

# Characterization of tandem aerosol classifiers for selecting particles: implication for eliminating multiple charging effect

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**Abstract.** Accurate particle classification plays a vital role in aerosol studies. Differential mobility analyzer (DMA), centrifugal particle mass analyzer (CPMA) and aerodynamic aerosol classifier (AAC) are commonly used to select particles with a specific ~~size-mobility diameter, aerodynamic diameter~~ or mass, ~~respectively~~. However, multiple charging effects cannot be entirely avoided when using either individual techniques or tandem systems such as DMA-CPMA, especially when selecting soot particles with fractal structures. In this study, we ~~demonstrate-calculate~~ the transfer functions of the DMA-CPMA and DMA-AAC in static configurations ~~for flame generated soot particles~~. We propose an equation that constrains the resolutions of DMA and CPMA to eliminate the multiple charging effect when selecting particles with a certain mass-mobility relationship using the DMA-CPMA system. The equation for the DMA-AAC system is also derived. ~~For DMA-CPMA in a static configuration, Our results show that the ability to remove multiply charged particles mainly depends on the particle morphology and resolutions~~ ~~settings~~ of the DMA and CPMA. Using measurements from soot experiments and literature data, a general trend in the appearance of multiple charging effect with decreasing size when selecting aspherical particles is observed. ~~Otherwise As for DMA-AAC in a static configuration, our results indicate that the ability of the DMA-AAC in a static configuration~~ to eliminate particles with multiple charges is mainly related to the resolutions of classifiers. In most cases, the DMA-AAC in a static configuration can eliminate multiple charging effect regardless of the particle morphology, but multiply charged particles will be selected when decreasing the resolution of the DMA or AAC. We propose that the potential influence of the multiple charging effect should be considered when using the DMA-CPMA or DMA-AAC systems in estimating size- and mass-resolved optical properties in field and lab experiments.

## 33 1 Introduction

34 Atmospheric aerosol particles span a wide size range from 1 nm to > 100  $\mu\text{m}$ . A significant size dependence  
35 of aerosol physicochemical properties has been widely reported. Particle size can strongly alter the  
36 hygroscopic behavior (Biskos et al., 2006), phase state (Cheng et al., 2015) and cloud-nucleating ability  
37 (Dusek et al., 2006) of aerosol nanoparticles, indicating the importance of particle size when assessing the  
38 climate effect. Hence, accurate particle classification is essential when investigating the size ~~dependence~~  
39 ~~dependent~~ behavior of aerosol particles.

40 At present, particles are generally classified by either size or mass in atmospheric aerosol studies. A  
41 differential mobility analyzer (DMA) is the most commonly used size classifier, which selects particles based  
42 on electrical mobility (Knutson and Whitby, 1975; Park et al., 2008; Stolzenburg and McMurry, 2008;  
43 Swietlicki et al., 2008; Wiedensohler et al., 2012). A particle mass analyzer (PMA) includes an aerosol  
44 particle mass analyzer (APM) and a centrifugal particle mass analyzer (CPMA), both of which classify  
45 particles based on their mass-to-charge ratio (Ehara et al., 1996; Olfert and Collings, 2005). ~~However, The~~  
46 ~~charge distribution of~~ particles must be ~~known by passing through an neutralizer or similar precharged~~ when  
47 classified by ~~a~~-DMA or PMA ~~because DMA and PMA classify particles based on electrical mobility and~~  
48 ~~mass to charge ratio, respectively, resulting in. However,~~ particles with higher-order charges and identical  
49 apparent mobility or mass-to-charge ratio ~~being can be~~ selected simultaneously, which are referred to as the  
50 multiple charging effect. This may introduce uncertainty in the subsequent characterization. Radney et al.  
51 (2013) demonstrated that although single-charged particles account for the highest number fraction (46.3%)  
52 of DMA-classified particles (200 nm), their contributions to the total mass concentration and extinction are  
53 insignificant (10.8% and 7.96%, respectively). Thus, the reported extinction of particles with a certain  
54 diameter has been greatly overestimated due to the multiple charging effect.

55 Previous studies (Shiraiwa et al., 2010; Rissler et al., 2013; Johnson et al., 2014; Johnson et al., 2021) tried to  
56 utilize the combination of size and mass classifiers, such as DMA-APM or DMA-CPMA systems, to obtain  
57 singly charged particles. Theoretically, the ability of a DMA-APM to eliminate multiply charged particles is  
58 governed by the particle morphology and setups of ~~the~~ DMA- ~~and~~ APM (Kuwata, 2015). This conclusion  
59 implies that multiply charged particles cannot be effectively excluded for aspherical particles, especially for  
60 soot particles. Radney and Zangmeister (2016) investigated the limitations of a DMA-APM with three types  
61 of particles (polystyrene latex (PSL) spheres, ammonium sulfate (AS) and soot particles). Their results  
62 demonstrated that a DMA-APM can resolve multiply charged particles for spherical particles (PSL and AS  
63 particles), but it failed for aspherical soot particles. Multiply charged soot particles led to over 110% errors  
64 in retrieving the mass specific extinction cross section.

65 In contrast to DMA and PMA, an aerodynamic aerosol classifier (AAC) is a novel instrument that selects the  
66 aerodynamic equivalent diameter of aerosol particles based on their relaxation time. The advantage of  
67 utilizing an AAC is that ~~the charge state of the particles does not need to be known~~ ~~no charging process is~~  
68 ~~needed~~ in particle classification compared with the aforementioned classifiers; hence, multiple charging

69 effects can be avoided (Tavakoli and Olfert, 2013). However, the selected particles are not monodispersed in  
70 mobility diameter when an AAC is used to select aspherical particles (Kazemimanesh et al., 2022).  
71 Morphology information, such as effective density ( $\rho_{\text{eff}}$ ), mass–mobility exponent ( $D_{\text{fm}}$ ) and dynamic shape  
72 factor ( $\chi$ ), can be inferred using tandem DMA-PMA system (Park et al., 2003; Zhang et al., 2008; Rissler et  
73 al., 2013; Pei et al., 2018; Zangmeister et al., 2018), DMA-AAC (Tavakoli and Olfert, 2014) and AAC-  
74 CPMA systems (Kazemimanesh et al., 2022; Johnson et al., 2018). The derived  $\rho_{\text{eff}}$  and  $\chi$  depend upon the  
75 combination of instruments used, while the nonphysical values of  $\chi$  and  $\rho_{\text{eff}}$  for aspherical particles can be  
76 determined by the AAC-APM (Yao et al., 2020) and AAC-CPMA (Kazemimanesh et al., 2022).  
77 The theoretical transfer functions of individual classifiers (DMA, CPMA and AAC) and the DMA-APM  
78 system have been previously discussed (Knutson and Whitby, 1975; Ehara et al., 1996; Olfert and Collings,  
79 2005; Stolzenburg and McMurry, 2008; Tavakoli and Olfert, 2013). In this study, we focus on a DMA-  
80 CPMA and DMA-AAC in static configurations to eliminate multiply charged particles. The DMA-CPMA  
81 and DMA-AAC systems mentioned below refer to the tandems of a DMA and CPMA or a DMA and AAC  
82 in a static configuration, respectively. We calculate the transfer functions of the DMA-AAC and DMA-  
83 CPMA systematically. Combined with soot experiments, we demonstrate that multiple charging effects may  
84 still exist after DMA-CPMA classification when selecting aspherical particles and evaluate the light  
85 absorption of selected particles with different charging states using Mie theory. Furthermore, we propose  
86 operating conditions for the DMA-CPMA and DMA-AAC to eliminate multiply charged particles in future  
87 studies. Our results suggest that the size- and mass-resolved optical properties may be overestimated for  
88 small soot particles when using the DMA-CPMA system, which will lower the prediction accuracy of the  
89 fresh soot climate effect. In Sect. 3.1, we calculate the transfer functions of the DMA-CPMA and DMA-  
90 AAC utilizing the literature data of soot particles from Pei et al. (2018). In Sect. 3.2, we measure the multiple  
91 charging effect of the DMA-CPMA using laboratory-generated soot particles, and the bias of optical  
92 measurement induced by multiply charged particles is evaluated in Sect. 3.3.

## 93 2 Theory and experiment

### 94 2.1 Transfer function for individual aerosol classifiers

#### 95 DMA

96 The DMA, consisting of two coaxial electrodes, classifies particles based upon electrical mobility  $Z_p$   
97 (Knutson and Whitby, 1975), which can be calculated as follows:

$$98 Z_p = qB = \frac{neCc(d_p)}{3\pi\mu d_m}, \quad (1)$$

99 where  $q$  is the particle charge,  $n$  is the number of elementary charges,  $B$  is the mobility of the particle,  $e$  is  
100 the elementary charge,  $\mu$  is the viscosity of air, and  $Cc(d_p)$  is the Cunningham slip correction factor. When  
101 the aerosol inlet flow rate equals the aerosol sampling outlet flow rate, the centroid mobility,  $Z_p^*Z_p^*$ -selected  
102 by the DMA is defined as

$$Z_p^* = \frac{Q_{sh}}{2\pi V_{DMA} L_{DMA}} \ln\left(\frac{r_{2,DMA}}{r_{1,DMA}}\right), \quad (2)$$

where  $Q_{sh}$  is the sheath flow rate,  $V_{DMA}$  is the voltage between the two electrodes,  $L_{DMA}$  is the length of the DMA, and  $r_{1,DMA}$  and  $r_{2,DMA}$  are the inner and outer radii of the DMA electrodes, respectively. Assuming that the aerosol inlet and aerosol sampling flow rates are equal, the transfer function of the DMA can be expressed as follows when particle diffusion is negligible (Knutson and Whitby, 1975; Stolzenburg and McMurry, 2008):

$$\Omega(\bar{Z}_p, \beta_{DMA}) = \frac{1}{2\beta_{DMA}} [|\bar{Z}_p - (1 + \beta_{DMA})| + |\bar{Z}_p - (1 - \beta_{DMA})| - 2|\bar{Z}_p - 1|], \quad (3)$$

where,  $\bar{Z}_p = Z_p/Z_p^*$ ,  $\beta_{DMA} = Q_s/Q_{sh}$ , and  $Q_s$  is the sample flow rate. The limiting electrical mobilities that DMA can select are  $(1 \pm \beta_{DMA})Z_p^*$ . The maximum and minimum values of  $d_m$  for particles with  $n$  charges can be derived combining  $(1 \pm \beta_{DMA})Z_p^*$  and Eq. (1), and denote as  $d_{m-n,max}$  and  $d_{m-n,min}$ , respectively. The transfer function is an isosceles triangle with value of 1 at  $Z_p^*$  and going to 0 at  $(1 \pm \beta_{DMA})Z_p^*$ . It translates to asymmetry in  $d_m$  since the relationship between  $d_m$  and  $Z_p$  is nonlinear.

#### CPMA

The APM consists of two coaxial electrodes which are rotating at an equal angular velocity and a voltage is applied between these electrodes to create an electrostatic field (Ehara et al., 1996). The construction of the CPMA is similar to the APM, but its inner cylinder rotates faster than the outer cylinder to create a stable system of forces (Olfert and Collings, 2005). In the CPMA, the equation of particle motion is expressed as

$$\frac{m}{\tau} \frac{dr}{dt} = \frac{mv_\theta(r)^2}{r} - \frac{qV_{CPMA}}{r \ln\left(\frac{r_{2,CPMA}}{r_{1,CPMA}}\right)}, \quad (4)$$

and the trajectory equation is

$$\frac{dr}{dz} = \frac{dr}{dt} \left(\frac{dz}{dt}\right)^{-1} = \frac{c_r}{v_z}, \quad (5)$$

where  $\tau$  is the relaxation time,  $m$  is the mass of the particle,  $t$  is time,  $V$  is the voltage difference between the two electrodes, and  $r_{1,CPMA}$  and  $r_{2,CPMA}$  are the radii of the inner and outer electrodes, respectively.  $c_r$  is the particle migration velocity,  $v_z$  is the axial flow distribution and  $v_\theta$  is the velocity profile in the angular direction,

$$v_\theta = \omega_1 \frac{\hat{r}^2 - \hat{\omega}}{\hat{r}^2 - 1} r + \omega_1 r_{1,CPMA}^2 \frac{\hat{\omega} - 1}{\hat{r}^2 - 1} \frac{1}{r} = \alpha r + \frac{\beta}{r}, \quad (6)$$

where  $\hat{\omega} = \omega_2/\omega_1$  is the ratio of the rotational speed of the outer electrode to the inner electrode and  $\omega_1$  and  $\omega_2$  are the rotational speeds of the inner and outer electrodes, respectively.  $\hat{r}$  is the ratio of the inner and outer radii.  $\alpha$  and  $\beta$  are the azimuthal flow velocity distribution parameters.

Sipkens et al. (2019) presented methods to calculate the transfer function of the CPMA. They considered the Taylor series expansion about the center of the gap ( $r_c = (r_{2,CPMA} + r_{1,CPMA})/2$ ) instead of the equilibrium radius to avoid problems with the scenario in which the equilibrium radius does not exist. This method is much simpler and more robust. In this case, the particle migration velocity in the radial direction is

$$c_r \approx C_3 + C_4(r - r_c), \quad (7)$$

where

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137  $C_3 = \tau \left( \alpha^2 r_c + \frac{2\alpha\beta}{r_c} + \frac{\beta^2}{r_c^2} - \frac{C_0}{mr_c} \right),$  (8)

138  $C_4 = \tau \left( \alpha^2 - \frac{2\alpha\beta}{r_c} - \frac{3\beta^2}{r_c^2} + \frac{C_0}{mr_c^2} \right),$  (9)

139  $C_0 = \frac{qV_{CPMA}}{\ln(r_{2,CPMA}/r_{1,CPMA})},$  (10)

140 Assuming a plug flow, the transfer function would be

141  $\Omega = \frac{r_b - r_a}{2\delta},$  (11)

142 where  $\delta = (r_{2,CPMA} - r_{1,CPMA})/2$  is the half width of the gap between the two electrodes, and

143  $r_a = \min\{r_{2,CPMA}, \max\{r_{1,CPMA}, G_0(r_{1,CPMA})\}\},$  (12)

144  $r_b = \min\{r_{2,CPMA}, \max\{r_{1,CPMA}, G_0(r_{2,CPMA})\}\},$  (13)

145  $G_0(r_L) = r_c + (r_L - r_c + \frac{C_3}{C_4}) \exp(-C_4 L \bar{v}) - \frac{C_3}{C_4},$  (14)

146 where  $G_0(r)$  is the operator used to map the final radial position of the particle to its position at the inlet and  
 147  $\bar{v}$  is the average flow velocity. min{ } and max{ } are the minimum and maximum values of the quantities in  
 148 the brackets, respectively.

149 Reavell et al. (2011) calculated the resolution of the CPMA assuming that the gap between two electrodes is  
 150 narrow enough that the variation of force in the gap can be ignored. The mass resolution ( $R_m$ ) of CPMA is  
 151 related to particles mobility. When selecting the particles with mass of  $m_1$  and mobility of  $B_1$ , the  $R_m$  can be  
 152 calculated by

153  $R_m = \frac{2\pi B_1 L_{CPMA} r_c^2 \omega^2 m_1}{Q_{CPMA}},$  (15)

154 where  $\omega$  is the equivalent rotational speed calculated by  $\omega = \alpha + \frac{\beta}{r_c}$ ,  $m_1$  is the nominal mass that the CPMA  
 155 can select,  $Q_{CPMA}$  is the volumetric flow rate. The limiting mass can be calculated by

156  $m_{n,min}^{n,max} = n \cdot m_1 \pm \frac{Q_{CPMA}}{2\pi B_{n,min}^{n,max} L_{CPMA} r_c^2 \omega^2} = n \cdot m_1 \pm \frac{m_1}{R_m} \cdot \frac{B_1}{B_{n,min}^{n,max}},$  (1516)

158 ~~where  $\omega$  is the equivalent rotational speed calculated by  $\omega = \alpha + \frac{\beta}{r_c}$ ,  $m_1$  is the nominal mass that the CPMA~~  
 159 ~~can select, and where  $m_{n,min}^{n,max}$  and  $B_{n,min}^{n,max}$  are the maximum and minimum mass and corresponding mobility~~  
 160 ~~of particles bearing number of elementary charges of  $n$  that the CPMA can select, respectively. Further details~~  
 161 ~~can be found in Reavell et al. (2011) and Sipkens et al. (2019).~~

162 **AAC**

163 The AAC classifies particles based on relaxation time, which is defined by

164  $\tau = Bm = \frac{Cc(d_{ae})\rho_0 d_{ae}^2}{18\mu},$  (1617)

165 where  $\mu$  is the viscosity of air.  $Cc(d_{ae})$  is the slip correction factor.  $\rho_0$  is the standard density with a value of 1  
 166 g/cm<sup>3</sup> (Johnson et al. 2018). When the aerosol inlet flow rate equals the aerosol sampling outlet flow rate, it  
 167 can be expressed as (Tavakoli and Olfert, 2013)

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168 
$$\Omega = \frac{1}{2\beta_{AAC}} [|\bar{\tau} - (1 - \beta_{AAC})| + |\bar{\tau} - (1 + \beta_{AAC})| - 2|\bar{\tau} - 1|], \quad (4718)$$

169  $\tau^*$  is the nominal relaxation time, which is classified by the AAC,

170 
$$\tau^* = \frac{2Q_{sh}}{\pi\omega^2(r_{1,AAC} + r_{2,AAC})^2 L},$$

171 (4819)

172 where  $\beta_{AAC} = \frac{Q_a}{Q_{sh}}$ ,  $\bar{\tau} = \frac{\tau}{\tau^*}$ ,  $r_{1,AAC}$  and  $r_{2,AAC}$  are the inner and outer radii of the AAC, respectively. The  
 173 limiting  $\tau$  that AAC can select are  $(1 \pm \beta_{AAC}) \cdot \tau^*$ . The maximum and minimum values of  $d_{ae}$  can be derived  
 174 and denoted as  $d_{ae,max}$  and  $d_{ae,min}$ , respectively.

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## 175 2.2 Experimental setup

176 A schematic of the experimental setup is illustrated in Fig. 1. Soot particles were generated by a miniature  
 177 inverted soot generator (Argonaut Scientific Ltd., Canada) with a propane flow of 74.8 SCPM (standard mL  
 178 per minute, flow in mL min<sup>-1</sup> converted from ambient to T = 298.15 K and P = 101.325 kPa) and an air flow  
 179 rate of 12 SLPM (Standard L per minute, flow in L min<sup>-1</sup> converted from ambient to T = 298.15 K and P =  
 180 101.325 kPa). Although this operation setting is not in the open-tip flame regime, the flame is open-tip  
 181 consistent with Fig. 2d in Moallemi et al. (2019). Detailed aerosol generation methods can be found in  
 182 Kazemimanesh et al. (2019b) and Moallemi et al. (2019). The polydispersed aerosols were dried to a relative  
 183 humidity of <20% by a silica dryer and then passed through a soft X-ray neutralizer (Model 3088, TSI, Inc.,  
 184 USA). Five mobility diameters (80 nm, 100 nm, 150 nm and 250 nm) of soot particles were selected  
 185 with the DMA (Model 3081, TSI Inc., USA,  $\beta_{DMA} = Q_{sh}/Q_p = 10$ ). For the soot characterization, the flow of  
 186 aerosol which is monodispersed in  $Z_p$ , monodisperse mobility-selected aerosol flow was switched between  
 187 two parallel lines and fed into the CPMA (Cambusion Ltd., UK) and AAC (Cambusion, Ltd., UK,  $\beta_{AAC}$   
 188  $= Q_{sh}/Q_p = 10$ ); meanwhile, the condensation particle counter (CPC, Model 3756, TSI, Inc., USA, 0.3 L min<sup>-1</sup>)  
 189 was switched between the CPMA and AAC. The distributions of particle number concentration as a  
 190 function of particle mass ( $m$ ) and aerodynamic diameter ( $d_{ae}$ ) were determined-measured by the scanning  
 191 mode of the CPMA and AAC, respectively, while the CPC recorded their corresponding number  
 192 concentrations at each setpoint. For each  $d_m$ , the  $m$  and  $d_{ae}$  distributions were measured three times. Between  
 193 measurements of each  $d_m$ , the CPC was used behind the DMA, and the number size distribution of the  
 194 generated soot particles was measured by a scanning mobility particle sizer (SMPS) to ensure that the number  
 195 size distribution of generated soot particles did not change during the whole experiment. The  $m$  and  $d_{ae}$   
 196 distributions were fitted to log-normal distributions; thus, the modales values denoted as  $m_c$  and  $d_{ae,c}$  for the  
 197 mobility-selected particles were determined. The equation of log-normal distribution used in this study is  
 198 expressed as

199 
$$\begin{cases} N(m) = \frac{N_0}{\sqrt{2\pi}\ln\sigma_m} \exp\left(-\frac{(\log(m)-\log(m_c))^2}{2(\ln\sigma_m)^2}\right) \\ N(d_{ae}) = \frac{N_0}{\sqrt{2\pi}\ln\sigma_{ae}} \exp\left(-\frac{(\log(d_{ae})-\log(d_{ae,c}))^2}{2(\ln\sigma_{ae})^2}\right) \end{cases} \quad N(m) = \frac{N_0}{\sqrt{2\pi}\ln\sigma_m} \exp\left(-\frac{(\log(m)-\log(m_c))^2}{2(\ln\sigma_m)^2}\right)$$

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$$N(d_{ae}, d_p, x) = \frac{N_0}{\sqrt{2\pi} \ln \sigma_{ae} \sigma} \exp\left(-\frac{(\ln(d_{ae} x d_p) - \ln(d_{ae} \mu))^2}{2(\ln \sigma_{ae} \sigma)^2}\right), \quad (1920)$$

where  $\sigma_m$  and  $\sigma_{ae}$  are the geometric standard deviations of  $m$  and  $d_{ae}$  distributions, respectively, and  $\mu$ ,  $m_c$  and  $d_{ae,c}$  are the geometric mean of  $m$ ,  $\sigma$  and  $\mu$  are fitted from  $m$  or  $d_{ae}$  distributions, respectively. The CPMA and AAC were calibrated with certified PSL spheres (Thermo, USA) with sizes of 70 nm, 150 nm and 303 nm before the measurement. The measured  $m$  and  $d_{ae}$  were compared to  $m_{PSL}$  and  $d_{ae, PSL}$ , which were calculated with the nominal diameter and density of PSL (1050 kg m<sup>-3</sup>). The deviations between measured  $m$  and  $m_{PSL}$  or measured  $d_{ae}$  and  $d_{ae, PSL}$  were 2.75% and 5.14%, respectively. To quantify the multiple charging effect of particles selected by the DMA-CPMA system, the soot particles were initially selected by the DMA-CPMA at different  $d_m$  and the corresponding  $m$ . Then, the  $d_{ae}$  distribution of mobility and mass selected particles was obtained by stepping the AAC rotation speed of the cylinder with simultaneous measurement of the particle concentration at the AAC outlet using a CPC (Fig. 1b).

### 3 Results and discussion

#### 3.1 Transfer function of the tandem system

The DMA, PMA and AAC select particles based on the electrical mobility diameter, mass and aerodynamic diameter, respectively. These properties can be connected as follows (Decarlo et al. 2004):

$$\frac{Cc(d_{ae})\rho_0 d_{ae}^2}{6} = \frac{Cc(d_m)\rho_{eff} d_m^2}{6} = m \frac{Cc(d_m)}{\pi d_m}, \quad (2021)$$

where  $\rho_{eff} = \frac{6m}{\pi d_m^2}$ . The transfer function of the DMA-APM has been well documented and can be found in Kuwata (2015). The convolution of the transfer functions of the DMA-CPMA and DMA-AAC were calculated by the following equations.

$$\Phi_{DMA-CPMA} = \Omega_{CPMA} \Omega_{DMA}, \quad (2022)$$

$$\Phi_{DMA-AAC} = \Omega_{DMA} \Omega_{AAC}, \quad (2023)$$

where  $\Phi$  and  $\Omega$  are the transfer functions of the combined and individual classification systems expressed by subscripts, respectively each classification system expressed by subscripts. In the following discussion, we explain the transfer functions of the DMA-CPMA and DMA-AAC utilizing the literature data of soot particles (Pei et al., 2018). The  $d_m$  and  $m$  of the representative particles are 100 nm and 0.33 fg, respectively, and the corresponding  $d_{ae}$  is 68.3 nm according to Eq. (2021). In the calculation, the following parameter set was employed:  $d_m = 80-100$  nm,  $Q_{DMA} = 0.3$  L min<sup>-1</sup>,  $\beta_{DMA} = 0.1$ ,  $m = 0.16-33$  fg,  $Q_{CPMA} = 0.3$  L min<sup>-1</sup>,  $R_m = 8$ ,  $d_{ae} = 68.3$  nm,  $Q_{AAC} = 0.3$  L min<sup>-1</sup>,  $\beta_{AAC} = 0.1$ . The transfer functions of DMA-CPMA and DMA-AAC were solved iteratively using logarithmically spaced  $d_m$ ,  $m$  and  $d_{ae}$ , which included 600 points, respectively each. The ranges of  $d_m$ ,  $m$  and  $d_{ae}$  used in the calculations were from  $<0.8$  times of  $d_{m1,min}$  to  $>1.2$  times of  $d_{m2,max}$ , and from  $0.8$  times of  $<m_{1,min}$  to  $1.2$  times of  $>m_{2,max}$ , from  $0.8$  times of  $<d_{ae,min}$  to  $1.2$  times of  $>d_{ae,max}$ , respectively. The dimensions of the individual classifiers are summarized in Table 1.

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233 **DMA-CPMA**

234 The DMA-CPMA transfer function ( $\Phi_{\text{DMA-CPMA}}$ ) for particles mentioned above, i.e. particles with  $d_p$  of 100  
 235 nm and  $m$  of 0.33 fg, is calculated in  $\log(d_m)$ - $\log(m)$  space, as shown in Fig. 2. The particles are shown in  
 236 Fig. 2 in actual  $d_p$  and  $m$ , but when we calculate the resolution of DMA and CPMA, the mobility and effective  
 237 mass are used. The resolution of CPMA can be calculated by Eq. (15), where  $m_s$  is the mass of singly charged  
 238 particles which can be selected by the CPMA, i.e. effective mass. In  $\log(d_m)$ - $\log(m)$  space, the mass-mobility  
 239 relationship is

240  $m = k_f(d_m/nm)^{D_{fm}}$ , (2324)

241  $\log(m) = D_{fm} \log(d_m/nm) + \log(k_f)$ , (2425)

242 In theory general,  $D_{fm}$  equals 3 for spherical particles and smaller than 3 for aspherical particles, although  
 243  $D_{fm}$  can be larger than 3 for particles that are non-spherical at small  $d_m$  and approach spherical as  $d_m$  increases.

244 In the  $\log(d_m)$ - $\log(m)$  space, the relationship of  $m$  and  $d_m$  is linear, with the slope expressed as the mass-  
 245 mobility exponent ( $D_{fm}$ ) and the intercept representing the pre-exponential factor ( $k_f$ ). Under this specific  
 246 operation condition, no overlap was observed between the spherical particle population (black line) and the  
 247 classification region (the colored blocks) for doubly charged particles, implying that only the singly charged  
 248 particles were selected. For aspherical particles with  $D_{fm} < 3$ , such as soot particles with aggregate structures,  
 249 the particle population may overlap the doubly charged region when the slope ( $D_{fm}$ ) is small enough; however,  
 250 the combination of DMA and CPMA is generally used to avoid the multiple charge effect in soot studies.  
 251 The reported  $D_{fm}$  values are typically in the range of 2.2–2.4 for fresh soot particles (Rissler et al., 2013) and  
 252 diesel soot particles (Park et al., 2003). In the exemplary case (Pei et al., 2018), the derived  $D_{fm}$  of premixed  
 253 flame-generated soot particles was 2.28, resulting in the particles population always going through the  
 254 transfer area of doubly charged particles. This implies that the performance of the DMA-CPMA to eliminate  
 255 multiply charged particles to a certain extent depends on the particle morphology.

256 The DMA-CPMA system can eliminate the multiply charged particles only if the  $D_{fm}$  of the particles is larger  
 257 than the slope of a line connecting  $(d_m, m) = (d_{m2,\min}, m_{2,\max})(d_{m1}, m_1)$  (as PP<sub>0</sub> shown in Fig. 2). Since the  
 258 CPMA is used downstream of the DMA, the value of the mass limit of particles with a certain mobility of  $B$   
 259 can be expressed as follows according to Eq. (15):

260  $m_{n,\min}^{n,\max} = n \cdot m_s \pm \frac{q_{CPMA}}{2\pi\beta L_{CPMA} r_m^2 \omega^2}$ , (25)

261 where  $m_{n,\min}^{n,\max}$  is the maximum or minimum particle mass of particles with the mobility of  $B$  that would be  
 262 selected by the CPMA. The subscript  $n$  is the charge quantity  $m_{2,\max}$  at the  $d_p$  of  $d_{m2,\min}$  can be calculated  
 263 using Eq. (16) with the known mobility. Accordingly, the ideal condition under static operation to completely  
 264 eliminate the multiply charged particles is

265  $D_{fm} > PP_0 = \frac{\log(m_{2,\max}/m_1)}{\log(d_{m2,\min}/d_{m1})} = \frac{\log(2 + \frac{4z}{R_m(1+\beta_{DMA})})}{\log(\frac{z}{(1+\beta_{DMA})} \frac{Cc(d_{m2,\min})}{Cc(d_{m1})})}$  (26)

266 The ability of the DMA-CPMA to eliminate multiply charged particles depends on the selected  $d_m$ ,  $m$  and  
 267 resolutions of both the DMA and CPMA. Combining Eq. (165), Equation (26) gives instructions in actual

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268 operation to eliminate multiply charged particles. When selecting particles of certain  $d_m$  and  $m$ , by decreasing  
 269  $Q_{CPMA}$ , or increasing  $\omega$  and  $\beta_{DMA}$ , i.e., by increasing the resolution of the measurement, the potential of  
 270 multiply charged particles is reduced. Thus, the key to evaluating whether there is a multiple charging effect  
 271 lies in the particle morphology ( $D_{fm}$ ) and the slope of  $PP_0$  ~~derived from the actual condition~~ calculated from  
 272 Eq. (26) theoretically. ~~Compared with the DMA-CPMA, the selection of the DMA-APM is more susceptible~~  
 273 ~~to multiple charging effect. According to the theoretical calculation described in Kuwata (2015), the slope of~~  
 274  ~~$PP_0$  of 3.55 was derived when the DMA-APM selects the same example soot particles from Pei et al. (2018)~~  
 275 ~~( $d_m$  of 100 nm and  $m$  of 0.33 fg) with a  $D_{fm}$  of 2.28, indicating that the DMA-APM is more subject to the~~  
 276 ~~multiple charging effect.~~

277 In addition to the instrument setup, the particle morphology is also crucial for the DMA-CPMA. Here, we  
 278 simulate the critical slope of  $PP_0$  when selecting different  $d_m$  and  $m$  under the common selecting conditions  
 279 ( $\beta_{DMA} = 0.1$ ,  $Q_{CPMA} = 0.3 \text{ L min}^{-1}$ ,  $R_m = 8$ ) using Eq. (26), which is represented as contour lines in Fig. 3 (A  
 280 black and white version is shown as Fig. S4). Under these selection conditions, the DMA-CPMA can select  
 281 monodispersed particles when the  $D_{fm}$  of the particles is larger than the critical slope of  $PP_0$ . When selecting  
 282 small aspherical particles or particles with extremely low density, the critical slope of  $PP_0$  is relatively higher,  
 283 and the DMA-CPMA classification is sensitive to multiple charging effect. As shown in Fig. 3,  $d_m$ ,  $m$  and  
 284 the corresponding  $D_{fm}$  were taken from the literature (Park et al., 2003; Rissler et al., 2013; Tavakoli et al.,  
 285 2014; Ait Ali Yahia et al., 2017; Dastanpour et al., 2017; Forestieri et al., 2018; Pei et al., 2018;  
 286 Kazemimanesh et al., 2019a). Generally, for soot particles with  $D_{fm}$  of 2.2-2.4, the multiple charging effect  
 287 can be avoided for the DMA-CPMA when selecting soot particles with mobility diameters larger than 200  
 288 nm, while it fails to eliminate multiply charged particles when selecting small soot particles, as shown by the  
 289 circles and squares in Fig. 3. These potential uncertainties are discussed in detail with flame-generated soot  
 290 particles in Sect. 3.2.

### 291 DMA-AAC

292 The advantage of the AAC versus the CPMA is that there is no need for a neutralizer to charge aerosol  
 293 particles to a known charge state. Measuring solely with an AAC will avoid multiple charging. However,  
 294 aspherical particles with different mass can be selected by the AAC as having identical aerodynamic diameter  
 295 cannot constrain the properties of aspherical particles as monodisperse as DMA or CPMA classification  
 296 (Kazemimanesh et al., 2022). According to Eq. (291), the population selected by AAC has one physical size  
 297 ( $d_{ae}$ ) but the  $d_m$  range of this population is wide since soot particles have different densities. Multiple charging  
 298 becomes a problem when the tandem measurement is made with a DMA or PMA. ~~The transfer function of~~  
 299 ~~the DMA-AAC selecting the same representative particles was calculated and is shown in  $\log(d_{ae}) - \log(d_m)$~~   
 300 ~~(Fig. 4a). Moreover, according to Eq. (291) and Eq. (2324), the relationship of  $d_{ae}$  and  $d_m$  of aspherical~~  
 301 particles can be expressed as follows:

$$302 \log(d_{ae}) = \frac{1}{2}(D_{fm} - 1)\log(d_m) + \frac{1}{2}\log\left(\frac{6}{\pi} \frac{Cc(d_m)k_f}{Cc(d_{ae})\rho_0} \cdot 10^{9D_{fm}-10}\right), \quad (27)$$

303 which indicates that the relationship between  $d_{ae}$  and  $d_m$  is nonlinear since  $Cc(d_m)$  and  $Cc(d_{ae})$  vary with  $d_m$   
 304 and  $d_{ae}$ , respectively. Particle morphology can be derived from the relationship between  $d_m$  and  $d_{ae}$  measured

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305 by a DMA and AAC, respectively. To simulate the transfer function of the DMA-AAC, the same particles  
 306 ( $d_m = 100 \text{ nm}$ ,  $\mu = 0.33 \text{ fg}$ ,  $D_{fm} = 2.28$ ) as those used in the calculations of the DMA-CPMA were selected.  
 307 The corresponding  $d_{ae}$  was numerically solved using the known mass–mobility relationship. The transfer  
 308 function of the DMA-AAC selecting the same representative particles was calculated and is shown in  
 309  $\log(d_{ae})-\log(d_m)$  (Fig. 4a). In the transfer function of DMA-CPMA, the classification regions of singly  
 310 charged particles and doubly charged particles are on the diagonal. The oblique line of particles population  
 311 is more likely to go through the region of doubly charged particles in the transfer function of DMA-  
 312 CPMA. Unlike the DMA-CPMA system, the transfer functions of singly charged and doubly charged  
 313 particles are in parallel for the DMA-AAC, suggesting that the particles population is less likely to overlap  
 314 with the region of multiply charged particles. Using the example setups ( $d_m = 100 \text{ nm}$ ,  $Q_{DMA} = 0.3 \text{ L min}^{-1}$ ,  
 315  $\beta_{DMA} = 0.1$ ,  $d_{ae} = 68.3 \text{ nm}$ ,  $Q_{AAC} = 0.3 \text{ L min}^{-1}$ ,  $\beta_{AAC} = 0.1$ ) of the DMA-AAC, truly monodispersed particles  
 316 are selected for spherical particles and typical soot particles.

317 Similar to the DMA-CPMA system, eliminating multiply charged particles requires that the  $d_{ae,max}$  of the  
 318 AAC at  $d_{m2,min}$  must be smaller than the  $d_{ae}$  of particles of interest, which can be derived from  $d_{m2,min}$  and  $D_{fm}$   
 319 (Eq. (27)).

$$320 \quad d_{ae}(d_{m2,min}, D_{fm}) > d_{ae,max}(d_{m2,min}),$$

$$321 \quad \Rightarrow D_{fm} > \frac{\log(2 \frac{1+\beta_{AAC}}{1+\beta_{DMA}})}{\log[\frac{2}{1+\beta_{DMA}} \frac{cc(d_{m2,min})}{cc(d_{m1})}]}, \quad (28)$$

322 This equation describes the minimum value of  $D_{fm}$  to eliminate the multiple charging effect. It is clearly  
 323 shown that the mobility resolution of the DMA and the relaxation time resolution of the AAC determine the  
 324 limiting condition, and the resolution of the AAC is more important compared with the resolution of the  
 325 DMA. The limiting condition is also related to the selected  $d_m$  of the DMA but independent of the selected  
 326  $d_{ae}$  of the AAC (Fig. S1). Setting the same resolutions for the DMA and AAC, particle selection is more  
 327 susceptible to multiple charging effects when selecting small sizes. In Fig. 4a, the values of  $\beta_{DMA}$  and  $\beta_{AAC}$   
 328 are 0.1, resulting in a minimum  $D_{fm}$  of 1.41. ~~This  $D_{fm}$  is smaller than that for most aerosols which is the ease~~  
 329 ~~for most atmospheric aerosol particles.~~ Hence, the selected particles of the DMA-AAC are truly  
 330 monodisperse regardless of the particle morphology. However, in actual operations, a larger sample flow rate  
 331 ~~may be~~ required to satisfy the apparatus downstream, while the maximum sheath flow rate of the classifier  
 332 is restricted by the instrument design (e.g.,  $30 \text{ L min}^{-1}$  for the DMA and  $15 \text{ L min}^{-1}$  for the AAC). In addition,  
 333 the maximum size ranges are also restricted by the sheath flow, so in some cases, a lower sheath flow rate is  
 334 required to select larger particles. When increasing  $\beta_{AAC}$  to 0.3 (decreasing the resolution of AAC) and  
 335 leaving  $\beta_{DMA}$  unchanged, the transfer function becomes broader (Fig. 4b). The minimum  $D_{fm}$  is 2.44, which  
 336 indicates that the multiple charging effect exists for typical soot particles with  $D_{fm}$  of 2.2-2.4. The line  
 337 representing soot particles overlaps with the region of doubly charged particles. Thus, reducing the  
 338 resolutions of the DMA or AAC is not suggested in actual operations.

339 We think the transfer functions of DMA-AAC or AAC-DMA are identical regardless of the order of DMA  
 340 and AAC. For example, we use AAC-DMA to select particles with  $d_{ae}$  of 68 nm and  $d_m$  of 100 nm. In Fig.

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341 [4a](#), the transfer function of AAC is the region between the horizontal lines of  $d_{ae,max}$  (75 nm) and  $d_{ae,min}$  (63  
 342 nm). The soot particles population (red line) goes through this region will be selected by AAC. The mobility  
 343 diameter distribution of these relaxation time selected particles is around 80 nm to 120 nm. Then the DMA  
 344 is fixed to select particles with  $d_m$  of 100 nm, the particles with double charges and the same mobility ( $d_m$  of  
 345 150 nm) have been excluded by AAC. As a result, AAC-DMA select monodispersed particles with  $d_{ae}$  of  
 346 68.3 nm and  $d_m$  of 100 nm. In Fig. 4b, the resolution of AAC is lower and transfer function of AAC is broader  
 347 than that in Fig. 4a. The soot particles population (red line) goes through the transfer function region between  
 348 the horizontal lines at  $d_{ae}$  of  $d_{ae,max}$  (50 nm) and  $d_{ae,min}$  (86 nm). The mobility diameter distribution of these  
 349 relaxation time selected particles is very wide from less than 80 nm to about 158 nm. Then these relaxation  
 350 time selected particles were charged and selected by DMA at  $d_m$  of 100 nm, singly charged particles with  $d_m$   
 351 of 95 nm~106 nm and doubly charged particles with  $d_m$  of 142 nm~158 nm will be selected.  
 352 If we use the DMA-AAC, the particles are selected by DMA first. For example, in Fig. 4b, the transfer  
 353 function of DMA is shown as two vertical regions which particles with single and double charges can  
 354 penetrate. The soot particles (red line) goes through it and two populations of soot particles with mode  $d_m$  of  
 355 100 nm and 150 nm will be selected. The corresponding  $d_{ae}$  distributions of these singly and doubly charged  
 356 particles are 66 nm~70 nm and 81 nm~87 nm. These mobility-selected particles are selected at  $d_{ae}$  of 68.3  
 357 nm by AAC and the transfer function of AAC shows that particles with  $d_{ae}$  of 50 nm~86 nm can penetrate.  
 358 As a result, singly charged particles with  $d_{ae}$  of 66 nm ~70 nm and doubly charged particles with  $d_{ae}$  of 81  
 359 nm ~86 nm can be selected.  
 360 As a summary, the transfer functions of DMA-AAC and AAC-DMA in a static configuration are the same  
 361 no matter the ordering of DMA and AAC.

### 362 3.2 Evaluation of the multiple charging effect

363 To quantify the possible biases of the multiple charging effect in the DMA-CPMA system, we conducted a  
 364 soot experiment, as demonstrated in Fig. 1. For each mobility-selected particles, the distributions of number  
 365 density as a function of  $d_{ae}$  and  $m$  were determined by the scans. These distributions were then fit to a log-  
 366 normal to determine the modal values of ( $d_{ae,c}$  and  $m_c$ ) and from these values the  $\rho_{eff}$  were determined. the  
 367 corresponding  $d_{ae}$  and  $m$  were determined using the AAC and CPMA scan modes, from which the effective  
 368 densities were derived. The uncertainties of  $d_{ae,c}$  and  $m_c$  were standard deviation of multiple measurements.  
 369 Representative plots for the measured spectral density distributions of mass and aerodynamic diameter/ $d_{ae}$  of  
 370 particles with  $d_m$  of 150 nm and 250 nm are shown in Fig. S2. The results are summarized in Table 2. The  
 371 fitted values of  $D_{fm}$  and  $k_f$  were 2.28 and  $7.49 \times 10^{-6}$  fg, respectively, indicating a fractal structure, which is  
 372 the same as in previous studies (Pei et al., 2018). The effective densities of generated soot particles vary  
 373 from  $>500 \text{ kg m}^{-3}$  at  $d_m = 80 \text{ nm}$  to  $<300 \text{ kg m}^{-3}$  at  $d_m$  of 250 nm for the two methods determined by DMA-  
 374 CPMA and DMA-AAC. In general, the deviation of values of  $\rho_{eff}$  measured by DMA-CPMA and DMA-  
 375 AAC monotonically decreases with increasing particle size. The deviation is 7.65% for particles of 80 nm,

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411 The results of other experiments are shown in Fig. S3. Although the critical slope of  $PP_d$  when selecting 150  
 412 nm particles is close to  $D_{im}$  and the transfer function of DMA-CPMA also showed that negligible multiply  
 413 charged particles would be selected (Fig. S3d), doubly charged particles were measured in  $PNSD_{ae}$  (Fig. S3e).  
 414 These doubly charged particles were selected, probably owing to particle diffusion. The nondiffusion models  
 415 were used to calculate the transfer function, but the transfer function can be broader because of diffusion. In  
 416 summary, for a type of particle with the same mass–mobility relationship, the possibility of multiple charging  
 417 increases for small particles when selected by the DMA-CPMA system, which is consistent with the  
 418 theoretical calculation in Sect. 3.1.

### 419 3.3 Atmospheric implication

420 The DMA-APM and DMA-CPMA systems are usually adopted to eliminate multiply charged particles in  
 421 soot aerosol studies. Although they might fail to select monodispersed particles, downstream measurements  
 422 by instruments such as a single-particle soot photometer (SP2) will not be interfered with, which characterizes  
 423 the distinct information of a single particle. Nevertheless, for techniques measuring the properties of an entire  
 424 aerosol population, e.g., scattering coefficient by a nephelometer or absorption coefficient by a photoacoustic  
 425 spectrometer, multiply charged particles can induce significant bias. A previous study (Radney and  
 426 Zangmeister, 2016) noted that the DMA-APM failed to resolve multiply charged particles for soot particles  
 427 when selecting 150 nm flame-generated particles, which caused a 110% error in extinction measurement. To  
 428 investigate the multiple charging effect for DMA-CPMA classification, the optical absorption coefficient of  
 429 particles with different charging states after DMA-CPMA classification was calculated from  $PNSD_{ae}$ . Mie  
 430 theory was used to calculate the theoretical absorption coefficient at a wavelength of 550 nm. Mie theory is  
 431 probably not the “best” method to use here since soot particles are aspherical agglomerates. Realistically,  
 432 however, the Mie comparison is only being used to prove a point about the impact of multiple charging.  
 433 Therefore, in this instance, any errors in the calculated optical properties are somewhat inconsequential. The  
 434 refractive index used in the Mie code was  $1.95+0.79i$  (Bond and Bergstrom, 2006). The  $PNSD_{ae}$  for different  
 435 charging state particles was converted to volume-equivalent diameter size distributions ( $PNSD_{ve}$ ), which was  
 436 used in Mie theory to determine the absorption coefficient. The method to calculate  $PNSD_{ve}$  is described in  
 437 Sect. S1. Subsequently, the absorption coefficient,  $\alpha_{abs}$ , was derived using Mie theory and the  $PNSD_{ve}$  of  
 438 particles with different charging states.

438 The fractional absorption coefficient ( $f_{abs,n}$ ) for particles with different  
 439 charging state was calculated using Eq. (28) by replacing  $N$  with  $\alpha_{abs}$  and replacing  $d_p$  with  $d_{ve}$  as follows,

$$440 f_{abs,n} = \frac{\int_{d_{ve,low,n}}^{d_{ve,high,n}} \frac{d\alpha_{abs,n}}{d\log(d_{ve})} d\log(d_{ve})}{\sum_{i=1}^3 \int_{d_{ve,low,n}}^{d_{ve,high,n}} \frac{dN_n}{d\log(d_{ve})} d\log(d_{ve})} \quad (30)$$

441 where  $f_{abs,n}$  and  $\alpha_{abs,n}$  are the fractional absorption coefficient and absorption coefficient of particles bearing  
 442  $n$  charges, respectively.  $d_{ve,low,n}$  and  $d_{ve,high,n}$  denote the minimum and maximum value of  $d_{ve}$  of particles with  
 443  $n$  charges, which are converted from  $d_{ae,low}$  and  $d_{ae,high}$  scanned by AAC, respectively.

444 The overestimation of mass absorption cross-section (MAC) was calculated by

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$$\frac{\Delta \text{MAC}}{\text{MAC}} = \frac{\frac{\alpha_{\text{abs,tot}}}{m_p N_{\text{tot}}} \frac{f_{\text{abs},1} \alpha_{\text{abs,tot}}}{m_p f_{N,1} N_{\text{tot}}}}{\frac{f_{\text{abs},1} \alpha_{\text{abs,tot}}}{m_p f_{N,1} N_{\text{tot}}}} = \frac{f_{N,1}}{f_{\text{abs},1}} - 1 \quad (39)$$

where  $\alpha_{\text{abs,tot}}$  and  $N_{\text{tot}}$  is the total absorption coefficient and number concentration of particles selected by DMA-CPMA, respectively.  $m_p$  is the actual mass of singly charged particles selected by DMA-CPMA. The uncertainties were calculated from propagation of errors. For soot particles with diameters <200 nm, the optical absorption contributions of particles with different charging states and the mass-absorption-cross-section (MAC) overestimation are summarized in Table 3. For soot particles with a diameter of 80 nm, the contributions of particles with different charging states are shown in Fig. 5c. Doubly charged particles only account for 26.7% ± 3.0% of the total number concentration but provide a large fractional contribution to the total absorption (45.7% ± 4.2%). Additionally, a small fraction (1.1% ± 0.4%) of triply charged particles accounted for 3.7% ± 1.5% of the absorption. As a result, the MAC was overestimated by 43.042.7% ± 2.79.1%, and the directive radiative force (DRF) was overestimated by 43.042.7% ± 2.79.1%. The DRF was calculated using previous global climate models (Bond et al., 2016). For particles selected by the DMA-CPMA at a  $d_m$  of 200 nm and an  $m$  of 1.28 fg, the selected particles were truly dispersed, and the measured optical properties were valid (Fig. 6c).

A large amount of 70 nm -90 nm soot particles was emitted from diesel engine (Wierzbicka et al., 2014), and neglecting the multiple charging effect in the measurement of mass-specific MAC on this size range will result in significant bias in the estimation of radiative forcing of automobile-emitted soot particles, which may lead to large errors in climate model.

According to Table 3, the number fraction of doubly charged particles declines with the size of the nominated particles, i.e., 26.7% ± 3.0% and 17.6% ± 0.5% for 80 and 100 nm particles, respectively, but only 4.2% ± 1.1% for 150 nm particles. Accordingly, the MAC was largely overestimated for 80 and 100 nm particles (43.042.7% ± 2.79.1% and 27.928.0% ± 0.81.8%, respectively) but moderately overestimated for 150 nm particles (9.39.2% ± 2.64.1%). To summarize, our results indicated that the combination of tandem classifiers is not sufficient to completely eliminate multiply charged particles when selecting small flame-generated soot particles, which introduced noticeable bias for absorption measurements and led to overestimation of the MAC. As a result, the DRF of soot particles was also overestimated.

#### 4 Conclusion

In this study, we demonstrate the transfer functions of DMA-CPMA and DMA-AAC and discuss their limitations to eliminate multiply charged particles. For aspherical particles, there is no guarantee that the multiple charging effect can be avoided in DMA-CPMA or DMA-AAC systems. Usually, a DMA-AAC can select truly monodisperse particles, but the method can suffer from multiple charging when decreasing the resolutions of the DMA and AAC. The ability of the DMA-CPMA to eliminate multiple charging effect mainly depends on the particle morphology and the instrument resolutions. Under the same setups of DMA-CPMA, this tandem system is more sensitive to multiple charging effect with decreasing  $D_m$  and decreasing

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479 nominal size of particles. The DMA-CPMA failed to eliminate multiply charged particles when selecting  
 480 soot particles with diameters < 150 nm. Although doubly charged particles accounted for a small fraction of  
 481 the number concentration, they contributed most significantly to light absorption, which indicated that  
 482 multiply charged particles can induce an obvious contribution to light absorption and lead to an  
 483 overestimation of DRF for flame-generated soot particles.

484 *Code/Data availability.* Code/Data are available upon request.

485 *Author contributions.* ZW determined the main goal of this study. YS and XP designed the methods. YS  
 486 carried them out and prepared the paper with contributions from all coauthors. YS, HL and JZ analyzed the  
 487 optical data.

488 *Competing interests.* The authors declare that they have no conflicts of interest.

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 490 and 41805100). We especially acknowledge useful comments and suggestions on the MATLAB script of the  
 491 CPMA transfer function from Timothy A. Sipkens.

493 **Appendix A**

494 **Table A1. Nomenclature Symbols used in this study**

Parameter	Definition
$\beta$	The ratio of flow rates of aerosol flow and sheath flow, $Q_a/Q_{sh}$
$\tau$	Relaxation time
$\omega_1$	Rotational speed of the inner electrode
$\omega_2$	Rotational speed of the outer electrode
$\bar{\omega}$	$\omega_1 - \omega_2$
$\delta$	Half width of the gap between the two electrodes
$\Omega$	Transfer function
$\rho_{\text{ST}}$	Standard density, which equals $1 \text{ kg/m}^3$
$\tau$	Relaxation time
$\tau^*$	$\tau$ at the maximum of the transfer function
$\tilde{\tau}$	Dimensionless particle relaxation time, $\tilde{\tau} = \tau/\tau^*$
$\rho_{\text{eff}}$	Effective density
$k_{\text{E}}$	Mass-mobility pre-exponential factor
$\alpha_{\text{abs}}$	Absorption coefficient
$B$	Mechanical mobility
$C_c(d_p)$	Cunningham slip correction factor
$c_r$	Particle migration velocity

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$D_{fm}$	<b>Mass-mobility-exponent</b>
$d_{ac}$	Aerodynamic equivalent diameter
$d_{ac,c}$	<u>the geometric mean of <math>d_{ac}</math> distribution measured by AAC-CPC</u>
$d_{ac,high}$	<u>The maximum value of <math>d_{ac}</math> scanned by AAC</u>
$d_{ac,low}$	<u>The minimum value of <math>d_{ac}</math> scanned by AAC</u>
$d_{ac,max}$	<u>The maximum <math>d_{ac}</math> of particles that can be selected in AAC classification</u>
$d_{ac,min}$	<u>The minimum <math>d_{ac}</math> of particles that can be selected in AAC classification</u>
$d_m$	Mobility equivalent diameter
$d_{m,max}$	<u>The maximum <math>d_m</math> of particles with n charges that can be selected in DMA classification</u>
$d_{m,min}$	<u>The minimum <math>d_m</math> of particles with n charges that can be selected in DMA classification</u>
$d_{ve}$	Volume-equivalence size
$D_{fm}$	<b>Mass-mobility exponent</b>
$e$	Elementary charge
$f_{n,n}$	<u>The fractional number concentration of particles with n charges</u>
$f_{abs,n}$	<u>The fractional absorption coefficient of particles with n charges</u>
$k_T$	<b>Mass-mobility pre-exponential factor</b>
$L$	Length of DMA, CPMA or AAC
$m$	Particle mass
$m_c$	<u>the geometric mean of <math>m</math> distribution measured by CPMA-CPC</u>
$m_{q,max}$	<u>The maximum <math>m</math> of particles with n charges that can be selected in CPMA classification</u>
$m_{q,min}$	<u>The minimum <math>m</math> of particles with n charges that can be selected in CPMA classification</u>
$n$	Number of elementary charges on the particle
$N_{tot}$	<u>The total number concentration of particles selected by DMA-CPMA</u>
PNSD	Particle number size distribution
PNSD <sub>ac</sub>	Particle number aerodynamic size distribution
PNSD <sub>ve</sub>	Particle number volume-equivalent size distribution
$q$	<b>Electrical charge on the particle</b>
$Q_a$	Sample flow rate
$Q_{sh}$	Sheath flow rate
$\varphi$	<b>Electrical charge on the particle</b>
$R_m$	<b>Mass resolution of CPMA</b>
$r_a$	Lower initial radial position that passes through the classifier
$r_b$	Upper initial radial position that passes through the classifier

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$r_1$	Inner radius
$r_2$	Outer radius
$\hat{r}$	$r_1 / r_2$
$R_m$	<u>Mass resolution of CPMA</u>
$t$	Time
$V$	<u>Voltage between the two electrodes of DMA or CPMA</u>
$\bar{v}$	Average flow velocity
$v_z$	Axial flow distribution
$v_\theta$	Velocity profile in the angular direction
$V$	<u>Voltage between the two electrodes of DMA or CPMA</u>
$Z_p$	<u>Electrical mobility</u>
$Z_p^* Z_p^{*\#}$	$Z_p$ at the maximum transfer function of DMA
$Z_p$	Electrical mobility
$\bar{Z}_p$	$Z_p / Z_p^* Z_p^{*\#}$
$\alpha \beta$	<u>Azimuthal flow velocity distribution parameter</u>
$\alpha_{\text{abs}}$	<u>Absorption coefficient</u>
$\alpha_{\text{abs,tot}}$	<u>The total absorption coefficient of particles selected by DMA-CPMA</u>
$\beta$	<u>Azimuthal flow velocity distribution parameter</u>
$\beta_{\text{AAC}}$	<u>The ratio of flow rates of aerosol flow and sheath flow of AAC</u>
$\beta_{\text{DMA}}$	<u>The ratio of flow rates of aerosol flow and sheath flow of DMA</u>
$\delta$	<u>Half width of the gap between the two electrodes</u>
$\mu$	<u>Air viscosity</u>
$\rho_0$	<u>Standard density, which equals 1 kg/m<sup>3</sup></u>
$\rho_{\text{eff}}$	<u>Effective density</u>
$\sigma_m$	<u>The geometric standard deviation of <math>m</math> distribution</u>
$\sigma_{\text{asc}}$	<u>The geometric standard deviation of <math>d_{\text{asc}}</math> distribution</u>
$\tau$	<u>Relaxation time</u>
$\tau^*$	<u><math>\tau</math> at the maximum of the transfer function</u>
$\tilde{\tau}$	<u>Dimensionless particle relaxation time, <math>\tilde{\tau} = \tau / \tau^*</math></u>
$\omega_1$	<u>Rotational speed of the inner electrode</u>
$\omega_2$	<u>Rotational speed of the outer electrode</u>
$\hat{\omega}$	<u><math>\omega_1 / \omega_2</math></u>
$\Omega$	<u>Transfer function</u>

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605

**Table 1 Dimensions of the three classifiers used for transfer function calculation**

Parameter	DMA	CPMA	AAC
$r_1$ (mm)	9.37	100	43
$r_2$ (mm)	19.61	103	45
L (mm)	44,369	200	210
$\omega_2/\omega_1$	—	0.945	—

606

**Table 2. Mobility diameter, mass, aerodynamic diameter, effective densities calculated by DMA-AAC and DMA-CPMA, and the deviation between them for fresh soot particles in the size range of 80–250 nm.**

$d_m$ (nm)	$Mm_k$ (fg)	$d_{ac,e}$ (nm)	$\rho_{DMA-AAC}$ (kg m <sup>-3</sup> )	$\rho_{DMA-CPMA}$ (kg m <sup>-3</sup> )	Deviation
80	0.16±0.01	48.2±0.3	551.2±6.9	596.8±37.30	7.65%
100	0.27±0.01	54.8±0.3	488.0±5.32	515.7±19.10	5.38%
150	0.66±0.07	67.8±0.3	359.1±3.22	373.5±39.61	3.86%
200	1.28±0.10	82.1±0.6	303.2±4.44	305.6±23.87	0.77%
250	2.17±0.16	95.9±0.9	262.8±4.92	265.2±19.56	0.90%

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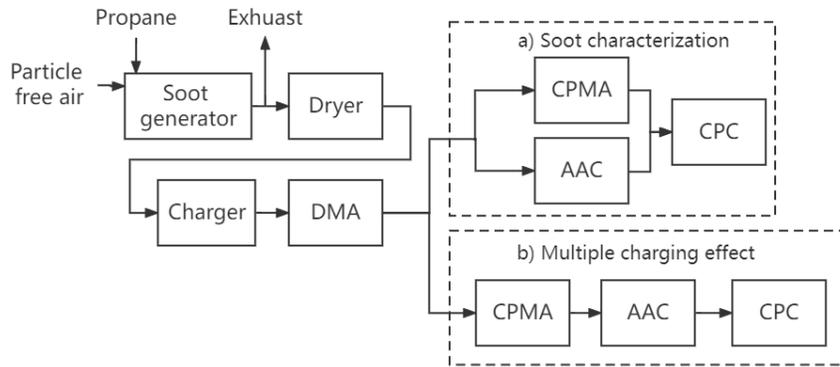
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**Table 3. Number concentration fractions and absorption contributions for different size fresh soot particles with single, double or triple charges and the overestimation of MAC accordingly.**

$d_m$ (nm)	$f_{N,1}$ (%)	$f_{abs,1}$ (%)	$f_{N,2}$ (%)	$f_{abs,2}$ (%)	$f_{N,3}$ (%)	$f_{abs,3}$ (%)	MAC overestimation(%)
80	72.2±2.5	50.6±2.7	26.7±3.0	45.7±4.2	1.1±0.4	3.7±1.5	<del>43.02.7</del> <del>+2.79.1</del>
100	82.4±0.5	64.4±0.8	17.6±0.5	35.6±0.8	-	-	<del>27.98.0</del> <del>+01.8</del>
150	95.8±1.2	87.7±3.1	4.2±1.1	12.3±3.1	-	-	<del>9.32</del> <del>+2.64.1</del>

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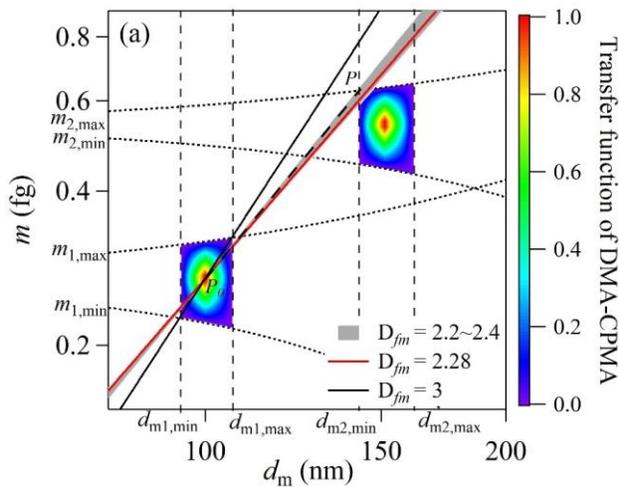
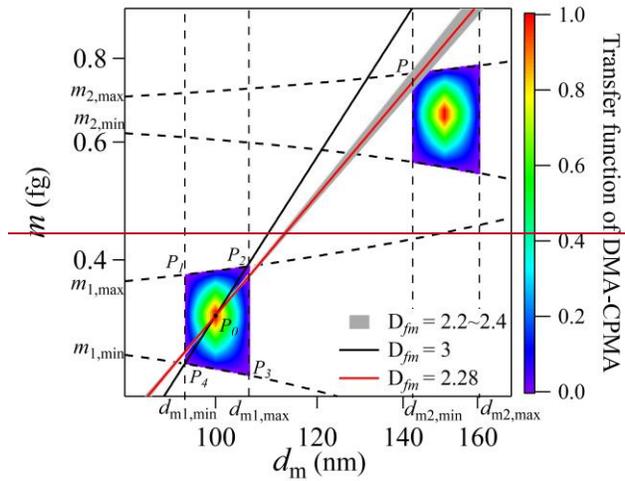
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**Figure 1: Schematic of the experimental setup: (a) soot characterization and (b) evaluation of multiple charging effects.**

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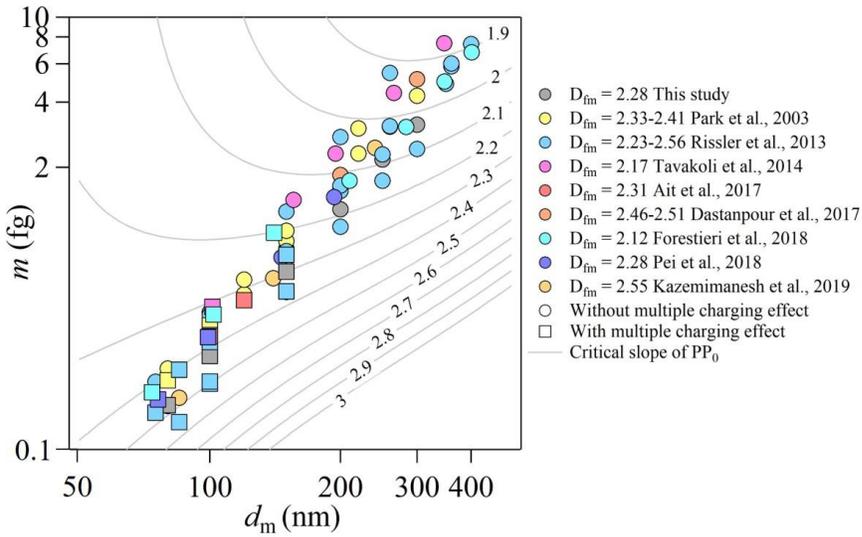
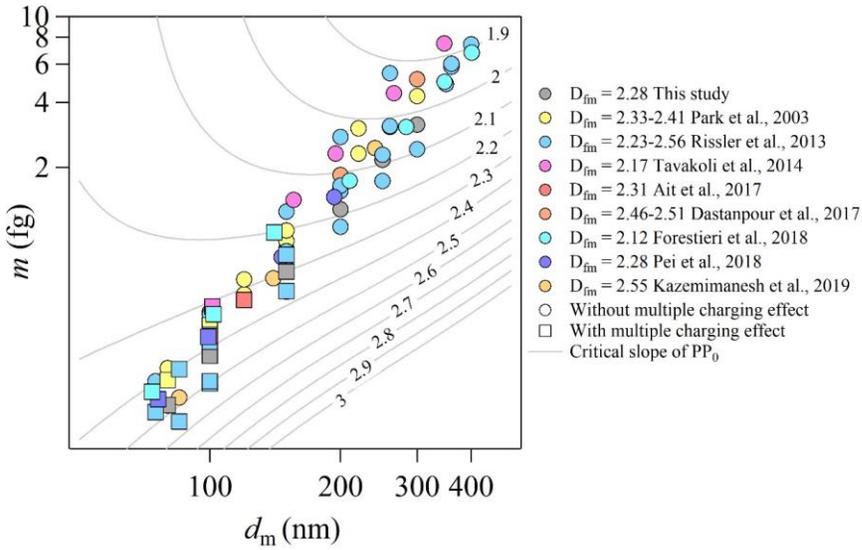
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618 **Figure 2: Example of the DMA-CPMA transfer function of flame-generated soot particles (Pei et al., 2018) in**  
 619  **$\log(m) - \log(d_m)$ .** The following parameter set was employed for the calculations:  $d_m = 100$  nm,  $\beta_{DMA} = 0.1$ ,  $m = 0.33$   
 620 **fg**,  $Q_{CPMA} = 0.3$  L min<sup>-1</sup>,  $R_m = 8$ . The color blocks are the transfer function of DMA-CPMA, with the rainbow color  
 621 representing the transfer function for singly charged (lower left block) and doubly charged (upper right block)  
 622 particles. The black and red solid lines are particles populations with  $D_{fm}$  values of 3 and 2.28, respectively. The  
 623 gray region is the particle population with  $D_{fm}$  of 2.2-2.4, which is typical for soot aerosols. The dashed-dotted lines  
 624 are the limits of  $d_m$  and  $m$  of DMA and CPMA, respectively. The dashed line is the critical slope of  $PP_0$ . The DMA-  
 625 CPMA transfer function for +2 particles does not overlap with the line for spherical particles with a single charge  
 626 ( $D_{fm}=3$ ).

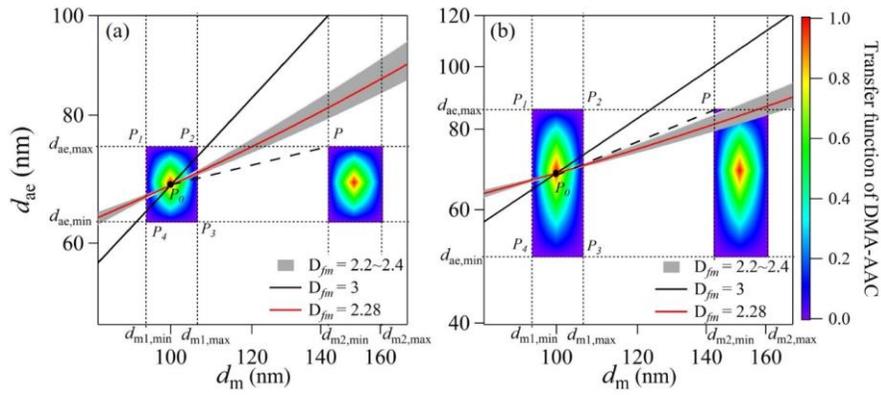
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629 **Figure 3: Variations of the slope of  $PP_0$  as a function of classified  $d_m$  and  $m$ . The following parameter set was**  
 630 **employed for the calculations:  $\beta_{DMA} = 0.1$ ,  $Q_{CPMA} = 0.3 \text{ L min}^{-1}$ ,  $R_m = 8$ . The contour lines denote the critical slope**  
 631 **of  $PP_0$ , with values labeled on them. The data points are soot particles measured in the literature (Park et al., 2003;**  
 632 **Rissler et al., 2013; Tavakoli et al., 2014; Ait Ali Yahia et al., 2017; Dastanpour et al., 2017; Forestieri et al., 2018;**  
 633 **Pei et al., 2018; Kazemimanesh et al., 2019) and generated in this study (see details in Sect 3.2). The  $D_{fm}$  values of**  
 634 **these data points are listed in the legend. The data points become square when  $D_{fm}$  is smaller than the critical**  
 635 **slope of  $PP_0$  in the background, i.e., the potential multiple charging effect may exist.**



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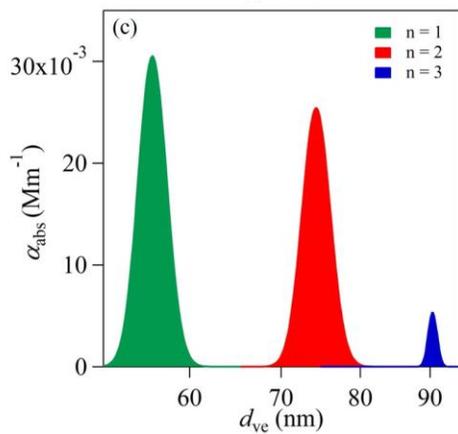
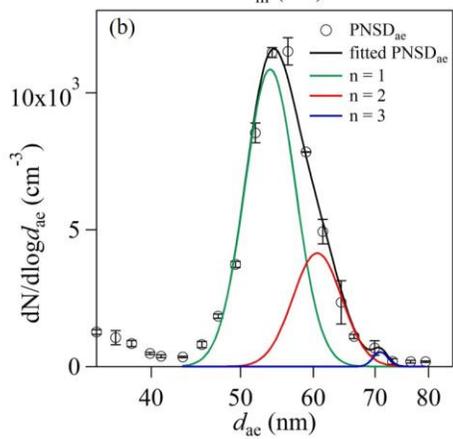
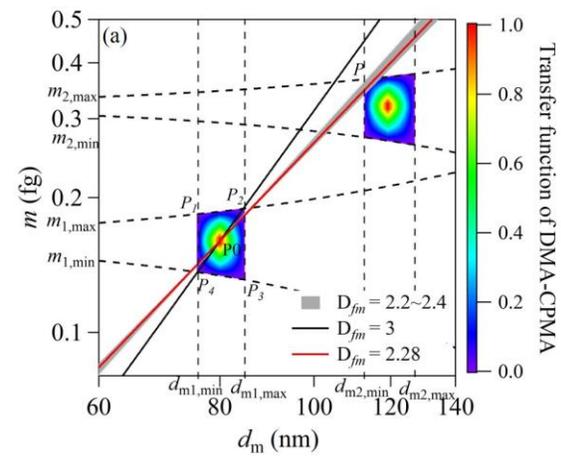
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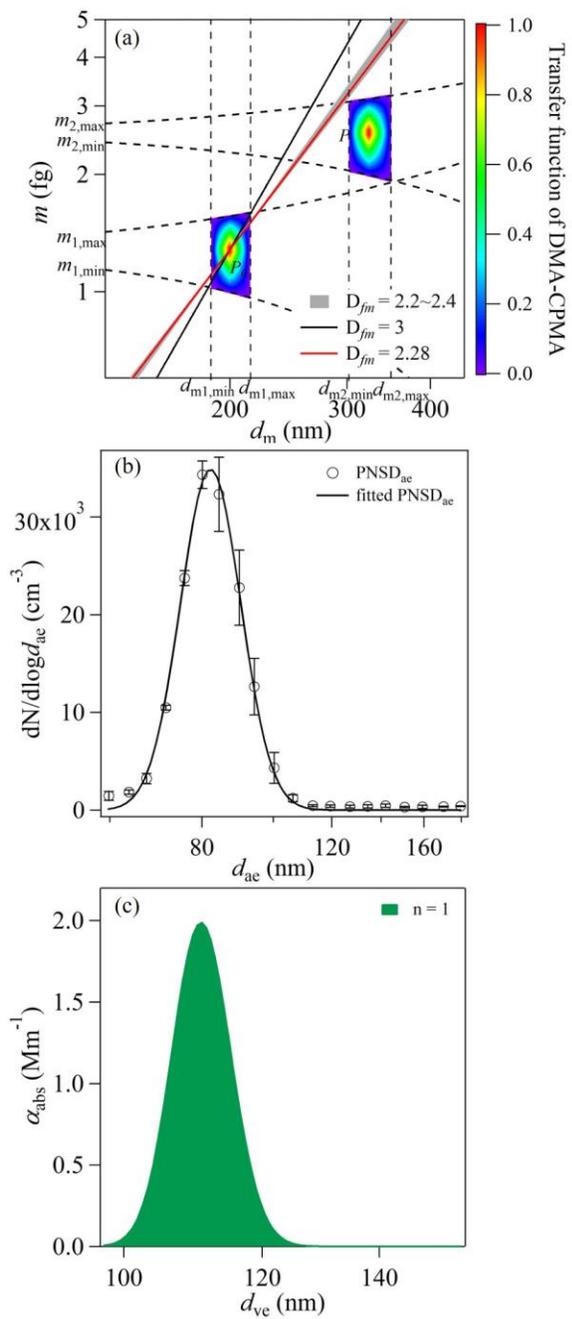
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Figure 4: Examples of transfer function calculation of DMA-AAC of flame-generated soot particles (Pei et al., 2018). The following parameter set was employed for the calculations:  $Q_a=0.3 \text{ L min}^{-1}$ ,  $d_{m1} = 100 \text{ nm}$ ,  $d_{ag} = 68.3 \text{ nm}$ , (a)  $\beta_{DMA} = 0.1$ ,  $\beta_{AAC} = 0.1$ , (b)  $\beta_{DMA} = 0.1$ ,  $\beta_{AAC} = 0.3$ . The color blocks are the transfer functions of DMA-AAC. The black and red solid lines are particle populations with  $D_{fm}$  values of 3 and 2.28, respectively. The gray region is the particles population with  $D_{fm}$  of 2.2-2.4, which is typical for soot aerosol. The dashed line is the critical slope of PP0. The dotted lines are the limiting  $d_m$  and  $d_{ag}$  of DMA and AAC, respectively.



644 Figure 5: (a) Transfer functions of DMA-CPMA when selecting 80 nm and 0.16 fg particles. The following  
645 parameter set was employed for the calculations:  $d_{m1} = 80$  nm,  $\beta_{DMA} = 0.1$ ,  $m_1 = 0.16$  fg,  $Q_{CPMA} = 0.3$  L min<sup>-1</sup>,  $R_m =$   
646 **8**. The red solid line is the generated soot particle population. (b) The aerodynamic size distribution of particles  
647 classified by DMA-CPMA. The circles are data measured by AAC-CPC, and the black, green, red and blue lines  
648 are log-normal fitted distributions of bulk, singly charged, doubly charged and triply charged particles  
649 populations. (c) The contributions to light absorption of particles with single, double and triple charges calculated  
650 with Mie theory.



652 **Figure 6: (a) The transfer functions of DMA-CPMA when selecting 200 nm and 1.28 fg particles. The following**  
653 **parameter set was employed for the calculations:  $d_{m1} = 200$  nm,  $\beta_{DMA} = 0.1$ ,  $m_1 = 1.28$  fg,  $Q_{CPMA} = 0.3$  L min<sup>-1</sup>,  $R_m =$**   
654 **8. The red solid line is the generated soot particle population. (b) The aerodynamic size distribution of particles**  
655 **classified by DMA-CPMA. The circles are data measured by AAC-CPC, and the solid line is the log-normal fitted**  
656 **distribution. (c) Contributions to light absorption of particles with a single charge calculated with Mie theory.**

657