Reactive uptake coefficients for multiphase reactions determined by a dynamic chamber system

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Abstract

15   Dynamic flow-through chambers are frequently used to measure gas exchange rates between the atmosphere and biosphere on the Earth's surface such as vegetation and soils. Here, we explore the performance of a dynamic chamber system in determining the uptake coefficient γ of exemplary gases (O_3 and SO_2) on bulk solid-phase samples. After characterization of the dynamic chamber system, the derived γ is compared with that determined from a coated-wall flow tube system. Our results show that the dynamic chamber system and the flow tube method show a good agreement for γ in the range of 10^{-8} to 10^{-3}. The dynamic

20   chamber technique can be used for liquid samples and real atmospheric aerosol samples without complicated coating procedures, which complements the existing techniques in atmospheric kinetic studies.

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1 Introduction

Multiphase and heterogeneous chemical reactions can influence the formation and transformation of atmospheric trace gases and aerosols, and thus play a crucial role in atmospheric chemistry, climate, and human health (Su et al., 2020;Zheng et al., 2020;Pöschl and Shiraiwa, 2015;Kolb et al., 2010;Pöschl, 2005;Rossi, 2003;Jang et al., 2002;Gard et al., 1998). To evaluate

5   their impacts, we need to understand the reaction kinetics of multiphase processes (Rossi, 2003;Kolb et al., 2010). Reactive uptake coefficients, commonly designated as γ, is an important parameter used to quantify uptake and reaction kinetics (Ravishankara, 1997;Davidovits et al., 2006;Seinfeld and Pandis, 2016b). Different experimental techniques have been developed to determine γ, such as droplet train flow reactors, Knudsen cells, flow tube reactors and aerosol/smog chambers (Usher et al., 2003;Davidovits et al., 2006;Kolb et al., 2010;Crowley et al., 2010;Ammann et al., 2013).

Among these diverse techniques, flow tube reactors and aerosol/smog chambers are two of the most widely adopted measurement methods. Flow tube reactors can generally be classified as coated- and wetted-wall flow tubes as well as aerosol flow tubes. The coatings of coated-wall flow tube reactors can be solids or semisolids including, for example, salts (Davies and Cox, 1998;Chu et al., 2002;Qiu et al., 2011), ice (Fernandez et al., 2005;McNeill et al., 2006;Petitjean et al.,

15   2009;Symington et al., 2012;Hynes et al., 2002;Hynes et al., 2001;Bartels-Rausch et al., 2005), mineral dust (El Zein and Bedjanian, 2012;Bedjanian et al., 2013), soot (McCabe and Abbatt, 2009;Khalizov et al., 2010;Monge et al., 2010), proteins (Shiraiwa et al., 2011) and soils (Stemmler et al., 2006;Wang et al., 2012;Donaldson et al., 2014a;Donaldson et al., 2014b;VandenBoer et al., 2015;Li et al., 2016). Wetted-wall flow tube reactors employ thin liquid films such as water (Henstock and Hanratty, 1979;Hanson et al., 1992), sulphuric acid (Hanson et al., 1992;Hanson and Ravishankara, 1995) or

20   other organic-containing liquids (Barcellos da Rosa et al., 2003;Thornberry and Abbatt, 2004). Additionally, aerosol flow tubes can be used to investigate the multiphase processes between gas phase and lab-generated liquid/solid particles, supposed to simulate realistic atmospheric conditions through laboratory studies (Davidovits et al., 2006;Kolb et al., 2010). On the other hand, large aerosol/smog chambers are commonly used for investigations of particles' formation and growth processes as well as the relevant formation kinetics under laboratory conditions (Shilling et al., 2008;Virtanen et al., 2010;Zhang et al.,

25   2011;Nakao et al., 2012;Schobesberger et al., 2013;Wang et al., 2014;Zhang et al., 2015;McVay et al., 2016;Tiitta et al., 2016;Matsuoka et al., 2017).

Despite numerous uptake/reaction kinetic studies using flow tube reactors and aerosol/smog chambers, some constraints still need to be considered. Experiments using flow tubes can be challenging when (1) the influence of coating surface roughness

30   on experiments for gas uptake and kinetic studies cannot be properly quantified (Li et al., 2018); (2) considering that measurements of ambient samples without changing their properties (e.g., aerosol mixing state) seem almost impossible to achieve; (3) most of the insoluble/low-soluble components of the investigated substances, for example ambient aerosols, are not incorporated into solution-prepared coatings or films, which results in the derived γ unrepresentative of real atmospheric

conditions. Considering the compositional complexity of ambient aerosols, the results obtained only through laboratory studies may not reflect the multiphase processes and respective synergetic effects occurring in the real world (Su et al., 2020). Chamber studies are usually limited to relatively fast uptake kinetics, while the signals of slow uptake will be buried by the competing wall loss effects for aerosols and gases of interest (Rossi, 2003).

In addition to applications in the field of atmospheric chemistry, the chamber technique has also been adopted to measure deposition velocities and further derive the reaction probabilities (i.e., γ) of ozone on surfaces of indoor material like carpets and clothing fabrics (Morrison and Nazaroff, 2000;Canoruiz et al., 1993;Coleman et al., 2008). However, the effectiveness of this technique in investigating uptake kinetics of different reactive trace gases on varying types of bulk samples, which are

10 more relevant to atmospheric kinetic studies, still needs to be evaluated.

Thus, in this work, we developed a method to measure gas uptake coefficients γ, which is suitable for (1) both surrogate aerosols and ambient aerosol samples from the real atmosphere; and (2) both solid and liquid samples. We explain the working principle of our approach based on dynamic chambers, and show how it can be applied to measure γ of various trace gases

15 interacting with different reactive bulk samples. To validate our method, we compare the derived γ with those from the well-established coated-wall flow tube technique and literature data, which shows a good agreement.

2 Material and methods

2.1 Working principle of the chamber method

2.1.1 Uptake coefficient determination

20 Dynamic flow-through chambers had been widely adopted in previous studies to measure trace gas exchange rates between the atmosphere and biosphere such as vegetation and soils (Pumpanen et al., 2001;Gut et al., 2002;Pape et al., 2009;Su et al., 2011;Breuninger et al., 2012;Oswald et al., 2013;Cowan et al., 2014;Almand-Hunter et al., 2015;Plake et al., 2015;Weber et al., 2015;Sun et al., 2016;Meusel et al., 2016;Meusel et al., 2018;Wu et al., 2019). Similarly, in our chamber the flux J of a gas reactant can be calculated from the mass balance by

25 $$J = Q \times (C_{in} - C_{out}) \tag{1}$$

where Q is the chamber flow rate, C_{in} is the supplied trace gas concentration at the chamber inlet, C_{out} is the trace gas concentration at the outlet of the chamber containing a sample. Note that in Eq. (1) the difference between C_{in} and C_{out} can be arised not only from gas uptake on the sample but also from its losses on the chamber wall. Here, as we only focus on gas uptake on samples, the chamber wall loss effect should be corrected beforehand. Thus, the flux J_{sam} caused solely by gas

30 reactant at the sample surface is calculated as

$$J_{sam} = Q \times (C_{ref} - C_{out}) \tag{2}$$

where C_{ref} is the gas reactant concentration measured at the outlet of a blank chamber prior to the uptake experiment.

Assuming a well-mixed and steady-state condition in the chamber, the deposition velocity V_d at the chamber outlet can be derived as (Seinfeld and Pandis, 2016a):

$$V_d = \frac{J_{sam}}{C_{out} \times A} \tag{3}$$

where A is the cross-sectional area at the chamber outlet, which equals the surface area of the chamber bottom.

The deposition velocity can be used to calculate the surface uptake/reaction kinetics. In analogy to electrical resistances under both ambient (Seinfeld and Pandis, 2016a) and chamber-modified conditions (Pape et al., 2009), the uptake process can be decomposed into two processes: transport to the surface and uptake on the surface. A simplified two-resistor model proposed by Canoruiz et al., (1993) is therefore used:

$$\frac{1}{V_d} = R_t + R_s = \left(\frac{1}{V_t} + \frac{4}{\gamma_{obs} \times \omega} \right) \tag{4}$$

where R_t is the transport resistance, which equals the reciprocal of the transport-limited deposition velocity V_t; R_s is the surface uptake resistance, which is determined by the observed uptake coefficient γ_{obs} and the mean molecular speed ω of the gas reactant. Comparison between this two-resistor model and the resistance model (for dry deposition) proposed by Seinfeld and Pandis (2016a) reveals that the transport resistance R_t can be viewed as the sum of the aerodynamic resistance R_a and the quasi-laminar layer resistance R_b. Thus, R_t (or V_t) is dependent on the flow/mixing conditions in the chamber (accounting for R_a and R_b) as well as the molecular diffusivity of the gas reactant itself (accounting for R_b).

Based on Eqn. (4), an expression for γ_{obs} can be given as:

$$\gamma_{obs} = \left(\frac{\omega}{4} \left(\frac{1}{V_d} - \frac{1}{V_t} \right) \right)^{-1} \tag{5}$$

After accounting for the sample mass m_s, we can finally get the mass-independent uptake coefficient γ_{BET}:

$$\gamma_{BET} = \gamma_{obs} \times \left(\frac{A}{A_{ss}} \right) = \gamma_{obs} \times \left(\frac{A}{m_s \times S_{BET}} \right) \tag{6}$$

where A_{ss} is the sample specific surface area (in m^2), which equals the sample mass m_s (in g) times the sample specific BET surface area S_{BET} (in m^2 g^{-1}). One should keep in mind that for liquid samples in a petri dish, A_{ss} is equivalent to the geometric surface area of the petri dish. Moreover, adopting A_{ss} for γ_{BET} calculation only holds when the whole sample coating contributes to uptake of the gas reactant within the experiment period. Using the method described in our previous study (Li et al., 2019) a maximum diffusion time of ~ 5 min is estimated for O$_3$/SO$_2$ penetrating through our solid samples, which is comparable to our uptake experiment time scale (i.e., residence time of ~ 5 min).

V_d can be calculated through Eqn. (3) based on chamber flux measurements. Actually, V_t can be viewed as a special situation when $R_s << R_t$ (i.e., when γ is in the range of 10^{-2} - 1, $4/(\gamma \times \omega)$ is in the range of $10^{-4} – 10^{-2}$ s cm^{-1}, which is two to four orders of magnitudes smaller than R_t, see Sect. 3.1.3. Note that at our experimental temperature of 23 °C, $\omega_{SO2} = 313$ m s^{-1} and $\omega_{O3} = 361$ m s^{-1}). Therefore, V_t can be obtained experimentally by finding a specific trace gas species with a γ on the order of 10^{-2} to

5   1. Saturated potassium iodide (KI) solutions and solid KI coatings have been demonstrated to be a perfect sink for O_3 with a γ up to 10^{-2} (Galbally and Roy, 1980;Parmar and Grosjean, 1990;Rouvière et al., 2010) and have been used to obtain V_t (Morrison and Nazaroff, 2000;Coleman et al., 2008;Pape et al., 2009). Note that the determined V_t depends on the chamber setup and experimental conditions (i.e., gas flow rate, gas mixing state, temperature, pressure and RH, and the speed of the mixing fan). Because physical properties of samples can potentially influence R_b (e.g., the surface roughness of a sample can affect the

10   thickness of the quasi-laminar layer above it) and hence R_t, the KI samples should also have the same or similar phase state and surface morphology as those of the investigated samples. Thus, in this study, V_t was determined by measuring O_3 uptake on different types of KI substrates (i.e., saturated KI solutions, KI films/grains held in a petri dish, see Sect. 3.1.3), to check the effects of their phase state and surface morphology on V_t. On the other hand, when R_b is the limiting step for V_t, the determined V_t based on O_3 uptake on KI cannot be directly used for other gas reactants. A correction is therefore necessary

15   (Goldan et al., 1988):

$$V_{t,i} = V_{t,O_3} \times \sqrt{\frac{M_{O_3}}{M_i}} \tag{7}$$

where $V_{t,i}$ is the transport-limited deposition velocity of gas reactant i, $V_{t,O3}$ is the observed transport-limited deposition velocity of O_3, and M_i and M_{O3} are the molar mass of i and O_3, respectively. Notably, turbulent diffusion is not affected by molecular weight, hence the V_t correction becomes exaggerated for cases where $R_a \gg R_b$. We estimated R_a and R_b according to our chamber

20   configuration and experimental conditions. Details about comparisons between R_a and R_b can be found in the Supplement. These results show that R_a is several times larger than R_b when solid oxide samples are used for uptake experiments. Herein, V_t measured by O_3 uptake on KI can be used as a close approximation of V_t in uptake experiments of other reactive gases.

2.1.2 Upper limit estimation

As discussed above, when $R_s << R_t$, the overall uptake is limited by the transport process (i.e., V_t). Under such conditions, a

25   significant change in γ can only result in a minute alteration of the measured V_d. For example, Figure 1 shows the variation trend of V_d of SO_2 as a function of its γ at four different V_t conditions. All the curves display a linear increase at the lower γ region, and then evolve into a plateau at the higher γ region where V_d becomes non-sensitive to the change of γ. Within this non-sensitive region, a remarkable change of γ (e.g., in several orders of magnitudes) may be reflected by a small change in V_d. However, tiny changes of V_d can also arise from intrinsic measurement errors of the used instruments (see Eqns. (1)-(3))

30   and these measurement uncertainties in V_d may bury those changes caused by variations of γ. This means that for a specific chamber measurement system there is an upper limit for the derived γ.

As shown in Fig.1, V_d becomes non-sensitive to the change of γ when V_d is quite close to V_t. Here, to estimate the maximum value of the derived γ by our chamber method, we define an upper limit of γ corresponding to the case when V_d reaches $0.95V_t$. With this definition, when a V_t is identified, the upper limit of the measurable γ can be calculated through Eqn. (5). The

5   identified V_t of our chamber system for the uptake experiments is ~ 0.7 cm s^{-1}, which allows for γ derivation with an upper limit of ~ 1.7×10^{-3} (indicated by the orange dotted line in Fig. 1).

For the lower limit of the derived γ by our method, as V_d is sensitive to the change of γ within the lower range, in principle there is no such a limit for our chamber system provided that the tiny concentration difference (caused by slow uptake processes)

10   between chamber inlet and outlet can be recognized by the adopted gas analyzers.
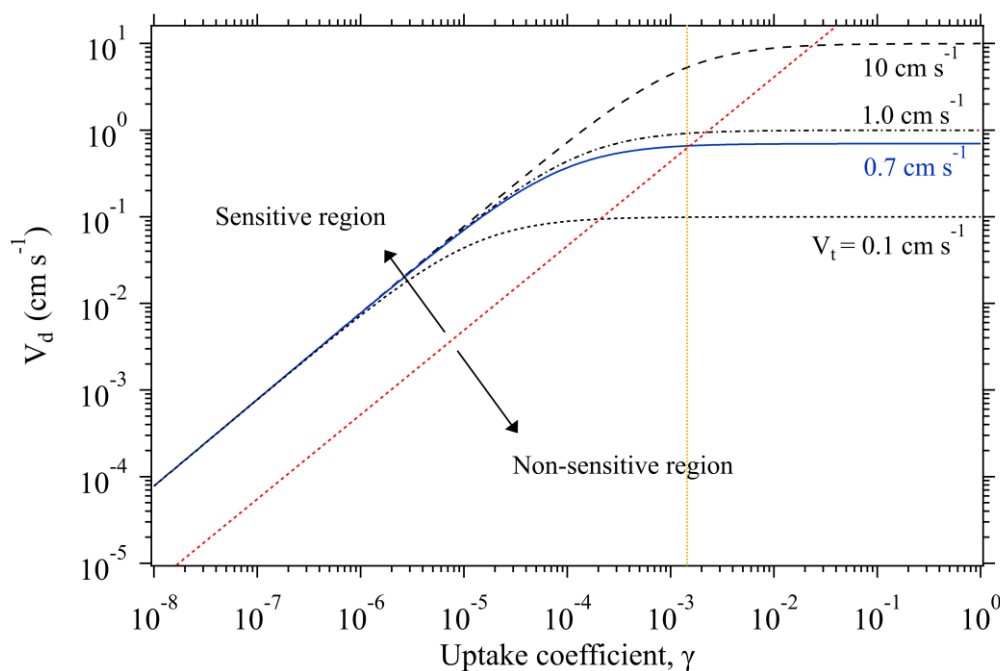
Figure 1. Change of deposition velocity V_d of SO_2 as a function of its uptake coefficient γ, at different transport-limited deposition velocity V_t conditions. The blue line shows the V_t obtained from our chamber measurements of O_3 deposition on KI

15   samples and used for γ derivation of the uptake experiments. The orange dotted line indicates the upper limit of the derivable γ by our chamber system. Based on the sensitivity of the change of V_d against the variation of γ, each function curve can be deemed to have two regions: sensitive and non-sensitive regions, as separated by the red dotted line. All the function curves correspond to the case with a constant experimental temperature of 296 K.

2.2 Experiment overview

A chamber system (see Sect. 2.4.1 for details) was built and employed for uptake experiments under controlled laboratory conditions at a pressure of 1 atm and at room temperature of 296 ± 1 K. After characterization and optimization of the chamber, the uptake of O_3 and SO_2 on different types of solid samples were measured to derive respective γ. To assess the performance of the dynamic chamber method, coated-wall flow tube experiments were also conducted. All uptake experiments were performed with pre-humidified ($50 \pm 1\%$ relative humidity (RH)) zero air. Details about the zero-air generation and humidification can be found in Sect. 2.4.1.

2.3 Sample preparation

Different solid-phase substrates including three types of oxide powders were used in this study. For flow tube experiments, solid-phase samples were coated onto the inner walls of the flow tubes. For uptake experiments applying the chamber technique, the samples were placed or coated into a glass petri dish, which was placed at the centre of the chamber bottom.

Commercially available oxide samples including SiO_2, TiO_2 and Fe_2O_3 (see Table 1 for details) were used in both chamber and flow tube uptake experiments. Their specific surface areas were measured using a water vapour adsorption method based on the Brunauer-Emmett-Teller (BET) adsorption theory (Brunauer et al., 1938). For calculation of the BET surface area, the mass of the adsorbed water on oxide sample after equilibrium with pre-defined RH levels was determined by a non-dispersive infrared (NDIR) gas analyzer (type: Li-6262, LI-COR Biosciences Inc.) operated in the differential mode. The flow tube coatings were prepared by first mixing SiO_2/TiO_2 with deionized water obtained from a Milli-Q system (18.2 MΩ·cm, Millipore) to prepare hydrosols and mixing Fe_2O_3 with ethanol ($\geq 70\%$, Roth, Germany) to prepare alcosol, respectively, and then coating the prepared hydrosols/alcosol onto the sand-blasted inner walls of the flow tubes. To obtain a homogeneous oxide coating, an air-dried continuous rotating coating tool (ACRO) was employed. Details about the ACRO can be found in our previous study (Li et al., 2016). After coating and drying, the coated oxide mass was ~ 55 mg for SiO_2, ~ 35 mg for TiO_2 and ~ 500 mg for Fe_2O_3, respectively. The coating thickness was in the range of several micro-meters to tens of micro-meters depending on the coated mass. For chamber experiments, the oxides were coated onto the bottom of a glass petri dish (I.D.: 116 mm or 90 mm, height: 10 mm). These oxide coatings were dried overnight by placing the hydrosols/alcosol-containing petri dish into a small dynamic drying chamber purged with dry N_2. The dried oxide coatings were smooth and homogeneous to the eye. To exclude potential effects of the coating thickness on uptake kinetics, we pre-determined the mass of the oxide coating needed in the petri dish based on the dry-coating mass on the flow tube wall and the ratio between the coated geometric surface area of the flow tube inner wall (S_1) and that of the petri dish bottom (S_2). That is, as S_1/S_2 equals 0.5, then the coated-oxide mass in the petri dish should be two times of that in the flow tube, assuming the two different drying methods could result in even coatings with similar densities.

Table 1. Commercial sources and physical properties of oxide samples used in this study

Oxide	Source	Type	Specific surface area (BET), $m^2\ g^{-1}$
SiO_2	Evonik Industries	Aerosil 200	200 ± 25
TiO_2	Evonik Industries	Aeroxide P 25	50 ± 13
Fe_2O_3	Sigma-Aldrich	$\alpha\text{-}Fe_2O_3$	4 ± 1.5

2.4 Systems used for kinetic experiments

5 ### 2.4.1 Chamber system

The chamber system can be divided into five units: (1) gas supply; (2) humidification; (3) chamber; (4) controlling and recording unit and (5) detection unit (see Fig. 2). The gas supply provided different types of gases: i.e., purified compressed air (zero air) serving as carrier gas, and reactant gas either from the gas cylinder (i.e., SO_2) or generated via a generator (i.e., O_3). Compressed dry air was supplied by a compressor and was purified by a series of filter columns filled with glass wool

10 (Merck, Germany), silica gel (2–5 mm, Merck, Germany), Purafil® ($KMnO_4/Al_2O_3$, Purafil Inc. USA) and activated charcoal (LS - labor service, Germany), respectively, producing an air flow free of O_3 and SO_2 (Sun et al., 2016). SO_2 was supplied from a calibration gas cylinder (Westfalen AG, Germany; SO_2 analytical value: 10.3 ppm, analytical accuracy: $\pm 5.00\%$) and O_3 was generated in zero air by photolysis of O_2 using a UV light (O_3 generator SOG-2, Analytic Jena, USA). Gas humidification was achieved by a split (dry/wet) gas system regulated by PID-controlled mass flow controller unit (MFCs)

15 (Bronkhorst® High-Tech, Netherland). A RH sensor was applied at the outlet of the humidifier as a reference for PID setpoint control. A similar humidification system had been tested earlier and showed a good stability in a previous study by Sun et al. (2016). Note that the addition of O_3 and SO_2 into the main gas flow was downstream of the humidification unit.

One dynamic flow-through chamber was employed in our chamber measurement system. A petri dish was placed on the

20 chamber bottom to hold the sample during the gas uptake experiments, as shown in Fig. 2. This chamber was 123 mm in diameter and 132 mm in height, which resulted in a chamber volume of ~ 1.56 L. The chamber wall was made of FEP foil (Saint Gobain Performance Plastics Corporation, USA) to minimize the wall loss of reactive gas species. Possible sample gas losses due to chamber wall/gas-phase reactions were checked before each uptake experiment and this effect was corrected during the subsequent data analyses (see Sect. 3.1). A fan coated with Teflon® was installed at the centre of the chamber lid

25 to ensure well-mixed turbulent conditions inside the chamber. Gas inlet was positioned at the chamber lid. The effects of different chamber outlet locations on the measured uptake are discussed in Sect. 3.1. The total flow rate of supplied gas was a bit higher than the flow going through the dynamic chamber which was determined by the trace gas analyzers. The flow of the

vent positioned upstream of the chamber could be adjusted by a needle valve. In this way, a small overpressure inside the chamber could be sustained, which avoided contaminations from lab air.

An O_3 analyzer (Model 49*i*, Thermo Fisher Scientific, USA, lower detection limit: 1 ppbv) and a SO_2 analyzer (Model 43*i*,

5 Thermo Fisher Scientific, USA, lower detection limit: 1 ppbv) were used for reactive trace gas analysis. Before uptake experiments, we calibrated the SO_2 analyzer by multi-stage dilution of a SO_2 calibration gas (10.3 ppm, analytical accuracy: ± 5.00%, Westfalen AG, Germany). Results of the SO_2 multi-point calibration can be found in the supplement (Fig. S1). A time resolution of 10 s was used for trace gas analysis and data were recorded by a PC.
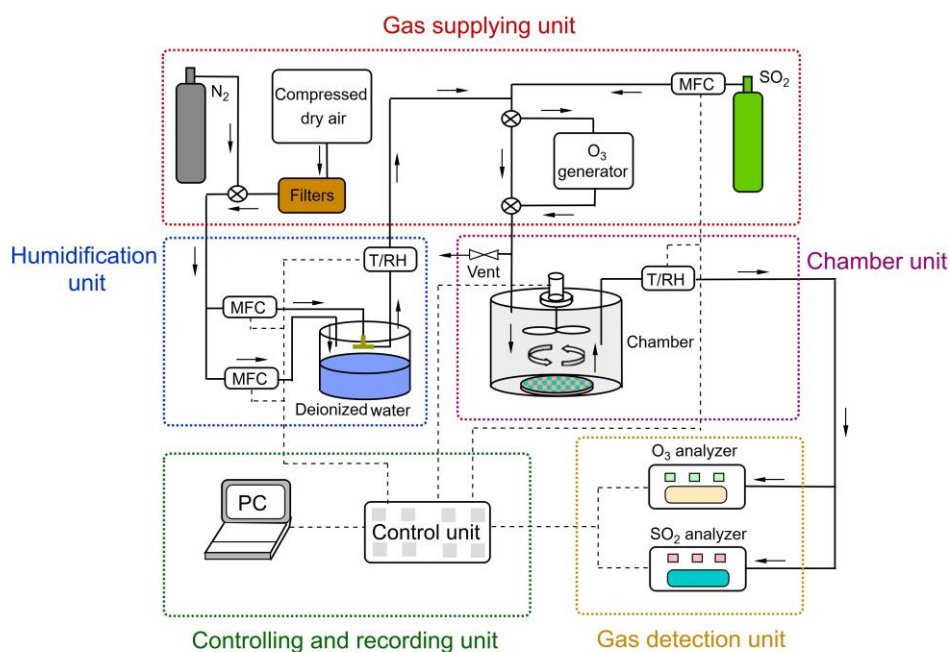
Figure 2. Schematic of the chamber system. The N_2 was only used to pre-condition the prepared samples at different RH and the filtered compressed air was used for uptake experiments.

2.4.2 Flow tube system

15 A coated-wall flow tube system was used to investigate the uptake of SO_2 and O_3 on oxide coatings. Briefly, the system consisted of four parts: (1) a sample and a reference tube; (2) a reactant gas (O_3/SO_2) supply; (3) a humidification unit; and (4) detection units. Two glass tubes (inner-wall surface sandblasted) with identical dimensions (I.D.: 17 mm, L: 100 mm) were employed, with one coated with the oxide samples (i.e., sample tube) and the other remained uncoated as a reference. Both

tubes were maintained at a temperature of 296 ± 0.5 K during the experiments. The same hardware components, except the chamber, were also used for the flow tube system (see Sect. 2.3.1).

A similar operation procedure of the flow tube experiments was described in our previous study (Li et al., 2016). For all the
5   uptake experiments employing flow tubes, the flow rate in the sample tube was kept constant at 1.3 L STP min^{-1} and the Reynolds number (R_e) was ~ 113 to ensure laminar flow conditions. Moreover, a pre-tube/entrance region (I.D.: 17 mm, L: 300 mm) without sample coatings was added in front of the coated tube region to allow for the development of a laminar flow near the tube entrance and finally a well-developed laminar flow pattern within the entire coated section (Li et al., 2018). Calculations of uptake coefficients were based on reactant gas concentration differences between the sample tube inlet and
10   outlet (i.e., penetration). Note that the reactant gas concentrations at the sample tube inlet were equal to those at the reference tube outlet. Gas diffusion correction on the uptake coefficients was achieved by using a numerical Cooney-Kim-Davis (CKD) method (Murphy and Fahey, 1987), which provides results agreeing well with those by other analytical correction methods such as the Knopf-Pöschl-Shiraiwa (KPS) method (Knopf et al., 2015;Li et al., 2016).

3 Results and discussion

15   ### 3.1 Chamber characterization

3.1.1 Chamber equilibrium time

To perform uptake experiments using our chamber system, a petri dish holding the sample needs to be placed into the chamber (see Sect. 2.3). To achieve this, the procedure is as follows: (1) determine C_{ref} of the blank chamber; (2) open the chamber lid; (3) put the sample-holding petri dish onto the chamber bottom; (4) and close the chamber lid. Opening the chamber lid to insert
20   a sample disrupts the steady-state conditions achieved during C_{ref} measurements. We here denote the time period needed to re-establish the steady-state condition as the chamber equilibrium time (Fig. 3).

Figure 3 shows the evolutions of mixing ratios of O_3 and SO_2 in two individual experiments respectively, due to insertion of a blank sample petri dish into the chamber. Please note that measurements of all the mixing ratios were achieved by using a
25   fixed chamber outlet position (C, see Sect. 3.1.2). O_3 and SO_2 are first monitored upstream of the chamber (inlet) for 10 min, in order to obtain the mixing ratios in the supply gas (background), which is not influenced by the uptake in the chamber (i.e., excluding the effects of wall losses and potential chemical reactions inside the chamber). Note that during the background check the chamber is continuously flushed with these gas reactants. After 10 minutes (Fig. 3) the outlet concentrations of the blank chamber are measured for another 10 minutes. A slight decrease of mixing ratios (~ 4 ppb) is found for O_3, which can
30   be assigned to a chamber wall-loss effect. To avoid this effect, the chamber could have been pre-conditioned by flushing with high O_3 mixing ratios over a long time period (e.g. overnight). The wall-loss effect is not observed for SO_2, though. Any observed wall-loss effect for O_3 was considered and corrected during subsequent data analyses. This 10 min measurement is

used to determine C_{ref}, afterwards the chamber lid is opened and then closed mimicking the process in the uptake experiments. From Fig. 3, we can see that the lab air with low mixing ratios enters into the chamber, followed by slowly recovering to the steady-state concentration (C_{ref}) after closing the chamber. From opening of the chamber lid to the point climbing back to C_{ref}, the chamber is in a non-steady state. As shown in Fig. 3, a total time of ~ 5 min (grey shaded area) is considered as the time

5   required for reaching a steady state/dynamic equilibrium of gas reactants in all subsequent data processing. This equilibrium time is subject to (1) the time for the sample petri dish placement operation (1.5 ~ 2 min), (2) the flush-out time of diluted gases inside the chamber (here a purging flow rate of 1.78 L min^{-1} was used, which resulted in a residence time of ~ 1 min in the chamber volume of ~ 1.56 L) and (3) the time for gas analyzers' responses (1.5 ~ 2 min, based on the instrument specifications). Shorter equilibrium times, however, can be achieved by increasing the chamber purging flow rate and/or

10   employing gas analyzers with faster response times. In fact, a shorter equilibrium time is required for rapid uptake kinetics or samples with low uptake capacity (i.e., fast surface saturation). For our uptake experiments, the freshly prepared samples were exposed to the gas reactants for 10 min and only uptake data in the second half of the exposure period (i.e., 6 - 10 min) were used for γ calculation.

15   Considering that γ can represent different uptake stages resulting from gradual surface saturation of a sample, two types of γ have been adopted (Hanisch and Crowley, 2003): the initial uptake coefficient γ_0 and the steady-state uptake coefficient γ_{ss}. γ_0 is obtained at the very beginning or the first few minutes when the sample is exposed to a gas reactant but yet without occurrence of significant saturation. For example, Underwood et al. (2001) studied the heterogeneous reaction of nitric acid on oxide and mineral dust particles, and further calculated γ_0 corresponding to a sample exposure time of ~ 9.5 min. On the

20   other hand, γ_{ss} is used to reflect the uptake properties when uptake comes into a (quasi-) steady state, such as after an exposure time of 3 hours Michel et al. (2003) found that the investigated samples (i.e., α-Al$_2$O$_3$ and α-Fe$_2$O$_3$) approached a steady-state uptake rate for O$_3$. With an exposure (uptake/reaction) time scale of 10 min without significant surface saturation, here the determined uptake coefficients are referred to as γ_0.
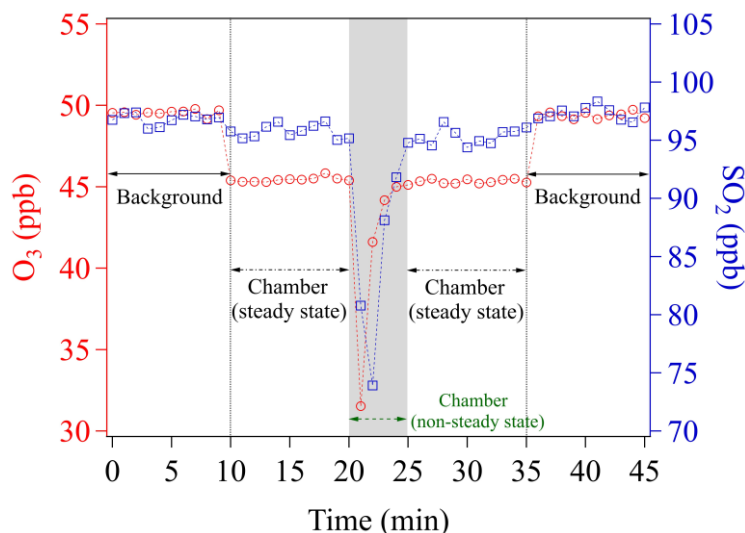
Figure 3. Time course of O_3 and SO_2 mixing ratios while placing an empty sample petri dish into the chamber. The time span of the grey shaded area corresponds to the chamber equilibrium time, which is omitted in any data evaluation.

5 3.1.2 Mixing in the chamber

Here, we used one mixing fan to achieve well-mixed flow conditions inside the chamber. To ensure that the incoming gas reactant is well mixed by the mixing fan prior to depositing on the sample (see Fig. 2), we tested its concentration profile by placing the outlet at different positions inside the chamber.

10 Measurements of O_3 uptake on saturated KI solutions were performed for a series of chamber outlet positions and the observed C_{out} are presented in Fig. 4. All the mixing ratios shown in Fig. 4 were obtained when the chamber reached a steady state, i.e., the mixing ratio at any fixed outlet position remained constant over time (see Fig. 3). Please note that steady-state conditions don't necessarily mean homogeneous distribution of mixing ratios inside the whole chamber (see Fig. 4). As the ab/adsorbing sink is situated on the chamber bottom, a (small) vertical concentration gradient from top to bottom of the chamber might be

15 established, of which the degree depends on the specific turbulent conditions (selection of the applied fan, flow rate and volume) and deposition velocities of the gas reactant.

Five different outlet positions, represented by the coloured squares (i.e., A, B, C, D and E), were chosen. For each experiment, 5 ml of newly prepared saturated KI solution, which formed a thin liquid film in a clean petri dish (I.D.: 90 mm), was exposed

20 to a constant O_3 mixing ratio of ~ 46 ppb. As shown in Fig. 4, discernible differences of the measured C_{out} can be found among three outlet heights: lower height (D and E), medial height (B and C), and upper height (A). C_{out} decreases with lowering the

outlet position height, implying the existence of a small vertical concentration gradient within the chamber: the measured maximum concentration difference between position D and A is 14%. C_{out} at the same outlet heights, i.e., B and C, as well as D and E, show smaller horizontal concentration differences. This demonstrates the measured mixing ratio at outlet position C and E can respectively represent the mixing ratios on the horizontal cross-section where each outlet is located.

To check the concentration gradient conditions inside the same chamber with a larger sample covering almost the entire bottom plate, we used a larger petri dish (I.D.: 116 mm) holding 20 ml of newly prepared saturated KI solution for O_3 (background mixing ratio: ~ 105 ppb) uptake experiments, and respective concentration gradients are shown in Fig. S2. Similar concentration gradient conditions can also be found in Fig. S2. A *t*-test between the measured mixing ratios at different outlet

10 positions also confirms the existence of a vertical concentration gradient inside our chamber, especially when the large sink is situated on the chamber bottom (Table S.1). The horizontal concentration gradient, however, can be much smaller due to the mixing effect of the fan. Therefore, in this study, the outlet position C was chosen for the uptake experiments to better represent the average concentration inside the chamber (see Sect. 2.3.3).
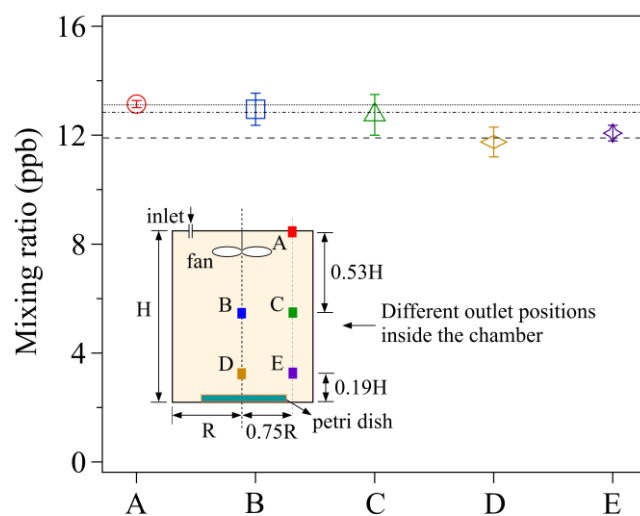
Figure 4. The effects of different chamber outlet positions on observed C_{out}. The labels (A - E) of the X axis represent the different outlet positions shown in the chamber sketch, and the lines are the averaged mixing ratios at the three different vertical outlet heights (A; B/C; D/E). The error bars represent the standard deviation of three replicate experiments. For details, see the text.

3.1.3 Effects of prepared KI coating surface state on V_t

As discussed above, the KI coating during the chamber characterisation tests should have a similar surface phase state as the samples of interest. We therefore checked the effects of the surface phase-state/morphology of different KI coatings on the derived transport-limited deposition velocity V_t.

KI chemicals ($\geq$ 99.0%, Sigma-Aldrich, USA) were used as commercially purchased. Four types of KI coatings were applied for O_3 uptake experiments and the subsequent V_t calculation, respectively: (A) KI film, which was prepared through dissolving ~ 3.8 g of KI into deionized water in a petri dish (I.D.: 50 mm) followed by drying with pure N_2 to form a thin solid film on the petri dish bottom; (B) KI grain, which was prepared by evenly spreading ~ 3.8 g of KI grain (exactly the same as the

10 original state of the obtained chemical, with particles' diameter around several tens of micrometers) in a petri dish and pre-humidified in a 50% RH N_2 environment for 30 min; (C) and the same KI grain pre-humidified in a 73% RH N_2 environment for 30 min. The latter became deliquescent, as at room temperature the deliquescence point of KI is 67% according to Kim et al. (2007) and Rouvière et al. (2010); (D) saturated KI solution, which was prepared by evenly spreading ~ 3.8 g of KI into a petri dish followed by adding several milliliters of deionized water to form a thin saturated-KI-liquid film. For these uptake

15 experiments, the purging flow rate was 1.31 L min^{-1} and the other parameters were the same as those described in Sect. 3.1.1.

Figure 5 shows the calculated V_t for the four types of surface phase-state/morphology of the prepared KI coatings. V_t derived for all these different KI surfaces are not significantly different from each other (with a t-test p values as 0.62, 0.81, 0.52 and 0.84 respectively for the measured V_t of Type I, II, III and IV), indicating that the KI surface characteristics have only a small

20 impact on the calculated V_t and γ, respectively. The averaged V_t in Fig. 5 corresponds to a R_t of ~ 1 s cm^{-1}. And O_3 uptake on KI coatings has a γ on the order of 10^{-2} (Rouvière et al., 2010) corresponding to a R_s of ~ 0.01 s cm^{-1}, which is two orders of magnitude smaller than R_t. This means that O_3 uptake on KI coatings is very efficient (see Sect. 2.3.3) and the uptake is dominantly limited by transport processes (see Fig. 7 for more detailed illustration). Based on the results in Fig. 5, we can have different surface states of KI coatings to imitate those of the investigated samples at the most extent, and these operations can

25 extend applications of the chamber system to a wide range of reactive bulk surfaces associated with uptake/reaction kinetics.
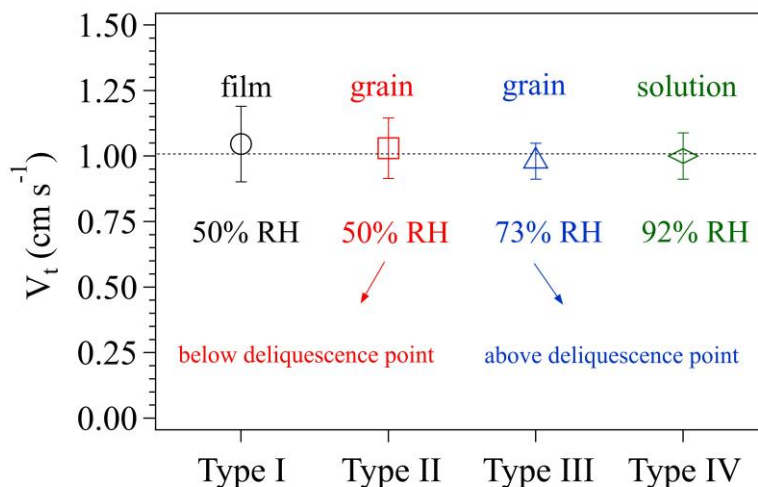
Figure 5. The effects of different surface phase states of KI coatings on the transport-limited deposition velocity V_t. The four types of KI coatings are indicated on the X axis and details of the coating preparation can be referred to the text. The RH values represent the relative humidity conditions of the air in the chamber. The error bars represent the standard deviation of three to four replicate experiments.

3.2 Inter-comparisons of uptake coefficients derived from chamber and flow tube techniques

To evaluate the reliability of the chamber system, γ of O_3 and SO_2 were also derived for three oxide samples by means of flow tube experiments. The flow tube sample preparation procedures and experimental configurations (e.g., flow rate, temperature, pressure and RH) can be found in Sect. 2.

The derived mass-independent uptake coefficients γ_{BET}, which were obtained based on the BET surface area of the investigated oxide samples (see Table. 1), are presented in Fig. 6. Generally, the γ_{BET} determined by both techniques are in good agreement. Note that the chamber technique required a time interval for chamber equilibrium (5 min as shown in Sect. 3.1.1), during which the fresh sample had already been exposed to the gas reactant and sample surface saturation might occur to some extent. This may explain the general tendency of slightly lower γ_{BET} derived from the chamber measurements (red columns) than from the flow tube technique (blue columns). Under comparable experimental conditions (i.e., ambient pressure, temperature and RH) as adopted in the current study, several previous kinetic studies reported γ_{BET} using various measurement techniques: aerosol chamber (Park et al., 2017;Chen et al., 2011;Mogili et al., 2006), coated-wall flow tube (Nicolas et al., 2009), reaction chamber/cell coupled with diffuse reflectance infrared Fourier transform spectroscopy (Shang et al., 2010;Fu et al., 2007;Ullerstam et al., 2002). These reported values are also shown in Fig. 6 by different symbols. Most of the reported γ_{BET} are comparable with our chamber results, which demonstrates the reliability of our chamber technique in determining γ.

However, there are still a few exceptions as represented by the brown diamond (Mogili et al., 2006) and the green hexagon (Fu et al., 2007). The much smaller γ_{BET} observed in the work of Mogili et al. (2006) may be due to the much higher O_3 concentration used in their uptake experiments (i.e., 3 ppm versus ~ 45 ppb in our study). A negative linear dependence of γ on O_3 concentration has been reported by Ullerstam et al. (2002), where the uptake kinetics of O_3 and SO_2 on one type of

5   mineral dust sample were investigated. Regarding the SO_2 uptake on Fe_2O_3, the huge difference of γ_{BET} (four orders of magnitude) between our study and Fu et al. (2007) may be attributed to the differences in surface and structure properties of the samples caused by the differing samples deployed and/or the preparation procedures (Ullerstam et al., 2003): The sample used by Fu et al. (2007) has a BET surface area of 10.2 m^2 g^{-1} and a particle diameter of 39.7 nm compared to our sample with a BET surface area of 4 m^2 g^{-1} and a diameter of < 5 µm. In the work of Fu et al. (2007), ~ 20 mg of oxide sample was prepared

10   by pressing it into a pallet with a diameter of 13 mm, while in our study ~ 500 mg of the sample were evenly coated onto the bottom of a glass petri dish (I.D.: 116 mm) resulting in a much larger geometric surface area for direct contact between SO_2 and Fe_2O_3 compared to Fu et al. (2007). The samples with smaller particle sizes are expected to be quite porous and some parts may be less accessible to SO_2 due to pore resistance and thus the γ_{BET} reported by Fu et al. (2007) can be considered as a lower limit.
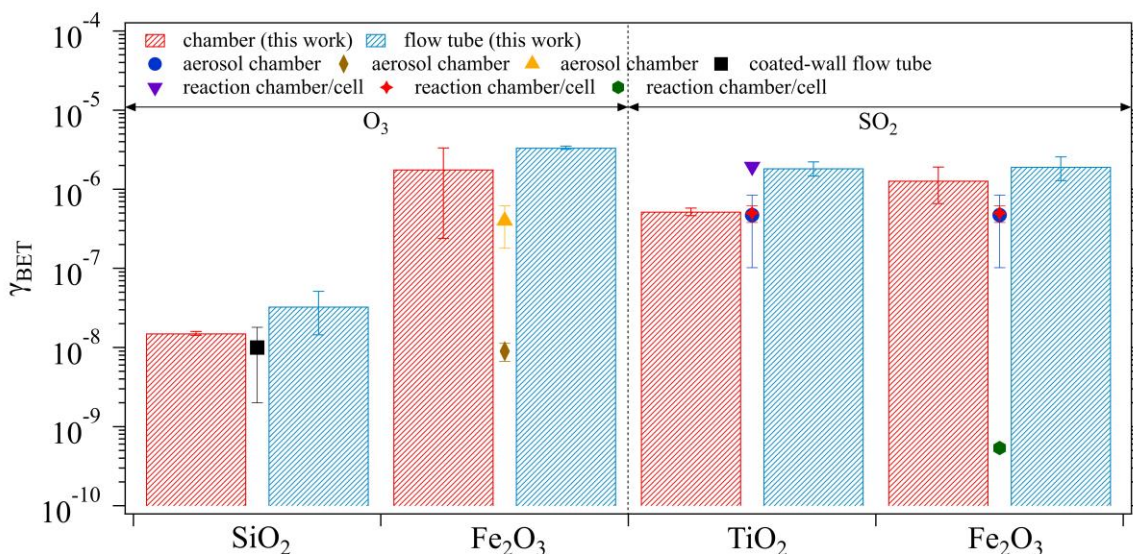
Figure 6. Comparisons between the γ_{BET} derived from the chamber and the flow tube techniques respectively, and from previous kinetic measurements. Previous studies summarized here are: black square (Nicolas et al., 2009), orange triangle (Chen et al., 2011), brown diamond (Mogili et al., 2006), purple triangle (Shang et al., 2010), blue circle (Park et al., 2017), red star (Ullerstam et al., 2002) and green hexagon

20   (Fu et al., 2007). The error bars of the columns represent the standard deviation of three replicate experiments and those of the symbols reflect the standard deviation of the measured γ_{BET} in previous studies.
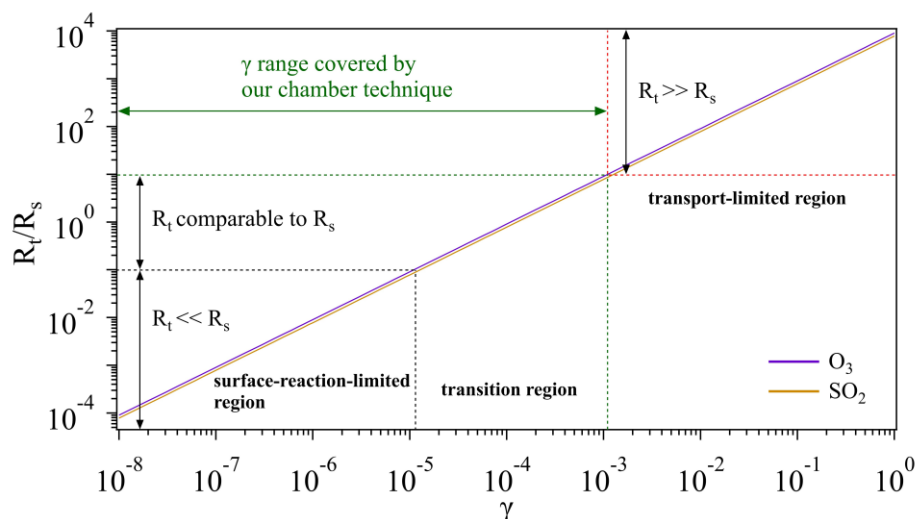
Figure 7. Schematic of different regions for O_3 and SO_2 uptake. The transport resistance R_t is calculated based on the measured average V_t (Sect. 3.1.3). Calculations for the surface resistance R_s are referred to conditions of room temperature (296 K) and 1 atm.

4 Conclusions

10   This study presents a chamber technique to determine uptake coefficients of reactive trace gases (O_3 and SO_2) onto bulk surface systems. Critical operational parameters of the chamber system, including equilibrium time, chamber outlet position and the choice of various KI-coating surface state/morphology were first examined. With these pre-defined parameters, the reliability of this technique to derive γ_{BET} during gas uptake on solid samples was proven through direct comparisons with a flow tube system. The chamber results agree well with those from the flow tube method and the literature data. Given the gas uptake

15   includes both mass transport and surface reaction, its limiting step can be changing as a function of γ. As shown in Fig. 7, when gas uptake comes into the surface-reaction-limited and transition regions the chamber system is sensitive to changes of γ and thus can be employed for the determination of γ within a range of 10^{-8} - 10^{-3}.

Data availability

The underlying research data can be accessed upon contact with Guo Li (guo.li@mpic.de).

Author contribution

Y.C. and H.S. conceived the study. G.L. performed experiments and data analysis. Y.C., H.S., U.P., U.K., G.Z., M.L., L.H., and F.B. discussed the results. G.L., Y.C. and H.S. wrote the manuscript with inputs from all co-authors.

Competing interests

5   Some authors are members of the editorial board of journal Atmospheric Measurement Techniques. The peer-review process was guided by an independent editor, and the authors have also no other competing interests to declare.

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