the ablation laser beam distance in analogy to Supplement Sect. S7. For the fit function additional assumptions had to be made: 1) The effective particle detection spot at the level of the ablation laser beam must be larger than the effective particle ablation spot of the ablation laser. 2) Negative background values for *bg* were not allowed. A parameter for the background *bg* was used, due to the low number of laser pulses per scan position. Especially at the edges of the detection area, individual hits can significantly change the curve fit. 3) The edges of the hit rate curve were determined considering that either the number of coincidences sized particles for the respective scan position contains at least five percent of the maximum number of coincidences sized particles per scan or if the number of hits was smaller than the number of laser pulses per scan position. The last point led to a slight distortion of the edges of the hit rate distributions. Otherwise, individual hits at the edges of the measuring range could have led to an increase in the distribution again, so that no meaningful results could have been obtained from the fit process. Here we focus on the maximum position of the hit rate distributions and on the effective width of the ablation laser beam.

The calculations of the particle deflection in an electric field (see Fig. 6 and Eq. 1) showed that the charge and size of particles have an influence on their flightpath through the mass spectrometer. To verify the charge effects, up to five different particle charges were used for each particle size. Using a DMA and monodisperse PSL particles enables a size-dependent charge selection. For the selection of differently charged particles of one size, the DMA voltage was calculated and set according to the manual of the DMA (TSI, 2009).

4.5 Results of the DIE and electric shielding characterization

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4.5.1 Influence of particle charge on the hit rate without electric shielding using a fixed ALS position

A simple approach to examine the effect of particle charge on the hit rate is shown in Fig. 17. The experiments were conducted with polydisperse mineral dust particles suspended in water and nebulized by an atomizer and with polydisperse particles sampled from laboratory air. In addition, two different measurement configurations were used: 1) suppressing the electric field using the DIE as described above; 2) using an aerosol neutralizer to modify the charge distribution of the particles. During the measurement of these two particle samples the ALABAMA was not yet equipped with the electric shielding.

Figure 17a shows that the hit rate for dust particles is lowest when neither the neutralizer nor the DIE is applied and highest when both devices are applied together. Thus, both delayed ion extraction and neutralizer applications increase the hit rate. This indicates that the deflection of charged particles from the straight flight path caused by the electric field is one of the reasons for the low hit rate. For laboratory air particles (Fig. 17b) the effect is similar, but no improvement is observed when the neutralizer is applied without the DIE. This suggests that particles in ambient air are in a Boltzmann charge equilibrium (Wiedensohler, 1988; Wiedensohler et al., 1986), such that a neutralizer does not change the natural charge distribution. In contrast, particles produced by an atomizer such as the dust particles in Fig. 17a appear to carry more elementary charges. Hence, modifying the charge distribution to a Boltzmann distribution by a neutralizer reduces the deflection of the dust particles in the electric field. Thus, it could be concluded that the different hit rates from the dust particle measurement using a neutralizer and the DIE to

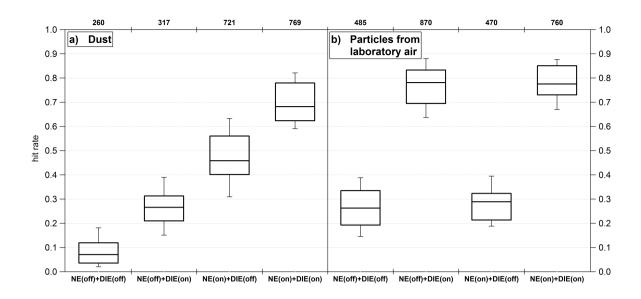


Figure 17. Hit rate for two particle types (dust and laboratory air) with and without a particle neutralizer (NE) and either using the setup DIE(on) with the delayed ion extraction or the setup DIE(off) with a constant ion extraction field. The results are presented as a box-and-whisker plot, with whiskers corresponding to the 10th and 90th percentile. The number of generated mass spectra for each experiment is given on top of the graph. Particle sizes of the samples given as median and inter-quartile range (Q75 – Q25): 1) dust: 575 nm and 115 nm, 2) laboratory air: 454 nm and 113 nm

the measurement using only the DIE are due to an electric field located outside the electrodes, which has an influence on the flight path of highly charged particles.

4.5.2 Influence of particle size and charge on the hit rate using a fixed ALS position

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To measure the size-resolved hit rate, PSL particles from the atomizer were size selected by the DMA. Not only singly charged particles were selected (as is the normal operation mode of the DMA), but also multiply charged particles as explained in Sect. 4.4. The influence of the particle charges on the hit rate was investigated using three different setups. The first setup, referred to as DIE(off), is the previous setup of the ALABAMA with a constant electric field between the first positive (nEx1) and negative (pEx1) ion extraction electrode (each 1100 V; according to Fig. 2). The second setup, referred to as DIE(off+), is similar to the prior mentioned one, but only the positive electrode is switched on and set to 1100 V. The idea behind this setup is to reduce the electric field within the ion extraction region. This should lead to a reduced deflection of charged particles. The third setup includes the newly installed delayed ion extraction, referred to as DIE(on). With the installed DIE no deflections of charged particles are expected. In the following, all three setups were used together with the electric shielding (see Fig. 8).

The size-resolved hit rate of the three setups differ significantly from each other, as shown in Fig. 18. Using the DIE(on) setup, a constant hit rate between 0.9 and 1.0 in the presented size range is achieved. Thus, we conclude that this setup

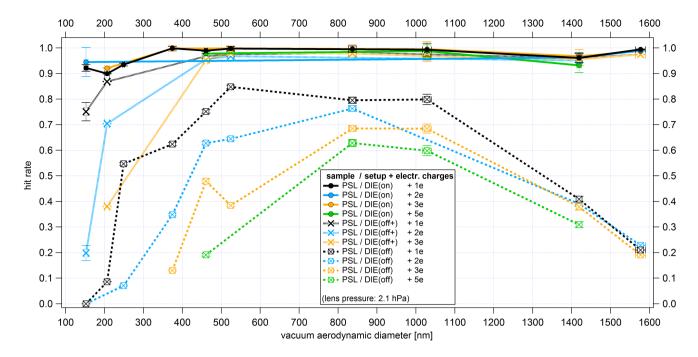


Figure 18. Size-resolved hit rate for PSL particles, using three different ion extraction field setups (line types) and differently charged particles (color code). The uncertainty of the hit rate is determined on the basis of binomial statistics related to the number of laser pulses from the ablation laser N_{Shots} and the number of successfully detected mass spectra N_{Hits} resulting from these laser pulses (see Supplement Sect. S15.3). The x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with the ALABAMA, converted into d_{va} according to Eq. S1 (Supplement).

eliminates the charge effects for all particle sizes. With the DIE(off+) setup, we observe also a large hit rate up to 1.0 in the size range from about 450 nm to 1600 nm (d_{va}). But in contrast to the previous setup with the DIE, a significant decrease of the hit rate is observed below about 450 nm, which is more pronounced for higher charged particles: For example, at 207 nm (d_{va}), the hit rate decreases from 0.87 for z = 1 to 0.38 for z = 3. This observation confirms the expected effects of size and charge on the deflection of charged particles (see Fig. 6). For the experiments with the DIE(off) setup, the observed hit rates are generally lower than in the two other experiments. Also here, the hit rate decreases with increasing charge numbers and decreasing particle size. Additionally, the hit rate decreases for particles larger than 1000 nm. However, the weaker charge dependence confirms Eq. 1 that the deflection in the electric field is weaker for large particles than for small particles. The decreasing trend above 1000 nm for this setup may be due to a size-dependent shift of the particle beam, which might be caused by mechanical imperfections of the ALS (e.g. Huffman et al., 2005). The reason behind this explanation for the assumption of a particle beam shift is that also for this setup hit rates up to 1.0 could be achieved for particles above 600 nm after changing the position of the aerodynamic lens.

4.5.3 Influence of particle size on the deflection of charged particles using the lens scan method

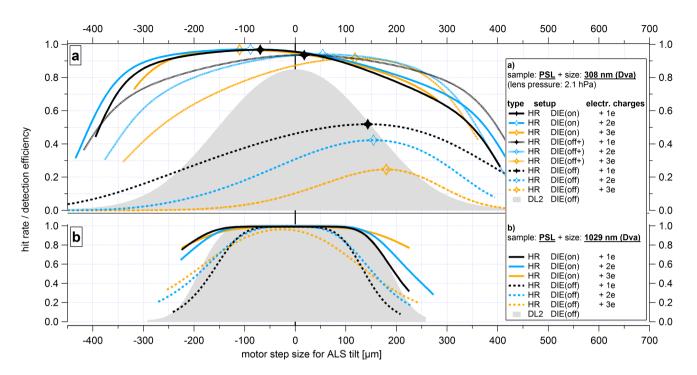


Figure 19. Hit rate (HR) distribution along the cross section of the ablation laser's beam path using differently charged PSL particles of size: a) 308 nm and b) 1029 nm for the three different ion extraction field setups. The curves are the fits through many data points, and the symbol marks the maximum of the curve, respectively. The bold solid (DIE(on)), dotted (DIE(off+)) and dashed lines (DIE(off)) correspond to fit curves with the hit rate resulting from the lens scans (according to Eq. 5). As a reference example, the detection efficiency at the second detection laser is shown by the gray shaded area. For this example, singly charged PSL particles in combination with DIE(off) setup were chosen. All hit rate curves are related to the maximum values resulting from the curve fit at the second detection laser (DL2) for each scan (0 on abscissa). The colors represent the different particle charges from z = 1 (black) to z = 3 (orange).

Using the automated lens scan, we determined the hit rate along the cross section of the ablation laser's beam path in relation to the detection efficiency along the cross section of the second detection laser. PSL particles with 308 nm and 1029 nm size were chosen for this experiment. Figure 19a demonstrates that with the DIE(on) setup almost no difference is observed between the curves for the differently charged 308 nm PSL particles. In contrast, scans with the DIE(off+) setup show a shift of the curves and their maximum positions with increasing charge number. Although the shape of the curves differ slightly between each other, a shift of their maxima of about 65 µm per charge number can be inferred. A calculation of the particle deflection within the electric field after Eq. 1, using 1100 V for both electrodes, resulted in a shift of roughly 90 µm for 300 nm PSL particles. However, for both first electrodes a voltage of 1100 V was assumed for the calculation. For the DIE(off) setup, the particle deflection is so strong that the shape of the curve seems to be deformed. Due to this deformation, the maximum

of the distributions can not be unambiguously determined. Nevertheless, the large deflection can be seen by the shift of the curves. For particles with higher charge numbers the curves deviate more from those of the DIE(on) setup.

To test whether the deflection only affects small particle sizes (as calculated before, see Fig. 6), the experiments were repeated for 1029 nm PSL particles as shown in Fig. 19b. It can be seen that neither the scans with the DIE(on) setup nor those with the DIE(off) setup show charge-dependent shifts of the curves. Furthermore, the curves are almost symmetric around the center point of the detection efficiency scan at the second detection laser (marked as the zero line). This shows that the particle beam for 1029 nm PSL is not dependent on their charges. However, it becomes clear that using the newly installed DIE results in a much broader range of effective ablation/ionisation and ion extraction compared to the setup without DIE. Thus, an enhanced hit rate can be achieved also at the edge of the ablation laser beam. The asymmetric curves for 308 nm PSL particles using the DIE(on) setup result from the assumptions made in Sect. 4.4, which lead to a slight distortion of the edges of the hit rate distributions. Furthermore, the measurements revealed a slight offset between the beam center position of the second detection laser and the beam center position of the ablation laser, which also contributes to an asymmetry.

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4.5.4 Influence of the ion extraction field setup on the effective width of the ablation laser beam using the lens scan method

The effective width of the ablation laser beam indicates the spatial extent to which the particles can still be ablated so effectively that they produce a sufficient amount of ions to generate a mass spectrum. As described above, the effective width for the ablation/ionisation and ion extraction process is derived from the hit rate fit function (see Eq. 5). This was done for the three different ion extraction field setups as a function of particle size.

It can be seen in Fig. 20 that the effective width of the ablation laser beam is much larger using the DIE(on) setup than with the DIE(off) setup, for all particle sizes. This indicates that using the DIE it is possible to generate mass spectra of particles that are further away from the center of the ablation laser's beam path, compared to the DIE(off) setup. This is particularly important for aspherical particles, because such particles are less well focused than spherical particles (see Fig. 14). A more detailed analysis of the influence of the DIE on the ion yield is shown below. For the DIE(off+) setup similar effective widths of the ablation laser beam can be achieved as for the case of the activated DIE. The reason for the larger discrepancy at about 600 nm could not explained. As already mentioned, the determination of the effective ablation laser beam width is dependent on the effective width of the detection lasers, which is also shown in Fig. 20, but extrapolated to the ablation point. Nevertheless, the results are useful to highlight the differences in the spatial extent of the effective ablation/ionisation and ion extraction process for the different setups.

4.5.5 Influence of the ion extraction field setup on the mass spectral signals using the lens scan method

To investigate how the different setups influence the quality of the mass spectra, two characteristic features of the spectra were investigated: Along the scan path, the number of resulting m/z-signals per PSL mass spectrum and their cumulative intensity were averaged for each position perpendicular to the ablation laser beam (see Fig. 21). The evaluation of the m/z-signals is based on ion peak area of the spectral lines that were obtained using the software tool CRISP (Concise Retrieval of Information

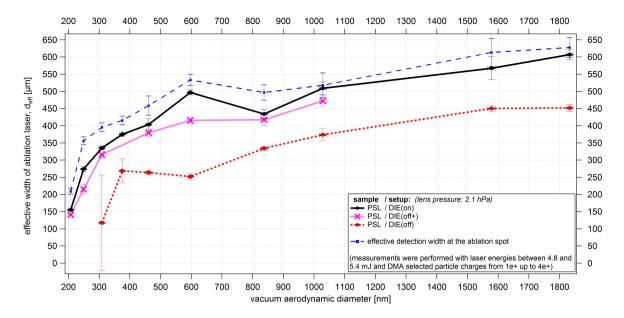


Figure 20. Averaged effective width of the ablation laser beam for the different ion extraction field setups resulting from lens scans (see Sect. 4.4). The y-uncertainty range is given by the uncertainty of the fit of each scan (see Fig. 12) and Gaussian error propagation. The x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with the ALABAMA, converted into d_{va} according to Eq. S1 (Supplement).

from Single Particles; Klimach, 2012). The ion peak area (in mV-sample) of a certain mass-to-charge ratio is determined by integrating the raw spectra of the ion flight times (Klimach, 2012). In the resulting mass spectrum the ion signals are displayed as sticks of which the height is proportional to the ion peak area ("stick spectrum"). In addition, a threshold value was defined for determining the number of m/z-signals. For this purpose, about 40000 empty spectra of particle free air were recorded and converted into stick spectra. Subsequently, all existing sticks were averaged (\bar{A}) and their standard deviation (σ) was determined. Using $\bar{A} \pm 3 \cdot \sigma$, the absolute anion and cation threshold is 8.19 mV-sample and 5.33 mV-sample, respectively. Thus, each m/z-signal of the PSL mass spectra above this threshold were counted as an actual signal. Using these counted signals, the number and sum of the m/z-signals per mass spectrum were determined and subsequently averaged over the total number of mass spectra detected per particle beam position.

Figure 21 shows an example for a scan through the cross section of the ablation laser's beam path, using 1029 nm (d_{va}) PSL particles. Panel a in Fig. 21 clearly indicates the differences in m/z-signals between the three setups: with DIE(on) the sum of m/z-signals is by more than a factor of seven higher compared to the other setups. It is not surprising that the DIE(off+) setup with the negative electrode pEx1 switched off has a reduced cation signal intensity. This is because pEx1 has an influence on the flight path of the positive ions in the extraction region, which is important for the number of ions collected and their mass separation. Similar differences exist for the number of m/z-signals per cation spectrum (Fig. 21c). A significantly higher

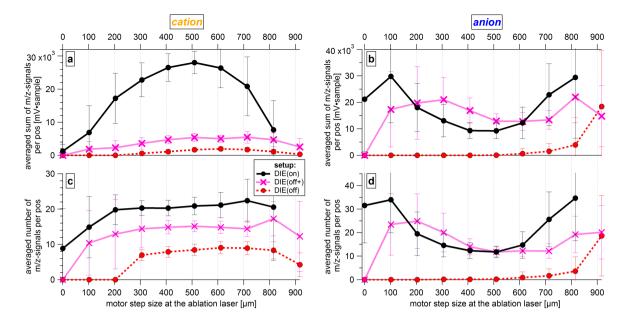


Figure 21. Mass spectral information in dependence of the particle beam position Dependence of mass spectral information on particle beam position along the cross section of the ablation laser's beam path and the applied ion extraction field setup using $1029 \text{ nm} (d_{va}) \text{ PSL}$ particles. Panel a) and b) represent the averaged signal intensities of the mass spectra per scan position. Panel c) and d) represent the averaged number of m/z-signals of the mass spectra per scan position. Measurements were performed with laser energies between 4.8 mJ and 5.4 mJ and with the DMA that selected particle charge number of z = 1. PSL particles of $1029 \text{ nm} (d_{va})$ result in a particle beam width as diameter of about $150 \,\mu\text{m}$ for 4σ (= 95 % of particles) at the ablation point and in an effective ablation laser beam width of about $500 \,\mu\text{m}$. The uncertainty bars correspond to the standard deviation of the number and sum of the m/z-signals of the mass spectra per position.

number of m/z-signals above the threshold is obtained when using the DIE. Again, the ion yield is lowest with the DIE(off) setup. Furthermore, along a wide range through the ablation laser beam the number of cation signals is quite constant for all three setups. The number of m/z-signals is an essential component for the application of cluster algorithms to mass spectra, which is useful to analyze a large amount of particle spectra. A different number of m/z-signals can result in a different particle classification. In addition, further chemical information can be obtained from additional m/z-signals, thereby allowing for a more accurate analysis of the particle composition. Moreover, an improved reproducibility of the cation mass spectra is observed when using the DIE (see Supplement Sect. S13).

In contrast to the cation signals, the anion signals result in similar values for the setups DIE(on) and DIE(off+) in both cases, the sum of the signal intensities (Fig. 21b) and the number of m/z-signals (Fig. 21d). However, the offset between the DIE(on) and the DIE(off+) curve is not fully understood yet. An even bigger difference is observed for the DIE(off) setup. It is also noteworthy that only a one-sided increase of the anion signals can be observed with the DIE(off) setup. For setups DIE(on) and DIE(off+), high anion signals are measured at both edges of the ablation laser beam, whereas anion signals using the DIE(off) setup are only observed when the particle beam is shifted towards the positive electrode (nEx1). One possible reason for this ef-

fect is that the path of the anions to the corresponding extraction grid is shorter in this case. However, the reasons for losing the anion signals at the other edge of the ablation laser beam are still unknown. Moreover, it affects all particle sizes above 461 nm (d_{va}). Below 461 nm, no anion signals can be detected with the DIE(off) setup at all (see Supplement Fig. S8 and S9, Sect. S12).

Interestingly, the cation and anion signals behave in an opposite manner in Fig. 21. With increasing laser intensity, more cations but fewer anions were detected. With decreasing laser intensity towards the edges of the ablation laser beam, however, more anions but fewer cations could be detected. This effect was observed in our experiments for all PSL particles larger than 290 nm (d_{va}). Similar observations have been reported from studies of oleic acid particles using varying laser intensities and wavelengths (Thomson et al., 1997). In Thomson et al. (1997) it was found that the ion formation process has a non-linear dependence on laser energy using laser wavelengths of 193 nm and 248 nm. Furthermore, they found out that the ion formation threshold depended on particle sizes and ion polarity. The latter point resulted in a lower ion formation threshold for cations than for anions. As a possible reason for the decreasing ion yield of anions at higher laser energies, an increasing formation of free electrons was assumed, whereby the electrons absorb so much energy that they can leave the solid before they can transfer the energy to the lattice, resulting in a reduced number of negatively charged ions (Thomson et al., 1997; Varel et al., 1998; Vertes et al., 1988). A possible explanation for the different ion yields (for both cations and anions) in the different setups is the spatial distribution of the ions directly after particle ablation and ion forming process, which is associated with the electric field within the extraction region. Using the DIE, the ions can first move away from the ablation spot according to the momentum they have received from the ablation process. After about 70 ns the electric field is applied and the ions are extracted. If the DIE is not used, the permanent electric field causes an immediate deflection of the ions. As cations and anions are accelerated in opposite directions, the probability of interactions or collisions between cations, anions, and neutral molecule fragments increases in a denser ablation/ion plume, resulting in a lower ion yield.

4.5.6 Comparison of the particle size-dependent hit rate using a fixed ALS position

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The particle size-dependent hit rate of the ALABAMA with the new installed components, compared to earlier data of Brands (2009) and Brands et al. (2011) is given in Fig. 22. The measurements of Brands et al. (2011) were conducted with an ALABAMA setup without delayed ion extraction and without electric shielding, together with the previously used Liu-type aerodynamic lens. In addition, the measurements of Brands et al. (2011) were carried out using a 100 µm pinhole as a critical nozzle and a pressure inside the aerodynamic lens of 3.8 hPa. The data with the new setup were taken at a lens pressure of 2.1 hPa and 2.4 hPa, respectively. Both the newly installed delayed ion extraction and the electric shielding, together with the improved particle beam properties, have a significant influence on the size-resolved hit rate. The results presented here were obtained at the same fixed ALS position as those which were used for the detection efficiency measurements of the coincidence sized particles in Sect. 4.3.1 (see Fig. 13).

Figure 22 shows that with the improvements of the ALABAMA a hit rate above 0.8 can be achieved for PSL particles between 150 nm and 2600 nm (d_{va}), with an ALS pressure of 2.1 hPa. Similar values are reached with a lens pressure of 2.4 hPa, with the exception of 153 nm PSL particles which are almost not hit at all. Possible reasons for this observation may

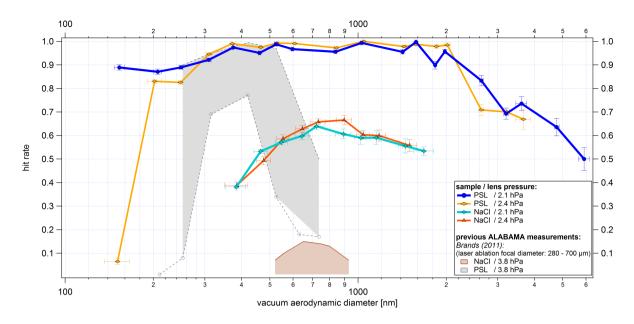


Figure 22. Size-resolved hit rate for PSL and NaCl particles using a lens pressure of 2.1 hPa and 2.4 hPa. ALABAMA measurements without the new features presented in this article are shown as colored areas. The colored areas (gray: PSL, red: NaCl) denote the hit rate achieved by Brands et al. (2011) by changing the diameter of the ablation laser beam focus from $280 \,\mu m$ to $700 \,\mu m$. The uncertainty of the hit rate is determined on the basis of binomial statistics related to the number of laser pulses from the ablation laser N_{Shots} and the number of successfully detected mass spectra N_{Hits} resulting from these laser pulses (see Supplement Sect. S15.3). The x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with the ALABAMA, converted into d_{va} according to Eq. S1 (Supplement).

be a stronger displacement of the particle beam axis or a significant change in the particle beam shape. The observed shift of the particle beam axis in the ablation region by roughly 300 µm between the particle size measurements from 153 nm to 1833 nm PSL using DIE and 2.1 hPa lens pressure (not shown here) suggests that the particle beam shift is a likely explanation.

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In contrast to the determination of the effective width of the ablation laser beam presented in Sect. 4.5.4, the diameter of the ablation laser beam in Brands et al. (2011) was determined by means of a microscope after laser pulses had previously been shot on photographic paper. With a diameter of 700 μ m, a hit rate of almost 100 % was achieved for PSL particles of about 400 nm, but at the same time no ion signals were detected for NaCl-particles at this focal diameter in their study. This finding was explained by a too low energy density in the area of the laser focus, such that NaCl particles were not ablated and/or not ionized (Brands et al., 2011). With a focus diameter of 280 μ m, the hit rate for PSL was reduced to below 80 %, since more particles miss the ablation laser beam. However, with the 280 μ m focal diameter the energy density was sufficient to generate and detect NaCl ions (Brands et al., 2011), resulting in hit rates up to 15 %. In comparison, using the newly installed components, hit rates of over 50 % in the size range from 460 nm to 1700 nm (d_{va}) can be achieved for NaCl particles. However, no significant difference in the hit rate is observed when increasing the ALS pressure from 2.1 hPa to 2.4 hPa.

The improved performance of the ALABAMA was further confirmed during aircraft-based measurements. In 2014, the ALABAMA was operated using the setup by Köllner (2020) during the ML-CIRRUS mission (Voigt et al., 2017), whereas in 2018, the ALABAMA was operated with all modifications presented here during the mission CAFE-Africa (Schneider et al., 2020). An increase in the hit rate of about five times was observed in both tropospheric and stratospheric aerosol particle analyses over the entire particle size range (Schneider et al., 2020).

Also with other single particle mass spectrometers, e.g. the LAAP-ToF-MS, hit rates between 80% and 100% can be achieved by using PSL particles over a wide size range (400 nm to 2000 nm) (Shen et al., 2018). The LAAP-ToF-MS is based on a different measuring principle compared to the ALABAMA: The ablation laser is already pulsed on particles when they trigger a scatter signal at the second detection unit. The ablation laser of the LAAP-ToF-MS is an excimer laser with a wavelength of 193 nm, which shoots in the opposite direction of the particles flight direction. On the one hand, this makes it possible to keep the device compact, on the other hand it makes the ablation laser less susceptible to variations in the timing of the laser pulse (Marsden et al., 2016). The increased ablation efficiency of the LAAP-ToF-MS is achieved at the expense of a lower detection efficiency, since the elliptical mirrors must be omitted due to the design, and so far only maximum detection efficiencies of about 25% at the first detection laser could be achieved using PSL (Marsden et al., 2016).

5 Application example: Ice nucleating particles

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To verify that the hit rate of INPs can be improved by applying the DIE, additional laboratory measurements at the Leibniz Institute for Tropospheric Research were conducted. The setup for these measurements has been described in Sect. 4.1.3 (see Fig. 10). The INP measurements were done with the new aerodynamic lens system, the delayed ion extraction and the installed electric shielding in the ALABAMA. Due to the complexity and expense of these measurements, only the DIE could be tested for improvements.

Three different particle samples were used for the analysis: a) Birch pollen (d_{mob} 500 nm); b) Snomax (d_{mob} 500 nm) and NaCl (d_{mob} 300 nm) externally mixed and c) Feldspar (d_{mob} 500 nm). Birch pollen, Snomax and Feldspar particles become immersed in a water droplet and freeze heterogeneously upon cooling under the aforementioned conditions inside of FINCH or SPIN. In contrast, NaCl particles activate to droplets, but freeze only homogeneously below -38° C. Since FINCH was operated at a temperature of about -24° C and SPIN at about -25° C and -36° C in operating mode, only heterogeneous ice nucleation was investigated. The particle samples a) -c) were measured with four different configurations. First, the test particles were guided to the ALABAMA after ice activation in FINCH/SPIN and ice residual separation in the PCVI. Second, the particles were collected from the particle generator without prior ice nucleation and counterflow separation. Third and fourth, both setups were tested with an activated and a non-activated DIE. Here we focus on the observed hit rate between the different setups.

In general, the hit rate is higher for experiments with DIE than for experiments without DIE (Fig. 23). For all analyzed types of ice residuals the hit rate (median) is higher by more than a factor of two with DIE than without DIE. Interestingly, for all test particle types the hit rate of the ice residuals is lower than for the particles without prior ice activation. Even if the difference

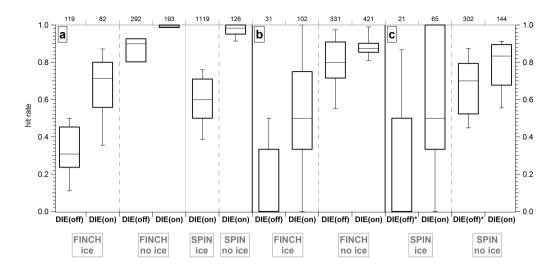


Figure 23. Hit rate for three particle samples a) Birch pollen (d_{mob} 500 nm), b) Snomax (d_{mob} 500 nm) and NaCl (d_{mob} 300 nm) externally mixed and c) Feldspar (d_{mob} 500 nm), and the different ice nucleation setups: FINCH or SPIN together with PCVI in ice activation mode (labeled as ice): with prior ice activation and separation process; FINCH or SPIN together with PCVI in no ice activation mode (labeled as no ice): without prior ice activation and separation process, but still with the particle flow through FINCH or SPIN and PCVI. Each particle sample was tested using the DIE(on) and DIE(off) setup in ice activation and no ice activation mode. For the Birch pollen sample the SPIN measurements were only performed with the DIE(on) setup. The measurements marked as DIE(off)* were performed with 450 V and 1100 V at the electrodes pEx1 and nEx1. In contrast, the unmarked measurements were carried out with 1100 V each. The results are presented as a box-and-whisker plot, with whiskers corresponding to the 10th and 90th percentile. The number of generated mass spectra for each experiment is given on top of the graph.

in the case of the externally mixed sample may be explained by the missing NaCl particles in the heterogeneous ice activation mode, it is not expected for birch pollen or Feldspar. This finding can not be explained by particle charging effects, because this should be compensated by the DIE. Since both the FINCH measurements and the SPIN measurements show a decrease of the hit rate in the ice activation mode, it also seems to be independent of the INP-counter used. The reasons for the lower hit rate of the ice residuals compared to the untreated test particles is not known. One possible explanation might be a modification of the particle shape caused by the ice activation and evaporation processes as described in Adler et al. (2013). Although a certain amount of contamination particles was detected, we can rule out that this was the main reason for the observed decrease in the hit rate (see Supplement Sect. S14). Nevertheless, the use of the DIE achieves a significant improvement in the hit rate of INPs, which generally leads to improved statistics.

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6 Summary and Conclusions

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We demonstrated that the performance of the single particle mass spectrometer ALABAMA was significantly improved by using a newly developed aerodynamic lens system, a delayed ion extraction, and a better electric shielding. Improvements in detection efficiency were observed over a wide particle size range, both for spherical and cubic particles. For PSL particles, detection efficiencies of 90 – 100 % in the particle size range of 350 – 1800 nm could be measured using the new ALS at a fixed position and at a lens pressure of 2.1 hPa. These high detection efficiencies were confirmed by measurements of the particle beam width and the effective width of the detection lasers. The particle beam width (four σ_P , including 95 % of all particles) in the size range from 350 nm to 1800 nm was smaller than 200 µm, whereas the effective width of the detection lasers was larger than 200 µm. With the new ALS it was further possible to extend the detectable particle size range especially for large particles compared to the Liu-type ALS, which was previously used in the ALABAMA. This led to an increase of the upper 50 % cut off diameter in detection efficiency $\frac{d_{50(coinc)}}{d_{50(sizedP)}}$ by more than 1300 nm with the new ALS, resulting in a $\frac{d_{50(coinc)}}{d_{50(coinc)}}$ $d_{50(sizedP)}$ size range of 230 – 3000 nm for PSL particles at a lens pressure of 2.1 hPa. However, whether the extended particle size range with the new ALS was due to reduced particle impaction losses in the ALS, a more effective focusing of larger particles within the new ALS and/or a smaller size-dependent shift of the particle beam could not be conclusively assessed. For cubic NaCl particles the modifications achieved up to two times higher detection efficiencies. Nevertheless, measurements with NaCl particles showed a significantly broader particle beam and smaller effective widths of the detection lasers compared to PSL particles, resulting in a maximum detection efficiency of about 25 %.

Further, the new components achieved an improved hit rate for particles of different shapes and compositions (e.g. PSL, NaCl, mineral dust, birch pollen washing water). On the one hand, the delayed ion extraction and the electric shielding prevent the undesired deflection of charged particles in the ion extraction field, which is particularly important for small, light and highly charged particles. On the other hand, the delayed ion extraction increases the ion yield from the ablation/ionization and ion extraction process, which led to more and higher mass spectral signals of the measured PSL particles. The increased ion yield further resulted in a larger effective width of the ablation laser beam, which in turn led to PSL particle hit rates of more than 80 % in the size range from 150 nm to 3000 nm. The hit rate of NaCl particles was approximately quadrupled compared to previous measurements. Additionally, an improved reproducibility of the cation mass spectra was found when using the DIE.

In summary, it can be stated that the previous design of the ALABAMA has been successfully modified, since both hit rates of up to 100% and detection efficiencies of up to 100% were achieved in a size range from 350 nm to 2000 nm. Thus, the new components of the ALABAMA generally result in a significantly improved particle analysis and sample statistics. This is particularly important for measurements of low number density particles such as ice nucleating particles and for aircraft-based measurements at high altitudes or where high temporal and spatial resolution is required. For future measurements in environments with low particle concentrations it would be conceivable to increase the sample statistics even further by increasing the sample flow into the ALABAMA. To achieve this, the skimmer opening could be reduced so that even with increasing sample flow, the maximum pressure for using the high voltages in the mass spectrometer is not exceeded.

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Author contributions. HCC measured all the particle samples, produced all figures and wrote the manuscript with the help of JS and FK. HCC, TK designed the aerodynamic lens. HCC designed the air diffusor. FH, FR designed the constant pressure inlet. FH designed the alignment holder for the ALS. FH, TK, HCC implemented the DC motors and the motor control for automated tilting of the aerodynamic lens system. HCC, TK, FH designed the electric shielding. HCC, FH, TK implemented the DIE. HCC analyzed the data with the help of TK, JS and FK. AH conducted and evaluated the ERICA measurements. JS, HW, SM and FS coordinated and supported the TROPOS measurements. SM operated the pumped counterflow virtual impactor. RK, FF operated the FINCH. AW operated the SPIN. SB, JS, FK, SM, HW, FH, TK, AW, FS and FF participated in the review of the analyses and manuscript preparation.

Competing interests. The authors declare that they have no competing interests.

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Optimizing the detection, ablation and ion extraction efficiency of a single particle laser ablation mass spectrometer for application in environments with low aerosol particle concentrations

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S1 Particle size measurement

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Size-resolved measurements with PSL particles of known size are used to convert the measured particle flight times between the two detection lasers into vacuum aerodynamic diameters at the respective ALS pressure. For this purpose, a corresponding averaged flight time between the first and the second detection laser was determined for each particle size, which results from a time counter of the electronics and is called "upcounts". The upcounts values multiplied by the 40 ns time steps of the time counter correspond to the flight time of the particles in nanoseconds. Afterwards Eq. S1 was fitted to the size-dependent upcounts values (see Fig. S1). This was performed for different lens pressures, since the particle velocity depends on the pressure gradient at the exit of the ALS. The PSL particles used here are regarded as almost perfect standard calibration particles due to their spherical shape and a particle density of 1.05 g cm⁻³. Using Eq. S1 and the resulting pressure specific curve fit parameters, the particle flight times were converted into vacuum aerodynamic diameters, taking into account the particle density. The correlation between the particle diameters and the determined flight times as upcounts values is shown in Fig. S1.

The size calibration equation modified according to Klimach (2012):

15
$$d_{va} = \frac{k}{\ln\left(\frac{a \cdot upcounts - b}{a \cdot upcounts - \frac{L}{upcounts \cdot 40 \cdot 10^{-9}}}\right)}$$
(S1)

with the dimensionless fit parameters k, a and b. L is kept constant at 0.07. Due to the modification, the physical relationship of the equation as described in Klimach (2012) and Köllner (2020) is no longer given and must be considered as purely empirical. The adaptation of the equation had become necessary due to the larger particle size range.

Equation S1 was fitted to the measured points in the particle size range between 150 nm and 3500 nm. Particle flight times above 3500 nm were not taken into account because the fit would have been overestimated and could therefore not represent

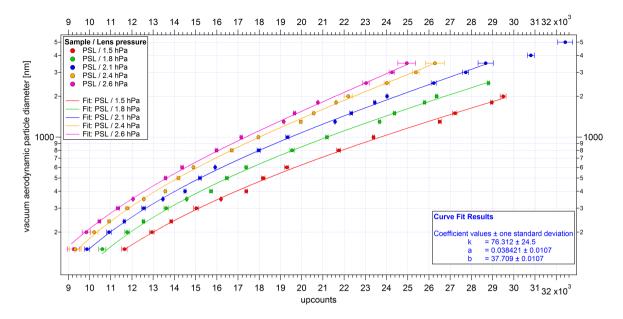


Figure S1. Size calibration curves using PSL particles for lens pressures between 1.5 hPa and 2.6 hPa. The curve fit results are obtained for a lens pressure of 2.1 hPa. The particle flight times were determined with the ALABAMA including the new ALS. The x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with ALABAMA.

well enough the smaller sizes. Thus, the flight times for the PSL particles at 4170 nm and 4900 nm (according to the manufacturer) were not used to determine the size calibration parameters at 2.1 hPa. Due to the fact that sizes above 3500 nm were not taken into account, extrapolation of the calibration curve for these particles ultimately resulted in significantly larger vacuum aerodynamic diameters than would result from calculations (DeCarlo et al., 2004).

S2 Calculations with the aerosol lens calculator

In the following a brief comparison between the results obtained by the aerosol lens calculator (Wang and McMurry, 2006a, b) for the Liu-type lens and our new aerodynamic lens, focusing on the particle beam width (Fig. S2). For particle sizes below 500 nm, the calculations of the aerosol lens calculator result in a slightly better focusing characteristic of the Liu-type lens compared to the aerodynamic lens developed in this study. However, above 500 nm the focusing property of the Liu-type lens decreases rapidly, whereas the newly developed lens geometry allows narrow particle beams over a much larger particle size range detectable by the ALABAMA. For the experimentally determined particle beam widths even better focusing properties are obtained in combination with the new lens design. A considerable discrepancy between theoretical and experimentally determined particle beam widths results from particle sizes larger than 1500 nm. Here, the conically shaped orifices in the aerodynamic lens system are probably a major reason for the significantly narrower particle beam widths in the experiments. As

already mentioned in the main part, the calculation with the aerosol lens calculator assumes the individual orifices correspond to thin cylindrical discs.

Inputs (ALC): Aer			odynamic Lenses Testing							
Gas Properties (@ 1atm, 296.15K)				Lens Conditions				Particle Properties		
Mass	28.964	g/mol		n (orifice)	5			ρ	1000	kg/m3
Specific heat ratio	1.4			Pressure before inlet	101325	Pa		dp1	5000	nm
Viscosity	1.8E-05	Pa s		Pressure before Lens#1		Pa		dpn	100	nm
Sutherland const.	110.4	K		Pressure after nozzle	2	Pa				
Mean free path	67.4	nm		Volumetric flowrate	1,00E-01	slm				
				Operating temperature	300	K				
				Detector distance	138.1	mm				
Lens Dimension: This study										
Lens#	0	1	2	3	4	5	6			
diameter(mm)		7.8	7	6.2	5.4	4	2.8			
spacer L(mm)	199.5	43.5	34	34	34	42.9				
tube D(mm)	39	31.2	31.2	31.2	31.2	31.2				
Lens Dimensions: Liu type Lens										
Lens#	0	1	2	3	4	5	6			
diameter(mm)		5	4.8	4.5	4.3	4	3			
spacer L(mm)	30	29	29	29	29	29				
tube D(mm)	6.4	9.5	9.5	9.5	9.5	9.5				

Output (ALC):	Experimental:		
Beam width (1σ) at the detector (μm)	Liu type Lens	Lens of this study	Lens of this study
dp(nm)	2. Detector	2. Detector	2. Detector
100	103	357	
150	70	106	133
200	54	131	102
300	40	70	67
400	36	58	51
500	73	62	33
600	264	53	41
800	2947	69	25
1000	3025	70	25
1325	3017	73	
1500	3012	276	23
2000	3011	2072	34
2550	3010	6855	81
3000	3010	13561	140
3775	3010	19523	
5000	3009	19523	-

Figure S2. A comparison of the results from the calculations of the aerosol lens calculator between the Liu-type lens and the aerodynamic lens from this study. The left table shows the input parameters and the right table shows the resulting size-resolved particle beam widths (in μm) for the respective lens design as output. The green marked particle sizes show the particle size range in which the new lens geometry results in a theoretical improved particle beam focusing. In the rightmost column, the particle beam widths experimentally determined in this study are shown for comparison. In order to compare the particle beam widths calculated with the aerosol lens calculator with the particle beam widths determined experimentally, the theoretical values were converted into widths of one sigma. For the conversion of the theoretical values it was assumed that the particle beam diameters originally resulting from the aerosol lens calculator, which comprise 90% of all particles (Wang and McMurry, 2006a), describe a 2-dimensional circular Gaussian distribution.

S3 Deflection of charged particles in an electric field

In order to assess the influence of an electric field on charged particles, their deflection in y-direction is determined theoretically (see Eq. (S2 - S3)).

The force on a charged particle in an electric field is determined by the electric charge of the particles q and the electric field strength E:

$$m_p \cdot a_y = q \cdot E \tag{S2a}$$

The electric field strength corresponds to the ratio of the voltage difference between the positive and the negative electrode U_y to the distance between the two electrodes d_{Ex} :

$$m_p \cdot a_y = q \cdot \frac{U_y}{d_{E_x}} \tag{S2b}$$

The integral is formed over the time the particle needs from the entry into the electric field t_0 to the ablation spot t:

$$\int_{t_0}^t a_y \, \mathrm{d}t = \frac{q}{m_p} \cdot \frac{U_y}{d_{Ex}} \cdot \int_{t_0}^t \mathrm{d}t = v_y(t) \tag{S2c}$$

Assuming t(0) = 0 and $v_u(t_0) = 0$, the particle velocity v in y-direction at time t results:

$$v_y(t) = \frac{q}{m_p} \cdot \frac{U_y}{d_{Ex}} \cdot t \tag{S2d}$$

To obtain the deflection of the particles (y) in the y-direction at time t, the integral over time is formed:

$$\int_{t_0}^t v_y \, \mathrm{d}t = \frac{q}{m_p} \cdot \frac{U_y}{d_{Ex}} \cdot \int_{t_0}^t t \, \mathrm{d}t \tag{S2e}$$

$$y(t) = \frac{1}{2} \cdot \frac{q}{m_p} \cdot \frac{U_y}{d_{Ex}} \cdot t^2 \tag{S2f}$$

Assuming a spherical particle shape, the particle mass can be expressed as a function of particle density ρ_p and particle radius r_p :

$$m_p = \rho_p \cdot V_p = \rho_p \cdot (\frac{4}{3} \cdot \pi \cdot r_p^3) \tag{S2g}$$

If the flight time t is replaced by the ratio of the flight distance L in the electric field (in x-direction) to the particle velocity v in x-direction and the electric charge q is replaced by the product of the elementary-charge constant e and the charge number z, the deflection of the particles at the ablation spot results as:

$$y(t) = \frac{1}{2} \cdot \frac{z \cdot e \cdot U_y \cdot L^2}{\rho_p \cdot (\frac{4}{3} \cdot \pi \cdot r_p^3) \cdot d_{Ex} \cdot v^2}$$
(S3)

Examples of the magnitude of the deflection are given in Sect. 3.2.1 of the main part.

S4 Determination of the NaCl particle shape

Using the approach and the assumptions made in DeCarlo et al. (2004) and Zelenyuk et al. (2006), both a dynamic shape factor and an effective density for individual particle types were determined, as shown for NaCl particles in Fig. S3 using the new ALABAMA setup.

To determine the dynamic shape factor \bar{X} and the effective density ρ_{eff} , the mobility diameter and the vacuum aerodynamic diameter are required according to the following equations (NaCl: $\rho_p = 2.17 g cm^{-3}$):

$$\bar{X} = \sqrt{\frac{\rho_p}{\rho_0} \cdot \frac{d_{mob}}{d_{va}}} \tag{S4}$$

$$70 \quad \rho_{eff} = \frac{d_{va}}{d_{mob}} \tag{S5}$$

The values for the dynamic shape factor and the effective density in Fig. S3 are comparable to the values for NaCl cubes shown in Zelenyuk et al. (2006), so it was concluded that the NaCl particles measured in this study have a cubic shape.

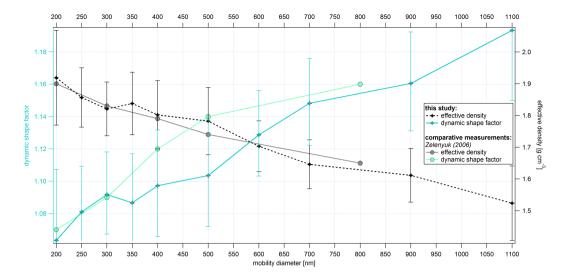


Figure S3. Determination of the size-dependent dynamic shape factors and effective densities for the measured NaCl particles. The values of the comparison measurement were taken from Zelenyuk et al. (2006). The y-uncertainties result from the standard deviations of the vacuum aerodynamic diameters determined with ALABAMA.

S5 Determination of the detection efficiency

For a conversion of the particle counts per seconds into a particle concentration, the flow into the device, which depends on the lens pressure, is required. The determination of the standard flow into ALABAMA was performed with the TSI flowmeter 4140 or with the DEFINER 220 Dry Cal at lens pressures between 1.5 hPa and 2.7 hPa. Afterwards, a polynomial function was fitted to the curve of the lens-pressure-dependent measuring points (see Fig. S4). The uncertainties of the manufacturer $(\pm 0.083\,cm^3s^{-1}$, TSI) were used for the additional weighting of the fit. A quadratic fit function $(f(x) = K0 + K1 \cdot x + K2 \cdot x^2)$ appears to be useful because the opening cross-section to be passed in the CPI should also have a quadratic dependence. Furthermore, it is assumed that at zero hPa lens pressure the flow into the device must be zero. Accordingly, K0 was set to zero to determine the parameters of the fit function.

To calculate the detection efficiency, the temperature and the pressure in the connected measuring system were used. The temperature information was taken from the flowmeter installed in the particle-free bypass line and the pressure was given by the OPC (see Sect. 4.1.2 and Fig. 9 in the main part). Thus it was possible to convert the standard flow rate ($flow_{Std}$) into a volume flow rate ($flow_V$, in cm^3s^{-1}), which is needed for a comparison with the OPC and the CPC.

$$flow_V = \frac{flow_{Std} \cdot p_{Std} \cdot \bar{T}}{\bar{p} \cdot T_{Std}}$$
(S6)

The terms p_{Std} and T_{Std} correspond to the standard pressure and standard temperature. The TSI standard conditions are 21.1°C and 1013 hPa. \bar{T} and \bar{p} represent the averaged temperature and pressure during the measurement time period. With the help

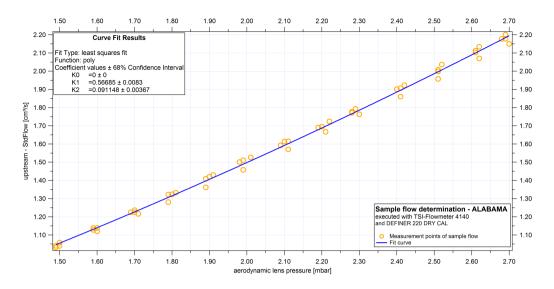


Figure S4. Determination of the lens pressure dependent sample flow into the ALABAMA (see text for details).

of the volume flow, the averaged number of particles detected per second can be converted into a particle concentration. This allows to determine both the detection efficiency of the individual detection units and those of the coincidences sized particles:

$$DE_{SizedP} = \frac{\frac{N_{SizedP}}{flow_V}}{C_{Ref}}$$
(S7)

 C_{Ref} corresponds to the averaged particle concentration measured at the same time with the reference instruments. N_{Coinc} is the number of particle coincidences sized particles per second.

S6 Cross talking

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Cross talking means if a high signal intensity is detected at one of the two photomultipliers of the detection units, this can cause a "ghost particle count" on the other detection record (the reason for this still has to be found), which would result in an incorrect particle concentration. This effect can be observed mainly at the first and sometimes at the second detection unit in the normal measurement mode. An increase in the detection threshold would lead to a loss of low signals in the edge areas of the laser and thus to a reduction in their effective laser widths. The thresholds were set in particle-free air in such a way that the background noise caused by the cw laser led to almost no erroneous particle counting. At the set thresholds, miscounts occured on average every 14 seconds for the first detection unit and every 18 seconds for the second. Incorrect coincidences sized particles were only counted every 912 seconds on average. In order to obtain results without cross talking effects, only one of the two detection lasers was used during some of the measurements and the other was switched off accordingly. With this procedure, the measurements were carried out individually for each detection unit. However, in order to measure the

coincidences sized particles and the hit rate, both detection units had to be switched on simultaneously. Due to the fact that two detectable light scattering signals within a time interval of ($\sim 0.3-1.3$ ms) are required for coincidences sized particles and due to the limitation of particle concentrations in the characterization measurements, an influence on the number of measured coincidences sized particles could not be observed.

S7 Conversion of the motor step size for the tilting of the aerodynamic lens system

The coefficients resulting from the fit function are initially only output in the step positions of the DC motors. Using calculations from the intercept geometry, a conversion factor can be determined for the step width at the respective measuring position in x-direction. For this, both the geometric distances of the DC motors and the distances of the individual lasers to the pivot point of the aerodynamic lens system must be known. With the respective conversion factors and the knowledge of the step sizes of the DC motors, the results can be given in metric units. An overview of the distances and conversion factors (CF) is given in Fig. S5.

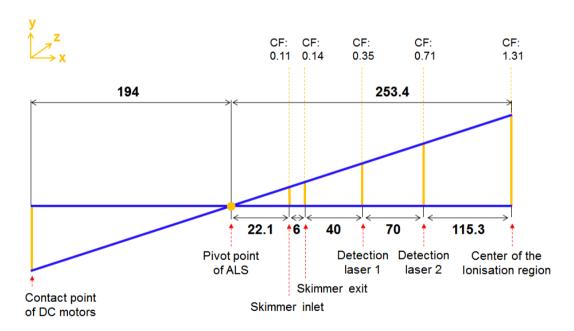


Figure S5. Distances of the components in the ALABAMA (in mm) and the corresponding conversion factors for the lens scan method; (not scaled)

S8 Particle detection rate

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Figure S6 presents the particle detection rate calculated as the product of particle detection efficiency (main part Sect. 4.3.1, Fig. 13), volume flow rate (Supplement Sect. S5), for a particle concentration of 1 particle cm⁻³. A higher flow rate only partly

compensates the lower detection efficiency for small particles (below 250 nm) with increasing lens pressure, but in general it becomes clear that a higher flow rate increases the particle detection rate. The current configuration limits the lens pressure to 2.6 hPa due to the vacuum requirements for the high voltages. In the future, the lens pressure (and thereby the flow rate) can possibly be further increased using a reduced skimmer opening without increasing the pressure in the high voltage area of the vacuum chamber.

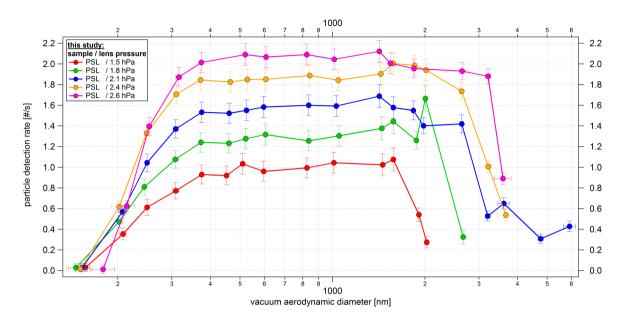


Figure S6. Size-resolved and lens pressure dependent particle detection rate. The y-uncertainty bars are given by the Gaussian error propagation of the detection efficiency and the volume flow rate. The x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with ALABAMA, converted into d_{va} according to Eq. S1

S9 Comparison of particle beam characteristics at a fixed ALS position

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Since no automated lens scan was possible in connection with the previous aerodynamic lens system used by Brands et al. (2011) and Köllner (2020), a qualitative comparison of the particle beam characteristics of the previously used (Köllner, 2020) and the new ALS is presented below. For this purpose, the ecincidences number of sized particles (particles detected at both detection lasers) are divided by the particle counts recorded at the same time at the first and the second detection unit. Thus, the results essentially depend only on the ALS (+ ALS holder) used and the detection units. Furthermore, uncertainties associated with the external reference devices are therefore irrelevant.

As can be seen in Fig. S7, measurements with the previously used ALS show a similar trend for both detection units, using the number ratio of particles resulting in coincidences (coinc) sized particles (SizedP) to particles counted at the two detection stages (DL1 and DL2) as c1 or c2, respectively. The coinc/c1-curve SizedP/c1-curve (DL1) can be explained in

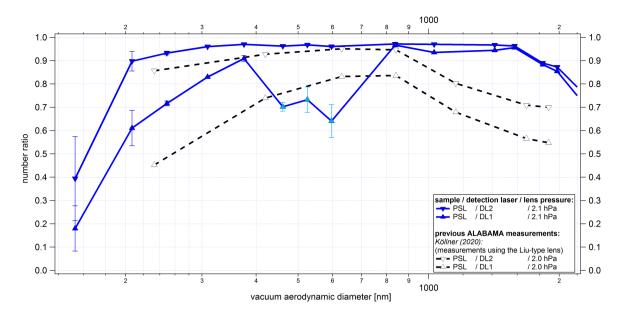


Figure S7. Qualitative comparison of particle beam divergences using the new ALS and the ALS previously used in ALABAMA with the Liu-type lens (Köllner, 2020). The number of particles resulting in coincidences sized particles is divided by the number of particles counted at the two detection stages (DL1 and DL2), respectively. The ratio is expected to decrease if the particle beam is wider than the effective width of the detection lasers. The measurement points displayed in a light blue were affected by cross talking effects. The y-uncertainty bars correspond to the standard deviation of the ratios.

that the particles tend to miss the second detection laser more quickly than the first detection laser as the width of the particle beam increases. However, a size-dependent displacement of the particle beam together with the alignment of the ALS specified by the holder or cross talking effects could also be of importance here. For *coincle2 SizedP/c2* (DL2), a similar curve can be explained by the fact that the second detection laser is aligned perpendicular to the first detection laser. This means that the particles can still be detected at the second detection laser despite missing the first detection laser. This in turn could mean that the particle beam for particles larger than about 900 nm is broader than the effective width of the first detection laser. Alternatively, the particle beam could be shifted along the beam path of the second laser and thus move out of the first laser at the same time. The same applies to *coincle2 SizedP/c2* for smaller particle sizes. However, the different ratios of c1/c2 indicate different causes for the decreasing ratios between smaller and larger sizes. In contrast, measurements with the new ALS show a more similar course between *coincle1* and *coincle2 SizedP/c1* and *SizedP/c2* over the same size range. In addition, the ratios over a wide size range are over 0.8. Thus, with the new ALS, the probability that a particle (PSL) triggers a signal at both detection lasers is higher. This applies to both smaller and larger particles. On the one hand, this could be explained by a narrower particle beam across all sizes or by a smaller size-dependent displacement of the particle beam. The outliers between about 400 nm and 600 nm that can be observed at the first detection unit are due to cross talking effects, the cause of which could not be definitively clarified. Regardless of whether the differences between the previously used and

the new ALS are caused by size-dependent particle beam widths or size-dependent displacements of the particle beam, the aforementioned indicators suggest that the new ALS achieves improved particle focusing.

S10 Multiple charge correction

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When using NaCl particles smaller than 600 nm (d_{va}), additional corrections were made to determine the detection efficiencies and hit rates. The reason for this is that below 600 nm not only singly charged but also multiply charged particles passed through the DMA, albeit only in low concentrations due to the impactor used. Thus, for the analysis an additional size-dependent selection was applied. For this purpose, the size-resolved UHSAS measurements were used. The corrected detection efficiency can be determined by selecting the corresponding size bins from the UHSAS and ALABAMA (according to Eq. S1). With this correction, for example, the detection efficiency of NaCl particles of size 464 nm (d_{va}) was adjusted from 3.8 % to 2 % in Sect. 4.3.1 (main part), whereas the particle number in the second size mode in the UHSAS is only about 3 % of the particle number in the size mode with the singly charged NaCl particles.

S11 Determination of stick spectra and units of measure

First, a wavelet transformation (Mexican hat wavelet) is performed to de-noise the raw spectra and correct the baseline. The positive part of the wavelet should then correspond to the measured signals (Klimach, 2012). Subsequently, a mass calibration over all mass spectra is performed with known ion masses (further details in Klimach, 2012). The resulting positions of the mass-to-charge ratios serve as starting points for the determination of the ion peak areas. For this purpose, a range around the respective mass-to-charge ratio is determined by means of a predetermined signal width, into which the raw signal is integrated over time. The averaged background level (defined by the height of the raw signal a half m/z position before and behind the respective mass-to-charge ratio) is then subtracted. The result is the so-called stick spectra. The height of a single stick for a specific mass-to-charge ratio thus corresponds to the ion peak area in mV*sample (sample: temporal resolution of the oscilloscope in 2 ns) for a mass-to-charge ratio and is referred to in this study as the m/z signal intensity.

S12 Size dependent characterization of mass spectral signals

To study the size dependence of the mass spectral signals, only the highest values (cumulated summed intensities and number of m/z-signals) were selected from each scan (as shown in Fig. 21 of the main part). These maximum values were averaged for measurements with different charge numbers (from z = 1 to z = 5) at this size, whereby the respective scan positions of the maximum values of the curves were not taken into account. Figure S8 shows the particle size resolved differences between the three setups for the cation m/z-signals.

First, there is a clear enhancement in intensity (upper panel at Fig. S8) and number (lower panel at Fig. S8) of cation signals using the delayed ion extraction compared to the setups DIE(off) and DIE(off+). Only for the particle sizes 837 nm and 1029 nm similar results can be observed in the number of m/z-signals using the DIE(off+) setup. The reason for this is not known. For

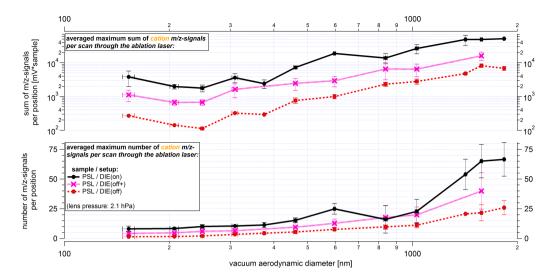


Figure S8. Size-resolved mass spectral information of cation m/z-signals in dependence of the ion extraction field setup. The upper panel shows the curve for the respective maximum signal intensities per lens scan (according to the approach shown in Fig. 21 of the main part). The lower panel shows the curve for the maximum number of m/z-signals per lens scan. Measurements were performed with laser energies between 4.8 and 5.4 mJ and DMA selected particle charge numbers from 1e+ up to 5e+. The y-uncertainty bars correspond to the standard deviation of the number and sum of the m/z-signals of the mass spectra. The x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with the ALABAMA, converted into d_{va} according to Eq. S1

all other particle sizes there is a clear separation between the results of both setups. As a result, there are more m/z-signals (cations) together with higher signal intensity resulting from using the delayed ion extraction.

In contrast to the cation signals, a comparison of the results from using the DIE(on) setup and DIE(off+) setup shows a very similar behavior in Fig. S9. Considering the sum of the m/z-signals or their number, differences can only be detected at the lower end or at the upper end of the size range. However, there is a big discrepancy to the DIE(off) setup. In this case anion signals can only be detected for particle sizes above $460 \text{ nm} (d_{va})$. However, the detected signal intensities and the number of m/z-signals are significantly below those of the two other setups.

S13 Reproducibility of mass spectral signals at a fixed ALS position

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To check whether the DIE also has a advantageous effect on the reproducibility of mass spectra, the relative dispersion of the number of m/z-signals was investigated. For this purpose, the respective number of the m/z-signals of cations and anions were formed for 100 randomly selected individual particle mass spectra. The lower and upper quartiles of the number of the m/z-signals were used to measure the dispersion. The difference between the upper and lower quartiles was divided by the median, which gives a relative dispersion based on the median (approach modified according to Drewnick, 2000). To define the

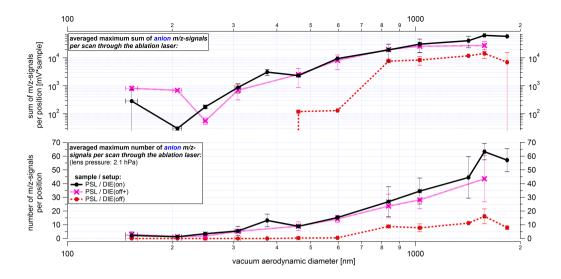


Figure S9. Caption the same as for Fig. S8, except for anions.

existence of a signal, the threshold value of $\bar{A}\pm 3\cdot \sigma$ was applied to the stick spectrum. To reduce the effect of charge-dependent particle deflection, only particle samples larger than 400 nm and with a charge number of z = 1 were used.

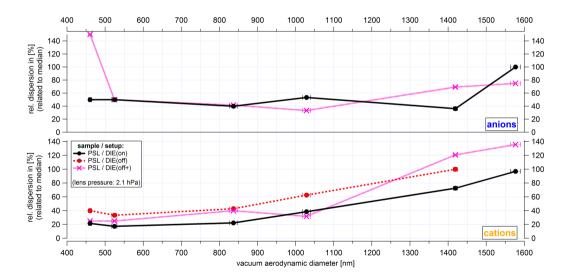


Figure S10. Reproducibility of mass spectral signals (upper panel: anion and lower panel: cation) in dependence of the ion extraction field setups. The x-uncertainty bars correspond to the standard deviation of the particle size distribution per particle size, particle type and lens pressure measured with ALABAMA, converted into d_{va} according to Eq. S1

Figure S10 shows that in the case of cations, the use of the DIE tends to lead to a slight improvement in the relative dispersion of the number of m/z-signals. The increase in dispersion towards larger particle sizes can be related to a shift in the particle

beam. If the particle beam is shifted to the area of the falling flanks of laser intensity, a larger variation of fragmentation may occur (as can be seen from the standard deviation in Fig. 21 of the main part). In the case of anions, on the other hand, no clear tendencies or improvements are discernible. Nevertheless, the advantage of using the delayed ion extraction becomes clear from the analysis of the cation signals.

S14 Mass spectral analysis of ice nucleating particles on the Birch pollen sample

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The evaluation of the birch pollen washing water (referred as Birch pollen) mass spectra indicates that contamination might play a role for the different hit rates with and without prior ice activation, as presented in Fig. 23 of the main part. Therefore, we first applied the fuzzy-c-means algorithm (Roth et al., 2016; Hinz et al., 1999; Bezdek et al., 1984) to the mass spectra of the particle sample experiments to check for different particle types, which are represented as clusters of mass spectra. Briefly, the algorithm was started with twenty randomly chosen mass spectra as starting points for the cluster centers. After that, every mass spectra spectrum was correlated with the mass spectra (cluster centers) of the twenty clusters and assigned to the cluster with the highest correlation coefficient. The resulting cluster mean mass spectra of the Birch pollen sample are comparable to those found by Schmidt (2016), although both the Birch pollen and the Sunflower pollen spectra shown there can be found in our data set. Based on the characteristic signals (ion markers) of the clusters a further analysis of the mass spectra was performed, the ion marker method (see Köllner, 2020, for more details). For this method, the ion markers must exceed a threshold value which has been determined by means of empty spectra as described in Sect. 4.5.5 (main part). Separate criteria had to be established for both polarities due to the partial absence of anion or cation signals. Typical biological ion marker for this interpretation include organic nitrogen and phosphorus: CN(-26), CNO(-42), $C_3H_3O_2(-71)$, $PO_3(-79)$, PO(+47)(Creamean et al., 2014). Further ion marker that could be assigned to birch pollen included K(+39) and $K_2CN(+104)$. In contrast to the fuzzy-c-means algorithm, the ion marker method is exactly reproducible and does not depend on randomly chosen mass spectra as starting points for the cluster centers.

Figure S11 shows the relative abundance of the particle types found in the six pollen experiments using the ion marker method. The gray colored particle types represent particles that can be attributed to biological origin like Birch pollen. Although it was not to be expected, particle compositions of mineral or metallic origin with signals of lithium, silicon oxide, aluminium, aluminosilicate, chromium and iron were found in addition to the mass spectra assigned to the Birch pollen. Furthermore, in some mass spectra, both mineral and biological signals were found together in the particles, hereinafter referred to as BioMin particles. It is shown that the mineral/metallic and BioMin particles make up a higher percentage of the total fraction during measurements with ice activation compared to measurements without ice activation, no matter if FINCH or SPIN is used. The difference in the FINCH measurement with ice activation can be attributed to the increased ion yield and larger effective width of the ablation laser when using the DIE(on) setup compared to the DIE(off) setup as described in Sect. 4.5.4 (main part). In general, it was not possible to clarify the origin of the mineral/metallic particle type within the scope of this work.

If the particles would indeed be due to contamination, this could result in a different hit rate, since mineral or metal containing particles have different shapes and chemical compositions compared to birch pollen, which can be assumed to be almost

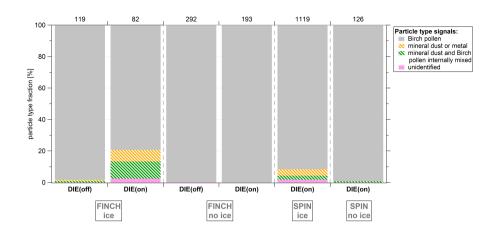


Figure S11. Particle type fractions using birch pollen sample as an example and using different measurement setups: FINCH or SPIN together with PCVI in ice activation mode (labeled as ice): with prior ice activation and separation process; FINCH or SPIN together with PCVI in no ice activation mode (labeled as no ice): without prior ice activation and separation process, but still with the particle flow through FINCH or SPIN and PCVI. For the Birch pollen sample the SPIN measurements were only performed with the DIE(on) setup. The unidentified particle type contains all those particles whose signals cannot be assigned to any of the other three particle types. The number of generated mass spectra for each experiment is given on top of the graph.

spherical (based on images under the microscope, Pummer et al., 2012; Augustin et al., 2013). The particle shape is decisive for particle focusing within the ALS. Further, the chemical elements of the contaminants can be ionized differently with the ablation laser, which has an influence on the ion yield and thus also on the hit rate. The assumption of a worse focusability/ionization of the mineral dust or metal containing particles compared to the birch pollen would therefore lead to a decrease of the hit rate if such contamination particles are present. Nevertheless, the following calculations suggest that contamination cannot be the main cause of the reduced hit rate:

$$HR_{ice} = HR_{no\ ice}(PS) \cdot nFrac(PS) + HR(cont) \cdot nFrac(cont)$$
 (S8)

where nFrac is the number fraction of the particle sample (PS) or of the contaminants (cont), HR_{ice} is the resulting hit rate with prior ice activation, $HR_{no\ ice}(PS)$ is the hit rate of the particle sample without prior ice activation, and HR(cont) is the hit rate of the contaminants. The highest percentage of the desired particle sample, i.e. nFrac(PS), and thus the lowest percentage of the contamination, i.e. nFrac(cont), we get for the worst acceptable hit rate of the contamination. Since there can be no negative hit rates, this would be HR(cont) = 0. Under these assumptions and using the results from Fig. 23 (Sect. 5, main part), the following number fractions result:

245 Birch pollen:

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FINCH and DIE(off): nFrac(PS) = 0.34 + nFrac(cont) = 0.66

FINCH and DIE(on): nFrac(PS) = 0.73 + nFrac(cont) = 0.27

SPIN and DIE(on): nFrac(PS) = 0.61 + nFrac(cont) = 0.39

250 Feldspar:

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SPIN and DIE(on): nFrac(PS) = 0.60 + nFrac(cont) = 0.40

This would be an immensely high contamination rate, which is actually even higher, since at least for DIE(on) the contamination hit rate is > 0 as Fig. S11 in the Supplement shows, where contamination was detected. Since this could not be seen in the number size distribution measurements behind the PCVI, it should therefore be excluded as a reason for the reduced hit rate at "ice" with prior ice activation and separation process.

S15 Uncertainty determination

S15.1 Uncertainties of the detection efficiency

The measurement uncertainty of the detection efficiency is determined as follows,

$$260 \quad \sigma_{DE} = \frac{C_{ALA}}{C_{Ref}} \sqrt{\left(\frac{1}{\sqrt{N_{ALA}}}\right)^2 + \left(\frac{1}{\sqrt{N_{Ref}}}\right)^2 + \left(\frac{\sigma_{flow_{Std}}}{flow_{Std}}\right)^2 + \left(\frac{\sigma_p}{p}\right)^2 + \left(\frac{\sigma_T}{T}\right)^2 + \left(\frac{\sigma_{C_{Ref}}}{C_{Ref}}\right)^2} \cdot 100$$
 (S9)

where C_{ALA} is the particle concentration calculated from the ALABAMA measurements. C_{ALA} can be both the calculated particle concentrations at the first or second detection unit, but also those of the coincidences sized particles. C_{Ref} corresponds to the particle concentration measured with the reference instruments (OPC, CPC). N_{ALA} and N_{Ref} are the particle counts measured with each instrument, which are required to determine the relative statistical uncertainties. The third term indicates the relative uncertainty of the standard sample flow into ALABAMA. The fourth and fifth terms represent the relative uncertainties of the measured pressure and temperature, which are given by the manufacturers with 2% and 1%. The last term indicates the uncertainties of the reference devices (Grimm OPC 1.129: 3% and TSI CPC 3010: 10%).

S15.2 Uncertainties of the flow determination

270 The polynomial fit function $f(x) = K0 + K1 \cdot x + K2 \cdot x^2$ (parameters see Fig. S4) and gaussian error propagation is used to determine the uncertainties of the sample flow $\sigma_{flow_{Std}}$ (Eq. S10), into ALABAMA. A 2.5 % uncertainty of the differential pressure sensor used (Analog Microelectronics) and a variation range of the lens pressure of 0.02 hPa are assumed.

$$\sigma_{flow_{Std}}a = \sqrt{((K1 \cdot p_L + K2 \cdot p_L^2) - (K1 \cdot (p_L + 0.02) + K2 \cdot (p_L + 0.02)^2))^2} / (K1 \cdot p_L + K2 \cdot p_L^2)$$

$$(S10)$$

$$275 \quad \sigma_{flow_{Std}}b = \sqrt{((K1 \cdot p_L + K2 \cdot p_L^2) - ((K1 + \sigma K1) \cdot p_L + (K2 + \sigma K2) \cdot p_L^2))^2} / (K1 \cdot p_L + K2 \cdot p_L^2)$$

$$\sigma_{flow_{Std}}c = \sqrt{((K1 \cdot p_L + K2 \cdot p_L^2) - (K1 \cdot (p_L + p_L \cdot 0.025) + K2 \cdot (p_L + p_L \cdot 0.025)^2))^2} / (K1 \cdot p_L + K2 \cdot p_L^2)$$

$$\sigma_{flow_{Std}} = \sqrt{\sigma_{flow_{Std}}a^2 + \sigma_{flow_{Std}}b^2 + \sigma_{flow_{Std}}c^2}$$

In addition, the uncertainties ($\sigma K1$ and $\sigma K2$) of the polynomial fit function is taken into account.

S15.3 Uncertainties of the hit rate

280 To determine the uncertainty of the hit rate σ_{HR} , the approach presented in Köllner (2020) is used.

$$\sigma_{HR} = \frac{\sqrt{N_{Hits} \cdot (1 - HR)}}{N_{Shots}} \tag{S11}$$

The uncertainty of the hit rate (HR) is thus determined on the basis of binomial statistics related to the number of laser pulses from the ablation laser N_{Shots} and the number of successfully detected mass spectra N_{Hits} resulting from these laser pulses.

S15.4 Uncertainties of the particle beam divergences

To determine the uncertainty of the particle beam divergence σ_{PBD} the uncertainties of the particle beam widths at the first $\sigma_{\overline{PBW_{DL1}}}$ and second $\sigma_{\overline{PBW_{DL2}}}$ detection lasers are used.

$$\sigma_{PBD} = \sqrt{\left(\frac{\sigma_{\overline{PBW_{DL2}}}}{7}\right)^2 + \left(\frac{\sigma_{\overline{PBW_{DL1}}}}{7}\right)^2} \tag{S12}$$

Since measurements at one particle size were usually performed several times, the standard errors of the mean of the particle beam widths were used for these measurement points. The nominal distance of 7 cm between the two detection lasers is taken from Brands et al. (2011).

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