

Supplementary material

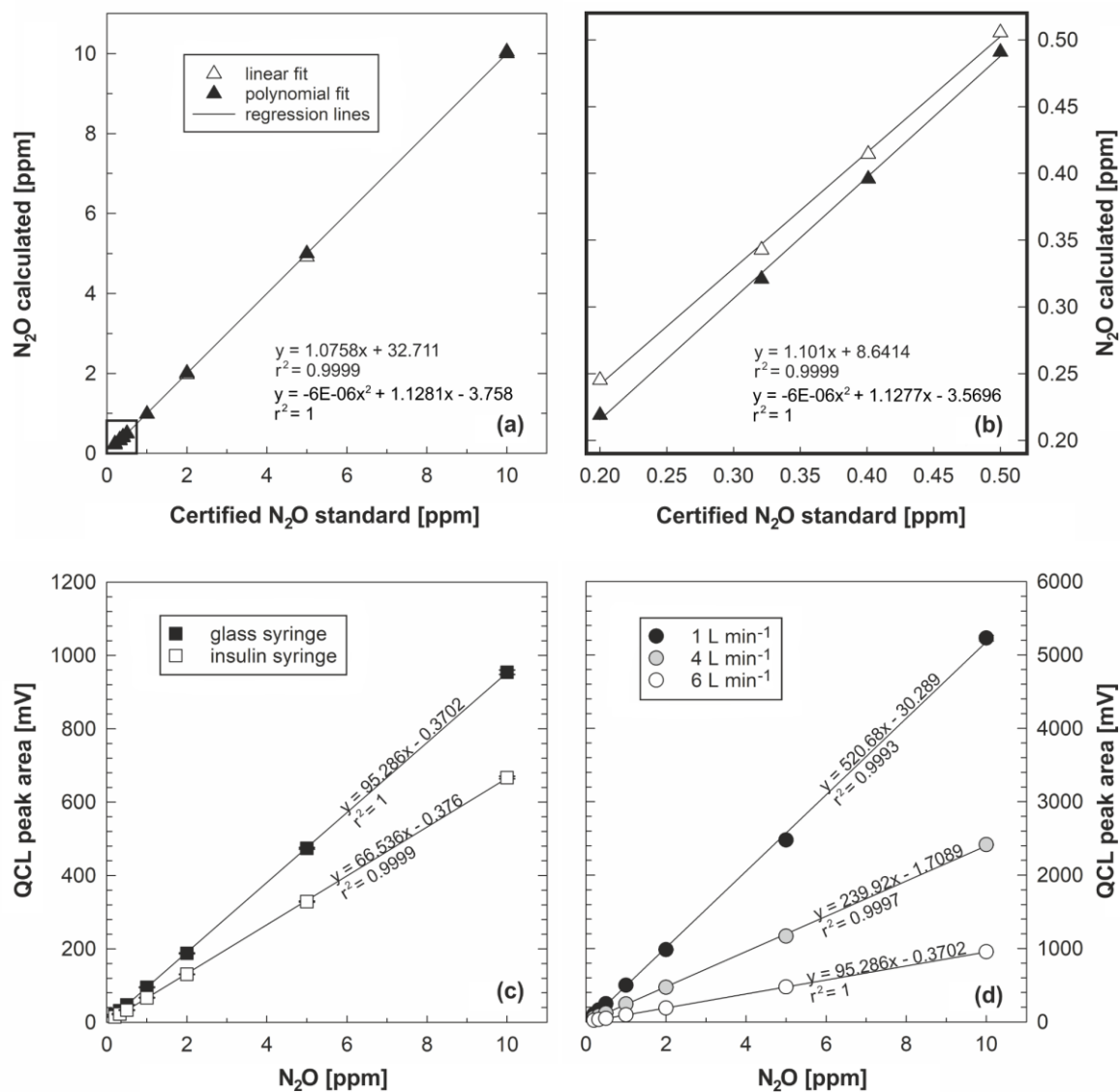


Figure S1: Tests conducted prior to the main study showing the calculated normal linear relationship between output peak area and N_2O concentration for different scenarios and for different ranges of N_2O standards injected (a) from 0.200 to 100 ppm and (b) from 0.200 to 5 ppm; regression lines in (c) illustrate the effect of using different syringe types on output peak area of the QCL; (d) demonstrates the effect of flow rate in $L\ min^{-1}$ on the slope of associated regression lines and output peak area.

Table S1: Chronology of experimental activities.

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| Date | Activity |
|-------------|---|
| 15-Aug-19 | Trial site fenced off Preliminary injection into QCL: testing different syringe types |
| 20-Aug-19 | Installation of chamber collars |
| 30-Aug-19 | Preliminary injections into QCL: testing different flow rates |
| 10-Sep-19 | Treatment application to chamber and soil plots Gas and soil sampling – run 1 |
| 11-Sep-19 | Gas and soil sampling – run 2 |
| 12-Sep-19 | Gas and soil sampling – run 3 & 4 |
| 13-Sep-19 | Gas and soil sampling – run 5 |
| 14-Sep-19 | Gas and soil sampling – run 6 |
| 15-Sep-19 | Gas and soil sampling – run 7 & 8 |
| 16-Sep-19 | Gas and soil sampling – run 9 |

15 **Table S2:** Certified N₂O standards used in this study and associated uncertainty levels. Certified N₂O standard concentrations printed in bold font were used in quadratic curve models to calculate final sample N₂O concentration.

| N₂O [μL L ⁻¹] [ppmv] | Uncertainty [alpha/beta] [%] | Background (gas) | Company (name) |
|--|---|----------------------------|--------------------------|
| 0.200 | ± 0.01 | Nitrogen | BOC Ltd. |
| 0.321 | ± 0.1–0.9% | Cryogenic UltraPure Air | Praxair, Inc. |
| 0.3252 | ± 0.01 | Air | NIWA |
| 0.401 | ± 0.1–0.9% | Cryogenic UltraPure Air | Praxair, Inc. |
| 0.500 | ± 0.01 | Nitrogen | BOC Ltd. |
| 1.00 | ± 0.01 | Nitrogen | BOC Ltd. |
| 2.00 | ± 0.02 | Nitrogen | BOC Ltd. |
| 5.00 | ± 0.1 | Nitrogen | BOC Ltd. |
| 10.00 | ± 0.2 | Nitrogen | BOC Ltd. |
| 20.00 | ± 0.2 | Nitrogen | BOC Ltd. |
| 50.00 | ± 1.0 | Nitrogen | BOC Ltd. |
| 100.00 | ± 1.0 | Nitrogen | BOC Ltd. |

Table S3: This table presents the measured values of nitrous oxide fluxes (F_{N_2O}) analysed by GC and QCL, soil water-filled pore space (WFPS), soil ammonium (NH_4^+) and nitrate (NO_3^-) content of the control (AN_0) and across the different treatments of ammonium-nitrate (AN_{300} , AN_{600} , AN_{900}) applied. The associated standard error of the mean (SEM) is provided at the right hand side of each control/treatment column.

| GC nitrous oxide flux [$F_{N_2O_GC}$ in $nmol\ N_2O\ m^{-2}\ s^{-1}$] | | | | | | | | |
|---|--------|------|------------|------|------------|-------|------------|-------|
| date | AN_0 | SEM | AN_{300} | SEM | AN_{600} | SEM | AN_{900} | SEM |
| 10-Sep-2019 | 0.04 | 0.05 | 3.56 | 1.20 | 1.95 | 0.19 | 2.49 | 0.52 |
| 11-Sep-2019 | 0.13 | 0.04 | 9.93 | 1.97 | 9.63 | 3.44 | 14.88 | 3.55 |
| 12-Sep-2019* | 0.06 | 0.05 | 8.67 | 1.73 | 8.02 | 2.92 | 15.87 | 3.96 |
| 12-Sep-2019* | 0.06 | 0.01 | 8.42 | 2.62 | 8.19 | 3.23 | 14.87 | 3.15 |
| 13-Sep-2019 | -0.05 | 0.03 | 6.43 | 3.00 | 11.57 | 3.68 | 15.16 | 3.76 |
| 14-Sep-2019 | 0.03 | 0.01 | 7.46 | 2.19 | 10.71 | 3.43 | 16.71 | 2.46 |
| 15-Sep-2019* | 0.02 | 0.03 | 5.03 | 0.80 | 10.21 | 2.84 | 14.85 | 3.58 |
| 15-Sep-2019* | 0.03 | 0.03 | 6.92 | 1.57 | 9.98 | 2.96 | 13.88 | 2.75 |
| 16-Sep-2019 | 0.02 | 0.04 | 3.06 | 1.33 | 6.37 | 2.45 | 10.29 | 1.67 |
| QCL nitrous oxide flux [$F_{N_2O_QCL}$ in $nmol\ N_2O\ m^{-2}\ s^{-1}$] | | | | | | | | |
| 10-Sep-2019 | 0.00 | 0.03 | 3.65 | 1.18 | 2.17 | 0.19 | 2.74 | 0.60 |
| 11-Sep-2019 | 0.21 | 0.05 | 9.40 | 1.83 | 8.88 | 3.14 | 13.57 | 3.04 |
| 12-Sep-2019* | 0.14 | 0.07 | 8.19 | 1.60 | 7.94 | 2.92 | 15.17 | 3.71 |
| 12-Sep-2019* | 0.06 | 0.02 | 8.02 | 2.47 | 8.04 | 3.11 | 15.46 | 3.57 |
| 13-Sep-2019 | 0.09 | 0.08 | 6.25 | 2.77 | 10.91 | 3.33 | 15.09 | 4.05 |
| 14-Sep-2019 | 0.03 | 0.02 | 7.30 | 2.10 | 10.66 | 3.24 | 17.22 | 2.71 |
| 15-Sep-2019* | 0.17 | 0.01 | 5.30 | 0.86 | 9.46 | 2.42 | 14.81 | 3.65 |
| 15-Sep-2019* | 0.18 | 0.03 | 6.95 | 1.33 | 10.27 | 2.89 | 14.36 | 2.69 |
| 16-Sep-2019 | 0.06 | 0.01 | 3.28 | 1.63 | 6.63 | 2.51 | 10.97 | 1.99 |
| Water filled pore space of the soil [%] | | | | | | | | |
| 10-Sep-2019 | 79.43 | 0.48 | 78.66 | 1.82 | 78.06 | 1.40 | 82.30 | 2.35 |
| 11-Sep-2019 | 81.64 | 0.59 | 84.97 | 1.68 | 80.16 | 0.53 | 82.13 | 1.79 |
| 12-Sep-2019 | 82.18 | 1.12 | 80.63 | 1.23 | 79.35 | 1.05 | 79.20 | 1.00 |
| 13-Sep-2019 | 79.62 | 0.95 | 79.72 | 1.87 | 76.62 | 2.08 | 78.13 | 1.76 |
| 14-Sep-2019 | 79.43 | 0.56 | 80.60 | 2.00 | 78.37 | 1.74 | 77.78 | 1.19 |
| 15-Sep-2019 | 79.79 | 0.50 | 81.70 | 2.65 | 77.17 | 1.49 | 76.81 | 0.37 |
| 16-Sep-2019 | 77.92 | 1.06 | 81.05 | 1.98 | 73.93 | 1.60 | 77.41 | 1.80 |
| Soil ammonium [$kg\ NH_4^+\ ha^{-1}$] | | | | | | | | |
| 10-Sep-2019 | 1.82 | 0.50 | 81.73 | 5.20 | 89.36 | 2.72 | 264.63 | 17.19 |
| 11-Sep-2019 | 0.81 | 0.11 | 52.26 | 7.18 | 141.51 | 11.08 | 233.63 | 33.62 |
| 12-Sep-2019 | 2.15 | 0.57 | 44.61 | 6.52 | 109.37 | 6.77 | 213.76 | 3.41 |
| 13-Sep-2019 | 2.21 | 0.33 | 36.88 | 6.75 | 124.48 | 9.36 | 194.76 | 18.88 |
| 14-Sep-2019 | 3.71 | 0.09 | 20.31 | 5.07 | 59.88 | 6.05 | 188.70 | 18.05 |
| 15-Sep-2019 | 1.84 | 0.64 | 9.58 | 0.99 | 78.98 | 12.30 | 155.84 | 18.49 |
| 16-Sep-2019 | 1.80 | 0.29 | 13.21 | 3.23 | 38.50 | 4.59 | 124.38 | 7.64 |

Soil nitrate [kg NO₃⁻ ha⁻¹]

| | | | | | | | | |
|-------------|------|------|-------|-------|--------|------|--------|-------|
| 10-Sep-2019 | 2.99 | 0.37 | 83.67 | 3.87 | 104.95 | 1.33 | 267.77 | 15.17 |
| 11-Sep-2019 | 2.46 | 0.18 | 69.08 | 6.54 | 149.95 | 8.62 | 248.89 | 33.69 |
| 12-Sep-2019 | 2.29 | 0.07 | 79.41 | 6.57 | 142.52 | 8.61 | 230.94 | 7.36 |
| 13-Sep-2019 | 1.64 | 0.20 | 82.21 | 7.92 | 149.85 | 6.25 | 232.40 | 13.77 |
| 14-Sep-2019 | 1.84 | 0.35 | 73.37 | 12.71 | 114.20 | 8.41 | 237.77 | 8.96 |
| 15-Sep-2019 | 2.47 | 0.31 | 78.91 | 1.51 | 162.60 | 8.72 | 231.51 | 16.94 |
| 16-Sep-2019 | 1.85 | 0.22 | 92.49 | 16.22 | 134.38 | 7.60 | 211.88 | 18.92 |

* flux measurements conducted twice daily at 10 AM and 12 PM

SEM = standard error of the mean

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55 **Table S4:** Results from the linear functional relationship analysis (orthogonal regression). Columns labelled C_{N2O} show results of the regression analysis when using standardised N₂O concentrations. Columns labelled F_{N2O} provide results based on standardised N₂O fluxes. Part of the regression analysis was to characterise both data streams by treatment and control, i.e. first including all data (AN₀, AN₃₀₀, AN₆₀₀, AN₉₀₀) in the analysis and then, separately, only the control (AN₀).

| | C _{N2O} all AN | C _{N2O} AN ₀ only | F _{N2O} all AN | F _{N2O} AN ₀ only |
|------------------------------------|----------------------------|--|----------------------------|--|
| Number of observations | 432 | 108 | 108 | 27 |
| Response mean | -0.003164 | 0.3272 | -0.004008 | 0.3776 |
| Explanatory mean | 0.003164 | -0.3272 | 0.004008 | -0.3776 |
| Response variance | 0.9811 | 1.238 | 0.9860 | 1.139 |
| Explanatory variance | 1.021 | 0.5551 | 1.023 | 0.6029 |
| r ² value | 0.9928 | 0.1753 | 0.9922 | 0.0939 |
| r value | 0.9964 | 0.4187 | 0.9961 | 0.3064 |
| Angle between Y on X and X on Y | 0.2068 | 42.32 | 0.2229 | 54.59 |
| Major eigenvalue | 1.999 | 1.384 | 2.005 | 1.241 |
| Minor eigenvalue | 0.003606 | 0.4096 | 0.003901 | 0.5017 |
| Bootstrap resampling | 200 | 200 | 200 | 200 |
| <i>Ordinary least squares:</i> | | | | |
| Constant | -0.006253 | 0.532 | -0.007926 | 0.537 |
| Standard error | 0.003914 | 0.1038 | 0.007861 | 0.26 |
| Lower | -0.01331 | 0.3101 | -0.02204 | -0.02 |
| Upper | 0.001710 | 0.734 | 0.006998 | 1.030 |
| Slope | 0.9766 | 0.625 | 0.9778 | 0.421 |
| <i>Inverse least squares:</i> | | | | |
| Constant | -0.006276 | 1.49 | -0.007957 | 2.072 |
| Standard error | 0.003902 | 0.6585 | 0.007902 | 82.46 |
| Lower | -0.01369 | 0.9211 | -0.02246 | -44.95 |
| Upper | 0.001786 | 3.478 | 0.007118 | 18.732 |
| Slope | 0.9837 | 3.567 | 0.9854 | 4.486 |
| <i>Major axis:</i> | | | | |
| Constant | -0.006264 | 1.108 | -0.007941 | 1.326 |
| Standard error | 0.003904 | 0.44 | 0.007872 | 40.17 |
| Lower | -0.01349 | 0.7105 | -0.02217 | -19.84 |
| Upper | 0.001610 | 2.484 | 0.006920 | 9.937 |
| Slope | 0.9801 | 2.387 | 0.9815 | 2.511 |

Table S5: Bland-Altman analysis for $F_{N_{2O_GC}}$ and $F_{N_{2O_QCL}}$ distinguished by treatment in units $\text{nmol m}^{-2} \text{s}^{-1}$, if not specified otherwise. This table provides a summary based on mean $F_{N_{2O_GC}}$ and $F_{N_{2O_QCL}}$ across replicates of the same treatment. Fig. 4, instead, illustrates the results of individual $F_{N_{2O_GC}}$ and $F_{N_{2O_QCL}}$ (not depicted in the below table) for each replicate and each treatment as the percentage mean difference between the two methods, i.e. GC (A) and QCL (B).

| Sampling | Treatment | GC (A) | QCL (B) | Mean | Difference | Difference (%) |
|-----------------|--------------------------|------------------|-------------------|-------------|-------------------|-----------------------|
| [No.] | [kg N ha ⁻¹] | $F_{N_{2O_GC}}$ | $F_{N_{2O_QCL}}$ | (A+B)/2 | (A-B) | ((A-B)/mean)*100 |
| 1 | 0 | 0.04 | 0.00 | 0.02 | 0.04 | 182.48 |
| 1 | 300 | 3.56 | 3.65 | 3.61 | -0.09 | -2.59 |
| 1 | 600 | 1.95 | 2.17 | 2.06 | -0.23 | -11.11 |
| 1 | 900 | 2.49 | 2.74 | 2.61 | -0.24 | -9.24 |
| 2 | 0 | 0.13 | 0.21 | 0.17 | -0.08 | -44.70 |
| 2 | 300 | 9.93 | 9.40 | 9.67 | 0.53 | 5.51 |
| 2 | 600 | 9.63 | 8.88 | 9.26 | 0.75 | 8.11 |
| 2 | 900 | 14.88 | 13.57 | 14.22 | 1.31 | 9.20 |
| 3 | 0 | 0.06 | 0.14 | 0.10 | -0.08 | -78.52 |
| 3 | 300 | 8.67 | 8.19 | 8.43 | 0.48 | 5.69 |
| 3 | 600 | 8.02 | 7.94 | 7.98 | 0.08 | 0.98 |
| 3 | 900 | 15.87 | 15.17 | 15.52 | 0.70 | 4.51 |
| 4 | 0 | 0.06 | 0.06 | 0.06 | 0.00 | 1.93 |
| 4 | 300 | 8.42 | 8.02 | 8.22 | 0.39 | 4.79 |
| 4 | 600 | 8.19 | 8.04 | 8.11 | 0.15 | 1.82 |
| 4 | 900 | 14.87 | 15.46 | 15.16 | -0.59 | -3.89 |
| 5 | 0 | -0.05 | 0.09 | 0.02 | -0.14 | -595.36 |
| 5 | 300 | 6.43 | 6.25 | 6.34 | 0.18 | 2.88 |
| 5 | 600 | 11.57 | 10.91 | 11.24 | 0.66 | 5.88 |
| 5 | 900 | 15.16 | 15.09 | 15.13 | 0.07 | 0.49 |
| 6 | 0 | 0.03 | 0.03 | 0.03 | 0.00 | 4.14 |
| 6 | 300 | 7.46 | 7.30 | 7.38 | 0.16 | 2.19 |
| 6 | 600 | 10.71 | 10.66 | 10.68 | 0.05 | 0.47 |
| 6 | 900 | 16.71 | 17.22 | 16.96 | -0.51 | -3.02 |
| 7 | 0 | 0.02 | 0.17 | 0.09 | -0.15 | -157.04 |
| 7 | 300 | 5.03 | 5.30 | 5.17 | -0.27 | -5.22 |
| 7 | 600 | 10.21 | 9.46 | 9.84 | 0.75 | 7.67 |
| 7 | 900 | 14.85 | 14.81 | 14.83 | 0.03 | 0.22 |
| 8 | 0 | 0.03 | 0.18 | 0.10 | -0.15 | -149.70 |
| 8 | 300 | 6.92 | 6.95 | 6.94 | -0.02 | -0.34 |
| 8 | 600 | 9.98 | 10.27 | 10.13 | -0.29 | -2.86 |
| 8 | 900 | 13.88 | 14.36 | 14.12 | -0.48 | -3.39 |

| | | | | | | |
|---|-----|-------|-------|-------|-------|---------|
| 9 | 0 | 0.02 | 0.06 | 0.04 | -0.04 | -105.26 |
| 9 | 300 | 3.06 | 3.28 | 3.17 | -0.22 | -6.86 |
| 9 | 600 | 6.37 | 6.63 | 6.50 | -0.26 | -4.02 |
| 9 | 900 | 10.29 | 10.97 | 10.63 | -0.68 | -6.39 |

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Table S6: Bioequivalence analysis for N₂O concentrations (C_{N2O}) and associated fluxes (F_{N2O}) in bottom panel of the table). C_{N2O_QCL} and F_{N2O_QCL} were considered bioequivalent when the 90% confidence interval of the difference was completely within the predefined $\pm 5\%$ bioequivalence range of difference to C_{N2O_GC} and F_{N2O_GC} (corresponding to a test with size 0.05). rep. = replicates, d.f = degrees of freedom, s.e.d = standard error of the difference, LSD = least significant difference

| Time/ Treatment | Mean | | Standard error of the difference of the mean | | LSD | 90% confidence interval | | Bioequivalence range | | | | | | |
|-------------------------|------------------------------|--|---|-----|--------|-------------------------|------------------------|----------------------|--------|-------------|-------------|--------------|--------------|-------|
| | C _{N2O_GC} [ppm] | C _{N2O_QCL} [ppm] | rep. | d.f | | s.e.d | difference (GC-QCL) | lower | upper | GC lower | GC upper | QCL lower | QCL upper | |
| AN₀ | t ₀ | 0.333 | 0.332 | 27 | 26 | 0.0027 | 0.0046 | 0.000 | -0.004 | 0.005 | -0.017 | 0.017 | -0.017 | 0.017 |
| | t ₁₅ | 0.333 | 0.342 | 27 | 26 | 0.0028 | 0.0048 | -0.009 | -0.013 | -0.004 | -0.017 | 0.017 | -0.017 | 0.017 |
| | t ₃₀ | 0.335 | 0.352 | 27 | 26 | 0.0029 | 0.0049 | -0.016 | -0.021 | -0.012 | -0.017 | 0.017 | -0.017 | 0.018 |
| | t ₄₅ | 0.340 | 0.354 | 27 | 26 | 0.0027 | 0.0046 | -0.014 | -0.019 | -0.009 | -0.017 | 0.017 | -0.017 | 0.018 |
| | AN₃₀₀ | 0.333 | 0.336 | 27 | 26 | 0.0028 | 0.0048 | -0.003 | -0.007 | 0.002 | -0.017 | 0.017 | -0.017 | 0.017 |
| AN₆₀₀ | t ₀ | 0.822 | 0.821 | 27 | 26 | 0.1090 | 0.0186 | 0.001 | -0.017 | 0.020 | -0.041 | 0.041 | -0.041 | 0.041 |
| | t ₁₅ | 1.341 | 1.327 | 27 | 26 | 0.0168 | 0.0286 | 0.014 | -0.015 | 0.042 | -0.067 | 0.067 | -0.066 | 0.066 |
| | t ₃₀ | 1.831 | 1.804 | 27 | 26 | 0.0192 | 0.0327 | 0.026 | -0.007 | 0.059 | -0.092 | 0.092 | -0.090 | 0.090 |
| | t ₄₅ | 0.336 | 0.335 | 27 | 26 | 0.0023 | 0.0042 | 0.001 | -0.003 | 0.005 | -0.017 | 0.017 | -0.017 | 0.017 |
| | AN₉₀₀ | 0.912 | 0.912 | 27 | 26 | 0.0160 | 0.0273 | 0.000 | -0.027 | 0.027 | -0.046 | 0.046 | -0.046 | 0.046 |
| Treatment | t ₀ | 1.563 | 1.550 | 27 | 26 | 0.0242 | 0.0412 | 0.013 | -0.028 | 0.054 | -0.078 | 0.078 | -0.078 | 0.078 |
| | t ₁₅ | 2.143 | 2.104 | 27 | 26 | 0.0250 | 0.0427 | 0.039 | -0.004 | 0.082 | -0.107 | 0.107 | -0.105 | 0.105 |
| | t ₃₀ | 0.338 | 0.337 | 27 | 26 | 0.0028 | 0.0319 | 0.001 | -0.004 | 0.005 | -0.017 | 0.017 | -0.017 | 0.017 |
| | t ₄₅ | 1.285 | 1.268 | 27 | 26 | 0.0136 | 0.1380 | 0.017 | -0.006 | 0.041 | -0.064 | 0.064 | -0.063 | 0.063 |
| | AN₃₀₀ | 2.338 | 2.294 | 27 | 26 | 0.0325 | 0.1959 | 0.044 | -0.012 | 0.100 | -0.117 | 0.117 | -0.115 | 0.115 |
| Treatment | t ₀ | 3.370 | 3.379 | 27 | 26 | 0.3900 | 0.2850 | -0.009 | -0.076 | 0.058 | -0.169 | 0.169 | -0.169 | 0.169 |
| | t ₁₅ | F _{N2O_GC} | F _{N2O_QCL} | | | | | | | | | | | |
| | t ₃₀ | [mmol N ₂ O m ⁻² s ⁻¹] | | | | | | | | | | | | |
| | t ₄₅ | 0.0387 | 0.1048 | 27 | 26 | 0.0187 | 0.0319 | -0.066 | -0.098 | -0.034 | -0.002 | 0.002 | -0.005 | 0.005 |
| | AN₃₀₀ | 6.610 | 6.483 | 27 | 26 | 0.0809 | 0.1380 | 0.127 | -0.011 | 0.265 | -0.331 | 0.331 | -0.324 | 0.324 |
| AN₆₀₀ | 8.514 | 8.329 | 27 | 26 | 0.1149 | 0.1959 | 0.185 | -0.011 | 0.381 | -0.426 | 0.426 | -0.416 | 0.416 | |
| | 13.222 | 13.265 | 27 | 26 | 0.1671 | 0.2850 | -0.043 | -0.328 | 0.242 | -0.661 | 0.661 | -0.663 | 0.663 | |