1 W-band S/Z Relationships for Rimed Snow Particles: Observational Evidence from

2 Combined Airborne and Ground-based Observations

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- 4 Shelby Fuller ¹, Sam Marlow ¹, Samuel Haimov ¹, Matthew Burkhart ¹, Kevin Shaffer ¹, Austin
- 5 Morgan ¹, and Jefferson R. Snider ^{1,2}

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Department of Atmospheric Science, University of Wyoming, Laramie, WY, USA

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² Corresponding Author, jsnider@uwyo.edu

Abstract

14	Values of undercatch-corrected liquid-equivalent snowfall rate (S) at a ground site and
15	microwave reflectivity (Z) retrieved using an airborne W-band radar were acquired during
16	overflights. The temperature at the ground site was between -6 and -15 °C. At flight level, within
17	clouds containing ice and supercooled liquid water, the temperature was approximately 7 $^{\rm o}{\rm C}$
18	colder. Additionally, airborne measurements of snow particle imagery were acquired. The
19	images demonstrate that most of the snow particles were rimed, at least a flight level. A
20	relatively small set of S/Z pairs (4) are available from the overflights. Important distinctions
21	between these measurements and those of Pokharel and Vali (2011), who also reported W-band
22	S/Z pairs and an S/Z relationship for rimed snow particles, are 1) the fewer number of S/Z pairs,
23	2) the method used to acquire S, and 3) the altitude, relative to ground, of the $\underline{\text{W-band}}$ Z
24	retrievals. This analysis corroborates that the S/Z relationship reported in Pokharel and Vali
25	(2011) yields an S - in scenarios with snowfall produced by riming - substantially larger than that
26	derived using an S/Z relationship developed for unrimed snow particles.
27	This analysis indicates that the S/Z relationship reported in Pokharel and Vali (2011) yields an S,
28	in scenarios with snowfall produced by riming, that is substantially larger than that derived using
29	an S/Z relationship developed for unrimed snow particles.

1 - Introduction

Improvement of methods used to measure snowfall and rainfall are an ongoing focus of meteorological research. The various methods are ground-based instruments that evaluate the mass of precipitation that falls into or onto a collector (precipitation gauges) (Brock and Richardson 2001), ground-based radars (Wilson and Brandes 1979), and airborne and spaceborne radars (Matrosov 2007; Kulie and Bennartz 2009; Geerts et al. 2010; Skofronick-Jackson et al. 2017). An objective of these approaches, whether used to make observations independent of other methods (e.g., Kulie and Bennartz 2009), or as a component of multiple observations (e.g., Cocks et al. 2016), is estimation of precipitation rate and accumulated on precipitation amount:

Many studies have investigated using radar for evaluating rainfall (for a review see Wilson and Brandes 1979). There are two approaches. The first is research, both observational and computational, that probes the relationship between rainfall rate (R) and radar-measured values of range-corrected backscattered microwave power. The latter is commonly reported as an equivalent radar reflectivity factor (Z_e). The second is operational in the sense that precipitation gauges are used to calibrate measurements acquired using weather surveillance radars. Complications associated with converting Z_e to R, or converting a radar reflectivity factor (Z) to R, can be grouped in four categories: 1) Inaccuracy in quantification of Z, 2) variation of the R/Z relationship stemming from precipitation processes (e.g., coalescence and break up), 3) difference between the volume of a radar range gate versus the much smaller volume of

¹ Radars are calibrated to report Z_e (Smith 1984). Herein, radar reflectivities are reported as $Z = Z_e$ and as $dBZ = 10log_{10}(Z_e)$.

atmosphere sampled as precipitation falls to a gauge, and 4) vertical displacement between a radar range gate and a calibrating gauge, especially at far ranges.

For situations with snowfall, methods employing either gauge or radar are associated with complications beyond that incurred in rainfall (Matrosov 2007; Martinaitis et al. 2015; Cocks et al. 2016). Problems associated with gauge measurements are wind-induced snow particle undercatch, gauge capping, delayed registration, and blowing snow aliasing as snowfall. Moreover, in a situation with snow particles more most abundant within a radar range gate, compared to rain drops, and where a measurement of Z is used to infer R via a R/Z relationship, the resultant precipitation rate will likely be inaccurate. This is because hydrometeor shape, density, and dielectric properties are all variable for snow particles while relatively invariant for rain drops. Additionally, a snow particle's terminal fall speed varies with size (as is the case for drops) and with particle shape and particle density. Going forward, we refer to the latter two properties as shape and density.

The goals of this paper are as follows: 1) to describe measurements of undercatch-corrected liquid-equivalent snowfall rate (S, mm h⁻¹) and how these were paired with W-band measurements of reflectivity (Z, mm⁶ m⁻³); 2) to contrast the S/Z pairs against S/Z relationships commonly applied in radar retrievals of S; and 3) to investigate why the S/Z pairs deviate from predictions of some S/Z relationships.

In calculations of paired values of S and Z, density is an important parameter. Density is commonly estimated using empirical data (e.g., Pokharel and Vali 2011, [PV11]). For graupel, a snow particle that grows via collection of supercooled cloud droplets in a process commonly referred to as riming, paired observations of particle mass and particle size have been used to estimate density. There is considerable uncertainty in this approach. Based on data collected at

two northwestern US surface sites (Zikmunda and Vali 1972; Locatelli and Hobbs 1974), density values differ by at least a factor of two at particle sizes smaller than 2000 µm (PV11; their Fig. 4). Given that the density of rime ice varies with droplet impact speed, droplet size, and temperature (Macklin 1962), it is not surprising that the density-size relationships analyzed by PV11 are so varied.

- Table 1 and the he following introductory paragraphs overview W-band S/Z relationships being applied in instances with snow particles grownof snowfall where mass is acquired by vapor deposition (crystal), by collection of crystals (aggregate snowflake), and by riming (rimed crystal and graupel). Henceforth, the latter two snow particle types are collectively referred to as rimed snow particles.
- In a computational study, Hiley et al. (2011) considered a variety of snow particle types (column, plate, bullet rosette, sector plate, dendrite, and aggregate snowflake), employed a parameterized ice particle size distribution (PSD) function (Field et al. 2005), accounted for a range of temperature (-5 to -15 °C) via the Field et al. parameterization, and developed a range of S/Z relationships for snow particles. Except for the aggregate snowflakes (henceforth, aggregates)s, the modeled particle types were vapor-grown crystals. Hiley et al.'s upper- and lower-limit relationships are S = 0.21·Z^{0.77} and S = 0.024·Z^{0.91}, respectively. —Matrosov (2007) developed an S/Z relationship for aggregates. In that work, parameterized PSDs from Braham (1990) were employed, and a range of particle aspect ratios were factored into the calculations. For aggregates, the S/Z relationship is S = 0.056·Z^{1.25} (Matrosov 2007). It should be noted that Hiley et al. (2011) and Matrosov (2007) employed similar, but not identical, computational methods. Computational research was also conducted by Kulie and Bennartz (2009) who developed adopted tan S/Z relationship for what they referred to as a "snow particle" type. The

wavelength-dependent density derived by Surussavadee and Staelin (2007) (200 kg m⁻³ at $\lambda = 3.2$ mm), modeled the was adopted, the snow particles were modeled as spheres, and applied PSDs based on the Field et al. parameterization was applied. The resultant S/Z relationship developed for this particle type is $S = 0.52 \cdot Z^{0.83}$ (Surussavadee and Staelin 2007; Kulie and Bennartz 2009; henceforth, SSKB). Variance in the calculations discussed in this paragraph originate from changes in density, shape, fall speed, PSD, and particle size as these changes are propagated through the cloud-microphysical and microwave-scattering calculations.

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In a hybrid approach (computational and an analysis of measurements airborne observations), PV11 concluded that most of the snow particles they imaged were rimed snow particles. Values of S were calculated using a density-size function (ρ_1 , discussed below), a fall speed-size function, a-measured PSDs and measured particle images, and a determination of particle volumes. It was assumed that a prolate spheroid approximated particle shape and that shape is was the basis for determining a particle's sphere-equivalent volume and the particle's sphere-equivalent size. The sphere-equivalent size was applied in the two functions. Values of Z were calculated using a measured PSD, sphere-equivalent sizes, the ρ_1 function, and Mie Theory. PV11 presented calculations of Z, obtained using two density-size relationships (their Eqs. 1 and 2) and compared their calculated reflectivities to measurements of Z from a W-band radar. That led to their conclusion that "...the lower density assumption...vielded closer correspondence to observed reflectivities." Their recommendation for S as a function of measured Z - hereafter the $S(\rho_1)/Z$ best-fit line - is $S=0.39\cdot Z^{0.58}$. Values of Z that were paired with the calculated values of S (i.e., the S/Z pairs from PV11 that we present in Sect. 4), and that were used to determine the $S(\rho_1)/Z$ best-fit line, came from the WCR. In addition to variance in their values of S, coming from a dependence on density, PV11 state that a value of S derived via their best-fit line is

uncertain by a factor-of-ten. That uncertainty is evident in the variance of S/Z data pairs about the $S(\rho_1)/Z$ line in Fig. 11 of PV11. Those investigators, and Geerts et al. (2010), attributed the variance to use of two-dimensional snow particle images in calculations of S and to actual variations of density, shape, and particle size not accounted for in the calculations.

Another set of hybrid-typelso relevant are S/Z relationships was developed reported by Falconi et al. (2018; their Table 2). These are based on were developed using measurements from a video disdrometer, weighing precipitation gauge, microwave radiometer, and a vertically-pointing W-band radar. All these systems were operated at the ground. The data set was stratified into intervals of lightly-rimed, moderately-rimed, and heavily-rimed snow. A proxy for snow particle riming - radiometer measurements of liquid water path – was the basis for the stratifications (von Lerber et al. 2017). The S/Z relationships are $S = 0.10 \cdot Z^{1.0}$ (lightly-rimed), $S = 0.079 \cdot Z^{1.3}$ (moderately-rimed), and $S = 0.060 \cdot Z^{1.4}$ (heavily-rimed).

Our focus is on surface measurements of S and on pairing of those measurements with airborne measurements of Z. We also analyze airborne measurements of snow particle imagery. The latter demonstrates that the particles observed at flight level were rimed. The <u>imagery is the</u> se measurements are the basis for our assertion that our data set is relevant to ongoing investigations of using Z to evaluate S in situations where precipitation is produced by riming.

Section 2 describes the setting of our study, the instruments we deployed, and recordings we obtained using two data acquisition systems. One of the data systems was operated at a ground site and the other on an aircraft. Section 3 is an analysis of the recordings; this section also considers recordings from two additional, but ancillary, ground sites. Our findings are discussed in Sect. 4 and summarized in Sect. 5. An Appendix (Sect. 6) explains how we

- averaged recordings of near-surface W-band reflectivities and surface-based recordings of
- snowfall.

144 Table 1 – W-band S/Z relationships from the literature, snow particle type, and values of minimum relative S difference

Reference	Abbreviation			<u>Minimum</u>	<u>Minimum</u>
	used for	S/Z relationship	Snow Particle Type	<u>relative</u>	<u>relative</u>
	reference			S deference on	S difference on
				December 15	January 3
				2016 a	2017 a
			Upper-limit S/Z		
Hiley et al. (2011)	Ξ.	$S=0.21\cdot Z^{0.77}$	<u>relationship for</u>	<u>0.7</u>	<u>1.0</u>
			vapor-grown crystals		
<u>Matrosov (2007)</u>	-	$S=0.056 \cdot Z^{1.2}$	<u>Aggregates</u>	<u>1.4</u>	8.5 b
Surussavadee and Staelin (2007)			Spherical snow		
and Kulie and Bennartz (2009)	<u>SSKB</u>	$S=0.52 \cdot Z^{0.83}$	particles with	<u>0.3</u>	<u>0.2 °</u>
			$\underline{\text{density}} = 200 \text{ kg m}^{-3}$		
			Rimed snow particles		
Pokharel and Vali (2011)	<u>PV11</u>	$S=0.39 \cdot Z^{0.58}$	assuming the	<u>0.3</u>	0.0 d
			lower of two density-size		
			<u>relationships</u>		
			Snow particles		
Falconi et al. (2018)	Ξ.	$S=0.060 \cdot Z^{1.4}$	classified as heavily	<u>0.6 e</u>	<u>8.5</u>
			rimed		

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a Minimum relative S difference is defined as the minimum of |(S_{HP}-S)|/S where S_{HP} is a measurement of undercatch-corrected liquid-equivalent snowfall rate (Table 6) and S is a snowfall rate on an S/Z relationship line evaluated at one of the attenuation-corrected reflectivities (Sect. 4).

b Attenuation-corrected Z on this day (0.6 mm⁶ m⁻³) is smaller than the lower-limit Z (1 mm⁶ m⁻³) advised for this S/Z relationship (Matrosov 2007).

^c Maximum relative S difference on this day is 0.4.

d Maximum relative S difference on this day is 0.7.

e Maximum relative S difference on this day is 0.9.

2 - Site, Aircraft, and Instruments

2.1 - Site

Analyzed herein are aircraft and ground data from 14/15 December 2016 and from 3 January 2017. The ground data were acquired in a forest/prairie ecotone on the eastern slope of the Medicine Bow Mountains in southeast Wyoming (Figs. 1a-b). No ground-based observers were deployed during the two snowfall events analyzed.

At one of three ground sites (HP in Figs. 1a-b) a hotplate precipitation gauge (Rasmussen et al. 2011; Zelasko et al. 2018), a GPS receiver, and a data acquisition system were deployed. Once per second, the data system ingested a hotplate-generated data string, combined that with time-of-day from the GPS receiver [Coordinated Universal Time (UTC)], and recorded the merged hotplate/UTC data string. The absolute accuracy of the time stamp is no worse than 2 s.

Overflights of the hotplate were done by the University of Wyoming King Air (WKA) on 14/15 December 2016 and on 3 January 2017. The flights were conducted in preparation for the SNOWIE field project (Tessendorf et al. 2019) and were flown from the Laramie, WY Airport (LA in Fig. 1a). Data acquisition on the WKA was also synchronized with UTC, but with much better accuracy than at the hotplate.

Measurements of horizontal wind (speed and direction), temperature, relative humidity, and pressure from the US-GLE AmeriFlux tower (AF in Figs. 1a-b) are also components the analysis. The AmeriFlux data were provided to us as 30-minute averages (AmeriFlux 2021; Marlow et al. 2023).

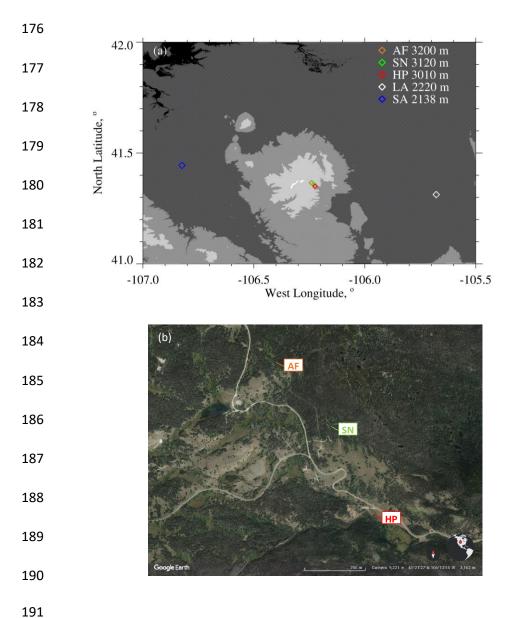


Figure 1 – (a) Southeast Wyoming, airport at Saratoga, WY (SA), airport at Laramie, WY (LA), and the ground sites: AF = US-GLE AmeriFlux tower, SN = Brooklyn Lake SNOTEL, and HP = hotplate. Altitudes of the airports and ground sites are in the legend. Altitude thresholds for the digital elevation map are 1500, 2000, 2500, 3000, and 3500 meters. (b) Close up of the AF, SN, and HP ground sites (from © Google Earth).

2.2 - University of Wyoming King Air (WKA)

The following WKA measurements were analyzed: aircraft position, temperature, snow particle imagery, and three moments of the cloud droplet size distribution function. A Cloud Droplet Probe (CDP; Faber et al. 2018) was the basis for the droplet size distribution measurements and the derived moments. The latter are droplet concentration (N), cloud liquid water content (LWC), and mean droplet diameter (<D>). Snow particle imagery was obtained using a precipitation particle imaging probe (2DP; Korolev et al. 2011) and a cloud particle imaging probe (2DS; Lawson et al. 2006). These acquired two-dimensional images of particles between 200 to 6400 µm (2DP) and between 10 to 1280 µm (2DS).

2.3 – The W-band Wyoming Cloud Radar (WCR)

Retrievals from the up-looking and down-looking antennas of the WCR, operated on the WKA, were also analyzed. For this we used Level 2 WCR data² with reflectivities recorded as $dBZ = 10 \cdot \log_{10}(Z)$. The reflectivities were converted from dBZ to Z prior to processing. Additionally, values of the vertical-component Doppler velocity retrieved from below the WKA using the WCR's down-looking antenna were analyzed. The Doppler velocities were corrected for aircraft motion as described in Haimov and Rodi (2013). We use V_D to symbolize the corrected vertical-component Doppler velocity and adopt the convention that $V_D > 0$ indicates upward hydrometeor motion.

² http://flights.uwyo.edu/uwka/wcr/projects/snowie17/PROCESSED_DATA/

The Level 2 WCR sampling was different on the two flight days and this difference is shown in Table $2\pm$. Ground-based calibrations of the WCR's up-looking antenna and correlations between in-flight retrievals acquired using the WCR's up-looking and down-looking antennas were used to estimate the precision and absolute accuracy of the WCR-derived values of dBZ. These are \pm 1.0 dBZ and \pm 2.5 dBZ, respectively (PV11).

Table 21 – Level 2 WCR sampling and the WKA overflight time

	Level 2 WCR	Level 2 WCR	Overflight
Date	Vertical	Along-track	Time,
	Sampling,	Sampling,	UTC
	m	S	
14/15 December 2016	23	0.23	00:00:38 (15 December 2016)
3 January 2017	30	0.36	20:32:03

2.4 - Hotplate Gauge

Algorithms used to process hotplate measurements are described in Rasmussen et al. (2011), Boudala et al. (2014), and Zelasko et al. (2018). Henceforth, these are referred to as R11, B14, and Z18, respectively. This section describes how hotplate measurements acquired at the HP site were analyzed. The hotplate deployed at the HP site is described in Wolfe and Snider (2012), Z18, and in Marlow et al. (2023).

Five measurements fundamental to the steady state energy budget of the hotplate's temperature-controlled up-viewing plate are output by the hotplate microprocessor as one-minute running averages (Z18). These averages were merged with the GPS time and recorded at 1 Hz by the data acquisition system (Sect. 2.1). With these measurements, calibration data (Marlow et al. 2023), and the algorithm developed by Z18, we calculated S in two steps. First, the five hotplate measurements (electrical power supplied to the plate, ambient temperature, wind speed, downwelling shortwave flux, and downwelling longwave flux) were input to Eq. 3 in Z18. The output of that equation is a provisional liquid-equivalent precipitation rate. Second, the snow particle catch efficiency, described in the next paragraph, was used to calculate S as the ratio of the provisional rate and the catch efficiency.

Marlow et al. (2023; their Fig. 3b) report the relationship between snow particle catch efficiency and wind speed that was applied in the calculation of S. There are three bases for this relationship. First is the catch efficiencies R11 derived using measurements obtained from a weighing gauge, operated within a double fence intercomparison reference shield, and collocated measurements from an unshielded hotplate gauge. These paired measurements are symbolized SRG (shielded reference gauge) and UHG (unshielded hotplate gauge). R11 plotted hotplate catch efficiencies (i.e., UHG/SRG) versus wind speeds measured at 10 m AGL (their Fig. 8).

Second is Marlow et al.'s adjustment of R11's 10 m AGL wind speeds to 2 m AGL. The basis for the adjustment is surface boundary layer parameters derived for R11's site (Kochendorfer et al. 2018) and an equation from Panofsky and Dutton (1984; their Eq. 6.7). The adjustment was made because the hotplate-derived wind speeds, both here and in Marlow et al. (2023), were acquired at approximately 2 m above the snowpack surface. Third is Marlow et al.'s comparison of SNOTEL-derived liquid-equivalent depth changes and hotplate-derived time-integrated accumulations. The interval for the comparisons is 24 hours. Based on the comparison, which has 57 paired values acquired at the sites labeled HP and SN in Fig. 1, the average fractional absolute relative difference is 0.30. Marlow et al. also provided an estimate of the error in a SNOTEL measurement (2.4 mm). At accumulation = 10 mm the error corresponds to a relative error = 0.24. This indicates that SNOTEL contributed significantly to the SNOTEL/hotplate variance and especially so for the smaller accumulations in Fig. 9a of Marlow et al. (2023). Because of this, we do not limit the following estimate of hotplate precision to a subset of the 57 paired measurements. Based on our assessment of the average fractional absolute relative difference, the hotplate precision applied in this analysis was taken to be 0.3.

The hotplate-derived wind speeds acquired at ~ 2 m, and discussed in the previous paragraph, are henceforth symbolized U_{PRO} . The basis for these is a steady state energy budget of the hotplate's temperature-controlled down-viewing plate and a proprietary algorithm (R11 and Z18). The U_{PRO} are reported by a hotplate as one-minute running averages (Z18) and we recorded these at 1 Hz. Examples are the gray dots in Fig. 2. Additionally, we calculated and analyzed one-minute-averaged values of U_{PRO} and the corresponding standard deviations. Examples of these are the black circles and the short vertical line segments in Fig. 2.

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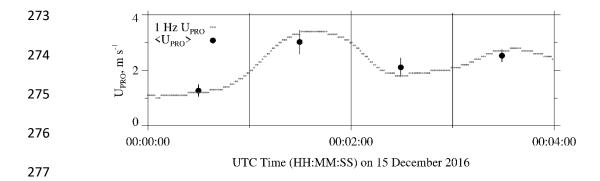


Figure 2 – Hotplate wind speed measurements (U_{PRO}) 00:00:00 to 00:04:00 on 15 December 2016. Gray dots are the one-minute running-average U_{PRO} recorded at 1 Hz. Black circles are the one-minute-averaged U_{PRO} (\pm 1 standard deviation).

3 - Analysis

3.1 - WKA Overflight Time

The focus of our analysis is the two WKA flight segments shown in Figs. 3a-b. The maps shown in the figures have the three ground sites (AF, SN, and HP) and the WKA flight tracks (white line). The beginning-to-end time interval for the flight tracks is 100 s and these are divided into ten 10-second intervals. The 10 s intervals are indicated with white diamonds. Except for the turn evident in Fig. 3b, the flight tracks are straight, and the track direction is approximately upwind to downwind.

Times that the WKA was closest to the HP site were evaluated by finding the point on the flight track where the horizontal position of the WKA was closest to the hotplate's coordinates. These times are symbolized t_0 and are referred to as overflight times. In Figs. 3a-b the downwind end of the flight tracks end at the overflight time. The latitude/longitude position of the aircraft was within 390 m of the hotplate at the overflight times. Table 21 has the overflight times on the two flight days.

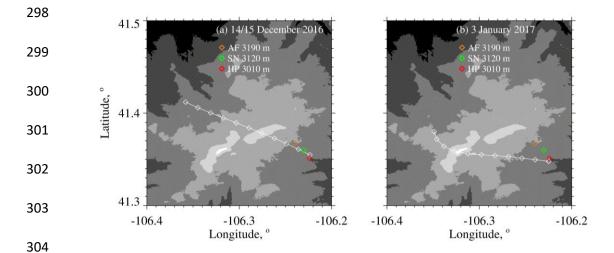


Figure 3 – (a) WKA flight track on 14/15 December 2016 for time interval = overflight time - 100 s to the overflight time. (b) WKA flight track on 3 January 2017 for time interval = overflight time - 100 s to the overflight time. The white diamonds on the tracks are separated, in time, by 10 s. Altitude thresholds for the digital elevation maps are 2600, 2800, 3000, 3200, 3400, and 3600 meters. Altitudes of the ground sites are in the legend.

3.2 – Effect of Attenuation on WCR Reflectivities

The presence of molecular oxygen, water vapor, cloud water, and snow particles within the WCR's transmission path will contribute to an attenuation of microwave intensity and will therefore negatively bias the retrieved reflectivities (Matrosov 2007; Hiley et al. 2011; Kneifel et al. 2015). Models of attenuation, radar remote sensing, and in situ measurements were used to calculate this bias. For oxygen, an attenuation coefficient from Ulaby et al. (1981; their Fig. 5.6), and temperature (T) and pressure (P) measurements from the AF (Table 32), were used. For vapor, an attenuation coefficient (Ulaby et al. 1981; their Eq. 5.22), and T, P, and relative humidity (RH) measurements from the AF (Table 32), were used. Concentrations of oxygen and water vapor and the oxygen and vapor path lengths are provided in Table 43. The latter is the vertical distance between the HP and the WKA. It was assumed that concentrations were uniform over this path length.

Attenuation by cloud water was derived using the WKA-measured T (Table 32), the WKA-measured LWC, path length (Table 43), and an attenuation formula (Liebe et al. 1989; Vali and Haimov 2001). The LWC applied in the formula is the maximum of CDP measurements acquired between t_0 - 10 s and t_0 . This interval coincides with the interval the WCR's down-looking antenna was used to acquire reflectivities over the HP (Sect. 3.5). The path length for cloud water was derived as the vertical distance between cloud base [derived thermodynamically using AF measurements (Table 32)] and flight level. LWC was assumed uniform, at the maximum value, over the path length.

Snow particle mass concentration is typically reported as an ice water content (IWC, g m⁻³) (Liu and Illingworth 2000). The contribution of IWC to attenuation was calculated using

measurements in Nemarich et. al (1988), who reported an attenuation coefficient equal to 0.9 dB/km per unit of IWC. Also used were retrievals of IWC acquired using the down-pointing WCR antenna. There are several steps in the calculation. First, all profiles of dBZ acquired between t_0 - 10 s and t_0 were selected. Second, a maximum dBZ was selected at each of the down-beam range gates (Table 2±). Third, the dBZ maxima were increased by the overall two-way attenuation in the final column of Table 43. Fourth, the profile of attenuation-corrected dBZ was converted to a profile of attenuation-corrected Z. Fifth, a Z-to-IWC parameterization was applied (IWC = 0.10·Z^{0.51}; PV11; their Table 3). Sixth, the IWC profile was integrated, and the derived ice water path was divided by the snow particle path length (Table 43). This calculation produced a time- and range-averaged maximum IWC (Table 43). This IWC is the value applied in the attenuation calculation.

Two-way attenuations (ΔdB), summed over contributions from the four components, are presented in the final column of Table 43. Attenuation by snow and attenuation by liquid were the most important components (> 50 %) on December 15 and January 3, respectively. Vapor contributed 32 % to the overall on December 15, and the combination of vapor and snow contributed 45 % on January 3. Equation 1 shows how an attenuation-corrected reflectivity (Z') was derived using an uncorrected reflectivity (Z) and the ΔdB .

 $Z' = 10^{\left[\left[10 \cdot \log_{10}(Z) + \Delta dB\right]/10\right]}$ (1)

Table 32 – Atmospheric state averages

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Date	WKA ^a Track Altitude, m	WKA ^a T, °C	AF ^b T, °C	AF ^b RH, %	WKA ^{a, c} Track Vector	WKA ^{a, c} Wind Vector	AF b, c Wind Vector
14/15 December 2016	4546	-13.9	-6.3	86	310 / 130	274 / 32	250 / 8.5
3 January 2017	4196	-21.7	-14.6	77	280 / 120	265 / 27	260 / 5.4

^a Altitude, temperature, track vector, and horizontal wind vector data obtained by averaging 1 Hz WKA measurements. The averaging interval is 60 s and the interval starts at the overflight time, minus 60 s, and ends at the overflight time.

b Temperature (T), relative humidity (RH), and horizontal wind vector data from sensors on the US-GLE AmeriFlux tower (Sect. 2.1). The wind sensor was deployed at 26 m AGL (3223 m MSL) and the T/RH sensor was deployed at 23 m AGL (3220 m MSL). The AF measurements correspond to 30-minute averages closest to the overpass time. In the AF data set, time stamps on the relevant AF recordings are 00:00 UTC (15 December 2016) and 20:30 UTC (3 January 2017).

^c Vectors are presented in the following format: Direction of motion (degree relative to true north) / speed (m s⁻¹).

Table $\frac{43}{2}$ – Attenuating component concentration, one-way pathlength, and the overall two-way attenuation

Date	Conc.	Conc.	Maximum	Maximum	One-way	One-way	Overall
	Oxygen,	Vapor,	LWC,	IWC,	Pathlength ^a	Pathlength ^b	Two-way
	kg m ⁻³	kg m ⁻³	g m ⁻³	g m ⁻³	Oxygen, Vapor,	Cloud Water,	Attenuation,
					and Snow,	km	ΔdB
					km		
15 December 2016	0.21	2.7x10 ⁻³	0.01	0.27	1.54	1.09	1.41 ^c
3 January 2017	0.21	$1.3x10^{-3}$	0.08	0.09	1.19	0.59	1.01 ^d

^a Vertical distance between HP and WKA

^b Vertical distance between cloud base [derived thermodynamically using AF measurements (Table 32)] and WKA

^c One-way attenuation coefficients are 0.03 dB/km for oxygen (Ulaby et al. 1981), 0.14 dB/km for vapor (Ulaby et al. 1981), 0.056 dB/km for cloud water (Liebe et al. 1989; Vali and Haimov 2001), and 0.24 dB/km for snow particles (Nemarich et. al 1988).

^d One-way attenuation coefficients are 0.03 dB/km for oxygen (Ulaby et al. 1981), 0.073 dB/km for vapor (Ulaby et al. 1981), 0.49 dB/km for cloud water (Liebe et al. 1989; Vali and Haimov 2001), and 0.077 dB/km for snow particles (Nemarich et. al 1988).

3.3 - Correction of Doppler Velocity

We accounted for bias in V_D (Sect. 2.3) due to deviation of the down-looking WCR antenna from vertical. This was done by applying the correction described in Zaremba et al. (2022) (their Eq. A4). The west-to-east and south-to-north particle velocities used in the correction were assumed to be equal to component wind velocities. The latter were expressed as linear functions of altitude using the information in the penultimate and last columns of Table 32. The component velocities as functions of altitude and the linear equations relating velocity and altitude are provided in the Appendix.

3.4 - Hotplate Measurement of Wind Speed

Here we compare the hotplate-derived wind speed to wind speed derived using an R.M.Young rotating anemometer (R.M.Young 2001). The second of these is symbolized U_{RMY} and the basis for the first (U_{PRO}) is a proprietary algorithm (Sect. 2.4). We are doing this comparison because B14 showed that U_{PRO} can be high-biased, relative to a conventional anemometer, and because U_{PRO} is the primary determinant of the rate that the up-viewing plate dissipates sensible heat energy. Diagnosis of that heat transfer rate is our basis for calculating the liquid-equivalent snowfall rate (Z18). The U_{PRO} also determines the snow particle catch efficiency and the latter was used in calculations of the undercatch-corrected liquid-equivalent snowfall rate (Sect. 2.4).

The comparisons reported here were done at the Laramie, WY Airport in December 2019, and in January 2020. Compared to the HP site, the Laramie Airport site (indicated LA in Fig. 1) is free of obstruction, out to 120 m, and experiences larger wind speeds. By mounting the hotplate and the R.M.Young anemometer on rigid metal pipes, the hotplate's heated horizontal

surfaces (the up- and down-viewing plates seen in Fig. 1 of Z18) and the anemometer's spinning axis (oriented horizontally) were both positioned at 2 m AGL. The pipes were separated horizontally by 5 m. There was no precipitation on the days selected for the wind speed comparisons. The values of U_{PRO} and U_{RMY} we analyzed were recorded with a data system that time stamped the 1 Hz U_{PRO} and 1 Hz U_{RMY} with a relative timing accuracy no worse than 1 s.

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A wind speed comparison - from 13 December 2019 - is shown in Fig. 4a. U_{PRO} was brought into the comparison by sampling it once per minute from files containing 1 Hz recordings of the one-minute running-average U_{PRO} (Sect. 2.4). U_{RMY} was brought into the comparison by starting with files containing 1 Hz recordings and converting these to one-minute averages. Fig. 4a shows no evidence of bias and Fig. 4b demonstrates that the average absolute departure between the U_{PRO} and U_{RMY} (both one-minute averages) is no larger than 10.5 m s⁻¹. Table 54 has eight more precipitation-free comparisons. Included in the table are temperature and wind speed averaged over the comparison intervals (4 to 20 UTC), the slope of the linearleast-squares fit line (forced through the origin, red line), and the lower and upper quartiles of the slope. The quartiles were calculated using the method of Wolfe and Snider (2012). In contrast to Figs. 4a-b, Figs. 4c-d make the comparison using 1 Hz values of U_{PRO} and U_{RMY}. The larger scatter and larger average absolute departure seen in these panels is a consequence of the hotplate's limited time response, compared to the R.M. Young. We quantify the hotplate's response time in terms of a calculated thermal response time. During wintertime at the Laramie Airport, and with wind speed at 5 m s⁻¹, the down-viewing plate's thermal response time is approximately 60 s (results not shown). Because the temperature of the down-viewing plate is actively controlled, this does not translate to a 60 s lag between changes in wind speed and the hotplate response. The U_{PRO}/U_{RMY} departure is most evident at $U_{PRO} > 5$ m s⁻¹ (Fig. 4d) but this is

- not a concern for U_{PRO} on 14/15 December 2016 or on 3 January 2017. Snider (2023)
- demonstrated that the U_{PRO} was less than 5 m s⁻¹ at the hotplate during the two WKA overflights.

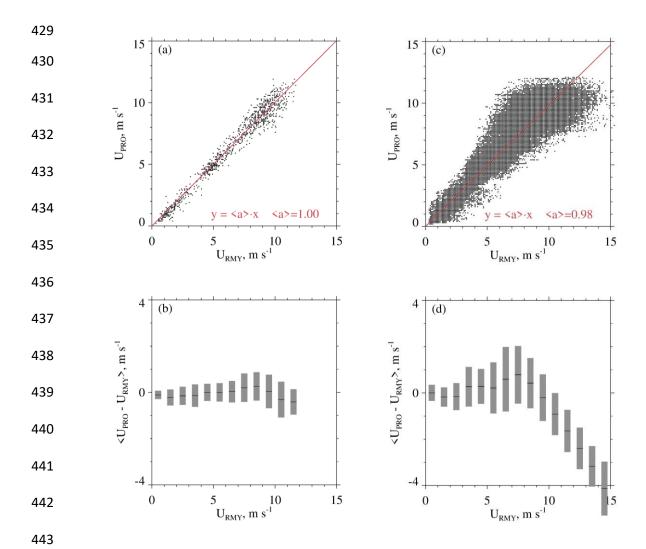


Figure 4 – (a) Scatterplot of one-minute-averaged U_{PRO} and one-minute-averaged U_{RMY} . Measurements were acquired at the Laramie, WY Airport 13 December 2019. The red line is a linear-least-squares fit line (forced through the origin). (b) Average departure between one-minute-averaged U_{PRO} and one-minute-averaged U_{RMY} . Average departures were calculated for discrete U_{RMY} intervals, and the averages are indicated with short black horizontal lines. Gray bars indicate \pm 1 standard deviation. (c) Same as in (a) except for 1 Hz values of U_{PRO} and U_{RMY} . (d) Same as in (b) except for 1 Hz values of U_{PRO} and U_{RMY} .

Table 54 - UPRO versus URMY correlations

Date,	$<$ T> 2 ,	$< U > ^{2}$,	< a > 3	a ⁴	a ⁴
UTC ¹	°C	m s ⁻¹		First	Third
				Quartile	Quartile
7 December 2019	-0.40	5.40	1.00	0.90	1.04
8 December 2019	2.70	4.10	0.99	0.90	1.04
10 December 2019	-5.20	3.80	0.99	0.83	1.04
13 December 2019	-1.50	6.60	1.00	0.93	1.06
18 December 2019	-6.20	3.60	0.99	0.92	1.04
19 December 2019	-6.90	2.70	0.95	0.84	0.99
6 January 2020	-6.40	8.80	1.01	0.96	1.06
8 January 2020	0.30	4.20	1.00	0.87	1.05
11 January 2020	-7.20	7.00	1.02	0.97	1.08

 1 Statistics presented are based on one-minute-averaged U_{PRO} and one-minute-averaged U_{RMY} measurements made between 04:00 to 20:00 UTC.

 $^{\rm 2}$ Interval-averaged temperature and interval-averaged wind speed.

 3 Slope of the one-minute-averaged U_{PRO} versus one-minute-averaged U_{RMY} linear-least-squares fit line, forced through the origin.

⁴ Quartiles of the slope (see text)

3.5 – Combined Aircraft and Surface Measurements

Figure 5 has WCR and WKA measurements starting 100 s prior to t_0 and ending at t_0 . The sequences in Figs. 5a and 5c are reflectivities from both the up- and down-looking antennas. In Fig. 5a the flight track (black dashed horizontal line) is at 4550 m and in Fig. 5c the flight track is at 4200 m. At the t_0 in Fig. 5a, below the WKA, the maximum radar echo is +6 dBZ (Z = $4 \text{ mm}^6 \text{ m}^{-3}$) and in Fig. 5c the maximum is -3 dBZ (Z = 0.5 mm⁶ m⁻³). Supercooled liquid water was detected as the aircraft approached the ridgeline (Fig. 5b) and during the last 10 seconds of the time sequence in Fig. 5d. During these encounters with supercooled liquid, the maximum LWC values were 0.03×10^{-3} and 0.08×10^{-3} kg m⁻³ on 14 December 2016 and 3 January 2017, respectively. Values of N (Sect. 2.2) at times of maximal LWC were $3x10^6$ and $100x10^6$ m⁻³ on 14 December 2016 and 3 January 2017, respectively. Even on 3 January 2017, the <D> (Sect. 2.2) associated with maximum LWC was sufficient for hexagonal plate crystals with diameter larger than 100 µm to collide with the observed droplets with efficiencies > 0.1 (Wang and Ji 2000). We temporally and spatially averaged the values of Z we compared with time-averaged values of S. There are two reasons for this: 1) As discussed in Sect. 3.1, the WCR did not sample

We temporally and spatially averaged the values of Z we compared with time-averaged values of S. There are two reasons for this: 1) As discussed in Sect. 3.1, the WCR did not sample Z exactly over the hotplate, and furthermore, the width of radar beam at 1500 m range - roughly the distance between the aircraft and the ground at the overflight times - is 30 m and thus considerably smaller than the minimum horizontal distance between the aircraft and the HP. 2) Compared to the WCR, the hotplate is a relatively slow-response measurement system whose output is commonly averaged over one-minute intervals (Z18).

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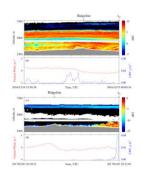


 Figure 5—(a) 100 s of WCR reflectivity and (b) 100 s of LWC and gust probe vertical wind velocity ending at t_0 on 14/15 December 2016. (c) 100 s of WCR reflectivity and (d) 100 s of LWC and gust probe vertical wind velocity ending at t_0 on 3 January 2017. In (a) and (c), above and below the flight track, is the roughly 200-m-deep WCR blind zone, reflectivity above (below) the flight track is from the up-looking (down-looking) WCR antenna, black indicates dBZ values smaller than minimum indicated in the color bar, white immediately above the terrain indicates echo that was discarded because of ground clutter, and white above the ground clutter and outside of the blind zone indicate dBZ < minimum detectable signal.

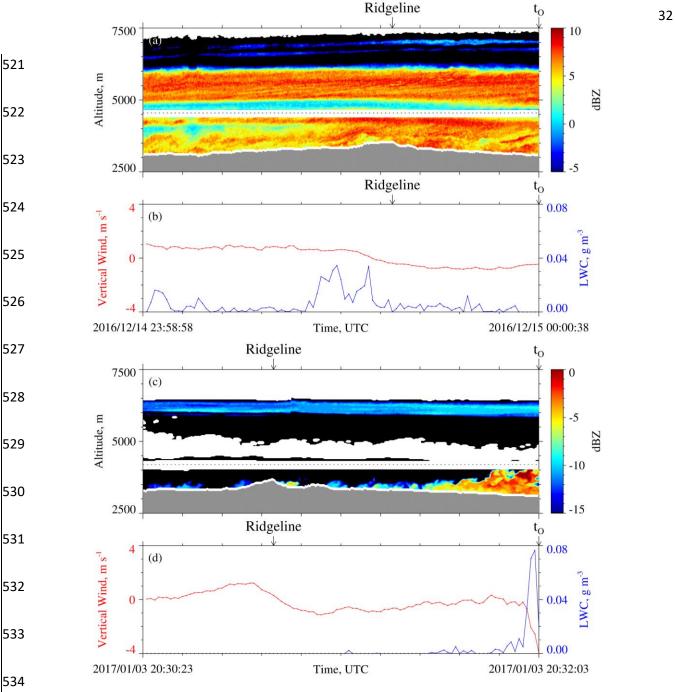


Figure 5 – (a) 100 s of WCR reflectivity and (b) 100 s of LWC and gust probe vertical wind velocity ending at t_0 on 14/15 December 2016. (c) 100 s of WCR reflectivity and (d) 100 s of LWC and gust probe vertical wind velocity ending at t_0 on 3 January 2017. In (a) and (c), above and below the flight track, the roughly 200-m-deep WCR blind zone is evident, reflectivity above (below) the flight track is from the up-looking (down-looking) WCR antenna,

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40	black indicates dBZ values smaller than the minimum indicated in the color bar, white
541	immediately above the terrain indicates echo that was discarded because of ground clutter, and
642	white above the ground clutter and outside of the blind zone indicate dBZ < minimum detectable
543	signal.

In our analysis, the HP measurements were averaged over two adjacent 60 s intervals. The first extends from t_0 to $t_0 + 60$ s (Fig. 6a) and the second from $t_0 + 60$ s to $t_0 + 120$ s (Fig. 6c). In Fig. 6a and in Fig. 6c, $t_{HP,B}$ symbolizes an interval's beginning time and $t_{HP,E}$ symbolizes an interval's ending time. Formulas describing how these times were related to the beginning and ending time of a corresponding WCR averaging interval are in the Appendix. Fig. 6b is a schematic of the first WCR averaging interval and Fig. 6d is a schematic of the second. Again, the subscripts "B" and "E" are used to indicate averaging beginning and ending times. Figures 6b and 6d both have lines at the top of an averaging interval/domain. The slopes of these lines are proportional to the ratio of two speeds. These speeds are a maximum likely snow particle speed toward the ground (v_p) and a horizontal wind advection speed (v_w) . The v_p was calculated using averaged vertical-component Doppler velocities and v_w was calculated using a vertical profile of horizontal winds, based on WKA horizontal wind measurements and AF horizontal wind measurements (Figs. A1a-b), and using the WKA track vector (Table $\underline{32}$). An altitude ($z' \neq z'$ = 3400 m) was assumed in the calculation of v_w . This is the altitude of the ridges west and northwest of the HP site (Figs. 3a-b). Picking the altitude to be either $z' \neq 3200$ m or $z' \neq 3200$ m or 3600 m does not alter our findings.

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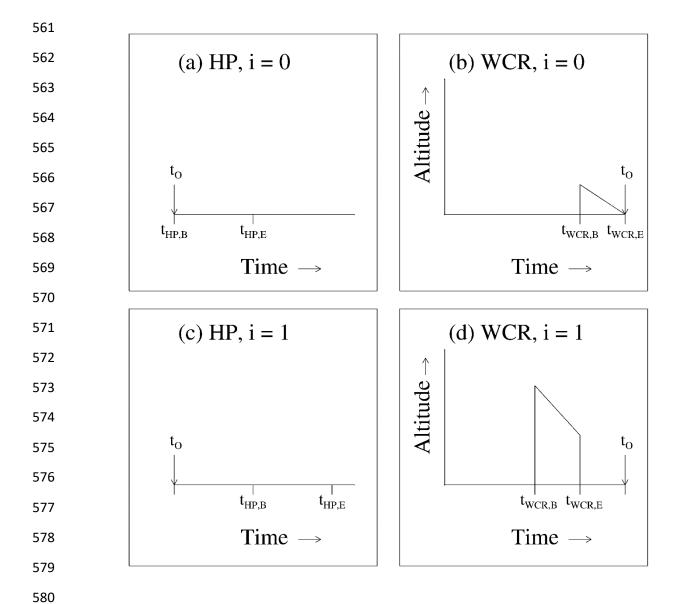


Figure 6 – (a and c) Representations of the i=0 and i=1 HP averaging intervals. (b and d) Representations of the i=0 and i=1 WCR averaging intervals/domains. The t_0 _is shown in all panels. The subscripts "B" and "E" indicate beginning and ending times of the HP averaging (panels a and c) and the beginning and ending times of the WCR averaging (panels b and d).

All panels in Fig. 6 are labeled with an index designating either the first averaging interval (i = 0) or the second averaging interval (i = 1). Figures 7 and 8 present hotplate snowfall measurements from 14/15 December 2016 and 3 January 2017. In these, and in subsequent figures, colored circles surround the $\underline{i = 0}$ and $\underline{i = 1}$ indexes, blue is used to colorcode 15 December 2016, and red is used to color-code 3 January 2017. Additionally, Fig. 8 has an i = 2 averaging interval. This is a special case discussed at the end of this section.

Figures 9a-b and Figs. 10a-b have enlarged views of the altitude-time WCR crossections recorded on the two flight days. Different from Fig. 5a and Fig. 5c, these measurements are only from the WCR's down-looking antenna. Additional differences are the following: 1) The plots are set up so that Z and $\frac{V_D}{V_D}$ structures downwind of the hotplate can be seen. These structures are discussed in the following section. 2) The WCR measurements are shown for 50 s of flight. With the WKA ground speed approximately 125 m s⁻¹ (Table 32), the distance along the abscissa is 6250 m. 3) Colored circles that surround the $\frac{i=0}{2}$ -indexes are placed below the WCR averaging intervals/domains. The latter are drawn with solid black lines and are seen to overlay both the Z and $\frac{V_D}{V_D}$ altitude-time crossections. Consistent with Figs. 6b and 6d, and the Appendix, one of these black lines is vertical and another the other is negatively sloped. Figs. 10a-b also have the $\frac{i=2}{2}$ intervals/domains discussed at the end of this section.

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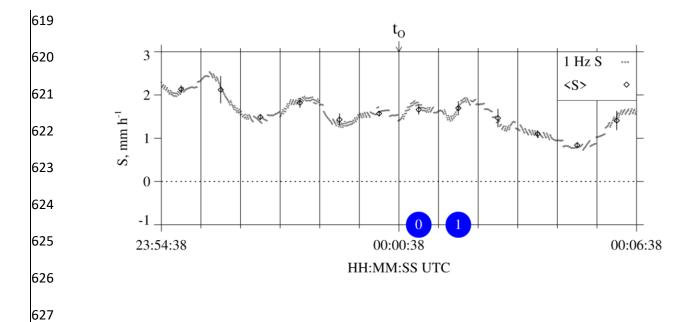
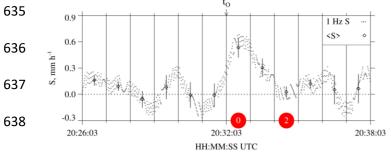


Figure 7 – Twelve minutes of HP snowfall measurements from 14/15 December 2016. Gray dots are S values calculated using hotplate output recorded at 1 Hz. Black diamonds are the one-minute-averaged values (\pm 1 standard deviation). The t_0 is shown above the panel and the blue circles designates the i=0 and i=1 HP averaging intervals.

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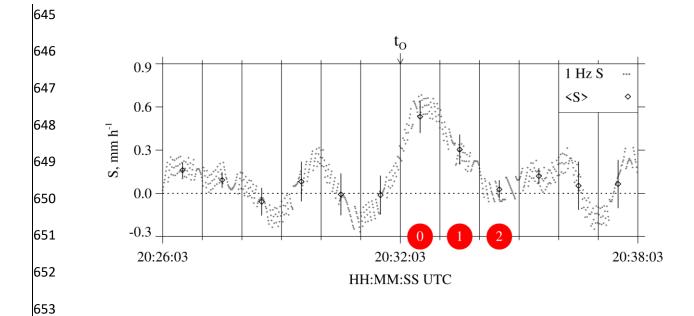


Figure 8 – Twelve minutes of HP snowfall measurements from 3 January 2017. Gray dots are S values calculated using hotplate output recorded at 1 Hz. Black diamonds are the one-minute-averaged values (\pm 1 standard deviation). The t_0 _is shown above the panel_and_, a-red circles designates the i=0__i=1_, and i=2_HP averaging intervals, and a red circle designates the i=2_HP averaging interval. The i=2_intervallatter is a special case discussed at the end of Sect. 3.5.

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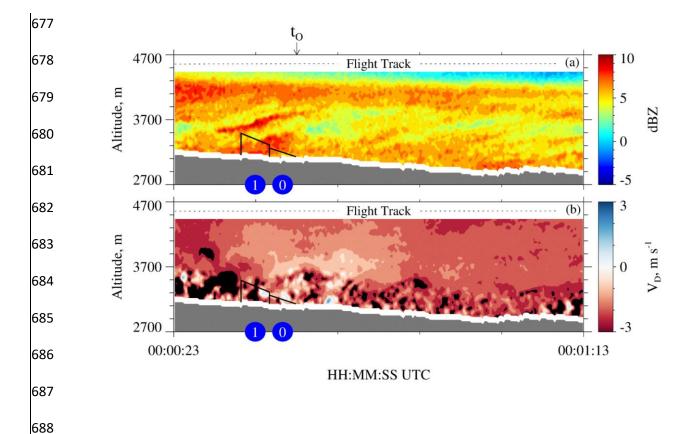


Figure 9 – 50 s of measurements from the down-looking WCR antenna on 15 December 2016. (a) Crossection of reflectivity t_0 – 15 s to t_0 + 35 s. (b) Crossection of Doppler velocity t_0 – 15 s to t_0 + 35 s. The t_0 is shown above the top panel. In both panels, the solid black lines (vertical and sloped) encompass the i = 0 and i = 1 WCR averaging intervals/domains and blue circles designate the the i = 0-WCR averaging intervals.

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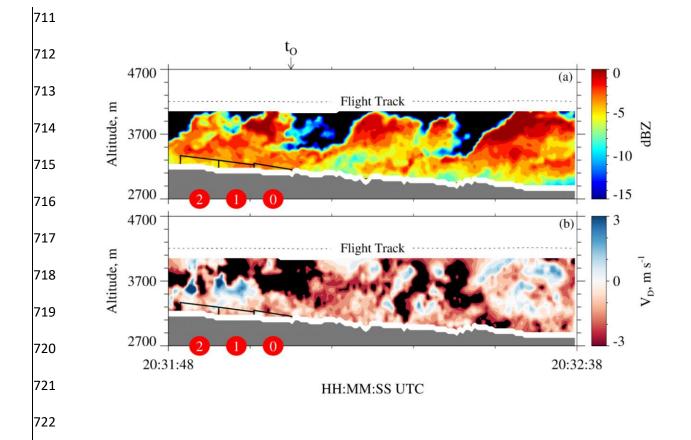


Figure 10-50 s of measurements from the down-looking WCR antenna on 3 January 2017. (a) Crossection of reflectivity t_0 - 15 s to t_0 + 35 s. (b) Crossection of Doppler velocity t_0 - 15 s to t_0 + 35 s. The t_0 is shown above the top panel. In both panels, the solid black lines (vertical and sloped) encompass the i=0, i=1, and and i=2 WCR averaging intervals/domains and, two red circles designate the i=0, i=1, and i=2 interval interval. The i=2 interval interval is domain in i=2 intervals/domain is i=2 intervals/domains are a special case discussed at the end of Sect. 3.5.

The i=0 and $\underline{i=1}$ averages of S and Z are presented in Table 65 and the corresponding averaging intervals are viewable in Fig. 7 and Fig. 9a (15 December 2016) and in Fig. 8 and Fig. 10a (3 January 2017). The i=1 averages are also presented in Table 5. According to the averaging scheme (Fig. 6), the i=1 HP averaging interval is time-shifted positively compared to the i=0 HP averaging interval and the i=1 WCR averaging interval is time-shifted negatively compared of the i=0 WCR averaging interval. This arrangement of the averaging intervals is one way to average while also accounting for wind advection of the snow particles.

As discussed earlier in this section, the averaging scheme initializes with 60-second blocks of HP data between $\underline{t_o}^{t_0}$ -and $\underline{t_o}^{t_0}$ -and $\underline{t_o}^{t_0}$ -120 s. When we applied the scheme to data from 3 January 2017, but outside the specified time range, an inconsistency was documented. This is apparent in Fig. 8, where the $\underline{t_o}^{t_0}$ +120 s to $\underline{t_o}^{t_0}$ +180 s interval (i.e., the $\underline{i=2}^{t=2}$ interval) has negligible average S, while in Fig. 10, the $\underline{i=2}^{t=2}$ interval has a non-negligible average Z (~0.3 mm⁶ m⁻³). A firm explanation is not available for the inconsistency, but a factor may be the convective nature of the fields in Figs. 10a-b. Because of the inconsistency, only averages corresponding to the $\underline{i=0}^{t=0}$ and $\underline{i=1}^{t=1}$ intervals are were analyzed further.

Table 6 – Average wind measurements, average hotplate measurements, average WCR measurements, and attenuation-corrected

749 reflectivities

<u>Date</u>	$\frac{v_w \frac{a}{2}}{m s^{-1}}$	<u>i index</u>	$\frac{S_{HP} \pm \sigma^{b}}{mm h^{-1}},$	WCR Samples ^c	$\frac{\langle V_D \rangle^d}{\underline{m} \ \underline{s}^{-1}}$	$\frac{\sigma_{V_D} \stackrel{\text{e}}{\vec{\cdot}}}{\underline{\text{m s}}^{-1}}$	$\frac{v_p \cdot \frac{f}{r}}{m \cdot s^{-1}}$	$\frac{\langle Z \rangle \pm \sigma_Z^g,}{mm^6 m^{-3}}$	$\frac{\underline{Z'}_{\underline{h}}}{\underline{m}\underline{m}^{6}}\underline{m}^{-3}$
<u>15 December 2016</u>	<u>7.4</u>	0	1.7±0.1	<u>42</u>	<u>-1.3</u>	0.9	2.2	4.9±2.1	<u>6.8</u>
<u>15 December 2016</u>	<u>7.4</u>	<u>1</u>	1.7±0.2	<u>149</u>	<u>-1.8</u>	1.2	3.0	5.6±1.1	<u>7.8</u>
3 January 2017	8.9	0	0.5±0.1	<u>22</u>	<u>-0.9</u>	0.8	1.7	0.49 ± 0.05	0.62
3 January 2017	8.9	<u>1</u>	0.3±0.1	<u>35</u>	<u>-0.8</u>	0.4	1.2	0.50±0.10	0.63

- 751 a Horizontal wind advection speed (Eq. A7) calculated using values from the penultimate and last columns of Table 3.
- 752 b One-minute average of the undercatch-corrected liquid-equivalent snowfall rate (± 1 standard deviation). An example averaging
- 753 <u>interval is the</u> i = 0 <u>interval in Fig. 7.</u>
- 754 $^{\circ}$ Number of samples used to calculate the WCR statistics. The averaging intervals/domains (e.g., i = 0 in Figs. 9a-b and in Figs. 10a-
- b) encompass the WCR samples which are the basis for the WCR statistics presented in this table.
- 756 d Average of Doppler velocity within the averaging intervals/domains.
- 757 Standard deviation of Doppler velocity within the averaging intervals/domains.
- 758 Maximum likely snow particle speed toward the ground (Eq. A8).
- 759 g Average reflectivity (± 1 standard deviation). These values are not corrected for attenuation.

h Attenuation-corrected reflectivities. These were derived using reflectivities from the penultimate column of this table, attenuations

761 <u>from Table 4, and Eq. 1.</u>

Table 5 Averaged wind, hotplate, and WCR measurements

Date	$\frac{V_w^{\text{a}}}{7}$, $\frac{\text{m s}^{-1}}{1}$	i index	<s>±σ_S-^b, mm h⁻¹</s>	WCR Samples-e	$ \begin{array}{c} \checkmark V_{D} > \stackrel{d}{\rightarrow}; \\ m s^{-1} \end{array} $	$\sigma_{V_D}^{\text{e}}$;	$\frac{\mathcal{V}_p^f}{m s^{-1}}$	< <u>Z>±σ</u> _Z - ^ε , mm ⁶ -m ⁻³
15 December 2016	7.4	0	1.7±0.1	42	-1.3	0.9	2.2	4.9 ± 2.1
15 December 2016	7.4	1	1.7±0.2	149	-1.8	1.2	3.0	5.6±1.1
3 January 2017	8.9	0	0.5±0.1	22	-0.9	0.8	1.7	0.49 ± 0.05
3 January 2017	8.9	1	0.3 ± 0.1	35	-0.8	0.4	1.2	0.50 ± 0.10

^a-Horizontal wind advection speed (Eq. A7) calculated using values from the penultimate and last

columns of Table 2.

^b One-minute average of the undereatch-corrected liquid-equivalent snowfall rate (± 1 standard deviation). An example averaging interval is the interval in Fig. 7.

^e Number of samples used to calculate WCR statistics in the penultimate four columns. The averaging intervals/domains (e.g., i=0 in Figs. 9a b and in Figs. 10a b) encompass the averaged WCR samples.

776 d-Average of Doppler velocity within the averaging intervals/domains.

^e Standard deviation of Doppler velocity within the averaging intervals/domains.

780 ^f-Maximum likely snow particle speed toward the ground (Eq. A8).

^g Average reflectivity (± 1 standard deviation). These values are not corrected for attenuation.

3.6 - Snow Particle Imagery

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In Fig. 9a and Fig. 10a, the time for a snow particle to move the abscissa and ordinate distances is different. The ratio of these two times is 2.6. This follows from our choice of abscissa and ordinate ranges, from values of particle fall speed (1 m s⁻¹) and horizontal wind advection speed (8 m s⁻¹), which we assumed, and from the WKA ground speed ($gs \sim 125$ m s⁻¹; Table 32). The assumed values are approximately consistent with values of $\langle V_D \rangle$ and V_w , in Table 65, and with the V_D sign convention (Sect. 2.3). We also used $gs = 125 \text{ m s}^{-1}$ to scale (virtually) the time axes in Fig. 9a and Fig. 10a to a horizontal distance. Within the scaled coordinate frames, we assumed that all snow particle trajectories have negative slope ($\Delta z / \Delta x = 1 \text{ m s}^{-1} / 8 \text{ m s}^{-1} = -0.12$) and that all trajectories are stationary. However, both assumptions seem inconsistent with the reflectivity structures in Fig. 5a, where positively-sloped particle fall streaks are evident at ~ 5500 m, inconsistent with Fig. 9a where positively-sloped fall streaks are at ~ 3500 m, and inconsistent with the positively-sloped fall streaks in Fig. 10a. On both flight days, the fall streaks evince particle sources that move horizontally and with a horizontal speed that is larger than the $v_w = 8 \text{ m s}^{-1}$ applied in the estimate of the trajectory slope. It may be that the source's horizontal speed is comparable to the flight-level WKA-derived horizontal wind (27 to 32 m s⁻¹; Table 32) but we do not have data needed to verify that assertion. Based on the assumption that snow particles followed the fall streaks while both were advecting horizontally, we looked downwind of the hotplate - at a time later than t_0 in Fig. 9a and Fig. 10a - for particles that became those that produced snowfall at the hotplate.

Particle images from 15 December 2016 were analyzed using the 2DP. With this instrument the maximum all-in particle size (in the horizontal direction perpendicular to flight) is

6400 μm and the particle size resolution is 200 μm (Sect. 2.2). Within the time interval picked for this analysis (discussed below), particles sizing in the smaller of the two spectral modes, with mode size ~ 400 μm, were more numerous (results not shown). Because the 400 μm particles are poorly resolved by the 2DP, and the same can be said for somewhat larger particles, those smaller than 1000 μm were excluded from the following analysis. Figure 11a shows imagery from 12 s of measurements acquired near the end of the sequence in Fig. 9a (00:01:02 to 00:01:14). This time interval was selected by tracing forward from t_0 , along the slope of the fall streaks, to the flight level. Many of the particles are rounded (indicating riming) and a few have arms likely due to incomplete conversion of branched crystals to rimed snow particles. The mode size corresponding to these images is 1600 μm. No liquid water was detected with these particles (LWC < 0.01×10^{-3} kg m⁻³; Fuller 2020; her Fig. 8), but liquid was detected, at ~ 00:00:00, as the aircraft approached the ridgeline (Figs. 5a-b).

Turning to imagery from 3 January 2017, the most appropriate location for analysis would be through the second billow structure evident in Fig. 10a (i.e., very close to the middle of the Fig. 10a sequence). This billow sourced a fall streak that terminated at the hotplate (i.e., at the time t_0 indicated in the figure). However, the aircraft only clipped the top of this billow, and it was only when sampling the billow seen ~ 13 s earlier that larger ice particle concentrations ($\sim 20,000 \text{ m}^{-3}$) (Fuller 2020; her Fig. 10) and larger LWC ($\sim 0.08 \times 10^{-3} \text{ kg m}^{-3}$; Fig. 5d) were detected. Maximum reflectivities were the same in all three billows ($Z \sim 1 \text{ mm}^6 \text{ m}^{-3}$; 0 dBZ), so it was assumed that imagery collected in the first billow (20:32:00 to 20:32:02) was representative of what was falling toward the hotplate. The 2DS was used to image these particles (Fig. 11b); with this instrument the maximum all-in particle size (in the horizontal direction perpendicular to flight) is 1280 µm and the size resolution is 10 µm (Sect. 2.2). Most of the objects in Fig. 11b

appear to be rimed and their mode size is $\sim 400~\mu m$. It is also noted that particles smaller than $100~\mu m$ were eliminated from these images, however, compared to the $\sim 400~\mu m$ particles those smaller than $100~\mu m$ were significantly less abundant (results not shown).

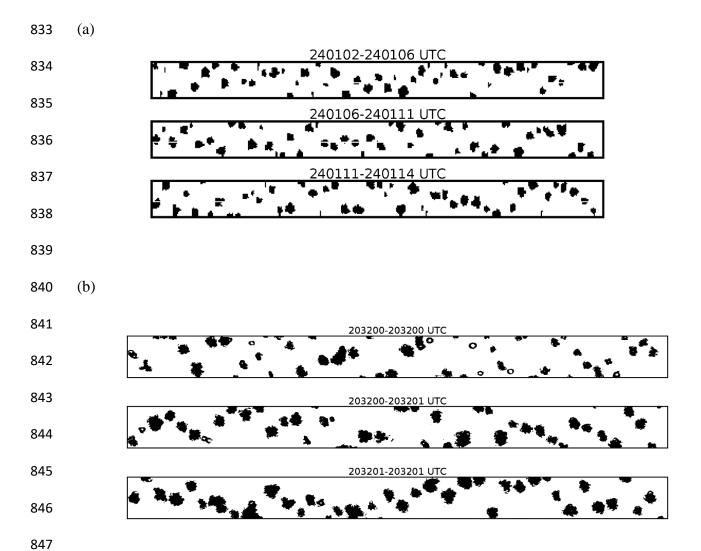


Figure 11 - (a) 2DP particle imagery from 15 December 2016. The height of the strips is 6400 μ m. These particles are estimated to be representative of those that fell from flight level toward the hotplate. (b) 2DS particle imagery from 3 January 2017. The height of the strips is 1280 μ m. These particles are estimated to be representative of those that fell from flight level toward the hotplate.

3.7 – S/Z Relationships

Our S/Z pairs are presented in Table 65 where the indexes (i = 0 and i = 1) are used to indicate results derived for the averaging intervals. In the penultimate column of Table 6, reflectivities are not corrected for attenuation, however, in the last column of Table 6 and in Fig. 12, the attenuation-corrected reflectivities are presented. In Table 5, reflectivities are not corrected for attenuation, however, in Fig. 12a, attenuation corrected reflectivities are plotted. Reflectivities from the penultimate column of Table 65, attenuations from Table 43, and Eq. 1 were used to calculate the corrected reflectivities. Also shown in Fig. 12 (black filled circles) is a subset of the S/Z pairs from PV11's Fig. 11 (0.01 < Z < 10 mm⁶ mm⁻³) and the PV11 best-fit line (black). Results from PV11 are specified as $S(\rho_1)/Z$ because those authors applied the lower of two density-size functions (ρ_1), and the lower of two fall speed-size functions, with airborne measurements, in calculations of snowfall rates (Sect. 1 and Table 1).

THIS FIGURE WAS REVISED IN REVISION3.

Figure 12—a) Snowfall rate versus radar reflectivity. Colored circles indicate attenuation-corrected reflectivities (Table 3, Table 5, and Eq. 1) for the i=0 and i=1-averaging intervals. Error bars on these points represent the precision of the Z measurement (Sect. 2.3) and the precision of the S measurement (Sect. 2.4). The $S(\rho_1)/Z$ -points are a subset from PV11's Fig. 11 $(0.01 < Z < 10 \text{ mm}^6 \text{ mm}^{-3})$. Also plotted is the PV11 best-fit line (black) (Sect. 1), the S/Z relationship from Matrosov (2007) (Sect. 1), the S/Z relationship abbreviated SSKB (Sect. 1), and the swath of S/Z relationships from Hiley et al. (2011) (Sect. 1). b) S/Z relationships from Falconi et al. (2018) (their Table 2) (Sect. 1), the Matrosov (2007) relationship, and the swath of S/Z relationships from Hiley et al. (2011) are shown.

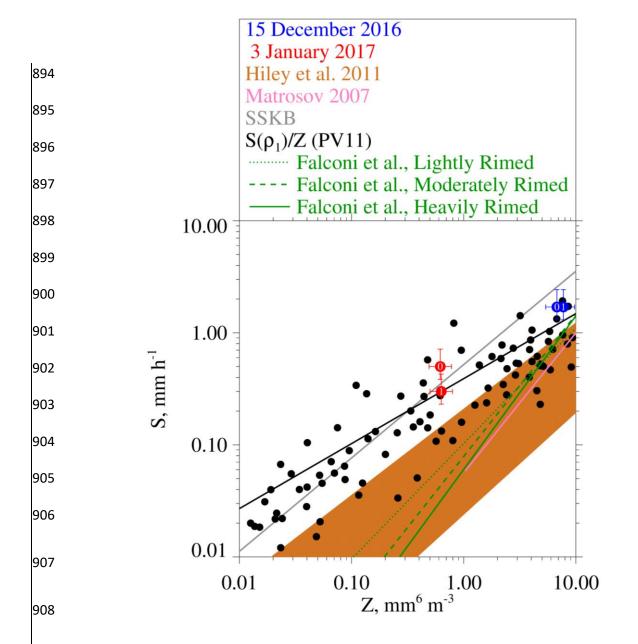


Figure 12 – Snowfall rate versus radar reflectivity. Red and blue circles are plotted at attenuation-corrected reflectivities (Table 6) for the $\underline{i} = 0$ and $\underline{i} = 1$ averaging intervals. Error bars on these points represent precisions of the reflectivity (Sect. 2.3) and snowfall rate (Sect. 2.4) measurements. Also plotted are the S/Z relationship lines from Sect. 1 and Table 1. These are the S/Z lines defining the swath of S/Z relationships from Hiley et al. (2011), the S/Z relationship from Matrosov (2007), the S/Z relationship abbreviated SSKB, PV11's best-fit line,

and the S/Z relationships from Falconi et al. (2018) (their Table 2). The $S(\rho_1)/Z$ points (black

916 <u>filled circles</u>) are a subset from PV11's Fig. 11 $(0.01 < Z < 10 \text{ mm}^6 \text{ mm}^{-3})$.

There are two potential biases in the values of snowfall rate we tabulate measured (Table 65) and plot (Fig. 12a). First, the two snowfall events had flight-level vertical wind velocities (Figs. 5b and 5d) that were positive (upward) upwind of the ridgeline summit, and vice versa downwind of the ridgeline summit. Except for the strongest downdraft on 3 January 2017, the magnitude of this variance is $\sim 1 \text{ m s}^{-1}$ (Figs. 5b and 5d). Assuming 1 m s⁻¹ was the downward wind immediately over the hotplate, the snow particles would have approached the HP gauge faster than their fall speed. Our basis for stating this is fall speeds for the mode sizes discussed in Sect. 3.6 (1600 and 400 µm) and our assumption that the particles were graupel. (Table 76 has these characteristic sizes and fall speeds.) However, the conjectured downdraft speed is likely an overestimate - because of divergence occurring as the draft approached the surface - and because the sizes in Table 76 likely underestimate what fell to the hotplate. Relevant to the last of these assertions, we used the altitude/T/RH measurements (Table 32) to calculate the vertical distance available for growth via riming, and thus for a fall speed increase, between the flight level and the lifted condensation level. Assuming an adiabatically-stratified liquid cloud and unit collection efficiency (these assumptions overestimate growth by riming), and no change of particle crossection (underestimates growth by riming), our calculations indicate that relative increases of size and fall speed were 40 and 20 %, respectively, on 3 January 2017, and that these relative increases were a factor-of-two larger on 15 December 2016.

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Table 76 – Estimates of snow particle fall speed

Date	Mode Size, um	Assumed Particle Type	Fall Speed, m s ⁻¹	Reference
15 December 201 <u>6</u> 5	1600	graupel	1.4	PV11; assuming ρ_1 in their Fig. 5
3 January 201 <u>7</u> 6	400	graupel	0.7	PV11; assuming ρ_1 in their Fig. 5

Second, there is concern that values of S from 3 January 2017 are underestimated.

Although values of S must be > 0, we presented 1 Hz values (gray points, Fig. 8) approaching - 0.3 mm h⁻¹. Negative values resulted because we did not impose a threshold of 0 mm h⁻¹ on the uncorrected snowfall rates (this thresholding is discussed in Z18) and because negative snowfall rate values (uncorrected for catch inefficiency) are amplified by the gauge-catch correction (Sect. 2.4). The implication is that 0.2 mm h⁻¹ could be added to the one-minute averaged values of snowfall rateS in Table 65 and in Fig. 12a. Here, the assumption is that an averaged S of -0.2 mm h⁻¹, in Fig. 8, is indicating indicates no snowfall at the hotplate; however, because the hotplate was operated autonomously (Sect. 2.1) we have no way to verify the assumption.

4 – Results

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Figure 12a shows ourthe four snowfall rate/reflectivity S/Z pairs (red and blue circles, our measurements) after the reflectivities were corrected for attenuation. The error bars on these data pairs represent the precision of the Z measurement (Sect. 2.3) and the precision of the S measurement (Sect. 2.4). Presentation clarity was what guided the selection of S and Z axis ranges in this figure but with the consequence that 32 of PV11's S/Z pairs are not shown because they plot at $Z > 10 \text{ mm}^6 \text{ m}^{-3}$. The way that the PV11 data pairs scatter closest to $Z = 10 \text{ mm}^6 \text{ m}^{-3}$, combined with the fact that the PV11 data pairs points at $Z > 10 \text{ mm}^6 \text{ m}^{-3}$ are not shown. could lead to the interpretation that the slope describing the best-fit relationship, at Z approximately > 2 mm⁶ m⁻³, -should be decreased relative to the actual slope of the PV11 best-fit line. Readers who view PV11's Fig. 11 will conclude that this interpretation is not warranted. The four S/Z pairs (red and blue circles) plot above the PV11 best-fit line but within the variability of PV11's S/Z pairs. As is discussed in Sect. 1, cComputation-based all W-band S/Z relationship have inputs from parameterized descriptions of density, shape, fall speed, PSD, and particle size (Sect. 1). The computation-based S/Z relationships are in the top three rows of Table 1; the subsequent two rows of Table 1 have S/Z relationships that resulted from a hybridization of measurements and calculations (PV11 and Falconi et al. 2018). Matrosov (2007) did calculations for the snow particle type known as aggregates. Hiley et al. (2011) did calculations for 20 snow particle types. Except for a S/Z calculation done for aggregate snowflakes, the calculations of Hiley et al. (2011) were for the particle type known as vapor-grown crystals. Hiley et al. (2011) did not

model spherical snow particles. The latter were modeled by Surussavadee and Staelin (2007) and

Kulie and Bennartz (2009). In Fig. 12a, the abbreviation SSKB is used to symbolize the computational S/Z relationship for spherical snow particles.

We now compare our snowfall rates (fourth column of Table 6) to snowfall rates where they plot on an S/Z relationship line evaluated at one of our attenuation-corrected reflectivities.

The departure between these is reported as a relative S difference expressed as |(S_{HP}-S)|/S where S_{HP} is from Table 6 and where S is on an S/Z relationship line. All possible comparisons are presented graphically in Fig. 12. Table 1 has both the minimum relative S differences and the salient maximum relative S differences. The comparisons will be discussed in the order of presentation in Table 1.

In comparisons of our snowfall rates and the upper-limit S/Z relationship line from Hiley et al. (2011) the relative difference is no smaller than 0.7 and 1.0 on 15 December and 3 January, respectively. These minimum relative differences exceed the hotplate precision (Sect. 2.4) by at least a factor of two. It is concluded that our paired values of undercatch-corrected precipitation rate and attenuation-corrected radar reflectivity provide evidence that a calculation of S based on the Hiley et al. (2011) upper-limit, when applied to rimed snow particles, is associated with a low-biased estimate of S. A retrieval based on Hiley et al.'s average S/Z relationship (not shown), which bisects the orange region in Fig. 12, corresponds to an even larger low bias. This is a concern because Hiley et al. (2011) used their average S/Z relationship to retrieve global snowfall distributions and since global observations reported in Wang et al. (2013) document the frequent occurrence of supercooled liquid within snowing clouds.

Figure: 12a shows the separation between our <u>measurements</u> S/Z pairs and the Matrosov (2007) calculation. The separation is about a factor of two <u>(minimum relative difference = 1.4)</u> for the points obtained on 15 December 2016 and corresponds to an underestimation of S (low bias) when compared to our measurements. The points <u>fromobtained on</u> 3 January 2017 plot at an <u>attenuation-corrected reflectivity</u> Z-smaller than the lower-limit of the calculation <u>(Matrosov 2007)</u>. Since the particle images (Fig. 11a-b) reveal no evidence <u>offor</u> the particle type modeled by Matrosov (2007) (aggregate <u>snowflakes</u>), it is not surprising that the <u>Matrosov S/Z</u> relationshipealculation is not representative of our measurements.

Departures between our S measurements (Fig. 12a) and S/Z calculations from Hiley et al. (2011) were evaluated as the vertical distance between the top of the orange region and our S/Z data pairs. Snowfall rates at the top of the orange region were calculated using attenuation-corrected reflectivities (Eq. 1 and Table 5) and using the upper limit S/Z equation from Hiley et al. (2011) (S=0.21 (Z')^{0.77}; Sect. 1 and Eq. 1). The departures were evaluated as a relative difference expressed as (S_{HP}-S)/S with S_{HP}-one of four snowfall rates from Table 5. The relative difference is no smaller than 0.7 and 1.0 on 15 December and 3 January, respectively. These minimum relative differences exceed the hotplate precision (Sect. 2.4) by at least a factor of two. It is concluded that our paired values of surface-measured precipitation rate and aircraft-measured radar reflectivity, after correcting for attenuation, provide evidence that a calculation of S based on the Hiley et al. (2011) upper limit, when applied to rimed snow particles, is associated with a low-biased estimate of S.

A plausible explanation One plausible reason for the low bias discussed in the previous two paragraphs is the smaller density implicit in most computationally-based S/Z relationships and especially those which assume that snow particles are crystals. Densities are quite different

for crystals versus that for rimed snow particles. For example, in Brown and Francis (1995), assuming a 2 mm crystal, the density is ~ 30 kg m⁻³, whereas in PV11 (their Eq. 1), assuming a 2 mm graupel particle, the density is ~ 200 kg m⁻³. Because aggregates are collections of crystals, this comparison of crystal and graupel densities also seems relevant to a comparison of graupel and aggregate snow particle densities.

Fig. 12a Figure 12 compares our S_{HP}/Z' data pairs to the SSKB S/Z relationship line developed using density = 200 kg m³ (Sect. 1). and Table 1 presents the relative differences between the data pairs and the SSKB line. also has the SSKB relationship. This was developed using density = 200 kg m³ (Sect. 1). Compared to the S/Z relationship represented by top of the orange region in Fig. 12, and compared to the Matrosov 2007 relationshipa, the SSKB line plots closer to our data points (minimum relative difference ~ 0.3). We note that the only instances of $S_{HP} < S$ are three of four comparisons of our measurements to the SSKB relationship. A possible reason for this is that the density applied in SSKB (Table 1) is not entirely representative of conditions during our study. An analysis of the sensitivity of the SSKB to a change in density is needed to investigate our assertion and closer to many of those reported by PV11.

Comparisons of our S_{HP}/Z' data pairs and PV11's best-fit line are also in Table 1. The table demonstrates that the agreement is reasonable - minimum relative difference no larger than 0.3 – and Fig. 12 shows that our data pairs plot at or above the PV11 best fit line.

Based on data from PV11 and our $\underline{S_{HP}/Z'}$ data pairs result, as well as the S/Z relationship abbreviated SSKB-(Sect. 1), it is expected that the S/Z relationships reported by Falconi et al. (2018) for rimed snow particles (Sect. 1) would plot higher in S-versus-Z space than is illustrated in Fig. 12b. Notably, only the upper-end of the Falconi et al. lines (i.e., at $Z > 8 \text{ mm}^6 \text{ m}^{-3}$) plot

above the upper_-limit that Hiley et al. (2011) <u>developedestablished</u> for unrimed snow particles. A plausible explanation for the lower-than-expected S/Z relationships of Falconi et al. is now offered. Falconi et al. used liquid water path as a proxy for the extent of snow particle riming (von Lerber et al. 2017). A consequence may have been that the proxy did not dependably exclude unrimed snow particles (crystals and aggregates) from the riming categories of Falconi et al. If this was the casetrue, then the data groupings that were the basis for the Falconi et al. S/Z relationships may have been affected. When applying the heavily-rimed S/Z relationship of Falconi et al. with our S_{HP}/Z' data pairs we find that the minimum relative differences are 0.6 (December 15) and 8.5 (January 3) (Table 1). Additionally, the differences are 0.5 (December 15) and 5.9 (January 3) when applying the moderately-rimed S/Z relationship of Falconi et al. (results not shown). Further research is needed to resolve the reason for the mismatch between S/Z pairs, the snowfall rate/reflectivity pairs reported both here and in PV11, here and the S/Z relationships reported in Falconi et al.

Our conclusion that the upper-limit S/Z relationship from Hiley et al. (2011) underestimates S would be modified if our WCR-derived reflectivities were negatively biased. Assuming the reflectivities are negatively biased by 2.5 dBZ, the minimum relative differences discussed previously are no smaller than 0.1 and 0.3 on 15 December and 3 January, respectively. A bias in reflectivity of this magnitude cannot be ruled out but neither can a positive bias of the same magnitude (Sect. 2.3). The latter increases the minimum relative differences to 1.6 and 2.2 on 15 December and 3 January, respectively. In each of these calculations we have summed the attenuations (Table 43) with ± 2.5 dBZ and used Eq. 1 to calculate error-perturbed reflectivities.

The scatter of measurements in Fig. 12 $\frac{1}{4}$, the plausibility of a -2.5 to +2.5 dBZ bias in WCR reflectivity measurements, and error in measurement of S (Sect. 2.4), indicate that refined techniques will be needed in future investigations which apply the approach described here. Taking into consideration the goal of evaluating snowfall rates from space, some advance in satellite remote sensing also seems warranted. One issue is diagnosing where riming is occurring within clouds. Both lidars and radiometers can sense supercooled liquid water from space (e.g., Battaglia and Panegrossi, 2020), and if combined with Doppler radars operating at multiple wavelengths, can diagnose precipitation attributable to rimed snow particles. Despite limitations of the multiple-wavelength Doppler method, for example in scenarios with vertical air speed comparable to and larger than particle fall speed (Vogl et al. 2022), the method has been validated in ground-based field studies (Kneifel et al. 2015; Mason et al. 2018). Technical challenges also remain for implementing the method from space (Battaglia et al. 2020). Additionally, improved methods are needed to diagnose situations where riming is occurring within clouds. Both lidars and radiometers can sense supercooled liquid water from space (e.g., Battaglia and Panegrossi, 2020), and if combined with Doppler radar, can diagnose precipitation attributable to rimed snow particles. These approaches are being tested in groundbased field studies (Kneifel et al. 2015; Moisseev et al. 2017; Mason et al. 2018) but are most reliable in scenarios with the magnitude of vertical air speed smaller than particle fall speed.

5 — Conclusions

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We have reported The reported measurements consist of surface measurements of S and near-surface measurements of Z. The latter came from overflights of a ground site, where a precipitation gauge was operated, and were acquired using an airborne W-band radar. The values of Z were corrected for attenuation.

The reported $S \neq S_{HP} / Z' \not\equiv Z$ pairs plot at or above the S-versus-Z best-fit line of PV11 (Fig. 12) and the—minimum relative S difference (Table 1) is no larger than 0.3 However, the points do not depart beyond the variability evident in a replotting of S/Z pairs from PV11. The PV11 data came from airborne measurements of W-band reflectivity, acquired within ± 100 m of flight level, and from coincident measurements of snow particle imagery. PV11 used a density-size function and a fall speed-size function, and measurements (PSD and particle images) to calculate S for snow particles that were classified as both rimed crystals and graupel. —This classification is also consistent with the particle imagery we have presented (Fig. 11).

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There is a We have documented a substantial difference in comparisons of the between our the snowfall rates points, reported here, and reflectivity-dependent S values calculated at using an upper-limit S/Z relationship for unrimed snow particles (Hiley et al. 2011). Here the minimum relative S differences are 0.7 and 1.0 for our two overflights and in a comparison to our measurements correspond to an underestimation of snowfall rate (Fig. 12). Thee relative differences offset are is approximately a factor of two larger than the precision of our snowfall ratethe S measurement. We also report a substantial difference, and S underestimation compared to our measurements (Fig. 12), for the comparison made to an S/Z relationship which assumes the snow particles are aggregates (Matrosov 2007). The snowfall rate underestimates obtained using both Hiley et al.'s and Matrosov's S/Z relationships (Fig. 12) are perhaps expected given that the density factored into those S/Z calculations is small compared to that for rimed snow particles. It is also expected that the larger density and spherical shape applied in the SSKB S/Z relationship contributed to the better agreement (minimum relative difference ~ 0.3) with our S_{HP} / Z^{\prime} pairs. Our conclusion is that some snowfall retrievals (e.g., Hiley et al. 2011) will underestimate S for weather targets containing rimed snow particles. We also state that our

conclusion is at odds with measurements and analysis in Falconi et al. Those researchers reported S/Z relationships for rimed snow particles which in instances with Z < 8 mm⁶ m⁻³ plot below the upper-limit of Hiley et al. (Fig. 12). The consequence is that the minimum relative S difference in our comparison to Falconi et al. (assuming Falconi et al.'s heavily-rimed classification) is comparable to and larger than in our comparison to the Hiley et al.'s upper-limit S/Z relationship.

6 - Appendix

This suggests that a measured Z and the Hiley et al. (2011) upper limit will produce an underestimate of precipitation in scenarios dominated by rimed snow particles.

New research is needed to refine the S/Z relationship for rimed snow particles. This could be computational – e.g., investigation of ing the utility of parameterizing S in terms of both Z and density – or could be observational. Unlike the investigation of PV11, where only an airborne platform was employed, we have demonstrated that useful information can be obtained using coordinated ground-based and airborne systems. Another approach would be with only ground-based instrumentation. This would avoid some of the complications encountered in this study, including _W-band attenuation and a reliance on particle imagery acquired aloft. A study with both ground-based and airborne systems would also be useful for understanding an S/Z mismatch; apparent at Z < 8 mm⁶ m⁻³; _ and which is larger than the offset summarized in the previous paragraph. Elements of the mismatch are the S/Z measurements reported by PV11, the measurements reported here, PV11's best-fit line, and the measurement-based S/Z relationships reported by Falconi et al. (2018). These three research teams reported measurements relevant to the development of an S/Z relationship for rimed snow particles.

This appendix explains how HP (hotplate) and WCR (Wyoming Cloud Radar) averages were evaluated. The scheme starts with an HP averaging interval (duration 60 s) and derives a WCR averaging interval and a WCR averaging domain. The latter encompasses a subset of the altitude-time crossection sampled by the WCR. The top boundary of the domain was derived using vertical-component Doppler velocities within the interval/domain. Because of this dependence, the line defining the top boundary had to be was derived iteratively.

With the overflight time symbolized t_0 , the beginning and ending times of the first of two 60-second HP averaging intervals are

1135
$$t_{HP,B} = t_O t_{HP,B} = t_O$$
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$$t_{HP,E} = t_O + 60$$
(A1)

Since two adjacent HP averaging intervals are evaluated in this analysis, we express the averaging times with the following recursive equations

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$$t_{HP,B}(i) = t_O + i \cdot 60 \tag{A3}$$

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$$t_{HP,E}(i) = t_O + (i+1) \cdot 60. \tag{A4}$$

- In Eqs. A3-A4 the index is $\underline{i} \in \{0, 1\}$. A special case with $\underline{i} = 2$ is also analyzed (in Sect.
- 1143 3.5).,

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Analogous to the recursion in Eq. A4, the ending time of a WCR averaging interval is

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$$t_{WCR,E}(i) = t_O - i \cdot 60 \cdot v_w / gs.$$
 (A5)

Here v_w is a wind advection speed (discussed below) and the second term on the rhs is a wind advection distance divided by the WKA (Wyoming King Air) ground speed ($_{gs}$ gs). Analogous 1147 to the Eq. A5, the beginning time of a WCR averaging interval is

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$$t_{WCR,B}(i) = t_{WCR,E} - (i+1) \cdot 60 \cdot v_{w} / gs$$
 (A6)

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The wind advection speed (v_w) in Eqs. A5-A6 was calculated using an altitudedependent west-to-east wind velocity (u_{tt}) and an altitude-dependent south-to-north wind velocity (v_{+}). These altitude-dependent component velocities were calculated using the horizontal wind vectors in the penultimate and last columns of Table 32. Plots of the component velocities versus altitude and the linear functions used to relate component velocities to altitude are presented in Figs. A1a-b.

An altitude ($z' \neq 3400$ m) was assumed for evaluating the horizontal wind advection vector. This is the altitude of the ridges west and northwest of the HP site (Figs. 3a-b).

The WKA track vector (Table 32) defines the vertical plane of the WCR measurements. We assumed that wind advection of snow particles occurred parallel to this vector. With the assumption stated in the previous paragraph, the horizontal wind advection speed (v_w) was calculated as the projection of the horizontal wind vector onto the track vector.

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$$v_{w} = \frac{u(z') \cdot gs_{x} + v(z') \cdot gs_{y}}{\left(gs_{x}^{2} + gs_{y}^{2}\right)^{1/2}}$$
(A7)

In Eq. A7 the west-to-east and south-to-north components of the track vector are symbolized gs_x 1163 and gs_y . Vector representations of the track vector are in Table 32. On 14/15 December 2016 and 1164 3 January 2017, the values of v_w are 7.4 and 8.9 m s⁻¹, respectively. 1165

In addition to the properties gs_{gs} and v_w used to evaluate Eqs. A5-A6, a WCR averaging interval/domain was evaluated using a snow particle downward speed (Eq. A8).

$$v_p = |\langle V_D \rangle| + \sigma_{V_D} \tag{A8}$$

Here, $\langle V_D \rangle$ is the average of Doppler velocities within an averaging interval/domain,

 $|< V_{\scriptscriptstyle D}>|$ is the absolute value of the average, and $\sigma_{\scriptscriptstyle V_{\scriptscriptstyle D}}$ is the standard deviation of the average.

On both the lhs and rhs of Eq. A8, all terms are greater than zero.

We interpret v_p as the maximum likely snow particle speed toward the ground. There are three reasons for this: 1) For the WCR averaging intervals/domains we analyzed, values of $\langle V_D \rangle$ were consistently less than zero (Table 65). This indicates that snow particles (on average) were moving toward the ground. 2) Again, for the WCR averaging intervals/domains we analyzed, σ_{V_D} was comparable to $|\langle V_D \rangle|$. This indicates that turbulent eddies transported snow particles upward and downward at a speed comparable their downward speed in still air. 3) The V_D are reflectivity weighted (Haimov and Rodi 2013) and are thus indicative of the motion of the largest particles within an averaging interval/domain.

We now focus on the top boundary of a WCR averaging interval/domain. Figures 6b and 6d have representations of the boundary. The slope defining this boundary was calculated as $-v_p \cdot gs/v_w$. That is, particles below this boundary moved downward sufficiently fast and horizontally sufficiently slow to advect reasonably close to the hotplate. Starting with diagnosed values of gs_{gs} and v_w , the values of v_p and slope, were derived iteratively. The precision of the derived v_p is \pm 0.1 m s⁻¹.

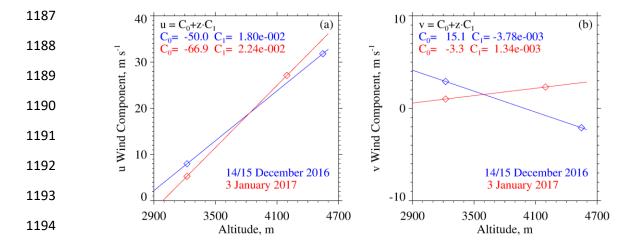


Figure A1 – (a) West-to-east (<u>u</u> **) wind velocity derived using measurements from the WKA and the AmeriFlux (AF) tower. Also shown is the linear function used to relate <u>u</u> ** to altitude.

(b) South-to-north (** v) wind velocity derived using measurements from the WKA and AF. Also shown is the linear function used to relate v **-to altitude. WKA and AF velocities are presented

as vectors in the penultimate and last columns of Table 32.

Data Availability. The WKA and WCR measurements can be obtained from the SNOWIE data archive of NCAR/EOL, which is sponsored by the National Science Foundation. Hotplate gauge measurements are at https://doi.org/10.15786/20103146. The US-GLE AmeriFlux measurements are at https://ameriflux.lbl.gov/. The Brooklyn Lake SNOTEL gauge measurements are at https://www.wcc.nrcs.usda.gov/snow/. Merged Hotplate, SNOTEL, and AmeriFlux data sequences from 14/15 December 2016 and 3 January 2017 are in Snider (2023).

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