

Characterization of tandem aerosol classifiers for selecting particles: implication for eliminating multiple charging effect

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Abstract. Accurate particle classification plays a vital role in aerosol studies. Differential mobility analyzer (DMA), centrifugal particle mass analyzer (CPMA) and aerodynamic aerosol classifier (AAC) are commonly used to select particles with a specific size or mass. However, multiple charging effects cannot be entirely avoided ~~when either~~ using ~~either~~ individual techniques or ~~using~~ tandem systems such as DMA-CPMA, especially when selecting soot particles with fractal structures. In this study, we demonstrate the transfer functions of ~~the~~ DMA-CPMA and DMA-AAC ~~both in a static configurations systems.~~ We propose an equation that constrains the resolutions of DMA and CPMA to eliminate the multiple charging effect when selecting particles with a certain mass-mobility relationship using the DMA-CPMA system. The equation for the DMA-AAC system is also derived. ~~as well as the potential multiple charging effect.~~ Our results show that the ability to remove multiply charged particles mainly depends on ~~the~~ particles morphology and ~~instruments setups resolutions of the~~ DMA and CPMA ~~DMA-CPMA system~~. Using measurements from soot experiments and literature data, a general trend in the appearance of multiple charging effect with decreasing size when selecting aspherical particles ~~was is~~ observed. Otherwise, our results indicated that the ability of ~~the~~ DMA-AAC ~~in a static configuration~~ to ~~resolve~~eliminate particles with multiple charges is mainly related to the resolutions of classifiers. In most cases, ~~the~~ DMA-AAC ~~in a static configuration~~ can eliminate multiple charging effect regardless of the particle morphology, ~~while particles with multiple charges can be selected when decreasing resolutions of DMA and AAC but multiply charged particles will be selected when decreasing the resolution of the DMA or AAC.~~ We propose that ~~the potential influence of multiple charging effect should be taken into account~~considered when using ~~the~~ DMA-CPMA or DMA-AAC system in estimating size- and mass- resolved optical properties in ~~the~~ field and lab experiments.

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1 Introduction

Atmospheric aerosol particles span a wide size range from 1 nm to > 100 μm . A significant size dependence of aerosol physicochemical properties has been widely reported. Particle size can strongly alter the hygroscopic behavior (Biskos et al., 2006), phase state (Cheng et al., 2015) and cloud-nucleating ability (Dusek et al., 2006) of aerosol nanoparticles, indicating the importance of particle size when assessing the climate effect. Hence, accurate particle classification is essential to investigate the size dependence behavior of aerosol particles.

At present, particles are generally classified by either size or mass in atmospheric aerosol studies. A Differential mobility analyzer (DMA) is the most commonly used size classifier, which selects particles based on the electrical mobility (Knutson and Whitby, 1975; Park et al., 2008; Stolzenburg and McMurry, 2008; Swietlicki et al., 2008; Wiedensohler et al., 2012). A Particle mass analyzer (PMA) includes the aerosol particle mass analyzer (APM) and the centrifugal particle mass analyzer (CPMA), both of which classify particles based on their mass-to-charge ratio (Ehara et al., 1996; Olfert and Collings, 2005). However, particles must be precharged when classified by the DMA or PMA because DMA and PMA classify particles based on electrical mobility and mass-to-charge ratio, resulting in that particles with higher-order charges and identical apparent mobility or mass-to-charge ratio will be being selected simultaneously, which are referred to as the multiple charging effect. This may introduce uncertainty in the subsequent characterization. Radney et al. (2013) demonstrated that although the single-charged particles account for the highest number fraction (46.3%) of the DMA-classified particles (200 nm), while their contributions to the total mass concentration and extinction are insignificant (10.8% and 7.96%, respectively). Thus, the reported extinction of particles with a certain diameter was has been greatly overestimated due to the multiple charging effect.

Previous studies (Shiraiwa et al., 2010; Rissler et al., 2013; Johnson et al., 2014; Johnson et al., 2021) tried to utilize the combination of size and mass classifiers, like such as DMA-APM or DMA-CPMA systems, to obtain singly charged particles. Theoretically, the ability of DMA-APM to eliminate multiply charged particles is governed by the particles morphology and setups of DMA-APM (Kuwata, 2015). This conclusion implies that it can hardly be achieved that all the multiply charged particles are cannot be effectively excluded for aspherical particles, especially for soot particles. Radney and Zangmeister (2016) conducted investigated the limitation of DMA-APM with three types of particles (polystyrene Latex (PSL) spheres (PSL), ammonium sulfate (AS) and soot particles). Their results demonstrated that a DMA-APM can resolve multiply charged particles for spherical particles (PSL and AS particles), but it failed for aspherical soot particles. Multiply charged soot particles led to over 110% errors in retrieving the mass specific extinction cross section.

In contrast to DMA and PMA, an aerodynamic aerosol classifier (AAC) is a novel instrument which that selects the aerodynamic equivalent diameter of aerosol particles based on their relaxation time. The advantage of utilizing an AAC is that no charging process is needed in particle classification compared with the aforementioned classifiers; hence, the multiple charging effects can be avoided (Tavakoli and Olfert, 2013).

However, the selected particles are not monodispersed in mobility diameter when an AAC is used to select aspherical particles (Kazemimanesh et al., 2022).

Morphology information, such as effective density (ρ_{eff}), mass-mobility exponent (D_{fm}) and dynamic shape factor (χ), can be inferred using the tandem systems of DMA-PMA system (Park et al., 2003; Zhang et al., 2008; Rissler et al., 2013; Pei et al., 2018; Zangmeister et al., 2018), DMA-AAC (Tavakoli and Olfert, 2014) and AAC-CPMA systems (Johnson et al., 2018), respectively. The derived ρ_{eff} and χ depend upon the combination of used instruments used, while nonphysical values of χ (<1) and ρ_{eff} ($>\text{bulk}$) for aspherical particles were can be determined by the AAC-APM (Yao et al., 2020) and AAC-CPMA (Kazemimanesh et al., 2022).

The theoretical transfer functions of individual classifiers (DMA, CPMA and AAC) and the DMA-APM system have been previously discussed (Knutson and Whitby, 1975; Ehara et al., 1996; Olfert and Collings, 2005; Stolzenburg and McMurry, 2008; Tavakoli and Olfert, 2013). In this study, we focus on a DMA-CPMA and DMA-AAC in static configurations to eliminate multiply charged particles. The DMA-CPMA and DMA-AAC systems mentioned below refer to the tandems of a DMA and CPMA or a DMA and AAC in a static configuration, respectively. We calculated the transfer functions of DMA-AAC and DMA-CPMA systematically. Combined with soot experiments, we demonstrated that multiple charging effects may still exist after DMA-CPMA classification when selecting aspherical particles, and evaluated the light absorption of selected particles with different charging states using Mie theory. Furthermore, we proposed the operating condition for DMA-CPMA and DMA-AAC to eliminate the multiply charged particles in the future studies. Our results suggest that the size- and mass-resolved optical properties may be overestimated for small soot particles when using DMA-CPMA system, which will lower the accuracy of predicting accuracy of the fresh soot climate effect. In Sect. 3.1, we calculate the transfer functions of the DMA-CPMA and DMA-AAC utilizing the literature data of soot particles from Pei et al. (2018). In Sect. 3.2, we measure the multiple charging effect of the DMA-CPMA using laboratory-generated soot particles, and the bias of optical measurement induced by multiply charged particles is evaluated in Sect. 3.3.

2 Theory and experiment

2.1 Transfer function for individual aerosol classifier

DMA

The DMA, consisting of two coaxial electrodes, classifies particles based upon electrical mobility Z_p (Knutson and Whitby, 1975), which can be calculated as follows:

$$Z_p = qB = \frac{neCc(d_{mp})}{3\pi\mu d_{mp}}, \quad (1)$$

where q is the particle charge, n is the number of particle-elementary charges, B is the mobility of particle, e is the elemental charge, μ is the viscosity of the air, and $Cc(d_p)$ is the Cunningham slip correction factor. When the aerosol inlet flow rate equals to the aerosol sampling outlet flow rate, the Z_p^* selected by the DMA is defined as

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$$Z_p^* = \frac{Q_{sh}}{2\pi V_{DMA} L_{DMA}} \ln\left(\frac{r_{2,DMA}}{r_{1,DMA}}\right), \quad (2)$$

where Q_{sh} is the sheath flow rate, V_{DMA} is the voltage between the two electrodes, L_{DMA} is the length of the DMA, and $r_{1,DMA}$ and $r_{2,DMA}$ are the inner and outer radii of the DMA, respectively. Assuming that the aerosol inlet and aerosol sampling flow rates are equal, the transfer function of the DMA can be expressed as follows when particle diffusion is negligible (Knutson and Whitby, 1975; Stolzenburg and McMurry, 2008),

$$\Omega(Z_p, \beta_{DMA}) = \frac{1}{2\beta_{DMA}} [|Z_p - (1 + \beta_{DMA})| + |Z_p - (1 - \beta_{DMA})| - 2|Z_p - 1|], \quad (3)$$

Where, $\tilde{Z}_p = Z_p/Z_p^*$, $\beta_{DMA} = Q_s/Q_{sh}$, and Q_s is the sample flow rate. The limiting electrical mobilities that DMA can select are $(1 \pm \beta_{DMA})Z_p^*$. The maximum and minimum values of d_m for particles with n charges can be derived and denote as $d_{m,n,max}$ and $d_{m,n,min}$, respectively. The transfer function is an isosceles triangle with value of 1 at Z_p^* and going to 0 at $(1 \pm \beta_{DMA})Z_p^*$. It translates to asymmetric in d_m since the relationship between d_m and Z_p is nonlinear.

CPMA

The construction of the CPMA is similar to the APM, but its inner cylinder rotates faster than the outer one cylinder to create a stable system of forces (Olfert and Collings, 2005). In the CPMA, the equation of particles motion is expressed as

$$\frac{m}{\tau} \frac{dr}{dt} = \frac{mv_\theta(r)^2}{r} - \frac{qV_{CPMA}}{r \ln\left(\frac{r_{2,CPMA}}{r_{1,CPMA}}\right)}, \quad (4)$$

and the trajectory equation is

$$\frac{dr}{dz} = \frac{dr}{dt} \left(\frac{dz}{dt} \right)^{-1} = \frac{c_r}{v_z}, \quad (5)$$

where τ is the relaxation time, m is the mass of the particle, t is time, V is the voltage difference between the two electrodes, and $r_{1,CPMA}$ and $r_{2,CPMA}$ are the radii of inner and outer electrodes, respectively. c_r is the particle migration velocity, v_z is the axial flow distribution and v_θ is the velocity profile in the angular direction,

$$v_\theta = \omega_1 \frac{\hat{r}^2 - \hat{\omega}}{\hat{r}^2 - 1} r + \omega_1 r_{1,CPMA}^2 \frac{\hat{\omega} - 1}{\hat{r}^2 - 1} \frac{1}{r} = \alpha r + \frac{\beta}{r}, \quad (6)$$

where $\hat{\omega} = \omega_2/\omega_1$ is the ratio of the rotational speed of the outer electrode to the inner electrode and ω_1 and ω_2 are the rotational speeds of the inner and outer electrodes, respectively. \hat{r} is the ratio of the inner and outer radii.

Sipkens et al. (2019) gave the presented methods to calculate the transfer function of the CPMA. They proposed-considered that the Taylor series expansion at the about the center of the gap ($r_c = (r_{2,CPMA} + r_{1,CPMA})/2$) instead of the equilibrium radius to avoid problems with the scenario that in which the equilibrium radius does not exist. This method is much simpler and more robust. In this case, the particle migration velocity in the radial direction is

$$c_r \approx C_3 + C_4(r - r_c), \quad (7)$$

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$$C_3 = \tau \left(\alpha^2 r_c + \frac{2\alpha\beta}{r_c} + \frac{\beta^2}{r_c^3} - \frac{C_0}{mr_c} \right), \quad (8)$$

$$C_4 = \tau \left(\alpha^2 - \frac{2\alpha\beta}{r_c} - \frac{3\beta^2}{r_c^3} + \frac{C_0}{mr_c^2} \right), \quad (9)$$

$$C_0 = \frac{qV_{CPMA}}{\ln(r_{2_CPMA}/r_{1_CPMA})}, \quad (10)$$

Assuming a plug flow, the transfer function should-would be

$$\Omega = \frac{r_b - r_a}{2\delta}, \quad (11)$$

where $\delta = (r_{2_CPMA} - r_{1_CPMA})/2$ is the half width of the gap between the two electrodes, and

$$r_a = \min \{ r_{2_CPMA}, \max \{ r_{1_CPMA}, G_0(r_{1_CPMA}) \} \}, \quad (12)$$

$$r_b = \min \{ r_{2_CPMA}, \max \{ r_{1_CPMA}, G_0(r_{2_CPMA}) \} \}, \quad (13)$$

$$G_0(r_L) = r_c + \left(r_L - r_c + \frac{C_3}{C_4} \right) \exp(-C_4 L \bar{v}) - \frac{C_3}{C_4}, \quad (14)$$

where $G_0(r)$ is the operator used to map the final radial position of the particle to its position at the inlet and. \bar{v} is average flow velocity.

Reavell et al. (2011) calculated the resolution of CPMA assuming that the gap between two electrodes is narrow enough that the variation of force in the gap can be ignored. The limiting mass can be calculated by

$$m_{n,min}^{n,max} - n \cdot m_1 = \pm \frac{Q_{CPMA}}{2\pi B_{n,min}^{n,max} r_{CPMA}^2 \omega^2}, \quad (15)$$

where ω is the equivalent rotational speed calculated by $\omega = \alpha + \frac{\beta}{r_c}$, m_1 is the nominal mass that the CPMA can select, $m_{n,min}^{n,max}$ and $B_{n,min}^{n,max}$ are the maximum and minimum mass and corresponding mobility of particles bearing number of elementary charges of n with single charge that the CPMA can select, respectively.

Further details can be found in Reavell et al. (2011) and Sipkens et al. (2019).

AAC

The AAC classifies particle based on relaxation time, which is defined by

$$\tau = Bm = \frac{Cc(d_{ae})\rho_0 d_{ae}^2}{18\mu}, \quad (16)$$

where μ is the viscosity of air. $Cc(d_{ae})$ is the slip correction factor. ρ_0 is the standard density with a value of 1 g/cm³ (Johnson et al. 2018). When the aerosol inlet flow rate equals to the aerosol sampling outlet flow rate, it can be expressed as (Tavakoli and Olfert, 2013)

$$\Omega = \frac{1}{2\beta_{AAC}} [|\tilde{\tau} - (1 - \beta_{AAC})| + |\tilde{\tau} - (1 + \beta_{AAC})| - 2|\tilde{\tau} - 1|], \quad (17)$$

τ^* is the nominated-nominal relaxation time, which is classified by the AAC,

$$\tau^* = \frac{2Q_{sh}}{\pi\omega^2(r_{1_AAC} + r_{2_AAC})^2 L}, \quad (18)$$

where $\beta_{AAC} = \frac{Q_a}{Q_{sh}}$, $\tilde{\tau} = \frac{\tau}{\tau^*}$, r_{1_AAC} and r_{2_AAC} are the inner and outer radii of the AAC, respectively. The limiting τ that AAC can select are $(1 \pm \beta_{AAC}) \cdot \tau^*$. The maximum and minimum values of d_{ae} can be derived and denote as $d_{ae,max}$ and $d_{ae,min}$, respectively.

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2.2 Experimental setup

A schematic of the experimental setup is illustrated in Fig. 1. Soot particles were generated by a miniature inverted soot generator (Argonaut Scientific Ltd., Canada) with thea propane flow of 74.8 SCPM and thean air flow rate of 12 SLPM. Although this operation setting is not in the open-tip flame regime, the flame is open-tip consistent with the Fig.2d in Moallemi et al.(2019). Detailed aerosol generation methods can be found in Kazemimanes et al. (2019b) and Moallemi et al. (2019). The poly-dispersed aerosols were dried to a relative humidity of <20% by a silica dryer, and then were-passed through a soft X-ray neutralizer (Model 3088, TSI, Inc., USA). Five mobility diameters (80 nm, 100 nm, 150 nm, 200 nm and 250 nm) of soot particles were selected with the DMA (Model 3081, TSI Inc., USA, $Q_{sh}/Q_a = 10$). For the soot characterization, the monodisperse aerosol flow was switched between two parallel lines and fed into the CPMA (Cambustion Ltd., UK) and AAC (Cambustion, Ltd., UK, $Q_{sh}/Q_a = 10$); respectively, meanwhile, the condensation particle counter (CPC, Model 3756, TSI, Inc., USA, 0.3 L min^{-1}) was switch between CPMA and AAC. The particles mass (m) and aerodynamic diameter (d_{ae}) were determined by the stepping-scanning mode of the CPMA and AAC while the condensation particle counter (CPC, Model 3756, TSI, Inc., USA)CPC recorded their corresponding number concentration at each setpoint, respectively. For each d_m , the m and d_{ae} distributions were measured three times, respectively. Between measurement of each d_m , the CPC was used behind the DMA and the number size distribution of the generated soot particles was measured by SMPS to ensure the generated soot particles did not change during the whole experiment. The m and d_{ae} distributions were measured and fitted to log-normal distribution, thus the mode m and d_{ae} for the mobility-selected particles were determined. The equation of log-normal distribution used in this study is expressed as,

$$N(d_p) = \frac{N_0}{\sqrt{2\pi}\ln\sigma} \exp\left(-\frac{(\ln(d_p) - \ln(\mu))^2}{2(\ln\sigma)^2}\right), \quad (19)$$

where the σ is the geometric standard deviation and μ is the geometric mean.

The CPMA and AAC were calibrated with certified PSL spheres (Thermo, USA) with sizes of 70 nm, 150 nm and 303 nm before the measurement. The measured m and d_{ae} were compared to m_{PSL} and $d_{ae, PSL}$ which were calculated with the nominal diameter and density of PSL (1050 kg m^{-3}). The deviations between measured m and m_{PSL} or measured d_{ae} and $d_{ae, PSL}$ were 2.75% and 5.14%, respectively. In order to quantify the multiple charging effect of particles selected by DMA-CPMA system, In order to quantify the multiple charging effect of particles selected by DMA-CPMA system, firstly the soot particles were initially selected by the DMA-CPMA at different d_m and the corresponding m . Then the d_{ae} distribution of twice classified mobility and mass selected particles was obtained by stepping the AAC rotation speed of the cylinder with simultaneous measurement of the particle concentration at the AAC outlet using a CPC (Fig. 1b).

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3 Results and discussion

3.1 Transfer function of the tandem system

The DMA, PMA and AAC select particles based on the electrical diameter, mass and aerodynamic diameter, respectively. These properties can be connected as follows (Decarlo et al. 2004)

$$\frac{Cc(d_{ae})\rho_0 d_{ae}^3}{6} = \frac{Cc(d_m)\rho_{eff} d_m^3}{6} = m \frac{Cc(d_m)}{\pi d_m}, \quad (1920)$$

The transfer function of DMA-APM has been well documented, ~~which and~~ can be found in Kuwata (2015). The convolution of transfer functions of DMA-CPMA and DMA-AAC were calculated by the following equations.

$$\Phi_{DMA-CPMA} = \Omega_{CPMA} \Omega_{DMA}, \quad (2021)$$

$$\Phi_{DMA-AAC} = \Omega_{DMA} \Omega_{AAC}, \quad (2422)$$

where Φ and Ω are the transfer functions of each classification system expressed by subscript. In the following discussion, we explain the transfer functions of DMA-CPMA and DMA-AAC utilizing the literature data of soot particles (Pei et al., 2018). The d_m and m of the representative particles are 100 nm and 0.33 fg, respectively, and the corresponding d_{ae} is 68.3 nm according to Eq. (2049). In the calculation, the following parameter set was employed: $d_m = 80$ nm, $Q_{DMA} = 0.3$ L min⁻¹, $\beta_{DMA} = 0.1$, $m = 0.16$ fg, $Q_{CPMA} = 0.3$ L min⁻¹, $R_m = 8$, $d_{ae} = 68.3$ nm, $Q_{AAC} = 0.3$ L min⁻¹, $\beta_{AAC} = 0.1$. The transfer functions of DMA-CPMA and DMA-AAC were solved iteratively using logarithmically spaced d_m , m and d_{ae} , which included 600 points, respectively. The ranges of d_m , m and d_{ae} used in the calculations were from $<d_{m1,min}$ to $>d_{m2,max}$, from $<m_{1,min}$ to $>m_{2,max}$, from $<d_{ae,min}$ to $>d_{ae,max}$, respectively. The dimensions of individual classifiers are summarized in Table 1.

DMA-CPMA

DMA-CPMA transfer function was calculated in the $\log(d_m)$ - $\log(m)$ space, as shown in Fig. 2. In the $\log(d_m)$ - $\log(m)$ space, the mass-mobility relationship is

$$m = \phi k_f (d_m/nm)^{D_{fm}}, \quad (2223)$$

$$\log(m) = D_{fm} \log(d_m/nm) + \log(k\phi_f), \quad (2324)$$

In theory, D_{fm} equals ~~to~~ 3 for spherical particles and smaller than 3 for aspherical particles. In the $\log(d_m)$ - $\log(m)$ space, the relationship of m and d_m is linear, with the slope expressed as the mass-mobility exponent (D_{fm}) and the intercept representing the pre-exponential factor ($k\phi_f$). Under this specific operation condition, no overlap was observed between the spherical particles population (black line) and the classification region for doubly charged particles, implying that only the singly charged particles were selected. ~~However,~~ ~~f~~For aspherical particles with $D_{fm} < 3$, such as soot particles with aggregate structures, the particles population may overlap the doubly charged region when the slope (D_{fm}) is small enough; ~~if~~ however, the combination of DMA and CPMA is generally used to avoid the multiple charge effect in soot studies. The reported D_{fm} values are typically in the range of 2.2-2.4 for fresh soot particles (Rissler et al., 2013) and diesel soot particles (Park et al., 2003). In the exemplary case (Pei et al., 2018), the derived D_{fm} of premixed flame-generated

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soot particles was 2.28, resulting in the particles population always ~~goes going~~ through the transfer area of doubly charged particles. This implies that the performance of ~~the~~ DMA-CPMA to eliminate multiplye-charged particles to a certain extent depends on the particle morphology.

The DMA-CPMA system can eliminate the multiply charged particles only if the D_{fm} of particles is larger than the slope of a line connecting $(d_m, m) = (d_{m2,min}, m_{2,max})(d_{m1}, m_1)$ (as PP_0 shown in Fig. 2). Since ~~the~~ CPMA is used downstream of the DMA, the value of ~~the~~ mass limit of particles with a certain mobility of B can be expressed as follows according to Eq. (15) ~~assuming that all the classified particles have the same mobility~~.

$$m_{n,min}^{n,max} = n \cdot m_1 \pm \frac{Q_{CPMA}}{2\pi B_{n,min}^{n,max} L_{CPMA} r_c^2 \omega^2}, \quad (2425)$$

where $m_{n,min}^{n,max}$ ~~and $B_{n,min}^{n,max}$ are~~ is the maximum ~~and or~~ minimum particle mass ~~and mechanical mobility of~~ particles with the mobility of B which ~~that~~ would be selected by CPMA ~~and DMA, respectively~~. The subscript n is charge quantity. Accordingly, the ideal condition to completely eliminate the multiply charged particles is

$$D_{fm} > PP_0 = \frac{\log(m_{2,max}/m_1)}{\log(d_{m2,min}/d_{m1})} = \frac{\log(2 + \frac{3Q_{CPMA} + d_{m1}}{(1-\beta_{DMA})L_{CPMA}r_c^2\omega^2m_1Cc(d_{m1})})}{\log(\frac{2}{(1-\beta_{DMA})Cc(d_{m1})})},$$

$$D_{fm} > PP_0 = \frac{\log(m_{2,max}/m_1)}{\log(d_{m2,min}/d_{m1})} = \frac{\log(2 + \frac{1}{R_m(1+\beta_{DMA})})}{\log(\frac{2}{(1+\beta_{DMA})Cc(d_{m1})})} \quad (2526)$$

The ability of ~~the~~ DMA-CPMA to eliminate multiply charged particles depends on the selected d_m , m and resolutions of both ~~the~~ DMA and CPMA. The Eq. (2526) gives instructions in actual operation to eliminate multiplye-y charged particles. When selecting particles of certain d_m and m , ~~the smaller by decreasing~~ Q_{CPMA} , ~~as well as larger or increasing~~ ω and β_{DMA} ~~are necessary to reduce the potential of multiply charged particles i.e. by increasing the resolution of the measurement, the potential of multiply charged particles is reduced~~. Thus, the key to ~~evaluate-evaluating~~ whether there is multiple charging effect lies ~~on-in the~~ particle morphology (D_{fm}) and the slope of PP_0 derived from the actual condition. Compared with ~~the~~ DMA-CPMA, the selection of ~~the~~ DMA-APM is more susceptible to multiple charging effect. According to the theoretical calculation described in Kuwata (2015), the slope of PP_0 of 3.55 was derived when ~~the~~ DMA-APM selects the same example soot particles ~~from~~ [Pei et al \(2018\)](#) (d_m of 100 nm and m of 0.33 fg) with ~~a~~ D_{fm} of 2.28, indicating that the DMA-APM is more subjected to the multiple charging effect.

~~Besides-In addition to~~ the instruments setups, ~~the~~ particles morphology is also crucial for ~~the~~ DMA-CPMA. Here we simulate the critical slope of PP_0 when selecting different d_m and m under the common selecting conditions ($\beta_{DMA} = 0.1$, $Q_{CPMA} = 0.3 \text{ L min}^{-1}$, $R_m = 8$), which is ~~shown-represented as contour lines~~ in Fig. 3 ~~(A black and white version is shown as Fig. S4)~~. Under ~~this-these~~ selecting conditions, ~~the~~ DMA-CPMA can select monodispersed particles when the D_{fm} of ~~the~~ particles is larger than the ~~critical~~ slope of PP_0 ~~which is represented as background color~~. When selecting small aspherical particles or particles with extremely low density, the slope of PP_0 is relatively higher, ~~and~~ ~~the~~ DMA-CPMA classification is sensitive to multiple

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charging effect. As shown in Fig. 3, ~~the~~ d_m , m and ~~the~~ corresponding D_{fm} were taken from ~~the~~ literature (Park et al., 2003; Rissler et al., 2013; Tavakoli et al., 2014; Ait Ali Yahia et al., 2017; Dastanpour et al., 2017; Forestieri et al., 2018; Pei et al., 2018; Kazemimanesh et al., 2019a). Generally, ~~for soot particles with D_{fm} of 2.2–2.4~~, multiple charging effect can be avoided for ~~the~~ DMA-CPMA ~~when~~ selecting soot particles with ~~mobility~~ diameter larger than 200 nm-, while ~~it~~ fails to eliminate multiply charged particles when selecting small soot particles. ~~The~~ ~~se~~ potential uncertainties ~~will be~~ ~~are~~ discussed in details with ~~flame-flame-~~ generated soot particles in Sect. 3.2.

DMA-AAC

The advantage of ~~the~~ AAC versus ~~the~~ CPMA is ~~that~~ there is no need for a neutralizer to charge aerosol particles. ~~Measuring solely with an AAC will avoid multiple charging. However, AAC cannot constrain the properties of aspherical particles as monodisperse as DMA or CPMA classification (Kazemimanesh et al., 2022). Multiple charging becomes a problem when the tandem measurement is made with a DMA or PMA. Therefore, the multiple charge effect could be avoided theoretically.~~ The transfer function of ~~the~~ DMA-AAC selecting the same representing particles was calculated and ~~is~~ shown in $\log(d_{ae})$ - $\log(d_m)$ (Fig. 4a). Moreover, according to Eqn. 19-20 and Eqn. 22-23, aspherical particles can be expressed as follows,

$$\log d_{ae} = \frac{1}{2}(D_{fm} - 1)\log d_m + \frac{1}{2}\log\left(\frac{6}{\pi} \frac{Cc(d_m)^{k\rho_f}}{Cc(d_{ae})\rho_0} \cdot 10^{9D_{fm}-18}\right), \quad (2627)$$

which indicates that the relationship between d_{ae} and d_m is non-linear since ~~the~~ $Cc(d_m)$ and $Cc(d_{ae})$ ~~varies~~ with d_m and d_{ae} , respectively. Particles morphology can be derived from the relationship between d_m and d_{ae} measured by ~~a~~ DMA and AAC, respectively. ~~In order to~~ ~~To~~ simulate the transfer function of ~~the~~ DMA-AAC, ~~selecting the same particles as that those used in the calculations of the DMA-CPMA were selected.~~ The corresponding d_{ae} was numerically solved using ~~the~~ known mass-size-mobility relationship. Unlike the DMA-CPMA system, the transfer functions of singly charged and doubly charged particles ~~is-are~~ in parallel for ~~the~~ DMA-AAC, suggesting that ~~the~~ particles population is less likely to overlap with the region of multiply charged particles. Using the example setups of DMA-AAC, truly monodispersed particles are selected for spherical particles and typical soot particles.

Similar to the DMA-CPMA system, ~~to eliminat~~ ~~ing~~ multiply charged particles requires ~~that~~ the $d_{ae,max}$ of the AAC at $d_{m2,min}$ must be smaller than the d_{ae} of particles of interest, which can be derived from $d_{m2,min}$ and D_{fm} (Eqn. 2627),

$$d_{ae}(d_{m2,min}, D_{fm}) > d_{ae,max}(d_{m2,min}),$$

$$\Rightarrow D_{fm} > \frac{\log(2 \frac{1+\beta_{AAC}}{1+\beta_{DMA}})}{\log[\frac{2}{1+\beta_{DMA}} \frac{Cc(d_{m2,min})}{Cc(d_{m1})}]}, \quad (2728)$$

This equation describes the minimum value of D_{fm} to eliminate ~~the~~ multiple charging effect. It is clearly shown that the mobility resolution of ~~the~~ DMA and the relaxation time resolution of ~~the~~ AAC determine the limiting condition, and ~~the~~ resolution of ~~the~~ AAC is more important compared with ~~the~~ resolution of ~~the~~ DMA. The limiting condition is also related to ~~the~~ selected d_m of ~~the~~ DMA but independent of ~~the~~ selected d_{ae} of ~~the~~ AAC (Fig. S1). Setting the same resolutions ~~of for the~~ DMA and AAC, particle selection is more

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susceptible to multiple charging effect when selecting small sizes. In Fig. 4a, the values of β_{DMA} and β_{AAC} are 0.1, resulting in the minimum D_{fm} of 1.41, which is the case for most atmospheric aerosol particles. Hence, the selected particles of the DMA-AAC are truly monodisperse regardless of the particles morphology. However, in actual operations, a larger sample flow rate is required to satisfy the apparatus downstream, while the maximum sheath flow rate of the classifier is restricted by the instrument design (e.g., 30 L min⁻¹ for the DMA and 15 L min⁻¹ for the AAC). Besides, in addition, the maximum size ranges are also restricted by the sheath flow, so in some cases, a lower sheath flow rate is required to select larger sizes particles. When increasing β_{AAC} to 0.3 and remaining leaving β_{DMA} unchanged, the transfer function becomes broader (Fig. 4b). The minimum D_{fm} is 2.44, which indicates that the multiple charging effect exists for typical soot particle with D_{fm} of 2.2-2.4. The line representing soot particles overlaps with the region of doubly charged particles. Thus, reducing the resolutions of the DMA or AAC is not suggested in actual operations.

3.2 Evaluation of the multiple charging effect

To quantify the possible uncertainties biases of the multiple charging effect in DMA-CPMA system, we conducted the a soot experiment, as demonstrated in Fig. 1. For each mobility-selected particles, the corresponding d_{ae} and m were determined using scan mode of the AAC and CPMA scan modes, from which the effective densities were derived, respectively. Representative plots for the measured spectral density of mass and aerodynamic diameter of particles with d_{m} of 150 nm and 250 nm are shown in Fig. S2. The results are summarized in table Table 2. The fitted values of D_{fm} and k_f were 2.28 and 7.49×10^{-6} , respectively. The fitted value of D_{fm} was 2.28, indicating a fractal structure, which is the same as the in previous studies (Pei et al., 2018). The effective densities of generated soot particles vary from $>500 \text{ kg m}^{-3}$ at $d_{\text{m}} = 80 \text{ nm}$ to $<300 \text{ kg m}^{-3}$ at d_{m} of 250 nm for the two methods. In general, the deviation monotonically decreases along with increasing particle size. The deviation is 7.65% for particles of 80 nm, whereas it decreased to $<1\%$ of for particles larger than 200 nm. The results reveal a strict agreement between the two methods for retrieving the particle effective density.

According to Fig. 3, the critical slopes of PP_0 for soot particles with d_{m} of 80 nm, 100 nm, 150 nm, 200 nm and 250 nm are 2.46, 2.4041, 2.29, 2.17 and 2.0708, respectively. The measured D_{fm} of 2.28 is smaller than the calculated PP_0 for particles with d_{m} smaller than 150-200 nm, which suggests that the contributions from the multiply charged particles can not be eliminated suggested that multiply charged particles are still classified in this circumstance.

When selecting particles with d_{m} of 80 nm and m of 0.16 fg, the corresponding transfer function is shown in Fig. 5a. The particle population overlaps the transfer function region of doubly charged particles, suggesting the potential interferences of doubly charged particles in DMA-CPMA selection. Since the classification of the AAC is insensitive to particle charging states different from the DMA and CPMA, the multiply-charged aerodynamic size distributions of mobility and mass selected particles can be resolved were characterized in aerodynamic size distribution. Fig. 5b shows the particles number aerodynamic size distribution (PNSD_{ae}) scanned by the AAC. PNSD_{ae} was fitted using log-normal distributions, and three peaks which corresponding

to singly, doubly and triply charged particles were identified. Some small particles remaining in the AAC induced the peak at $d_{ae} < 40$ nm. These residual particles were measured even if the sample flow is filtered. The mean d_{ae} were 53.89, ~~58.260.6~~ and ~~69.470.9~~ nm, and the corresponding d_{ae} were calculated as 51.45 nm, ~~61.22.0nm~~ and ~~69.470.7~~ nm using Eq. (1) and Eq. (16), respectively. The experimental results are consistent with the theoretical results with deviations within 5.3%.

~~On the~~In contrast, when selecting particles with d_m of 200 nm and m of 1.28 fg, the transfer function is shown in Fig. 6a. The ~~slope of PP0~~ slope of 2.07-17 is smaller than D_m of 2.28, the generated particles population does not overlap with the block of doubly charged particles; thus, the DMA-CPMA classified particles were truly mono-dispersed. PNSD_{ae} measured by AAC is unimodal, implying that the classified particles were singly charged (Fig. 6b).

The results of other experiments are shown in Fig. ~~S2S3~~. Although the critical slope of PP0 when selecting 150 nm particles is close to D_m and the transfer function of DMA-CPMA also showed that negligible multiply charged particles would be selected (Fig. S3d), doubly charged particles were measured in PNSD_{ae} (Fig. S3e). Although the transfer function of DMA-CPMA showed that no multiply charged particles would be selected when classifying 150 nm particles (Fig. S2d), doubly charged particles were resolved by AAC (Fig. S2e). These doubly charged particles were selected, probably owing to particles' diffusion. The non-diffusion models were used to calculate the transfer function, but ~~actually~~ the transfer function can be broader because of diffusion. In summary, for a type of particles (with the same mass-mobility relationship), the possibility of multiple charging increases for small particles when selected by DMA-CPMA system, which is consistent with the theoretical calculation in Sect. 3.1.

3.3 Atmospheric implication

The DMA-APM and DMA-CPMA systems are usually adopted to eliminate multiply charged particles in soot aerosol studies. ~~As previously discussed, a~~ Although they might fail to select monodispersed particles, downstream measurements by instruments such as single-particle soot photometer (SP2), will not be interfered with, which characterizes the distinct information of a single particle. Nevertheless, for techniques measuring the properties of an entire aerosol population, e.g., scattering coefficient by a nephelometer or absorption coefficient by a photoacoustic spectrometer, multiply charged particles can induce significant bias. ~~A Pervious-pervious~~ study (Radney and Zangmeister, 2016) ~~pointed-out~~ noted that the DMA-APM failed to resolve multiply charged particles for soot particles when selecting 150 nm flame-generated particles, which caused a 110% error in extinction measurement. ~~In order to~~ To investigate the multiple charging effect for DMA-CPMA classification, the optical absorption coefficient of particles with different charging states after DMA-CPMA classification was calculated from PNSD_{ae}. Mie theory was used to calculate the theoretical absorption coefficient at ~~the a~~ wavelength of 550 nm. Mie theory is probably not the "best" method to use here since soot particles are aspherical agglomerates. Realistically, however, the Mie comparison is only being used to prove a point about the impact of multiple charging. Therefore, in this instance, any errors in the calculated optical properties are somewhat inconsequential. The refractive index used in the Mie code

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was $1.95 \pm 0.79i$ (Bond and Bergstrom, 2006). The PNSD_{ae} for different charging state particles ~~were-was~~ converted to volume equivalent diameter size distributions (PNSD_{ve}) which ~~were-was~~ used in Mie theory to determine the absorption coefficient ~~for particles with single, double and triple charging, respectively~~. The method to calculate PNSD_{ve} is described in ~~section Sect. S1 of the Supplementary Material~~. Subsequently, ~~the absorption coefficient, α_{abs} , was derived using the Mie theory and the PNSD_{ve} of particles with different charging states. Subsequently, absorption coefficient, α_{abs} , was derived using the absorption coefficient and total number concentration of particles with different charging states~~. For soot particles with diameter < 200 nm, the optical absorption contributions of particles with different charging state and the mass absorption cross-section (MAC) overestimation are summarized in Table 3. For soot particles with diameter of 80 nm, the contributions of particles with different charging states are shown in Fig. 5c. Doubly charged particles only account for $29.66.7 \pm 3.0\%$ of the total number concentration but provide ~~the-a largest~~ fractional contribution ~~to~~ the total absorption ($45.7 \pm 4.253.1\%$). ~~Also~~ Additionally, small fraction ($1.1 \pm 0.40.7\%$) of triply charged particles accounted for $3.7 \pm 1.54.9\%$ of the absorption. As a result, the ~~mass absorption cross-section (MAC)~~ was overestimated by $43.0 \pm 2.754.8\%$ and the directive radiative force (DRF) was overestimated by $43.0 \pm 2.754.8\%$. DRF was calculated using previous global climate models (Bond et al., 2016). ~~As~~ For particles selected by the DMA-CPMA at d_m of 200 nm and m of 1.28 fg, the selected particles were truly dispersed, and the measured optical properties were valid (Fig. 6c). A ~~Large Huge~~ amount of 70 nm-90 nm soot particles was emitted from diesel engine (Wierzbicka et al., 2014), and neglecting ~~of~~ the multiple charging effect in the measurement of mass-specific MAC on this size range will result in significant bias in estimation of radiative forcing of automobile-emitted soot particles, which may lead to ~~huge-large~~ error in climate model. For soot particles with diameter < 200 nm, the optical absorption contributions of particles with different charging state and the MAC overestimation are summarized in Table 3. According to Table 3, (The number fraction of doubly charged particles declines with the size of nominated particles, i.e. $26.7 \pm 3.053.1\%$ and $17.6 \pm 0.534.8\%$ for 80 and 100 nm particle, respectively, but only $4.2 \pm 1.19.2\%$ for 150 nm particles. Accordingly, the MAC was largely overestimated for 80 and 100 nm particles ($43.0 \pm 2.754.8\%$ and $27.9 \pm 0.827.1\%$, respectively) but moderately overestimated for 150 nm particles ($9.3 \pm 2.60.69\%$). To summarize, our results indicated that the combination of tandem classifiers is not sufficient to completely eliminate multiply charged particles when selecting small size flame-generated soot particle, which introduced noticeable ~~severe~~ bias for absorption measurement and ~~leaded-led~~ to overestimation of the MAC. ~~as~~ As a result, the DRF of soot particles was also overestimated.

4 Conclusion

In this study, we demonstrate the transfer functions of DMA-CPMA and DMA-AAC and discuss their limitations to eliminate multiply charged particles. For aspherical particles, there is no guarantee that the multiple-charging effect can be avoided in DMA-CPMA or DMA-AAC systems. Usually, DMA-AAC can select truly monodisperse particles, but the method can suffer from multiple charging when it can be suffered

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of particles with multiple charges when decreasing the resolutions of the DMA and AAC. The ability of the DMA-CPMA to eliminate multiple charging effect mainly depends on the particles morphology and the instrument resolutions. Under the same setups of DMA-CPMA, this tandem system is more sensitive to multiple charging effect with decreasing D_{fm} and decreasing ~~nominated~~ nominal size of particles. DMA-CPMA failed to eliminate multiply charged particles when selecting soot particles with diameter < 150 nm. Although doubly charged particles accounted for a small fraction of the number concentration, they contributed most significantly to light absorption, which indicated that multiply charged particles can induce an obvious contribution on to light absorption and lead to an overestimation of DRF for flame-generated soot particles.

Code/Data availability. Code/Data is available upon request.

Author contributions. ZW determined the main goal of this study. YS and XP designed the methods. YS carried them out and prepared the paper with contributions from all coauthors. YS, HL and JZ analyzed the optical data.

Competing interests. The authors declare that they have no conflict of interest.

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Appendix A

Table A1. Symbol used in this study

μ	Air viscosity
β	The ratio of flow rates of aerosol flow and sheath flow, Q_a/Q_{sh}
τ	Relaxation time
ω_1	Rotational speed of the inner electrode
ω_2	Rotational speed of the outer electrode
$\hat{\omega}$	ω_1/ω_2
δ	Half width of the gap between the two electrodes
Ω	Transfer function
ρ_0	Standard density, which equals to 1kg/m^3
τ	Relaxation time
τ^*	τ at the maximum of the transfer function
$\tilde{\tau}$	Dimensionless particle relaxation time, $\tilde{\tau} = \tau/\tau^*$
ρ_{eff}	Effective density
ρ_{kf}	Mass-mobility pre-exponential factor

α_{abs}	Absorption coefficient
$\sigma_{\text{CAPS-ALB}}$	Absorption cross-section calculated with Mie theory
$\sigma_{\text{CAPS-ALB}}$	Absorption cross-section measured by CAPS-ALB
B	Mechanical mobility
$C_c(d_p)$	Cunningham slip correction factor
c_r	Particle migration velocity
D_{fin}	Mass-mobility exponent
d_{ae}	Aerodynamic equivalent diameter
d_m	Mobility equivalent diameter
d_{ve}	Volume-equivalence size
e	Elementary charge
L	Length of DMA, CPMA or AAC
m	Particle mass
n	Number of elementary charges on the particle
PNSD	Particle number size distribution
PNSD _{ae}	Particle number aerodynamic size distribution
PNSD _{ve}	Particle number volume-equivalence size distribution
Q_a	Sample flow rate
Q_{sh}	Sheath flow rate
q	Electrical charge on the particle
R_m	Mass resolution of CPMA
r_a	Lower initial radial position that passes through the classifier
r_b	Upper initial radial position that passes through the classifier
r_1	Inner radius
r_2	Outer radius
\hat{r}	r_1 / r_2
t	Time
V	Voltage between the two electrodes of DMA or CPMA
\bar{v}	Average flow velocity
v_z	Axial flow distribution
v_θ	Velocity profile in the angular direction
Z_p^*	Z_p at the maximum transfer function of DMA
Z_p	Electrical mobility
\tilde{Z}_p	Z_p / Z_p^*

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Table 1 Dimensions of the three classifiers used for transfer function calculation

Parameter	DMA	CPMA	AAC
r_1 (mm)	9.37	100	43
r_2 (mm)	19.61	103	45
L (mm)	44.369	200	210
ω_2/ω_1	—	0.945	—

Table 2. Mobility diameter, mass, aerodynamic diameter, effective densities calculated by DMA-AAC and DMA-CPMA, and the deviation between them for fresh soot particles in the size range of 80-250 nm.

d_m (nm)	m (fg)	d_{ac} (nm)	$\rho_{DMA-AAC}$ (kg m ⁻³)	$\rho_{DMA-CPMA}$ (kg m ⁻³)	Deviation
80	0.16±0.010.16	48.2±0.348	551.2±6.9551.2	596.8±37.30596.8	7.65%7.65%
100	0.27±0.010.27	54.8±0.355	488.0±5.32488.0	515.7±19.10515.7	5.38%5.38%
150	0.66±0.070.66	67.8±0.367	359.1±3.22359.1	373.5±39.61373.5	3.86%3.86%
200	1.28±0.101.28	82.1±0.682	303.2±4.44303.2	305.6±23.87305.6	0.77%0.77%
250	2.17±0.162.17	95.9±0.996	262.8±4.92262.8	265.2±19.56265.2	0.90%0.90%

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Table 3. Number concentration fractions and absorption contributions for different size fresh soot particles with single, double or triple charges and the overestimation of MAC accordingly.

d_m (nm)	singly charged particles		doubly charged particles		triply charged particles		MAC overestimation
	f_N (%)	f_{abs} (%)	f_N (%)	f_{abs} (%)	f_N (%)	f_{abs} (%)	
80	72.2±2.569.7%	50.6±2.745.0%	26.7±3.029.6%	45.7±4.253.1%	1.1±0.40.7%	3.7±1.54.9%	43.0±2.754.8%
100	82.4±0.582.9%	64.4±0.865.2%	17.6±0.517.1%	35.6±0.834.8%	—	—	27.9±0.827.1%
150	95.8±1.297.0%	87.7±3.190.8%	4.2±1.13.0%	12.3±3.19.2%	—	—	9.3±2.60.69%

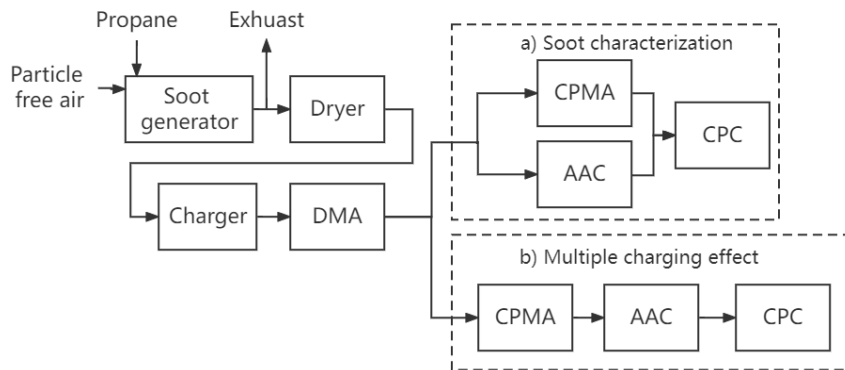
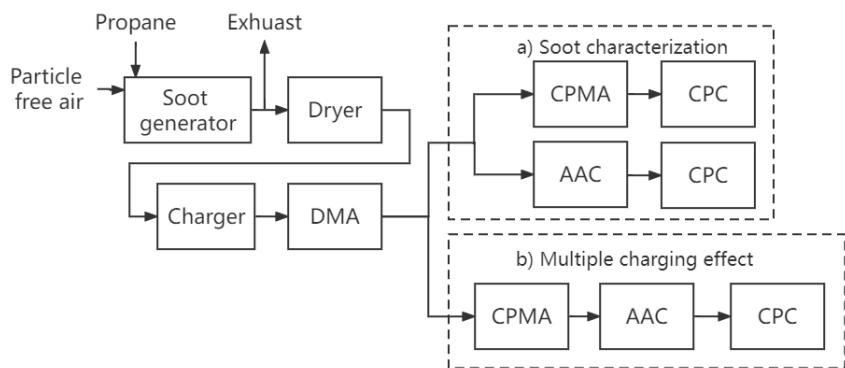


Figure 1: Schematic of the experimental setup: (a) soot characterization and (b) evaluation of multiple charging effects.

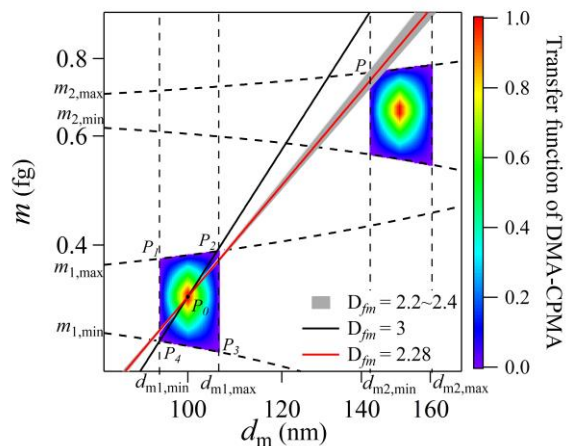


Figure 2: Example of DMA-CPMA transfer function of flame-generated soot particles (Pei et al., 2018). The following parameter set was employed for the calculations: $d_m = 100$ nm, $\beta_{DMA} = 0.1$, $m = 0.33$ fg, $Q_{CPMA} = 0.3$ L min^{-1} , $R_m = 8$. The color blocks are the transfer function of DMA-CPMA, with the rainbow color representing the transfer function for singly charged (lower left block) and doubly charged (upper right block) particles. The black and red solid lines are particles populations with D_{fm} values of 3 and 2.28, respectively. The grey region is the particle population with D_{fm} of 2.2-2.4, which is typical for soot aerosols. The dashed lines are the limits of d_m and m of DMA and CPMA. The DMA-CPMA transfer function for +2 particles does not overlap with the line for spherical particles with single charge ($D_{fm}=3$).

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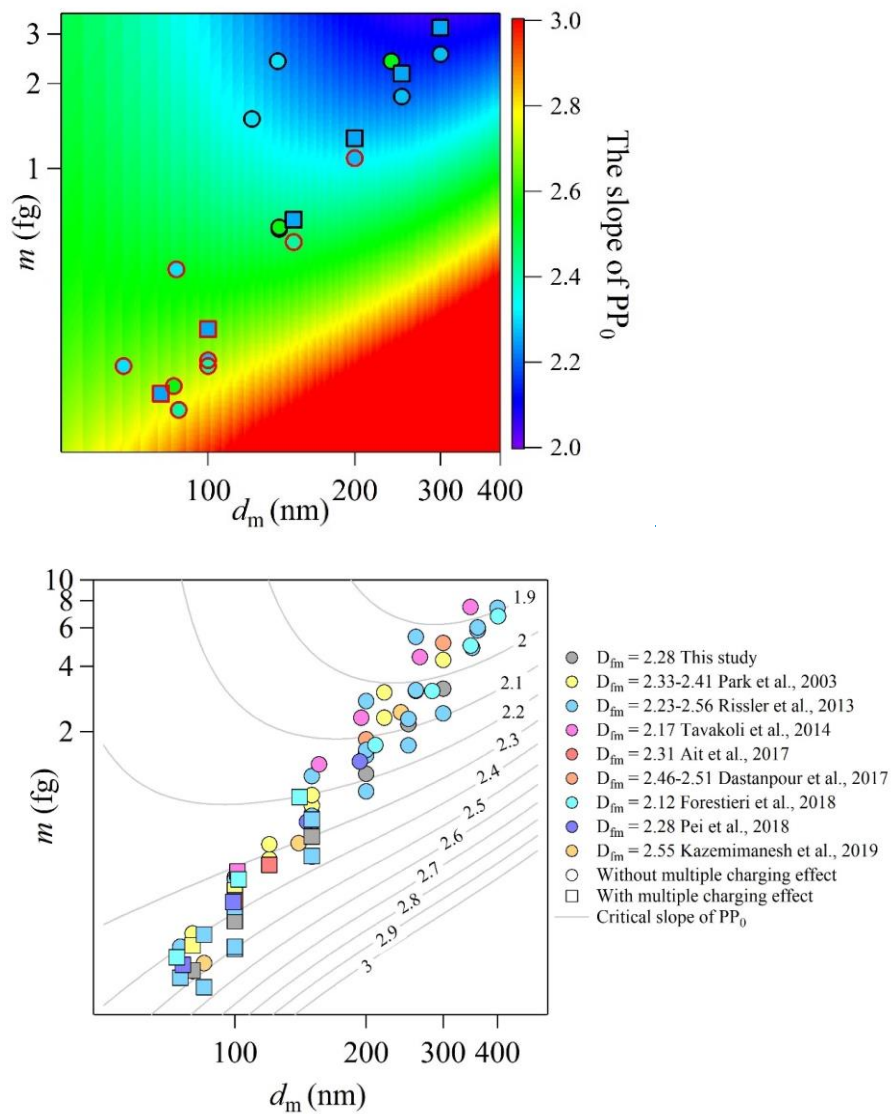


Figure 3: Variations of the slope of PP_0 as a function of classified d_m and m . The following parameter set was employed for the calculations: $\beta_{DMA} = 0.1$, $Q_{CPMA} = 0.3 \text{ L min}^{-1}$, $R_m = 8$. The background color coding contour lines denotes the slope of PP_0 , with red represents the slope of $PP_0 \geq 3$ values labeled on them. The data points are soot particles measured in the literature (Park et al., 2003; Rissler et al., 2013; Tavakoli et al., 2014; Ait Ali Yahia et al., 2017; Dastanpour et al., 2017; Forestieri et al., 2018; Pei et al., 2018; Kazemimanesh et al., 2019) and measured soot particles generated in this study (See details in section Sect. 3.2), respectively. Symbol colors indicate the particle d_m . The d_m values of these data points are listed in the legend. The data points become red square when the d_m is smaller than the critical slope of PP_0 in

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the background, i.e. the Symbols-with red border correspond to the cases that potential multiple charging effect may exist.

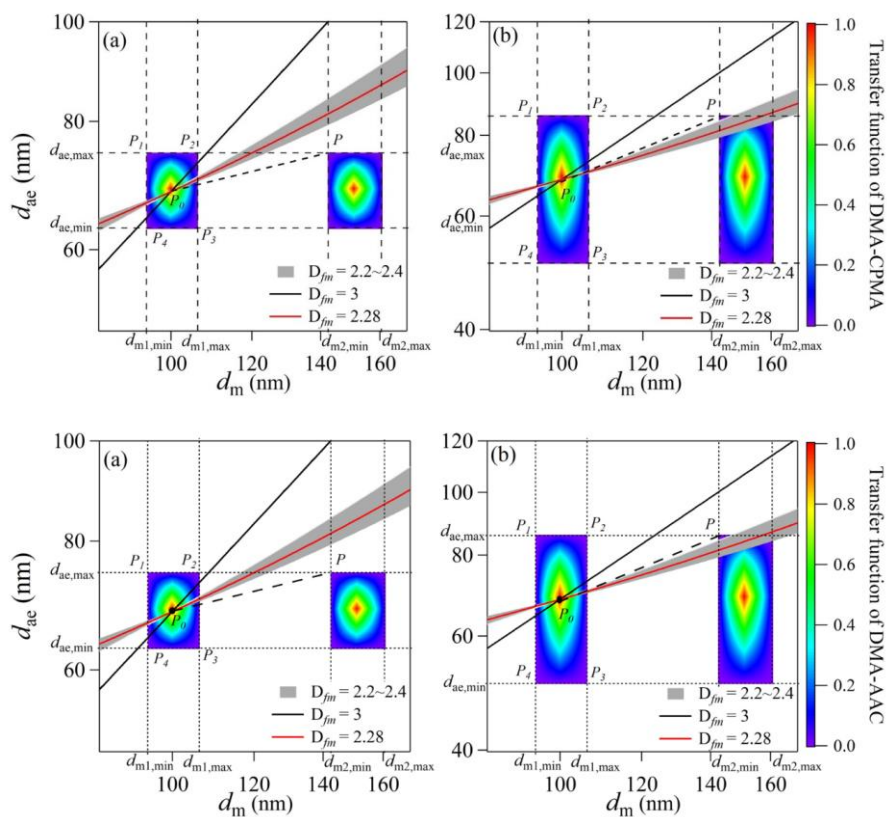
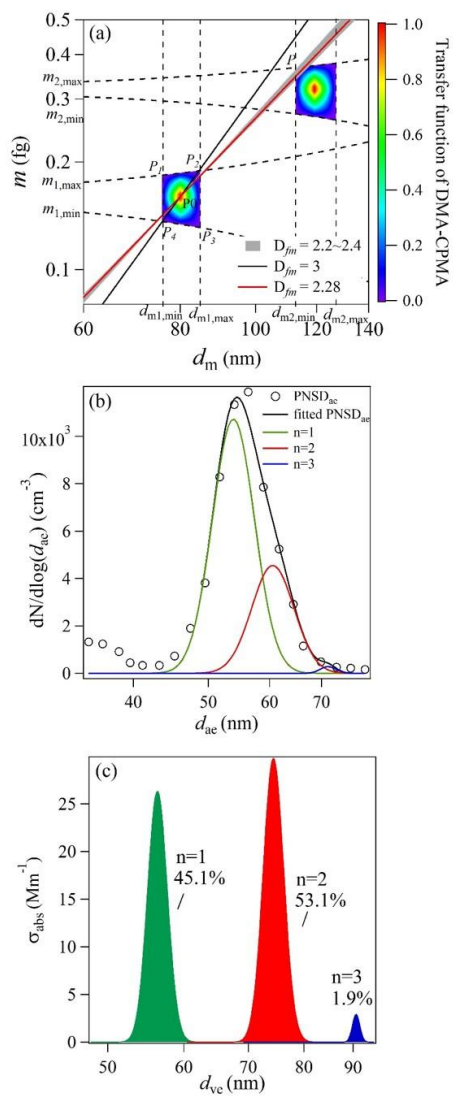


Figure 4: Examples of transfer function calculation of DMA-AAC of flame-generated soot particles (Pei et al., 2018). The following parameter set was employed for the calculations: $Q_a=0.3 \text{ L min}^{-1}$, $d_{m1} = 100 \text{ nm}$, $d_{ae} = 68.3 \text{ nm}$, (a) $\beta_{DMA} = 0.1$, $\beta_{AAC} = 0.1$, (b) $\beta_{DMA} = 0.1$, $\beta_{AAC} = 0.3$. The color blocks are the transfer functions of DMA-AAC. The black and red solid lines are particles populations with D_{fm} values of 3 and 2.28, respectively. The grey region is the particles population with D_{fm} of 2.2-2.4, which is typical for soot aerosols. The dashed line is the critical slope of PP_p . The dotted black-dashed lines are the limiting d_m and d_{ae} of DMA and AAC.

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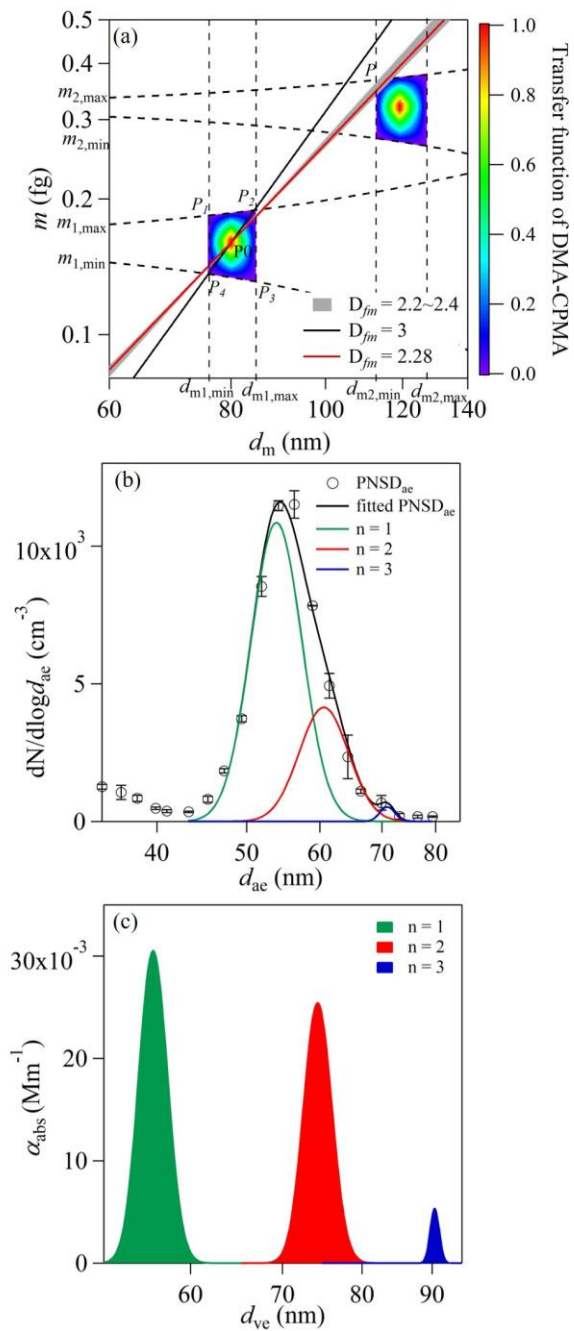
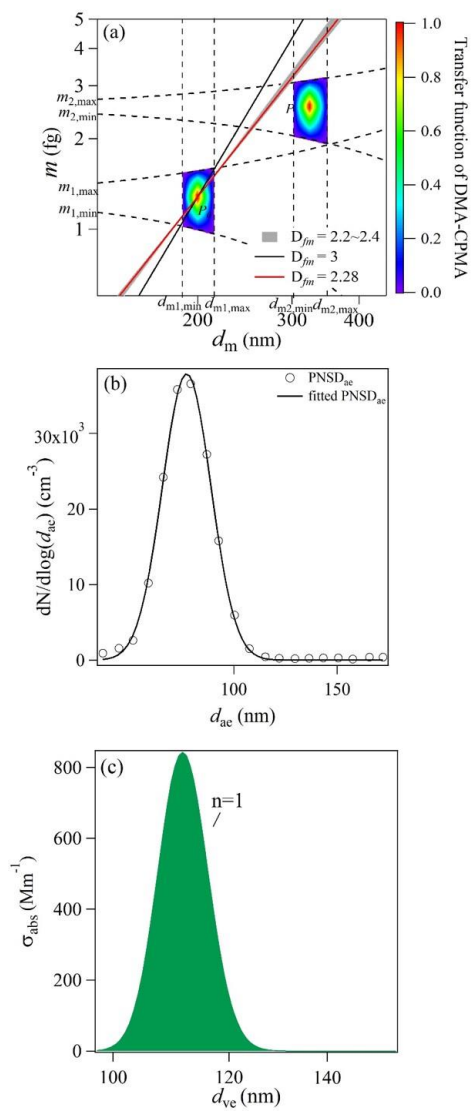


Figure 5: (a) The transfer functions of DMA-CPMA when selecting 80 nm and 0.16 fg particles. The following parameter set was employed for the calculations: $d_{m1} = 80$ nm, $\beta_{DMA} = 0.1$, $m_1 = 0.16$ fg, $Q_{CPMA} = 0.3$ L min⁻¹, $R_m = 8$. The red solid line is the generated soot particle population. (b) The aerodynamic size distribution of particles classified by DMA-CPMA. The circles are data measured by AAC-CPC, and the black, green red and blue lines are log-normal fitted distributions of bulk, singly charged, doubly charged and triply charged particles populations. (c) The contributions to light absorption of particles with single, double and triple charges calculated with Mie theory.



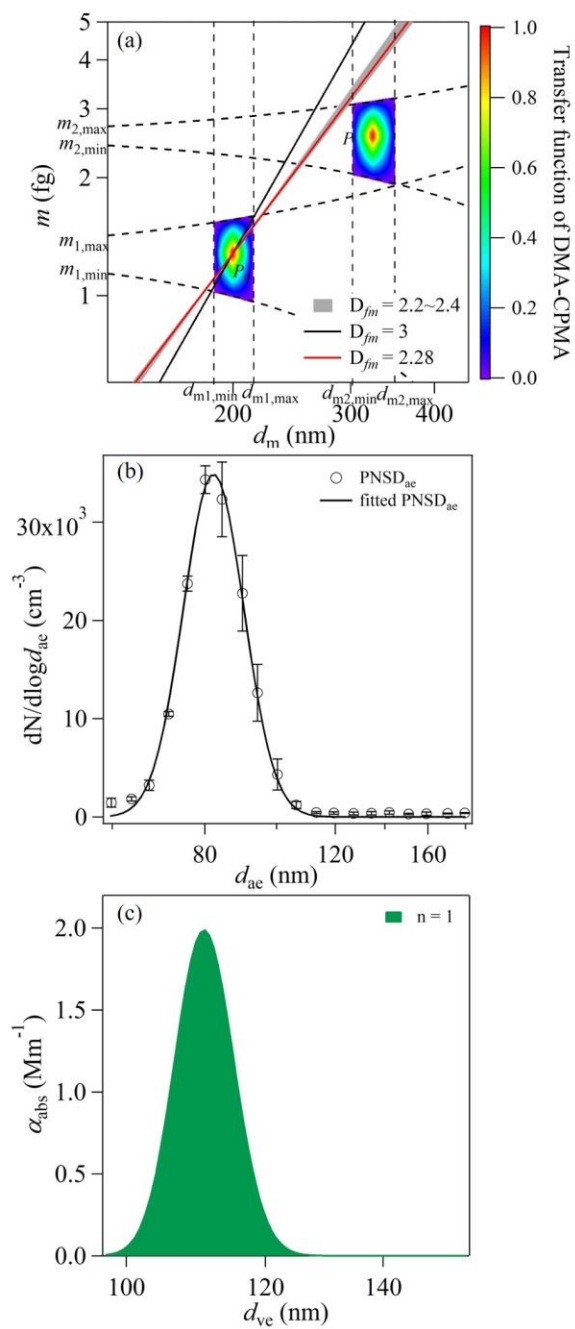


Figure 6: (a)The transfer functions of DMA-CPMA when selecting 200 nm and 1.28 fg particles. The following parameter set was employed for the calculations: $d_{m1} = 200$ nm, $\beta_{DMA} = 0.1$, $m_1 = 1.28$ fg, $Q_{CPMA} = 0.3$ L min⁻¹, $R_m = 8$. The red solid line is the generated soot particle population. (b)the aerodynamic size distribution of particles classified by DMA-CPMA. The circles are data measured by AAC-CPC, and the solid line is the log-normal fitted distribution. (c)the contributions to light absorption of particles with single charge calculated with Mie theory.