We thank the anonymous referee for the constructive comments that have been useful to improve the paper. Following the comments of the referee, corrections have been applied on the paper. The new version of the manuscript with highlighted changes can be found in last section of the response.

The paper presents a novel procedure to characterize the geometry, and its influence on receiving features, of a motor-controlled lidar. The aim of the paper is very interesting and I must thank the authors for this descriptive work, that is of practical interest for many lidar instruments.

I have some remarks:

1

The system analyzed is the multi-wavelength multi-telescope Rayleigh-Mie-Raman "9-eyes" lidar in Rome Tor Vergatta. The authors give a reference where the description of the lidar was included (Congeduti et al, 1999). Unfortunately this paper has little detail about the system, although the main innovations are pointed out. As a result, the present paper devotes section 2 to a further description of the system, in its present state. So this description is of great interest.

First of all, Congeduti et al, 1999 says very little about, for instance, the transmitted laser, and so Table 1 in the present paper includes some additional data. I am somehow puzzled about the energy distribution of the laser pulses (400 mJ @355 nm, 200 mJ @532 nm). Could the authors possibly confirm this data and elaborate a bit more? It would also be helpful knowing about the manufacturer and model of the laser, or knowing if it was developed by the Rome Tor Vergata team.

Manufacturer and model added to the description (line 91). The energy distribution is nominal and optimized for the UV output (line 92).

An additional issue is about the fibres that are used to bring the light collected in the different telescopes (after being separated in visible and UV bands near the telescope focal planes). The first mention (on line 113) does not say anything about the fibres, while later on we learn that they have 0.94 mm cores... which is not standard at all. Maybe some modified reference, as "large-core fibre" could be made from the first time. This would improve the reader's understanding.

"Large-core fibre" added to the text (line 112).

Table 8 depicts the correspondence of telescopes and received wavelengths. I presume that these are the actual implemented channels. To me it is not clear why, for instance, the smaller and widest field telescope is not used for the 355 channel... unless the "receiving block" depicted in figure 3(b) is not built for the small telescopes (3 and 4). If this is the case, it should be clearly stated. Any other details about the telescopes should be stated as well.

The smallest telescope does not have a dichroic beam splitter in the receiving block. The difference between this and the other receiving blocks is now also clarified in Fig. 3 caption. The lidar system was originally designed for the mid-upper atmosphere and the 355 nm capability was added in 2011. Table 4 was updated in order to clarify the definition of acquisition channels in terms of telescopes and received wavelengths.

Table 5 is somehow puzzling: according to table 4, some combinations of telescopes and received wavelength are not possible or are not implemented. Anyway, the different overlap parameters are computed for every channel and the two elastic wavelengths, with the only exception of R0 and R1 for 355 nm and telescope 4... so I would ask the authors to state clearly if table 4 counts for implemented interconnections or for the possible ones, and make it as coherent as possible with table 5.

The combinations are calculated for the two emitted wavelengths (now clarified in the table caption) for each telescope and consider the currently implemented interconnections. Please note that the 9 largest telescopes are not used for 355 nm acquisition but still receive Raman signals at 386 and 407 nm.

2

Section 3.1 is devoted to the description of the strategy for optimizing the mutual alignment of laser beams, telescope and the so-called "receiving blocks", which couple the collected light into one or two fibres (depending on the specific channel). I have not been able to find a detailed description of these receiving blocks, other than a very simplified sketch in figure 3.b. and some vague description around line 110; I have found no citation of any other source describing these blocks.

Knowing the equivalent focal distance of the optics that couples the incoming light to the fibre(s) at the output of the block is necessary to understand the influence of a given displacement in any of the XYZ axes. A more detailed description of these receiving blocks is expected from the authors. This data would allow a more complete analytical model of the method.

Information on the lenses and schematics of the receiving blocks added in the new version (Fig. 3).

Even though it is stated that the optimizing criterium is maximizing the normalized signal, for me it is not clear enough what would be taken as "reference signal" or, more precisely, how it was obtained (somewhere in the text it is suggested that it is channel 2?). It should be stated if this reference signal and the normalized signal is measured at a given range from the lidar (what is suggested later on in figure 16), maybe considered as the most significant; or if this figure is obtained from some integration of the detected signal profile for each position. This should be stated in a non-ambiguous way.

Clarified in the new version. See lines 280-288.

It would be desirable that the authors present a model for the expected variations in the signal for given deviations from the optimum position, that can be applied to the actual parameters of the receiver channels (focal distance of telescopes, receiving blocks, acceptance angle of the fibres, etc.).

The study is aimed to implement a procedure for the characterization of the relative beam-telescope FOV alignment and assumes that the optical system downstream of the field stop diaphragm is well aligned (see line 236 and 115). A full description of all the components in the optical path is outside of the scope of the study. We instead focus on the development of a simple operative procedure to optimize the performance of the system. Nevertheless, the cumulative effect of deviations from the nominal position of all the optical elements can be qualitatively identified by the procedure. This was clarified in line 250.

3

Section 3.2 describes very shortly the laser mapping procedure. This procedure is devoted to determine the overlap profile of the laser-telescope-receiver block system. The authors must include a description of how this profile is computed from the signals obtained during the laser mapping procedure. Later on (section 4.3) a model for retrieving this overlap profile is cited (Stelmaszczyk et al, 2005). This citation must be made in section 3.2 as well, with details of its implementation.

The procedure for the overlap function estimation follows an original approach and is described from line 308 to 312 (now updated for better clarity). The cited model was used only for the validation.

4

Section 4.1 describes the telescope mapping and alignment process. While the graphical presentation makes this process very easy to understand, some question still arise:

First of all, two telescope mapping sessions are reported, but Table 6 includes information about a later laser mapping session, reported in section 4.3. This should be clearly stated, as nothing is said about this later session in the table title or, better, collected in an additional table located in section 4.3. I must remind here my comment #3.

The information on the three sessions was left in a single table. The table format and caption are now corrected for better clarity.

This process is devoted to optimally align of channel 1, which is normalized with respect to channel 2. This seems OK with the first lines of table 6. So, why channels 4 and 8 (386 and 355 nm) are acquired? Are they used in any way? According to table 4, they are collected with the 30-cm telescope which does not seem to be part of the process. Please clarify the content of this table.

They are acquired but not used in the mapping procedure. Table 6 caption was corrected for better clarity.

Figure 10 shows normalized signals, obtained in a "coarse" mapping session. This is how it had been announced by the authors. They start from a "manual" previous alignment and explore different positions. Even though this is a coarse alignment, do the authors consider that there is an optimum position as a result of this first session? It is somehow suggested that one of the positions in Fig 10.b should be the one. Please confirm that this is the, let us say, provisional choice.

As stated in line 321 the coarse mapping session is used to preliminary identify the sub-volume of optimal alignment.The results of the first session are then used to center the second session movements around the presumed optimal position. To clarify the different steps of the procedure, the optimal position resulting from the coarse mapping has been added in line 344. This provisional choice differs slightly from the final choice.

Regarding the second session, the results are presented in absolute signal instead of normalized one. Even though this does not seem to me to be an issue, it is the only plot where such absolute signal intensity values are presented. In section 2 of my remarks I wrote that I was missing a definition of this signal, be it absolute or normalized.

The second channel was not used for normalization due to highly incomplete overlap in the low range. Clarified in the new version (line 358). For the definition of signal and normalized signal see line 212 and 280-288

Finally the variations for different z positions are depicted in figure 12, once again with normalized signal. Is there a plot like figure 12 available from session 1?

Both sessions are depicted in Fig. 12 (now Fig. 13). The figure was updated to better differentiate the two sessions.

I must emphasize that the definitions of "signal" and "normalized signal" must be stated.

The definition of signal and normalized signal are now in line 212 and 280-288.

5

No comments on section 4.2.

6

As I mentioned in comment #4, the details of the laser mapping should be detailed in a table included in this section.

As mentioned in a previous comment, the information on the three sessions was left in a single table. The table format and its caption were updated for better clarity.

For the first time in the article, it is somehow suggested that the signal values depicted are taken at a given range, here described by a delay value. If it is so, this must be stated here and in the previous sections.

Each mapping figure represent the signal (or normalized signal) at some selected range. All the captions were updated in order to clarify the range of each subplot.

Once again, absolute signal is used without any explanation.

The absolute signal was used only for the graphical representation in order to show both mapping signal and mapping in the reference position.

Line 426 states "…the experimental results are in agreements with the models". The authors must detail or cite these models clearly.

The models are detailed in line 436. An explicit citation of the Halldórsson and Langerholc (1978) model was added in the new version.

A semi-automated procedure for the emitter-receiver geometry characterization of motor-controlled lidars

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Abstract. To correctly understand and interpret lidar acquired signals and to provide high quality data, the characterization of the lidar transmitter-receiver geometry is required. For example, being fundamental to correctly align lidar systems, this characterization is useful to improve the efficiency of the alignment procedure. In addition, some applications (e.g. air quality monitoring) need to quantitatively interpret the observations even in the range where the overlap between the telescope field

10   of view and the laser beam is incomplete. This is generally accomplished by correcting for the overlap function. Within the frame of Lidar based networks (e.g. ACTRIS/EARLINET) there is a need to define standardized approaches to deal with lidar geometry issues. The multi-wavelength multi-telescope Rayleigh-Mie-Raman "9-eyes" system in Rome Tor Vergata, part of ACTRIS/EARLINET, has the capability to change through computer-controlled servomotors, the orientation of the laser beams and the 3D position of the diaphragm of the receiving optical system around the focal point of the telescopes. Taking

15   advantage of these instrumental design characteristics an original approach to characterize the dependency of the acquired signal from the system relative transmitter-receiver geometry (the *mapping* procedure) was developed. The procedure consists in a set of programs controlling both the signal acquisition as well as the motor movements. The approach includes solutions to account for atmospheric and laser power variability likely to occur during the mapping sessions. The paper describes in detail the developed procedure and applications such as the optimization of the telescope/beam alignment and the estimation

20   of the overlap function. The results of the mapping applied to a single combination of telescope-laser beam are shown and discussed. The effectiveness of the mapping-based alignment was successfully verified by comparing the whole signal profile and the outcome of the *telecover* test, adopted in EARLINET, for a manual and a mapping-based alignment. A significant signal increase and lowering of the full overlap height (from 1500 m to less than 1000 m) was found. The overlap function was estimated down to 200 m and compared against the one obtained from a geometric model. The developed procedure

25   allowed also estimating the absolute and relative tilt of the laser beam. The mapping approach, even in simplified versions, can be adapted to other lidars to characterize and align systems with non-motorized receiving geometry.

1 Introduction

Lidar (light detection and ranging) techniques are an efficient tool to provide quantitative information about vertical properties in the atmosphere (Measures, 1984; Weitkamp, 2005). Thanks to the technological advancement of the last twenty years, the

30   employment of lidar systems in sensing the Earth atmosphere has rapidly grown. As an example, aerosol properties are studied by spaceborne lidar observations (e.g. Winker et al., 2003; McGill et al., 2015; AEOLUS), by ground-based lidar networks (e.g. the European Aerosol Research Lidar Network, EARLINET, Pappalardo et al., 2014) and, recently, by single-channel automated lidar ceilometers (e.g. Wiegner et al., 2014; Dionisi et al., 2018). In particular, the advanced multiwavelength elastic and Raman lidars, which are part of EARLINET, provide unsurpassed information for the characterization of aerosol optical

35   properties. This network is now a key component of ACTRIS (the European Aerosol Cloud and Trace Gases Research, www.actris.eu), a research infrastructure that will coordinate the atmospheric composition observations in Europe. Within this frame, to provide quality-assured data sets by not standardized lidar systems, like most of those that are part of EARLINET, one of the major efforts of this community was to establish quality-assurance (QA) methodologies (Pappalardo et al., 2014; Wandinger et al., 2016; Freudenthaler et al., 2018). Expected outcome of this effort is to characterize lidar performances and

40   check, homogenize and attest the quality of the acquired data. After passing the QA tests, lidar raw data can be, then, processed by the Single Calculus Chain (SCC) that allows the "automatization and fully traceability of quality-assured aerosol optical products" (D'Amico et al., 2015). Within this frame, the characterization of lidar transmitter-receiver geometry (e.g. Halldórsson and Langerholc, 1978; Measures, 1984; Kokkalis, 2017) is essential to provide high quality data.

    As the main objective of EARLINET is the study of the aerosol in the troposphere and boundary layer (PBL), it is important

45   to correctly interpret the received lidar signal in the lowermost range. However, bi-axial lidar systems present an incomplete response in the near-range observational field due to the partial overlap of the receiver field of view (FOV) and the transmitted beam. Therefore, to use data from heights below the full overlap height, lidar signal profiles must be corrected for this near-field loss of signal, that is the overlap function $O(R)$ (Wandinger and Ansmann, 2002), which depends on the lidar system (e.g. Wandinger et al., 2016).

50   Within EARLINET, the telecover test, presented by Freudenthaler et al. (2018), is a useful and easily implementable tool for the evaluation of the correct alignment of the lidar system. This method allows identifying the lower height at which the lidar signal can be used to retrieve aerosol optical properties (i.e. the lower height of full overlap for ideal lidar system), however, it cannot provide an estimation of the overlap function. In literature various methods were developed to compute this function both analytically and experimentally. Analytical methods (e.g. Halldórsson and Langerholc, 1978; Jenness et al., 1997;

55   Chourdakis et al., 2002; Stelmaszczyk et al., 2005; Comeron et al., 2011) require knowledge of light distribution in the laser beam cross section, receiver characteristics and relative inclination of the laser beam with respect to the receiver axis. Experimental methods on the other hand make specific assumptions or have special requirements based on the method: clear air and homogeneous aerosol distribution (Sasano et al., 1979), statistically homogeneous distribution (Tomine et al., 1989), extrapolation via polynomial regression (Dho et al., 1997), a second profile with lower overlap (e.g. ceilometer, Guerrero-

60   Rascado et al., 2010; Sicard et al., 2020), or Raman channel with the assumption of similar receiver geometrical configuration (Wandinger and Ansmann, 2002).

The multi-wavelength multi-telescope Rayleigh-Mie-Raman (RMR) "9-eyes" system in Rome Tor Vergata (Congeduti et al., 1999) is an old-style powerful lidar developed in mid 90s with the objective of monitoring the mid and upper atmosphere (D'Aulerio et al., 2005; Campanelli et al., 2012; Dionisi et al., 2013a, b). To meet the EARLINET requirements, which the system has been part of since July 2016, in addition to the standard EARLINET procedure, specific tests, based on the characteristics of the system, were developed to characterize the RMR performance in the near range.

The RMR system was designed with the capability to control, through computer-controlled servomotors, the orientation of the laser beams and the 3D position of the diaphragm of the receiving optical system around the focal point of the telescopes. These instrumental characteristics were exploited to develop the *mapping* procedure: a set of semi-automated tools to characterize the dependency of the acquired signal from the relative transmitter-receiver geometry.

With respect to the existing approaches, the obtained results do not need any assumptions or external information and include all artefacts due to the system that may be difficult to account for in an analytical or numerical representation.

With the objective of optimizing the RMR observational performances in the troposphere and in the PBL, the developed procedure and two examples of applications are presented in this study:

- alignment optimization based on mapping information;
- experimental estimation of the overlap function $O(R)$.

In Section 2 the relevant instrumental characteristics of the RMR lidar system with a specific focus on the emitter-receiver geometry of the system are presented. Section 3 describes the developed methodology and reports examples of telescope and laser mapping. Section 4 presents the results obtained for two applications limited to a single wavelength telescope combination. The mapping-based alignment is verified through the comparison with telecover test results. The overlap estimation is compared to the full overlap height estimated with the telecover test and with the predicted values using a simple geometric model based on the nominal characteristic of the system as presented in Section 2.

Finally, Section 5 contains the summary of the developed approach, the achieved main results as well as short term perspectives in terms of potential development. The applicability of the proposed approach to other systems is also discussed.

2 System Description

The design of the multi-channel multi-telescope RMR "9-eyes" lidar was first presented by Congeduti et al. in 1999. Since 2002 the system is operating in the Tor Vergata experimental field in a semi urban area southeast of Rome (41.8422º N, 12.6474º E, 107 m ASL). Its current configuration is described in detail by Dionisi et al. (2010).

Here the relevant characteristics of the lidar system with emphasis on the geometry of the emitting/receiving components are presented.

The lidar transmitter is based on a Nd:YAG laser (Continuum Powerlite 8010) with 2nd (532 nm: Green) and 3rd (355 nm: UV) harmonic generators. The energy output is optimized for the exploitation of the UV Raman scattering. Backscattered

radiation is collected and analysed at 4 wavelengths of interest: 532 nm and 355 nm for the elastic backscattering, 386.7 nm and 407.5 nm for Raman scattering of N_2 and H_2O molecules, respectively. The characteristics of the transmitted beam are

95   reported in Table 1. In particular, it is noteworthy that 355 and 532 nm beams are collimated by means of 5x beam-expanders and, then, they are vertically projected into the atmosphere through two 45° mirrors that can be Azimuth and Zenith oriented through computer-controlled servomotors (Fig. 1).

Table 1: Transmitter characteristics of the RMR lidar system.

Laser Type	Nd:YAG
Wavelength [nm]	355 – 532
Nominal Energy per pulse [mJ]	~400 (355 nm), ~200 (532 nm)
Pulse duration [ns]	7
Pulse repetition rate [Hz]	10
Beam diameter d_L [cm]	5.0 (after the 5x beam expander)
Beam divergence Ψ_L [mrad]	0.1 (nominal, full angle after b.e.)
Pointing stability [mrad]	~0.05

100
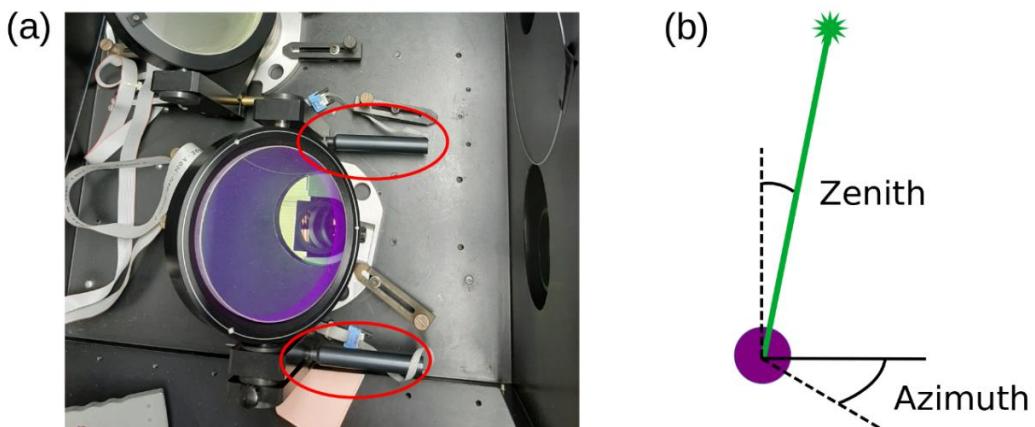
Figure 1: (a) Top view of the two 45° mirrors with azimuth and zenith servomotors (red circled components). (b) Schematic of the mirror/beam movements.

105   The receiver is based on a multiple-telescope configuration allowing the sounding of a wide altitude atmospheric interval:

- one single 15 cm aperture telescope for the lower layers,

- one single 30 cm telescope for the middle layers,

- an array of 9 x 50 cm telescopes for the upper layers (~1.7 m^2 total collecting area, see Fig. 2)

The characteristics of the telescopes are reported in Table 2. For each of the 11 telescopes, behind the field stop diaphragm

110 (0.2, 0.4, 0.6, 0.8 mm diameter for the 30 cm telescope, fixed 0.8 mm for the others) that is in the focal position, there is a dichroic beam splitting optical system that separates the signals at $\lambda < 440$ nm from the ones at $\lambda > 440$ nm and directs them in two different large-core optical fibres, with 0.94 mm core diameter and 0.22 numerical aperture. In this optical system (see Fig. 3 for a detailed description), a one-to-one coupling of the field diaphragm on the optical fibre is obtained employing a set of lenses ($f = 20$ mm), first to collimate the radiation on the dichroic mirror, then to focus the resulting different wavelength

115 signals on the input face of the respective fibre. Each receiving block has been aligned on an optical bench before being mounted on the lidar system.

Table 2: Telescope characteristics.

|	Collector 1	Collector 2	Collector 3
Type of telescope	9 Newtonians array	Single Newtonian	Single Newtonian
Diameter [cm]	50 (each)	30	15
Focal length f [cm]	150	90	45
f-number	f/3	f/3	f/3
FOV (full angle) Ψ_T [mrad]	0.5	0.9	1.8

120
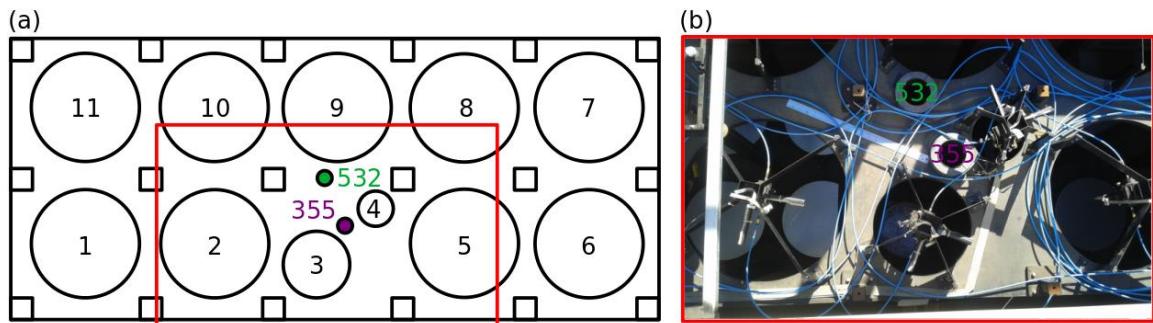
Figure 2: (a) Top view schematic of the relative position of the laser beams (355 and 532) and the 11 telescopes. (b) Details of the emission and low range telescopes (15 cm and 30 cm).

11
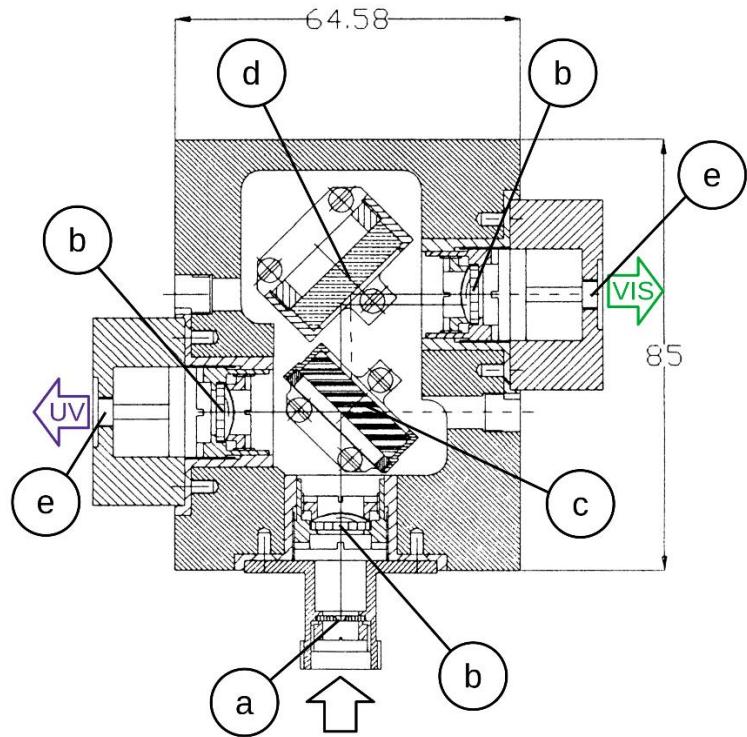
Figure 3: Schematics of the receiving block, a: field stop diaphragm (0.8 mm diameter), b: collimation lenses ($f = 20$ mm), c: dichroic beam splitter ($\lambda = 440$ nm), d: 45° mirror, e: optical fibre connector. Dichroic beam splitter and UV collimation lens are currently not present in the receiving block of the 15 cm telescope.

Field diaphragm, dichroic beam splitting optical system, and SMA connectors for the two optical fibre input faces are assembled in a small box supplied with adjustments for lens focusing and dichroic mirror alignment. A system of three orthogonal linear stages allows moving each box along the x, y, and z axes by means of computer-controlled servomotors, to find optimal alignment and focusing positions autonomously for each telescope.

A total of 37 servomotors (3 for each telescope and 2 for each emitting wavelength) are present. Two models of EOTECH Testine Micrometriche Servocontrollate (TMS) are used: the TMS-25 for the movements in the z-axis direction of the receiving system in the telescopes and the TMS-16 for all other movements. Table 3 reports the nominal characteristics of the employed servomotors. Each motor is controlled by a dedicated board. The boards can be connected in a serial way to control with a single RS-232 serial port more boards. A set of 3 racks containing up to 14 boards is used to control the motors through 3 serial ports. Motors relative to a given telescope or emitting mirror are grouped in a single rack: for this reason, it is possible to control only one motor at once.

Model	Range	Speed	Acceleration	Resolution	Accuracy
	[mm]	[mm/s]	[mm/s^2]	[μm]	[μm]
TMS-16	16	0.2	0.2	1	±3
TMS-25	25	0.2	0.2	1	±4

Two large carbon-fibre planes are utilized to support, respectively, the telescopes (the lower ones), and the spiders holding the

145 *x-y-z* motor-moved stages with the dichroic boxes; fiberglass columns stick together the two planes. With this architecture of the telescope supporting frame, effects on the alignment of thermal deformations are minimized. The receiving optical system with the servomotors is depicted in Fig. 4.

In the current setting, for the smallest telescope (15 cm), only the optical fibre carrying the signal return at $\lambda > 440$ nm exits the dichroic system, as this telescope is used only for the elastic backscattering at 532 nm. Then, the optical fibres bring the

150 light from the telescopes to the photomultipliers (PMTs) after passing collimating lens and interference filters that select the wavelengths of interests.
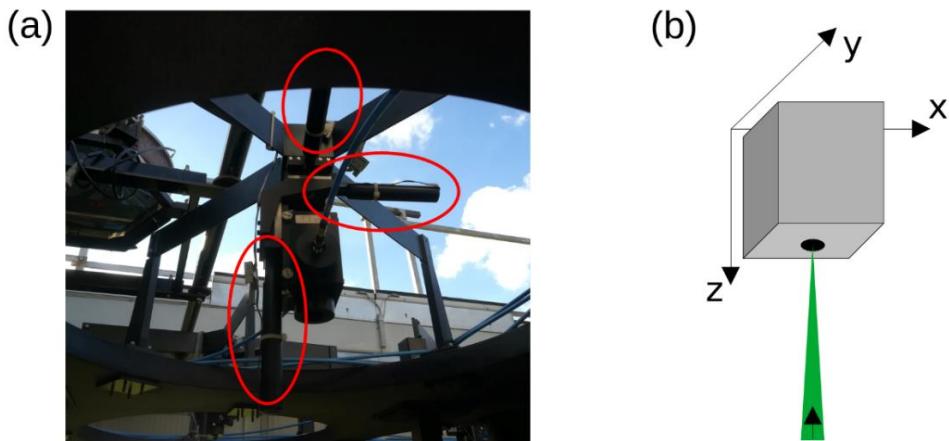
Figure 4: (a) Receiving optical system with the 3 axis servomotors (red circled components). (b) Schematic of the receiving block movements.

155

Currently 8 acquisition channels both in photon counting mode as well as analogue mode are implemented, Table 4 provides an overview of the RMR channels with their associated telescopes and receiving wavelengths.

For standard measurement sessions the acquisition system is set to acquire the photon counting mode signals for 2000 bins

160 with 0.5 μs integration per bin. Samples in the analogue channels are acquired at a fastest rate, with 0.05 μs sampling rate, but

they are averaged in groups of 10 to have identical vertical resolution as in the counting channels and, simultaneously, to improve the accuracy of the recorded data. Thus, in the usual operation, the vertical resolution is 75 m (corresponding to 0.5 µs bins) and the signals are generally integrated over 60 second (600 laser pulses) before recording.

Table 4: Wavelengths and telescopes used for each currently implemented channel.

	355 nm	386 nm	407 nm	532 nm
15 cm				CH01
30 cm	CH08	CH04	CH05	CH02
9 x 50 cm		CH06	CH07	CH03

The relative emitter-receiver geometry can be modelled knowing the characteristics of emitters and receivers (Table 1 and 2) and the distance between the centres of each combination of emitter and receiver.

Summarizing, given:

- d_{cc}: Distance between the centres of the laser beam and the telescope,
- Ψ_L, Ψ_T: the divergence (full opening angle) of the laser beam and the telescope respectively,
- d_L, d_T: beam and telescope diameter respectively,

and assuming:

- parallel vertical axes (beam and telescope FOV),
- aperture in the focal plane (focus at infinity),

it is possible to calculate the following geometrical characteristics relevant for the description of the overlap function $O(R)$ (Stelmaszczyk et al., 2005):

$$R_0 = \frac{2d_{cc} - d_T - d_L}{\Psi_T + \Psi_L} \tag{1}$$

$$R_1 = \frac{2d_{cc} + d_T + d_L}{\Psi_T - \Psi_L} \tag{2}$$

Where R_0 is the lowermost height at which the laser beam enters in the telescope field of view and R_1 is the full overlap height (i.e. the lowermost height with $O(R)=1$). As an example, Fig. 5 shows the case of the 15 cm telescope and 532 nm beam. These equations are equivalent to the ones calculated from the diaphragm point of view (Halldórsson and Langerholc, 1978; Measures, 1984) taking into account the previously stated assumptions.

Table 5 completes the description of the geometry by reporting, for each telescope, the telescope diameter (d_T), the field of view (Ψ_T) and the distance from each emitting source ($d_{cc\ 532}$, $d_{cc\ 355}$). Based on the nominal characteristics of the RMR system

and the analytical model described above (Eq. (1) and (2)), the values of R_0 and R_1 have been computed for all implemented combinations of <mark>emission laser wavelengths</mark> (355 and 532 nm) and telescopes. Results are reported in Table 5. It has to be noted that the full overlap height can be optimized by tilting properly the laser beam with respect to the telescope axis (Kokkalis, 2017).

Table 5: Characteristics, initial (R_0) and full (R_1) overlap heights of the 11 telescopes for each emitted wavelength. Laser beam radius d_L=5.0 cm and divergence Ψ_L=0.1 mrad were used for the calculations. The specifications of interest for this study (channel 1: 532 nm, 15 cm telescope) are highlighted in bold.

Telescope	1	2	3	**4**	5	6	7	8	9	10	11
$d_{cc\,532}$ [cm]	121	63	46	**32**	82	125	140	80	35	63	122
$d_{cc\,355}$ [cm]	124	62	25	**20**	66	141	138	85	56	84	137
d_T [cm]	50	50	30	**15**	50	50	50	50	50	50	50
Ψ_T [mrad]	0.53	0.53	0.89	**1.78**	0.53	0.53	0.53	0.53	0.53	0.53	0.53
$R_{0\,532}$ [m]	2953	1121	576	**234**	1721	3079	3553	1658	237	1121	2984
$R_{0\,355}$ [m]	3047	1089	152	**NA**	1216	3584	3489	1816	900	1784	3458
$R_{1\,532}$ [m]	6854	4177	1610	**501**	5054	7038	7731	4962	2885	4177	6900
$R_{1\,355}$ [m]	6992	4131	1077	**NA**	4315	7777	7638	5192	3854	5146	7592
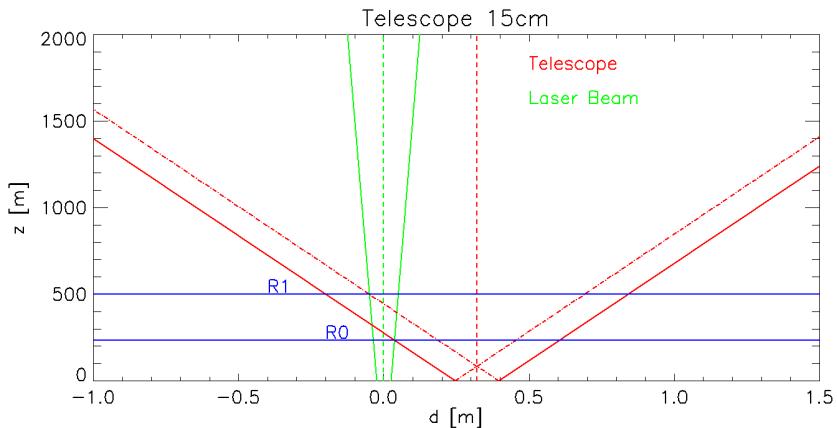
Figure 5: Schematic of the overlap between the telescope FOV (red) and the laser beam (green). Full overlap is reached inside the cone delimited by the dash-dotted lines. R_0 and R_1 heights are highlighted by the horizontal lines.

A more realistic theoretical estimation of the whole overlap function is possible. However, it requires accurate knowledge of the real characteristics and positions of the optical parts of the system (e.g. beam shape, relative inclination between the laser

beam and telescope axis). The estimation of these parameters needs a characterization of the lidar emitting-receiving components that is often difficult to perform. The proposed approach to characterize the geometry of the signal (Section 3) allows an estimation of the overlap function (Section 4.2).

The following sections will focus on the characterization of channel 1 (532 nm, 15 cm telescope). This is the channel dedicated to the PBL sensing for which is fundamental the knowledge of the overlap function. The procedure described is however applicable to all the remaining laser/telescope combinations for quality control and signal optimization.

3 The mapping procedure

The mapping procedure takes advantage of the possibility to investigate the dependency of the acquired signal $S(R)$ from the relative transmitter/receiver geometry by controlling the orientation of the laser beam and the 3D position of the diaphragm of the receiving optical system around the focal point of the telescopes. The procedure is based on a set of programs controlling both the signal acquisition as well as the motor movements and it is fully defined by setting the following variables:

- telescope/laser beam of interest
- reference/starting position (x_0, y_0, z_0 for the telescopes, Az_0, Zen_0 for the laser beams);
- range and regular step in each direction independently (i.e. number of acquisitions);
- channels to be acquired;
- acquisition characteristics (e.g. duration, bin size etc.).

Defining these parameters is a trade-off between having a detailed and low noise information and minimizing the signal variability introduced by changes in the atmosphere and in the lidar system (e.g. laser power). To minimize the atmospheric variability, the mapping procedure should be preferably performed in stable meteorological conditions (e.g. end of the night). However, strategies to monitor/account for these variabilities have been implemented and will be discussed for each example of mapping reported.

The single telescope and laser mapping are described in detail in the following subsections.

3.1 Telescope mapping

The telescope mapping procedure controls the position of the optical system in all three axes. This procedure is implemented by performing, for a given set of z positions, a series of acquisitions in the horizontal plane (x and y directions). Each x-y plane is scanned starting from a reference position (x_0, y_0) along a spiral path, in order to minimize the necessary motor movements (see example in Fig. 6).
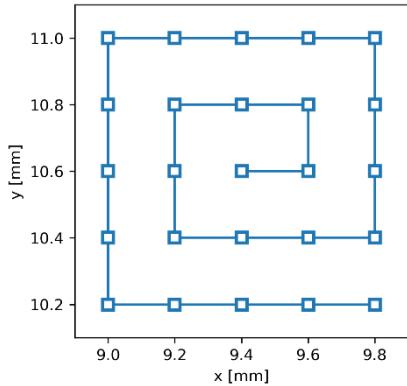
Figure 6: Example of telescope mapping geometry in the *x-y* plane (used for the first measurement session described in this work), *x* **and** *y* **relative position of the servomotors in the respective axis.**

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Given the relative dimension of the diaphragm and the optical fibre core, and assuming a well aligned receiving box, the procedure presented in this study takes into account only the characterizable effect of the field stop diaphragm displacement. Moving the diaphragm in the *x-y* plane on a fixed *z*, for an image of radius $r_i < r_d$, where r_d is the diaphragm radius, approximately constant counts are expected in a circle of radius $r_d - r_i$ and a decrease to zero counts within a radius $r_d + r_i$

240 (Fig. 7a). This of course under the assumption that all the signal passing through the diaphragm is captured by the PMT. When the signal is clipped in the path between the aperture and the sensor, the obtained mapping could be asymmetric and could diverge from the expected shape. The resulting image could also be affected by inhomogeneities in the PMT sensitivity (Freudenthaler, 2004), the use of optical fibres effectively acts as a light scrambler minimizing the impact of this problem (Sherlock et al., 1999). Small imperfections in the beam cross section, when the image is small and well-focused, should not

245 cause asymmetries in in the resulting mapping.

For a fixed range *R* in lidar the acquired profiles, when changing the *z* coordinate of the field stop/diaphragm, the image is expected to grow from the minimum in the focused position following the enlargement of the circle of confusion. If the image size is bigger than the receiving optical component (e.g. diaphragm, optical fibre, lens) part of the signal will be lost but the mapping will still be symmetric (Fig. 7b).

250 From the qualitative analyses of acquired signals from a single telescope mapping, knowing the ideal behaviour, it is possible to diagnose deviations from the nominal positions for all the optical components in the system not taken into account by the simplified model. As an example, Fig. 8 depicts a simulated single plane mapping in case of good alignment and a real mapping showing problems with the optical alignment (i.e. signal clipping in the optical system between the telescope and the photomultiplier).

255
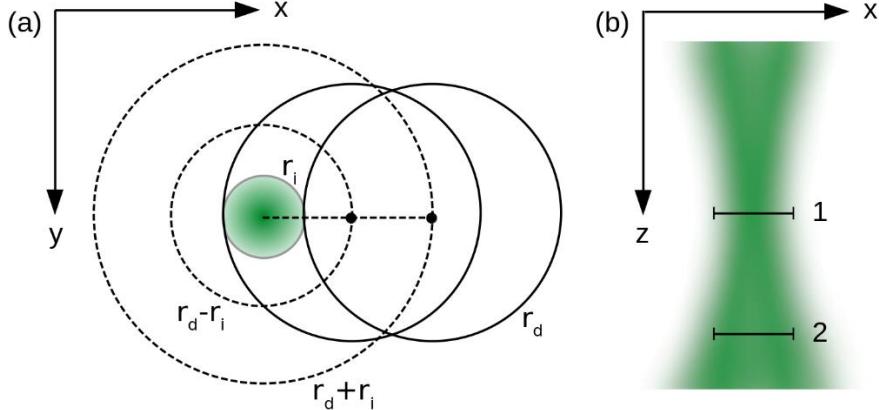
Figure 7: (a) Expected radii for maximum ($r_d - r_i$) and partial counts ($r_d + r_i$) in the signal map for an image of radius r_i and a diaphragm (solid line) of radius r_d for $r_i < r_d$. (b) Schematic longitudinal view of radiation intensity near the focal plane, diaphragm in a focused (1) and in an out of focus (2) position.


Figure 8: (a) Simulated signal map for a diaphragm of radius $r_d = 0.4$ mm and an image of radius $r_i = 0.2$ mm. The signal is normalized by the maximum value. (b) Result of a single plane mapping performed with misaligned optics, here the signal (normalized by the maximum value) is asymmetrically clipped by the optical system between the telescope and the photomultiplier.
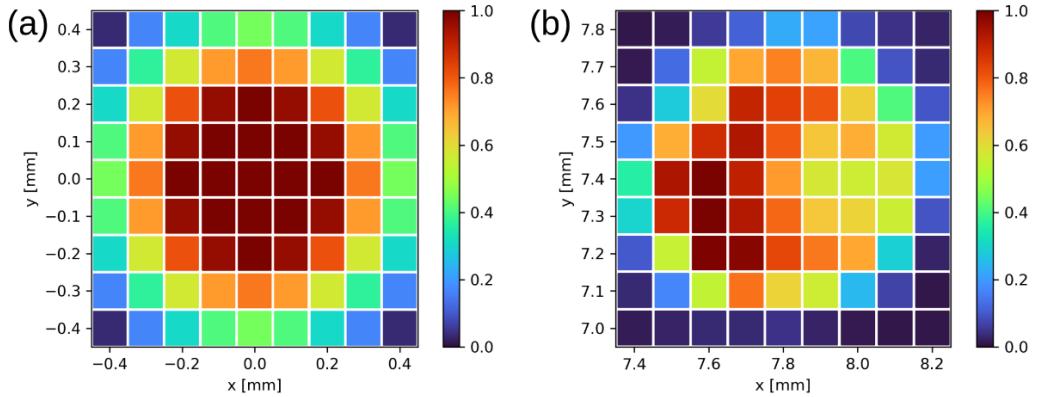
The information given by this type of mapping can be used to accurately position the receiving optical system as shown in Section 4. Another potential use of the information derived from the mapping is to estimate unknown characteristics of the system.

As an example, the relative tilt between the field of view axis and the laser beam can be computed once found the centre of the image in the focal plane (x_c, y_c). For high ranges, this position corresponds to a configuration with parallel beam and field of view axes. If the measurements are done at different positions of the receiving system in the horizontal plane, the relative tilt angle θ_{tilt} can be calculated for any given position (x, y) with the following formula:

18

$$\theta_{\text{tilt}} = \frac{D(x_c, y_c, x, y)}{f}$$

(3)

275

Where f is the telescope focal length and D is the geometric distance between the position x, y and the reference one x_c, y_c.

As previously mentioned, a trade-off between obtaining a reasonable SNR in the range of interest and minimizing possible changes in the signals due to atmospheric and system variability is needed.

In order to account for atmospheric/system variability two approaches have been tested:

280
- in case there is a channel acquiring information at the same wavelength of the channel being mapped but through another telescope, a normalized signal is obtained from the ratio of the profiles from the two channels. For example, the normalized signal $S'(R)=S_{\text{CH01}}(R)/S_{\text{CH02}}(R)$ used for the mapping of channel 1 described in the following section (Sect. 4.1) is defined as the ratio between the simultaneously acquired measurements from channel 1 and 2 (Table 4).
- in absence of a suitable signal from a second channel, the signal profile from the same channel, acquired periodically
285
in a reference position (e.g. the position chosen with a previous alignment) during the mapping, can be used to normalize the measurements within the interval of time between acquisitions in the reference position. This approach is used in the laser mapping (Sect. 3.2 and 4.2), in this case the normalized signal was calculated as $S'(R)=S_{\text{CH01}}(R)/S_{\text{CH01}}^{\text{ref}}(R)$.

3.2 Laser mapping

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In the case of lidar systems with the capability of electronically controlled azimuth and zenith orientation of the laser beam, an analogous procedure can be implemented, leading to similar insights on the geometry of the system.

For a given telescope-laser relative geometry the overlap function can be estimated through a mapping performed varying the laser beam zenith and azimuth angle. The lowermost range for which the overlap function can be estimated depends on the characteristics of the system being required that the laser beam can be tilted to have some position with full overlap. Moreover,
295
in order to define an absolute maximum with $O(R)=1$, the size of the image has to be smaller than the diaphragm (i.e. the image is sufficiently focused).

The scan is performed progressively, minimizing the necessary motor movements (Fig. 9) and the subsequent delay between acquisitions. To monitor changes in the atmospheric conditions and in the power output of the laser, an acquisition in a reference laser position (e.g. the setup chosen with the telescope mapping and used for routine measurements) is performed
300
before and after each zenith swipe. This is highlighted in Fig. 9, where at the beginning and at the end of each column (i.e. zenith angle swipe) the laser beam returns to the same pair of zenith and azimuth values. Time-interpolated data acquired in the reference position $S_{\text{CH01}}^{\text{ref}}(R)$ are used to normalize the measurements during the mapping.

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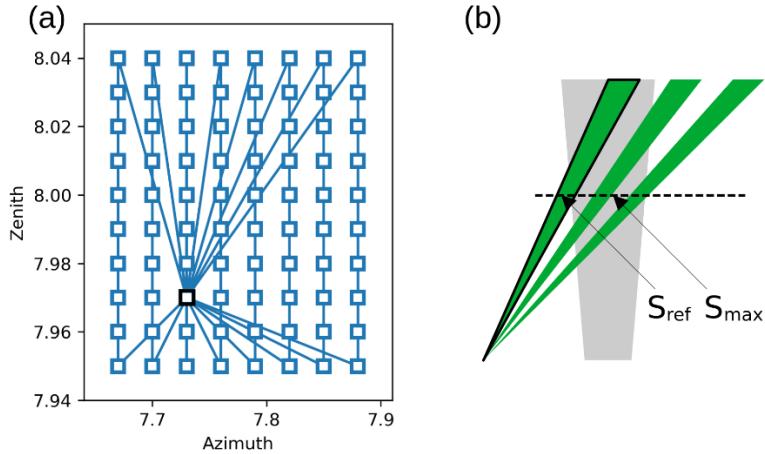
Figure 9: (a) Laser mapping scan geometry, after each zenith scan a measurement in the reference position (black square) is performed. **(b)** Schematic of the telescope FOV and laser beam for different orientations.

To estimate the overlap function, for each range value R, the maximum (or the mean of the highest n values, if the mapping is performed with sufficient x-y resolution) of the normalized signal S'_{max} is searched. Under the previously stated assumptions, this value should represent the ratio between a full overlap signal and S_{CH01}^{ref} affected by partial overlap. Consequently, for a given range R, the overlap factor in the reference position is $1/S'_{max}$. We therefore calculate the overlap function $O(R)$ for each R between the minimum range with useful signal and the range in which the full overlap is reached.

4 Results

4.1 Telescope mapping and alignment
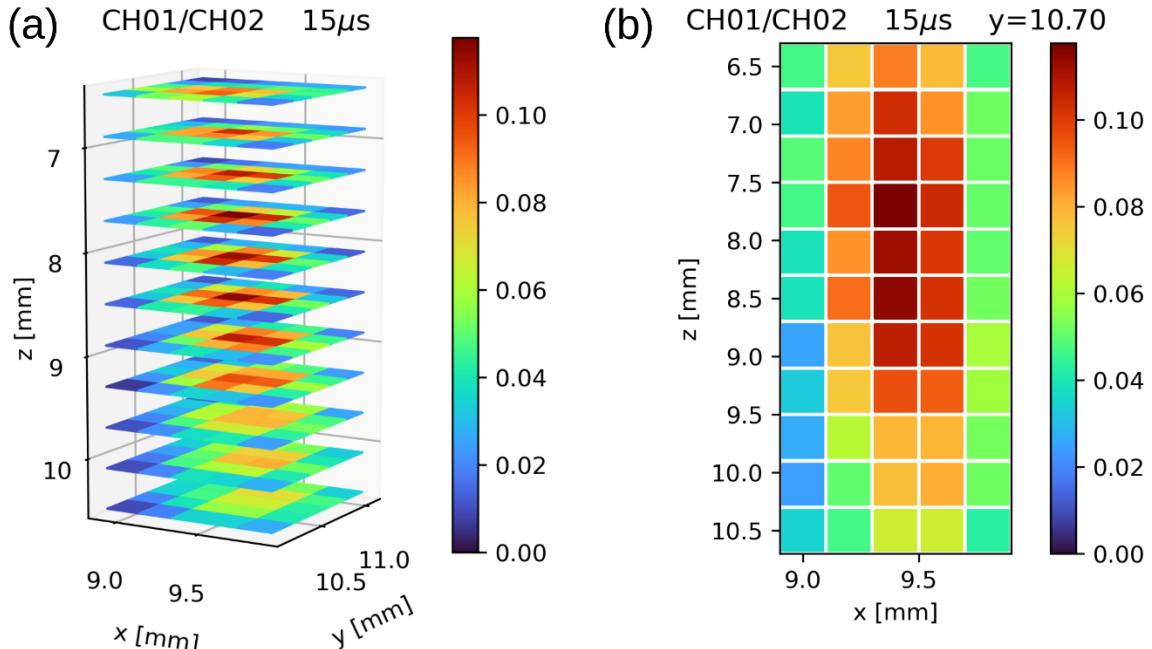
Figure 10: Overall view (a) and *x-z* section (b) of the results of the telescope mapping of the first session (13 January 2021) showing the normalized signal as a function of the *x-y-z* positions at a chosen range (15 µs - 2250 m AGL).

Objective of this telescope mapping session is to optimize the alignment relative to the acquisition of 532 nm elastic backscatter by the 15 cm telescope (CH01). This has been performed in two steps:

- a preliminary mapping with larger range and coarser step in the three dimensions to identify the sub-volume of optimal alignment;
- a mapping in the sub-volume identified in the first mapping, close to the optimal position and with finer resolution.

Two steps are needed due to the time necessary to perform a scan with both large *x-y-z* range and step. The first mapping could be skipped if the system was recently aligned.
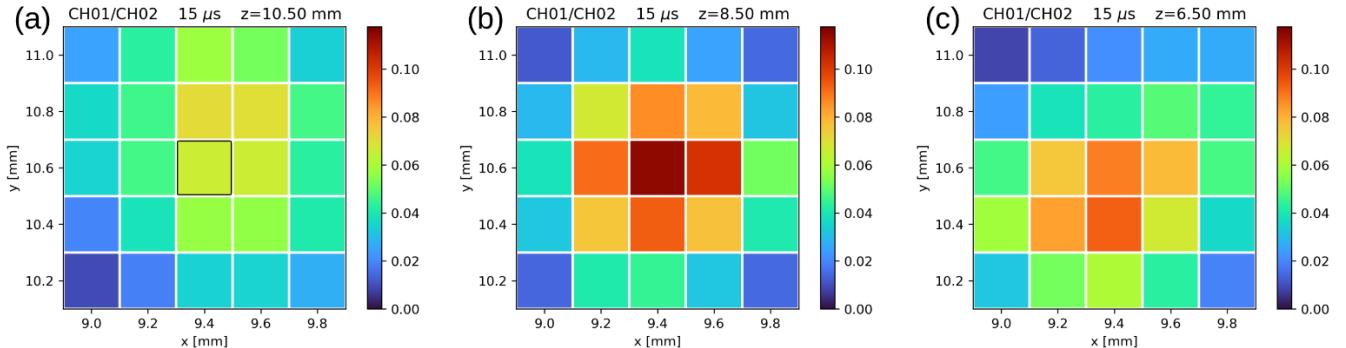
Figure 11: Signal mapping of the first session (13 January 2021) showing the normalized signal for three planes at different *z* positions and chosen range (15 µs - 2250 m AGL). The position derived from the manual alignment is highlighted by the black square.

The two sessions were performed on 13 January 2021 (18:01 - 23:04 UTC) and on 26 January 2021 (17:02-20:01 UTC).

Table 6 reports the characteristics of the performed mapping:

Table 6: Characteristics of the two telescope mapping sessions and the laser mapping session, the channels used for the procedure are highlighted in bold.

Mapping type	telescope	telescope	laser
Time	13 Jan 2021, 18:01-23:04 UTC	26 Jan 2021, 17:02-20:01 UTC	15 Feb 2021, 18:39-19:37 UTC
Mapped telescope / laser beam	4 (15 cm)	4 (15 cm)	532 nm
Starting / reference position x, y, z / Az, Zen [mm]	9.40, 10.60, 10.90	9.40, 10.60, 9.10	7.73, 7.97
Range, step for x-axis / Az-axis [mm]	0.8, 0.2	0.4, 0.1	0.21, 0.03
Range, step for y-axis / Zen-axis [mm]	0.8, 0.2	0.4, 0.1	0.09, 0.01
Range, step z-axis [mm]	4.4, 0.4	2.0, 0.2	
Channels acquired	**1, 2**, 4, 8	**1, 2**, 4, 8	**1, 2**, 4, 8
Single acquisition duration [s]	20	30	30
Bin size [µs]	5.0	0.5	0.5
Total mapping time	2 h 52 min	2 h 59 min	58 min

With these settings, each acquisition for the mapping procedure took about 38 s of which 30 s are the effective acquisition time and 8 s are dedicated to the data transfer and the movement of the motors that can be performed one motor at a time.

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From the results, which are depicted in Fig. 10 and 11, it is clear that the telescope in the manually optimized configuration (x = 9.40 mm, y = 10.50 mm, z = 10.50 mm, highlighted in Fig. 11a), despite being not far from the optimal x-y position, is highly out of focus due to its z position. The overall intensity of the signal in the x-y plane increases changing the z position (Fig. 11b), as the now focused image pass through the diaphragm without being clipped. Moving further in the z axis, the signal starts again to decrease (Fig. 11c). No clear asymmetries in the signal are found. The presumed optimal position resulting from this session is x = 9.40 mm, y = 10.60 mm, z = 8.50 mm.

The slight shift of the image centre (i.e. centre of the area with maximum values) at different z positions is caused by tilted, with respect to the z axis, incoming light rays. Moreover, looking at the uppermost useful range, for x-y positions at the centre of the image the beam and telescope axis (more precisely the FOV axis) should be approximately parallel. Assuming the z axis as vertical, this information can be used to estimate the tilt of the laser beam dividing the x-y shift of the centre of the image by the z displacement, resulting in a tilt of ~50 mrad.
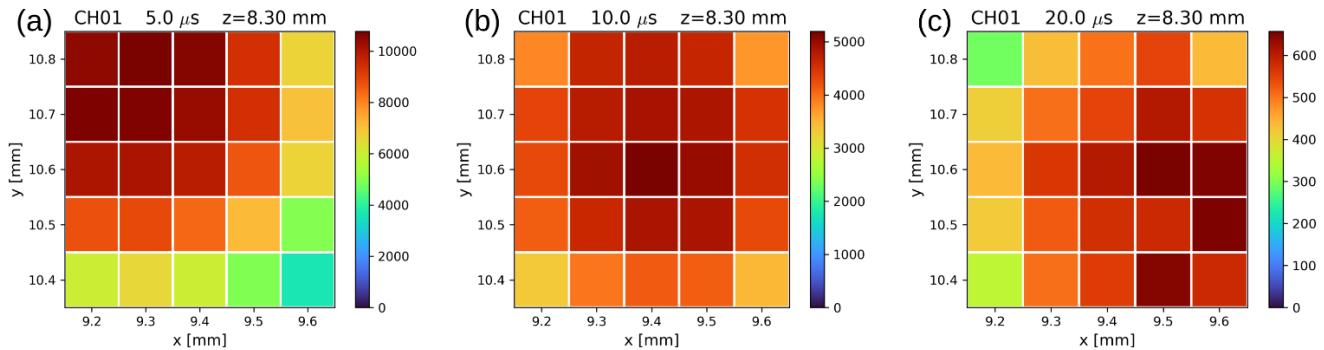
Figure 12: Signal mapping (CH01 photon counting signal) of the second session (26 January 2021) at same z and different ranges (a: 5.0 µs - 750 m, b: 10.0 µs - 1500 m, c: 20.0 µs - 3000 m). Here the signal is not normalized due to the lack of sufficient SNR from the second channel in the lower range (highly incomplete overlap).

The second session was performed with finer steps and centred around the presumed optimal position. In Figure 12 is plotted the signal intensity S at different ranges and fixed z coordinate. In this case, the signal has not been normalized due to highly incomplete overlap of the second channel in the low range. The atmospheric and power variability has been monitored qualitatively with channel 2 measurements at higher ranges. In the x-y plane, as expected, the image shifts at different altitudes. No evident asymmetries are present in the signal map.

Through this session, a definitive and well-aligned position can be selected in the x-y plane as a trade-off between maximizing counts in the lower range (optimizing the signal in the partial overlap range and lowering the full overlap height) and maintaining the beam in the telescope FOV at high ranges.

365 In the *z* coordinate, the optimal position is selected evaluating the normalized signals at medium range around the selected *x* and *y* position. As shown in Fig. 13, the curve has a plateau in which the maximum value is reached (i.e. the image is sufficiently focused and inside the diaphragm). The selection of a position in the higher values portion of the plateau corresponds to a diaphragm position that better captures the signal in the lowermost range (the focus shifts from infinity to lower ranges).

370 Based on the above considerations the derived optimal position is $x = 9.45$ mm, $y = 10.55$ mm, $z = 8.30$ mm.

As mentioned in Sect. 3.1, measuring the angular distance between the selected position and the centre of the image at high ranges (Eq. (3)), the relative tilt between the telescope FOV axis and the laser beam is about 0.3 mrad.
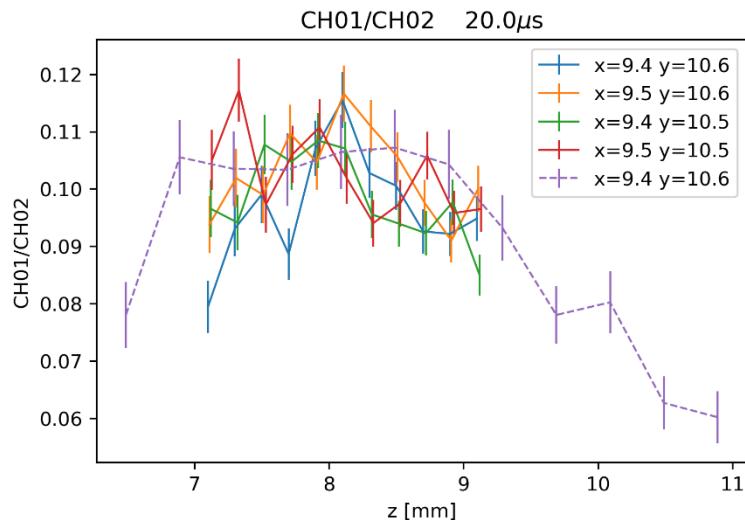
375 **Figure 13: Normalized signal at a chosen range (20 µs - 3000 m) for different x and y positions as a function of *z*, data from both mapping sessions (dashed line for the first session, solid line for the second). A plateau is reached approximately between *z* = 7 mm and *z* = 9 mm. Each colour corresponds to different *x* and *y* positions as indicated in the legend of the plot.**

4.2 Alignment validation

The selected alignment configuration was validated through a telecover test and direct comparison of the signal profiles in the
380 different positions.

The telecover test, described by Freudenthaler et al. (2018), is a quality assurance tool used for lidar system misalignment diagnostic and evaluation of the full overlap range. Lidar profiles taken with different sectors of the telescope aperture are compared to each other. For well-designed and correctly aligned systems, the normalized signals should only show differences in the partial overlap range.

385 Measurements were carried out during a single night session (02 February 2021, 18:55-21:26 UTC). Progressively the following measurements were performed (see Fig. 14): a telecover test in the non-optimized starting position (a), a full

telescope measurement in the same position (b) and one in the optimized position (c), finally a telecover test in the optimized position (d). Standard acquisition times were used (60 s), with an integration time of 10 minutes for each telecover test sector or comparison profile.

390
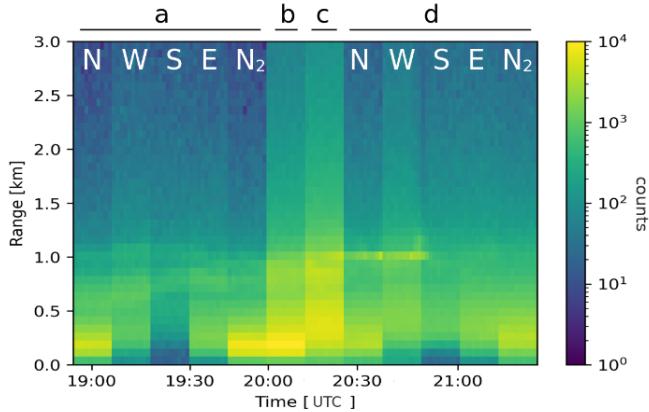
Figure 14: Validation measurement session (02 February 2021). Telecover (a) and full telescope measurement in the non-optimized position (b), and in the optimized position (d and c respectively).

395 **4.2.1 Profile comparison**

Figure 15a shows the direct comparison of the background subtracted signal profiles in the non-optimized starting position and in the optimized position. Higher signal is found in the whole optimized profile (>50% relative normalized difference), confirming the successful alignment procedure, and no signal loss in the high range (Fig. 15b). The negative difference in the lowermost range is well below the full overlap height (i.e. < 500 m) and can be explained considering that the large and less

400 focused image of the non-optimized position can maintain a partial overlap with the telescope FOV for a wider vertical range.

25
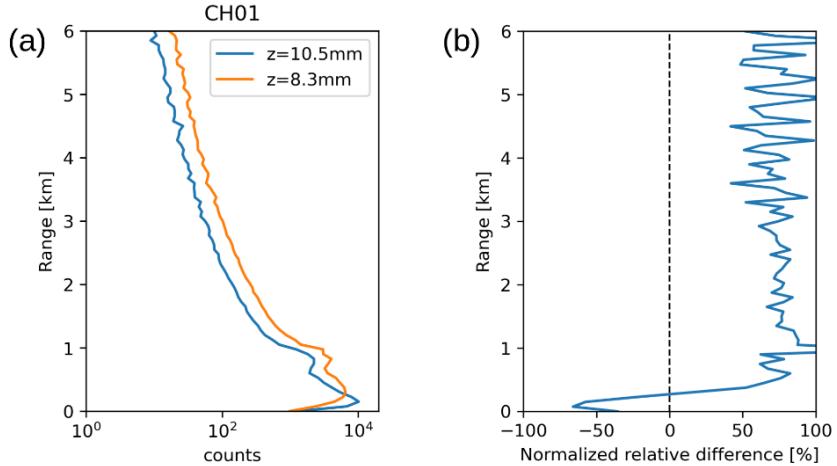
Figure 15: Background subtracted counts (a) and relative difference between the normalized signal CH01/CH02 profiles (b) in the selected position (*x*=9.45 mm *y*=10.55 mm *z*=8.30 mm) and the starting one (*x*=9.40 mm *y*=10.50 mm *z*=10.50 mm).

4.2.2 Telecover

Two telecover tests were conducted: one in the non-optimized starting position (Fig. 16a) and one in the optimized position (Fig. 16b). Figure 16a shows that the height of full overlap is higher than 1500 m, far from the expected modelled value of 501 m (see Table 5). Assuming a negligible impact of mirror imperfections and irregular shape of the laser beam, this has been confirmed to be due to the diaphragm in an out of focus position for the *z* axis. This leads to an image in the aperture plane with a large circle of confusion and non-optimal alignment of the field of view (*x* and *y* axes).

Figure 16b depicts the results in the optimized position. The full overlap height is around 1000 m or less and that the relative difference of the signals in the partial overlap region has decreased. Atmospheric variability and presence of aerosol layers prevent a more precise evaluation of the overlap height using the telecover QA method. As expected, less noise is detected at all ranges due to the increased signal.

26
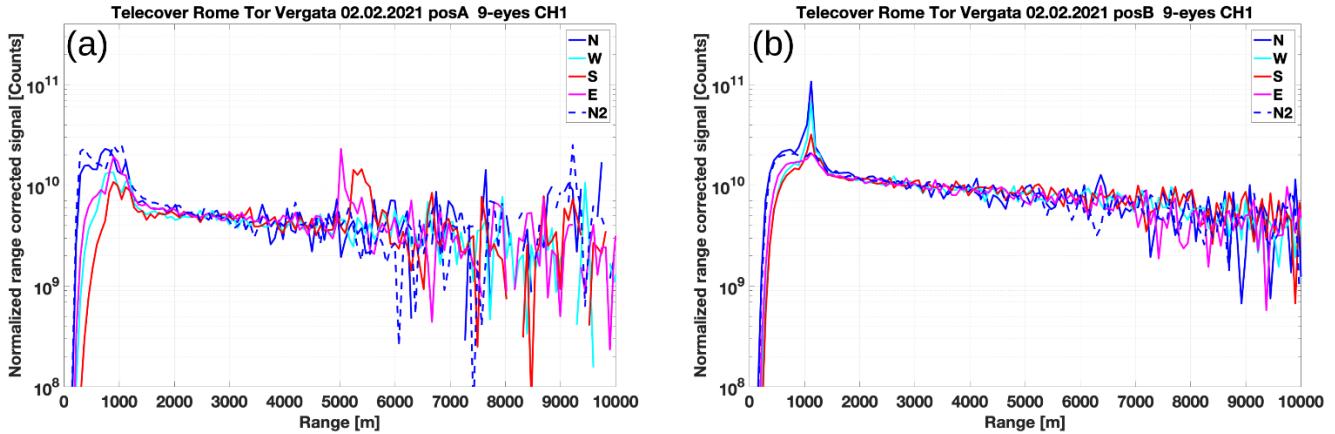
Figure 16: Telecover test results for the positions selected with manual (a) and mapping-based (b) alignment procedures.

## 4.3 Laser mapping and overlap estimation
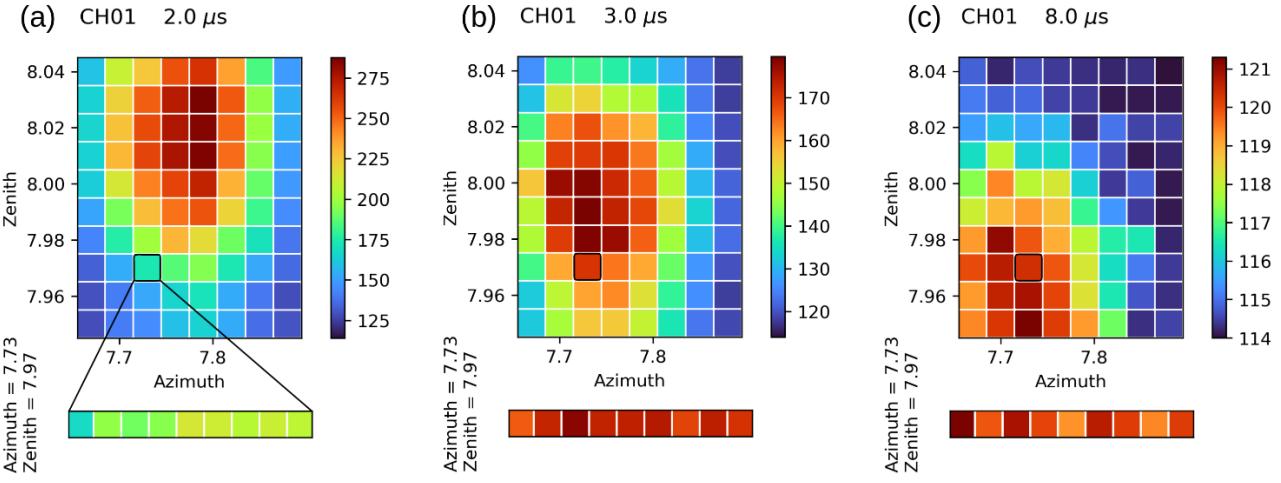
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Once an optimized position has been selected and verified (see Sect. 4.1 and 4.2), a laser beam mapping with the purpose of estimating the overlap function was performed (15 February 2021, 18:39-19:37 UTC). The characteristics of the mapping are reported in Table 6. In Figure 17 the mapped analogue signal at three different ranges is shown. As in the telescope mapping, a range dependent shift of the signal away from the reference position is visible in the lowermost range.

430 From this data, the overlap function using the methodology presented in Sect 3.2 is calculated. The first 5 highest values are used for the calculation of S'_{max} at each range. In order to evaluate the possible impact of dead-time effect in the PC mode (Donovan et al., 1993; Cairo et al., 1996), the analysis was performed also using data acquired in the analogue mode. Figure 18 shows the estimated overlap function from analogue (A) and photon counting (PC) data; the resulting uncertainty is evaluated by propagation of the signal uncertainties. As a reference, Fig. 18 shows also the overlap function computed with an analytical model with uniform beam energy distribution (Stelmaszczyk et al., 2005) and a Monte-Carlo integration of Halldórsson and Langerholc (1978) equations with gaussian beam energy distribution. Both models use the relative inclination of the laser beam estimated via the telescope mapping (see Sect 4.1).
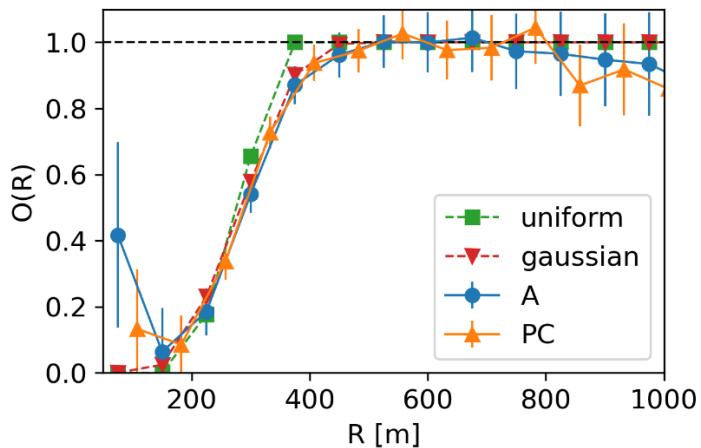
Figure 18: Estimated overlap function using analogue (A) and photon counting (PC) data compared to the overlap function calculated from models with the assumption of a uniform/gaussian beam, diaphragm in the focal plane and tilted beam (0.3 mrad).

The function $O(R)$ reaches unity in the expected range and the experimental results are in agreement with the models. Photon counting data was corrected for trigger delays (Freudenthaler et al., 2018) as described in Appendix A. One evident feature is that after having reached the maximum (at 500-800 m) the values start to slowly decrease. This underestimation of the retrieved overlap function in the high ranges can be explained by the methodology chosen for the maxima selection. In particular, the systematic overestimation of the maxima S'_{max} (due to the shot noise) becomes relevant only above the range of interest (i.e. where $O(R)$ has already reached unity). The difference between the modelled/retrieved full overlap height and the one found via the telecover test could be due to aerosol variability in the latter or slight instabilities of the system beam/telescope alignment and need to be further investigated.

As an example of application, Fig. 19 shows an uncorrected aerosol backscattering profile and the corrected one using the PC-retrieved overlap function applied from 200 to 500 m for channel 1 (11 February 2021, 19:45-20:44 UTC). Both the uncertainty associated to the overlap for the first 4 bins and the retrieval algorithm one have been taken into account for the corrected

profile. Applying the overlap correction allows the extension of the useful range of the aerosol backscattering profile down to
455   200 m.
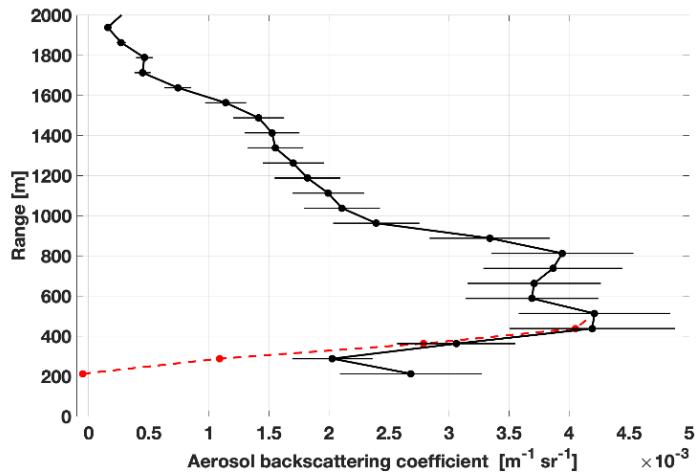
Figure 19: Aerosol backscattering coefficient (11 Feb 2021, 19:45-20:44 UTC), comparison between the overlap-corrected (solid black line) and uncorrected (dashed red line) profile.

460   **5 Summary and conclusions**

Taking advantage of the capability of the RMR "9-eyes" lidar system to electronically control with motors the orientation of the laser beam and the position of the receiving optical system around the focal point of the telescopes, a mapping procedure was developed to characterize the dependency of the acquired signal from the system relative transmitter-receiver geometry. The procedure consists in a set of programs controlling both the signal acquisition as well as the motor movements. The
465   developed approach also includes solutions to account for atmospheric and laser power variability likely to occur during the mapping sessions. The mapping procedure allows applications such as the optimization of the telescope/beam alignment and the estimation of the overlap function. It should be noted that the results of the procedure can also be used to diagnose the overall optical alignment and verify the adopted assumptions.

To optimize the RMR system for the objectives of ACTRIS/EARLINET network (e.g. the description of aerosol optical
470   properties in the lower troposphere and PBL) this procedure was applied to the single combination of telescope and laser beam (15 cm telescope, 532 nm) of the system that better sense this region of the atmosphere.

Another output of the procedure was the estimation of the absolute tilt of the laser beam with respect to the z axis (~50 mrad) and the relative tilt with respect to the FOV axis (~0.3 mrad). Such values are fundamental to model the dependency of the signal from the system geometry.

475 The presented methodology was tested to obtain an optimized laser-telescope configuration starting from a non-optimized one. The mapping procedure diagnosed an out of focus image and identified the correct z position. As a result, the signal intensity increased in the whole channel 1 profile with respect to the previous configuration. The effectiveness of the procedure was verified comparing the results of a telecover test before and after the alignment. The new configuration resulted in a lower full overlap height (from 1500 m to less than 1000 m).

480 Once an optimized position has been selected and verified, a laser beam mapping with the purpose of estimating the overlap function was performed. The retrieved function was compared to the ones modelled using as input the parameters obtained from the procedure showing good agreement. Correcting the lidar profiles of channel 1 with this function, allows extending the useful range down to 200 m.

The developed mapping procedure will be applied to the remaining channels in order to characterize each transmitter-receiver

485 combination. Based on the retrieved information it will be possible to define a set of configurations aimed to satisfy the different scientific objectives (e.g. PBL, upper troposphere – lower stratosphere).A simplified mapping procedure can be used to complement the standard EARLINET quality assurance tests. For example, a protocol coupling telecover tests and mapping sessions is currently implemented in the RMR system. Monthly mappings are performed to monitor and optimize the alignment and to estimate the overlap function, whereas periodically required telecover tests (e.g. 1-2 times per year) check and attest the

490 obtained alignment and identify the minimum height with full overlap.

Besides the applications presented in this study, a similar approach could be adapted also to lidar systems with different hardware capabilities to provide essential information about their transmitter-receiver geometry that is needed for a complete characterization of the received signal.

Appendix A

495 Lidar photon counting data range was corrected for trigger delay relatively to the analogue data range using the following procedure. Assuming a linear relation between photon counting and analogue data (i.e. no saturation) and after correcting the latter for voltage offset and dividing it by the proportionality constant between the two, it is possible to write the following equations:

$$A = \frac{f(R)}{R^2} \tag{A1}$$

500 $$PC = \frac{f(R-\Delta)}{(R-\Delta)^2} \tag{A2}$$

Where A is the corrected analogue signal, PC is the photon counting signal, $f(R)$ is a function encompassing all the lidar equation terms apart from the inverse square law, and Δ is the spatial delay between analogue and photon counting sampling ranges.

For low R a limited dependence of the function f on R variations with respect to the inverse square law can be assumed. This is true especially for the first bins where limited or no overlap is present and most of the signal comes from laser secondary reflections and multiple scattering:

$$f(R) \sim f(R - \varDelta) \tag{A3}$$

Under this assumption, the ratio between the analogue and photocounting signals is:

$$\frac{A}{PC}(R) = \frac{(R - \varDelta)^2}{R^2} \tag{A4}$$

from which it is possible to derive the difference $\varDelta$ as a function of R:

$$\varDelta(R) = -R \left(\sqrt{\frac{A}{PC}} - 1 \right) \tag{A5}$$

Figure A1a depicts the retrieved spatial delay computed with Equation (A5) using laser mapping data from Sect. 4.3. The assumptions hold for the first two bins from which a delay of ~25 m can be derived using an average value. For higher ranges, the overlap function dependency from R begins to be relevant, preventing the computation of the delay (i.e. the assumption in Eq. (A3) is not valid anymore). This dependency is not definite and partially randomized due to the variable emitting geometry and resulting overlap function of the mapping lidar profiles. Once a delay is retrieved the A/PC ratio can be plotted and compared with the range function $(R- \varDelta)^2/R^2$ (Fig. A1b). As shown in Figure A1b, the computed range function well represents the normalized ratio.
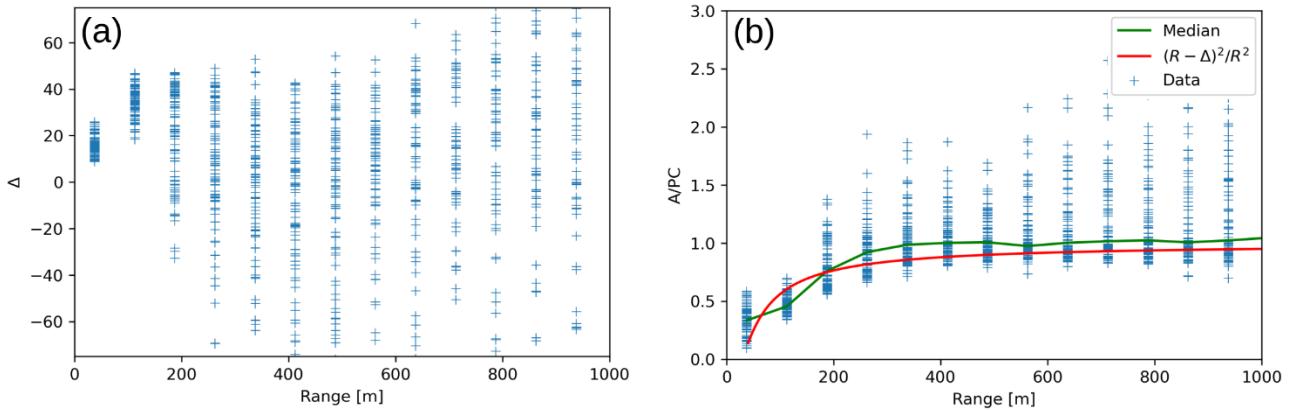

Figure A1: Spatial delay (a) and ratio A/PC (b) as a function of range.

Author contribution

MDP, GLL, and DD conceived the concept of this study. MDP, GLL, and DD performed the lidar measurements. MDP
525   developed the presented methods, processed the data and carried out the analysis. MDP, GLL, and DD contributed to the interpretation, the validation and the visualization of the results. MDP wrote the original draft with input from all other co-authors. All co-authors provided the review and the editing of the manuscript.

Competing interests

The authors declare that they have no known competing financial interests or personal relationships that could have appeared
530   to influence the work reported in this paper.

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