

Ozone Deposition to a Coastal Sea: Comparison of Eddy Covariance Observations with Reactive Air-Sea Exchange Models

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Abstract. A fast response (10 Hz) chemiluminescence detector for ozone (O₃) was used to determine O₃ fluxes using the eddy covariance technique at the Penlee Point Atmospheric Observatory (PPAO) on the south coast of the UK during April and May 2018. The median O₃ flux was -0.132 mg m⁻² h⁻¹ (0.018 ppbv m s⁻¹) corresponding to a deposition velocity of 0.037 cm s⁻¹ (interquartile range 0.017–0.065 cm s⁻¹) – similar to the higher values previously reported for open ocean flux measurements, but not as high as some other coastal results. We demonstrate that a typical single flux observation was above the 2σ limit of detection, but had considerable uncertainty. The median 2σ uncertainty of deposition velocity was 0.031 cm s⁻¹ for each 20-minute period, which reduces with the square root of the sample size. Eddy covariance footprint analysis of the site indicates that the flux footprint was predominantly over water (> 96%), varying with atmospheric stability and, to a lesser extent, with the tide. At very low wind speeds when the atmosphere was typically unstable, the observed ozone deposition velocity was elevated, most likely because the footprint contracted to include a greater land contribution in these conditions. At moderate-to-high wind speeds when atmospheric stability was near-neutral, the ozone deposition velocity increased with wind speed, and showed a linear dependence with friction velocity. This observed dependence on friction velocity (and therefore also wind speed) is consistent with the predictions from the one-layer model of Fairall et al. (2007), which parameterises the oceanic deposition of ozone from the fundamental conservation equation, accounting for both ocean turbulence and near-surface chemical destruction, while assuming that chemical O₃ destruction by iodide is distributed over depth. In contrast to our observations, the deposition velocity predicted by the recently developed two-layer model recently developed by Luhar et al. (2018) (which considers iodide reactivity in both layers, but with molecular diffusivity dominating over turbulent diffusivity assumes that the destruction of ozone by iodide occurs predominantly in the first layer), and that turbulence chemistry interaction is weak compared to transfer by turbulent mixing in the layer below. The Luhar et al. (2018) parameterisation shows no major dependence of deposition velocity on wind speed, in contrast to our

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observations, and underestimates the measured deposition velocities. These results call for further investigation into the mechanisms and control of oceanic O₃ deposition.

35 1 Introduction

Tropospheric ozone is important due to its considerable effects on human health (Medina-Ramón et al., 2006), agricultural yields (Heck et al., 1982) and global warming (Stevenson et al., 2013). Dry deposition is a major sink of tropospheric ozone, comprising as much as 25% of total loss from the troposphere (Ganzeveld et al., 2009; Lelieveld and Dentener, 2000; Pound et al., 2019). Deposition to the sea surface is the greatest source of uncertainty in global estimates of total ozone dry
40 deposition (Hardacre et al., 2015) due to deposition occurring at a slow and highly uncertain rate, but over a vast area. Ozone deposition flux is commonly parameterised according to Eq. (1) (Pacyna, 2008):

$$F = -v_d[O_3] \quad (1)$$

where F is flux in mol cm⁻² s⁻¹, v_d is deposition velocity in cm s⁻¹, and $[O_3]$ is ozone concentration in mol cm⁻³. In models, the deposition velocity is commonly calculated using a series of resistance terms, each defining barriers to deposition in
45 separate layers (Wesely and Hicks, 2000):

$$v_d = (R_a + R_b + R_c)^{-1} \quad (2)$$

R_a is the aerodynamic resistance, independent from the species being considered. R_b represents the resistance through the quasi-laminar thin layer of air in contact with a surface – this varies with the species' diffusivity. Lastly R_c is the surface resistance, which is typically the largest barrier to deposition for insoluble gases – roughly 95% of total resistance in the case
50 of ozone (Chang et al., 2004; Lenschow et al., 1982).

There are few reported observations of ozone deposition to the sea surface. Early work to determine oceanic O₃ deposition velocity was either laboratory-based (Garland et al, 1980; McKay et al., 1992) or used box enclosure loss rate experiments in the field (Aldaz, 1969; Galbally and Roy, 1980). Such experiments are valuable in determining surface resistance (describing the affinity of a surface for absorbing a given gas) for ozone deposition. However, these experiments are limited
55 in their ability to represent real-world physical processes such as turbulence at the air/sea interface. More recent flux measurements have been made with the eddy covariance method, which is the best way of observing fluxes in the atmospheric surface layer~~a system~~ without perturbing it. Eddy covariance measurements have been made from coastal towers (Gallagher et al., 2001; Whitehead et al., 2009; McVeigh et al., 2010), aircraft (Lenschow et al., 1982; Kawa and Pearson, 1989), and ships (Bariteau et al., 2010; Helmig et al., 2012). The deposition velocities reported in the few eddy
60 covariance observations over saltwater vary greatly: 0.01–0.15 cm s⁻¹, with windspeed dependencies evident in some measurements and not in others.

The reported eddy covariance measurements use two different techniques to measure ozone at high frequency, both utilising chemiluminescent reactions of ozone. In the instruments used for tower-based measurements (Gallagher et al., 2001; McVeigh et al., 2010; Whitehead et al., 2009), ozone is reacted with a coumarin-based dye on the surface of a silica gel disk.

65 Aircraft (Kawa and Pearson, 1989; Lenschow et al., 1982) and ship-borne (Bariteau et al., 2010; Helmig et al., 2012) instruments have instead utilised the reaction between ozone and gas phase nitric oxide.

Ozone deposition to the ocean depends both upon physical exchange, facilitated by diffusion and turbulence, and chemical reaction at the water-s surface (Chang et al., 2004; Fairall et al., 2007; Luhar et al., 2018). Iodide in sea water has been identified as a key reactant (Garland et al., 1980). There has been considerable recent progress in understanding the global distribution of oceanic surface iodide (Chance et al., 2014, 2019; Macdonald et al., 2014; Sherwen et al., 2019). However, there has only been one report of the dependence of the iodide – ozone rate constant with temperature (Magi et al., 1997), and this remains a considerable uncertainty in global models. Dissolved organic material (DOM) has been suggested to be of similar importance for ozone deposition as iodide (Martino et al., 2012; Shaw and Carpenter, 2013), especially given its enrichment in the sea surface microlayer (SML) (Zhou and Mopper, 1997). The complex and variable composition of DOM makes assessing its global reactivity with ozone a challenge.

Early work by Garland et al. (1980) formulated a description of ozone loss to sea water based on surface properties:

$$v_{dw} = \sqrt{aD} \quad (3)$$

where a is the reactivity of iodide with ozone, D is the diffusivity of ozone in water, and v_{dw} is the waterside deposition velocity, related to surface resistance (R_c) by

$$80 \quad R_c = \frac{1}{\alpha v_{dw}} \quad (4)$$

where α is the dimensionless solubility (liquid/gas) of ozone in water. This interpretation incorporates the chemical properties of the reaction, but neglects turbulent diffusion and underestimates the deposition velocity in cold water. Fairall et al. (2007) allowed deposition velocity to vary with oceanic turbulence by considering the O₃-iodide reaction beyond the molecular sublayer, obtaining the dependence:

$$85 \quad v_{dw} = \sqrt{aD} \frac{K_1(\xi_0)}{K_0(\xi_0)} \quad (5)$$

K_0 and K_1 are modified Bessel functions of the second kind, of order 0 and 1 respectively, and

$$\xi_0 = \frac{2}{\kappa u_{*w}} \sqrt{aD} \quad (6)$$

where κ is the von Kármán constant (~0.4) and u_{*w} is the waterside friction velocity. This is sometimes referred to as a one-layer model, due to the assumption that reactivity is uniform with depth. This one-layer approach has been reported to match observations better than a using a fixed surface resistance term, but overestimates deposition velocity by a factor of 2-3 in colder waters where the rate of reaction between ozone and iodide is slower.

An alternative, two-layer scheme is explored by Fairall et al. (2007) and expanded upon by Luhar et al. (2017). The authors consider an enhancement in reactivity in a very thin layer (reaction-diffusion sublayer) at the surface, while the water beneath has only very minor background reactivity. In a revision of the two-layer scheme, Luhar et al. (2018) assumed turbulent transfer to be negligible compared with chemical removal of ozone within the reaction-diffusion sublayer, but with both turbulence and chemistry accounted for in the layer beneath, defining the waterside deposition velocity:

$$v_{dw} = \sqrt{aD} \frac{[\psi K_1(\xi_\delta) \cosh(\lambda) + \psi K_0(\xi_\delta) \sinh(\lambda)]}{[\psi K_1(\xi_\delta) \sinh(\lambda) + \psi K_0(\xi_\delta) \cosh(\lambda)]} \quad (7)$$

The terms ψ , ξ_δ and λ in Eq. (7) all vary according to the reaction-diffusion sublayer depth, δ_m :

$$\psi = \sqrt{1 + \frac{\kappa u_* \delta_m}{D}} \quad (8)$$

$$100 \quad \xi_\delta = \sqrt{\frac{4a}{\kappa u_*} \left(\delta_m + \frac{D}{\kappa u_*} \right)} \quad (9)$$

$$\lambda = \delta_m \sqrt{\frac{a}{D}} \quad (10)$$

Eqs. (7-10) describe the two-layer scheme that will be discussed in this work. The method of assigning a value to δ_m is discussed by Luhar et al. (2018), who found that a fixed depth of 3 μm was a good fit to the data of Helmig et al. (2012). When a variable reaction-diffusion sublayer depth was considered as proportional to the reaction-diffusion length scale
105 ($l_m = \sqrt{D/a}$), Luhar et al. (2018) found it necessary to multiply l_m by a factor of 0.7 to obtain a δ_m value that fitted reasonably with observations. Pound et al. (2019) were however able to obtain a good fit to observational data without this factor by using the oceanic iodide parameterisation of Sherwen et al. (2019) in place of that of Macdonald et al. (2014). Pound et al. (2019), define the reaction-diffusion layer depth according to Eq. (11).

$$\delta_m = \sqrt{\frac{D}{a}} \quad (11)$$

110 The dependence of deposition velocity with wind speed (or friction velocity, u_* , which scales linearly with wind speed over the ocean) within ~~these the~~ Fairall et al. (2007) and Luhar et al. (2018) models is markedly different, and it is not clear which is a better fit to existing observations. The deposition velocity estimated by the one-layer model of Fairall et al. (2007), increases linearly with friction velocity and compares favourably with the TexAQS06 and GOMECC07 cruises (Helmig et al., 2012). However, observations made during other cruises discussed by Helmig et al. (2012) show no dependence on
115 friction velocity. The two-layer model of Luhar et al. (2018) predicts almost no influence of friction velocity on deposition velocity, except at very low ($< 2 \text{ m s}^{-1}$) wind speeds.

Better characterisation of the effects of wind speed and ~~the chemical composition of the surface water~~ sea surface composition on ozone deposition velocity to the sea surface would significantly improve our understanding of the global tropospheric O_3 budget (Ganzeveld et al., 2009; Pound et al., 2019). Here we present coastal ozone flux measurements made
120 at Penlee Point Atmospheric Observatory (PPAO; <https://www.westernchannelobservatory.org.uk/penlee/>) on the southwest coast of the UK using a fast response gas phase chemiluminescence detector (CLD). Factors affecting the variation and uncertainty in the observed deposition velocity are discussed, including the effects of changing relative contributions from sea and land within the flux footprint.

2 Materials and methods

125 2.1 Measurement location

The PPAO is situated on a headland just south-west of Plymouth, UK (50° 19.08' N, 4° 11.35' W). The observatory is located 11 m a.m.s.l. with an extendable mast on the roof. It lies 30–60 m away from the sea, depending on tide, with the intervening land predominantly bare rock with some grass immediately surrounding the tower. For the work presented here, the top of the tower was extended to 19 m a.m.s.l. The dominant wind directions are from the south-west, followed by the north-east (Figure 1). The focus of this work is the south-west (180–240°) wind sector, which brings in air from the Atlantic Ocean and English Channel to the site (Yang et al., 2016).

2.2 Experimental set-up

The ozone chemiluminescence detector was adapted from an Eco Physics® CLD 886 NO_x detector, working on the same principle as the instrument used by Helmig et al. (2012). A supply of excess NO is introduced to the sample, which reacts with O₃ to generate NO₂ in an excited state. The relaxation process leads to emission of a photon that is amplified and detected using a photomultiplier tube (PMT). In order to maintain a low number of dark counts, the PMT is cooled to -5°C by a Peltier cooler. Clean dry air is continuously pumped over the PMT to avoid the build-up of water (Figure 2).

Sample air was drawn from the top of the tower through ~10 m of 3/8'' PFA tubing by a vacuum pump at 13.5 ~~min⁻¹SLPM~~ min⁻¹SLPM. This maintained a turbulent flow in the main sampling line (Reynolds number ~3000). A flow of 300 mL min⁻¹ was drawn from this sample manifold-line through 1/8'' PFA tubing and into the analyser using an internal vacuum pump (Figure 2), limited by a critical orifice. Before entering the analyser, the sample air was first passed through a dryer consisting of 60 cm of Nafion™ tubing coiled in a container of desiccant (indicating Drierite) to reduce humidity. A three-way solenoid valve allowed for a sample of indoor air passed through a charcoal filter to remove O₃ to record an instrument zero. A 50 mL min⁻¹ flow of 2% NO in N₂ was supplied separately to the analyser at a pressure of 4 bar through approximately 1.5 m of 1/8'' PFA tubing. The NO and O₃ were then mixed immediately before the reaction chamber (at ~26 mbar pressure) and the resulting chemiluminescence detected by the PMT.

The CLD counts were logged at 10 Hz and converted into ozone mixing ratios using the signal from a co-located, recently calibrated 2B model 205 dual beam ozone monitor. The CLD sensitivity was determined to be 240 counts s⁻¹ ppbv⁻¹ and showed no obvious dependence on ambient humidity (Figure S1) providing evidence for the efficacy of the dryer. Instrument dark counts were 480±40 count s⁻¹, leading to a 10 Hz signal-to-noise ratio of 33 for the average 46 ppbv O₃ measured during this work.

Three-dimensional wind data were obtained from a Gill WindMaster Pro 3D sonic anemometer at 10 Hz. Humidity, air pressure and temperature data were logged at 0.25 Hz from a Gill MetPak Pro. Vertical wind data were adjusted by +16.6% and +28.9% in magnitude for positive and negative values, respectively, in line with the corrections recommended for a reported firmware bug in the Gill WindMaster instruments: (http://gillinstruments.com/data/manuals/KN1509_WindMaster_WBug_info.pdf).

2.3 Pre-flux processing

The eddy covariance method (EC) relies on the simultaneous measurement of vertical wind speed (w) and the relevant scalar (in this case, ozone dry mixing ratio). These values were determined at 10 Hz in order to resolve the full range of eddies responsible for vertical ozone transport. It is necessary to ~~calculate eddy covariance fluxes average data~~ over a suitable ~~averaging interval period~~ to reduce random noise and capture transport from large eddies, whilst avoiding too long a period such that non-turbulent transport and non-stationarity become more important. An averaging time of around 30 minutes is often recommended (Foken, 2008). Previous measurements of O₃ flux have used ~~averaging period~~~~averaging interval~~s from 10 minutes (Helmig et al., 2012) to 1 hour (Gallagher et al., 2001), and a 20-minute period was chosen for this work. Prior to the flux calculation, data were despiked using a median filter despiking method (Brock, 1986; Starckenburg et al., 2016) using an order of $N = 4$ (9 points in a window). This involves binning the differences from the normalised data into exponentially more bins until bins exist within the range of the histogram that have zero values. Difference values beyond these empty bins are then identified as spikes and removed. For the flux calculation, data were linearly detrended to determine deviation from the mean within the ~~averaging period~~~~averaging interval~~. A double rotation was applied to the wind data in each ~~averaging period~~~~averaging interval~~ to align the u axis with the mean wind and remove any tilt in the wind vector, resulting in a mean vertical wind of zero. A planar fit method (Wilczak et al., 2001) was considered as an alternative to double rotation, but a single set of planar fit coordinates was found to be inappropriate for the Penlee site. Instead, an approach defining separate planar fit coefficients for each 10° sector (e.g. Mammarella et al., 2007; Yuan et al., 2011) was used, resulting in a median 7% increase in flux compared with the double rotation method. This sector-wise approach does, however, introduce discontinuous adjustments at the boundaries of the somewhat arbitrarily chosen sectors. A possible solution is to define the tilt angle as a continuous function of the wind direction (Ross and Grant, 2015), but given the minor difference between the fluxes resulting from the sector planar fit and double rotation methods, the latter was chosen for this work.

Due to the Nafion™ dryer and the fixed temperature and pressure of the reaction chamber, density corrections known as WPL corrections (Webb et al., 1980) were unnecessary for determining an accurate ozone mixing ratio. However, the presence of water vapour was taken into account for the determination of ancillary parameters such as the Obukhov length used in footprint modelling. It should be noted that in addition to its effect on mixing ratio, water vapour also quenches the chemiluminescence of the reaction of NO with O₃. This can be dealt with either by determining the instrument sensitivity over a range of water vapour conditions (at the cost of some sensitivity) and applying a correction, or by sufficiently drying the sample air. The latter approach was taken here. Despite a range of humidity (2.8×10^{-5} – 1.8×10^{-2} mol/mol, Figure S1) over the 42-day observation period, the two instruments compare well when using a fixed sensitivity for the CLD. The sensitivity value of 240 ppbv s⁻¹ also compares favourably to 213 ppbv s⁻¹, which was estimated using a supply of known ozone in the absence of water vapour (supplied from a calibrated Thermo model 49i-PS ozone primary standard) during lab tests prior to deployment. These results suggest that the dryer removed any major water vapour effect on the detection of ozone concentration and flux.

190 The sample air must travel –to the detector through the inlet tubing, which introduces a time lag relative to the
instantaneously measured wind data. The two datasets must therefore be realigned in order to calculate the covariance. A
cross-correlation function (CCF) was calculated at different time lags, with a high-pass Butterworth filter applied to the input
values. The presence of a negative peak in the resulting CCF spectrum indicated a strong anticorrelation between ozone
concentration and vertical wind, characteristic of deposition. Individual CCF plots were noisy, and gave scattered lag values,
195 with a high density around 4 seconds. Daily average CCF plots indicated clear peaks in all but one case and drifted from 3.9
to 4.1 seconds over the course of the experiment (e.g. Figure 3). This is likely a consequence of slight particulate build-up in
the sample line filters over the course of the measurements. Individual 20-minute flux interval lags were accepted if they fell
between 3.5 and 4.5 seconds to allow for some variability in conditions (e.g. atmospheric pressure), vacuum pump strength
etc. Lags that fell outside of these boundaries were then set to a value determined by a linear fit of the accepted data (Figure
200 S2). Simply setting the lag to 4 seconds in all instances was found to decrease the flux by 5% relative to the method used
here (CCF lag determination maximises the flux magnitude). The expected lag was also estimated from the inlet setup: a
13.5 L min⁻¹ flow rate through 10 m of 3/8” tubing plus a 300 mL min⁻¹ sample flow through 2 m of 1/8” tubing yields a
calculated lag of 4.2 seconds, similar to the CCF-determined values.

Following these steps, the ozone flux was calculated on a 20-minute basis using eddy4R (Metzger et al., 2017) with a
205 ~~modified~~ workflow customised for our measurements. Flux values were then used to determine the deposition velocity
according to Eq. (1). The mMolar flux was calculated using the instantaneous vertical wind, ozone mixing ratio and density
of dry air. Similarly, the ozone concentration used in Eq. (1) was calculated for dry air using the mean ozone mixing ratio for
the ~~averaging period~~averaging interval to avoid introducing a dependence on water vapour to the deposition velocity.

2.4 Data selection

210 A series of selection criteria were applied to the calculated 20-minute flux data. Firstly, periods with more than 10% missing
data were excluded. Missing data were most commonly caused by periods of maintenance, or when heavy rain disrupted the
sonic anemometer readings. Data were also selected by wind direction – only data between the true wind direction of 180°
and 240° were accepted to avoid observing deposition on the headland to the north-west.

A selection criterion based on ozone variation, as used by Bariteau et al. (2010), was introduced to avoid periods of non-
215 stationarity i.e. significantly different conditions within an ~~averaging period~~averaging interval (such as a sudden change in
the air mass passing by the sensor, or a change in wind direction). Data were excluded if the ozone concentration drifted
significantly (> 6 ppbv in 20 minutes) or if the standard deviation in ozone was above 2 ppbv. Data with a standard deviation
in wind direction of > 10° were also removed to avoid non-stationarity of wind, as performed by Yang et al. (2016) for the
same site.

220 Flux footprint analysis was used to investigate the potential for land influence within the footprint area. Land influence may
increase as the footprint contracts during the unstable conditions coinciding most frequently with low wind speeds. Using the

flux footprint parameterisation of Kljun et al. (2015), footprints were calculated for each ~~averaging period~~averaging interval. These were defined using tide-adjusted measurement height, roughness length, friction velocity, wind speed (and direction), crosswind variability, and stability conditions, then aggregated into 1 m s⁻¹ wind speed bins. Using these aggregated
 225 footprints, the percentage of land area contribution in the footprint area was estimated to increase from 1–2% at high wind speeds, when atmospheric stability was predominantly neutral, to 15% at winds below 2 m s⁻¹ when the atmosphere was generally unstable (Figure 4). It should be noted that the footprint model is designed for flat homogeneous terrain – not a heterogeneous coastal site. This will therefore introduce some additional uncertainty to footprint extent and land coverage beyond that inherent to the parameterisation.

230 Roughness lengths (z_0), derived from eddy covariance measurements using the logarithmic wind profile and Eqs. (12–15), were also elevated at low wind speeds (Figure 5).

$$z_0 = z / e^{\left(\frac{\kappa U}{u_*} \Psi_m\left(\frac{z}{L}\right)\right)} \quad (12)$$

Where z_0 is roughness length in m, z is measurement height in m, κ is the von Kármán constant, U is wind speed in m s⁻¹, u_* is friction velocity in m s⁻¹ (determined directly from the covariance of the fluctuations of horizontal and vertical wind
 235 components), and $\Psi_m\left(\frac{z}{L}\right)$ is the integral of the universal function (with dimensionless Obukhov stability z/L calculated from observed heat flux and u_*), defined as (Businger et al., 1971; Högström, 1988):

$$\Psi_m\left(\frac{z}{L}\right) = -6\frac{z}{L} \quad \text{for } \frac{z}{L} \geq 0 \quad (13)$$

$$\Psi_m\left(\frac{z}{L}\right) = \ln\left[\left(\frac{1+x^2}{2}\right)\left(\frac{1+x}{2}\right)^2\right] - 2\tan^{-1}x + \frac{\pi}{2} \quad \text{for } \frac{z}{L} < 0 \quad (14)$$

where

$$240 \quad x = \left(1 - 19.3\frac{z}{L}\right)^{1/4} \quad (15)$$

Roughness lengths at high wind speeds are scattered approximately around 0.0002 m, which is expected for an open sea fetch (World Meteorological Organisation, 2008), but a large increase can be seen at wind speeds < 3 m s⁻¹ (Figure 5). Roughness length can be slightly higher during very low wind speed, low u_* conditions (Vickers and Mahrt, 2006). However the scale of the increase at the PPAO is indicative of a surface with more roughness elements, such as the rocks and grass
 245 found on the headland. Greater inaccuracies in the double rotation method at low wind speeds can mean that the removal of horizontal wind from the rotated vertical component is incomplete, further contributing to the elevated surface roughness values. Additionally, higher deposition velocities were observed during periods of very low winds, contrasting with the trend of increasing deposition velocity with wind speed proposed by Chang et al. (2004) and observed during open ocean cruises by Helmig et al. (2012). Yang et al. (2016, 2019) observed a similar enhancement in CO₂ transfer at low wind
 250 speeds, and chose to filter out low wind speed data. The above discussion indicates the need for a filter to exclude land-

influenced flux data. A wind speed filter of $> 3 \text{ m s}^{-1}$ was used in this work where median fluxes and deposition velocities are reported for the whole dataset (or model work), though filters on the basis of z_0 could also be used to similar effect.

Previous eddy covariance work on CO_2 flux over land has applied filters on the basis of friction velocity (e.g. Barr et al., (2013)) to avoid underestimation of flux during periods of poorly developed turbulence, especially at night (Aubinet, 2008).

255 However past measurements of oceanic ozone deposition velocity have not reported using such a filter (Gallagher et al., 2001; Helmig et al., 2012; McVeigh et al., 2010) because very low wind speeds and u_* are uncommon over the ocean. For our data, removing data with $u_* < 0.1 \text{ cm s}^{-1}$ in addition to the criteria in Table 1 made no difference to the observed median deposition velocity. Therefore, given that a wind speed filter was already applied, no additional friction velocity filter was included.

260 Longer ~~averaging period~~averaging intervals than 20-minutes were also considered, but 60-minute averaging caused a large loss of data to the selection criteria. Missing data, as well as non-stationarity of wind and ozone contributed to an overall 23% reduction in total data accepted when using 60-minute averaging compared with 20-minute averaging. This shorter averaging time was therefore retained.

2.5 Flux uncertainty

265 Flux uncertainty can be estimated in a number of ways, and in this work we make use of an empirical method (Langford et al., 2015; based on Wienhold, 1995) and a theoretical method (Fairall et al., 2000). In the method of (Langford et al., 2015), cross-correlation functions (discussed in Sect. 2.3) are calculated at a series of improbable lag times (150–180 seconds) for each ~~averaging period~~averaging interval, and the root mean squared deviation of these values is taken to be representative of the random error of the flux measurement. Alternatively, the theoretical estimation of flux uncertainty of Fairall et al. (2000)
270 can be made according to the expression:

$$\Delta F_X = \Delta \overline{w'X'} \approx \frac{\sigma_w \sigma_X}{\sqrt{T/\tau_{wca}}} \quad (16)$$

where ΔF_X is flux uncertainty, w' is instantaneous vertical wind velocity fluctuation, X' is instantaneous ozone fluctuation, σ_w is the standard deviation in vertical wind velocity, σ_X is the standard deviation in ozone concentration, T is length of the ~~averaging period~~averaging interval in seconds, and τ_{wca} is the integral timescale for the instantaneous covariance time series
275 $w'X'$. A factor with a value of 1–2 is sometimes also included in the numerator of Eq. (16) to reflect uncertainty in this relationship (Blomquist et al., 2010). A factor of 1 is used in this work. The integral timescale τ_{wca} can either be determined from a flux co-spectrum peak frequency:

$$\tau_{wca} = \frac{1}{2\pi f_{max}} \quad (17)$$

or empirically according to:

280 $\tau_{wca} = \frac{bz}{U}$ (18)

where z is measurement height in meters, U is mean wind speed, and b is a value that varies with atmospheric stability. The value of b has been reported variably as 0.3–3 for near neutral conditions (Blomquist et al., 2010; Lenschow and Kristensen, 1985) and on the order of 10–12 for convective/unstable conditions (Blomquist et al., 2010; Fairall, 1984). The application of these methods to our data is discussed further in Sect. 3.5.

285 **3 Results**

3.1 Flux and deposition velocity values

From April 10th to May 21st, 2018, the median O₃ deposition velocity was 0.037 cm s⁻¹ (interquartile range 0.017–0.063 cm s⁻¹) with a median mass flux of -0.132 mg m⁻² h⁻¹ and a median ozone concentration of 48 ppbv (Figure 6). The resulting distribution of v_d values was compared to that obtained with the lag time set to 180s, and was significantly different from the results of the disjointed data (Kolmogorov-Smirnov test, $p < 0.001$; Figure S3), rejecting the null hypothesis that the two sets of values could be taken by chance from the same distribution. This confirms that the experimental set-up used here has a sufficiently low limit of detection to discern the flux from noise over the whole duration of the measurements. The 2 σ flux uncertainty was determined for each 20-minute period (see Sect. 3.5), with a median uncertainty of 0.113 mg m⁻² h⁻¹, corresponding to a deposition velocity uncertainty of 0.031 cm s⁻¹. A typical single flux observation is therefore above the 290 2 σ limit of detection, albeit with considerable uncertainty, although this uncertainty reduces with the square root of the sample size where averaged results are presented.

Previous eddy covariance ozone deposition velocity measurements have yielded values of 0.009–0.034 cm s⁻¹ over five open ocean cruises (Helmig et al., 2012) with higher values typically corresponding to warmer oceans. Additionally, tower-based measurements have reported deposition velocities at coastal locations to be 0.025 cm s⁻¹ (McVeigh et al., 2010), 0.030 cm s⁻¹ (Whitehead et al., 2009) and 0.13 cm s⁻¹ (Gallagher et al., 2001). These measurements were carried out at Mace Head (west Ireland), Weybourne (east UK) and Roscoff (north-west France) respectively. Our median v_d of 0.037 cm s⁻¹ is towards the upper end of previous work, though much lower than Gallagher et al. (2001). 300

3.2 Wind speed dependence

Reports on the dependence of v_d on wind speed and friction velocity (u_*) have varied considerably; the cruise observations discussed by Helmig et al. (2012) vary from strong to zero dependence, while both McVeigh et al. (2010) and Gallagher et al. (2001) observed tentative relationships. We examine this relationship for our data in Figure 8. Individual values that passed the filtering criteria exhibited a large degree of scatter, and are therefore presented alongside median values within wind speed bins of 1 m s⁻¹. Note that v_d values removed by the wind speed filter (Sect. 2.4) are shown in the shaded region 305

of Figure 8 and demonstrate the elevated v_d at low wind speeds. Outside of the excluded low wind speed region, v_d values are relatively constant up to 10 m s^{-1} . Above 10 m s^{-1} , v_d begins to increase, though data are sparse above 14 m s^{-1} .

The wind speed dependency of v_d has been discussed in a number of other studies. Chang et al. (2004) reported a five-fold increase in v_d ($0.0158\text{--}0.0775 \text{ cm s}^{-1}$) from 0 to 20 m s^{-1} , with v_d near constant below 4 m s^{-1} , and approximately doubling from $4\text{--}10 \text{ m s}^{-1}$. Tower-based eddy covariance measurements by Gallagher et al. (2001) exhibited increasing ozone deposition velocity as wind speed increases, with v_d tripling over the range $u_* = 0.05\text{--}0.5 \text{ m s}^{-1}$. Using the same type of instrument, McVeigh et al. (2010) reported a similar trend, fitting an exponential curve to their data. Lastly, deposition velocity during two of the five cruises reported by Helmig et al. (2012) increased with increasing wind speeds. The dependence observed in our data is discussed further in Sect. 4.2.

3.3 Land influence

Aggregate flux footprint analysis of the PPAO site (as discussed in Sect. 2.4) shown in Figure 9, suggests that the spatial contribution of land surfaces to our observed deposition velocity is approximately 3.9% (Figure 9). However, deposition velocity to land is typically greater than to the ocean, amplifying the potential influence of land deposition on our data. If our observations were adjusted for 3.9% spatial contribution of grassland ($v_d \approx 0.25 \text{ cm s}^{-1}$, median land deposition value from datasets analysed by Hardacre et al., (2015)), then our calculated median coastal water v_d would be 0.028 cm s^{-1} (23% lower than we measured). In reality the terrain is a mixture of grassland and rocky shoreline, varying in extent with the tide, so the land v_d discussed above may be an overestimate. It should also be noted that the grassland deposition velocity value used here is itself prone to considerable uncertainty due to the variability of the datasets used in the model. Although there are insufficient data over the land to the north-west to reliably determine a v_d value to the land around the PPAO, an estimate can be made by obtaining a least square solution using the land cover determined in Figure 4 and the observed v_d values in Figure 8. Data from wind speeds $> 14 \text{ m s}^{-1}$ were not used (only 4 data points). Using all data from $2\text{--}13 \text{ m s}^{-1}$ yielded values of $0.167 \pm 0.080 \text{ cm s}^{-1}$ and $0.034 \pm 0.016 \text{ cm s}^{-1}$ for land and sea respectively, suggesting a lesser effect from land than using the fixed value from Hardacre et al. (2015). Given that the land contribution in Figure 4 doesn't stabilise until 9 m s^{-1} , it is possible that constant v_d between 4 and 10 m s^{-1} wind speeds (Figure 8) may be a consequence of land influence and wind speed enhancement counteracting one another. Estimated water-only v_d values, calculated by subtracting the product of the land fraction and the land v_d value from the measured v_d , are shown in Figure 10.

It is worth reiterating that the Kljun footprint model is designed for use in homogenous environments, which is not the case for our site. Furthermore, the double rotation applied to the wind data will result in varying pitch angles relative to the water surface, introducing a dependence of the footprint extent on this pitch angle. These limitations may be important for work relying on direct interpretations of the flux footprint, such as comparisons to emissions inventories (Squires et al., 2020; Vaughan et al., 2017). In contrast to an inventory comparison, we only use the flux footprint model to develop a strategy for robust data selection, and generate an aggregate footprint from several individual footprints. This approach follows the

works of Amiro (1998), Göckede et al. (2006, 2008); Kirby et al. (2008), Metzger (2018) and Xu et al. (2018) who have demonstrated the utility of aggregation for deriving robust footprint-based metrics in heterogeneous environments.

3.4 Tidal influence

The PPAO site flux footprint also experiences periodic variations associated with the tide, which alters the effective measurement height and changes the land type in the footprint when the shoreline is exposed. Whitehead et al. (2009) provide an extreme example of this, reporting v_d increasing from 0.030 cm s^{-1} at high tide to 0.21 cm s^{-1} at low tide during the day. This large variation in their work was a consequence of a 9 m tidal range exposing the sea floor up to 3 km from the shore. At Penlee, the tide also causes periodic movement of the river plume around the headland, altering the salinity and composition of the surface water (Yang et al., 2016). This altered composition could affect the reactivity of ozone at the sea surface. Such effects will be examined in future work. Tower height above the water was determined for all flux calculations using tidal data from the British Oceanographic Data Centre (BODC), measured approximately 6 km upstream. Periodograms were also used to look for periodic variation in deposition velocity from exposed shoreline or riverine water, but none could be identified above the variability in the data. We note that previous measurements of air-sea exchange of momentum (Yang et al., 2016a), CO_2 (Yang et al., 2019a) and sea spray (Yang et al., 2019b) at the PPAO were also unable to identify tidal cycles in the data. Gallagher et al. (2001) report a tentative (though statistically insignificant) diurnal cycle for coastal water during observations made at Weybourne in East Anglia, UK. However, no diurnal variability was observed in the PPAO O_3 flux data (as might be expected due to deposition to land), again implying minimal land influence in our filtered observations.

3.5 Measurement uncertainty

To understand the variability in our v_d observations, a flux limit of detection was obtained empirically according to the method of Langford et al. (2015) (Sect. 2.5). Limits of detection were calculated for each ~~averaging period~~ averaging interval due to its dependence on wind speed and atmospheric stability, giving a median 2σ flux limit of detection of $0.113 \text{ mg m}^{-2} \text{ h}^{-1}$. At the average ozone concentration of 48 ppbv, this equates to a deposition velocity of 0.031 cm s^{-1} , with 305 of the 491 ~~averaging period~~ averaging intervals exceeding their individually determined 2σ limit of detection.

To determine a theoretical uncertainty using Eq. (16), the peak frequency of the co-spectrum shown in Figure 11 (0.07 Hz), was used to determine τ_{wca} as approximately 2.2 s during near-neutral conditions and wind speeds of 12.1 m s^{-1} . Using Eq. (17) and Eq. (18), this corresponds to a value for b of 1.5, similar to the literature values for near neutral conditions (Blomquist et al., 2010; Lenschow and Kristensen, 1985). Since individual 20-minute co-spectra were too noisy, this b value was used with Eq. (18) to determine τ_{wca} for each 20-minute period. It should be noted that the value of b is stability dependent. However, since stability was near neutral for most periods ($z/L = -0.39$ to 0.15 , 20th–80th percentile), the effects of varying stability on b are expected to be small.

Using these integral timescales, a theoretical flux uncertainty can be calculated for each ~~averaging period~~averaging interval using Eq. (16). The theoretical values obtained were much higher than those found empirically – the median theoretical 2σ limit of detection was $0.241 \text{ mg m}^{-2} \text{ h}^{-1}$ compared with the empirical value of $0.113 \text{ mg m}^{-2} \text{ h}^{-1}$. We note however that this is an approximation, derived from the work of Lenschow & Kristensen (1985) who multiplied the right-hand side of Eq. (16) by 2 to derive an upper limit on flux uncertainty.

Equation (16) demonstrates how the variability of ozone and vertical wind within averaging intervals are directly related to uncertainty in the measured flux. White noise in the wind measurement is expected to be very small, whereas random noise in the ozone instrument likely represents a significant contribution to the total variance of ozone observed at 10 Hz. Given the relatively low sensitivity of the instrument used in this work ($240 \text{ counts ppbv}^{-1} \text{ s}^{-1}$ compared to $2800 \text{ counts ppbv}^{-1} \text{ s}^{-1}$ reported by Helmig et al. (2012)), autocovariances were calculated for each ~~averaging period~~averaging interval using the 10 Hz ozone data to examine the extent to which variance in ozone concentration is caused by instrument white noise. White noise only correlates with itself at zero lag time, so it can be estimated from the difference between the first and second points in an autocovariance plot (Blomquist et al., 2010). Instrument white noise derived using this approach was found to contribute 45–98% to the total ozone variance (10^{th} – 90^{th} percentile), with a median σ_{noise} of 1.4 ppbv. A more sensitive ozone instrument could therefore significantly improve the flux uncertainty at a 20-minute ~~averaging period~~averaging interval.

Besides the random uncertainty discussed above, systematic errors are also worthy of some consideration. Specifically, whether the highest and lowest frequencies of turbulence have been adequately observed. High frequency information can be lost if measurements are made too infrequently, or if the sample is attenuated significantly in the sample tubing. Measurements at 10 Hz, as performed here, are widely considered sufficient to observe this high frequency structure. Sensor separation was minimised by locating the sample inlet directly beneath the sonic anemometer ($\sim 20 \text{ cm}$ below). Laminar flow was also avoided through the length of the sample line (Reynolds number = 3000). As a result, the co-spectrum in Figure 11 shows no major loss of high frequency information compared to theory. Since fluxes were calculated over 20-minute ~~averaging period~~averaging intervals using linear detrending, there is also a chance that low frequency information may not be fully observed. Firstly, using a simple block average in place of linear detrending had little effect on the median flux observed (+1.7%), implying that linear detrending is not causing much low frequency information loss. Using an ~~averaging period~~averaging interval of 1 hour instead of 20 minutes gave slightly larger magnitude flux (+4.1%) as well. However, the longer period lead to much greater data loss (22%) to the selection criteria in Sect. 2.4, hence the 20-minute average was used for this work. This suggests that any low frequency loss is approximately 5% of the total flux – a small amount relative to the calculated 2σ random uncertainty (85%).

4 Discussion

4.1 Model comparison

For the average meteorological conditions observed during this work, the one-layer model of Fairall et al. (2007) predicts a deposition velocity of 0.037 cm s^{-1} , assuming reaction of ozone with iodide only. Here, one-layer refers to considering the water column to have uniform reactivity to ozone with depth. This is not the same as considering the chemical reaction only in the reaction-diffusion sublayer, and both chemical reaction and turbulent transfer in the layer beneath (the two-layer model). By contrast, the revised two-layer model of Luhar et al. (2018) predicts a deposition velocity of 0.018 cm^{-1} for the same conditions using a reaction-diffusion sublayer (δ_m) of $4.2 \text{ }\mu\text{m}$, parameterized using Eq. (11). An iodide concentration of $\sim 600 \text{ nmol dm}^{-3}$ would be necessary to yield the observed deposition velocity – much higher than a typical oceanic value of $\sim 80 \text{ nmol dm}^{-3}$ (Chance et al., 2014). However, DOM (Shaw and Carpenter, 2013), chlorophyll (Clifford et al., 2008) and surfactants (McKay et al., 1992) have also been shown to increase ozone deposition velocity. Therefore the effective pseudo-first order rate constant for the reaction of ozone with water, a , is likely to be higher than accounted for by iodide alone. Chang et al. (2004) defined this total reactivity as:

$$a = \sum_i k_i C_i \quad (19)$$

Where a is the effective pseudo-first order rate constant for the reaction of ozone with water, and k_i and C_i are the second order rate constant and concentration of species i , respectively. We include an estimate of the effects of DOM reactivity using a typical oceanic DOM concentration of $52 \text{ }\mu\text{mol dm}^{-3}$ (Massicotte et al., 2017) and a rate constant of $3.7 \times 10^{-6} \text{ dm}^3 \text{ mol}^{-1} \text{ s}^{-1}$ (average of the values reported by Sarwar et al. (2016) and Coleman et al. (2010)). Doing so increases a from 544 s^{-1} to 737 s^{-1} and leads to average deposition velocities for our field campaign of 0.048 cm s^{-1} and 0.028 cm s^{-1} for the models of Fairall and Luhar, respectively.

The magnitude of the effect of DOM on O_3 deposition velocity remains highly uncertain due to the uncertainties in how O_3 interacts with DOM and surfactants, variability in the sea-surface microlayer (SML) composition, and the effect of temperature. The coastal waters near the PPAO experience large phytoplankton growth during the ‘spring bloom’ (Cushing, 1959; Smayda, 1998), and the organic content and composition of the SML could be very different compared to the open ocean. The seasonal and spatial variations in these O_3 -reactive substances could in turn drive differences in ozone deposition velocity. For example, Bariteau et al. (2010) reported v_d increasing from 0.034 cm s^{-1} to 0.065 cm s^{-1} as the waters changed from open ocean to coastal during the TexAQS-2006 cruise. It is unclear how much of the observed gradient is a result of SML composition or of terrestrial influence. Similarly, the model of Ganzeveld et al. (2009) underestimated coastal ozone deposition velocities when DOM reactivity was omitted, suggesting that this may be a particularly important factor in coastal environments. While the model of Fairall et al. (2007) appears to match our observed v_d well, it is possible that this is a consequence of some missing reactivity. Inclusion of DOM causes the one-layer model to overestimate v_d , as reported by Luhar et al. (2018).

4.2 Wind speed dependence

In their discussion on wind speed dependence, Helmig et al. (2012) found [that](#) their data fit reasonably well with the parameterisation of Fairall et al. (2007):

$$v_d \cong \alpha \sqrt{aD_c} + \frac{\alpha}{6} \kappa u_{*w} \quad (20)$$

where α is the dimensionless solubility of ozone in water, a is the effective rate constant for the reaction of ozone with molecules in the surface water in s^{-1} , D_c is the molecular diffusion coefficient of ozone in water in $\text{m}^2 \text{s}^{-1}$, κ is the von Kármán constant (0.4), and u_{*w} is the water-side friction velocity in m s^{-1} . The fit shown in blue in Figure 12 was determined using parameter values relevant to the experiment at the PPAO, with u_{*w} derived from u_* assuming atmospheric surface stress to be equal to the waterside surface stress (Luhar et al., 2017):

$$u_{*w} = \sqrt{\frac{\rho_{air}}{\rho_{water}}} u_* \quad (21)$$

where ρ_{air} and ρ_{water} are the densities of air and water respectively. α , a , and D_c were determined empirically according to Eq. (22) (Morris, 1988), Eq. (23) (Magi et al., 1997), and Eq. (24) (Johnson and Davis, 1996):

$$\alpha = 10^{-0.25-0.013(T_s-273.16)} \quad (22)$$

$$a = [I^-] e^{\left(\frac{-8772.2}{T_s} + 51.5\right)} \quad (23)$$

$$D_c = 1.1 \times 10^6 e^{\left(\frac{-1896}{T_s}\right)} \quad (24)$$

where T_s is the sea surface temperature (in K) and $[I^-]$ is the aqueous iodide concentration in mol dm^{-3} . We note that Eq. (23) only accounts for the reactivity of ozone with iodide in the sea surface. Other species present in the SML have also been shown to react with ozone (Martino et al., 2009; Shaw and Carpenter, 2013), but given the uncertainty surrounding their reactivity and any temperature dependence, they have been omitted here. Fixed T_s (284 K) and $[I^-]$ (85 nmol dm^{-3}) values from April-May 2018 and representative of the footprint of PPAO (Sherwen et al., 2019) were used to determine α , a , and D_c , and thus v_d (cm s^{-1}) using Eq. (20) (blue dashed line in Figure 12). This can be simplified to:

$$v_{d \text{ predicted}} = 0.01324 + 0.09378u_*$$

In comparison, the linear fit (red dashed line in Figure 12) of our experimental 20-minute v_d values against u_* (with standard errors) is:

$$v_{d \text{ measured}} = (0.02017 \pm 0.00570) + (0.07537 \pm 0.01953)u_*$$

Our results therefore show comparable, but slightly lower dependence on friction velocity (and therefore also wind speed) than predicted by the parameterisation of Fairall et al. (2007). Comparison of our data to this parameterisation yielded a root mean square error (RMSE) of 0.0522 cm^{-1} and a mean bias of 0.0020 cm s^{-1} (a positive bias here denoting observations

greater than the model). Given the assumptions of the simplified model (Eq. (20)) and the uncertainties in various parameters, not least the rate constant for the reaction of O₃ with I⁻ (e.g. Moreno & Baeza-Romero, 2019), this agreement is perhaps surprising. The two-layer model of Luhar et al. (2018) for the same data is shown in black in Figure 12. Considering only iodide reactivity (i.e. omitting any enhancement in reaction rate due to the presence of organic material in both models), this model appears to under-predict deposition velocity compared with the one-layer model of Fairall et al. (2007), and lacks any major dependence on wind speed except during very calm conditions. Comparison of our data to the two-layer model gave higher RMSE and mean bias (0.0584 cm s⁻¹ and 0.0247 cm s⁻¹ respectively).

The two-layer model is set up to account for ozone reactions with chemical species other than iodide. Inclusion of these additional reactions would increase the predicted deposition velocity to be more similar to our observations. However, the two-layer model also predicts that v_d does not strongly depend upon variations in wind speed, which is in contrast with our observations.

5 Summary and conclusions

An ozone chemiluminescence detector adapted from an Eco Physics® CLD 886 NO_x detector was used to measure the ozone deposition velocity to the sea surface at a coastal site near Plymouth, on the southwest coast of the UK. The median observed deposition velocity was 0.037 cm s⁻¹, comparable with previous values from tower-based measurements of 0.025 cm s⁻¹ (McVeigh et al., 2010) and 0.030 cm s⁻¹ (Whitehead et al., 2009). Furthermore, our data are at the upper end of the values obtained by Helmig et al. (2012) during ship-based, open-ocean measurements (0.009–0.034 cm⁻¹). Cross-covariance was used to empirically determine a 2σ limit of detection for the O₃ flux for each ~~averaging period~~averaging interval. This limit of detection had a median value of 0.113 mg m⁻² h⁻¹, and was exceeded in 305 out of 491 flux intervals. Auto-covariance of high-frequency ozone data indicated that instrument noise was a significant component in the observed ozone variability (45-98%), and lowering the noise level would reduce the flux uncertainty.

In moderate to high winds, the observed deposition velocity showed a linear dependence on friction velocity in the mean. This is comparable to that predicted by the one-layer model of Fairall et al. (2007) considering only ozone-iodide reaction. However, including estimated (but unverified) contributions from ozone-DOM reactions causes the one-layer model to overpredict the observations.

For the conditions encountered during the campaign, the two-layer model of Luhar et al. (2018) yields a ~~predicted~~ v_d of 0.018 cm s⁻¹ with iodide reaction only, and 0.026 cm s⁻¹ with reactions of both iodide and ~~estimated~~ contributions from DOM. While the latter value is close to our median observation, the two-layer model does not reproduce the observed wind speed dependence in v_d .

Elevated deposition velocities were observed at low wind speeds, contrary to predictions (Chang et al., 2004) and to previous observations (Helmig et al., 2012). We attribute this observation to a contribution to v_d from land within the footprint during periods of low wind. Periods with wind speeds > 3 m s⁻¹ (corresponding to approximately < 10% land cover in the footprint)

were used to evaluate v_d . However, the possibility of land influence could not be completely removed, with our oceanic v_d estimates potentially overestimated by 8%, even after wind speed filtering. The potential for tidal effects on v_d (exposing shoreline and input of river water with different chemical composition) were also examined, though no clear periodicity could be observed, either at the tidal frequency or on a diurnal timescale.

Future work will link the properties of the sea-surface microlayer in the footprint area to observed O_3 fluxes. A longer time series with more observations of microlayer chemical composition may help to elucidate the influence of biogeochemical parameters, seasonal variation and wind speed dependence, which have not been definitively characterised to date.

Code and data availability: the eddy4R software packages used in these analyses are maintained at <https://github.com/NEONScience/NEON-FIU-algorithm>. 20-minute data have been submitted to the Centre for Environmental Data Analysis (CEDA), doi:10.5285/8351ed155b134155848d03a7cdce9f02. The corresponding author can be contacted directly for the full high-frequency data.

Author contribution: Experimental work was carried out by DCL, TGB and MY. DCL also conducted the formal analysis and visualisation of the results, with relevant supervision from TGB and MY. SM developed the eddy4R codebase, with ARV providing modification for its use here. RJP provided software for instrumentation and validation of model applications to the data. JDL and LJC supervised the interpretation of the results. The work was proposed by LJC, who also acquired the necessary funding. DCL prepared the manuscript with all authors contributing to the editing process.

Competing interests: The authors declare that they have no conflict of interest.

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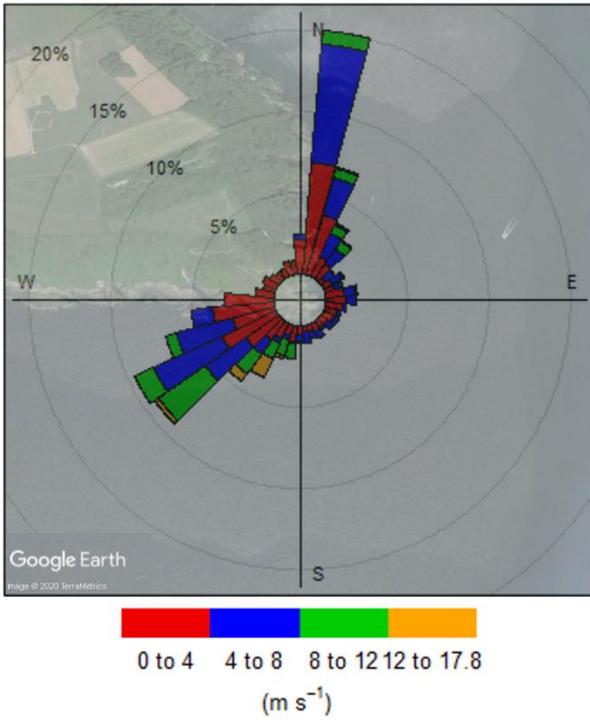
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715 **Table 1: Selection criteria applied to calculated fluxes, with number (and percent) of points remaining.**

Selection Criterion	Number of 20-minute periods (%)
Sufficient data in 180–240° wind sector	723 (100%)
Ozone stationarity (trend < 6 ppbv)	689 (95.3%)
Wind stationarity (σ_{wd}) < 10°	655 (90.6%)
Ozone variability σ_{O_3} < 2 ppbv	609 (84.2%)
Sensitivity within 3 σ of mean	710 (98.2%)
Wind speed > 3 m s ⁻¹	584 (80.8%)
All of the above	491 (67.9%)



720 Figure 1: Wind directions and speeds at the PPAO during the study period. Radial percentage values indicate the portion of all observed wind that fell within a given sector. ~~Winds are strong and frequent from the direction of interest in the south west.~~ © Google Earth.

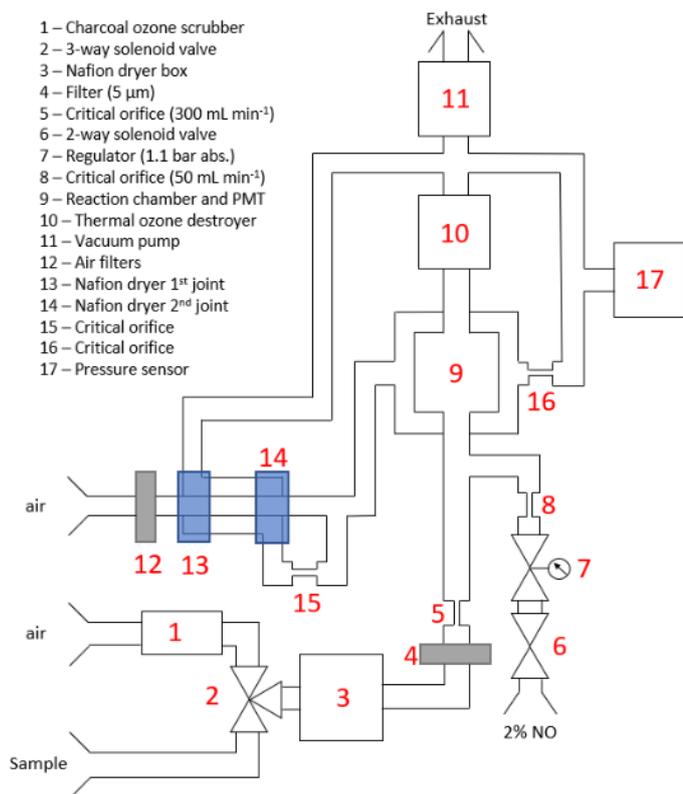
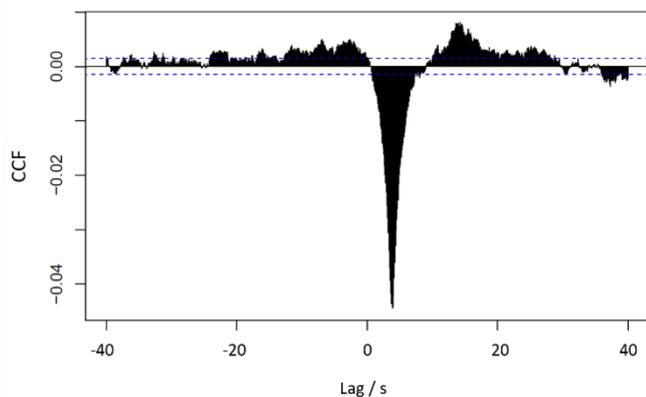
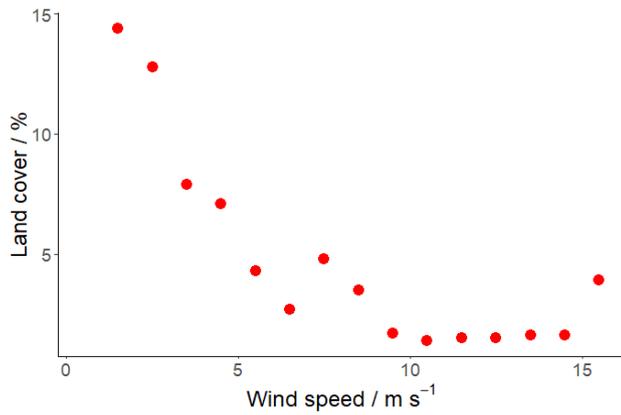


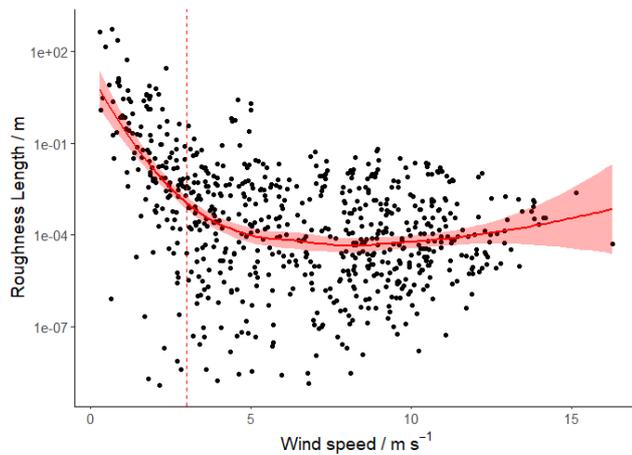
Figure 2: Schematic of the ozone chemiluminescence detector.



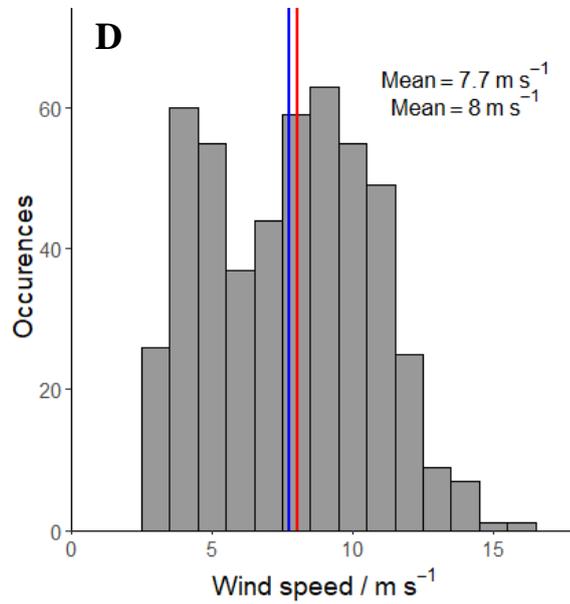
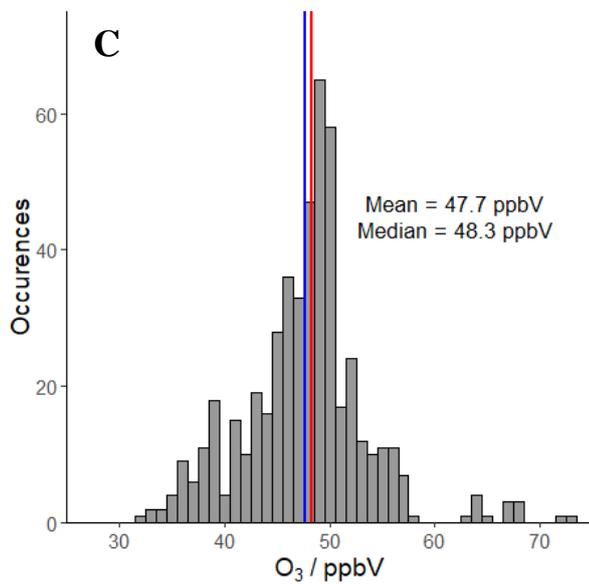
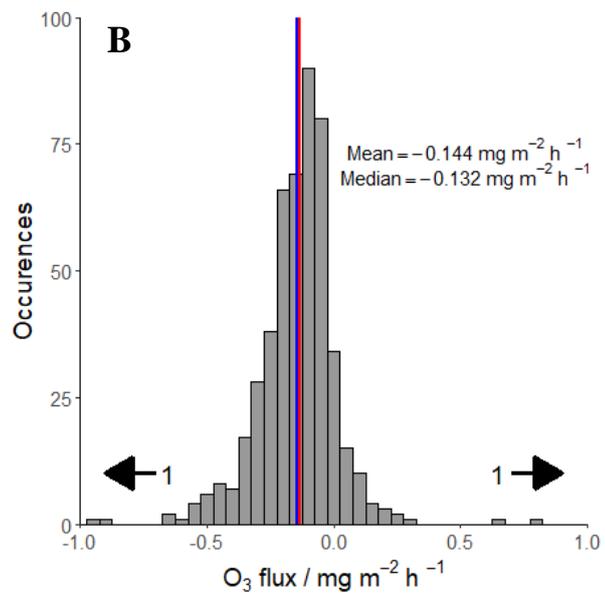
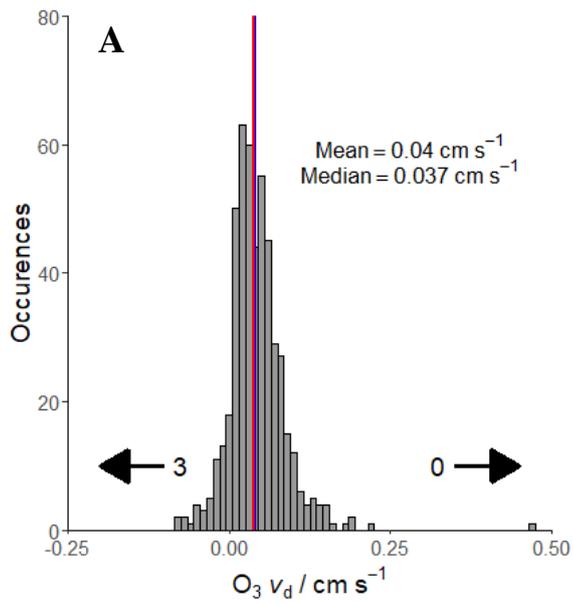
725 **Figure 3: Example cross correlation function (CCF) for ozone and vertical wind on 10th April. The negative peak minimum indicates that ozone data lags 3.9 seconds behind the wind data.**



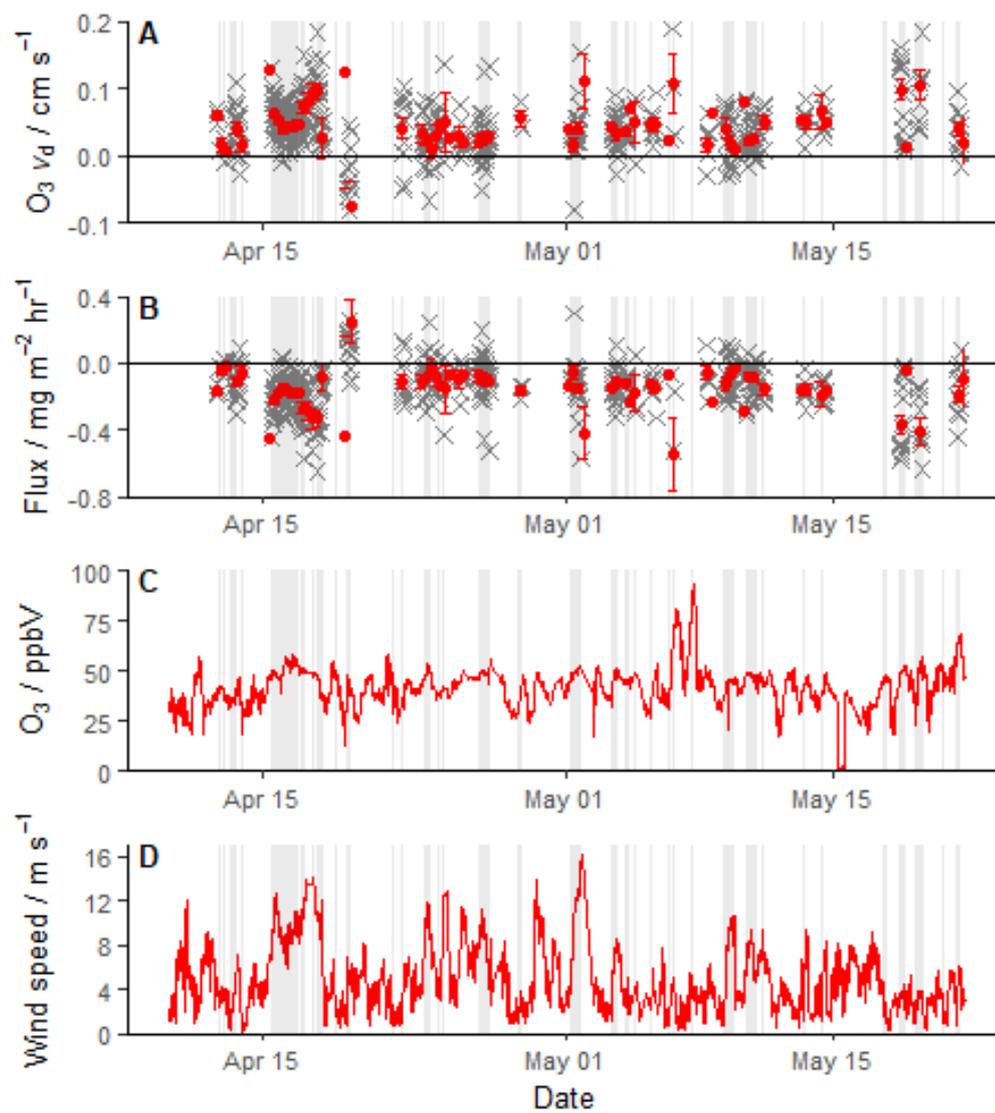
730 **Figure 4: Land cover percentage within the average flux footprint for 1 m s⁻¹ wind speed bins as calculated with the Kljun et al. (2015) flux footprint parameterisation. The presence of land within the footprint area was greater during periods of low wind speed and atmospheric instability**

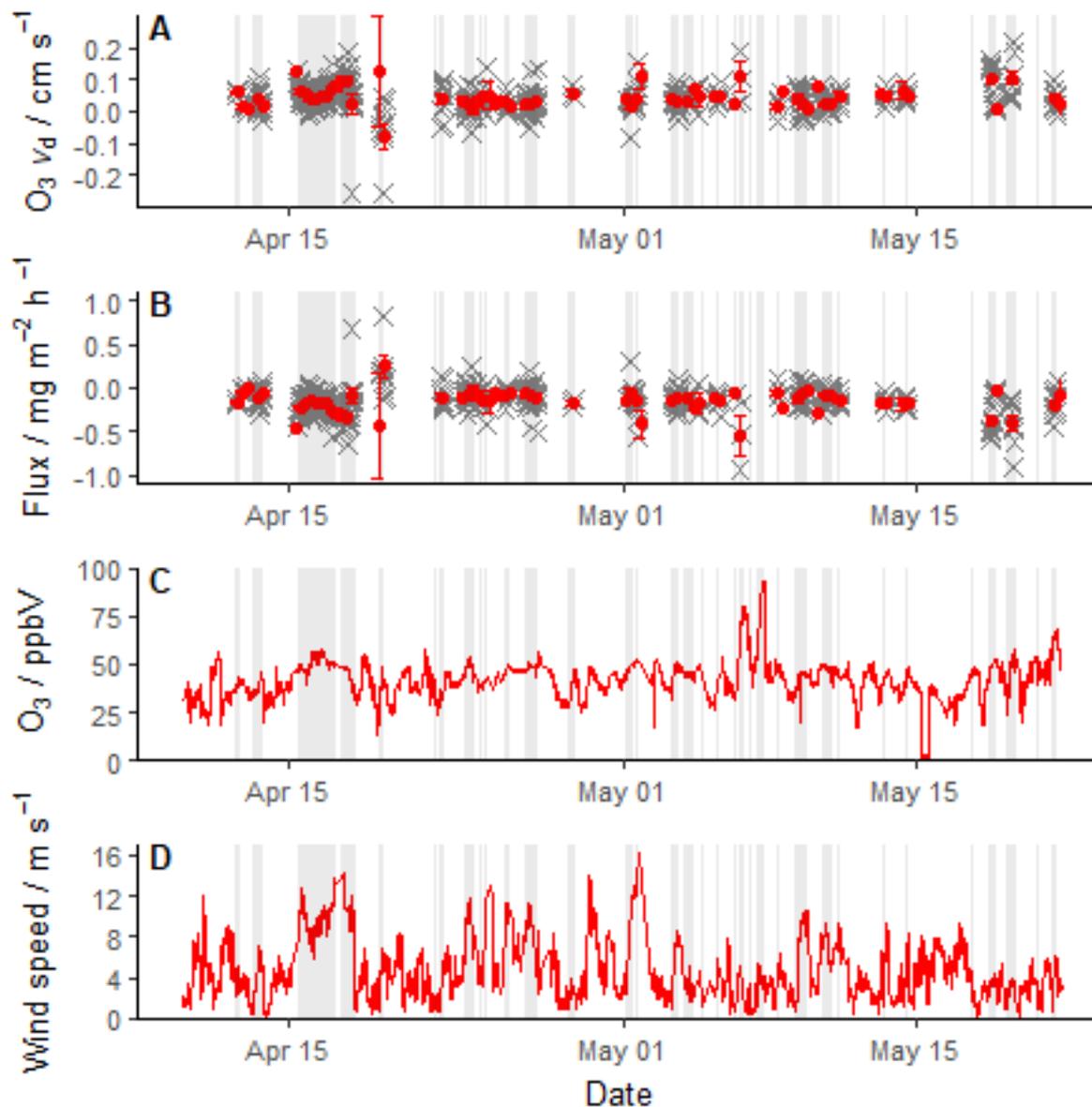


735 **Figure 5: Roughness length for each averaging period/averaging interval (black dots), increased by land influence within the footprint at low wind speeds, with a smoothed line of fit/local regression (LOESS) line (solid red, 95% confidence interval shaded). Points left of the 3 m s⁻¹ filter threshold (dashed red) are not used in subsequent discussions of oceanic deposition velocity. Y axis limited for clarity, with 17 points < 10⁻⁹ m not shown.**

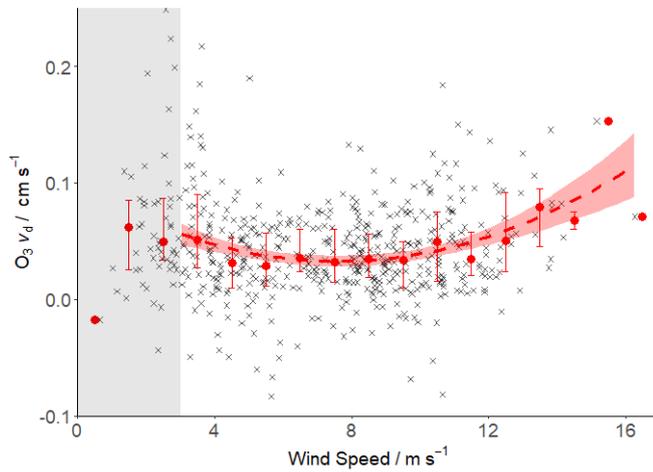


740 **Figure 6: Ozone deposition velocity (A), mass flux (B), ozone concentration (C) and wind speed (D) histograms for all periods that passed the filtering criteria. Mean values are represented by blue lines, median values by red lines. Deposition velocity and mass flux are plotted in the range $-0.25 - 0.50 \text{ cm s}^{-1}$ and $-1.0 - 1.0 \text{ mg m}^{-2} \text{ h}^{-1}$ respectively for clarity, with arrows indicating the number of points beyond these limits.**

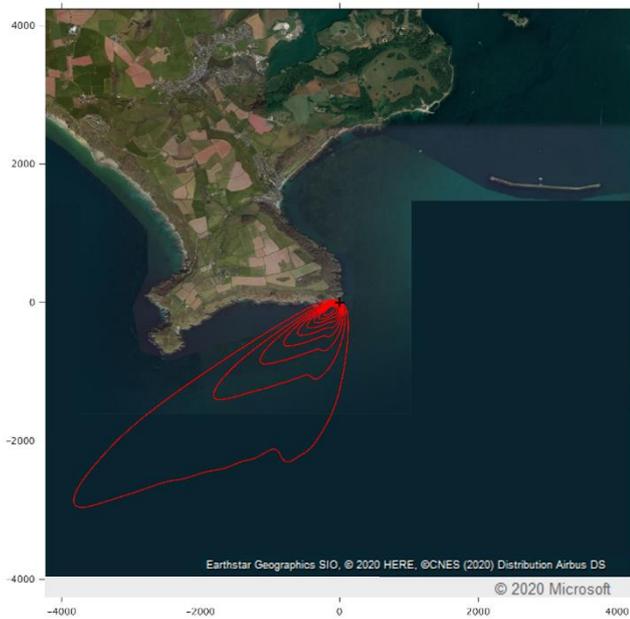




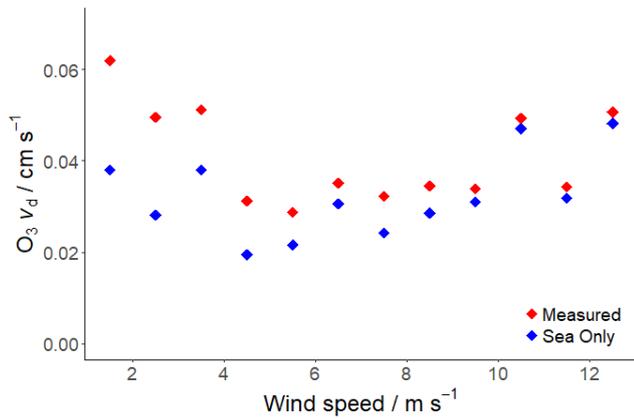
745 Figure 7: Time series of ozone deposition velocity (A), ozone mass flux (B), mean ozone concentration (C) and mean
 750 wind speed (D) from 10th April to 21st May 2018. Grey crosses represent 20-minute values, with red dots for 6-hour
 means with standard errors. All concentration and wind speed data are shown from 10th April to 21st May, with only
 deposition/flux values that passed filtering criteria shown in (A) and (B). Periods with an accepted wind direction
 (180-240°) are shaded. Flux and deposition velocity data are thus only presented from these periods and when the
 wind speed was > 3 m s⁻¹ (D). The y axis in (A) and (B) are limited as -0.1 to ± 0.23 cm s⁻¹ and ± -0.8 - 0.41 mg m⁻²
h⁻¹ respectively for clarity. Points beyond these y axis bounds are $v_a = -0.442$ (1.47 mg m⁻² h⁻¹) and $v_a = 0.472$ (-1.64
mg m⁻² h⁻¹), which cause the large error bars on April 19th.



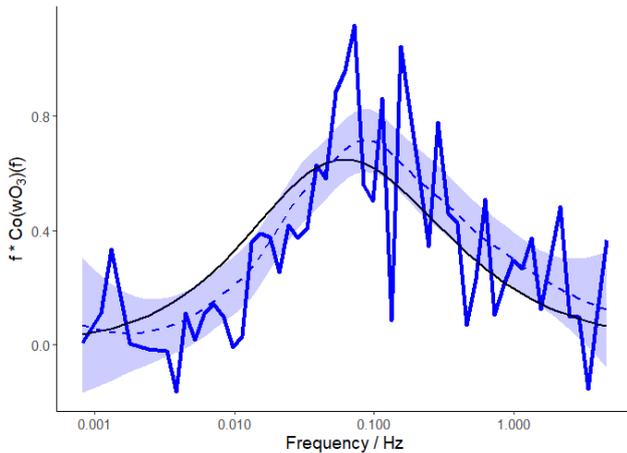
755 **Figure 8: Deposition velocity dependence on wind speed. 20-minute values are shown in grey, with bin-averaged medians (1 m s^{-1}) with and interquartile ranges shown in as red dots with bars. Wind speed dependence is shown with a 2nd order polynomial fit is plotted as a dotted red line. The grey region below 3 m s^{-1} indicates values removed by the wind speed filter (Sect. 2.4) that are not included in the fit.**



760 **Figure 9: Flux footprint climatology for all 20-minute data that passed the selection criteria according to the Kljun et al. (2015) footprint model. Each contour represents the area contributing 10% of the observed flux, up to 90% for the outermost contour. A binary land/sea classification estimated a mean land contribution of 3.9%.**

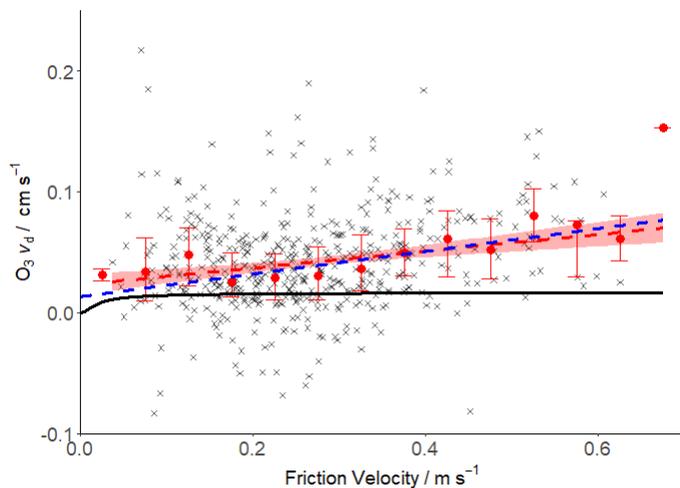


765 **Figure 10: Median deposition velocities in 1 m s^{-1} wind speed bins for combined land and water-sea surfaces as measured (red) and for water-surfaces/sea only (blue). Sea only values were calculated by subtracting the land contribution, estimated from the land cover and land deposition determined by least square regression. Values at the lowest wind speeds are most influenced by land, and pPeriods with wind speeds below 3 m s^{-1} were not included in the**



final results.

770 **Figure 11: Average ozone flux co-spectrum for the 17th April, normalised to area = 1. Wind speeds were $10.3 - 12.3 \text{ m s}^{-1}$ and dimensionless Obukhov lengths were $0.14 - 0.17$, representing near neutral, slightly stable conditions. Expected co-spectral shape predicted by Kaimal et al. (1972) shown in black. The agreement between observations and Kaimal suggests that the full range of flux-carrying turbulent eddies are being reasonably well measured.**



775

Figure 12: Deposition velocity dependence on friction velocity. 20-minute values are shown in grey, ~~with bin-~~ averaged median fluxes (0.05 m s⁻¹ bins) are presented with interquartile ranges ~~shown~~ in red. Dependence of O₃ deposition velocity on friction velocity is presented with a linear fit in red, with the dependence predicted by Fairall et al. (2007) in blue, and that predicted by Luhar et al. (2018) in black.

780

Response to Editor's Comments

Below we present each comment (black) followed by what changes were made (blue). Line numbers given in blue refer to the document with track changes displayed.

785

Line 28ff. Rephrase (and shorten) these two sentences to better focus on the results of the present study. E.g. "In contrast to our observations, the ozone deposition velocity in the recently developed two-layer model by Luhar et al. (2018) shows not major dependence on wind speed and underestimates the measured values."

790

L28: Two sentences condensed: 'In contrast to our observations, the deposition velocity predicted by the recently developed two-layer model of Luhar et al. (2018) (which considers iodide reactivity in both layers, but with molecular diffusivity dominating over turbulent diffusivity in the first layer) shows no major dependence of deposition velocity on wind speed, and underestimates the measured deposition velocities.'

795

Line 54: This is too generalized for eddy covariance. Specify to: "...is the best way of observing fluxes in the atmospheric surface layer ..."

L54-56: Changed to 'More recent flux measurements have been made with the eddy covariance method, which is the best way of observing fluxes in the atmospheric surface layer without perturbing it'

Line 114: I think the meaning of "sea-surface composition" is not clear to the average reader. Please explain.

800 L116-117: Changed to specify chemical composition of the water - 'Better characterisation of the effects of wind speed and the chemical composition of the surface water on ozone deposition velocity to the sea surface...'

Line 134: Do you mean 'standard' liters at atmospheric pressure? If not, define the pressure for this value.

L137-138: Yes, this is standard litres per minute – changed to '...by a vacuum pump at 13.5 SLPM'

805 Line 136: The meaning of "this sample manifold" is unclear. A manifold was not mentioned previously.

L139: Changed 'manifold' to 'line' to match the previously mentioned sample line.

Line 156: I suggest to clarify the sentence as follows: "It is necessary to calculate EC fluxes over a suitable averaging interval to reduce ..."

810 L159-160: changed as suggested to 'It is necessary to calculate eddy covariance fluxes over a suitable averaging interval...'

Line 159: I suggest to replace "averaging period" by the more common and specific term "averaging interval" for the EC flux calculation here and throughout the text.

815 'averaging period' replaced with 'averaging interval' throughout the document

Line 182: What "supply of ozone" was used here? How was the concentration determined? With a gas-phase titration?

L185-186: qualified 'known' ozone, and the model of the source – 'which was estimated using a supply of known ozone in the absence of water vapour (supplied from a calibrated Thermo model 49i-PS ozone primary standard)'

820

Line 200: What do you mean with "a modified workflow"?

L204: changed to 'a workflow customised for our measurements' – The eddy4R code still undergoes development by many people in different development branches. Our workflow was therefore slightly different from the 'core' code, such as including the 'drifting lag time' that was applied, discussed later in the Materials and Methods section.

825

Line 221: It should be added here, what this means for the uncertainty of the (quantitative) footprint estimates.

L227-228: added a sentence to acknowledge the additional uncertainty - 'This will therefore introduce some additional uncertainty to footprint extent and land coverage, beyond that inherent to the parameterisation.'

830 All Figures: I do not at all agree with the request of Reviewer #1 that the figure captions should include an interpretative take home message! Please remove the corresponding statements e.g. in Figs. 1, 5, 10, 11. The captions have to include all necessary information to read the figure, but the interpretation should be placed in the main text when citing the figure.

Corresponding explanatory statements removed

835 Figure 5 caption: Specify "Roughness length for each EC flux interval (black dots) and smoothed fit line (solid red)"
Also specify how the fit line was calculated and what the red shaded range around the line represents.

L732-734: specified requested details: 'Roughness length for each averaging interval (black dots) with a smoothed local regression (LOESS) line (solid red, 95% confidence interval shaded)'

840 Figure 7: Panels A and B are not very informative with present scaling (dominated by few outliers). In panel A use the same y-axis scaling as in Fig. 8 (-0.1 ... +0.2) and add the horizontal zero line. In panel B rescale y-axis (e.g. -0.8 ... +0.4) and add the horizontal zero line.

Requested changed made to Figure 7. Updated caption and removed listing of points beyond limits (as there are now more than is practical to list. The number of points should be apparent from Figure 6).

845

Figure 8 caption: Specify to "...with interquartile ranges shown as red circles with vertical bars. A 2nd order polynomial fit function is plotted as dotted red line. ..."

L755-756: Changed to 'with bin-averaged medians (1 m s^{-1}) and interquartile ranges shown as red dots with bars. A 2nd order polynomial fit is plotted as a dotted red line.'

850

Figure 9: In this figure it is not possible for the reader to really see the land surface part of the flux footprint. I suggest to add a second zoom-in picture (e.g. 500x500m) with more details about the direct surrounding of the tower (similar to Fig. 1).

We realise the exact land presence is not very easy to see in the footprint plot, but the output from the online parameterisation is not of sufficiently high image quality to zoom in very far in a neat fashion. Resolution aside, the presence of every contour bunched near the observation point makes a zoomed image of limited extra use:

855



As this is not a plotting script developed by us, these are non-trivial issues to try and resolve, and we feel a zoomed image would not be able to offer any additional clarity in this case.

860 Figure 10 caption: Use consistent labelling ("Sea only", "water surfaces only") in diagram and caption. Also mention, how the "Sea only" data were determined from the measured fluxes.

L763-766: Changed to 'sea only' consistently. Added 'Sea only values were calculated by subtracting the land contribution, estimated from the land cover and land deposition determined by least square regression'

Figure 12 caption: Improve the phrasing. Use full individual sentences instead of "with ... with ..."

865 L775-776: Changed phrasing to '20-minute values are shown in grey. Bin-averaged median fluxes (0.05 m s^{-1} bins) are presented with interquartile ranges in red.'

LANGUAGE CORRECTIONS

Line 21: better write "with the tide."

870 Line 42: "the deposition velocity is ..."

Line 61: replace "in" by "from" or "based on"

If this refers to line 60, 'In the instruments used for...', I would disagree that 'from/based on' makes more sense. If it refers to the 'on' in line 61, I maintain the 'on' is most correct, as the dye is physically positioned on the surface of the disc.

875

Line 65: change to "at the water surface" (the genitive 's is mainly used for persons)

Line 108: replace "these" by "the"

Line 200: change to "The molar flux ..."

Line 299,299,306,308,309: use past tense "varied", "observed", "exhibited", "reported", "increased"

880 Line 427: change to "...found that their data ..."

Line 479: omit "predicted" here (the model was used in a diagnostic, not in a prognostic way)

Line 480: omit "estimated". It is unnecessary here.

All other language corrections have been made as requested