



# A Software Package to Simplify Tikhonov Regularization with Examples for Matrix-Based Inversion of SMPS and HTDMA Data

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**Abstract.** Tikhonov regularization is a tool for reducing noise amplification during data inversion. This work introduces *RegularizationTools.jl*, a general-purpose software package to apply Tikhonov regularization to data. The package implements well-established numerical algorithms and is suitable for systems of up to ~1000 equations. Included is an abstraction to systematically categorize specific inversion configurations and their associated hyperparameters. A generic interface translates

- 5 arbitrary linear forward models defined by a computer function into the corresponding design matrix. This obviates the need to explicitly write out and discretize the Fredholm integral equation, thus facilitating fast prototyping of new regularization schemes associated with measurement techniques. Example applications include the inversion involving data from scanning mobility particle sizers (SMPS) and humidified tandem differential mobility analyzers (HTDMA). Inversion of SMPS size distributions reported in this work builds upon the freely-available software *DifferentialMobilityAnalyzers.jl*. The speed of
- 10 inversion is improved by a factor of ~200, now requiring between 2 and 5 ms per SMPS scan when using 120 size bins. Previously reported occasional failure to converge to a valid solution is reduced by switching from the L-curve method to generalized cross-validation as the metric to search for the optimal regularization parameter. Higher-order inversions resulting in smooth, denoised reconstructions of size distributions are now included in *DifferentialMobilityAnalyzers.jl*. This work also demonstrates that an SMPS-style matrix-based inversion can be applied to find the growth factor frequency distribution from
- 15 raw HTDMA data, while also accounting for multiply-charged particles. The outcome of the aerosol-related inversion methods is showcased by inverting multi-week SMPS and HTDMA datasets from ground-based observations, including SMPS data obtained at Bodega Bay Marine Laboratory during the Calwater 2/ACAPEX campaign, and co-located SMPS and HTDMA data collected at the U.S. Department of Energy observatory located at the Southern Great Plains site in Oklahoma, U.S.A. Results show that the proposed approaches are suitable for unsupervised, nonparametric inversion of large-scale datasets as well as
- 20 inversion in real-time during data acquisition on low-cost reduced-instruction-set architectures used in single-board computers. The included software implementation of Tikhonov regularization is freely-available, general, and domain-independent, and thus can be applied to many other inverse problems arising in atmospheric measurement techniques and beyond.

# 1 Introduction

Atmospheric aerosol play an important role in shaping the microphysics of clouds and the Earth's climate (Farmer et al., 2015; Kreidenweis et al., 2019). To predict the impact of aerosol on the Earth system, the distributions of particle size, chemical



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composition, hygroscopicity, and morphology must be known. Together these contribute to the mixing state of the aerosol. Accurate measurements of these distributions are critical for formulating models that link aerosol, cloud, and climate properties (Riemer et al., 2019).

Differential mobility analyzers (DMAs) select particles as a function of their size, charge, and an applied voltage. DMAs and tandem DMAs are widely used to measure the distributions of size and distributions of aerosol physicochemical properties

- (Park et al., 2008). For examples, a single DMA can be used to measure the aerosol size distribution by scanning voltage (Wang and Flagan, 1990). Humidified tandem DMAs (HTDMAs) can be used to measure the growth factor or hygroscopicity frequency distribution (Gysel et al., 2009). DMA-particle mass analyzer measurements can be used to resolve particle density distributions (Rawat et al., 2016; Sipkens et al., 2020). Tandem DMAs are important because they are one of only a handful
- 35 techniques that can specifically characterize aspects of the aerosol mixing state (Riemer et al., 2019). Unfortunately, particles carrying multiple charges and different sizes transmit through the DMA at a single voltage, which creates artifacts in the raw instrument response that must be removed during post-processing of the data.

Humidified tandem DMAs select a single particle mobility diameter, pass this quasi-monodisperse aerosol through a humidification system, and then measure the humidified mobility response function using a second DMA operated in stepping or

40 scanning mode (Rader and McMurry, 1986; Suda and Petters, 2013; Dawson et al., 2016). The humidified mobility response function is influenced by the particle size distribution, aerosol charge distribution, and growth factor frequency distribution function of the upstream aerosol. Gysel et al. (2009) show that the inversion from the humidified mobility response function to the growth factor frequency distribution is an ill-posed problem.

The inverse solution of ill-posed problems is characterized by strong sensitivity to noise superimposed on the data. Regular-

- 45 ization methods are needed to relate an observed instrument response to the underlying physical property of the system under investigation. A common inverse method is  $L_2$ -regularization, developed independently by Phillips (1962), Twomey (1963), and Tikhonov (1963). Some examples of  $L_2$ -regularization involving atmospheric measurement techniques include inversion to find aerosol microphysical properties from measurements of optical properties (Dubovik and King, 2000; Müller et al., 2019), retrieve trace gas concentrations from remote sensors (Borsdorff et al., 2014), or estimate fluxes from a combination
- 50 of measurements and atmospheric transport models (Krakauer et al., 2004). Application of  $L_2$ -regularization for problems involving DMAs include the reconstruction of the particle size distribution downstream of a single DMA (Wolfenbarger and Seinfeld, 1990; Kandlikar and Ramachandran, 1999; Talukdar and Swihart, 2003; Petters, 2018) and inversion to find size–mass distributions from coupled DMA-particle mass analyzer measurements (Rawat et al., 2016; Sipkens et al., 2020).

To date,  $L_2$ -regularization has not been applied to the inversion of HTDMA data. However, multiple other approaches have 55 been used to estimate the growth factor frequency distribution from the humidified mobility response function. Stolzenburg and McMurry (1988) introduce the TDMAfit method. TDMAfit assumes a multi-mode normally-distributed hygroscopic growth factor frequency distribution. Parameters of the growth factor frequency distribution are varied such that the error between the modeled and observed humidified mobility response-functions are minimized. Cubison et al. (2005) apply the optimal estimation method (OEM) to derive the growth factor frequency distribution. This method uses an estimate of the covariance

60 matrix, the measurements, and the forward model to retrieve the growth factor frequency distribution. The advantage of the





optimal estimation method over TDMAfit is that it is nonparametric, i.e., it makes no prior assumption about the shape of the growth factor frequency distribution. However, the method sometimes produces oscillatory and negative solutions. Gysel et al. (2009) introduce TDMAinv, a piecewise linear version of TDMAfit. The piecewise method is also nonparametric. Constrained minimization is applied to find the growth factor frequency distribution; this avoids the negative solutions encountered in the

- 65 optimal estimation method. Gysel et al. (2009) briefly discuss the role of multiple charges in the inversion and state that "the measured humidified mobility response function is a superposition of contributions from different dry sizes [...] and appropriate data inversion is hardly possible. Unfortunately an SMPS-style multicharge correction cannot be applied because the relative contributions from singly and multiply charged particles to every data point of the MDF cannot be distinguished." (In the direct quote, SMPS denotes scanning mobility particle sizer (Wang and Flagan, 1990) and MDF denotes mobility distribution
- function). Nevertheless, Shen et al. (2021) compute the contribution of multiply charged particles to the humidified mobility response function assuming that the larger multiply charged particles express the mean growth factor. However, they state that the correction of growth factor frequency distribution for multiply charged particles "is too complicated" (Shen et al., 2021) due to the need for multidimensional integration. Finally, Oxford et al. (2020) introduced a forward model named TAO that corrects for the contribution of multiply charged particle to the signal when interpreting volatility tandem DMA measurement.
- This work revisits the challenge to perform an SMPS-style inversion of the humidified mobility distribution to retrieve the growth factor frequency distribution while also accounting for multiply charged particles.  $L_2$ -regularization is used to find the inverse. The remainder of the work is structured as follows: Section 2 describes the theory of  $L_2$ -regularization and the numerical solution of the equations. The software package *RegularizationTools.jl* is introduced, which is a general domainindependent implementation of  $L_2$ -regularization. Forward models for transfer through the single DMA and tandem DMA
- are formulated using the formalism developed in Petters (2018) and cast into matrix form using abstractions introduced in *RegularizationTools.jl*. Section 3 uses synthetic data to demonstrate that  $L_2$ -regularization can be used to invert the humidified mobility distribution function to find the growth factor frequency distribution. Section 4 uses real-world data to showcase improvements for size distribution inversion and the newly introduced tandem DMA inversion that were added to the freely-available software package *DifferentialMobilityAnalyzers.jl* (Petters, 2018). Finally, Section 5 summarizes the improvements,
- 85 advantages, and limitations of the methodologies introduced in this work.

### 2 Theory

This work uses the following linear algebra notation. Capital bold-roman letters denote matrices, lower case roman letters denote vectors and italic symbols denote scalars.  $\mathbf{A}^{\mathrm{T}}$  denotes the matrix transpose, and  $\mathbf{A}^{+}$  the matrix pseudo-inverse.





# 2.1 L<sub>2</sub> Regularization

# 90 2.1.1 Theory

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The formalisms closely follow the description in Hansen (2000). Consider a system of equations

$$\mathbf{b} = \mathbf{A}\mathbf{x} + \boldsymbol{\epsilon} \tag{1}$$

where b is the measured response, A is the design matrix, x is the true quantity of interest, and  $\epsilon$  is the random error. The regular least-squares solution computed using the pseudo inverse via  $x = A^+b$  is often dominated by contributions from the error and the thus-obtained estimate for x is useless. Regularization addresses this issue by solving the minimization problem

$$x_{\lambda} = \arg\min\left\{ \|\mathbf{A}x - b\|_{2}^{2} + \lambda^{2} \|\mathbf{L}(x - x_{0})\|_{2}^{2} \right\}$$
(2)

where  $x_{\lambda}$  is the regularized estimate of x,  $\|\cdot\|_2$  is the Euclidean norm, **L** is a filter matrix,  $\lambda$  is the regularization parameter, and  $x_0$  is a vector of an *a-priori* estimate of the solution. The *a-priori* estimate can be taken to be  $x_0 = 0$  if no *a-priori* information is known. The filter matrix is often taken to be the identity matrix **I** or a derivative operator. Common choices are the first and second derivative operator defined as the bidiagonal(-1,1) and the upper tridiagonal(1,-2,1) matrix, respectively. For  $\lambda = 0$ , the solution is equivalent to  $x_{\lambda} = \mathbf{A}^+$ b. In the limit  $\lim_{\lambda \to \infty} x_{\lambda} = x_0$ . Thus the regularization parameter "interpolates" between the noisy ordinary least squares solution and the *a-priori* estimate  $x_0$ .

The analytical solution for Eq. (2) is the regularized normal equation

$$\mathbf{x}_{\lambda} = \left(\mathbf{A}^{\mathrm{T}}\mathbf{A} + \lambda^{2}\mathbf{L}^{\mathrm{T}}\mathbf{L}\right)^{-1}\left(\mathbf{A}^{\mathrm{T}}\mathbf{b} + \lambda^{2}\mathbf{L}^{\mathrm{T}}\mathbf{L}\mathbf{x}_{0}\right)$$
(3)

105 which is derived by taking the derivative of the right hand side of Eq. (2), setting it to zero, and solving for x. Equation (3) is in standard form if  $\mathbf{L} = \mathbf{I}$ . The optimal regularization parameter can be obtained using a variety of techniques, including the Lcurve method (Hansen, 2000) and generalized cross-validation (GCV, Golub et al., 1979). The L-curve methods involves a plot of  $\log \|\mathbf{A}x - b\|_2^2$  vs.  $\log \|\mathbf{L}(x - x_0)\|_2^2$ . The optimal  $\lambda$  occurs at the corner of the L-curve, which can be found algorithmically. The generalized cross-validation estimator is

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$$V(\lambda) = \frac{n \left\| (\mathbf{I} - \mathbf{A}_{\lambda}) \mathbf{b} \right\|_{2}^{2}}{tr(\mathbf{I} - \mathbf{A}_{\lambda})^{2}}$$
(4)

where  $\mathbf{A}_{\lambda} = \mathbf{A} \left( \mathbf{A} \mathbf{A}^{T} - \lambda^{2} \mathbf{I} \right)^{-1} \mathbf{A}^{T}$  is the influence matrix, tr is the matrix trace, and n is the size of b. The optimal  $\lambda_{opt}$  coincides with the global minimum of  $V(\lambda)$ . Equation (4) requires that the system is in standard form. For systems in non-standard form, conversion to standard form is required before computing  $V(\lambda)$ . In many cases  $\lambda_{opt}$  found by the L-curve and generalized cross-validation are similar, and the retrieved solutions  $\mathbf{x}_{\lambda}$  are nearly indistinguishable. Differences between these

115 two estimates are related to the computational speed-to-converge and robustness, i.e., that the system converges to the optimal solution.





# 2.1.2 Algorithms

Equation (3) can be solved straightforwardly using any software that supports linear algebra operations. This brute force approach, however, is slow. Efficient algorithms to solve Eqs. (3) and (4) have been developed. The algorithms used here are
briefly described. The regularized normal equations are transformed to standard form using the generalized singular value decomposition of A and L as derived by Eldén (1982) and summarized by Hansen (1998). Equation (3) is solved using Cholesky factorization when possible since it is the computationally fastest approach (Lira et al., 2016). If Cholesky factorization fails, one of the fallback solvers selected by the linear algebra package of the programming language is used. Equation (4) is solved using the singular value decomposition of A and the iterative algorithm described in Bates et al. (1986). The optimal λ<sub>opt</sub> for
generalized cross-validation is found by minimizing V(λ) on a bounded interval using Brent's method.

# 2.1.3 Classification of Methods

The inverse problem can be solved using specific methods. Here, method refers to the content of the filter matrix **L**, whether 130 an *a-priori* estimate is used, and whether constraints are imposed on the solution. Methods are encoded through the following expression

$$L_k x_0 D_\epsilon B_{[lb,ub]}(alg) \tag{5}$$

where L<sub>k</sub> denotes the order of the filter matrix L, x<sub>0</sub> denotes whether an *a-priori* estimate is used, D<sub>ε</sub> denotes whether data-based constraints are used (explained further below), and B<sub>[lb,ub]</sub> denotes whether a lower bound (lb) or upper bound
(ub) is imposed on the solution (explained further below). The argument ("alg") denotes constraints on the search algorithms, e.g., L\_curve or gcv and/or the bounded interval over which λ is varied. The expression is composable. For examples, the method L<sub>2</sub> denotes inversion using the second order derivative without an *a-priori* estimate, data-based constraints, and lower/upper bound constraints. The method L<sub>0</sub>B<sub>[0,1]</sub>(alg = L\_curve, λ<sub>1</sub> = 0.01, λ<sub>2</sub> = 100) denotes inversion with L = I, imposing that all x<sub>λ</sub> ∈ [0, 1], the use of the L-curve method, and λ<sub>opt</sub> ∈ [0.01, 100]. If alg is unspecified, defaults of alg = gcv, λ<sub>1</sub> = 0.001, λ<sub>2</sub> = 1000 are implied. This approach of method encoding provides a convenient classification system to enumerate the set of available methods as well as to specify the method in a high-level application interface for software function calls. There are eight combinations by which to compose methods via Eq. (5); combined with the three most common filter matrices L<sub>0</sub>= I, L<sub>1</sub> = bidiagonal(-1,1) and, L<sub>2</sub> = upper tridiagonal(1, -2, 1) this results in 24 unique methods.

145 *Data-based constraints:* Huckle and Sedlacek (2012) proposed a two-step data-based regularization where the filter matrix is modified according to

$$\mathbf{L} = \mathbf{L}_k \mathbf{D}_{\hat{x}}^{-1} \tag{6}$$





where L<sub>k</sub> is one of the finite difference approximations of a derivative, D<sub>x̂</sub> = diag(|x̂<sub>1</sub>|,...|x̂<sub>n</sub>|), x̂ is the reconstruction of x using L<sub>k</sub>, and (D<sub>x̂</sub>)<sub>ii</sub> = ε ∀ |x̂<sub>i</sub>| < ε, with ε << 1. The method L<sub>1</sub>D<sub>0.01</sub> represents a filter matrix with a first-order derivative
operator applied to Eq. (6) with ε = 0.01.

Lower/upper bound constraints: The retrieved x<sub>λ</sub> from the regularized normal equation can have oscillatory and/or nonphysical solutions. An alternative approach is to treat Eq. (2) as a constrained minimization such that the solution is subject to the optional constraint x<sub>lb</sub> < x < x<sub>ub</sub>. Here, the following procedure is implemented for the bounded search: first, the optimal λ<sub>opt</sub>
155 is found using the regularized normal equations. The thus-obtained solution x<sub>λ</sub> is truncated at the upper and lower bounds and then passed as an initial condition to a least-squares numerical solver. The Ceres solver (Agarwal et al.) is used with the Dogleg method and QR solver as implemented in the freely-available *LeastSquaresOptim.jl*<sup>1</sup> library. The upper and lower bounds are

#### 2.1.4 Software Implementation

vectors of the same size asx.

160  $L_2$ -regularization, as described in the previous sections, is implemented in a freely-available software package *Regularization-Tools.jl* that is written by the author and provided as a supplement to this work. The implementation is in the Julia programming language (Bezanson et al., 2017). The package has a similar name and some overlap with the package Regularization Tools by Hansen (2007). However, the packages differ in software architecture, programming language, and scope. *Regularization-Tools.jl* provides a simple high-level interface to compute  $x_\lambda$  using a single function call, for example

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$$x\lambda = invert(A, b, L_k x_0 B(k, x_0, lb, ub); alg =: L_curve)$$
 (7)

where A is the design matrix, b is the observation vector,  $L_k x_0 B$  is a parameterized algebraic data type that encodes the specific method. The hyper parameter k specifies the order,  $x_0$  specifies a vector of the initial guess, lb and ub specifies vectors of the lower and upper bounds. Other methods can be specified according to Eq. (5). Examples are provided in the documentation of the package.

# 170 2.2 Computing the Design Matrix

The design matrix can be obtained from a forward model

$$\mathbf{y} = F(\mathbf{x}, \mathbf{c}) \tag{8}$$

where y is a vector representing the error-free observations, x is the vector of true inputs, c is a vector of controlling parameters, and F is the linear forward model function that maps over x to compute y subject to the constraint of c. The matrix of the linear 175 transformation y = Ax is then given by

$$\mathbf{A} = [F(\mathbf{e}_1) \ F(\mathbf{e}_2) \ \dots \ F(\mathbf{e}_n)] \tag{9}$$

<sup>&</sup>lt;sup>1</sup>https://github.com/matthieugomez/LeastSquaresOptim.jl





where e<sub>1</sub>,...,e<sub>n</sub> is the standard basis. *RegularizationTools.jl* also provides abstract generic interface that simplifies computation of the design matrix from arbitrary forward models of linear processes. Examples demonstrating how to use this generic interface are provided in the documentation of the package. The examples include the solution for transit through the tandem
DMA described further below, the solution of the Fredholm integral equation of the first kind given by Baart (1982), the optical convolution that underlies size distribution retrieval from scattering and absorption properties (Müller et al., 2019), and the 2D Gaussian blur function encountered in image processing.

## 2.3 Design Matrices For Differential Mobility Analyzers

Differential mobility analyzers consist of two electrodes held at a constant- or time-varying electric potential. Cylindrical
(Knutson and Whitby, 1975) and radial (Zhang et al., 1995; Russell et al., 1996) electrode geometries are the most common. Charged particles are deflected to an exit slit and measured by a suitable detector, usually a condensation particle counter. The fraction of particles carrying k charges is described by a statistical distribution that is created by the charge conditioner used upstream of the DMA. The functions governing the transfer through bipolar charge conditioners, single DMAs, and tandem DMAs is well understood (Knutson and Whitby, 1975; Rader and McMurry, 1986; Reineking and Porstendörfer, 1986; Wang

190 and Flagan, 1990; Stolzenburg and McMurry, 2008; Jiang et al., 2014). These functions are usually cast in the form of a Fredholm integral equation and discretized to find the inversion matrix.

Petters (2018) introduced a formal language to simplify this process. At the core of the language are size distributions encoded as a *SizeDistribution* composite data type. Composite data types combine multiple arrays into a single symbol for ease of use, facilitating faster experimental design and analysis. *SizeDistribution* consists of vectors of bin edges, bin midpoints,

- 195 number concentration, log-normalized spectral density, and logarithmic bin widths. *SizeDistributions* are denoted in blackboard bold font (e.g., n, r, etc.). *SizeDistributions* are the building block of composable algebraic expressions that evaluate to transformed *SizeDistributions*. For examples,  $n_1 + n_2$  is the superposition of two size distributions, f \* n is the uniform scaling of the concentration fields by factor f, T.\*n is the elementwise scaling of the concentration fields by factor T, A\*n is matrix multiplication of A and concentration fields of the size distribution,  $f \cdot n$  is the uniform scaling of the diameter field of the
- 200 size distribution by factor f, and T · n is the elementwise scaling of the diameter field by factor T. DMA geometry, dimensions, and configuration are abstracted into composite types Λ (configuration comprising flow rates, power supply polarity, and thermodynamic state) and δ (DMA domain defined by a mobility/size grid). Each DMA is fully described by a pair Λ,δ. Subscripts and superscripts are used to distinguish between different configurations in chained DMA setups, e.g. δ<sub>1</sub> and δ<sub>2</sub> denoting the first and second DMA, respectively. Application of size distribution expressions to transfer functions constructs
- 205 a concise model of the transmitted DMA mobility distribution, denoted as the DMA response function. Implementation of the language is distributed through a freely-available and independently documented package *DifferentialMobilityAnalyzers.jl*, written in the Julia language.

Petters (2018) shows that the convolution matrix for passage through a single DMA is given by the expression

$$\mathbf{A} = (\operatorname{hcat}(\operatorname{map}(z^s \to \sum (k \to T_{size}^{\Lambda,\delta}(k, z^s), m), Z)...))^T$$
(10)



measurement uncertainties.



where ∑(f,m) evaluates the function f(x) for x = [1,...,m] and sums the result, m is the upper number of multiply charged particles, Z is a vector of centroid mobilities scanned by the DMA, hcat() is a function that concatenates arrays, "..." is the Julia splatting operator, which combines multiple arguments passed to the function hcat() into a single variable, and T<sup>A,δ</sup><sub>size</sub>(k, z<sup>s</sup>) = Ω(Z, z<sup>s</sup><sub>k</sub>).\*T<sub>c</sub>(k, D<sub>p,1</sub>).\*T<sub>l</sub>(D<sub>p,1</sub>) is a function that evaluates to a vector representing the fraction of particles carrying k charges that exit DMA<sup>A,δ</sup> as a function of diameter, Ω is the diffusing DMA transfer function (Stolzenburg and McMurry, 2008), T<sub>c</sub>
is the charge frequency distribution (Wiedensohler, 1988), and T<sub>l</sub> is the diameter-dependent transmission loss (Reineking and Porstendörfer, 1986). The size distribution after passage through the DMA is given by r = An + ε, where r is the response function, n is the true size distribution, and ε is a vector denoting the random error that may be superimposed as a result of

The mobility distribution exiting DMA 2 in the humidified tandem DMA is evaluated using the expressions

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$$\mathbb{M}_{k}^{\delta_{1}} = \left(\frac{D_{1}(z^{s})}{D_{k}(z^{s})}\right) \cdot \left(gf_{k}(z^{s}, gf_{0}) \cdot \left(T_{size}^{\Lambda, \delta}(k, z^{s}) * \mathbb{n}^{cn}\right)\right)$$
(11)

$$\mathbf{m}_{t}^{\delta_{2}} = \mathbf{O} * \left( \sum_{k=1}^{m} \mathbb{M}_{k}^{\delta_{1}} \right)$$
(12)

In Eq. (11),  $\mathbb{M}_{k}^{\delta_{1}}$  evaluates to the size distribution of particles that exit the DMA<sup> $\Lambda,\delta$ </sup> at the nominal setpoint-diameter defined by mobility  $z^{s}$  (or z-star) in DMA 1 and particle charge k. Subscripts are used to differentiate DMA 1 and 2 which possibly have different geometries, flow rates, and grids, e.g.  $\Lambda_{1}$ ,  $\Lambda_{2}$  and  $\delta_{1}$ ,  $\delta_{2}$ .  $D_{k}(z^{s})$  is the mobility diameter selected by the DMA if the particle carries k charges,  $gf_{0} = D_{wet}/D_{dry}$  is the true diameter growth factor,  $D_{dry}$  is the selected diameter by DMA 1,  $D_{wet}$ is the diameter after the humidifier,  $gf_{k}(z^{s}, gf_{0})$  is the effective growth factor for particles carrying k charges,  $T_{size}^{\Lambda,\delta}(k, z^{s})$  is as in Eq. (10), and  $\mathbb{n}^{cn}$  is the size distribution upstream of DMA 1. In Eq. (12),  $\mathbb{m}_{t}^{\delta_{2}}$  is the total humidified mobility distribution exiting DMA 2, m is upper number of charges on the multiply charged particles, Z is a vector of centroid mobilities scanned by

DMA 2, and O = (hcat(map(z<sup>s</sup> → ∑(k→Ω<sup>Λ<sub>2</sub>,δ<sub>2</sub></sup>(Z, z<sup>s</sup><sub>k</sub>). \*T<sup>Λ<sub>2</sub>,δ<sub>2</sub>(D<sub>p,1</sub>),1),Z)...))<sup>T</sup> is the convolution matrix for transport through DMA 2. Equations (11) and (12) are identical to those given in Petters (2018), except for the gf<sub>k</sub>(z<sup>s</sup>,gf<sub>0</sub>) function, which was then assumed to be a constant. This is incorrect. Particles carrying more than a single charge alias at a smaller particle size (Gysel et al., 2009; Shen et al., 2021). The effect is due to the size dependence of the slip-flow correction factor. The function must be solved iteratively and is now included in the *DifferentialMobilityAnalyzers.jl* package. Equation (11),
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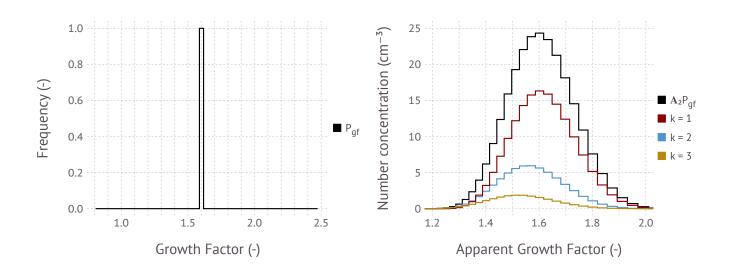
and specifically  $gf_k(z^s, gf_0)$ , assumes that  $gf_0$  applies to all particle sizes.

If the aerosol is externally mixed, the humidified distribution function is given by

$$\mathbf{m}_{t}^{\delta_{2}} = \int_{0}^{\infty} P_{gf} \left[ \mathbf{O} * \left( \sum_{k=1}^{m} \mathbb{M}_{k}^{\delta_{1}} \right) \right] dgf_{0} \tag{13}$$







**Figure 1.** Left: Input growth factor frequency distribution assuming that all particles have a single growth factor ~1.6. Right: Modeled apparent mobility distribution function calculated using Eq. (15) and partial distributions for individual charges k = +1, +2, +3 computed via  $\mathbf{O} * \mathbb{M}_{k}^{\delta_{1}}$ . The example is free of measurement error, i.e.,  $\epsilon = 0$ . The black trace is observed.

where  $P_{gf}$  is the growth factor frequency distribution.  $m_t^{\delta_2}$  in Eq. (13) is the forward model through the tandem DMA. Using the notation in section 2.2,

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$$F(\mathbf{x},\mathbf{c}) = \int_{0}^{\infty} P_{gf} \left[ \mathbf{O} * \left( \sum_{k=1}^{m} \mathbb{M}_{k}^{\delta_{1}} \right) \right] dg f_{0}$$
(14)

where x is the true  $P_{gf}$  and the vector c of constraining parameters comprises the DMA setup  $\Lambda_1, \Lambda_2, \delta_1, \delta_2$  and upstream size distribution  $n^{cn}$ . Computer code that creates a forward model for tandem DMAs has been added to the *DifferentialMobiltyAnalyzers.jl* package and is annotated in the documentation of the package. The forward model is used to cast Eq. (14) into matrix form such that the humidified mobility distribution function is given by

$$\mathbf{245} \quad \mathbf{m}_t^{\mathbf{o}_2} = \mathbf{A}_2 P_{gf} + \epsilon \tag{15}$$

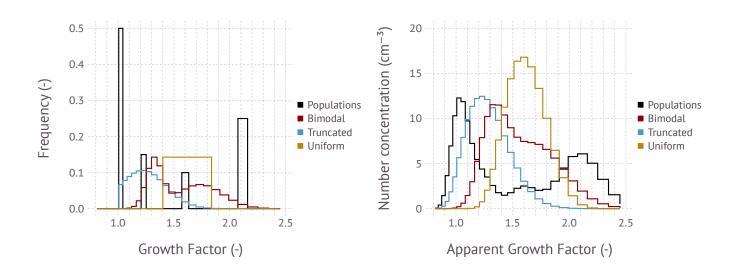
where the subscript 2 specifies transmission through DMA 2, the matrix  $A_2$  is understood to be computed for a specific input aerosol size distribution, and  $\epsilon$  is a vector that denotes the random error that may be superimposed as a result of measurement uncertainties. The size of  $A_2$  is  $n^2$ , where n is the number of bins in the growth factor frequency distribution.

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Figure 1 shows an example application of Eq. (15) for an input growth factor frequency distribution where all particles are assumed to have the same growth factor ~1.6. The frequency distribution is evaluated along a discrete growth factor grid with 60 bins. The assumed input size distribution is bimodal with mode diameters of 60 and 140 nm, geometric standard deviations of 1.4 and 1.6, and number concentrations of 1300 and 2000 cm<sup>-3</sup> in modes 1 and 2, respectively. The assumed sheath-to-sample flow ratios are 5:1 in both DMAs. The product  $A_2P_{gf}$  is the raw response that would be measured by a condensation







**Figure 2.** *Left:* Illustrative input growth factor frequency distributions. *Right:* Corresponding modeled apparent mobility distribution function calculated using Eq. (15). The example is free of measurement error, i.e.  $\epsilon = 0$ .

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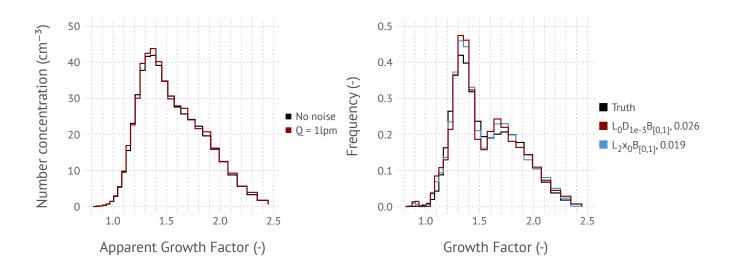
particle counter at the exit of the instrument. Contribution of +1, +2, and +3 charged particles to the total can be computed via  $\mathbf{O} * \mathbb{M}_{k}^{\delta_{1}}$ . Although the nominal growth factor is the same for all sizes, the apparent mode of the growth factor decreases with increasing particle charge (see also Gysel et al., 2009; Shen et al., 2021). Therefore the axis is denoted as the apparent growth factor. Summing the partial distributions results in  $\mathbf{A}_{2}P_{gf}$ , demonstrating that the matrix equation correctly maps  $P_{gf}$ to the response, including multiply charged particles.

Figure 2 shows the relationship between four illustrative growth factor frequency distributions and the modeled apparent mobility distribution functions. The selected examples comprise a testbed to evaluate the feasibility of an SMPS-style matrixbased inversion to recover  $P_{gf}$ . The *Populations* example consists of an external mixture with compositions corresponding to four unique growth factors. The *Bimodal* example is the superposition of two Gaussian distributions with 70% of particles in the less hygroscopic mode. The *Truncated* example is a Gaussian distribution truncated at gf = 1.0. The *Uniform* example is a uniform distribution over a fixed interval. All frequency distributions sum to unity, thus accounting for 100% of the particle population. The dry diameter and assumed input size distribution to compute the matrix  $A_2$  is the same as in Fig. 1. However, unlike in Fig. 1, the frequency distribution and matrix are evaluated along a coarser discrete growth factor grid with 30 bins. Note that the growth factor bin width is not constant, with wider bins at larger growth factors. This is due to the evaluation of the humidified size distribution along a geometrically stepped mobility grid, which is typical in scanning DMA setups. As will be shown next, 30-bin resolution is a suitable compromise between speed, accuracy, and resolution when computing the matrix-based inversion to infer  $P_{gf}$  from noise-perturbed apparent growth factor frequency distributions.

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**Figure 3.** Left: Humidified apparent growth factor distribution function for the *Bimodal* example comprising superposition of two Gaussian distributions with 70% of particles in the less hygroscopic mode. The distributions are calculated  $m_t^{\delta_2} = \mathbf{A}_2 P_{gf} + \epsilon$ . "No noise" corresponds to  $\epsilon = 0$ . "Q = 1 l pm" corresponds to simulated Poisson noise equivalent for a condensation particle counter measuring at a flow rate of 1 L min<sup>-1</sup> and bin integration time of 2 seconds per bin. *Right:* Inverted size distribution using the  $L_0 D_{1e-3} B_{[0,1]}$  and  $L_2 x_0 B_{[0,1]}$  method. The *a-priori* estimate  $x_0$  is the normalized apparent growth factor distribution. Values in the legend (0.026 and 0.019) correspond to the root mean square error between the true input (Truth) and the regularized solution.

Simulated examples are used to test if Eq. (15) is invertible. Figure 3 shows an example simulation for the Bimodal growth

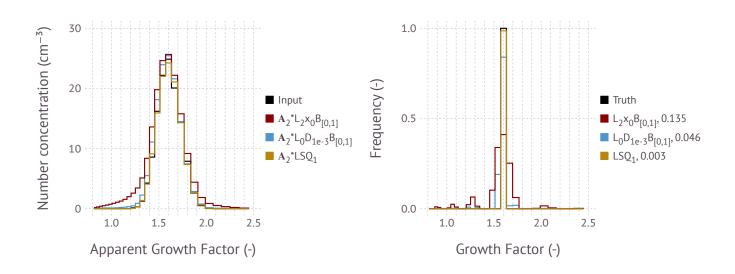
## 3 Matrix Inversion of the Humidified Mobility Distribution Function using Synthetic Data

factor distribution test case. The humidified apparent growth factor distributions are calculated using Eq. (15). The noise-free example corresponds to ε = 0 and represents the idealized measurement. Poisson counting statistics are simulated by
converting concentration to the expected number of counts for a typical particle counter flow rate and bin integration time. Counts in each bin are computed by drawing a pseudo-random number from a Poisson distribution and converting the result back to concentration. Lower flow rates and shorter integration times increase the noise-perturbation of the apparent growth factor distribution is then inverted using the L<sub>0</sub>D<sub>1e-3</sub>B<sub>[0,1]</sub> and L<sub>2</sub>x<sub>0</sub>B<sub>[0,1]</sub> method. Here B<sub>[0,1]</sub> is shorthand for setting all lower bounds equal to zero and all upper bounds equal to one. The *a-priori* estimate
x<sub>0</sub> is taken to be the normalized apparent growth factor frequency distribution is known, the fidelity of the inversion can be evaluated by computing the root mean square error between the noise-free solution and the regularized solution. The figure shows that both inversion methods produce a root mean square error between 0.02 and 0.03. These values are typical for the of reconstruction (see supporting information). Visual evaluation of the agreement between the reconstruction and the input

suggest that either method is suitable for inversion.







**Figure 4.** *Left:* Humidified apparent growth factor distribution function assuming that all particles have a single growth factor ~1.6. The black histogram corresponds to the input to the inversion, which is the noise-perturbed apparent growth factor distribution with simulated Poisson noise equivalent for a condensation particle counter measuring at a flow rate of 1 L min<sup>-1</sup> and bin integration time of 2 s per bin. Color lines depict the predicted apparent growth factor distributions based on the corresponding inversion shown in the right panel. *Right:* Inverted growth factor frequency distribution from the noise-perturbed spectrum. The true growth factor frequency distribution (black line) is obscured behind the gold and blue lines and is as in Fig. 1, left panel. Colors correspond to the inverted size distribution using the  $L_0D_{1e-3}B_{[0,1]}$ ,  $L_2x_0B_{[0,1]}$ , and  $LSQ_1$  methods. The *a-priori* estimate  $x_0$  is the normalized apparent growth factor distribution. Values in the legend (0.135, ...) correspond to the root mean square error between the true noise-free solution and the proposed solution.

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have the same growth factor. Although the  $L_2 x_0 B_{[0,1]}$  approach correctly infers the most probable growth factor, the predicted distribution is incorrect. Multiple modes to the left and right of the main mode are observed. The  $L_2 x_0$  method produces an oscillatory solution with negative values (not shown). The small modes are the residual of this oscillatory solution that is truncated by the enforced [0,1] bound and the inability of the least-squares solver to converge on a better solution. A large root mean square error of 0.135 results. In contrast, the data-constrained method  $L_0 D_{1e-3} B_{[0,1]}$  leads to better reconstruction of the true input. The main advantage of the  $L_0 D_{1e-3} B_{[0,1]}$  inversion method over  $L_2 x_0 B_{[0,1]}$  is that it is better able to reconstruct inputs with sharp edges.

Figure 4 is similar to Figure 3, showing an example simulation for an aerosol with uniform composition, i.e., all particles

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The total number of composable regularization methods according to Eq. (5) is 24. Half of these methods do not include lower and upper bounds and these are not suitable for tandem DMA inversion due to the negative and oscillatory solutions for narrow inputs. The remaining 12 methods have been systematically tested using Monte-Carlo analysis described in detail in the supporting information. Briefly, 60000 inversions were performed on synthetic data similar to the examples shown in Figs. 3 and 4. The total number concentration, dry diameter, number of bins, and random seeds were varied and the root mean square error was evaluated for each simulation. Results compiled in Fig. S1 show that all of the methods perform equally well for the





Bimodal, Uniform, and Truncated Normal examples shown in Fig. 3. Method  $L_0 D_{1e-3} B_{[0,1]}$  outperforms the other methods 300 for grids with 20 and 30 growth factor bins and test cases with either one (e.g., Fig. 4) or two discrete populations. However, even  $L_0 D_{1e-3} B_{[0,1]}$  can lead to results similar to the example  $L_2 x_0 B_{[0,1]}$  shown in Fig. 4 for some random seeds. Higher resolution grids generally lead to poor performance even for method  $L_0 D_{1e-3} B_{[0,1]}$ .

An alternative approach to fit single component data is to perform a nonlinear least squares fit to match the apparent growth factor distribution using the forward model while restricting the number of compositions to either one or two. This corresponds 305 to a two- or four-parameter fit. Results from this procedure are either one or two growth factors and one or two fractions. The corresponding methods are denoted as  $LSQ_1$  and  $LSQ_2$ , respectively. In the example shown in Fig. 4,  $LSQ_1$  has the smallest root mean square error and is the best method to reconstruct the true growth factor. The  $LSQ_1$  method is most suitable to infer the growth factor for laboratory measurements when it is known that the aerosol is internally mixed and only a single growth

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      factor is expected.
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Which method, however, should be selected when inverting real-world data and the number of components is unknown? Since the true solution is also unknown, the root mean square error between the truth and reconstruction is unavailable. It is, however, possible to compute the residual between the measured apparent growth factor distribution and the predicted apparent growth factor distribution from different reconstructions. A large residual can be used to flag truncated oscillatory solutions

- such as  $L_2 x_0 B_{[0,1]}$  for narrow/single composition cases. Similarly, the residual is high is the true input is a broad growth 315 factor frequency distribution that is attempted to be fitted using  $LSQ_1$ . For example, the red spectrum in the left graph of Fig. 4 shows poor agreement with the input and results in a much larger residual than  $LSQ_1$  (values not shown). Therefore, a proposed unsupervised inversion scheme is to compute the solution of  $LSQ_1$ ,  $LSQ_2$  and  $L_0D_{1e-3}B_{[0,1]}$  and then select the solution with the lowest residual relative to the apparent growth factor distribution.
- 320 A limitation of the above approach is that the forward model (and thus matrix  $A_2$ ) assumes that the larger multiply charged particles have the same growth factor frequency distribution as the smaller singly charged particles. This limitation can in principle be eliminated by specifying a 2D probability frequency distribution that also depends on dry diameter. Constructing an appropriate forward model that adds another integration dimension to Eq. (14) is straightforward. An inversion that solves for the 2D frequency distribution, similar to those performed elsewhere (Rawat et al., 2016; Sipkens et al., 2020), is feasible
- 325 using the algorithms in RegularizationTools. jl and has been attempted by the author. In practice, however, this approach proved impractical. For example, using 10 dry diameters and a 30-bin size resolution results in a large inversion matrix. Adding an integration dimension to the forward model and recomputing this matrix for each scan significantly slows the inversion. Furthermore, interpolation is needed to estimate the growth factor frequency distribution for the multiply charged particles. The physical size of the multiply charged particles depends on their charge. For example, +2 charged particles are approximately
- 1.5 times larger than +1 charged particles. The diameter of the multiply charged particles will therefore not necessarily coincide 330 with any of the 10 dry diameters selected for direct measurement. This introduces additional uncertainty due to assumptions that need to be made in the interpolation scheme. Errors from scans with low concentration at the edge of the size distribution propagate back into the inversion at other dry sizes. Finally, only a single size distribution can be used to compute the matrix A<sub>2</sub>. Collecting data for 10 dry sizes can take 20 min or longer, during which the aerosol size distribution may change, thus





335 invalidating the use of a single inversion matrix. Although no exhaustive analysis was performed, the compounding errors during a 2D inversion seem to outweigh the benefits of relaxing the assumption that +2 and +3 charged particles have the same growth factor frequency distribution as the +1 charged particles.

# 4 Inversion of Real-World Data

# 4.1 Data Sources

# 340 4.1.1 Bodega Bay Marine Laboratory

Aerosol size distribution data to contrast inversion schemes were obtained from measurements taken at Bodega Bay Marine Laboratory ( $39^{\circ}18'25''N 123^{\circ}3'58''W$ ) between 16 January 2015 and 8 March 2015 as part of the Calwater 2/ACAPEX campaign. A subset of the data have been published by Atwood et al. (2019). Sample flow was brought into a mobile laboratory using an inlet, dried to  $10 \pm 2\%$  relative humidity using a Nafion membrane drier, and brought to charge equilibrium using an

- 345 X-ray source (TSI 3088, TSI Inc., Shoreview, MN, U.S.A.) prior to entering a cylindrical DMA column (TSI 3080). The DMA was configured to measure the size distribution in scanning mobility particle sizer mode. Voltage was scanned exponentially from 10 kV to 10 V over 300 s. A condensation particle counter (TSI 3771, flow rate =  $1 \text{ L min}^{-1}$ ) and a cloud condensation nuclei counter (DMT Model 100, Droplet Measurement Technologies, Boulder, CO, U.S.A., flow rate =  $0.3 \text{ L min}^{-1}$ ) were used to measure particle concentration downstream of the DMA. The sheath-to-sample flow rate in the DMA was 5:1.3 L min<sup>-1</sup>.
- 350 Raw DMA response distributions comprising CPC concentration vs. apparent +1 mobility diameter were constructed along a 120-bin, geometrically-stepped mobility grid. Response distributions are denoted as r. The apparent +1 mobility diameter is computed from the centroid mobility selected by the DMA assuming that all particles are singly charged. The dynamic diameter range for this setup is from 12 to 550 nm. The inversion matrix **A** is computed using Eq. (10) for the diffusionallybroadened transfer function (Stolzenburg and McMurry, 2008) and transmission loss correction through the DMA (Reineking
- and Porstendörfer, 1986). Inclusion of these terms results in a more ill-posed inverse problem due to the addition of small terms in the matrix **A**. The DMA response functions were inverted using the  $L_0 x_0 B_{[0,\infty]}$  and  $L_2 B_{[0,\infty]}$  methods. The *a*-*priori* estimate for  $L_0 x_0 B_{[0,\infty]}$  was taken to be  $x_0 = S^{-1}r$ , where **S** is obtained by summing the rows of **A** and placing the results on the diagonal of **S** (Talukdar and Swihart, 2003). The method  $L_0 x_0 B_{[0,\infty]}$  with  $x_0 = S^{-1}r$  is essentially equivalent to the method used by Petters (2018), where it was shown that the thus-inverted spectra are similar to those output by the
- inversion algorithm employed by the commercial TSI Aerosol Instrument Manager software suite. Small differences between  $L_0 x_0 B_{[0,\infty]}$  employed here and the approach of Petters (2018) include the use of generalized cross-validation instead of the L-curve method to search for the optimal regularization parameter and the method to eliminate negative values after inversion. Petters (2018) truncated negative values instead of using a least squares numerical solver as described in section 2.1.3.





### 4.1.2 Southern Great Plains Site

- Aerosol size distribution and humidified tandem DMA data to illustrate the tandem DMA inversion schemes were taken from measurements made by the U.S. Department of Energy (DOE) Atmospheric Radiation Measurement (ARM) program. The Southern Great Plains (SGP) site is located in Lamont, OK, U.S.A. (Lat: 36.604937, Long:-97.485561) and placed in a rural continental setting that is surrounded by agricultural activity as well as oil and gas production. The aerosol evolution at the site is influenced by frequent new particle formation events (Hodshire et al., 2016; Chen et al., 2018; Marinescu et al., 2019).
  Number concentrations fluctuate in response to the nitrate and organic aerosol cycle on short time scales and synoptic weather variability on longer time scales. During winter months, the inorganic aerosol composition at the site is dominated by nitrate
  - aerosols (Jefferson et al., 2017; Mahish et al., 2018) and hygroscopicity derived from scattering measurements is largest during those months (Jefferson et al., 2017).
- The instruments/measurements are part of the Aerosol Observing System (AOS, Uin and Smith, 2020). The instruments are operated by DOE personnel and data are distributed through a publicly accessible archive. Size distributions were measured with a scanning mobility particle sizer (TSI Model 3936, Kuang, 2016). Data in the archive are already inverted and reported at 5-min intervals. Humidified DMA response functions were measured using a humidified tandem DMA (Model 3100, Brechtel Manufacturing, Inc., Hayward, CA, U.S.A.). The first and second DMA are operated at 5:0.63 L min<sup>-1</sup> and 5:1 L min<sup>-1</sup> sheathto-sample flow ratio, respectively (Janek Uin, personal communication). The instrument measures the humidified mobility distribution function at 85% relative humidity for 50, 100, 150, 200, and 250 nm dry diameter particles. Typical data density
- results in 228 scans per day, with equal coverage for the five dry sizes. Pre-processing that is already applied to the archived data accounts for conversion between mobility and apparent mobility diameter, the size-dependent detector counting efficiency, and number count smearing during the scan resulting from insufficient particle counter response time. When divided by the dry diameter, the archived data correspond to the apparent growth factor distribution evaluated by the forward model in Eq. (15).
- The matrix  $A_2$  was evaluated for each scan using the flow rates given above, the dimensions of the DMAs given in Lopez-Yglesias et al. (2014), and the aerosol size distribution measured by the co-located SMPS with the timestamp closest to the a scan of the humidified tandem DMA. Typical time differences between the two instruments' scan times are between 1 and 3 min. The humidified size distribution was interpolated onto a discrete growth factor grid with 30 bins to match the matrix  $A_2$ . The data were then inverted using the  $L_0D_{1e-3}B_{[0,1]}$  method. The method  $L_0D_{1e-3}B_{[0,1]}$  was further constrained such that
- 390 growth factors < 1 are disallowed. This is achieved by setting the upper bound to zero for bins with gf < 1. Growth factors less than unity can occur due to particle restructuring upon humidification (Mikhailov et al., 2004; Shingler et al., 2016) or evaporation during transit through the humidifier and second DMA. Both effects are assumed to be less important for ambient aerosol compared to the desire to constrain the inversion. In addition, the efficacy of the LSQ<sub>1</sub> and LSQ<sub>2</sub> methods for inverting the data was tested. For each scan, the root mean square error between the measured apparent growth factor distribution and the predicted growth factor distribution was evaluated for all three inversion approaches (L<sub>0</sub>D<sub>1e-3</sub>B<sub>[0,1]</sub>, LSQ<sub>1</sub>, and LSQ<sub>2</sub>).
- The method that resulted in the smallest residual was taken to be the inverted growth factor frequency distribution.





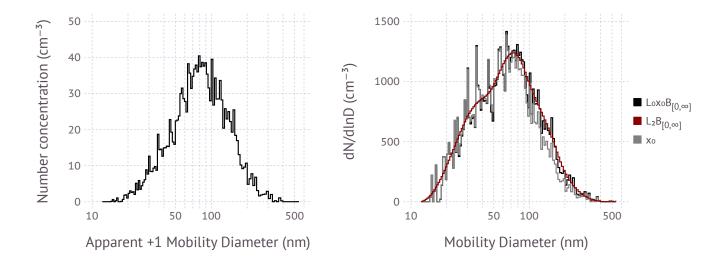


Figure 5. Left: Raw DMA response function for a single scan on 5 March 2015 at 10:40 UTC at Bodega Bay Marine Laboratory. Right: Inverted size distribution using the  $L_0 x_0 B_{[0,\infty]}$  and  $L_2 B_{[0,\infty]}$  method and the *a-priori* estimate of the solution  $x_0 = \mathbf{S}^{-1} \mathbf{r}$ .

#### 4.2 Results

#### Inversion of Size Distribution Data (Bodega Bay Marine Laboratory Site) 4.2.1

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Figure 5 shows a real-world example size distribution response function gridded into 120 size bins. The total particle concentration is  $\approx 2000 \text{ cm}^{-3}$ . The ragged structure is typically explained by random noise due to Poisson counting statistics. At this diameter resolution, and with inclusion of the diffusion and loss terms in the forward model, the unregularized matrix inverse is entirely dominated by amplified random noise and is useless. The  $L_0 x_0 B_{[0,\infty]}$  method converges to the solution with slight amplification of the random noise presented in the raw response function. The random noise is carried over into the *a-priori* estimate  $x_0 = S^{-1}r$ , which roughly represents the noise visible in the reconstructed solution. Nevertheless,  $L_0 x_0 B_{[0,\infty]}$  is 405 highly robust and unlikely to go astray, because  $x_0$  is an excellent approximation of the solution at diameters less than 100 nm where singly charged particles dominate and is a good initial estimate for larger particles. Second order inversion using  $L_2B_{[0,\infty]}$  produces a smooth, denoised solution due to application of the derivative operator in the regularization filter matrix. The solution converges even though no *a-priori* estimate is used, i.e.,  $x_0 = 0$ . The algorithms specified in Section 2.1.2 significantly speed up the inversion relative to previous versions of the software (Petters, 2018). Wall-clock times on an i7-8559U

CPU for the inversion of a single spectrum are 5 and 2 ms for  $L_0 x_0 B_{[0,\infty]}$  and  $L_2 B_{[0,\infty]}$ , respectively. This contrasts to 500 to 410 1000 ms required by the brute force algorithm – approximately equivalent to  $L_0 x_0 B_{[0,\infty]}$  – used previously. Finding the global minimum of  $V(\lambda)$  to identify the optimal regularization parameter also eliminates the occasional failure to converge when the L-curve algorithm is used (Petters, 2018). Either  $L_0 x_0 B_{[0,\infty]}$  or  $L_2 B_{[0,\infty]}$ , combined with generalized cross-validation, are suitable to be used in routine unsupervised inversion of size distribution data.





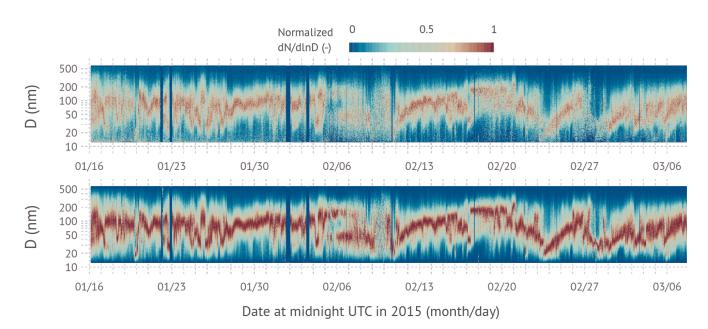


Figure 6. Time evolution of the normalized particle size distributions collected between 16 January and 7 March at Bodega Bay Marine Laboratry. The normalization is for each size distribution such that the maximum of the spectral density equals to unity. The red color visualizes the time evolution of the mode diameter of the dominant mode. Top panel: inverted using  $L_0 x_0 B_{[0,\infty]}$ ; bottom panel: inverted using  $L_2 B_{[0,\infty]}$ .

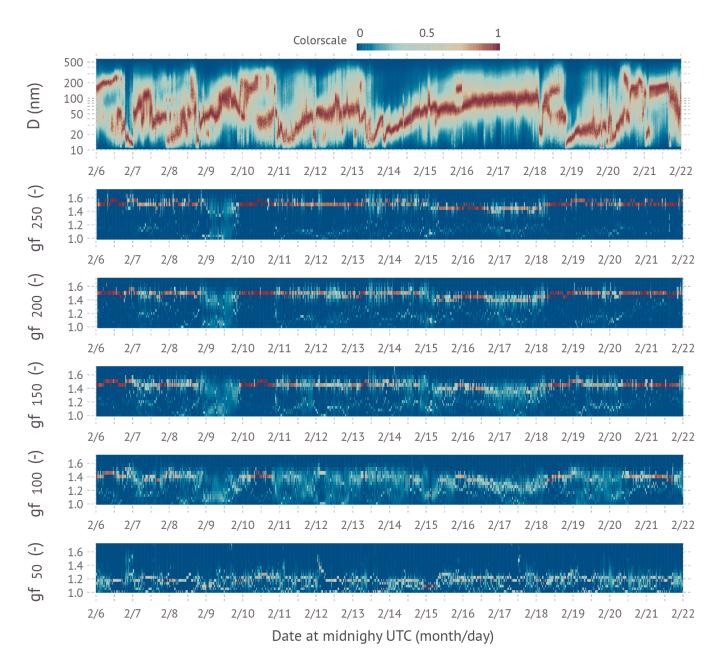
Figure 6 shows the time evolution of the normalized particle size distributions over a seven week period. The normalization is to highlight changes in the mode diameter(s). In general, the aerosol at the site is dominated by continental rural background conditions and the land-sea breeze circulation (Atwood et al., 2019). The timeseries is punctuated by aerosol transported from the California Central Valley to the site through the Petaluma Gap (Martin et al., 2017). Periods of low particle concentration occurred during the passage of an atmospheric river on 7 – 9 February 2015 and a marine inflow event on March 27 – 28 2015.
The atmospheric river brought heavy precipitation and marine airmasses from the southwest direction, while the marine inflow event brought strong winds and precipitation free maritime air from the northwest direction. Several periods of prolonged modal growth were observed starting, e.g., 9 February 2015, 24 February 2015, and 29 February 2015. Figure 6 demonstrates the influence of inversion noise on visualizing the dynamic evolution of the size distribution. The denoised L<sub>2</sub>B<sub>[0,∞]</sub> solution significantly improves visualization of modes without the need to reduce the size resolution in the inversion. The signal is especially improved during low concentration periods during the atmospheric river passage and marine inflow event.

# 4.2.2 Inversion Humidified Tandem DMA Data (DOE ARM SGP Site)

Figure 7 shows real-world examples of growth factor frequency distributions for five dry sizes. Also shown for context is the evolution of the normalized aerosol number size distribution. Figure 7 shows dynamic evolution of the size distribution







**Figure 7.** *Top:* Time evolution of the normalized particle size distributions collected between 6 February and 22 February at the Southern Great Plains research site. The normalization is for each size distribution such that the maximum of the spectral density equals to unity. *Second-Top to Bottom:* Inverted growth factor frequency distributions at 85% relative humidity for 250, 200, 150, 100, and 50 nm particles, respectively.





with sudden changes in mode diameter, several apparent new particle formation events, and several prolonged modal growth
events. The distribution of the methods selected for best inversion was LSQ1 (~5% of spectra), LSQ2 (~50% of spectra), and L<sub>0</sub>D<sub>1e-3</sub>B<sub>[0,1]</sub> (~45% of spectra). In Fig. 7, the LSQ2 inverted frequency distributions show a clean bimodal structure (2 colors per scan), while the L<sub>0</sub>D<sub>1e-3</sub>B<sub>[0,1]</sub> spectra appear more smeared. The 250 nm dry diameter data show a dominant contribution of more hygroscopic particles with gf ~1.5 - 1.6 and a small contribution of less hygroscopic particles with gf ~1.05 - 1.2. Similar trends are observed for 200, 150, and 100 nm particles. However, the hygroscopicity of the dominant mode
decreases with decreasing diameter. The fraction of cases where a broad hygroscopicity frequency distribution is observed is larger than for the 250 nm particles. Notably, time periods with broad growth factor frequency distribution at 100, 150, 200, and

250 nm dry diameter. Occasionally temporal trends in the hygroscopicity of the less hygroscopic mode are observed. For example, the growth factor of the less hygroscopic mode systematically increases on 20 February 2020 for 150, 200, and 250
nm particles, indicative of a chemical transformation of some, but not all, of the particles. The 50 nm dry particle hygroscopicity frequency distributions are also predominantly bimodal. However, the overall growth factor is significantly smaller, with most

gf < 1.2.

# 5 Discussion, Summary, and Conclusions

RegularizationTools.jl is a general purpose software package to invert data using  $L_2$ -regularization. It is included as a supplement to this work and published as free software through the GNU General Public License. The package implements well-established numerical algorithms (Golub et al., 1979; Eldén, 1982; Bates et al., 1986; Hansen, 1998, 2000; Mogensen and Riseth, 2018) and filter matrices (Huckle and Sedlacek, 2012). Systems with up to ~1000 equations can be inverted. The upper limit is determined by the need to compute the generalized singular value decomposition of the design matrix and filter matrix, which has at minimum  $O(n^2)$  time complexity. The time to compute the generalized singular value decomposition exceeds several 10s of seconds for systems exceeding 1000 equations. Iterative methods to support inversion of large-scale systems have been formulated (e.g. Lampe et al., 2012), but these are currently not implemented.

The software package can be used to simplify the prototyping of a wide variety of inverse problems that arise in science and engineering applications. Although the package does not add any novel regularization methods, it provides a systematic method to categorize inversion methods via the expression in Eq. (5). A total of 24 basic permutations can be combined with

- 455 a set of hyperparameters to attempt the inversion of ill-posed problems. Hyperparameters include boundary constraints, values for *a-priori* estimates, and the lower bound  $\epsilon$  for the Huckle and Sedlacek (2012) two-pass inversion approach. Users can define custom filter matrices and thus are able to further extend the number of methods. Equation (7) provides an example of a simplified interface that allows testing of different permutations with a simple function call. Furthermore, a generic interface is provided to translate arbitrary linear forward models defined by a computer function into the corresponding matrix of
- 460 linear transformation. This obviates the need to explicitly write out the Fredholm integral equation and discretize it using the quadrature or the Galerkin method. For example, the forward model for transfer of a growth factor frequency distribution



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through the tandem DMA in Eq. (14) represents a triple integral and also contains a sum term for the multiple charges. Explicit discretization of this model would be tedious compared to the method employed here. As demonstrated in the documentation of the package, the generic interface can readily be used to solve other common inversion problems. Only a few lines of new
code are needed to reproduce the essential core of the algorithm used in the unsupervised inversion of Lidar data (Müller et al., 2019), which involves the retrieval of a size distribution from multi-wavelength scattering and absorption data (see package documentation for code).

 $L_2$ -regularization has been used previously for size-distribution inversion (e.g. Wolfenbarger and Seinfeld, 1990; Talukdar and Swihart, 2003; Petters, 2018). However, to the author's knowledge the package *DifferentialMobilityAnalyzers.jl* is the only publicly available free-software for size distribution inversion from DMA data. This work extends the capabilities of that package. The  $L_0 x_0 B_{[0,\infty]}$  and  $L_2 B_{[0,\infty]}$  methods can be used with generalized cross-validation to perform fast unsupervised

inversion of size distribution data. Convergence issues resulting from the use of the L-curve method used previously (Petters, 2018) are resolved by switching to the generalized cross-validation approach to find the optimal regularization parameter. Higher-order inversions resulting in smooth, denoised solutions are now available. It is expected that such denoised spectra

- 475 will benefit unsupervised machine-learning approaches that seek to extract features from such datasets (e.g. Joutsensaari et al., 2018; Atwood et al., 2019), although this hypothesis has not been tested by the author. Revision of the numerical algorithms improves the speed of inversion by a factor ~200. The millisecond inversion speed for a single scan permits rapid inversion of large datasets and facilitates inversion in real-time during data acquisition on low-cost and low computational power hardware platforms. For example, the inversion has been tested on ARM Cortex A72/A53 64 bit reduced-instruction-set architecture used
- 480 by the ROCKPro64 single board computer. The Julia language provides tier 1 support for this architecture. Julia binaries are available; *DifferentialMobilitityAnalyzers.jl* and *RegularizationTools.jl* compile and run without any modification. Inversion speeds on the order of several 10s of milliseconds are fast enough on this inexpensive but relatively low-powered platform to permit embedding the inversion into the data acquisition and display software and running the inversion before each display update.
- To the author's knowledge this is the first time  $L_2$ -regularization has been applied to the inversion of tandem DMA data. Inversion of simulated data shows that the an SMPS-style matrix-based inversion is possible, while also accounting for multiply charged particles. Application of solution constraints fixes the issue of oscillatory and negative solutions that were encountered with the matrix-based optimal estimation method used by Cubison et al. (2005). The 12 methods that include boundary constraints were systematically tested against five test cases. All of the methods performed similarly well when inverting frequency
- 490 distributions. However, poor results were obtained when inverting narrow distributions or data produced by single compositions. The method  $L_0D_{1e-3}B_{[0,1]}$  is often, but not always, able to invert these data. For narrow distributions a nonlinear least squares fit with either one or two growth factors, termed  $LSQ_1$  and  $LSQ_2$ , can fill this gap. Ambient data can be inverted by applying all three methods and then selecting the inversion with the smallest root mean square error between the data and the prediction. In contrast to previous inversion routines (Stolzenburg and McMurry, 1988; Cubison et al., 2005; Gysel
- et al., 2009), explicit knowledge of the aerosol size distribution is needed. These data can either be obtained using a co-located scanning mobility particle sizer, or by configuring the tandem DMA to also measure the size distribution every few scans.



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The resulting algorithm is unsupervised and nonparametric, i.e., it can be fully automated and does not require any *a-priori* assumption about the shape of the growth factor frequency distribution. The speed of the inversion algorithm is much slower than for size distribution inversion for several reasons. For each scan, the matrix  $A_2$  must be recomputed to account for changes in the size distribution. This requires recomputing the generalized singular value decomposition for  $A_2$  and L, which is slow. Furthermore, three inversions are computed for each scan. The  $LSQ_1$  and  $LSQ_2$  methods use a gradient descent algorithm together with the forward model, which is slower than the matrix inverse. Nevertheless, a single day's worth of data can be inverted on a regular personal computer within a few minutes.

Application of the inversion to a 16-day dataset demonstrates that the thus-obtained growth factor frequency distribution data can reveal significant details about the mixing state of the aerosol. The inverted dataset is suitable as input to carry out common analyses made with growth factor frequency distributions, including characterization of the evolution of aerosol mixing state as a function of time, characterization of changes in growth factor with dry diameter and its relationship to chemical composition, characterization of the growth factor at the mode diameter of particles during modal growth events (Park et al., 2008; Wu et al., 2013; Jung and Kawamura, 2014), decomposition of the hygroscopicity frequency distributions into distinct growth factor

510 classes (Swietlicki et al., 2008), evaluation of the temporal trends of spectral concentration for hygroscopicity-resolved data (Royalty et al., 2017), evaluation of the accuracy of aerosol mass spectrometer measured (organic) mass concentration through hygroscopicity constraints (Jimenez et al., 2016), and inclusion of growth factor frequency distributions to account for mixing state in aerosol hygroscopicity to cloud condensation nuclei closure (Mahish et al., 2018).

#### Code and data availability.

- SGP SMPS Data: Atmospheric Radiation Measurement (ARM) user facility. 2016, updated hourly. Scanning mobility particle sizer (AOSSMPS). 2020-01-01 to 2020-09-27, Southern Great Plains (SGP) Lamont, OK (Extended and Co-located with C1) (E13). Compiled by C. Kuang, C. Salwen, M. Boyer and A. Singh. ARM Data Center. Data set accessed 2020-09-29 at http://dx.doi.org/10.5439/ 1095583.
  - SGP HTDMA Data: Atmospheric Radiation Measurement (ARM) user facility. 2017, updated hourly. Humidified Tandem Differential Mobility Analyzer (AOSHTDMA). 2020-01-01 to 2020-02-22, Southern Great Plains (SGP) Lamont, OK (Extended and Co-located with C1) (E13). Compiled by J. Uin, C. Salwen and G. Senum. ARM Data Center. Data set accessed 2020-09-25 at http://dx.doi.org/ 10.5439/1095581.
    - Bodega Bay Preprocessed Data: Petters, Markus D., Rothfuss, Nicholas E., Taylor, Hans, Kreidenweis, Sonia M., DeMott, Paul J., and Atwood, Samuel A. (2019). Size-resolved cloud condensation nuclei data collected during the CalWater 2015 field campaign (Version v1.0) [Data set]. Zenodo. http://doi.org/10.5281/zenodo.2605668.
    - 4. DifferentialMobilityAnalyzers.jl: A general purpose software package implementing the "Language to Simplify Computation of Differential Mobility Analyzer Response Functions" is available using the GPL-v3 license and is hosted is on GitHub. Version 2.5 was used in this work. The version of the software will be permanently archived with a doi upon acceptance of the manuscript for publication.



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530	Documentation: https://mdpetters.github.io/DifferentialMobilityAnalyzers.jl/stable/
	Source Code: https://github.com/mdpetters/DifferentialMobilityAnalyzers.jl

5. RegularizationTools.jl: A general purpose software package implementing Phillips-Twomey-Tikhonov Regularization. The package is available using the GPL-v3 license and source code and documentationa are hosted on GitHub. Version 0.4.0 was used in this work. The version of the software will be permanently archived with a doi upon acceptance of the manuscript for publication. Documentation: https://mdpetters.github.io/RegularizationTools.jl/stable/

Source Code: https://github.com/mdpetters/RegularizationTools.jl

6. Source Code to reproduce the figures and derived datasets, and copies of the derived dartasets are temporarily hosted on GitHub and will be permanently archived on Zenodo with a doi upon final acceptance of the manuscript for publication.

540 Source Code: https://github.com/mdpetters/softwarePackageSimplify2021

Competing interests. The author declares no competing interests.

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