

1 **W-band S/Z Relationships for Rimed Snow Particles: Observational Evidence from**  
2 **Combined Airborne and Ground-based Observations**

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**13 Abstract**

14 Values of undercatch-corrected liquid-equivalent snowfall rate ( $S$ ) at a ground site and  
15 microwave reflectivity ( $Z$ ) retrieved using an airborne W-band radar were acquired during  
16 overflights. The temperature at the ground site was between -6 and -15 °C. At flight level, within  
17 clouds containing ice and supercooled liquid water, the temperature was approximately 7 °C  
18 colder. Additionally, airborne measurements of snow particle imagery were acquired. The  
19 images demonstrate that most of the snow particles were rimed, at least a flight level. A  
20 relatively small set of  $S/Z$  pairs (4) are available from the overflights. Important distinctions  
21 between these measurements and those of Pokharel and Vali (2011), who reported  $S/Z$  pairs and  
22 an  $S/Z$  relationship for rimed snow particles, are 1) the fewer number of  $S/Z$  pairs, 2) the method  
23 used to acquire  $S$ , and 3) the altitude, relative to ground, of the W-band  $Z$  retrievals. This  
24 analysis corroborates that the  $S/Z$  relationship reported in Pokharel and Vali (2011) yields an  $S$  -  
25 in scenarios with snowfall produced by riming - substantially larger than that derived using an  
26  $S/Z$  relationship developed for unrimed snow particles.

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## 29 **1 - Introduction**

30 Improvement of methods used to measure snowfall and rainfall are an ongoing focus of  
31 meteorological research. The various methods are ground-based instruments that evaluate the  
32 mass of precipitation that falls into or onto a collector (precipitation gauges) (Brock and  
33 Richardson 2001), ground-based radars (Wilson and Brandes 1979), and airborne and space-  
34 borne radars (Matrosov 2007; Kulie and Bennartz 2009; Geerts et al. 2010; Skofronick-Jackson  
35 et al. 2017). An objective of these approaches, whether used to make observations independent  
36 of other methods (e.g., Kulie and Bennartz 2009), or as a component of multiple observations  
37 (e.g., Cocks et al. 2016), is estimation of precipitation rate and accumulated precipitation  
38 amount.

39 Many studies have investigated using radar for evaluating rainfall (for a review see  
40 Wilson and Brandes 1979). There are two approaches. The first is research, both observational  
41 and computational, that probes the relationship between rainfall rate (R) and radar-measured  
42 values of range-corrected backscattered microwave power. The latter is commonly reported as an  
43 equivalent radar reflectivity factor ( $Z_e$ ). The second is operational in the sense that precipitation  
44 gauges are used to calibrate measurements acquired using weather surveillance radars.  
45 Complications associated with converting  $Z_e$  to R, or converting a radar reflectivity factor<sup>1</sup> (Z) to  
46 R, can be grouped in four categories: 1) Inaccuracy in quantification of Z, 2) variation of the  
47 R/Z relationship stemming from precipitation processes (e.g., coalescence and break up), 3)  
48 difference between the volume of a radar range gate versus the much smaller volume of

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<sup>1</sup> Radars are calibrated to report  $Z_e$  (Smith 1984). Herein, radar reflectivities are reported as  $Z = Z_e$  and as  $\text{dBZ} = 10\log_{10}(Z_e)$ .

49 atmosphere sampled as precipitation falls to a gauge, and 4) vertical displacement between a  
50 radar range gate and a calibrating gauge, especially at far ranges.

51 For situations with snowfall, methods employing either gauge or radar are associated  
52 with complications beyond that incurred in rainfall (Matrosov 2007; Martinaitis et al. 2015;  
53 Cocks et al. 2016). Problems associated with gauge measurements are wind-induced snow  
54 particle undercatch, gauge capping, delayed registration, and blowing snow aliasing as snowfall.  
55 Moreover, in a situation with snow particles more abundant within a radar range gate, compared  
56 to rain drops, and where a measurement of  $Z$  is used to infer  $R$  via an  $R/Z$  relationship, the  
57 resultant precipitation rate will likely be inaccurate. This is because hydrometeor shape, density,  
58 and dielectric properties are all variable for snow particles while relatively invariant for rain  
59 drops. Additionally, a snow particle's terminal fall speed varies with size (as is the case for  
60 drops) and with particle shape and particle density. Going forward, we refer to the latter two  
61 properties as shape and density.

62 The goals of this paper are as follows: 1) to describe measurements of undercatch-  
63 corrected liquid-equivalent snowfall rate ( $S$ ,  $\text{mm h}^{-1}$ ) and how these were paired with W-band  
64 measurements of reflectivity ( $Z$ ,  $\text{mm}^6 \text{m}^{-3}$ ); 2) to contrast the  $S/Z$  pairs against  $S/Z$  relationships  
65 commonly applied in radar retrievals of  $S$ ; and 3) to investigate why the  $S/Z$  pairs deviate from  
66 predictions of some  $S/Z$  relationships.

67 In calculations of paired values of  $S$  and  $Z$ , density is an important parameter. Density is  
68 commonly estimated using empirical data (e.g., Pokharel and Vali 2011, [PV11]). For graupel, a  
69 snow particle that grows via collection of supercooled cloud droplets in a process commonly  
70 referred to as riming, paired observations of particle mass and particle size have been used to  
71 estimate density. There is considerable uncertainty in this approach. Based on data collected at

72 two northwestern US surface sites (Zikmunda and Vali 1972; Locatelli and Hobbs 1974), density  
73 values differ by at least a factor of two at particle sizes smaller than 2000  $\mu\text{m}$  (PV11; their Fig.  
74 4). Given that the density of rime ice varies with droplet impact speed, droplet size, and  
75 temperature (Macklin 1962), it is not surprising that the density-size relationships analyzed by  
76 PV11 are so varied.

77 Table 1 and the following paragraphs overview W-band S/Z relationships applied in  
78 instances with snow particles grown by vapor deposition (crystal), by collection of crystals  
79 (aggregate snowflake), and by riming (rimed crystal and graupel). Henceforth, the latter two  
80 snow particle types are collectively referred to as rimed snow particles.

81 In a computational study, Hiley et al. (2011) considered a variety of snow particle types  
82 (column, plate, bullet rosette, sector plate, dendrite, and aggregate snowflake), employed a  
83 parameterized ice particle size distribution (PSD) function (Field et al. 2005), accounted for a  
84 range of temperature (-5 to -15  $^{\circ}\text{C}$ ) via the Field et al. parameterization, and developed a range of  
85 S/Z relationships for snow particles. Except for the aggregate snowflakes (henceforth,  
86 aggregates), the modeled particle types were vapor-grown crystals. Hiley et al.'s upper- and  
87 lower-limit relationships are  $S = 0.21 \cdot Z^{0.77}$  and  $S = 0.024 \cdot Z^{0.91}$ , respectively. Matrosov (2007)  
88 developed an S/Z relationship for aggregates. In that work, parameterized PSDs from Braham  
89 (1990) were employed, and a range of particle aspect ratios were factored into the calculations.  
90 For aggregates, the S/Z relationship is  $S = 0.056 \cdot Z^{1.2}$  (Matrosov 2007). It should be noted that  
91 Hiley et al. (2011) and Matrosov (2007) employed similar, but not identical, computational  
92 methods. Computational research was also conducted by Kulie and Bennartz (2009) who  
93 adopted the wavelength-dependent density derived by Surussavadee and Staelin (2007) ( $200 \text{ kg}$   
94  $\text{m}^{-3}$  at  $\lambda = 3.2 \text{ mm}$ ), modeled the snow particles as spheres, and applied PSDs based on Field et

95 al. The resultant  $S/Z$  is  $S = 0.52 \cdot Z^{0.83}$  (Surussavadee and Staelin 2007; Kulie and Bennartz 2009;  
96 henceforth, SSKB). Variance in the calculations discussed in this paragraph originate from  
97 changes in density, shape, fall speed, PSD, and particle size as these changes are propagated  
98 through the cloud-microphysical and microwave-scattering calculations.

99 In a hybrid approach (computational and an analysis of measurements), PV11 concluded  
100 that most of the snow particles they imaged were rimed snow particles. Values of  $S$  were  
101 calculated using a density-size function ( $\rho_1$ , discussed below), a fall speed-size function,  
102 measured PSDs and measured particle images, and a determination of particle volumes. It was  
103 assumed that a prolate spheroid approximated particle shape and that shape was the basis for  
104 determining a particle's sphere-equivalent volume and the particle's sphere-equivalent size. The  
105 sphere-equivalent size was applied in the two functions. Values of  $Z$  were calculated using a  
106 measured PSD, sphere-equivalent sizes, the  $\rho_1$  function, and Mie Theory. PV11 presented  
107 calculations of  $Z$ , obtained using two density-size relationships (their Eqs. 1 and 2) and compared  
108 their calculated reflectivities to measurements of  $Z$  from a W-band radar. That led to their  
109 conclusion that "...the lower density assumption...yielded closer correspondence to observed  
110 reflectivities." Their recommendation for  $S$  as a function of measured  $Z$  - hereafter the  $S(\rho_1)/Z$   
111 best-fit line - is  $S = 0.39 \cdot Z^{0.58}$ . Values of  $Z$  that were paired with the calculated values of  $S$  (i.e.,  
112 the  $S/Z$  pairs from PV11 that we present in Sect. 4), and that were used to determine the  $S(\rho_1)/Z$   
113 best-fit line, came from the WCR. In addition to variance in their values of  $S$ , coming from a  
114 dependence on density, PV11 state that a value of  $S$  derived via their best-fit line is uncertain by  
115 a factor-of-ten. That uncertainty is evident in the variance of  $S/Z$  data pairs about the  $S(\rho_1)/Z$  line  
116 in Fig. 11 of PV11. Those investigators, and Geerts et al. (2010), attributed the variance to use of

117 two-dimensional snow particle images in calculations of  $S$  and to actual variations of density,  
118 shape, and particle size not accounted for in the calculations.

119 Another set of hybrid-type  $S/Z$  relationships was developed by Falconi et al. (2018; their  
120 Table 2). These are based on measurements from a video disdrometer, weighing precipitation  
121 gauge, microwave radiometer, and a vertically-pointing W-band radar. All these systems were  
122 operated at the ground. The data set was stratified into intervals of lightly-rimed, moderately-  
123 rimed, and heavily-rimed snow. A proxy for snow particle riming - radiometer measurements of  
124 liquid water path - was the basis for the stratifications (von Lerber et al. 2017). The  $S/Z$   
125 relationships are  $S = 0.10 \cdot Z^{1.0}$  (lightly-rimed),  $S = 0.079 \cdot Z^{1.3}$  (moderately-rimed), and  $S =$   
126  $0.060 \cdot Z^{1.4}$  (heavily-rimed).

127 Our focus is on surface measurements of  $S$  and on pairing of those measurements with  
128 airborne measurements of  $Z$ . We also analyze airborne measurements of snow particle imagery.  
129 The latter demonstrate that the particles observed at flight level were rimed. The imagery is the  
130 basis for our assertion that our data set is relevant to ongoing investigations of using  $Z$  to  
131 evaluate  $S$  in situations where precipitation is produced by riming.

132 Section 2 describes the setting of our study, the instruments we deployed, and recordings  
133 we obtained using two data acquisition systems. One of the data systems was operated at a  
134 ground site and the other on an aircraft. Section 3 is an analysis of the recordings; this section  
135 also considers recordings from two additional, but ancillary, ground sites. Our findings are  
136 discussed in Sect. 4 and summarized in Sect. 5. An Appendix (Sect. 6) explains how we  
137 averaged recordings of near-surface W-band reflectivities and surface-based recordings of  
138 snowfall.

139 Table 1 – W-band S/Z relationships from the literature, snow particle type, and values of minimum relative S difference

Reference	Abbreviation used for reference	S/Z relationship	Snow Particle Type	Minimum relative S difference on December 15 2016 <sup>a</sup>	Minimum relative S difference on January 3 2017 <sup>a</sup>
Hiley et al. (2011)	-	$S=0.21 \cdot Z^{0.77}$	Upper-limit S/Z relationship for vapor-grown crystals	0.7	1.0
Matrosov (2007)	-	$S=0.056 \cdot Z^{1.2}$	Aggregates	1.4	8.5 <sup>b</sup>
Surussavadee and Staelin (2007) and Kulie and Bennartz (2009)	SSKB	$S=0.52 \cdot Z^{0.83}$	Spherical snow particles with density = 200 kg m <sup>-3</sup>	0.3	0.2 <sup>c</sup>
Pokharel and Vali (2011)	PV11	$S=0.39 \cdot Z^{0.58}$	Rimed snow particles assuming the lower of two density-size relationships	0.3	0.0 <sup>d</sup>
Falconi et al. (2018)	-	$S=0.060 \cdot Z^{1.4}$	Snow particles classified as heavily rimed	0.6 <sup>e</sup>	8.5

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141 <sup>a</sup> Minimum relative S difference is defined as the minimum of  $|(S_{HP}-S)|/S$  where  $S_{HP}$  is a measurement of undercatch-corrected liquid-equivalent  
 142 snowfall rate (Table 6) and S is a snowfall rate on an S/Z relationship line evaluated at one of the attenuation-corrected reflectivities (Sect. 4).

143 <sup>b</sup> Attenuation-corrected Z on this day (0.6 mm<sup>6</sup> m<sup>-3</sup>) is smaller than the lower-limit Z (1 mm<sup>6</sup> m<sup>-3</sup>) advised for this S/Z relationship (Matrosov  
 144 2007).

145 <sup>c</sup> Maximum relative S difference on this day is 0.4.

146 <sup>d</sup> Maximum relative S difference on this day is 0.7.

147 <sup>e</sup> Maximum relative S difference on this day is 0.9.

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## 149 2 - Site, Aircraft, and Instruments

### 150 2.1 - Site

151 Analyzed herein are aircraft and ground data from 14/15 December 2016 and from 3  
152 January 2017. The ground data were acquired in a forest/prairie ecotone on the eastern slope of  
153 the Medicine Bow Mountains in southeast Wyoming (Figs. 1a-b). No ground-based observers  
154 were deployed during the two snowfall events analyzed.

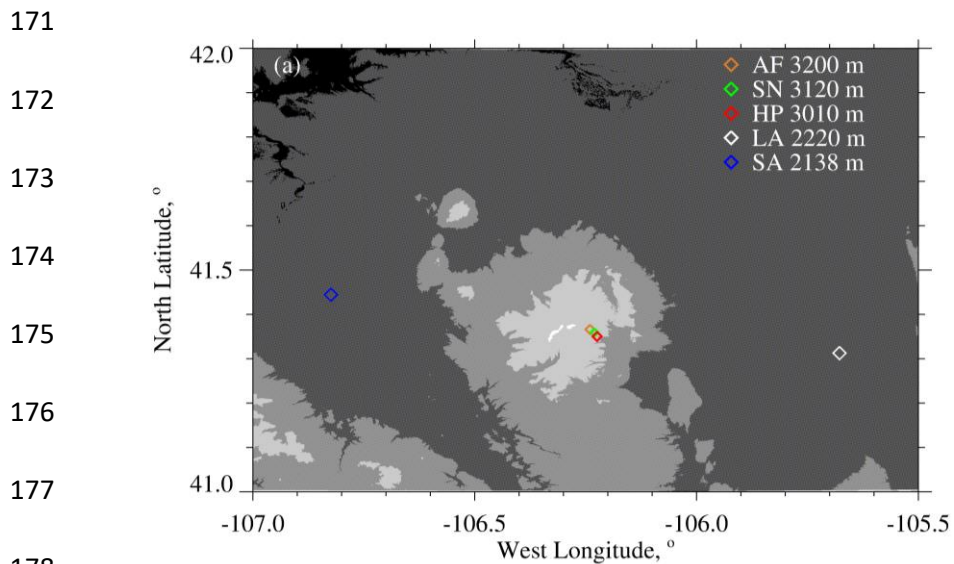
155 At one of three ground sites (HP in Figs. 1a-b) a hotplate precipitation gauge (Rasmussen  
156 et al. 2011; Zelasko et al. 2018), a GPS receiver, and a data acquisition system were deployed.  
157 Once per second, the data system ingested a hotplate-generated data string, combined that with  
158 time-of-day from the GPS receiver [Coordinated Universal Time (UTC)], and recorded the  
159 merged hotplate/UTC data string. The absolute accuracy of the time stamp is no worse than 2 s.

160 Overflights of the hotplate were done by the University of Wyoming King Air (WKA) on  
161 14/15 December 2016 and on 3 January 2017. The flights were conducted in preparation for the  
162 SNOWIE field project (Tessendorf et al. 2019) and were flown from the Laramie, WY Airport  
163 (LA in Fig. 1a). Data acquisition on the WKA was also synchronized with UTC, but with much  
164 better accuracy than at the hotplate.

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166           Measurements of horizontal wind (speed and direction), temperature, relative humidity,  
167 and pressure from the US-GLE AmeriFlux tower (AF in Figs. 1a-b) are also components the  
168 analysis. The AmeriFlux data were provided to us as 30-minute averages (AmeriFlux 2021;  
169 Marlow et al. 2023).

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187 Figure 1 – (a) Southeast Wyoming, airport at Saratoga, WY (SA), airport at Laramie, WY (LA),

188 and the ground sites: AF = US-GLE AmeriFlux tower, SN = Brooklyn Lake SNOTEL, and HP =

189 hotplate. Altitudes of the airports and ground sites are in the legend. Altitude thresholds for the

190 digital elevation map are 1500, 2000, 2500, 3000, and 3500 meters. (b) Close up of the AF, SN,

191 and HP ground sites (from © Google Earth).

192

## 193 2.2 - University of Wyoming King Air (WKA)

194 The following WKA measurements were analyzed: aircraft position, temperature, snow  
195 particle imagery, and three moments of the cloud droplet size distribution function. A Cloud  
196 Droplet Probe (CDP; Faber et al. 2018) was the basis for the droplet size distribution  
197 measurements and the derived moments. The latter are droplet concentration (N), cloud liquid  
198 water content (LWC), and mean droplet diameter ( $\langle D \rangle$ ). Snow particle imagery was obtained  
199 using a precipitation particle imaging probe (2DP; Korolev et al. 2011) and a cloud particle  
200 imaging probe (2DS; Lawson et al. 2006). These acquired two-dimensional images of particles  
201 between 200 to 6400  $\mu\text{m}$  (2DP) and between 10 to 1280  $\mu\text{m}$  (2DS).

## 202 2.3 – The W-band Wyoming Cloud Radar (WCR)

203 Retrievals from the up-looking and down-looking antennas of the WCR, operated on the  
204 WKA, were also analyzed. For this we used Level 2 WCR data<sup>2</sup> with reflectivities recorded as  
205  $dBZ = 10 \cdot \log_{10}(Z)$ . The reflectivities were converted from dBZ to Z prior to processing.  
206 Additionally, values of the vertical-component Doppler velocity retrieved from below the WKA  
207 using the WCR's down-looking antenna were analyzed. The Doppler velocities were corrected  
208 for aircraft motion as described in Haimov and Rodi (2013). We use  $V_D$  to symbolize the  
209 corrected vertical-component Doppler velocity and adopt the convention that  $V_D > 0$  indicates  
210 upward hydrometeor motion.

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<sup>2</sup> [http://flights.uwyo.edu/uwka/wcr/projects/snowie17/PROCESSED\\_DATA/](http://flights.uwyo.edu/uwka/wcr/projects/snowie17/PROCESSED_DATA/)

212           The Level 2 WCR sampling was different on the two flight days and this difference is  
213 shown in Table 2. Ground-based calibrations of the WCR's up-looking antenna and correlations  
214 between in-flight retrievals acquired using the WCR's up-looking and down-looking antennas  
215 were used to estimate the precision and absolute accuracy of the WCR-derived values of dBZ.  
216 These are  $\pm 1.0$  dBZ and  $\pm 2.5$  dBZ, respectively (PV11).

217

218 Table 2 – Level 2 WCR sampling and the WKA overflight time

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Date	Level 2 WCR Vertical Sampling, m	Level 2 WCR Along-track Sampling, s	Overflight Time, UTC
14/15 December 2016	23	0.23	00:00:38 (15 December 2016)
3 January 2017	30	0.36	20:32:03

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221

## 222 2.4 - Hotplate Gauge

223 Algorithms used to process hotplate measurements are described in Rasmussen et al.  
224 (2011), Boudala et al. (2014), and Zelasko et al. (2018). Henceforth, these are referred to as R11,  
225 B14, and Z18, respectively. This section describes how hotplate measurements acquired at the  
226 HP site were analyzed. The hotplate deployed at the HP site is described in Wolfe and Snider  
227 (2012), Z18, and in Marlow et al. (2023).

228 Five measurements fundamental to the steady state energy budget of the hotplate's  
229 temperature-controlled up-viewing plate are output by the hotplate microprocessor as one-minute  
230 running averages (Z18). These averages were merged with the GPS time and recorded at 1 Hz by  
231 the data acquisition system (Sect. 2.1). With these measurements, calibration data (Marlow et al.  
232 2023), and the algorithm developed by Z18, we calculated  $S$  in two steps. First, the five hotplate  
233 measurements (electrical power supplied to the plate, ambient temperature, wind speed,  
234 downwelling shortwave flux, and downwelling longwave flux) were input to Eq. 3 in Z18. The  
235 output of that equation is a provisional liquid-equivalent precipitation rate. Second, the snow  
236 particle catch efficiency, described in the next paragraph, was used to calculate  $S$  as the ratio of  
237 the provisional rate and the catch efficiency.

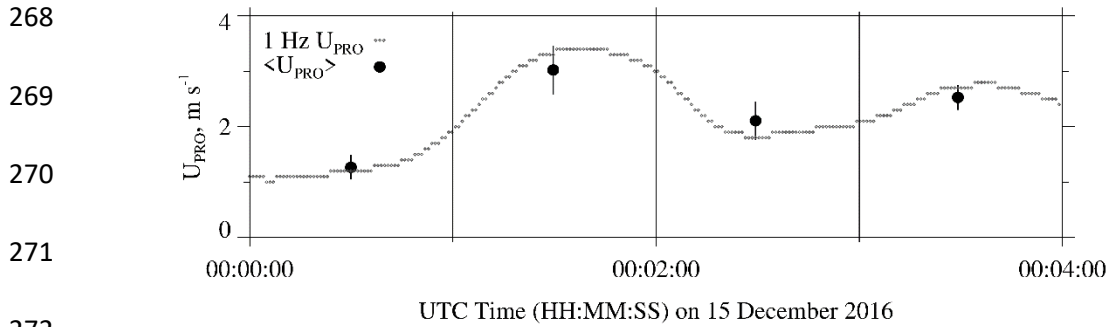
238 Marlow et al. (2023; their Fig. 3b) report the relationship between snow particle catch  
239 efficiency and wind speed that was applied in the calculation of  $S$ . There are three bases for this  
240 relationship. First is the catch efficiencies R11 derived using measurements obtained from a  
241 weighing gauge, operated within a double fence intercomparison reference shield, and collocated  
242 measurements from an unshielded hotplate gauge. These paired measurements are symbolized  
243 SRG (shielded reference gauge) and UHG (unshielded hotplate gauge). R11 plotted hotplate  
244 catch efficiencies (i.e., UHG/SRG) versus wind speeds measured at 10 m AGL (their Fig. 8).

245 Second is Marlow et al.'s adjustment of R11's 10 m AGL wind speeds to 2 m AGL. The basis  
246 for the adjustment is surface boundary layer parameters derived for R11's site (Kochendorfer et  
247 al. 2018) and an equation from Panofsky and Dutton (1984; their Eq. 6.7). The adjustment was  
248 made because the hotplate-derived wind speeds, both here and in Marlow et al. (2023), were  
249 acquired at approximately 2 m above the snowpack surface. Third is Marlow et al.'s comparison  
250 of SNOTEL-derived liquid-equivalent depth changes and hotplate-derived time-integrated  
251 accumulations. The interval for the comparisons is 24 hours. Based on the comparison, which  
252 has 57 paired values acquired at the sites labeled HP and SN in Fig. 1, the average fractional  
253 absolute relative difference is 0.30. Marlow et al. also provided an estimate of the error in a  
254 SNOTEL measurement (2.4 mm). At accumulation = 10 mm the error corresponds to a relative  
255 error = 0.24. This indicates that SNOTEL contributed significantly to the SNOTEL/hotplate  
256 variance and especially so for the smaller accumulations in Fig. 9a of Marlow et al. (2023).  
257 Because of this, we do not limit the following estimate of hotplate precision to a subset of the 57  
258 paired measurements. Based on our assessment of the average fractional absolute relative  
259 difference, the hotplate precision applied in this analysis was taken to be 0.3.

260 The hotplate-derived wind speeds acquired at ~ 2 m, and discussed in the previous  
261 paragraph, are henceforth symbolized  $U_{\text{PRO}}$ . The basis for these is a steady state energy budget of  
262 the hotplate's temperature-controlled down-viewing plate and a proprietary algorithm (R11 and  
263 Z18). The  $U_{\text{PRO}}$  are reported by a hotplate as one-minute running averages (Z18) and we  
264 recorded these at 1 Hz. Examples are the gray dots in Fig. 2. Additionally, we calculated and  
265 analyzed one-minute-averaged values of  $U_{\text{PRO}}$  and the corresponding standard deviations.  
266 Examples of these are the black circles and the short vertical line segments in Fig. 2.

267





274 Figure 2 – Hotplate wind speed measurements ( $U_{\text{PRO}}$ ) 00:00:00 to 00:04:00 on 15 December

275 2016. Gray dots are the one-minute running-average  $U_{\text{PRO}}$  recorded at 1 Hz. Black circles are the

276 one-minute-averaged  $U_{\text{PRO}}$  ( $\pm 1$  standard deviation).

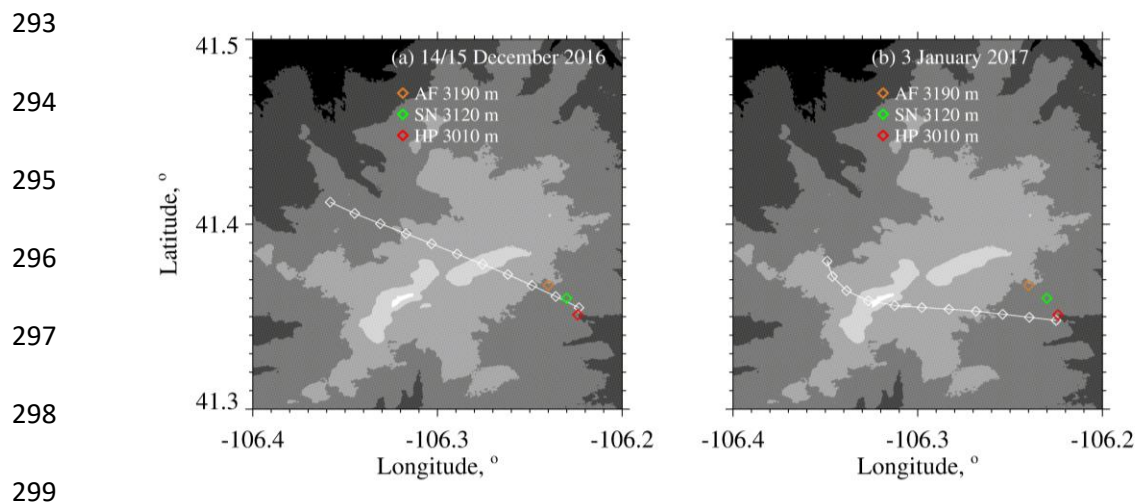
## 278 **3 - Analysis**

### 279 **3.1 - WKA Overflight Time**

280           The focus of our analysis is the two WKA flight segments shown in Figs. 3a-b. The maps  
281 shown in the figures have the three ground sites (AF, SN, and HP) and the WKA flight tracks  
282 (white line). The beginning-to-end time interval for the flight tracks is 100 s and these are  
283 divided into ten 10-second intervals. The 10 s intervals are indicated with white diamonds.  
284 Except for the turn evident in Fig. 3b, the flight tracks are straight, and the track direction is  
285 approximately upwind to downwind.

286           Times that the WKA was closest to the HP site were evaluated by finding the point on the  
287 flight track where the horizontal position of the WKA was closest to the hotplate's coordinates.  
288 These times are symbolized  $t_0$  and are referred to as overflight times. In Figs. 3a-b the downwind  
289 end of the flight tracks end at the overflight time. The latitude/longitude position of the aircraft  
290 was within 390 m of the hotplate at the overflight times. Table 2 has the overflight times on the  
291 two flight days.

292



300 Figure 3 – (a) WKA flight track on 14/15 December 2016 for time interval = overflight time -

301 100 s to the overflight time. (b) WKA flight track on 3 January 2017 for time interval =

302 overflight time - 100 s to the overflight time. The white diamonds on the tracks are separated, in

303 time, by 10 s. Altitude thresholds for the digital elevation maps are 2600, 2800, 3000, 3200,

304 3400, and 3600 meters. Altitudes of the ground sites are in the legend.

305

### 306 3.2 – Effect of Attenuation on WCR Reflectivities

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308 The presence of molecular oxygen, water vapor, cloud water, and snow particles within  
309 the WCR's transmission path will contribute to an attenuation of microwave intensity and will  
310 therefore negatively bias the retrieved reflectivities (Matrosov 2007; Hiley et al. 2011; Kneifel et  
311 al. 2015). Models of attenuation, radar remote sensing, and in situ measurements were used to  
312 calculate this bias. For oxygen, an attenuation coefficient from Ulaby et al. (1981; their Fig. 5.6),  
313 and temperature (T) and pressure (P) measurements from the AF (Table 3), were used. For  
314 vapor, an attenuation coefficient (Ulaby et al. 1981; their Eq. 5.22), and T, P, and relative  
315 humidity (RH) measurements from the AF (Table 3), were used. Concentrations of oxygen and  
316 water vapor and the oxygen and vapor path lengths are provided in Table 4. The latter is the  
317 vertical distance between the HP and the WKA. It was assumed that concentrations were  
318 uniform over this path length.

319 Attenuation by cloud water was derived using the WKA-measured T (Table 3), the  
320 WKA-measured LWC, path length (Table 4), and an attenuation formula (Liebe et al. 1989; Vali  
321 and Haimov 2001). The LWC applied in the formula is the maximum of CDP measurements  
322 acquired between  $t_0 - 10$  s and  $t_0$ . This interval coincides with the interval the WCR's down-  
323 looking antenna was used to acquire reflectivities over the HP (Sect. 3.5). The path length for  
324 cloud water was derived as the vertical distance between cloud base [derived thermodynamically  
325 using AF measurements (Table 3)] and flight level. LWC was assumed uniform, at the maximum  
326 value, over the path length.

327 Snow particle mass concentration is typically reported as an ice water content (IWC,  $\text{g m}^{-3}$ )  
328 (Liu and Illingworth 2000). The contribution of IWC to attenuation was calculated using

329 measurements in Nemanich et. al (1988), who reported an attenuation coefficient equal to 0.9  
 330 dB/km per unit of IWC. Also used were retrievals of IWC acquired using the down-pointing  
 331 WCR antenna. There are several steps in the calculation. First, all profiles of dBZ acquired  
 332 between  $t_0 - 10$  s and  $t_0$  were selected. Second, a maximum dBZ was selected at each of the  
 333 down-beam range gates (Table 2). Third, the dBZ maxima were increased by the overall two-  
 334 way attenuation in the final column of Table 4. Fourth, the profile of attenuation-corrected dBZ  
 335 was converted to a profile of attenuation-corrected Z. Fifth, a Z-to-IWC parameterization was  
 336 applied ( $IWC = 0.10 \cdot Z^{0.51}$ ; PV11; their Table 3). Sixth, the IWC profile was integrated, and the  
 337 derived ice water path was divided by the snow particle path length (Table 4). This calculation  
 338 produced a time- and range-averaged maximum IWC (Table 4). This IWC is the value applied in  
 339 the attenuation calculation.

340 Two-way attenuations ( $\Delta dB$ ), summed over contributions from the four components, are  
 341 presented in the final column of Table 4. Attenuation by snow and attenuation by liquid were the  
 342 most important components ( $> 50$  %) on December 15 and January 3, respectively. Vapor  
 343 contributed 32 % to the overall on December 15, and the combination of vapor and snow  
 344 contributed 45 % on January 3. Equation 1 shows how an attenuation-corrected reflectivity ( $Z'$ )  
 345 was derived using an uncorrected reflectivity ( $Z$ ) and the  $\Delta dB$ .

346

$$347 \quad Z' = 10^{\left[ \frac{10 \cdot \log_{10}(Z) + \Delta dB}{10} \right]} \quad (1)$$

348 Table 3 – Atmospheric state averages

349

Date	WKA <sup>a</sup> Track Altitude, m	WKA <sup>a</sup> T, °C	AF <sup>b</sup> T, °C	AF <sup>b</sup> RH, %	WKA <sup>a, c</sup> Track Vector	WKA <sup>a, c</sup> Wind Vector	AF <sup>b, c</sup> Wind Vector
14/15 December 2016	4546	-13.9	-6.3	86	310 / 130	274 / 32	250 / 8.5
3 January 2017	4196	-21.7	-14.6	77	280 / 120	265 / 27	260 / 5.4

350

351

352 <sup>a</sup> Altitude, temperature, track vector, and horizontal wind vector data obtained by averaging 1 Hz  
 353 WKA measurements. The averaging interval is 60 s and the interval starts at the overflight time,  
 354 minus 60 s, and ends at the overflight time.

355

356 <sup>b</sup> Temperature (T), relative humidity (RH), and horizontal wind vector data from sensors on the  
 357 US-GLE AmeriFlux tower (Sect. 2.1). The wind sensor was deployed at 26 m AGL (3223 m  
 358 MSL) and the T/RH sensor was deployed at 23 m AGL (3220 m MSL). The AF measurements  
 359 correspond to 30-minute averages closest to the overpass time. In the AF data set, time stamps on  
 360 the relevant AF recordings are 00:00 UTC (15 December 2016) and 20:30 UTC (3 January  
 361 2017).

362

363 <sup>c</sup> Vectors are presented in the following format: Direction of motion (degree relative to true  
 364 north) / speed ( $\text{m s}^{-1}$ ).

365 Table 4 – Attenuating component concentration, one-way pathlength, and the overall two-way attenuation

Date	Conc. Oxygen, kg m <sup>-3</sup>	Conc. Vapor, kg m <sup>-3</sup>	Maximum LWC, g m <sup>-3</sup>	Maximum IWC, g m <sup>-3</sup>	One-way Pathlength <sup>a</sup> Oxygen, Vapor, and Snow, km	One-way Pathlength <sup>b</sup> Cloud Water, km	Overall Two-way Attenuation, ΔdB
15 December 2016	0.21	2.7x10 <sup>-3</sup>	0.01	0.27	1.54	1.09	1.41 <sup>c</sup>
3 January 2017	0.21	1.3x10 <sup>-3</sup>	0.08	0.09	1.19	0.59	1.01 <sup>d</sup>

366

367 <sup>a</sup> Vertical distance between HP and WKA

368

369 <sup>b</sup> Vertical distance between cloud base [derived thermodynamically using AF measurements (Table 3)] and WKA

370

371 <sup>c</sup> One-way attenuation coefficients are 0.03 dB/km for oxygen (Ulaby et al. 1981), 0.14 dB/km for vapor (Ulaby et al. 1981), 0.056  
372 dB/km for cloud water (Liebe et al. 1989; Vali and Haimov 2001), and 0.24 dB/km for snow particles (Nemarich et. al 1988).

373

374 <sup>d</sup> One-way attenuation coefficients are 0.03 dB/km for oxygen (Ulaby et al. 1981), 0.073 dB/km for vapor (Ulaby et al. 1981), 0.49  
375 dB/km for cloud water (Liebe et al. 1989; Vali and Haimov 2001), and 0.077 dB/km for snow particles (Nemarich et. al 1988).

376

### 377 **3.3 - Correction of Doppler Velocity**

378 We accounted for bias in  $V_D$  (Sect. 2.3) due to deviation of the down-looking WCR  
379 antenna from vertical. This was done by applying the correction described in Zaremba et al.  
380 (2022) (their Eq. A4). The west-to-east and south-to-north particle velocities used in the  
381 correction were assumed to be equal to component wind velocities. The latter were expressed as  
382 linear functions of altitude using the information in the penultimate and last columns of Table 3.  
383 The component velocities as functions of altitude and the linear equations relating velocity and  
384 altitude are provided in the Appendix.

### 385 **3.4 - Hotplate Measurement of Wind Speed**

386 Here we compare the hotplate-derived wind speed to wind speed derived using an  
387 R.M.Young rotating anemometer (R.M.Young 2001). The second of these is symbolized  $U_{RMY}$   
388 and the basis for the first ( $U_{PRO}$ ) is a proprietary algorithm (Sect. 2.4). We are doing this  
389 comparison because B14 showed that  $U_{PRO}$  can be high-biased, relative to a conventional  
390 anemometer, and because  $U_{PRO}$  is the primary determinant of the rate that the up-viewing plate  
391 dissipates sensible heat energy. Diagnosis of that heat transfer rate is our basis for calculating the  
392 liquid-equivalent snowfall rate (Z18). The  $U_{PRO}$  also determines the snow particle catch  
393 efficiency and the latter was used in calculations of the undercatch-corrected liquid-equivalent  
394 snowfall rate (Sect. 2.4).

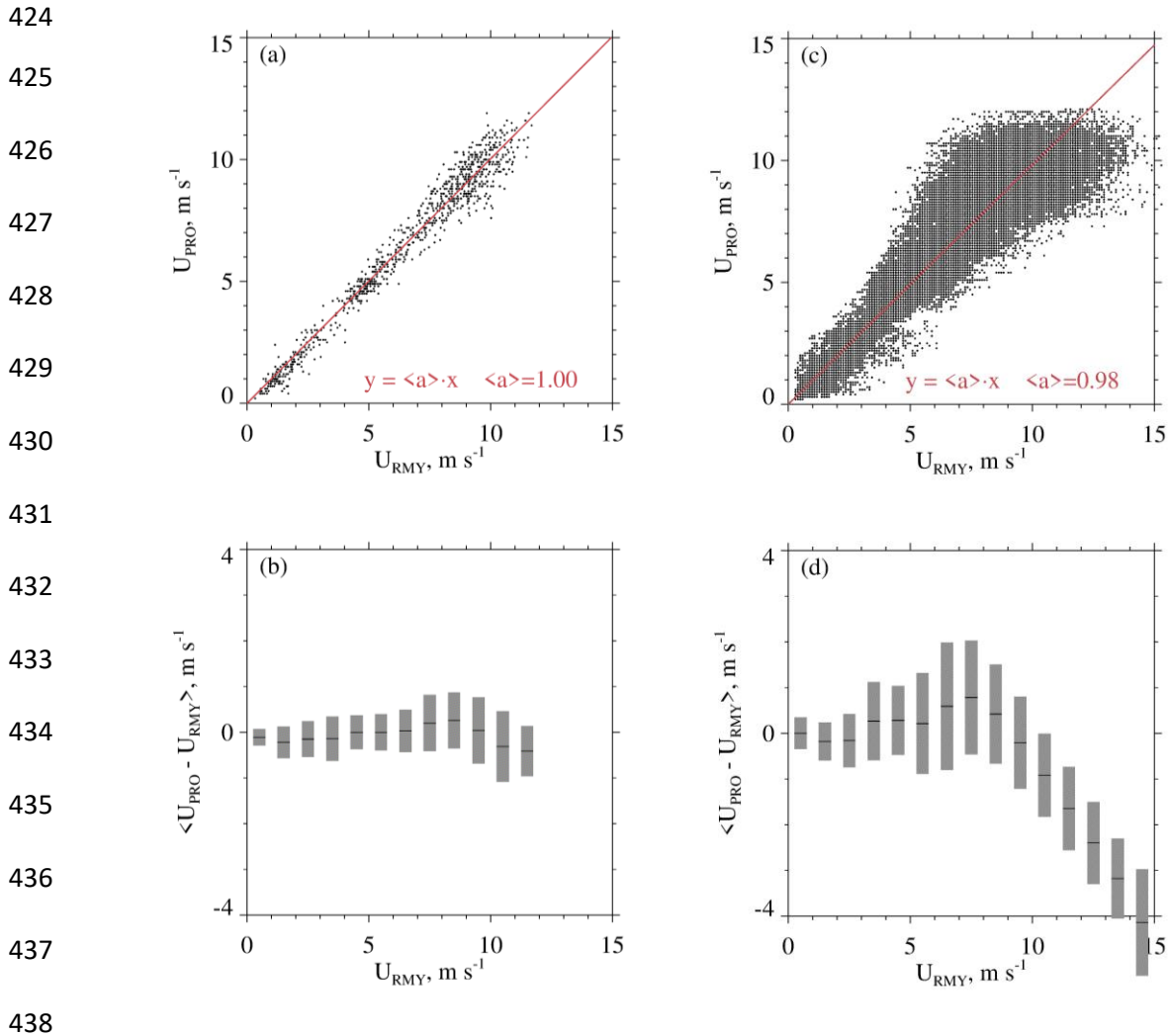
395 The comparisons reported here were done at the Laramie, WY Airport in December  
396 2019, and in January 2020. Compared to the HP site, the Laramie Airport site (indicated LA in  
397 Fig. 1) is free of obstruction, out to 120 m, and experiences larger wind speeds. By mounting the  
398 hotplate and the R.M.Young anemometer on rigid metal pipes, the hotplate's heated horizontal



399 surfaces (the up- and down-viewing plates seen in Fig. 1 of Z18) and the anemometer's spinning  
400 axis (oriented horizontally) were both positioned at 2 m AGL. The pipes were separated  
401 horizontally by 5 m. There was no precipitation on the days selected for the wind speed  
402 comparisons. The values of  $U_{\text{PRO}}$  and  $U_{\text{RMY}}$  we analyzed were recorded with a data system that  
403 time stamped the 1 Hz  $U_{\text{PRO}}$  and 1 Hz  $U_{\text{RMY}}$  with a relative timing accuracy no worse than 1 s.

404 A wind speed comparison - from 13 December 2019 - is shown in Fig. 4a.  $U_{\text{PRO}}$  was  
405 brought into the comparison by sampling it once per minute from files containing 1 Hz  
406 recordings of the one-minute running-average  $U_{\text{PRO}}$  (Sect. 2.4).  $U_{\text{RMY}}$  was brought into the  
407 comparison by starting with files containing 1 Hz recordings and converting these to one-minute  
408 averages. Fig. 4a shows no evidence of bias and Fig. 4b demonstrates that the average absolute  
409 departure between the  $U_{\text{PRO}}$  and  $U_{\text{RMY}}$  (both one-minute averages) is no larger than  $1 \text{ m s}^{-1}$ . Table  
410 5 has eight more precipitation-free comparisons. Included in the table are temperature and wind  
411 speed averaged over the comparison intervals (4 to 20 UTC), the slope of the linear-least-squares  
412 fit line (forced through the origin, red line), and the lower and upper quartiles of the slope. The  
413 quartiles were calculated using the method of Wolfe and Snider (2012). In contrast to Figs. 4a-b,  
414 Figs. 4c-d make the comparison using 1 Hz values of  $U_{\text{PRO}}$  and  $U_{\text{RMY}}$ . The larger scatter and  
415 larger average absolute departure seen in these panels is a consequence of the hotplate's limited  
416 time response, compared to the R.M.Young. We quantify the hotplate's response time in terms of  
417 a calculated thermal response time. During wintertime at the Laramie Airport, and with wind  
418 speed at  $5 \text{ m s}^{-1}$ , the down-viewing plate's thermal response time is approximately 60 s (results  
419 not shown). Because the temperature of the down-viewing plate is actively controlled, this does  
420 not translate to a 60 s lag between changes in wind speed and the hotplate response. The  
421  $U_{\text{PRO}}/U_{\text{RMY}}$  departure is most evident at  $U_{\text{PRO}} > 5 \text{ m s}^{-1}$  (Fig. 4d) but this is not a concern for

422  $U_{\text{PRO}}$  on 14/15 December 2016 or on 3 January 2017. Snider (2023) demonstrated that the  $U_{\text{PRO}}$   
423 was less than  $5 \text{ m s}^{-1}$  at the hotplate during the two WKA overflights.



439 Figure 4 – (a) Scatterplot of one-minute-averaged  $U_{\text{PRO}}$  and one-minute-averaged  $U_{\text{RMY}}$ .  
 440 Measurements were acquired at the Laramie, WY Airport 13 December 2019. The red line is a  
 441 linear-least-squares fit line (forced through the origin). (b) Average departure between one-  
 442 minute-averaged  $U_{\text{PRO}}$  and one-minute-averaged  $U_{\text{RMY}}$ . Average departures were calculated for  
 443 discrete  $U_{\text{RMY}}$  intervals, and the averages are indicated with short black horizontal lines. Gray  
 444 bars indicate  $\pm 1$  standard deviation. (c) Same as in (a) except for 1 Hz values of  $U_{\text{PRO}}$  and  $U_{\text{RMY}}$ .  
 445 (d) Same as in (b) except for 1 Hz values of  $U_{\text{PRO}}$  and  $U_{\text{RMY}}$ .

446

447

448 Table 5 -  $U_{\text{PRO}}$  versus  $U_{\text{RMY}}$  correlations

449

Date, UTC <sup>1</sup>	$\langle T \rangle$ <sup>2</sup> , °C	$\langle U \rangle$ <sup>2</sup> , m s <sup>-1</sup>	$\langle a \rangle$ <sup>3</sup>	a <sup>4</sup> First Quartile	a <sup>4</sup> Third Quartile
7 December 2019	-0.40	5.40	1.00	0.90	1.04
8 December 2019	2.70	4.10	0.99	0.90	1.04
10 December 2019	-5.20	3.80	0.99	0.83	1.04
13 December 2019	-1.50	6.60	1.00	0.93	1.06
18 December 2019	-6.20	3.60	0.99	0.92	1.04
19 December 2019	-6.90	2.70	0.95	0.84	0.99
6 January 2020	-6.40	8.80	1.01	0.96	1.06
8 January 2020	0.30	4.20	1.00	0.87	1.05
11 January 2020	-7.20	7.00	1.02	0.97	1.08

450

451

452 <sup>1</sup> Statistics presented are based on one-minute-averaged  $U_{\text{PRO}}$  and one-minute-averaged  $U_{\text{RMY}}$   
 453 measurements made between 04:00 to 20:00 UTC.

454

455 <sup>2</sup> Interval-averaged temperature and interval-averaged wind speed.

456

457 <sup>3</sup> Slope of the one-minute-averaged  $U_{\text{PRO}}$  versus one-minute-averaged  $U_{\text{RMY}}$  linear-least-squares  
 458 fit line, forced through the origin.

459

460 <sup>4</sup> Quartiles of the slope (see text)

461

### 462 3.5 – Combined Aircraft and Surface Measurements

463 Figure 5 has WCR and WKA measurements starting 100 s prior to  $t_0$  and ending at  $t_0$ .  
464 The sequences in Figs. 5a and 5c are reflectivities from both the up- and down-looking antennas.  
465 In Fig. 5a the flight track (black dashed horizontal line) is at 4550 m and in Fig. 5c the flight  
466 track is at 4200 m. At the  $t_0$  in Fig. 5a, below the WKA, the maximum radar echo is +6 dBZ ( $Z =$   
467  $4 \text{ mm}^6 \text{ m}^{-3}$ ) and in Fig. 5c the maximum is -3 dBZ ( $Z = 0.5 \text{ mm}^6 \text{ m}^{-3}$ ). Supercooled liquid water  
468 was detected as the aircraft approached the ridgeline (Fig. 5b) and during the last 10 seconds of  
469 the time sequence in Fig. 5d. During these encounters with supercooled liquid, the maximum  
470 LWC values were  $0.03 \times 10^{-3}$  and  $0.08 \times 10^{-3} \text{ kg m}^{-3}$  on 14 December 2016 and 3 January 2017,  
471 respectively. Values of  $N$  (Sect. 2.2) at times of maximal LWC were  $3 \times 10^6$  and  $100 \times 10^6 \text{ m}^{-3}$  on  
472 14 December 2016 and 3 January 2017, respectively. Even on 3 January 2017, the  $\langle D \rangle$  (Sect.  
473 2.2) associated with maximum LWC was sufficient for hexagonal plate crystals with diameter  
474 larger than  $100 \text{ }\mu\text{m}$  to collide with the observed droplets with efficiencies  $> 0.1$  (Wang and Ji  
475 2000).

476 We temporally and spatially averaged the values of  $Z$  we compared with time-averaged  
477 values of  $S$ . There are two reasons for this: 1) As discussed in Sect. 3.1, the WCR did not sample  
478  $Z$  exactly over the hotplate, and furthermore, the width of radar beam at 1500 m range - roughly  
479 the distance between the aircraft and the ground at the overflight times - is 30 m and thus  
480 considerably smaller than the minimum horizontal distance between the aircraft and the HP. 2)  
481 Compared to the WCR, the hotplate is a relatively slow-response measurement system whose  
482 output is commonly averaged over one-minute intervals (Z18).

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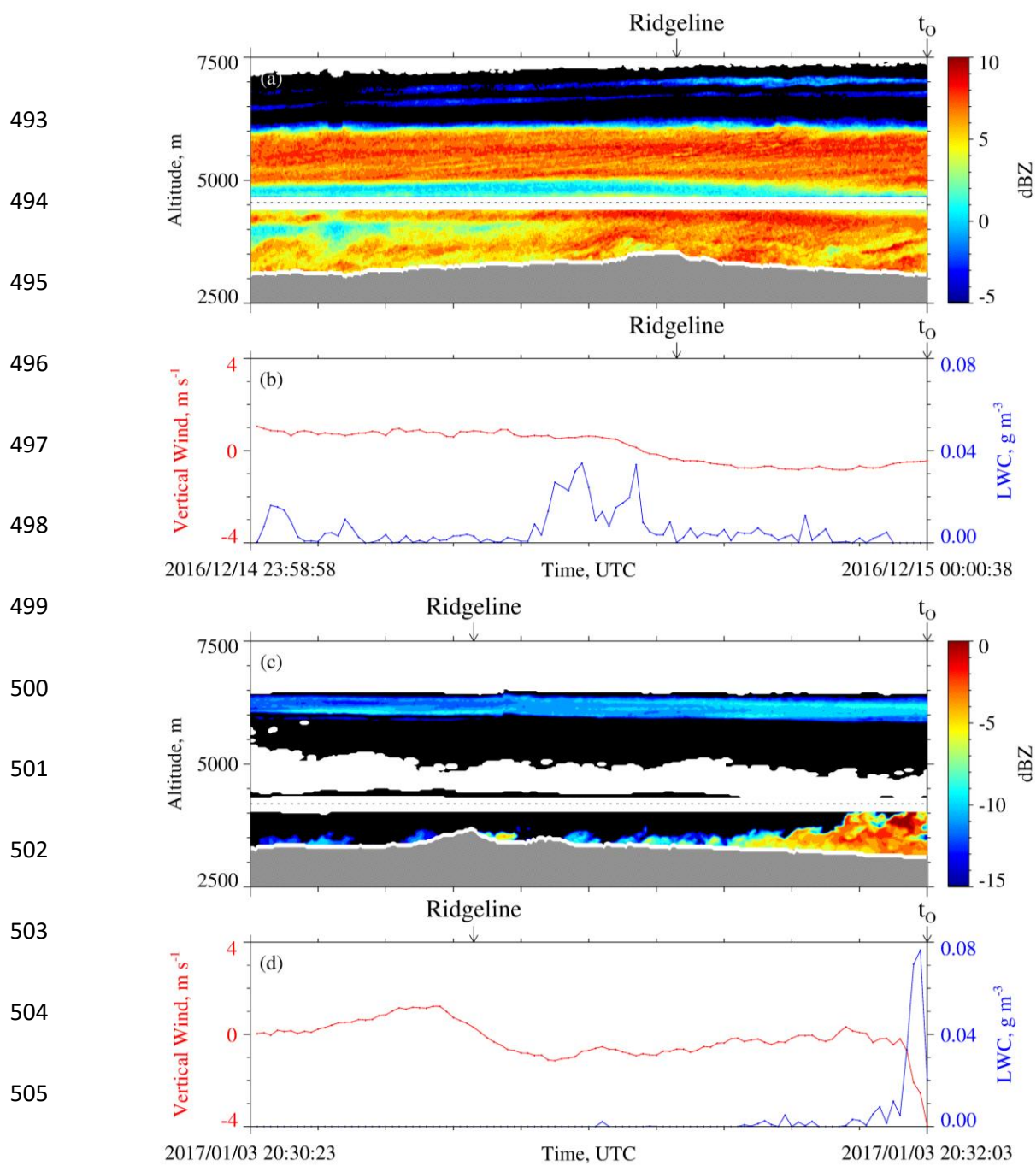
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507 Figure 5 – (a) 100 s of WCR reflectivity and (b) 100 s of LWC and gust probe vertical  
 508 wind velocity ending at  $t_0$  on 14/15 December 2016. (c) 100 s of WCR reflectivity and (d) 100 s  
 509 of LWC and gust probe vertical wind velocity ending at  $t_0$  on 3 January 2017. In (a) and (c),  
 510 above and below the flight track, the roughly 200-m-deep WCR blind zone is evident,  
 511 reflectivity above (below) the flight track is from the up-looking (down-looking) WCR antenna,

512 black indicates dBZ values smaller than the minimum indicated in the color bar, white  
513 immediately above the terrain indicates echo that was discarded because of ground clutter, and  
514 white above the ground clutter and outside of the blind zone indicate dBZ < minimum detectable  
515 signal.



516 In our analysis, the HP measurements were averaged over two adjacent 60 s intervals.  
517 The first extends from  $t_0$  to  $t_0 + 60$  s (Fig. 6a) and the second from  $t_0 + 60$  s to  $t_0 + 120$  s (Fig.  
518 6c). In Fig. 6a and in Fig. 6c,  $t_{HP,B}$  symbolizes an interval's beginning time and  $t_{HP,E}$  symbolizes  
519 an interval's ending time. Formulas describing how these times were related to the beginning and  
520 ending time of a corresponding WCR averaging interval are in the Appendix. Fig. 6b is a  
521 schematic of the first WCR averaging interval and Fig. 6d is a schematic of the second. Again,  
522 the subscripts "B" and "E" are used to indicate averaging beginning and ending times. Figures 6b  
523 and 6d both have lines at the top of an averaging interval/domain. The slopes of these lines are  
524 proportional to the ratio of two speeds. These speeds are a maximum likely snow particle speed  
525 toward the ground ( $v_p$ ) and a horizontal wind advection speed ( $v_w$ ). The  $v_p$  was calculated  
526 using averaged vertical-component Doppler velocities and  $v_w$  was calculated using a vertical  
527 profile of horizontal winds, based on WKA horizontal wind measurements and AF horizontal  
528 wind measurements (Figs. A1a-b), and using the WKA track vector (Table 3). An altitude ( $z' =$   
529 3400 m) was assumed in the calculation of  $v_w$ . This is the altitude of the ridges west and  
530 northwest of the HP site (Figs. 3a-b). Picking the altitude to be either  $z' = 3200$  m or  $z' = 3600$  m  
531 does not alter our findings.

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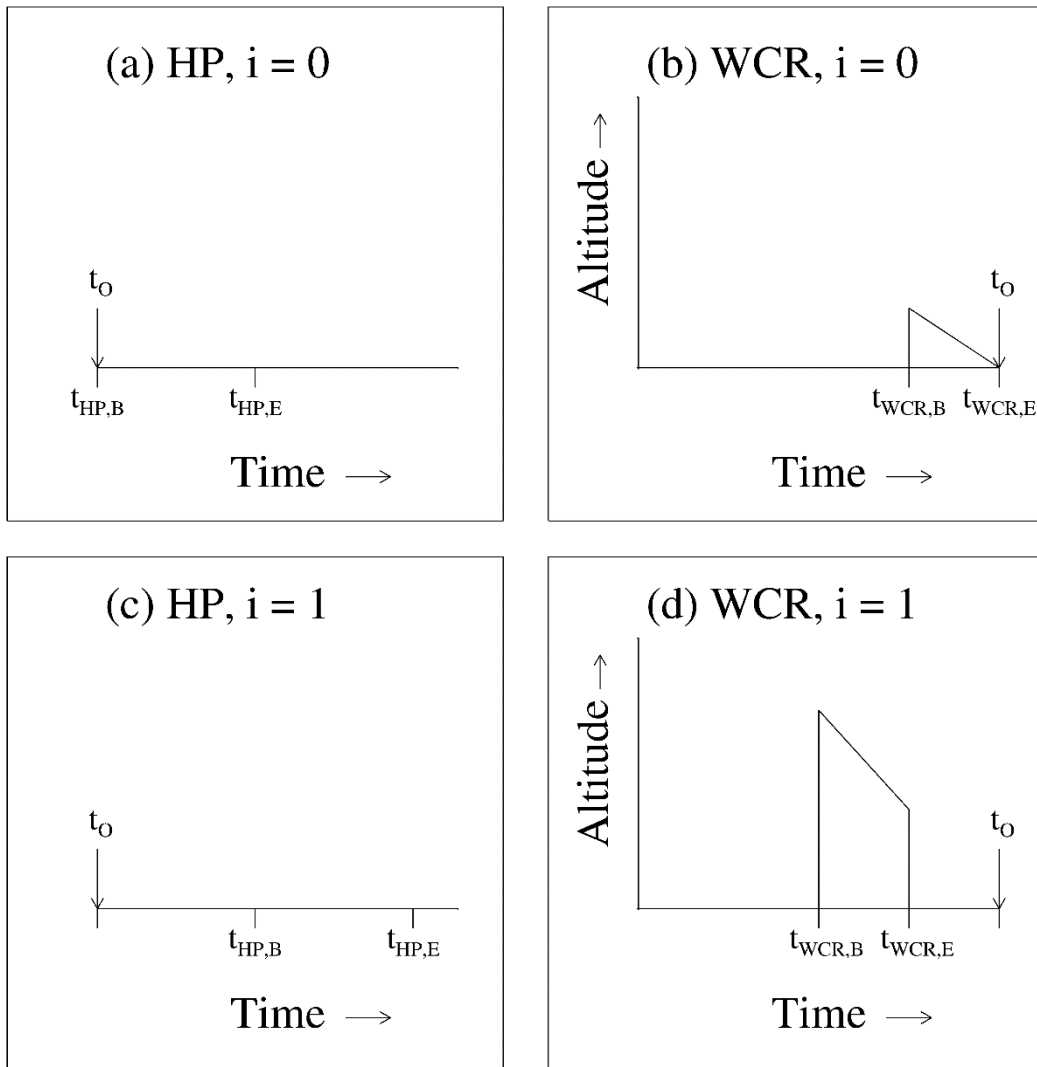


Figure 6 – (a and c) Representations of the  $i = 0$  and  $i = 1$  HP averaging intervals. (b and d) Representations of the  $i = 0$  and  $i = 1$  WCR averaging intervals/domains. The  $t_0$  is shown in all panels. The subscripts “B” and “E” indicate beginning and ending times of the HP averaging (panels a and c) and the beginning and ending times of the WCR averaging (panels b and d).

558

559 All panels in Fig. 6 are labeled with an index designating either the first averaging  
560 interval ( $i = 0$ ) or the second averaging interval ( $i = 1$ ). Figures 7 and 8 present hotplate  
561 snowfall measurements from 14/15 December 2016 and 3 January 2017. In these, and in  
562 subsequent figures, colored circles surround the  $i = 0$  and  $i = 1$  indexes, blue is used to color-  
563 code 15 December 2016, and red is used to color-code 3 January 2017. Additionally, Fig. 8 has  
564 an  $i = 2$  averaging interval. This is a special case discussed at the end of this section.

565 Figures 9a-b and Figs. 10a-b have enlarged views of the altitude-time WCR crosssections  
566 recorded on the two flight days. Different from Fig. 5a and Fig. 5c, these measurements are only  
567 from the WCR's down-looking antenna. Additional differences are the following: 1) The plots  
568 are set up so that Z and  $V_D$  structures downwind of the hotplate can be seen. These structures are  
569 discussed in the following section. 2) The WCR measurements are shown for 50 s of flight. With  
570 the WKA ground speed approximately  $125 \text{ m s}^{-1}$  (Table 3), the distance along the abscissa is  
571 6250 m. 3) Colored circles that surround the indexes are placed below the WCR averaging  
572 intervals/domains. The latter are drawn with solid black lines and are seen to overlay both the Z  
573 and  $V_D$  altitude-time crosssections. Consistent with Figs. 6b and 6d, and the Appendix, one of  
574 these black lines is vertical and another is negatively sloped. Figs. 10a-b also have the  $i = 2$   
575 intervals/domains discussed at the end of this section.

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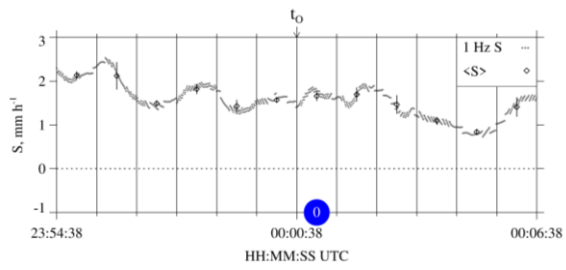
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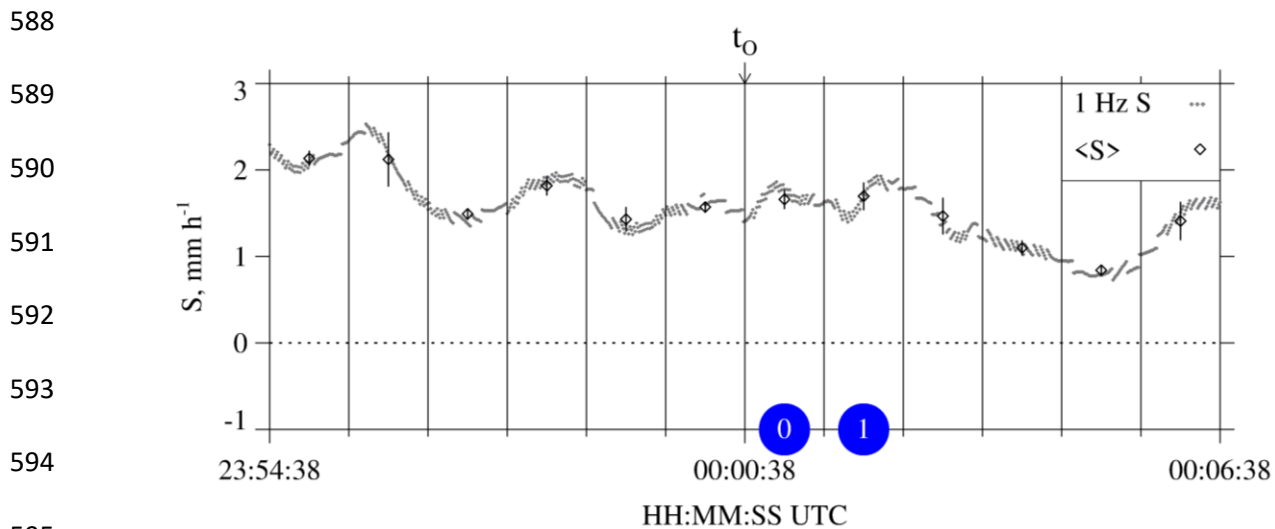


Figure 7 – Twelve minutes of HP snowfall measurements from 14/15 December 2016. Gray dots are  $S$  values calculated using hotplate output recorded at 1 Hz. Black diamonds are the one-minute-averaged values ( $\pm 1$  standard deviation). The  $t_0$  is shown above the panel and blue circles designate the  $i = 0$  and  $i = 1$  HP averaging intervals.

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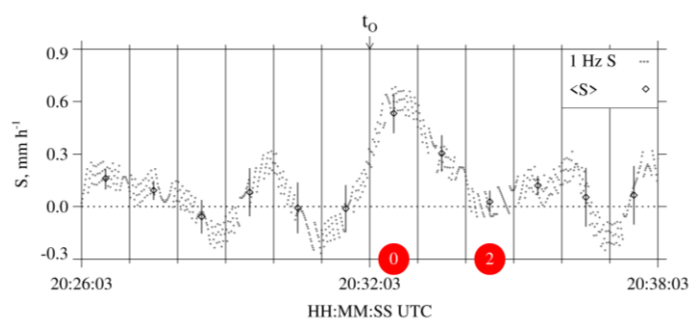
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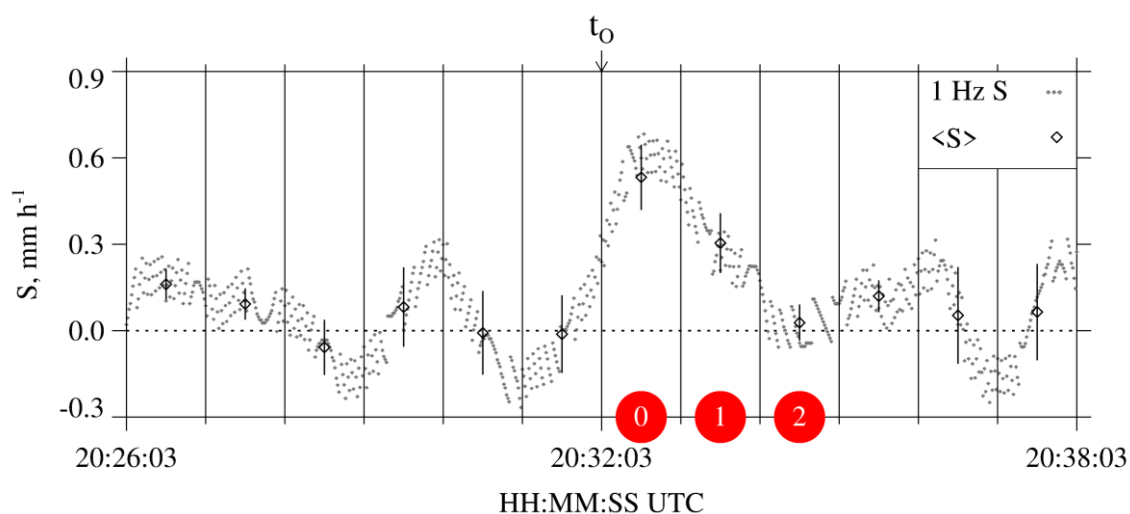
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620 Figure 8 – Twelve minutes of HP snowfall measurements from 3 January 2017. Gray dots are S

621 values calculated using hotplate output recorded at 1 Hz. Black diamonds are the one-minute-

622 averaged values ( $\pm 1$  standard deviation). The  $t_0$  is shown above the panel and red circles

623 designate the  $i = 0$ ,  $i = 1$ , and  $i = 2$  HP averaging intervals. The  $i = 2$  interval is a special case

624 discussed at the end of Sect. 3.5.

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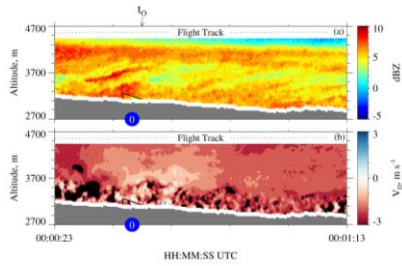
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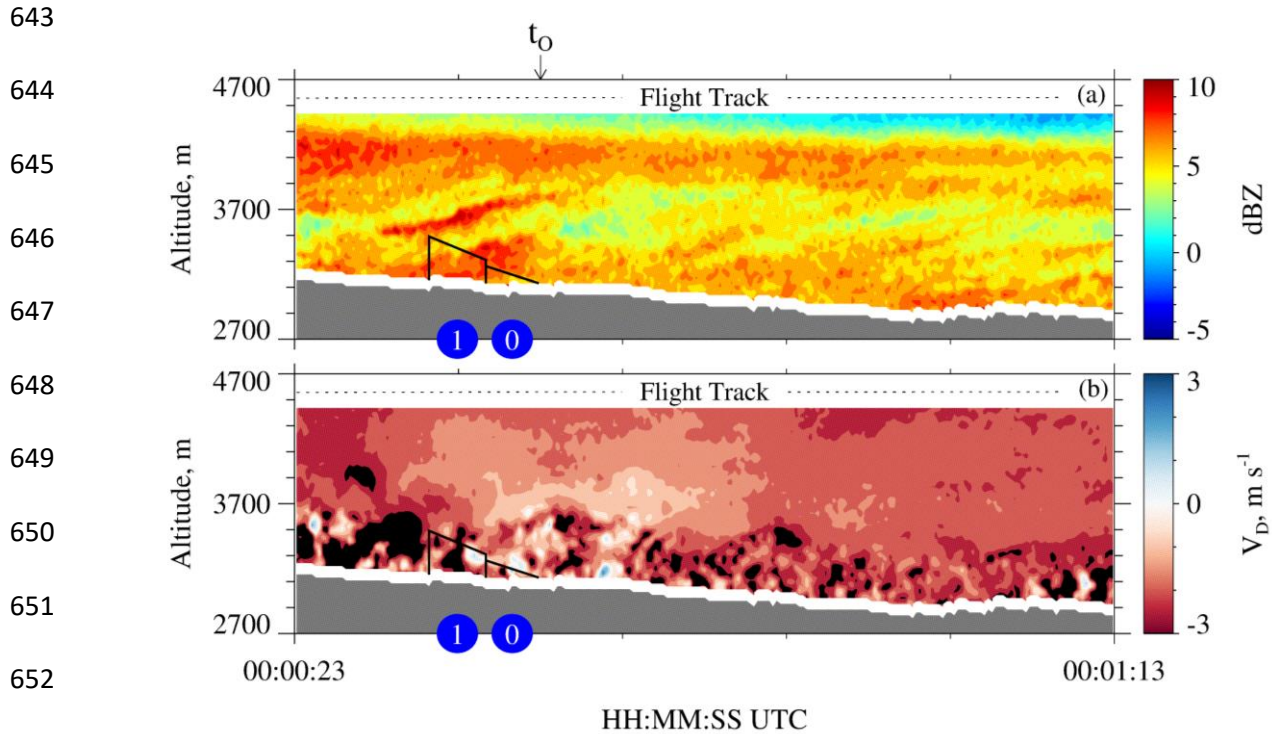


Figure 9 – 50 s of measurements from the down-looking WCR antenna on 15 December 2016.

(a) Crosssection of reflectivity  $t_0 - 15$  s to  $t_0 + 35$  s. (b) Crosssection of Doppler velocity  $t_0 - 15$  s to  $t_0 + 35$  s. The  $t_0$  is shown above the top panel. In both panels, the solid black lines (vertical and sloped) encompass the  $i = 0$  and  $i = 1$  WCR averaging intervals/domains and blue circles designate the WCR averaging intervals.

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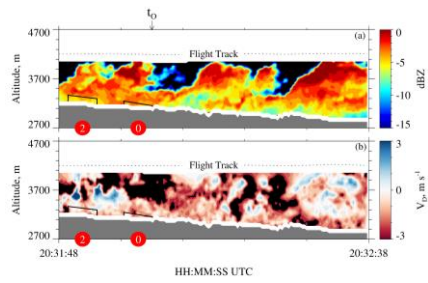
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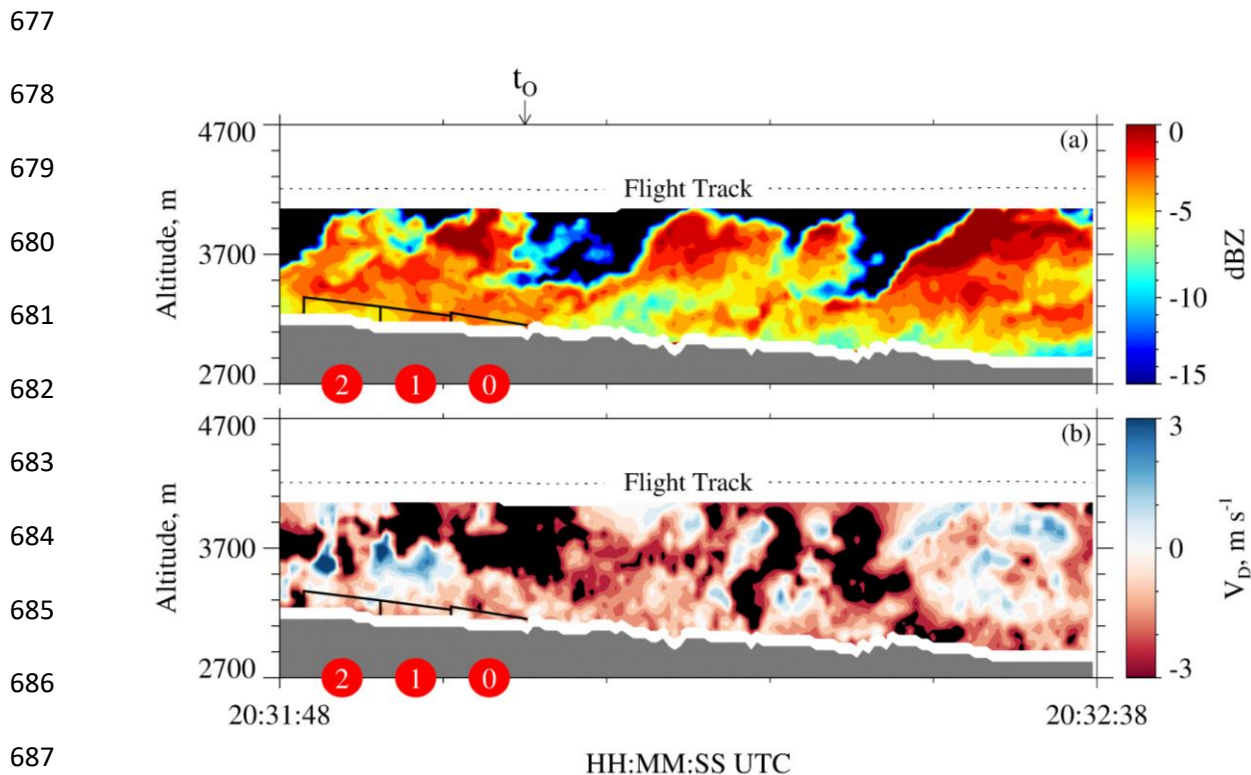


Figure 10 – 50 s of measurements from the down-looking WCR antenna on 3 January 2017. (a) Crossection of reflectivity  $t_0 - 15$  s to  $t_0 + 35$  s. (b) Crossection of Doppler velocity  $t_0 - 15$  s to  $t_0 + 35$  s. The  $t_0$  is shown above the top panel. In both panels, the solid black lines (vertical and sloped) encompass the  $i = 0$ ,  $i = 1$ , and  $i = 2$  WCR averaging intervals/domains and red circles designate the  $i = 0$ ,  $i = 1$ , and  $i = 2$  WCR averaging intervals/domains. The  $i = 2$  interval/domain is a special case discussed at the end of Sect. 3.5.

697           The  $i = 0$  and  $i = 1$  averages of S and Z are presented in Table 6 and the corresponding  
698 averaging intervals are viewable in Fig. 7 and Fig. 9a (15 December 2016) and in Fig. 8 and Fig.  
699 10a (3 January 2017). According to the averaging scheme (Fig. 6), the  $i = 1$  HP averaging  
700 interval is time-shifted positively compared to the  $i = 0$  HP averaging interval and the  $i = 1$   
701 WCR averaging interval is time-shifted negatively compared of the  $i = 0$  WCR averaging  
702 interval. This arrangement of the averaging intervals is one way to average while also accounting  
703 for wind advection of the snow particles.

704           As discussed earlier in this section, the averaging scheme initializes with 60-second  
705 blocks of HP data between  $t_o$  and  $t_o + 120$  s. When we applied the scheme to data from 3 January  
706 2017, but outside the specified time range, an inconsistency was documented. This is apparent in  
707 Fig. 8, where the  $t_o + 120$  s to  $t_o + 180$  s interval (i.e., the  $i = 2$  interval) has negligible average S,  
708 while in Fig. 10, the  $i = 2$  interval has a non-negligible average Z ( $\sim 0.3 \text{ mm}^6 \text{ m}^{-3}$ ). A firm  
709 explanation is not available for the inconsistency, but a factor may be the convective nature of  
710 the fields in Figs. 10a-b. Because of the inconsistency, only averages corresponding to the  $i = 0$   
711 and  $i = 1$  intervals are analyzed further.

712 Table 6 – Average wind measurements, average hotplate measurements, average WCR measurements, and attenuation-corrected  
 713 reflectivities

Date	$v_w^a$ , m s <sup>-1</sup>	i index	$S_{HP} \pm \sigma^b$ , mm h <sup>-1</sup>	WCR Samples <sup>c</sup>	$\langle V_D \rangle^d$ , m s <sup>-1</sup>	$\sigma_{V_D}^e$ , m s <sup>-1</sup>	$v_p^f$ , m s <sup>-1</sup>	$\langle Z \rangle \pm \sigma_Z^g$ , mm <sup>6</sup> m <sup>-3</sup>	$Z'^h$ , mm <sup>6</sup> m <sup>-3</sup>
15 December 2016	7.4	0	1.7±0.1	42	-1.3	0.9	2.2	4.9±2.1	6.8
15 December 2016	7.4	1	1.7±0.2	149	-1.8	1.2	3.0	5.6±1.1	7.8
3 January 2017	8.9	0	0.5±0.1	22	-0.9	0.8	1.7	0.49±0.05	0.62
3 January 2017	8.9	1	0.3±0.1	35	-0.8	0.4	1.2	0.50±0.10	0.63

714

715 <sup>a</sup> Horizontal wind advection speed (Eq. A7) calculated using values from the penultimate and last columns of Table 3.

716 <sup>b</sup> One-minute average of the undercatch-corrected liquid-equivalent snowfall rate ( $\pm 1$  standard deviation). An example averaging  
 717 interval is the  $i = 0$  interval in Fig. 7.

718 <sup>c</sup> Number of samples used to calculate the WCR statistics. The averaging intervals/domains (e.g.,  $i = 0$  in Figs. 9a-b and in Figs. 10a-  
 719 b) encompass the WCR samples which are the basis for the WCR statistics presented in this table.

720 <sup>d</sup> Average of Doppler velocity within the averaging intervals/domains.

721 <sup>e</sup> Standard deviation of Doppler velocity within the averaging intervals/domains.

722 <sup>f</sup> Maximum likely snow particle speed toward the ground (Eq. A8).

723 <sup>g</sup> Average reflectivity ( $\pm 1$  standard deviation). These values are not corrected for attenuation.

724 <sup>h</sup> Attenuation-corrected reflectivities. These were derived using reflectivities from the penultimate column of this table, attenuations  
 725 from Table 4, and Eq. 1.

### 726 3.6 - Snow Particle Imagery

727 In Fig. 9a and Fig. 10a, the time for a snow particle to move the abscissa and ordinate  
 728 distances is different. The ratio of these two times is 2.6. This follows from our choice of  
 729 abscissa and ordinate ranges, from values of particle fall speed ( $1 \text{ m s}^{-1}$ ) and horizontal wind  
 730 advection speed ( $8 \text{ m s}^{-1}$ ), which we assumed, and from the WKA ground speed ( $gs \sim 125 \text{ m s}^{-1}$ ;  
 731 Table 3). The assumed values are approximately consistent with values of  $\langle V_D \rangle$  and  $v_w$ , in  
 732 Table 6, and with the  $V_D$  sign convention (Sect. 2.3). We also used  $gs = 125 \text{ m s}^{-1}$  to scale  
 733 (virtually) the time axes in Fig. 9a and Fig. 10a to a horizontal distance. Within the scaled  
 734 coordinate frames, we assumed that all snow particle trajectories have negative slope ( $\Delta z / \Delta x = -$   
 735  $1 \text{ m s}^{-1} / 8 \text{ m s}^{-1} = -0.12$ ) and that all trajectories are stationary. However, both assumptions seem  
 736 inconsistent with the reflectivity structures in Fig. 5a, where positively-sloped particle fall  
 737 streaks are evident at  $\sim 5500 \text{ m}$ , inconsistent with Fig. 9a where positively-sloped fall streaks are  
 738 at  $\sim 3500 \text{ m}$ , and inconsistent with the positively-sloped fall streaks in Fig. 10a. On both flight  
 739 days, the fall streaks evince particle sources that move horizontally and with a horizontal speed  
 740 that is larger than the  $v_w = 8 \text{ m s}^{-1}$  applied in the estimate of the trajectory slope. It may be that  
 741 the source's horizontal speed is comparable to the flight-level WKA-derived horizontal wind (27  
 742 to  $32 \text{ m s}^{-1}$ ; Table 3) but we do not have data needed to verify that assertion. Based on the  
 743 assumption that snow particles followed the fall streaks while both were advecting horizontally,  
 744 we looked *downwind* of the hotplate - at a time later than  $t_0$  in Fig. 9a and Fig. 10a - for particles  
 745 that became those that produced snowfall at the hotplate.

746 Particle images from 15 December 2016 were analyzed using the 2DP. With this  
 747 instrument the maximum all-in particle size (in the horizontal direction perpendicular to flight) is

748 6400  $\mu\text{m}$  and the particle size resolution is 200  $\mu\text{m}$  (Sect. 2.2). Within the time interval picked  
749 for this analysis (discussed below), particles sizing in the smaller of the two spectral modes, with  
750 mode size  $\sim 400 \mu\text{m}$ , were more numerous (results not shown). Because the 400  $\mu\text{m}$  particles are  
751 poorly resolved by the 2DP, and the same can be said for somewhat larger particles, those  
752 smaller than 1000  $\mu\text{m}$  were excluded from the following analysis. Figure 11a shows imagery  
753 from 12 s of measurements acquired near the end of the sequence in Fig. 9a (00:01:02 to  
754 00:01:14). This time interval was selected by tracing forward from  $t_0$ , along the slope of the fall  
755 streaks, to the flight level. Many of the particles are rounded (indicating riming) and a few have  
756 arms likely due to incomplete conversion of branched crystals to rimed snow particles. The mode  
757 size corresponding to these images is 1600  $\mu\text{m}$ . No liquid water was detected with these particles  
758 ( $\text{LWC} < 0.01 \times 10^{-3} \text{ kg m}^{-3}$ ; Fuller 2020; her Fig. 8), but liquid was detected, at  $\sim 00:00:00$ , as the  
759 aircraft approached the ridgeline (Figs. 5a-b).

760 Turning to imagery from 3 January 2017, the most appropriate location for analysis  
761 would be through the second billow structure evident in Fig. 10a (i.e., very close to the middle of  
762 the Fig. 10a sequence). This billow sourced a fall streak that terminated at the hotplate (i.e., at  
763 the time  $t_0$  indicated in the figure). However, the aircraft only clipped the top of this billow, and  
764 it was only when sampling the billow seen  $\sim 13$  s earlier that larger ice particle concentrations ( $\sim$   
765  $20,000 \text{ m}^{-3}$ ) (Fuller 2020; her Fig. 10) and larger LWC ( $\sim 0.08 \times 10^{-3} \text{ kg m}^{-3}$ ; Fig. 5d) were  
766 detected. Maximum reflectivities were the same in all three billows ( $Z \sim 1 \text{ mm}^6 \text{ m}^{-3}$ ; 0 dBZ), so it  
767 was assumed that imagery collected in the first billow (20:32:00 to 20:32:02) was representative  
768 of what was falling toward the hotplate. The 2DS was used to image these particles (Fig. 11b);  
769 with this instrument the maximum all-in particle size (in the horizontal direction perpendicular to  
770 flight) is 1280  $\mu\text{m}$  and the size resolution is 10  $\mu\text{m}$  (Sect. 2.2). Most of the objects in Fig. 11b

771 appear to be rimed and their mode size is  $\sim 400 \mu\text{m}$ . It is also noted that particles smaller than  
772  $100 \mu\text{m}$  were eliminated from these images, however, compared to the  $\sim 400 \mu\text{m}$  particles those  
773 smaller than  $100 \mu\text{m}$  were significantly less abundant (results not shown).

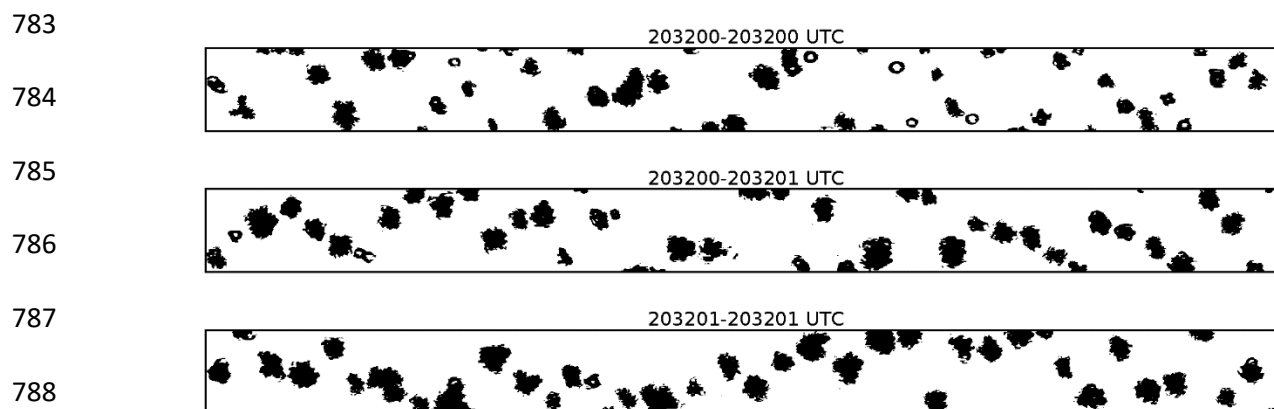
774



775 (a)



782 (b)



790 Figure 11 – (a) 2DP particle imagery from 15 December 2016. The height of the strips is 6400  
791  $\mu\text{m}$ . These particles are estimated to be representative of those that fell from flight level toward  
792 the hotplate. (b) 2DS particle imagery from 3 January 2017. The height of the strips is 1280  $\mu\text{m}$ .  
793 These particles are estimated to be representative of those that fell from flight level toward the  
794 hotplate.

795

### 796 3.7 – S/Z Relationships

797 Our S/Z pairs are presented in Table 6 where the indexes ( $i = 0$  and  $i = 1$ ) are used to  
798 indicate results derived for the averaging intervals. In the penultimate column of Table 6,  
799 reflectivities are not corrected for attenuation, however, in the last column of Table 6 and in Fig.  
800 12, the attenuation-corrected reflectivities are presented. Reflectivities from the penultimate  
801 column of Table 6, attenuations from Table 4, and Eq. 1 were used to calculate the corrected  
802 reflectivities. Also shown in Fig. 12 (black filled circles) is a subset of the S/Z pairs from PV11's  
803 Fig. 11 ( $0.01 < Z < 10 \text{ mm}^6 \text{ mm}^{-3}$ ) and the PV11 best-fit line (black). Results from PV11 are  
804 specified as  $S(\rho_1)/Z$  because those authors applied the lower of two density-size functions ( $\rho_1$ ),  
805 and the lower of two fall speed-size functions, with airborne measurements, in calculations of  
806 snowfall rates (Sect. 1 and Table 1).

807 THIS FIGURE WAS REVISED IN REVISION3.

808

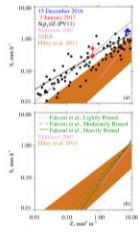
809

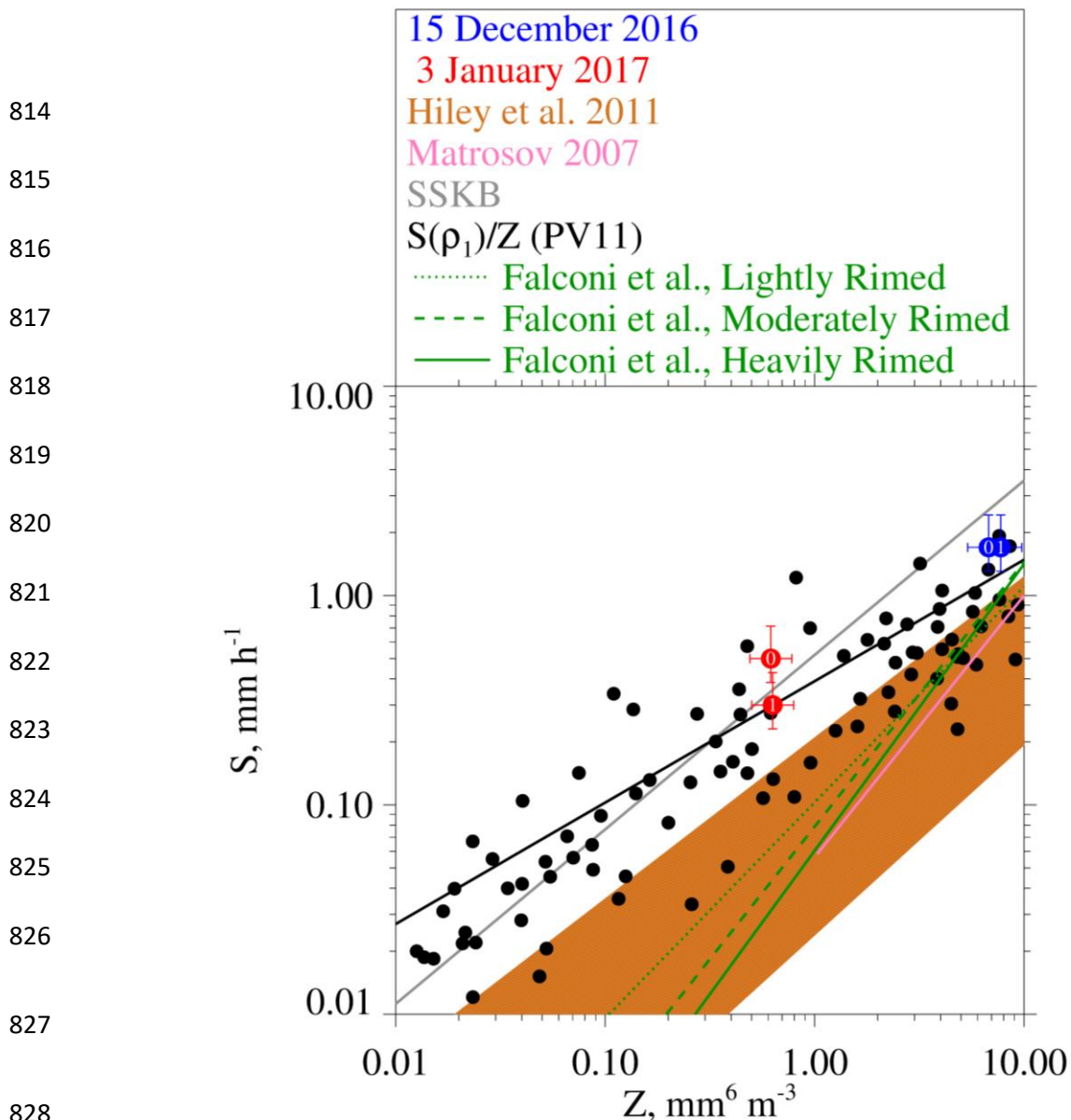
810

811

812

813





829 Figure 12 – Snowfall rate versus radar reflectivity. Red and blue circles are plotted at  
 830 attenuation-corrected reflectivities (Table 6) for the  $i = 0$  and  $i = 1$  averaging intervals. Error  
 831 bars on these points represent precisions of the reflectivity (Sect. 2.3) and snowfall rate (Sect.  
 832 2.4) measurements. Also plotted are the  $S/Z$  relationship lines from Sect. 1 and Table 1. These  
 833 are the  $S/Z$  lines defining the swath of  $S/Z$  relationships from Hiley et al. (2011), the  $S/Z$   
 834 relationship from Matrosov (2007), the  $S/Z$  relationship abbreviated SSKB, PV11’s best-fit line,  
 835 and the  $S/Z$  relationships from Falconi et al. (2018) (their Table 2). The  $S(\rho_1)/Z$  points (black  
 836 filled circles) are a subset from PV11’s Fig. 11 ( $0.01 < Z < 10 \text{ mm}^6 \text{ mm}^{-3}$ ).

837           There are two potential biases in the values of snowfall rate we tabulate (Table 6) and  
838 plot (Fig. 12). First, the two snowfall events had flight-level vertical wind velocities (Figs. 5b  
839 and 5d) that were positive (upward) upwind of the ridgeline, and vice versa downwind of the  
840 ridgeline. Except for the strongest downdraft on 3 January 2017, the magnitude of this variance  
841 is  $\sim 1 \text{ m s}^{-1}$  (Figs. 5b and 5d). Assuming  $1 \text{ m s}^{-1}$  was the downward wind immediately over the  
842 hotplate, the snow particles would have approached the HP gauge faster than their fall speed.  
843 Our basis for stating this is fall speeds for the mode sizes discussed in Sect. 3.6 (1600 and 400  
844  $\mu\text{m}$ ) and our assumption that the particles were graupel. (Table 7 has these characteristic sizes  
845 and fall speeds.) However, the conjectured downdraft speed is likely an overestimate - because  
846 of divergence occurring as the draft approached the surface - and because the sizes in Table 7  
847 likely underestimate what fell to the hotplate. Relevant to the last of these assertions, we used the  
848 altitude/T/RH measurements (Table 3) to calculate the vertical distance available for growth via  
849 riming, and thus for a fall speed increase, between the flight level and the lifted condensation  
850 level. Assuming an adiabatically-stratified liquid cloud and unit collection efficiency (these  
851 assumptions overestimate growth by riming), and no change of particle cross-section  
852 (underestimates growth by riming), our calculations indicate that relative increases of size and  
853 fall speed were 40 and 20 %, respectively, on 3 January 2017, and that these relative increases  
854 were a factor-of-two larger on 15 December 2016.

855

856 Table 7 – Estimates of snow particle fall speed

Date	Mode Size, $\mu\text{m}$	Assumed Particle Type	Fall Speed, $\text{m s}^{-1}$	Reference
15 December 2016	1600	graupel	1.4	PV11; assuming $\rho_1$ in their Fig. 5
3 January 2017	400	graupel	0.7	PV11; assuming $\rho_1$ in their Fig. 5

857

858

859           Second, there is concern that values of  $S$  from 3 January 2017 are underestimated.  
860   Although values of  $S$  must be  $> 0$ , we presented 1 Hz values (gray points, Fig. 8) approaching -  
861    $0.3 \text{ mm h}^{-1}$ . Negative values resulted because we did not impose a threshold of  $0 \text{ mm h}^{-1}$  on the  
862   uncorrected snowfall rates (this thresholding is discussed in Z18) and because negative snowfall  
863   rate values (uncorrected for catch inefficiency) are amplified by the gauge-catch correction (Sect.  
864   2.4). The implication is that  $0.2 \text{ mm h}^{-1}$  could be added to the one-minute averaged values of  
865   snowfall rate in Table 6 and in Fig. 12. Here, the assumption is that an averaged  $S$  of  $-0.2 \text{ mm h}^{-1}$ ,  
866   in Fig. 8, indicates no snowfall at the hotplate; however, because the hotplate was operated  
867   autonomously (Sect. 2.1) we have no way to verify the assumption.

868

#### 869 4 – Results

870 Figure 12 shows our four snowfall rate/reflectivity pairs (red and blue circles) after the  
871 reflectivities were corrected for attenuation. The error bars on these data pairs represent the  
872 precision of the  $Z$  measurement (Sect. 2.3) and the precision of the  $S$  measurement (Sect. 2.4).  
873 Presentation clarity was what guided the selection of  $S$  and  $Z$  axis ranges in this figure but with  
874 the consequence that 32 of PV11's  $S/Z$  pairs are not shown because they plot at  $Z > 10 \text{ mm}^6 \text{ m}^{-3}$ .  
875 The way that the PV11 data pairs scatter closest to  $Z = 10 \text{ mm}^6 \text{ m}^{-3}$ , combined with the fact that  
876 the PV11 data pairs at  $Z > 10 \text{ mm}^6 \text{ m}^{-3}$  are not shown, could lead to the interpretation that the  
877 slope describing the best-fit relationship, at  $Z$  approximately  $> 2 \text{ mm}^6 \text{ m}^{-3}$ , should be decreased  
878 relative to the actual slope of the PV11 best-fit line. Readers who view PV11's Fig. 11 will  
879 conclude that this interpretation is not warranted.

880 As is discussed in Sect. 1, computation-based W-band  $S/Z$  relationships have inputs from  
881 parameterized descriptions of density, shape, fall speed, PSD, and particle size. The  
882 computation-based  $S/Z$  relationships are in the top three rows of Table 1; the subsequent two  
883 rows of Table 1 have  $S/Z$  relationships that resulted from a hybridization of measurements and  
884 calculations (PV11 and Falconi et al. 2018).

885 We now compare our snowfall rates (fourth column of Table 6) to snowfall rates where  
886 they plot on an  $S/Z$  relationship line evaluated at one of our attenuation-corrected reflectivities.  
887 The departure between these is reported as a relative  $S$  difference expressed as  $|(S_{\text{HP}}-S)|/S$  where  
888  $S_{\text{HP}}$  is from Table 6 and where  $S$  is on an  $S/Z$  relationship line. All possible comparisons are  
889 presented graphically in Fig. 12. Table 1 has both the minimum relative  $S$  differences and the  
890 salient maximum relative  $S$  differences. The comparisons will be discussed in the order of  
891 presentation in Table 1.



892 In comparisons of our snowfall rates and the upper-limit S/Z relationship line from Hiley  
893 et al. (2011) the relative difference is no smaller than 0.7 and 1.0 on 15 December and 3 January,  
894 respectively. These minimum relative differences exceed the hotplate precision (Sect. 2.4) by at  
895 least a factor of two. It is concluded that our paired values of undercatch-corrected precipitation  
896 rate and attenuation-corrected radar reflectivity provide evidence that a calculation of S based on  
897 the Hiley et al. (2011) upper-limit, when applied to rimed snow particles, is associated with a  
898 low-biased estimate of S. A retrieval based on Hiley et al.'s average S/Z relationship (not  
899 shown), which bisects the orange region in Fig. 12, corresponds to an even larger low bias. This  
900 is a concern because Hiley et al. (2011) used their average S/Z relationship to retrieve global  
901 snowfall distributions and since global observations reported in Wang et al. (2013) document the  
902 frequent occurrence of supercooled liquid within snowing clouds.

903 Figure 12 shows the separation between our measurements and the Matrosov (2007)  
904 calculation. The separation is about a factor of two (minimum relative difference = 1.4) for the  
905 points obtained on 15 December 2016 and corresponds to an underestimation of S (low bias)  
906 when compared to our measurements. The points from 3 January 2017 plot at an attenuation-  
907 corrected reflectivity smaller than the lower-limit of the calculation (Matrosov 2007). Since the  
908 particle images (Fig. 11a-b) reveal no evidence of the particle type modeled by Matrosov (2007)  
909 (aggregates), it is not surprising that the Matrosov S/Z relationship is not representative of our  
910 measurements.

911 One plausible reason for the low bias discussed in the previous two paragraphs is the  
912 smaller density implicit in most computationally-based S/Z relationships and especially those  
913 which assume that snow particles are crystals. Densities are quite different for crystals versus  
914 that for rimed snow particles. For example, in Brown and Francis (1995), assuming a 2 mm

915 crystal, the density is  $\sim 30 \text{ kg m}^{-3}$ , whereas in PV11 (their Eq. 1), assuming a 2 mm graupel  
916 particle, the density is  $\sim 200 \text{ kg m}^{-3}$ . Because aggregates are collections of crystals, this  
917 comparison of crystal and graupel densities also seems relevant to a comparison of graupel and  
918 aggregate snow particle densities.

919 Figure 12 compares our  $S_{HP} / Z'$  data pairs to the SSKB S/Z relationship line and Table 1  
920 presents the relative differences between the data pairs and the SSKB line. Compared to the S/Z  
921 relationship represented by the top of the orange region in Fig. 12, and compared to the Matrosov  
922 2007 relationship, the SSKB line plots closer to our data points (minimum relative difference  $\sim$   
923 0.3). We note that the only instances of  $S_{HP} < S$  are three of four comparisons of our  
924 measurements to the SSKB relationship. A possible reason for this is that the density applied in  
925 SSKB (Table 1) is not entirely representative of conditions during our study. An analysis of the  
926 sensitivity of the SSKB to a change in density is needed to investigate our assertion.

927 Comparisons of our  $S_{HP} / Z'$  data pairs and PV11's best-fit line are also in Table 1. The  
928 table demonstrates that the agreement is reasonable - minimum relative difference no larger than  
929 0.3 – and Fig. 12 shows that our data pairs plot at or above the PV11 best fit line.

930 Based on data from PV11 and our  $S_{HP} / Z'$  data pairs, as well as the S/Z relationship  
931 abbreviated SSKB, it is expected that the S/Z relationships reported by Falconi et al. (2018) for  
932 rimed snow particles (Sect. 1) would plot higher in S-versus-Z space than is illustrated in Fig. 12.  
933 Notably, only the upper-end of the Falconi et al. lines (i.e., at  $Z > 8 \text{ mm}^6 \text{ m}^{-3}$ ) plot above the  
934 upper-limit that Hiley et al. (2011) developed for unrimed snow particles. A plausible  
935 explanation for the lower-than-expected S/Z relationships of Falconi et al. is now offered.  
936 Falconi et al. used liquid water path as a proxy for the extent of snow particle riming (von Lerber

937 et al. 2017). A consequence may have been that the proxy did not dependably exclude unrimed  
938 snow particles (crystals and aggregates) from the riming categories of Falconi et al. If this was  
939 the case, then the data groupings that were the basis for the Falconi et al. S/Z relationships may  
940 have been affected. When applying the heavily-rimed S/Z relationship of Falconi et al. with our  
941  $S_{HP} / Z'$  data pairs we find that the minimum relative differences are 0.6 (December 15) and 8.5  
942 (January 3) (Table 1). Additionally, the differences are 0.5 (December 15) and 5.9 (January 3)  
943 when applying the moderately-rimed S/Z relationship of Falconi et al. (results not shown).  
944 Further research is needed to resolve the reason for the mismatch between the snowfall  
945 rate/reflectivity pairs reported here and the S/Z relationships reported in Falconi et al.

946 Our conclusion that the upper-limit S/Z relationship from Hiley et al. (2011)  
947 underestimates S would be modified if our WCR-derived reflectivities were negatively biased.  
948 Assuming the reflectivities are negatively biased by 2.5 dBZ, the minimum relative differences  
949 discussed previously are no smaller than 0.1 and 0.3 on 15 December and 3 January,  
950 respectively. A bias in reflectivity of this magnitude cannot be ruled out but neither can a  
951 positive bias of the same magnitude (Sect. 2.3). The latter increases the minimum relative  
952 differences to 1.6 and 2.2 on 15 December and 3 January, respectively. In each of these  
953 calculations we have summed the attenuations (Table 4) with  $\pm 2.5$  dBZ and used Eq. 1 to  
954 calculate error-perturbed reflectivities.

955 The scatter of measurements in Fig. 12, the plausibility of a -2.5 to +2.5 dBZ bias in  
956 WCR reflectivity measurements, and error in measurement of S (Sect. 2.4), indicate that refined  
957 techniques will be needed in future investigations which apply the approach described here.  
958 Taking into consideration the goal of evaluating snowfall rates from space, some advance in  
959 satellite remote sensing also seems warranted. One issue is diagnosing where riming is occurring

960 within clouds. Both lidars and radiometers can sense supercooled liquid water from space (e.g.,  
961 Battaglia and Panegrossi, 2020), and if combined with Doppler radars operating at multiple  
962 wavelengths, can diagnose precipitation attributable to rimed snow particles. Despite limitations  
963 of the multiple-wavelength Doppler method, for example in scenarios with vertical air speed  
964 comparable to and larger than particle fall speed (Vogl et al. 2022), the method has been  
965 validated in ground-based field studies (Kneifel et al. 2015; Mason et al. 2018). Technical  
966 challenges also remain for implementing the method from space (Battaglia et al. 2020).

## 967 **5 – Conclusions**

968 We have reported surface measurements of  $S$  and near-surface measurements of  $Z$ . The  
969 latter came from overflights of a ground site, where a precipitation gauge was operated, and were  
970 acquired using an airborne W-band radar. The values of  $Z$  were corrected for attenuation.

971 The reported  $S_{HP} / Z'$  pairs plot at or above the  $S$ -versus- $Z$  best-fit line of PV11 (Fig. 12)  
972 and the minimum relative  $S$  difference (Table 1) is no larger than 0.3. The PV11 data came from  
973 airborne measurements of W-band reflectivity, acquired within  $\pm 100$  m of flight level, and from  
974 coincident measurements of snow particle imagery. PV11 used a density-size function and a fall  
975 speed-size function, and measurements (PSD and particle images) to calculate  $S$  for snow  
976 particles that were classified as both rimed crystals and graupel. This classification is also  
977 consistent with the particle imagery we have presented (Fig. 11).

978 We have documented a substantial difference in comparisons between our snowfall rates  
979 and reflectivity-dependent  $S$  values calculated using an upper-limit  $S/Z$  relationship for unrimed  
980 snow particles (Hiley et al. 2011). Here the minimum relative  $S$  differences are 0.7 and 1.0 for  
981 our two overflights and in a comparison to our measurements correspond to an underestimation

982 of snowfall rate (Fig. 12). The relative differences are approximately a factor of two larger than  
983 the precision of our snowfall rate measurement. We also report a substantial difference, and S  
984 underestimation compared to our measurements (Fig. 12), for the comparison made to an S/Z  
985 relationship which assumes the snow particles are aggregates (Matrosov 2007). The snowfall rate  
986 underestimates obtained using both Hiley et al.'s and Matrosov's S/Z relationships (Fig. 12) are  
987 perhaps expected given that the density factored into those S/Z calculations is small compared to  
988 that for rimed snow particles. It is also expected that the larger density and spherical shape  
989 applied in the SSKB S/Z relationship contributed to the better agreement (minimum relative  
990 difference  $\sim 0.3$ ) with our  $S_{HP} / Z'$  pairs. Our conclusion is that some snowfall retrievals (e.g.,  
991 Hiley et al. 2011) will underestimate S for weather targets containing rimed snow particles. We  
992 also state that our conclusion is at odds with measurements and analysis in Falconi et al. Those  
993 researchers reported S/Z relationships for rimed snow particles which in instances with  $Z < 8$   
994  $\text{mm}^6 \text{m}^{-3}$  plot below the upper-limit of Hiley et al. (Fig. 12). The consequence is that the  
995 minimum relative S difference in our comparison to Falconi et al. (assuming Falconi et al.'s  
996 heavily-rimed classification) is comparable to and larger than in our comparison to the Hiley et  
997 al.'s upper-limit S/Z relationship.

998         New research is needed to refine the S/Z relationship for rimed snow particles. This could  
999 be computational – e.g., investigation of the utility of parameterizing S in terms of both Z and  
1000 density – or could be observational. Unlike the investigation of PV11, where only an airborne  
1001 platform was employed, we have demonstrated that useful information can be obtained using  
1002 coordinated ground-based and airborne systems. Another approach would be with only ground-  
1003 based instrumentation. This would avoid some of the complications encountered in this study,  
1004 including W-band attenuation and a reliance on particle imagery acquired aloft. A study with

1005 both ground-based and airborne systems would also be useful for understanding an S/Z  
 1006 mismatch apparent at  $Z < 8 \text{ mm}^6 \text{ m}^{-3}$ . Elements of the mismatch are the measurements reported  
 1007 here, PV11's best-fit line, and the measurement-based S/Z relationships reported by Falconi et al.  
 1008 (2018). These three research teams reported measurements relevant to the development of an S/Z  
 1009 relationship for rimed snow particles.

## 1010 **6 – Appendix**

1011 This appendix explains how HP (hotplate) and WCR (Wyoming Cloud Radar) averages  
 1012 were evaluated. The scheme starts with an HP averaging interval (duration 60 s) and derives a  
 1013 WCR averaging interval and a WCR averaging domain. The latter encompasses a subset of the  
 1014 altitude-time cross-section sampled by the WCR. The top boundary of the domain was derived  
 1015 using vertical-component Doppler velocities within the interval/domain. Because of this  
 1016 dependence, the line defining the top boundary was derived iteratively.

1017 With the overflight time symbolized  $t_0$ , the beginning and ending times of two 60-second  
 1018 HP averaging intervals are

$$1019 \quad t_{HP,B} = t_0 \quad (\text{A1})$$

$$1020 \quad t_{HP,E} = t_0 + 60 \quad (\text{A2})$$

1021 Since two adjacent HP averaging intervals are evaluated in this analysis, we express the  
 1022 averaging times with the following recursive equations

$$1023 \quad t_{HP,B}(i) = t_0 + i \cdot 60 \quad (\text{A3})$$

1024 and

$$1025 \quad t_{HP,E}(i) = t_0 + (i+1) \cdot 60. \quad (\text{A4})$$

1026 In Eqs. A3-A4 the index is  $i \in \{0, 1\}$ . A special case with  $i = 2$  is also analyzed (Sect. 3.5).

1027 Analogous to the recursion in Eq. A4, the ending time of a WCR averaging interval is

$$1028 \quad t_{WCR,E}(i) = t_O - i \cdot 60 \cdot v_w / gs. \quad (A5)$$

1029 Here  $v_w$  is a wind advection speed (discussed below) and the second term on the rhs is a wind

1030 advection distance divided by the WKA (Wyoming King Air) ground speed ( $gs$ ). Analogous to

1031 the Eq. A5, the beginning time of a WCR averaging interval is

$$1032 \quad t_{WCR,B}(i) = t_{WCR,E} - (i+1) \cdot 60 \cdot v_w / gs \quad (A6)$$

1033 The wind advection speed ( $v_w$ ) in Eqs. A5-A6 was calculated using an altitude-

1034 dependent west-to-east wind velocity ( $u$ ) and an altitude-dependent south-to-north wind velocity

1035 ( $v$ ). These altitude-dependent component velocities were calculated using the horizontal wind

1036 vectors in the penultimate and last columns of Table 3. Plots of the component velocities versus

1037 altitude and the linear functions used to relate component velocities to altitude are presented in

1038 Figs. A1a-b.

1039 An altitude ( $z' = 3400$  m) was assumed for evaluating the horizontal wind advection

1040 vector. This is the altitude of the ridges west and northwest of the HP site (Figs. 3a-b).

1041 The WKA track vector (Table 3) defines the vertical plane of the WCR measurements.

1042 We assumed that wind advection of snow particles occurred parallel to this vector. With the

1043 assumption stated in the previous paragraph, the horizontal wind advection speed ( $v_w$ ) was

1044 calculated as the projection of the horizontal wind vector onto the track vector.

$$1045 \quad v_w = \frac{u(z') \cdot gs_x + v(z') \cdot gs_y}{(gs_x^2 + gs_y^2)^{1/2}} \quad (A7)$$

1046 In Eq. A7 the west-to-east and south-to-north components of the track vector are symbolized  $gs_x$   
 1047 and  $gs_y$ . Vector representations of the track vector are in Table 3. On 14/15 December 2016 and  
 1048 3 January 2017, the values of  $v_w$  are 7.4 and 8.9 m s<sup>-1</sup>, respectively.

1049 In addition to the properties  $gs$  and  $v_w$  used to evaluate Eqs. A5-A6, a WCR averaging  
 1050 interval/domain was evaluated using a snow particle downward speed (Eq. A8).

$$1051 \quad v_p = |\langle V_D \rangle| + \sigma_{V_D} \quad (\text{A8})$$

1052 Here,  $\langle V_D \rangle$  is the average of Doppler velocities within an averaging interval/domain,  
 1053  $|\langle V_D \rangle|$  is the absolute value of the average, and  $\sigma_{V_D}$  is the standard deviation of the average.

1054 On both the lhs and rhs of Eq. A8, all terms are greater than zero.

1055 We interpret  $v_p$  as the maximum likely snow particle speed toward the ground. There are  
 1056 three reasons for this: 1) For the WCR averaging intervals/domains we analyzed, values of  
 1057  $\langle V_D \rangle$  were consistently less than zero (Table 6). This indicates that snow particles (on  
 1058 average) were moving toward the ground. 2) Again, for the WCR averaging intervals/domains  
 1059 we analyzed,  $\sigma_{V_D}$  was comparable to  $|\langle V_D \rangle|$ . This indicates that turbulent eddies transported  
 1060 snow particles upward and downward at a speed comparable to their downward speed in still air.  
 1061 3) The  $V_D$  are reflectivity weighted (Haimov and Rodi 2013) and are thus indicative of the  
 1062 motion of the largest particles within an averaging interval/domain.

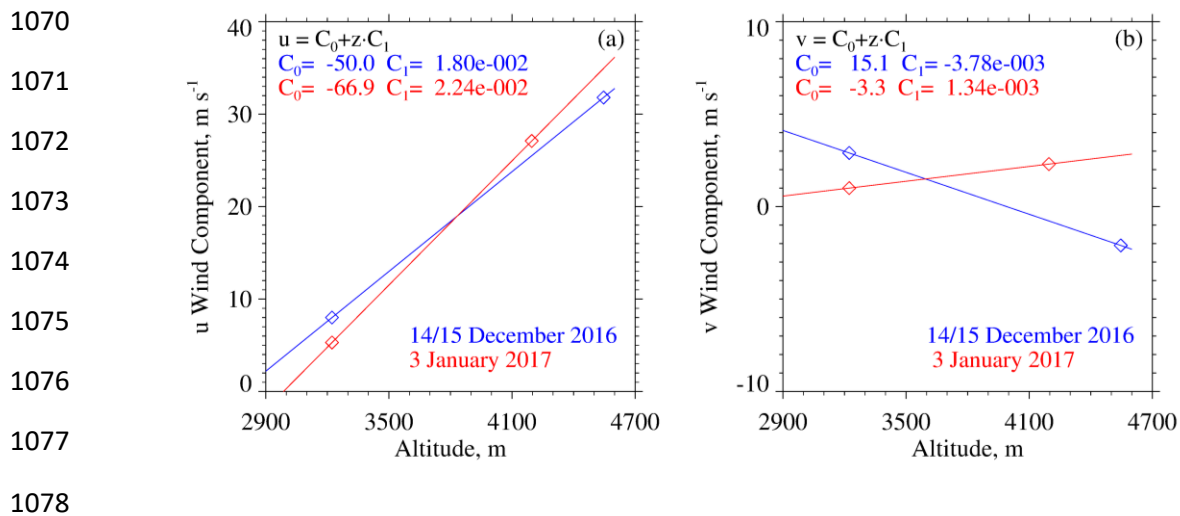
1063 We now focus on the top boundary of a WCR averaging interval/domain. Figures 6b and  
 1064 6d have representations of the boundary. The slope defining this boundary was calculated as  
 1065  $-v_p \cdot gs / v_w$ . That is, particles below this boundary moved downward sufficiently fast and  
 1066 horizontally sufficiently slow to advect reasonably close to the hotplate. Starting with diagnosed



1067 values of  $gs$  and  $v_w$ , the values of  $v_p$  and slope, were derived iteratively. The precision of the

1068 derived  $v_p$  is  $\pm 0.1 \text{ m s}^{-1}$ .

1069



1079 Figure A1 – (a) West-to-east ( $u$ ) wind velocity derived using measurements from the WKA and  
 1080 the AmeriFlux (AF) tower. Also shown is the linear function used to relate  $u$  to altitude. (b)  
 1081 South-to-north ( $v$ ) wind velocity derived using measurements from the WKA and AF. Also  
 1082 shown is the linear function used to relate  $v$  to altitude. WKA and AF velocities are presented as  
 1083 vectors in the penultimate and last columns of Table 3.

1084

1085 Data Availability. The WKA and WCR measurements can be obtained from the SNOWIE data  
1086 archive of NCAR/EOL, which is sponsored by the National Science Foundation. Hotplate gauge  
1087 measurements are at <https://doi.org/10.15786/20103146>. The US-GLE AmeriFlux measurements  
1088 are at <https://ameriflux.lbl.gov/>. The Brooklyn Lake SNOTEL gauge measurements are at  
1089 <https://www.wcc.nrcs.usda.gov/snow/>. Merged Hotplate, SNOTEL, and AmeriFlux data  
1090 sequences from 14/15 December 2016 and 3 January 2017 are in Snider (2023).

1091

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1096

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1104

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