# Estimation of raindrop size distribution and rain rate with infrared surveillance camera in dark conditions

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7 Abstract. This study estimated raindrop size distribution (DSD) and rainfall intensity with an infrared surveillance camera in dark conditions. Accordingly, rain streaks were extracted using a k-nearest neighbor (KNN)-based algorithm. The rainfall 8 9 intensity was estimated using DSD based on physical optics analysis. The estimated DSD was verified using a disdrometer-Furthermore, a tipping bucket rain gauge was used for comparison. for the two rainfall events. The results are summarized as 10 follows. First, a KNN-based algorithm can accurately recognize rain streaks from complex backgrounds captured by the 11 12 camera. Second, the number concentration of raindrops obtained through closed-circuit television (CCTV) images was similar tohad values between 100 mm<sup>-1</sup>m<sup>-3</sup> and 1,000 mm<sup>-1</sup>m<sup>-3</sup>, the actual PArticle SIzeRMSE for the number concentration by CCTV 13 14 and PARticle Slize and VELocity (PARSIVEL) observed number concentration) was 72.3 mm<sup>-1</sup>m<sup>-3</sup> and 131.6 mm<sup>-1</sup>m<sup>-3</sup> in the 15 0.5 to 1.5 mm section. Third, maximum raindrop diameter and the number concentration of 1 mm or less produced similar results during the period with a high ratio of diameters of 3 mm or less. Finally, after comparing with the 15-min cumulative 16 PARSIVEL rain rate, the mean absolute percent error (MAPE) was 44%, The 49% and 23%, respectively, In addition, the 17 differences according to rain rate can be determined. The found that the MAPE was 3236% at a rain rate of less than 2 mm h<sup>-1</sup> 18 and 7380% at a rate above 2 mm h<sup>-1</sup>, Also, when the rain rate was greater than 5 mm h<sup>-1</sup>, MAPE was 33%. We confirmed the 19

20 possibility of estimating an image-based DSD and rain rate obtained based on low-cost equipment during dark conditions.

## 21 1 Introduction

22 Precipitation data is vital in water resource management, hydrological research, and global change analysis. The primary means of measuring precipitation is to use a rain gauge (Allamano et al., 2015) to collect raindrops from the ground. Due to the 23 restrictions on the installation environment of the rain gauge, it is difficult to understand the spatial rainfall distribution in 24 25 mountains and urban areas (Kidd et al., 2017). Furthermore, the tipping-bucket-type rain gauge, which accounts for most rain gauges, has a discrete observation resolution (0.1 or 0.5 mm) for the discrete time-steps, producing uncertainty in temporal 26 27 rainfall variation. For this reason, weighing gauges are nowadays used very often instead of tipping-bucket-type. the weighing 28 gauge is a meteorological instrument used to observe and analyze various precipitation, including rainfall and snowfall. Also, 29 the tipping bucket has a large error due to the observation time delay when the rainfall is less than 10 mm h<sup>-1</sup> compared to the

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| Y                 | 서식 | <b>있음:</b> 위 첨자    |
|                   | 서식 | <b>있음:</b> 글꼴색:자동  |
| $\mathbb{Z}$      | 서식 | <b>있음:</b> 글꼴 색:지동 |
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weighing gauge. However, when the observation time size is set to 10 to 15 minutes, the relative percentage error has a very
 low value of -6.7~2.5%, resulting in high accuracy (Colli et al., 2014).

In contrast, it is possible to obtain spatial rainfall information on a global scale with remote sensing techniques (Famiglietti et al., 2015). However, remote sensing techniques provide only indirect measurements that must be continuously calibrated and verified through ground-level precipitation measurements (Michaelides et al., 2009). Recently, a disdrometer capable of investigating the microphysics characteristics of rainfall has been used for observation instead of the traditional rainfall observation instrument (Kathiravelu et al., 2016). However, these devices cannot be widely installed because of their high cost and difficulty in accessing observational data. Consequently, a high-resolution and low-cost ground precipitation monitoring network has not yet been established.

With the advent of the Internet of Things (IoT) era, using non-traditional sources is attractive for improving the spatiotemporal scale of existing observation networks (McCabe et al., 2017). In recent years, such cases have been common in rainfall observation. For example, there have been attempts to estimate rainfall using sensors to capture signal attenuation characteristics in commercial cellular communication networks (Overeem et al., 2016), vehicle wipers (Raibei et al., 2013), and smartphones (Guo et al., 2019). Furthermore, crowdsourcing information has been used to confirm the utility of estimating regional rainfall (Haberlandt and Sester, 2010; Rabiei et al., 2016; Yang and Ng, 2017).

In a similar context, a surveillance camera is a sensor with high potential. Surveillance cameras are often referred to as closed-circuit television (CCTV). Compared with other crowdsourcing methods, the visualization data of surveillance cameras are highly intuitive (Guo et al., 2017). Therefore, they have been used in various fields (Cai et al., 2017; Nottle et al., 2017; Hua, 2018). In Korea, public surveillance camera installations have been rapidly increasing, from approximately 150,000 in 2008 to 1.34 million in 2020—approximately a public CCTV camera per 0.07 km<sup>2</sup>. Thus, the potential for precipitation estimation using camera sensing is expected to be greater in Korea.

Recently, various studies have been conducted to estimate rainfall intensity using the rain streak image obtained from surveillance camera videos. Many studies attempted to use artificial intelligence to capture changes in the image captured by the camera when it rains (Zen et al., 2019; Avanzato and Beritelli, 2020; Wang et al., 2022). In contrast, some studies have tried to estimate rainfall intensity using geometrical optics and photographic analyses. Typically, the rain streak layer is separated from the raw image or video. A rain streak is the visual appearance of raindrops caused by visual persistence raindrops falling because of the blur phenomenon of raindrop movement from the camera's exposure time appears as streaks on the image. Garg and Navar (2005) made one of the first attempts to measure this rainfall.

Since then, many studies have been conducted to develop and improve efficient algorithms. Allamano et al. (2015) proposed a framework to estimate the quantitative rainfall intensity using camera images based on physical optics from a hydrological perspective. Dong et al. (2017) proposed a more robust approach to identifying raindrops and estimating rainfall using a grayscale function, making grayscale subtraction nonlinear. Jiang et al. (2019) proposed an algorithm that decomposes rain-containing images into rain streak layers and rainless background layers using convex optimization algorithms and estimates instantaneous rainfall intensity through geometric optical analysis. 64 Some studies (e.g., Dong et al., 2017) have sought to estimate raindrop size distribution (DSD) using a surveillance camera. 65 However, nothe existing studies have focused on the time when video can be captured with visible light. It is impossible to obtain input data without visible light using the existing image-based rainfall measurement method. Thus, these methodologies 66 67 are only applicable in daytime conditions. However, when recording using infrared rays, it is possible to obtain a rainfall image 68 even when there is no sunlight. No study has estimated the rain in dark conditions to our knowledge. Furthermore, most 69 previous studies did not verify the estimated DSD using a disdrometer. In contrast, this study estimated DSD with an infrared 70 surveillance camera in dark conditions, based on which rainfall intensity was also estimated. Rain streaks were extracted using 71 a k-nearest neighbor (KNN)-based algorithm. The DSD was used to calculate rainfall intensity with physical optics analysis 72 and verified using a PAR-rticle SIze and VELocity (PARSIVEL) disdrometer- (Löffler-Mang and Joss, 2000).

## 73 2 Methodology

# 74 2.1 Recording video containing rain streaks using infrared surveillance camera

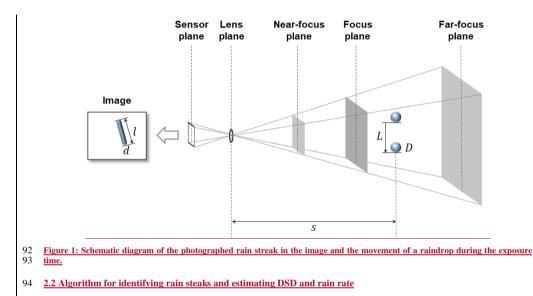
75 The surveillance camera records video. The video looks continuous, but it is also composed of discrete still images, so-called 76 frames. The frequency of recording frames (i.e., acquisition rate) is called frames per second (fps). In other words, fps is how 77 many images are taken per second for recording video. Another important factor in video recording is exposure time. Exposure time, also called shutter speed, refers to the time the camera sensor is exposed to light to capture a single frame. The real 78 79 raindrops are close to a circle, but in a single image, the raindrops look like a streak. This is because raindrops move at a high 80 speed during the exposure time. Therefore, the raindrops that moved during the exposure time are visualized in the rain streaks 81 in a single frame. 82 Fig. 1 shows an example of capturing a raindrop for a single frame. Here, only the raindrops near the point of focus are

visible, and objects that are more than a certain distance appear invisible. That is, the point where the focus is best is called the
 focus plane, and there is a range in which it can be recognized that objects are focused before and after the focus plane. The
 closest plane that can be considered to be in focus is called the near-focus plane, and the farthest plane is called the far-focus
 plane. This range is generally called depth of field (DoF). Ultimately, the rainfall intensity can be estimated based on the
 volume and raindrops in the DoF.
 In this study, an infrared surveillance camera was considered under dark conditions. Here, the dark condition refers to a

89 condition in which raindrops cannot be captured by a general surveillance camera with visible light. Infrared cameras emit

90 near-infrared rays through an infrared emitter and receive the reflected light from the objects. Accordingly, it has the advantage

91 of being able to detect raindrops that are invisible to the human eye.

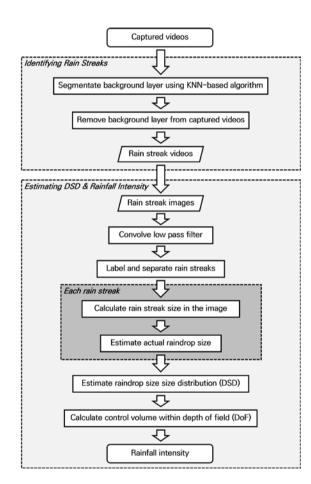


95 Image-based rainfall estimation can be divided into two processes: identifying rainfall streaks and estimating DSD. Fig. +2

96 illustrates these processes in a flowchart. Identifying rain streaks requires an algorithm that separates the moving rain streaks

97 from the background layer, as explained in Section 2.1., Next, in estimating DSD, raindrops are extracted from the image of

98 the rain streaks, and the overall distribution is obtained. This process is explained in Section 2.2.



99 Figure 12: Flowchart of the methodology for estimating DSD and rainfall intensity.

## 100 2.1 Algorithm for identifying rain steaks

- 101 Most existing algorithms aim to remove raindrops in images because raindrops are considered noise in object detection
- 102 and tracking (Duthon et al., 2018). Such algorithms are categorized into multiple-image-based and single-image-based
- 103 approaches (Jiang et al., 2018).

For example, Garg and Nayar (2007) classified the conditions in which the brightness difference between the previous pixel and that of the next pixel exceeds a specific threshold over time, assuming that the background is fixed. Improved algorithms were then developed considering the temporal correlation of raindrops (Kim et al., 2015) and chromatic properties (Santhaseelan and Asari, 2015). Tripathi and Mukhopadhyay (2014) proposed a framework that removes rain that reduces the visibility of the scene to improve the detection performance of image feature information. However, single-image-based algorithms rely more on the properties of raindrops (Deng et al., 2018). The central idea of a single-image-based algorithm is to decompose rain-containing images into rainless layers (Li et al., 2016; Deng et al., 2018; Jiang et al., 2018).

111 An image including grayscale rainfall may be mathematically expressed in a two-dimensional (2D) matrix in which each 112 element has a grayscale value. A single image ( $m \times n$ ) is expressed as follows (Jiang et al., 2018):

## 113 O = B + R,

(1)

114 where  $O \in \mathbb{R}^{m \times n}$ ,  $B \in \mathbb{R}^{m \times n}$ , and  $R \in \mathbb{R}^{m \times n}$  are the raw image, rain-free background layer, and rain streak layer. Accordingly, various algorithms are available for rain streak identification. Different still image and video-based algorithms 115 116 have been proposed to eliminate objects such as moving objects for application to actual surveillance cameras. However, most 117 of these algorithms face optimization problems because of the vast number of decision variables (Jiang et al., 2019). This task 118 is not easy to solve or requires excessive computation time. Therefore, existing studies present techniques suitable for post-119 analysis rather than application in real-time. The use of complex algorithms can increase versatility and accuracy, but there is a trade-off that reduces computational speed. The time required for such computing is a critical disadvantage in practical 120 121 applications for estimating rainfall intensity. 122 In this study, a KNN-based segmentation algorithm (Zivkovic and Heijden, 2006), a popular non-parametrical method for 123 background subtraction, was considered for segmenting the rain streaks (foreground) and background layers. KNN is used in

124 classification and regression problems (Bouwmans et al., 2010). The concept of KNN is that similar things are close-the KNN-based segmentation algorithm finds the closest k samples (neighbors) to the unknown sample using Euclidean distance 125 to determine the class (i.e., foreground or background). Thus, the KNN-based segmentation method to detect foreground 126 127 changes in the video was used to identify rain streaks by recording infrared videos under conditions with little background 128 influence. In the algorithm, The KNN subtractor works by updating the parameters of a Gaussian mixture model for more 129 accurate kernel density estimation (Trnovszký et al., 2017). KNN is more efficient for local density estimation (Oasim et al., 130 2021); therefore, the algorithm is highly efficient if the number of foreground pixels is low. 131 We used the package provided by OpenCV to implement the KNN-based segmentation algorithm (Zivkovic and Heijden,

we used the package provided by openet v to implement the KNN-based segmentation agonum (2)/vkove and reliden,
 2006). Accordingly, three main parameters (history, dist2Threshold, detectShadows) needed to be set. Table 1 presents the
 description of the parameters used for the KNN background subtractor package.

134 Table 1: Parameters in KNN background subtractor package in OpenCV.

## Parameter

Description

| history        | Length of the history                                                                                                                                                       |
|----------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| dist2Threshold | Threshold on the squared distance between the pixel and the sample to decide whether a pixel is close to that sample. This parameter does not affect the background update. |
| detectShadows  | If true, the algorithm will detect shadows and mark them. This decreases the speed slightly, so if you do not need this feature, set the parameter to false.                |

### 135 2.2 Estimation of DSD and rain rate

136 It is essential to capture raindrops within the camera's depth of field (DoF) to calculate the final DSD and rainfall intensity.

137 Accordingly, this study proposed a novel algorithm to extract each rain streak from the rain streaks image. First, we applied a 138 low-pass filter to the rain streaks image to remove unfocused raindrops that may remain in the image, which smooths each

139 pixel using a 2D kernel. Videos from infrared mode have usually a blur effect. Thus, the additional 2D kernel was applied to

Prior using a 22 normal reason normalised mode have assumed a star encoder reason and additional 22 normal reason approved to

140 <u>remove the pixels having blur.</u> Highly detailed parts (e.g., out-of-focus raindrops and some noises) are erased, leaving some 141 clear rain streaks. A background layer with a value of 0 and a part not in the image were separated to extract the rain streaks

142 and labeled one by one to identify each rain streak from the image.

Because the rain streak observed in the surveillance camera image causes an angle difference (influenced by the wind), a diameter estimation process considering the angle of the rain streak (fall angle of a raindrop) is required. If the angle of rain steak is considered and converted to the raindrop diameter through the horizontal pixel size in the image, the shape change in the raindrop because of air buoyancy (i.e., during the falling of the raindrop) may not be reflected, and overestimation can occur.

Accordingly, the representative angle of each extracted rain streak was calculated. The border information of each rain streak was obtained, and center axis information of the rain streak was obtained based on the border information to calculate the drop angle. Moreover, the rain streak was rotated to set the long and short axes of the streak at 0° and 90°, using the angle information.

The size of raindrops in the rain streaks image can be estimated through the analysis of microphysical characteristics of raindrop and geometric optical analysis (Keating, 2002). The instantaneous velocity of a raindrop on the ground can be estimated from the exposure time and the size of the raindrop. However, the distance from the raindrop to the lens surface (i.e., the object distance) is unknown and should be inferred. Object distance can be calculated through physical optics analysis because it causes perspective distortion. Assuming a raindrop is spherical, the length of the trajectory where the raindrop falls when the camera is exposed and the diameter of the raindrop can be inferred through the lens equation (Keating, 2002):

158 
$$L(s) = \frac{d_f - f}{d_f \cdot f} \frac{h_s}{h_p} l_p s,$$
(2)

159 
$$D(s) = \frac{d_f - f w_s}{d_f \cdot f w_p} d_p s,$$
 (3)

서식 있음: 들여쓰기 첫 줄: 1.42 글자

160 where s is the distance from the raindrop to the lens plane (mm). L(s) and D(s) are the length of falling trajectory during camera

161 exposure (rain streak) and the raindrop's diameter.  $d_f$  is the focus distance (mm), f is focal length (mm).  $h_s$  and  $w_s$  are the

162 vertical and horizontal sizes of the active area of the image sensor (mm), and  $h_p$  and  $w_p$  are the vertical and horizontal sizes of

163 the captured image (in number of pixels).  $l_p$  and  $d_p$  are the length and width of the rain streaks in the image (in number of

164 pixels).

165 It is then possible to infer the falling speed of raindrops using the camera's exposure time (Jiang et al., 2019), as follows:

166 
$$v(s) = \frac{L(s)}{1000\tau}$$
, (4)

where  $\tau$  is the exposure time of the camera (seconds) and v(s) is the fall velocity of the raindrop from the image. Furthermore, the fall velocity of a raindrop can be approximated by an empirical formula for raindrop diameter. The most frequently used

(5)

169 equation is as follows (Atlas et al., 1973; Friedrich et al., 2013):

$$v(D) = 9.65 - 10.3 \exp(-0.6D),$$

where *D* is the raindrop diameter and v is the fall velocity of raindrop. The actual diameter of raindrops can be obtained by solving the equation with the fall velocity obtained through the exposure time and Eqs. (4) and (5). Furthermore, the DoF for the images using the camera's setting information can be calculated, and the effective volume for estimating rainfall intensity can be obtained. Details of the process are described in previous studies (Allamano et al., 2015; Jiang et al., 2019).

175 The control volume must be determined to estimate the rainfall intensity using the diameter of each raindrop. An understanding 176 of DoF is required to achieve the volume. The DoF, is simply the range at which the camera can accurately focus and capture 177 the raindrops. Calculating this range requires obtaining the near and far focus planes as follows:

178 
$$s_n = \frac{d_f \cdot f^2}{f^2 + N \cdot c_p \cdot (d_f - f)},$$
 (6)

179 
$$s_f = \frac{d_f \cdot f^2}{f^2 - N \cdot c_P \cdot (d_f - f)},$$
 (7)

where  $s_n$  and  $s_f$  are the distances from the near and far focus planes.  $c_p$  is the maximum permissible circle of confusion, a constant determined by the camera manufacturers. *N* is the F-number of the lens relevant to the aperture diameter. Accordingly, the theoretical sampling volume (*V*, m<sup>3</sup>) indicate the truncated rectangular pyramid between the near and far focus planes:

183 
$$V = \frac{1}{3 \cdot 10^9} \left( \frac{d_f - f}{d_f \cdot f} \right)^2 w_s h_s (s_f^3 - s_n^3), \tag{8}$$

184

Then, we used the gamma distribution equation, Eq. (6), proposed by Ulbrich (1983), to calculate DSD parameters using data at every 1 min interval.

187 
$$N(D) = N_0 D^{\mu} \exp(-AD),$$
 (9)

where N(D) (mm<sup>-1</sup>m<sup>-3</sup>) is the number concentration value per unit volume for each size channel, and  $N_{\theta}$  (mm<sup>-1-µ</sup>m<sup>-3</sup>) is an intercept parameter representing the number concentration when the diameter has 0 value. D (mm) and  $\Lambda$  (mm<sup>-1</sup>) are the drop diameter (mm) and slope parameter. Raindrops smaller than 8.0 mm were used to avoid considering non-weather data such as

191 leaps and bugs (Friedrich et al., 2013).

192 The gamma distribution relationship is a function of formulating the number concentration per unit diameter and unit 193 volume. It was proposed by Marshall and Palmer (1948) as improved model of exponential distribution as a favorable form to 194 reflect various rainfall characteristics. By including the term containing  $\mu$  in the distribution function, the shape of the number 195 concentration distribution for small drops smaller than 1 mm is improved.

196  $N(D) = N_0 \exp(-\Lambda D),$ 

(10)

197 As the  $\Lambda$  decreases, the slope of the distribution shape decreases and the proportion of large drop increases. Conversely, as 198 the value increases, the distribution slope becomes steeper, and the weight of the large particles decreases. When  $\mu$  has a large 199 value, the distribution is convex upward, and it has a distribution with a sharp decrease in number concentration at small 200 diameters. Whereas when it has a negative value, the distribution is convex downward with an increase in the concentration 201 of drops smaller than 1 mm. In the gamma distribution, the  $\mu$  is mainly affected by the difference in concentration of raindrops 202 smaller than 3 mm (Vivekanandan et al., 2004).

Vivekanandan et al. (2004) explained the reason for using the gamma distribution as follows. First, it is sufficient to calculate the rainfall estimation equation using only the first, third, and fourth moments (Eq. (11)) (Smith, 2003). Second, the long-term raindrop size distribution has an exponential distribution shape (Yuter and Houze, 1997).

The raindrop size distribution observed from the ground is the result of the microphysical development of raindrops falling from precipitation clouds. The drop size distribution shape is changed during fall by microphysical processes such as collision, merging, and evaporation, and changes in the concentration of drops larger than 7.5 mm and small drops occur mainly. As a result, the drop size distribution observed on the ground mainly follows the gamma distribution shape (Ulbrich, 1983; Tokay and Short, 1996). The gamma distribution relationship should be used to analyze the distribution of raindrops that are actually floating and falling.

212 
$$M_n = \int_{D_{min}}^{D_{max}} D^n N(D) dD,$$
 (11)

Eq. (11) indicate a moment expression for the  $n^{th}$  order. For example, the second moment is calculated as the product of the square of the diameter of each channel and the number concentration and the diameter of each channel. Each moment value has a different microphysical meaning. Therefore, the gamma distribution including three dependent parameters is more advantageous in reflecting the microphysical characteristics of the precipitation system than the exponential distribution including two dependent parameters. Eq. (11) can be expressed in gamma distribution format as follows:

218 
$$M_n = \int_{D_{min}}^{D_{max}} D^n N(D) dD = N_0 \Lambda^{-(\mu+n+1)} \Gamma(\mu+n+1),$$
(12)

- 219 where  $N_T$  (total number concentration, m<sup>-3</sup>) is the zero-order moment ( $M_0$ ) and represents the total number concentration of
- raindrops per unit volume.  $\eta$  was determined for calculating  $\mu$  and  $\Lambda$ . In this study, a combination of moments in the ratio of
- 221  $M_2$ ,  $M_4$ , and  $M_6$ , which accurately represents the characteristics of small rainfall particles, was applied (Vivekanandan et al., 222 2004):

223 
$$\eta = \frac{\langle M_4 \rangle^2}{\langle M_2 \rangle \langle M_6 \rangle} = \frac{(\mu+3)(\mu+4)}{(\mu+5)(\mu+6)},$$
 (13)

224  $\mu$  and  $\Lambda$  are calculated as follows:

225 
$$\mu = \frac{(7-11\eta) - [(7-11\eta)^2 - 4(\eta-1)(30\eta-12)]^{1/2}}{2(\eta-1)},$$
(14)

226 
$$\Lambda = \left[\frac{M_2\Gamma(\mu+5)}{M_4\Gamma(\mu+3)}\right]^{1/2} = \left[\frac{M_2(\mu+4)(\mu+3)}{M_4}\right]^{1/2},$$
(15)

A larger value of  $D_m$  (mm) estimated using Eq. (16), the diameter of the average mass of raindrops contained in the unit volume, indicates that predominantly larger drops are distributed.

229 
$$D_m = \frac{M_4}{M_2}$$
, (16)

230  $R (\text{mm h}^{-1})$  is the rain rate calculated using Eq. (17).

231 
$$R = \frac{6\pi}{10^4} \int_{D_{min}}^{D_{max}} D^3 N(D) V(D) dD,$$
 (17)

# 232 3 Study site and observation equipment

233 This study used a building's rooftop as the study site. The building is the Chung-Ang University's Bobst Hall, located in the

central region of Seoul in Korea. It is located at 37° 30' 13" north latitude and 126° 57' 27" east longitude, at an elevation of
42 m. Fig. 23 illustrates the CCTV (marked with a red circle) and PARSIVEL installed at the study point. The CCTV was

236 used for the main analysis, and PARSIVEL was considered for verification purposes.



## (a) Surveillance camera Figure 23: Observation measurements considered in this study.

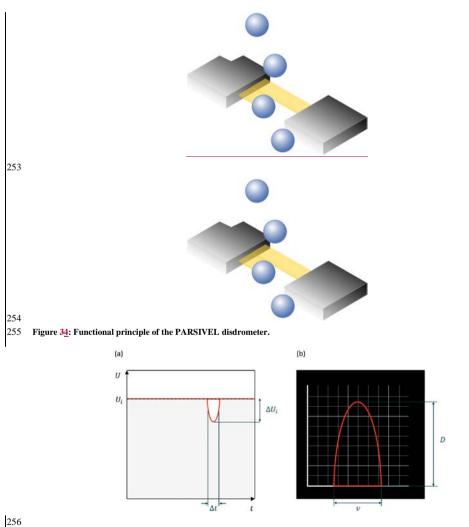
237

(b) PARSIVEL

The CCTV model used in this study is DC-T333CHRX, developed by IDIS. The camera has a 1/1.7 inch complementary metal-oxide semiconductor (CMOS) with a height and width of 5.70 mm and 7.60 mm. The focal length is 4.5 mm, and the F-number of the lens is 1.6. The shutter speed was set to 1/250 s, and the frame per second (fps) was set to 30. The infrared ray distance is 50 m. The maximum permissible circle of confusion is 0.005 mm. The camera's resolution is 1,080 pixels for the height and 1,920 pixels for the width, but the cropped images ( $640 \times 640$  pixels) were considered for the analysis.

The PARSIVEL is a ground meteorological instrument that can observe precipitation particles' diameter and fall speed (e.g., raindrops, snow particles, hail) (Löffler-Mang and Joss, 2000).). The meteorological information, including raindrop size, is used to estimate the quantitative precipitation amount and reveal the precipitation system's microphysical characteristics and development mechanism.

The PARSIVEL used in this study is the second version of the instrument manufactured by OTT in Germany, and it is improved observation accuracy of small particles. The PARSIVEL uses a laser-based optical sensor to send a laser from the transmitter and continuously receive it from the receiver (Fig. 34). As the laser beam moves from the transmitter to the receiver, the precipitation particle passes over the laser beam, and the size and velocity of the precipitation particle are observed (Nemeth and Hahn, 2005). The diameter and velocity of the particle are calculated by calculating the time the particle passes through the laser and the laser intensity that decreases during the passage (Fig. 45).





258 Figure 45: (a) Signal changes whenever a particle falls through the beam anywhere within the measurement area. (b) The degree of dimming is a measure of the particle's size; together with the duration of the signal, the fall velocity can be derived.

259 Parameters such as rain rate, reflectivity, and momentum of raindrops are calculated through particle concentration values for each diameter and falling speed channel obtained through PARSIVEL observation. In this 260 261 study, the temporal resolution of the observation data was set to 1 minute. The particle diameters from 0.2 to 25 mm 262 (Table 21 in Appendix) and fall velocity from 0.2 to 20 m s<sup>-1</sup> (Table 32 in Appendix) can be observed by the PARSIVEL. 263 The particle diameter and the fall speed each have 32 observation channels, so the number of observed particles for the 264 time resolution set in 1,024 channels (32×32) is observed. The first and second channels of diameter are not included in the observable range of the PARSIVEL and are treated as noise. Therefore, the observation data of the first and 265 266 second diameter channels were not considered in the actual analysis. The detailed information on the specifications of 267 the PARSIVEL is presented in Table 42.

268 269

## 270 Table 2: The representative diameter and spread for each diameter channel class.

| Class number  | Class average (mm) | <del>Class spread</del><br><del>(mm)</del> | <del>Class number</del> | Class-average (mm) | Class spread in<br>(mm) |
|---------------|--------------------|--------------------------------------------|-------------------------|--------------------|-------------------------|
| ŧ             | 0.062              | 0.125                                      | <del>17</del>           | 3.250              | 0.500                   |
| 글             | 0.187              | 0.125                                      | <del>18</del>           | <del>3.750</del>   | 0.500                   |
| 3             | 0.312              | 0.125                                      | <del>19</del>           | 4.250              | 0.500                   |
| 4             | <del>0.437</del>   | 0.125                                      | <del>20</del>           | <del>4.750</del>   | 0.500                   |
| 5             | 0.562              | 0.125                                      | 21                      | <del>5.500</del>   | 1.000                   |
| 6             | <del>0.687</del>   | 0.125                                      | 22                      | <del>6.500</del>   | 1.000                   |
| ₽             | 0.812              | 0.125                                      | 23                      | 7.500              | 1.000                   |
| 8             | <del>0.937</del>   | 0.125                                      | 24                      | <del>8.500</del>   | 1.000                   |
| ₽             | <del>1.062</del>   | 0.125                                      | 25                      | <del>9.500</del>   | 1.000                   |
| <del>10</del> | <del>1.187</del>   | 0.125                                      | 26                      | 11.000             | 2.000                   |
| #             | <del>1.375</del>   | 0.250                                      | 27                      | <del>13.000</del>  | 2.000                   |
| <del>12</del> | <del>1.625</del>   | 0.250                                      | 28                      | <del>15.000</del>  | 2.000                   |
| <del>13</del> | <del>1.875</del>   | 0.250                                      | <del>29</del>           | 17.000             | 2.000                   |
| 14            | 2.125              | 0.250                                      | <del>30</del>           | <del>19.000</del>  | 2.000                   |
| <del>15</del> | 2.375              | 0.250                                      | 31                      | 21.500             | 3.000                   |
| <del>16</del> | <del>2.750</del>   | 0.500                                      | 32                      | 24.500             | 3.000                   |

271 272

# 273 Table 3: The representative fall velocity and spread for each diameter channel class.

| Class number | <del>Class average</del><br><del>(m s<sup>-1</sup>)</del> | <del>Class spread</del><br>( <del>m s<sup>-1</sup>)</del> | Class number | <del>Class average</del><br><del>(m s<sup>-t</sup>)</del> | <del>Class spread</del><br>( <del>m-s<sup>-1</sup>)</del> |
|--------------|-----------------------------------------------------------|-----------------------------------------------------------|--------------|-----------------------------------------------------------|-----------------------------------------------------------|
|--------------|-----------------------------------------------------------|-----------------------------------------------------------|--------------|-----------------------------------------------------------|-----------------------------------------------------------|

|                                       | 서식 있음: 들여쓰기 첫 줄: 1.42 글자 줄 간격 1.5줄                              |
|---------------------------------------|-----------------------------------------------------------------|
|                                       | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
| ///                                   | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 가로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>가로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
| $\sum$                                | 서식 있음: 위치 가로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>가로 :0 글자 텍스트 배치 둘러싸기 |
| $\langle \rangle$                     | 서식 있음: 위치 가로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>가로 :0 글자 텍스트 배치 둘러싸기 |
| $\left  \right\rangle$                | 서식 있음: 위치 가로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 .<br>가로 :0 글자 텍스트 배치 둘러싸기 |
| $\left  \left  \right\rangle \right $ | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 가로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 .<br>가로 :0 글자 텍스트 배치 둘러싸기 |
|                                       | 서식 있음: 위치 가로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 .<br>가로 :0 글자 텍스트 배치 둘러싸기 |

· 비사 이유· 드어씨가 최 주·1 42 구대 주기계 1 5주

| ŧ                 | 0.050            | 0.100 | 17            | 2.600             | 0.400 |
|-------------------|------------------|-------|---------------|-------------------|-------|
| <br>₽             | 0.150            | 0.100 | <del>18</del> | 3.000             | 0.400 |
| <br>3             | 0.250            | 0.100 | <del>19</del> | <del>3.400</del>  | 0.400 |
| <br>4             | 0.350            | 0.100 | 20            | 3.800             | 0.400 |
| <br>5             | 0.450            | 0.100 | 21            | 4.400             | 0.800 |
| <br>6             | <del>0.550</del> | 0.100 | 22            | <del>5.200</del>  | 0.800 |
| <br>₽             | 0.650            | 0.100 | 23            | <del>6.000</del>  | 0.800 |
| <br>윻             | <del>0.750</del> | 0.100 | 24            | <del>6.800</del>  | 0.800 |
| <br>₽             | 0.850            | 0.100 | 25            | 7.600             | 0.800 |
| <br><del>10</del> | <del>0.950</del> | 0.100 | <del>26</del> | <del>8.800</del>  | 1.600 |
| <br>##            | 1.100            | 0.200 | 27            | <del>10.400</del> | 1.600 |
| <br>+2            | <del>1.300</del> | 0.200 | <del>28</del> | 12.000            | 1.600 |
| <br><del>13</del> | <del>1.500</del> | 0.200 | <u>29</u>     | <del>13.600</del> | 1.600 |
| <br><del>14</del> | <del>1.700</del> | 0.200 | <del>30</del> | <del>15.200</del> | 1.600 |
| <br><del>15</del> | <del>1.900</del> | 0.200 | <del>31</del> | <del>17.600</del> | 3.200 |
| <br><del>16</del> | 2.200            | 0.400 | 32            | 20.800            | 3.200 |

274

## 275 Table 24: Technical information of the PARSIVEL disdrometer.

| Ite                       | ems              | Technical information Technical specifications    |  |  |
|---------------------------|------------------|---------------------------------------------------|--|--|
| Wavelength o              | f optical sensor | 780 nm                                            |  |  |
| Measur                    | ring area        | $30 \times 180 \text{ mm} (54 \text{ cm}^2)$      |  |  |
| Macauring ronga           | Size             | 0.2 ~ 25 mm (32 channel class)                    |  |  |
| Measuring range           | Fall velocity    | $0.2 \sim 20 \text{ m s}^{-1}$ (32 channel class) |  |  |
| Precipitati               | on intensity     | $0.001 \sim 1,200 \text{ mm h}^{-1}$              |  |  |
| Measurement time interval |                  | 10 sec ~ 60 min                                   |  |  |
| Instrument dime           | nsions (H×W×D)   | $670 \times 600 \times 114 \text{ mm}$            |  |  |

276

#### 277 4 Application result

#### 278 4.1 Rainfall event

279 We considered atwo rainfall events from 1945 LST on March 25, 2022, to 0615 LST on March 26, 2022- (case 1), and

2100 LST on September 5, 2022, to 0300 LST on September 5, 2022 (case 2). Fig. 56 illustrates the hyetographs of the rainfall 280

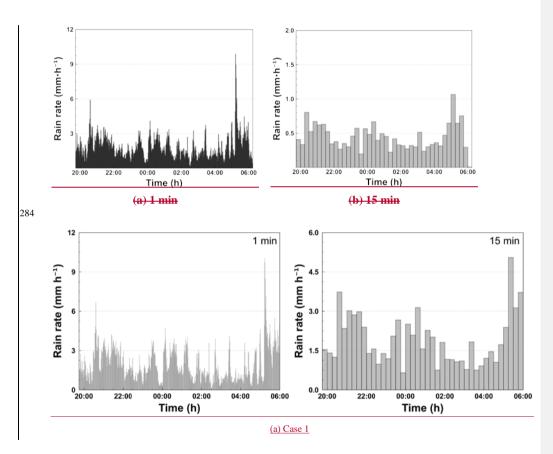
event considered in this study according to the time resolution. The total rainfall of case 1 and 2 is 18.619.5 and 48.7 mm based 281

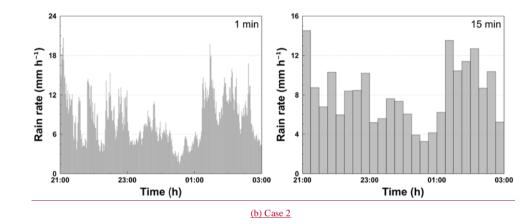
282 on the PARSIVEL-, respectively. The maximum rain rate is 9.910.0 and 20.7 mm h<sup>-1</sup> based on the 1 min resolution, and 1.15.0

283 and 14.5 mm h<sup>-1</sup> based on the 15 min resolution for case 1 and case 2.

|                  |                           |          |     | 위지 기도 :<br>,텍스트 배치  |  | 빅내영 | 刘仝 | 기논 | 기군 | .0455 | , |
|------------------|---------------------------|----------|-----|---------------------|--|-----|----|----|----|-------|---|
|                  |                           |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
|                  | $\left  \right $          |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
|                  | $\left( \right)$          |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| /                | $\langle \rangle$         |          |     | 위치 '가로 #<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| /                |                           |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| $\left  \right $ | )/(                       |          |     | 위치 '가로 #<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| h                | $\langle \rangle \rangle$ |          |     | 위치 '가로 #<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| ľ                |                           |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| //               |                           |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
|                  |                           |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| Ŵ                |                           |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
|                  |                           |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| <b>\</b>         |                           |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| h                | $\langle   $              |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| //               | $\langle \rangle$         |          |     | 위치 '가로 :<br>,텍스트 배치 |  | 막대형 | 세로 | 기본 | 기준 | :여백   | , |
| Ϊ,               | ///                       | 서식       | 있음: | 줄간격 1줄              |  |     |    |    |    |       |   |
| Ϊ,               | ///                       | 서식       | 있음: | 줄간격 1줄              |  |     |    |    |    |       |   |
| /'               | ///                       | <u> </u> |     | 줄간격 1줄              |  |     |    |    |    |       |   |
| )                | ///                       | 서식       | 있음: | 줄간격 1줄              |  |     |    |    |    |       |   |
|                  |                           | 서식       | 있음: | 줄간격 1줄              |  |     |    |    |    |       |   |
|                  | Y                         | 서식       | 있음: | 줄간격 1줄              |  |     |    |    |    |       |   |
|                  |                           |          |     |                     |  |     |    |    |    |       |   |

- 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 .







287

## 288 4.2 Identifying rainfall streaks

289 The rain streaks were distinguished from the original raw images using the KNN-based algorithm described in Section 2.42.

290 Accordingly, two parameters (history and dist2Threshold) were set to default values (500 and 400). The other parameter

291 (detectShadows) was set to "false." Fig. 67 illustrates the raw, background, and rain streaks images for an example time image

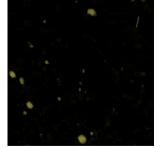
292 (20:30:57 March 25, 2022), scaled in yellow to make it easier to verify the visual change.



(a) Raw image



(b) Background image



(c) Rain streaks image

Figure 67: Segmentation example of raw image into background and rain streaks image based on KNN-based algorithm (20:30:57 March 25, 2022)). As confirmed in Fig. 67, adequate background separation performance can be achieved using the KNN-based method used

296 in this study. Because it is an infrared camera and the camera's exposure time is 1/250 s, the length of rain streaks is relatively

short. The longer the exposure time, the longer the raindrops appear on the image (Schmidt et al., 2012; Allamano et al., 2015).
If the exposure time is too long, some rain streaks may penetrate the image. In this case, it is difficult to estimate the rain streak

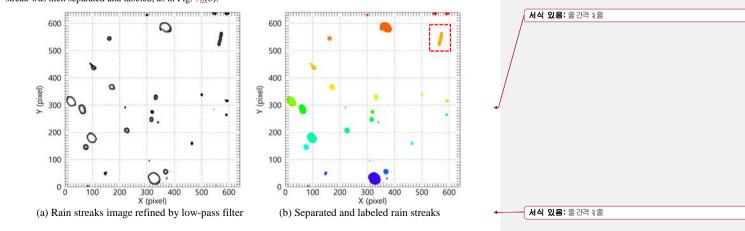
299 length, a clue for estimating raindrop size.

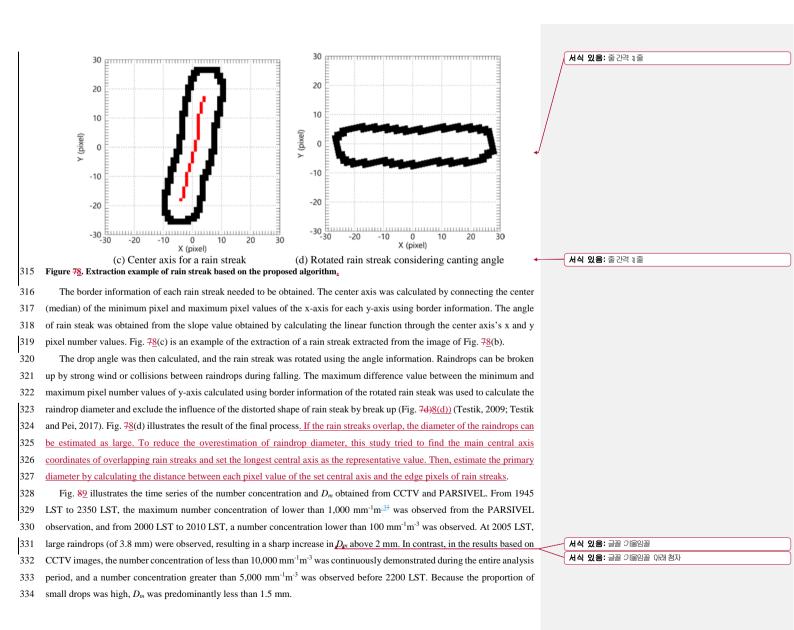
The identification algorithm was implemented using Anaconda Software Distribution on a workstation with an AMD Ryzen 5 5600X 6-Core Processor and 32 GB RAM. The computing time for the 15 min video was approximately 50 s using only CPU computation. As described previously, the KNN-based algorithm used in this study has high-speed computing performance compared with various algorithms based on optimization, so it will likely have an advantage in real-time applications.

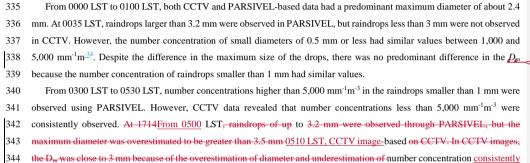
## 305 4.3 Estimation of DSD and rain rate

The rain streaks image presented in Fig.  $6\underline{7}(c)$  was not considered for the final DSD estimation because of noise and factors other than rain caused by the sudden brightness change. As described in Section 3, a low-pass filter was first applied rain streaks image.

The  $10 \times 10$  kernel was applied considering the total image size (640×640), and each grid value of the kernel was set to 0.01. The set kernel was filtered by convolution pixel by pixel. Moreover, the convolution was performed once more using the following 2D kernel [0 1 0; -1 0 1; 0 -1 0] to highlight the rim of the rain streaks. A background layer with a value of 0 and a part not in the image were separated to extract the rain streaks, which were labeled one by one to identify each rain streak from the image. Fig. 78(a) illustrates the example result after performing the processes described above to Fig. 67(c). Each rain streak was then separated and labeled, as in Fig. 78(b).







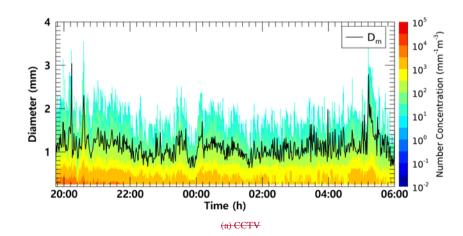
345 appeared as about 1.2 mm, whereas D<sub>m</sub> was smaller than 0.7 mm in PARSIVEL. The cause for raindrops less than 1 mm.

346 Therethe rapid decrease in D<sub>m</sub> of the PARSIVEL was that the CCTV-based maximum diameter is about 2.4 mm, which was a

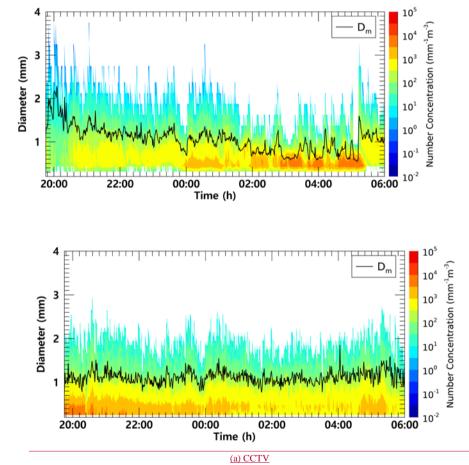
347 difference with similar to the  $D_{m}$  value obtained through PARSIVEL observation data, but the number concentration of 0.5 to

348 <u>0.6 mm raindrops observed by PARSIVEL had a large value of more than 10,000 mm<sup>-1</sup>m<sup>3</sup></u>.

349

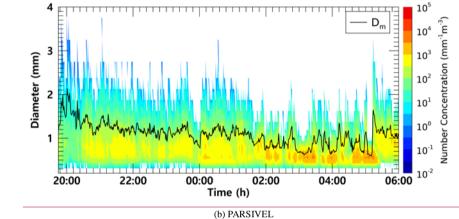


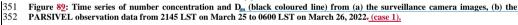
- 서식 있음: 글꼴 기물임꼴 서식 있음: 글꼴 기물임꼴 이래 첨자









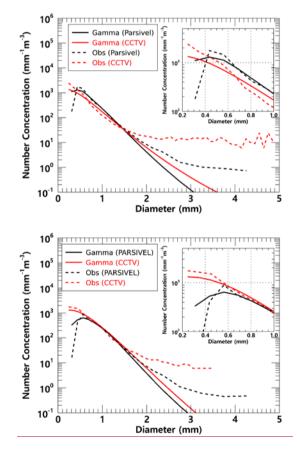


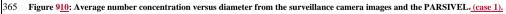
서식 있음: 아래 첨자

Fig. 910 illustrates the average number concentration versus diameter of raindrops calculated using CCTV image and PARSIVEL observation data from 1945 LST on March 25 to 0600 LST on March 26, 2022. The PARSIVEL disdrometer data has a fixed raindrop diameter channel; thus, it can differ in number concentration depending on the diameter channel setting. Therefore, in this study, the simulated DSD through the gamma model was also analyzed to compare the distribution of rainfall particles.

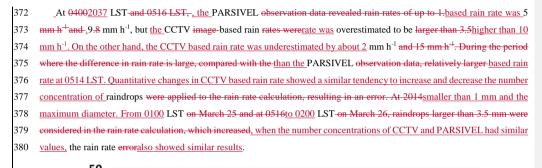
For raindrop diameters from 0.7 to 1.5 mm, the simulated and observed number concentrations produced similar values. However, above 1.5 mm, the model-based number concentration was under-simulated. From these results, in the precipitation easescase selected in this study, the gamma model appears limited in simulating the number concentration of raindrops larger than 3 mm. In diameters from 0.52 to 1.50 mm and above 1.5 mm, the number concentration obtained from CCTV images tended to be lowerhigher than that from PARSIVEL observation and higher in diameters above 1.5 mm. PARSIVEL observation data decreased sharply for diameters smaller than 0.3 mm. In contrast, CCTV gradually increased the number

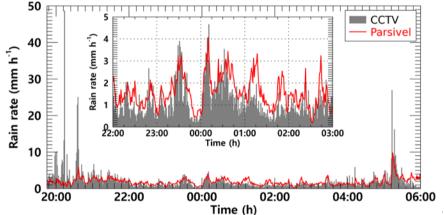
364 concentration as the diameter decreased.

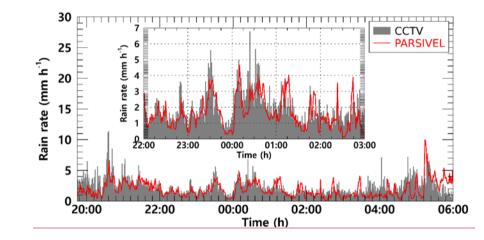




Rainfall intensity was estimated based on the obtained number concentration from CCTV images and PARSIVEL. The near ( $s_n$ ) and far ( $s_f$ ) focus planes were calculated as 718 and 1,648 mm from Eqs. (8) and (9). The DoF was calculated as 930 mm. The focal distance was set to 1 m, referring to previous studies (Dong et al., 2017; Jiang et al., 2019). The control volume was 2.9 m<sup>-3</sup>, applying Eq. (10) with the variables determined above. Fig. <u>4011</u> illustrates the rain rate time series calculated using CCTV images and PARSIVEL observation data. The increase or decrease in rain rate according to time change based on CCTV data followed the trend of rainfall intensity change based on PARSIVEL observation data.







 381
 Figure 1011: The rain rate time series calculated from the surveillance camera images (gray bar) and PARSIVEL observation data

 382
 (red line) from 2145 LST on March 25 to 0600 LST on March 26, 2022; (case 1).

Fig. <u>1112</u> illustrates the scatter plot of the average rain rate every 15 min from the PARSIVEL observation and the CCTV images. Uncertainty exists in the resolution of the rain gauge in the 1 min step. Accordingly, the time step for analysis is set to 15 min. The slope of the rainfall intensityregression line was close to 1 except for <u>0.71 because</u> the period when the <u>CCTV</u> <u>based</u> rain rate <u>wastended to be</u> overestimated by the rainfall intensity. <u>of weaker than 2 mm h<sup>-1</sup></u>.

The cumulative average rainfall intensity every 15 min was weaker than 10 mm h<sup>-1</sup>, concentrated at a rain rate less than 46mm h<sup>-1</sup>, so the correlation coefficient (CC) was 0.<u>5864</u>. Furthermore, the mean absolute error (MAE), root mean square error (RMSE), and mean absolute percent error (MAPE) were 0.<u>8461</u> mm h<sup>-1</sup>, <u>1.430.99</u> mm h<sup>-1</sup>, and <u>4448</u>%. Differences according to rain rate can also be determined. The accuracy is higher at a rain rate smaller than 2 mm h<sup>-1</sup> as a boundary. The MAE, RMSE, and MAPE were 0.<u>3229</u> mm h<sup>-1</sup>, 0.<u>6772</u> mm h<sup>-1</sup>, and <u>3238</u>% for a rain rate of 2 mm h<sup>-1</sup> or less, and <u>1.490.58</u> mm h<sup>-1</sup>, <u>2.371.17</u> mm h<sup>-1</sup>, and <u>7355</u>% for a rain rate above 2 mm h<sup>-1</sup>.

The statistical values of the rain rate and DSD parameters for the rainfall cases analyzed in this study are summarized in Table 53. The rain rate and  $D_m$  calculated using CCTV images were 0.46459 mm h<sup>-1</sup> and 0.05025 mm more than the values calculated using PARSIVEL observation data on average, respectively. A high rain rate and  $D_m$  were caused by overestimating the number concentration for raindrops larger than 1.5 mm confirmed in Fig. 910. The number concentration for the small diameter (less than 0.3 mm) was higher in the CCTV data than in the PARSIVEL data. Due to the high concentration value of the number concentration of raindrops below 0.5 mm and above 2 mm, the CCTV based rain rate had a large value. 400 However, the rain rate was not significantly affected by small raindrops. Although D<sub>w</sub> calculated from the PARSIVEL 401 observation data had a low value (1.061 mm), the CCTV data revealed a high skewness (of 1.793) because of the high number eoncentration for raindrops smaller than 0.1 mm. the high kurtosis (104.945 and 7.849) for the rain rate and D<sub>m</sub> of the CCTV-402 403 based data were caused by the overestimated number concentration of 1.5 mm or larger. Moreover, as the distribution spread 404 widely,  $\mu$  was as low as 1.312. Because of the high number concentration for raindrops larger than 3 mm of CCTV, the 405 PARSIVEL observation data had a A value of 9.982 mm<sup>-1</sup>, whereas the CCTV data had a low value (5.187 mm<sup>-1</sup>). 406 In the D<sub>m</sub> calculated through the PARSIVEL observation data, the concentration change of small drops over time was large, 407 and the variance (0.063 mm) of  $D_m$  was large due to the rapid change in number concentration. The variability of the maximum 408 diameter was greater in the PARSIVEL observation data, but the variance of the rain rate was greater in the CCTV data. The 409 large variability of the concentration of raindrops below 3 mm was effected the change in the rain rate. Also, due to the high

410 number concentration of small drops, the skewness of CCTV (1.903) based rain rate had a higher value than that of the

411 PARSIVEL (1.589) based rain rate. The low variability (0.063 mm) of the  $D_m$  calculated from CCTV data means that the

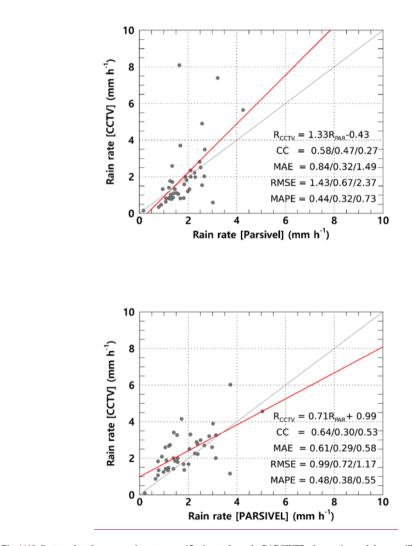
412 change in the shape of the raindrop size distribution was small, supported by the low variance of  $\Lambda$  (3.016 mm<sup>-1</sup>).

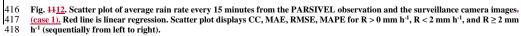
413

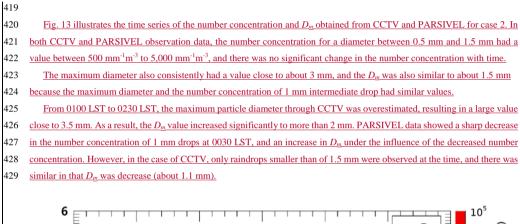
# Table 53: Statistical values of the rain rate and DSD parameters for the rainfall case in this study1.

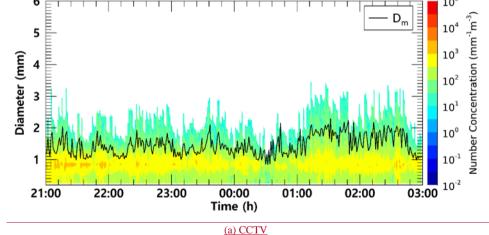
|          |          | <i>R</i> (mm h <sup>-1</sup> ) | $D_m$ (mm)                  | Log <sub>10</sub> No<br>log10No       | μμ (unitless)               | A                     |
|----------|----------|--------------------------------|-----------------------------|---------------------------------------|-----------------------------|-----------------------|
|          |          |                                |                             | (mm <sup>-1-µ</sup> m <sup>-3</sup> ) |                             | <u>л_(mm ·)</u>       |
|          | Mean     | 1. <del>829</del> 905          | 1. <del>061<u>091</u></del> | 6.5837.379                            | 5.1037.394                  | 9.98211.829           |
| PARSIVEL | Variance | 1. <del>013<u>667</u></del>    | 0.088063                    | 11.768 <u>15.170</u>                  | 24.124 <u>35.975</u>        | 69.899 <u>88.288</u>  |
| PARSIVEL | Skewness | 2.341 <u>1.589</u>             | 0.814551                    | 2.447 <u>470</u>                      | 2. <del>11</del> 015        | 2. <del>687</del> 714 |
|          | Kurtosis | 12.295 <u>5.189</u>            | 1. <del>562</del> 233       | 7. <del>226</del> 751                 | 5. <del>335<u>132</u></del> | 8.54 <u>9.165</u>     |
|          | Mean     | 1.994 <u>2.364</u>             | 1.116                       | 4.405 <u>857</u>                      | 1.3122.131                  | 5. <del>187</del> 713 |
| CCTV     | Variance | 9.274 <u>1.998</u>             | 0.07021                     | 0.422472                              | 0.913 <u>1.680</u>          | 3. <u>527016</u>      |
| CCIV     | Skewness | 8.5281.903                     | 1.7930.536                  | 1.427 <u>109</u>                      | 1.0750.628                  | 1.441151              |
|          | Kurtosis | 104.945 <u>6.073</u>           | <del>7.849</del> 1.041      | 2. <del>731</del> 188                 | 1.664 <u>0.739</u>          | 2. <del>802</del> 506 |

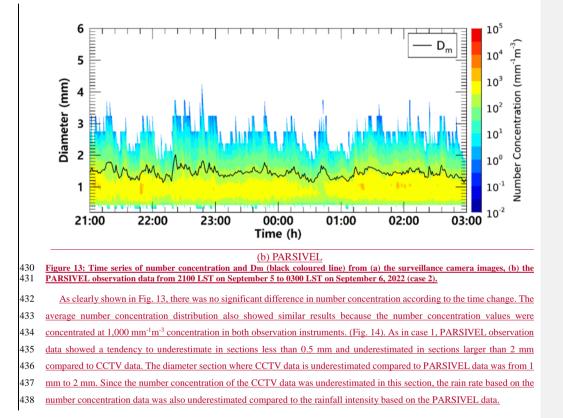
| -(                | 서식 | 있음: 글꼴 기울임꼴            |
|-------------------|----|------------------------|
| $\square$         | 서식 | 있음: 간격단락뒤:0 pt, 줄간격 1줄 |
| Y                 | 서식 | 있음: 글꼴 기물임꼴            |
| $\neg$            | 서식 | <b>있음:</b> 줄간격 1줄      |
| $\mathbb{K}$      | 서식 | 있음: 간격단락뒤:0 pt, 줄간격 1줄 |
| X                 | 서식 | <b>있음:</b> 줄간격 1줄      |
| $\langle \rangle$ | 서식 | <b>있음:</b> 줄간격 1줄      |
| $\langle \rangle$ | 서식 | <b>있음:</b> 줄간격 1줄      |
| X                 | 서식 | <b>있음:</b> 줄간격 1줄      |
| //                | 서식 | 있음: 간격단락뒤:0 pt, 줄간격 1줄 |
|                   | 서식 | <b>있음:</b> 줄간격 1줄      |
| Y                 | 서식 | <b>있음:</b> 줄간격 1줄      |
|                   |    |                        |

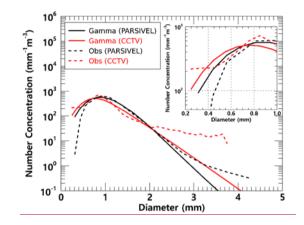












439 Figure 14: Average number concentration versus diameter from the surveillance camera images and the PARSIVEL (case 2).

440 Between 2100 LST on September 5 and 0100 LST on September 6, when the number concentration of about 1 mm

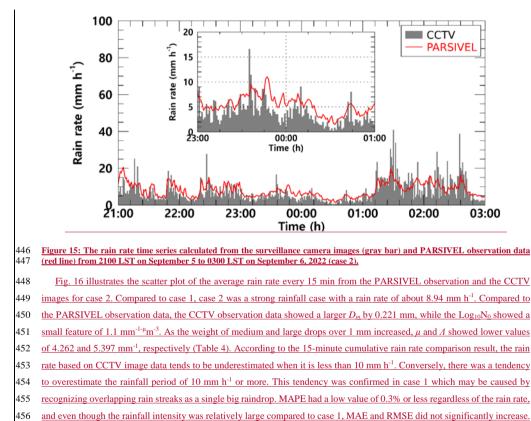
441 raindrops is similar and the maximum diameter size is similar, the rain rate time series distribution has a value of about 5 mm

442 h<sup>-1</sup> and has a very similar flow. However, between 0130 LST and 0300 LST, which is a time period with overestimation of

443 raindrop diameter in CCTV observation data, the increase and decrease in rain rate was similar. However, the magnitude of

the increase and decrease rain rate differed every 15 minutes. During that time, the maximum rain rate was less than 20 mm h

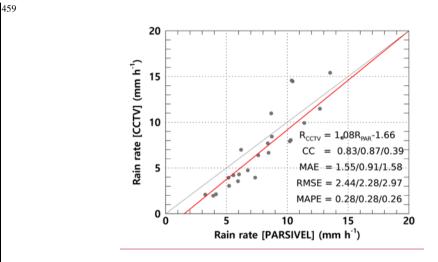
445 <sup>1</sup> in the PARSIVEL observation data, while strong rainfall of 30 mm h<sup>-1</sup> or more was observed in the CCTV observation data.



<sup>457</sup> This is because there was no abnormally large value of CCTV rainfall during the rainfall period of case 2 compared to case 1.

<sup>458</sup> Table 4: Statistical values of the rain rate and DSD parameters for case 2.

|             |          | <u>R (mm h<sup>-1</sup>)</u> | <u>D<sub>m</sub> (mm)</u> | <u>log10N0</u><br>(mm <sup>-1-µ</sup> m <sup>-3</sup> ) | μ <u>(unitless)</u> | Λ <u>(mm<sup>-1</sup>)</u> |
|-------------|----------|------------------------------|---------------------------|---------------------------------------------------------|---------------------|----------------------------|
|             | Mean     | 8.12                         | 1.445                     | 5.900                                                   | 6.379               | 7.341                      |
| PARSIVEL    | Variance | 13.82                        | 0.020                     | <u>1.160</u>                                            | 6.498               | 5.596                      |
| TARSIVEL    | Skewness | 0.65                         | 0.447                     | 1.061                                                   | 0.9467              | <u>1.198</u>               |
|             | Kurtosis | <u>-0.13</u>                 | 0.472                     | 2.480                                                   | 1.818               | <u>2.792</u>               |
|             | Mean     | 8.94                         | 1.666                     | 4.813                                                   | 4.262               | <u>5.397</u>               |
| CCTV        | Variance | <u>69.33</u>                 | 0.121                     | 1.185                                                   | 4.577               | 6.714                      |
| <u>ccrv</u> | Skewness | 2.75                         | 0.355                     | 2.596                                                   | 1.903               | <u>2.640</u>               |
|             | Kurtosis | 11.71                        | -0.202                    | 8.962                                                   | 5.714               | 9.756                      |





461 (case 2). Red line is linear regression. Scatter plot displays CC, MAE, RMSE, MAPE for R > 0 mm h-1, R < 5 mm h-1, and  $R \ge 5$ 

## 463 6 Conclusion

464 This study estimated DSD with an infrared surveillance camera, based on which rainfall intensity was also estimated. Rain 465 streaks were extracted using a KNN-based algorithm. The rainfall intensity was estimated based on DSD using physical optics 466 analysis. A rainfall event was selected, and the applicability of the method in this study was examined. The estimated DSD 467 was verified using a PARSIVEL. Furthermore, a tipping bucket rain gauge was used for comparison. The results from this 468 study can be summarized as follows.

469 KNN-based algorithm illustrates suitable performance in separating the rain streaks and background layers. Furthermore,
 470 the possibility of separation for each rain streak and estimation of DSD was sufficient.

471 The number concentration of raindrops obtained through the CCTV images was similar to the actual PARSIVEL observed

472 number concentration in the 0.5 to 1.5 mm section. In the small raindrops in the section of 0.4 mm or less, the PARSIVEL

473 observation data underestimates the actual DSD. However, the CCTV image-based rain rate had an advantage over the

475 0.3 mm diameter section.

<sup>462 &</sup>lt;u>mm h-1 (sequentially from left to right).</u>

The maximum raindrop diameter and number concentration of less than 1 mm produced similar results during the period with a high ratio of diameters less than 3 mm. However, the number concentration was overestimated during the period when raindrops larger than 3 mm were observed. The CCTV image-based data revealed that the rain rate was overestimated because of the overestimation of raindrops larger than 3 mm. After comparing with the 15-min cumulative PARSIVEL rain rate, the CCs—MAE, RMSE, and MAPE—<u>of case 1 (case 2)</u>—were 0.8461 mm h<sup>-1</sup>; (1.55 mm h<sup>-1</sup>), 0.99 mm h<sup>-1</sup> (1.43 mm h<sup>-1</sup>;), and <u>481</u> <u>48% (44%-%)</u>. The differences according to rain rate can be identified. The accuracy is higher at a rain rate smaller than 2<u>10</u> mm h<sup>-1</sup> as a boundary.

The rain rate and  $D_{\mu\nu}$  calculated using CCTV images exhibited similar average values. The overestimated number concentration of 1.5 mm or larger caused high kurtosis for the rain rate and  $D_m$  of CCTV-based data and a low  $\mu$  value. Because of the high number concentration for raindrops larger than 3 mm of CCTV, the PARSIVEL observation data had a higher  $\Lambda$ value than the result based on the CCTV data.

In this study, DSD was estimated using an infrared surveillance camera; the rain rate was also estimated. Consequently, we could confirm the possibility of estimating an image-based DSD and rain rate obtained based on low-cost equipment in dark conditions. Though, the infrared surveillance camera considered in this study will not be able to replace traditional observation devices, if future studies can be continued to secure robustness, it will be an excellent complement to the existing observation system in terms of spatiotemporal resolution and accuracy improvement.

## 492 Appendix. The diameter and fall velocity information for each diameter channel class.

## 493 <u>Table 1: The representative diameter and spread for each diameter channel class.</u>

| Class number | Class average (mm) | <u>Class spread</u><br>(mm) | Class number | Class average (mm) | <u>Class spread in</u><br>(mm) |
|--------------|--------------------|-----------------------------|--------------|--------------------|--------------------------------|
| 1            | 0.062              | 0.125                       | <u>17</u>    | 3.250              | 0.500                          |
| <u>2</u>     | <u>0.187</u>       | 0.125                       | <u>18</u>    | <u>3.750</u>       | 0.500                          |
| <u>3</u>     | 0.312              | 0.125                       | <u>19</u>    | 4.250              | 0.500                          |
| <u>4</u>     | <u>0.437</u>       | 0.125                       | <u>20</u>    | <u>4.750</u>       | 0.500                          |
| <u>5</u>     | <u>0.562</u>       | 0.125                       | <u>21</u>    | <u>5.500</u>       | <u>1.000</u>                   |
| <u>6</u>     | 0.687              | 0.125                       | <u>22</u>    | <u>6.500</u>       | <u>1.000</u>                   |
| <u>7</u>     | <u>0.812</u>       | <u>0.125</u>                | <u>23</u>    | <u>7.500</u>       | <u>1.000</u>                   |
| <u>8</u>     | 0.937              | 0.125                       | <u>24</u>    | 8.500              | <u>1.000</u>                   |
| <u>9</u>     | <u>1.062</u>       | 0.125                       | <u>25</u>    | <u>9.500</u>       | <u>1.000</u>                   |
| <u>10</u>    | <u>1.187</u>       | <u>0.125</u>                | <u>26</u>    | <u>11.000</u>      | <u>2.000</u>                   |
| <u>11</u>    | <u>1.375</u>       | 0.250                       | <u>27</u>    | 13.000             | <u>2.000</u>                   |
| <u>12</u>    | <u>1.625</u>       | 0.250                       | <u>28</u>    | <u>15.000</u>      | <u>2.000</u>                   |
| <u>13</u>    | <u>1.875</u>       | 0.250                       | <u>29</u>    | 17.000             | 2.000                          |
| <u>14</u>    | <u>2.125</u>       | 0.250                       | <u>30</u>    | <u>19.000</u>      | <u>2.000</u>                   |
| <u>15</u>    | 2.375              | 0.250                       | <u>31</u>    | 21.500             | 3.000                          |

(서식 있음: 글꼴 기울임꼴 (서식 있음: 글꼴 기울임꼴 이래 첨자

|                 | 1                | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
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|                 |                  | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
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|                 | $\parallel$      | 서식 있음: 위치 기로 왼쪽 기준 네로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자,텍스트 배치 둘러싸기 |
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| $\parallel$     | '/               | 서식 있음: 위치 기로 왼쪽 기준 네로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자,텍스트 배치 둘러싸기 |
| $\ $            | $\left  \right $ | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
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|                 |                  | 서식 있음: 위치 가로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>가로 :0 글자 텍스트 배치 동러싸기 |
|                 | -                | 서식 있음: 위치 기로 왼쪽 기준 세로 막대형 세로 기본 기준 여백 ,<br>기로 :0 글자 텍스트 배치 둘러싸기 |
|                 |                  |                                                                 |

|                                                                                       | <u>16</u>    | <u>2.750</u>                                      | 0.500                                                                                                     | <u>32</u> | <u>24.500</u>                                | <u>3.000</u>                                      |  |  |  |  |
|---------------------------------------------------------------------------------------|--------------|---------------------------------------------------|-----------------------------------------------------------------------------------------------------------|-----------|----------------------------------------------|---------------------------------------------------|--|--|--|--|
| Table 2: The representative fall velocity and spread for each diameter channel class. |              |                                                   |                                                                                                           |           |                                              |                                                   |  |  |  |  |
|                                                                                       | Class number | <u>Class average</u><br><u>(m s<sup>-1</sup>)</u> | Class spread         Class number         C           (m s <sup>-1</sup> )         Class number         C |           | <u>Class average</u><br>(m s <sup>-1</sup> ) | <u>Class spread</u><br>( <u>m s<sup>-1</sup>)</u> |  |  |  |  |
|                                                                                       | <u>1</u>     | 0.050                                             | <u>0.100</u>                                                                                              | <u>17</u> | <u>2.600</u>                                 | <u>0.400</u>                                      |  |  |  |  |
|                                                                                       | 2            | 0.150                                             | <u>0.100</u>                                                                                              | <u>18</u> | 3.000                                        | 0.400                                             |  |  |  |  |
|                                                                                       | <u>3</u>     | 0.250                                             | <u>0.100</u>                                                                                              | <u>19</u> | <u>3.400</u>                                 | <u>0.400</u>                                      |  |  |  |  |
|                                                                                       | <u>4</u>     | 0.350                                             | <u>0.100</u>                                                                                              | <u>20</u> | <u>3.800</u>                                 | <u>0.400</u>                                      |  |  |  |  |
|                                                                                       | 5            | 0.450                                             | <u>0.100</u>                                                                                              | 21        | 4.400                                        | 0.800                                             |  |  |  |  |
|                                                                                       | <u>6</u>     | 0.550                                             | 0.100                                                                                                     | 22        | 5.200                                        | 0.800                                             |  |  |  |  |
|                                                                                       | <u>7</u>     | 0.650                                             | <u>0.100</u>                                                                                              | 23        | 6.000                                        | 0.800                                             |  |  |  |  |
|                                                                                       | <u>8</u>     | <u>0.750</u>                                      | <u>0.100</u>                                                                                              | <u>24</u> | <u>6.800</u>                                 | 0.800                                             |  |  |  |  |
|                                                                                       | <u>9</u>     | 0.850                                             | 0.100                                                                                                     | 25        | 7.600                                        | 0.800                                             |  |  |  |  |
|                                                                                       | <u>10</u>    | <u>0.950</u>                                      | 0.100                                                                                                     | <u>26</u> | 8.800                                        | <u>1.600</u>                                      |  |  |  |  |
|                                                                                       | <u>11</u>    | <u>1.100</u>                                      | <u>0.200</u>                                                                                              | <u>27</u> | <u>10.400</u>                                | <u>1.600</u>                                      |  |  |  |  |
|                                                                                       | <u>12</u>    | <u>1.300</u>                                      | 0.200                                                                                                     | <u>28</u> | 12.000                                       | <u>1.600</u>                                      |  |  |  |  |
|                                                                                       | <u>13</u>    | 1.500                                             | <u>0.200</u>                                                                                              | <u>29</u> | 13.600                                       | <u>1.600</u>                                      |  |  |  |  |
|                                                                                       | <u>14</u>    | <u>1.700</u>                                      | 0.200                                                                                                     | <u>30</u> | <u>15.200</u>                                | <u>1.600</u>                                      |  |  |  |  |
|                                                                                       | <u>15</u>    | <u>1.900</u>                                      | <u>0.200</u>                                                                                              | <u>31</u> | 17.600                                       | <u>3.200</u>                                      |  |  |  |  |
|                                                                                       | <u>16</u>    | <u>2.200</u>                                      | 0.400                                                                                                     | <u>32</u> | 20.800                                       | <u>3.200</u>                                      |  |  |  |  |

## 495 Data availability

494

496 The data and code can be provided by the corresponding author (hjkim22@cau.ac.kr) upon request.

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