

1 **W-band S/Z Relationships for Rimed Snow Particles: Observational Evidence from**
2 **Combined Airborne and Ground-based Observations**

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13 Abstract

14 Values of undercatch-corrected liquid-equivalent snowfall rate (S) at a ground site and
15 microwave reflectivity (Z) retrieved using an airborne W-band radar were acquired during
16 overflights. The temperature at the ground site was between -6 and -15 °C. At flight level, within
17 clouds containing ice and supercooled liquid water, the temperature was approximately 7 °C
18 colder. Additionally, airborne measurements of snow particle imagery were acquired. The
19 images demonstrate that most of the snow particles were rimed, at least a flight level. A
20 relatively small set of S/Z pairs (4) are available from the overflights. Important distinctions
21 between these measurements and those of Pokharel and Vali (2011), who reported S/Z pairs and
22 an S/Z relationship for rimed snow particles, are 1) the fewer number of S/Z pairs, 2) the method
23 used to acquire S , and 3) the altitude, relative to ground, of the W-band Z retrievals. This
24 analysis corroborates that the S/Z relationship reported in Pokharel and Vali (2011) yields an S -
25 in scenarios with snowfall produced by riming - substantially larger than that derived using an
26 S/Z relationship developed for unrimed snow particles.

27

28

29 1 - Introduction

30 Improvement of methods used to measure snowfall and rainfall are an ongoing focus of
31 meteorological research. The various methods are ground-based instruments that evaluate the
32 mass of precipitation that falls into or onto a collector (precipitation gauges) (Brock and
33 Richardson 2001), ground-based radars (Wilson and Brandes 1979), and airborne and space-
34 borne radars (Matrosov 2007; Kulie and Bennartz 2009; Geerts et al. 2010; Skofronick-Jackson
35 et al. 2017). An objective of these approaches, whether used to make observations independent
36 of other methods (e.g., Kulie and Bennartz 2009), or as a component of multiple observations
37 (e.g., Cocks et al. 2016), is estimation of precipitation rate and accumulated precipitation amount

38 Many studies have investigated using radar for evaluating rainfall (for a review see
39 Wilson and Brandes 1979). There are two approaches. The first is research, both observational
40 and computational, that probes the relationship between rainfall rate (R) and radar-measured
41 values of range-corrected backscattered microwave power. The latter is commonly reported as an
42 equivalent radar reflectivity factor (Z_e). The second is operational in the sense that precipitation
43 gauges are used to calibrate measurements acquired using weather surveillance radars.
44 Complications associated with converting Z_e to R, or converting a radar reflectivity factor¹ (Z) to
45 R, can be grouped in four categories: 1) Inaccuracy in quantification of Z, 2) variation of the
46 R/Z relationship stemming from precipitation processes (e.g., coalescence and break up), 3)
47 difference between the volume of a radar range gate versus the much smaller volume of
48 atmosphere sampled as precipitation falls to a gauge, and 4) vertical displacement between a
49 radar range gate and a calibrating gauge, especially at far ranges.

¹ Radars are calibrated to report Z_e (Smith 1984). Herein, radar reflectivities are reported as $Z = Z_e$ and as $\text{dBZ} = 10\log_{10}(Z_e)$.

50 For situations with snowfall, methods employing either gauge or radar are associated
51 with complications beyond that incurred in rainfall (Matrosov 2007; Martinaitis et al. 2015;
52 Cocks et al. 2016). Problems associated with gauge measurements are wind-induced snow
53 particle undercatch, gauge capping, delayed registration, and blowing snow aliasing as snowfall.
54 Moreover, in a situation with snow particles more abundant within a radar range gate, compared
55 to rain drops, and where a measurement of Z is used to infer R via a R/Z relationship, the
56 resultant precipitation rate will likely be inaccurate. This is because hydrometeor shape, density,
57 and dielectric properties are all variable for snow particles while relatively invariant for rain
58 drops. Additionally, a snow particle's terminal fall speed varies with size (as is the case for
59 drops) and with particle shape and particle density. Going forward, we refer to the latter two
60 properties as shape and density.

61 The goals of this paper are as follows: 1) to describe measurements of undercatch-
62 corrected liquid-equivalent snowfall rate (S , mm h^{-1}) and how these were paired with W-band
63 measurements of reflectivity (Z , $\text{mm}^6 \text{m}^{-3}$); 2) to contrast the S/Z pairs against S/Z relationships
64 commonly applied in radar retrievals of S ; and 3) to investigate why the S/Z pairs deviate from
65 predictions of some S/Z relationships.

66 In calculations of paired values of S and Z , density is an important parameter. Density is
67 commonly estimated using empirical data (e.g., Pokharel and Vali 2011, [PV11]). For graupel, a
68 snow particle that grows via collection of supercooled cloud droplets in a process commonly
69 referred to as riming, paired observations of particle mass and particle size have been used to
70 estimate density. There is considerable uncertainty in this approach. Based on data collected at
71 two northwestern US surface sites (Zikmunda and Vali 1972; Locatelli and Hobbs 1974), density
72 values differ by at least a factor of two at particle sizes smaller than $2000 \mu\text{m}$ (PV11; their Fig.

73 4). Given that the density of rime ice varies with droplet impact speed, droplet size, and
74 temperature (Macklin 1962), it is not surprising that the density-size relationships analyzed by
75 PV11 are so varied.

76 Table 1 and the following paragraphs overview W-band S/Z relationships applied in
77 instances with snow particles grown by vapor deposition (crystal), by collection of crystals
78 (aggregate snowflake), and by riming (rimed crystal and graupel). Henceforth, the latter two
79 snow particle types are collectively referred to as rimed snow particles.

80 In a computational study, Hiley et al. (2011) considered a variety of snow particle types
81 (column, plate, bullet rosette, sector plate, dendrite, and aggregate snowflake), employed a
82 parameterized ice particle size distribution (PSD) function (Field et al. 2005), accounted for a
83 range of temperature (-5 to -15 °C) via the Field et al. parameterization, and developed a range of
84 S/Z relationships for snow particles. Except for the aggregate snowflakes (henceforth,
85 aggregates), the modeled particle types were vapor-grown crystals. Hiley et al.'s upper- and
86 lower-limit relationships are $S = 0.21 \cdot Z^{0.77}$ and $S = 0.024 \cdot Z^{0.91}$, respectively. Matrosov (2007)
87 developed an S/Z relationship for aggregates. In that work, parameterized PSDs from Braham
88 (1990) were employed, and a range of particle aspect ratios were factored into the calculations.
89 For aggregates, the S/Z relationship is $S = 0.056 \cdot Z^{1.2}$ (Matrosov 2007). It should be noted that
90 Hiley et al. (2011) and Matrosov (2007) employed similar, but not identical, computational
91 methods. Computational research was also conducted by Kulie and Bennartz (2009) who
92 adopted the wavelength-dependent density derived by Surussavadee and Staelin (2007) (200 kg
93 m^{-3} at $\lambda = 3.2 \text{ mm}$), modeled the snow particles as spheres, and applied PSDs based on Field et
94 al. The resultant S/Z is $S = 0.52 \cdot Z^{0.83}$ (Surussavadee and Staelin 2007; Kulie and Bennartz 2009;
95 henceforth, SSKB). Variance in the calculations discussed in this paragraph originate from

96 changes in density, shape, fall speed, PSD, and particle size as these changes are propagated
97 through the cloud-microphysical and microwave-scattering calculations.

98 In a hybrid approach (computational and an analysis of measurements), PV11 concluded
99 that most of the snow particles they imaged were rimed snow particles. Values of S were
100 calculated using a density-size function (ρ_1 , discussed below), a fall speed-size function,
101 measured PSDs and measured particle images, and a determination of particle volumes. It was
102 assumed that a prolate spheroid approximated particle shape and that shape was the basis for
103 determining a particle's sphere-equivalent volume and the particle's sphere-equivalent size. The
104 sphere-equivalent size was applied in the two functions. Values of Z were calculated using a
105 measured PSD, sphere-equivalent sizes, the ρ_1 function, and Mie Theory. PV11 presented
106 calculations of Z , obtained using two density-size relationships (their Eqs. 1 and 2) and compared
107 their calculated reflectivities to measurements of Z from a W-band radar. That led to their
108 conclusion that "...the lower density assumption...yielded closer correspondence to observed
109 reflectivities." Their recommendation for S as a function of measured Z - hereafter the $S(\rho_1)/Z$
110 best-fit line - is $S = 0.39 \cdot Z^{0.58}$. Values of Z that were paired with the calculated values of S (i.e.,
111 the S/Z pairs from PV11 that we present in Sect. 4), and that were used to determine the $S(\rho_1)/Z$
112 best-fit line, came from the W-band radar. In addition to variance in their values of S , coming
113 from a dependence on density, PV11 state that a value of S derived via their best-fit line is
114 uncertain by a factor-of-ten. That uncertainty is evident in the variance of S/Z data pairs about
115 the $S(\rho_1)/Z$ line in Fig. 11 of PV11. Those investigators, and Geerts et al. (2010), attributed the
116 variance to use of two-dimensional snow particle images in calculations of S and to actual
117 variations of density, shape, and particle size not accounted for in the calculations.

118 Another set of hybrid-type S/Z relationships was developed by Falconi et al. (2018; their
119 Table 2). These are based on measurements from a video disdrometer, weighing precipitation
120 gauge, microwave radiometer, and a vertically-pointing W-band radar. All these systems were
121 operated at the ground. The data set was stratified into intervals of lightly-rimed, moderately-
122 rimed, and heavily-rimed snow. A proxy for snow particle riming - radiometer measurements of
123 liquid water path – was the basis for the stratifications (von Lerber et al. 2017). The S/Z
124 relationships are $S = 0.10 \cdot Z^{1.0}$ (lightly-rimed), $S = 0.079 \cdot Z^{1.3}$ (moderately-rimed), and $S =$
125 $0.060 \cdot Z^{1.4}$ (heavily-rimed).

126 Our focus is on surface measurements of S and on pairing of those measurements with
127 airborne measurements of Z. We also analyze airborne measurements of snow particle imagery.
128 The latter demonstrate that the particles observed at flight level were rimed. The imagery is the
129 basis for our assertion that our data set is relevant to ongoing investigations of using Z to
130 evaluate S in situations where precipitation is produced by riming.

131 Section 2 describes the setting of our study, the instruments we deployed, and recordings
132 we obtained using two data acquisition systems. One of the data systems was operated at a
133 ground site and the other on an aircraft. Section 3 is an analysis of the recordings; this section
134 also considers recordings from two additional, but ancillary, ground sites. Our findings are
135 discussed in Sect. 4 and summarized in Sect. 5. An Appendix (Sect. 6) explains how we
136 averaged recordings of near-surface W-band reflectivities and surface-based recordings of
137 snowfall.

138 Table 1 – W-band S/Z relationships from the literature, snow particle type, and values of minimum relative S difference

Reference	Abbreviation used for reference	S/Z relationship	Snow Particle Type	Minimum relative S difference on December 15 2016 ^a	Minimum relative S difference on January 3 2017 ^a
Hiley et al. (2011)	-	$S=0.21 \cdot Z^{0.77}$	Upper-limit S/Z relationship for vapor-grown crystals	0.7	1.0
Matrosov (2007)	-	$S=0.056 \cdot Z^{1.2}$	Aggregates	1.4	8.5 ^b
Surussavadee and Staelin (2007) and Kulie and Bennartz (2009)	SSKB	$S=0.52 \cdot Z^{0.83}$	Spherical snow particles with density = 200 kg m ⁻³	0.3	0.2 ^c
Pokharel and Vali (2011)	PV11	$S=0.39 \cdot Z^{0.58}$	Rimed snow particles assuming the lower of two density-size relationships	0.3	0.0 ^d
Falconi et al. (2018)	-	$S=0.060 \cdot Z^{1.4}$	Snow particles classified as heavily rimed	0.6 ^e	8.5

139

140 ^a Minimum relative S difference is defined as the minimum of $|(S_{HP}-S)|/S$ where S_{HP} is a measurement of undercatch-corrected liquid-equivalent
 141 snowfall rate (Table 6) and S is a snowfall rate on an S/Z relationship line evaluated at one of the attenuation-corrected reflectivities (Sect. 4).

142 ^b Attenuation-corrected Z on this day (0.6 mm⁶ m⁻³) is smaller than the lower-limit Z (1 mm⁶ m⁻³) advised for this S/Z relationship (Matrosov
 143 2007).

144 ^c Maximum relative S difference on this day is 0.4.

145 ^d Maximum relative S difference on this day is 0.7.

146 ^e Maximum relative S difference on this day is 0.9.

147

148 2 - Site, Aircraft, and Instruments

149 2.1 - Site

150 Analyzed herein are aircraft and ground data from 14/15 December 2016 and from 3
151 January 2017. The ground data were acquired in a forest/prairie ecotone on the eastern slope of
152 the Medicine Bow Mountains in southeast Wyoming (Figs. 1a-b). No ground-based observers
153 were deployed during the two snowfall events analyzed.

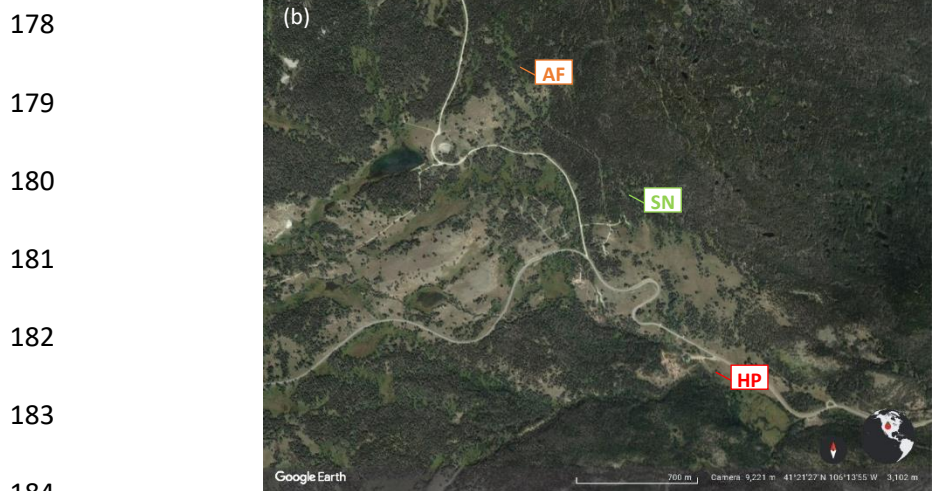
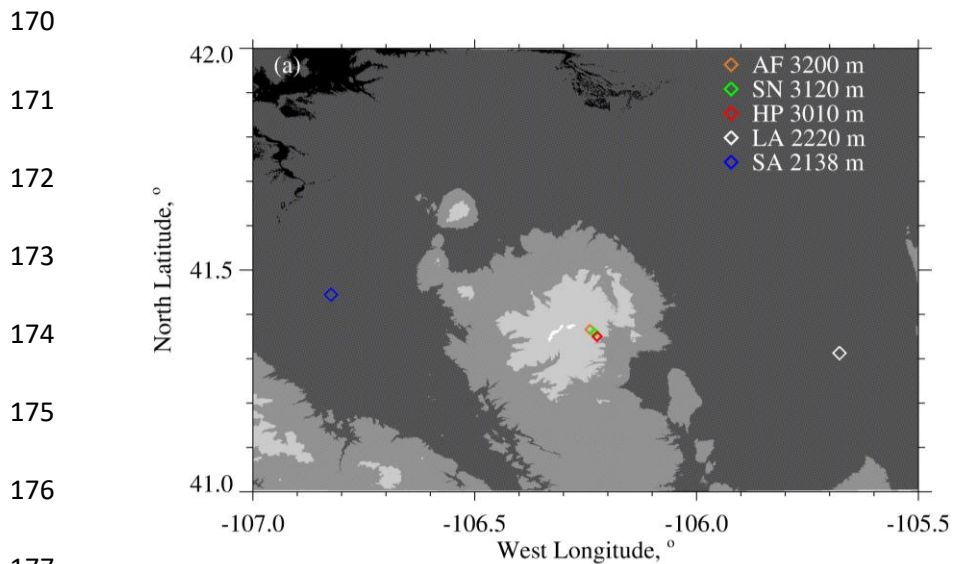
154 At one of three ground sites (HP in Figs. 1a-b) a hotplate precipitation gauge (Rasmussen
155 et al. 2011; Zelasko et al. 2018), a GPS receiver, and a data acquisition system were deployed.
156 Once per second, the data system ingested a hotplate-generated data string, combined that with
157 time-of-day from the GPS receiver [Coordinated Universal Time (UTC)], and recorded the
158 merged hotplate/UTC data string. The absolute accuracy of the time stamp is no worse than 2 s.

159 Overflights of the hotplate were done by the University of Wyoming King Air (WKA) on
160 14/15 December 2016 and on 3 January 2017. The flights were conducted in preparation for the
161 SNOWIE field project (Tessendorf et al. 2019) and were flown from the Laramie, WY Airport
162 (LA in Fig. 1a). Data acquisition on the WKA was also synchronized with UTC, but with much
163 better accuracy than at the hotplate.

164

165 Measurements of horizontal wind (speed and direction), temperature, relative humidity,
166 and pressure from the US-GLE AmeriFlux tower (AF in Figs. 1a-b) are also components the
167 analysis. The AmeriFlux data were provided to us as 30-minute averages (AmeriFlux 2021;
168 Marlow et al. 2023).

169



186 Figure 1 – (a) Southeast Wyoming, airport at Saratoga, WY (SA), airport at Laramie, WY (LA),

187 and the ground sites: AF = US-GLE AmeriFlux tower, SN = Brooklyn Lake SNOTEL, and HP =

188 hotplate. Altitudes of the airports and ground sites are in the legend. Altitude thresholds for the

189 digital elevation map are 1500, 2000, 2500, 3000, and 3500 meters. (b) Close up of the AF, SN,

190 and HP ground sites (from © Google Earth).

191

192 **2.2 - University of Wyoming King Air (WKA)**

193 The following WKA measurements were analyzed: aircraft position, temperature, snow
194 particle imagery, and three moments of the cloud droplet size distribution function. A Cloud
195 Droplet Probe (CDP; Faber et al. 2018) was the basis for the droplet size distribution
196 measurements and the derived moments. The latter are droplet concentration (N), cloud liquid
197 water content (LWC), and mean droplet diameter ($\langle D \rangle$). Snow particle imagery was obtained
198 using a precipitation particle imaging probe (2DP; Korolev et al. 2011) and a cloud particle
199 imaging probe (2DS; Lawson et al. 2006). These acquired two-dimensional images of particles
200 between 200 to 6400 μm (2DP) and between 10 to 1280 μm (2DS).

201 **2.3 – The W-band Wyoming Cloud Radar (WCR)**

202 Retrievals from the up-looking and down-looking antennas of the WCR, operated on the
203 WKA, were also analyzed. For this we used Level 2 WCR data² with reflectivities recorded as
204 $dBZ = 10 \cdot \log_{10}(Z)$. The reflectivities were converted from dBZ to Z prior to processing.
205 Additionally, values of the vertical-component Doppler velocity retrieved from below the WKA
206 using the WCR's down-looking antenna were analyzed. The Doppler velocities were corrected
207 for aircraft motion as described in Haimov and Rodi (2013). We use V_D to symbolize the
208 corrected vertical-component Doppler velocity and adopt the convention that $V_D > 0$ indicates
209 upward hydrometeor motion.

210

² http://flights.uwyo.edu/uwka/wcr/projects/snowie17/PROCESSED_DATA/

211 The Level 2 WCR sampling was different on the two flight days and this difference is
212 shown in Table 2. Ground-based calibrations of the WCR's up-looking antenna and correlations
213 between in-flight retrievals acquired using the WCR's up-looking and down-looking antennas
214 were used to estimate the precision and absolute accuracy of the WCR-derived values of dBZ.
215 These are ± 1.0 dBZ and ± 2.5 dBZ, respectively (PV11).

216

217 Table 2 – Level 2 WCR sampling and the WKA overflight time

218

Date	Level 2 WCR Vertical Sampling, m	Level 2 WCR Along-track Sampling, s	Overflight Time, UTC
14/15 December 2016	23	0.23	00:00:38 (15 December 2016)
3 January 2017	30	0.36	20:32:03

219

220

221 **2.4 - Hotplate Gauge**

222 Algorithms used to process hotplate measurements are described in Rasmussen et al.
223 (2011), Boudala et al. (2014), and Zelasko et al. (2018). Henceforth, these are referred to as R11,
224 B14, and Z18, respectively. This section describes how hotplate measurements acquired at the
225 HP site were analyzed. The hotplate deployed at the HP site is described in Wolfe and Snider
226 (2012), Z18, and in Marlow et al. (2023).

227 Five measurements fundamental to the steady state energy budget of the hotplate's
228 temperature-controlled up-viewing plate are output by the hotplate microprocessor as one-minute
229 running averages (Z18). These averages were merged with the GPS time and recorded at 1 Hz by
230 the data acquisition system (Sect. 2.1). With these measurements, calibration data (Marlow et al.
231 2023), and the algorithm developed by Z18, we calculated S in two steps. First, the five hotplate
232 measurements (electrical power supplied to the plate, ambient temperature, wind speed,
233 downwelling shortwave flux, and downwelling longwave flux) were input to Eq. 3 in Z18. The
234 output of that equation is a provisional liquid-equivalent precipitation rate. Second, the snow
235 particle catch efficiency, described in the next paragraph, was used to calculate S as the ratio of
236 the provisional rate and the catch efficiency.

237 Marlow et al. (2023; their Fig. 3b) report the relationship between snow particle catch
238 efficiency and wind speed that was applied in the calculation of S . There are three bases for this
239 relationship. First is the catch efficiencies R11 derived using measurements obtained from a
240 weighing gauge, operated within a double fence intercomparison reference shield, and collocated
241 measurements from an unshielded hotplate gauge. These paired measurements are symbolized
242 SRG (shielded reference gauge) and UHG (unshielded hotplate gauge). R11 plotted hotplate
243 catch efficiencies (i.e., UHG/SRG) versus wind speeds measured at 10 m AGL (their Fig. 8).

244 Second is Marlow et al.'s adjustment of R11's 10 m AGL wind speeds to 2 m AGL. The basis
245 for the adjustment is surface boundary layer parameters derived for R11's site (Kochendorfer et
246 al. 2018) and an equation from Panofsky and Dutton (1984; their Eq. 6.7). The adjustment was
247 made because the hotplate-derived wind speeds, both here and in Marlow et al. (2023), were
248 acquired at approximately 2 m above the snowpack surface. Third is Marlow et al.'s comparison
249 of SNOTEL-derived liquid-equivalent depth changes and hotplate-derived time-integrated
250 accumulations. The interval for the comparisons is 24 hours. Based on the comparison, which
251 has 57 paired values acquired at the sites labeled HP and SN in Fig. 1, the average fractional
252 absolute relative difference is 0.30. Marlow et al. also provided an estimate of the error in a
253 SNOTEL measurement (2.4 mm). At accumulation = 10 mm the error corresponds to a relative
254 error = 0.24. This indicates that SNOTEL contributed significantly to the SNOTEL/hotplate
255 variance and especially so for the smaller accumulations in Fig. 9a of Marlow et al. (2023).
256 Because of this, we do not limit the following estimate of hotplate precision to a subset of the 57
257 paired measurements. Based on our assessment of the average fractional absolute relative
258 difference, the hotplate precision applied in this analysis was taken to be 0.3.

259 The hotplate-derived wind speeds acquired at ~ 2 m, and discussed in the previous
260 paragraph, are henceforth symbolized U_{PRO} . The basis for these is a steady state energy budget of
261 the hotplate's temperature-controlled down-viewing plate and a proprietary algorithm (R11 and
262 Z18). The U_{PRO} are reported by a hotplate as one-minute running averages (Z18) and we
263 recorded these at 1 Hz. Examples are the gray dots in Fig. 2. Additionally, we calculated and
264 analyzed one-minute-averaged values of U_{PRO} and the corresponding standard deviations.
265 Examples of these are the black circles and the short vertical line segments in Fig. 2.

266

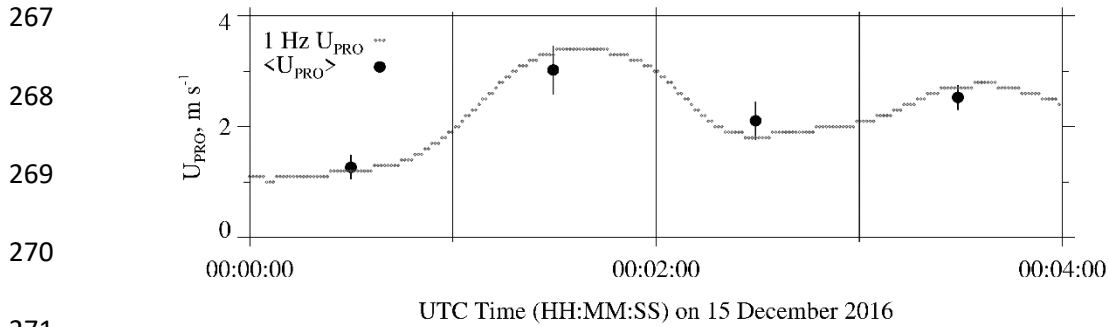


Figure 2 – Hotplate wind speed measurements (U_{PRO}) 00:00:00 to 00:04:00 on 15 December 2016. Gray dots are the one-minute running-average U_{PRO} recorded at 1 Hz. Black circles are the one-minute-averaged U_{PRO} (± 1 standard deviation).

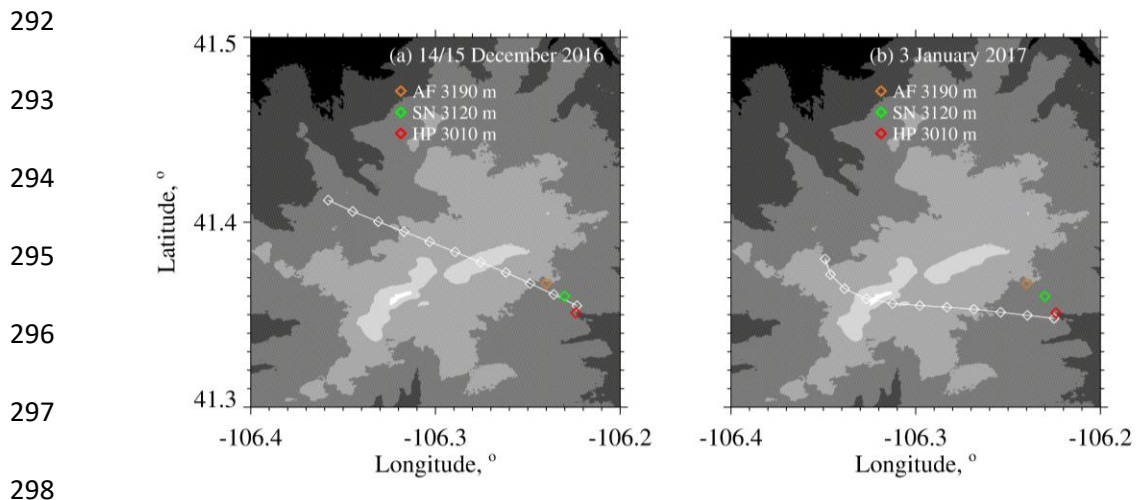
277 **3 - Analysis**

278 **3.1 - WKA Overflight Time**

279 The focus of our analysis is the two WKA flight segments shown in Figs. 3a-b. The maps
280 shown in the figures have the three ground sites (AF, SN, and HP) and the WKA flight tracks
281 (white line). The beginning-to-end time interval for the flight tracks is 100 s and these are
282 divided into ten 10-second intervals. The 10 s intervals are indicated with white diamonds.
283 Except for the turn evident in Fig. 3b, the flight tracks are straight, and the track direction is
284 approximately upwind to downwind.

285 Times that the WKA was closest to the HP site were evaluated by finding the point on the
286 flight track where the horizontal position of the WKA was closest to the hotplate's coordinates.
287 These times are symbolized t_0 and are referred to as overflight times. In Figs. 3a-b the downwind
288 end of the flight tracks end at the overflight time. The latitude/longitude position of the aircraft
289 was within 390 m of the hotplate at the overflight times. Table 2 has the overflight times on the
290 two flight days.

291



299 Figure 3 – (a) WKA flight track on 14/15 December 2016 for time interval = overflight time -
 300 100 s to the overflight time. (b) WKA flight track on 3 January 2017 for time interval =
 301 overflight time - 100 s to the overflight time. The white diamonds on the tracks are separated, in
 302 time, by 10 s. Altitude thresholds for the digital elevation maps are 2600, 2800, 3000, 3200,
 303 3400, and 3600 meters. Altitudes of the ground sites are in the legend.

304

305 3.2 – Effect of Attenuation on WCR Reflectivities

306

307 The presence of molecular oxygen, water vapor, cloud water, and snow particles within
308 the WCR's transmission path will contribute to an attenuation of microwave intensity and will
309 therefore negatively bias the retrieved reflectivities (Matrosov 2007; Hiley et al. 2011; Kneifel et
310 al. 2015). Models of attenuation, radar remote sensing, and in situ measurements were used to
311 calculate this bias. For oxygen, an attenuation coefficient from Ulaby et al. (1981; their Fig. 5.6),
312 and temperature (T) and pressure (P) measurements from the AF (Table 3), were used. For
313 vapor, an attenuation coefficient (Ulaby et al. 1981; their Eq. 5.22), and T, P, and relative
314 humidity (RH) measurements from the AF (Table 3), were used. Concentrations of oxygen and
315 water vapor and the oxygen and vapor path lengths are provided in Table 4. The latter is the
316 vertical distance between the HP and the WKA. It was assumed that concentrations were
317 uniform over this path length.

318 Attenuation by cloud water was derived using the WKA-measured T (Table 3), the
319 WKA-measured LWC, path length (Table 4), and an attenuation formula (Liebe et al. 1989; Vali
320 and Haimov 2001). The LWC applied in the formula is the maximum of CDP measurements
321 acquired between $t_0 - 10$ s and t_0 . This interval coincides with the interval the WCR's down-
322 looking antenna was used to acquire reflectivities over the HP (Sect. 3.5). The path length for
323 cloud water was derived as the vertical distance between cloud base [derived thermodynamically
324 using AF measurements (Table 3)] and flight level. LWC was assumed uniform, at the maximum
325 value, over the path length.

326 Snow particle mass concentration is typically reported as an ice water content (IWC, g m^{-3})
327 (Liu and Illingworth 2000). The contribution of IWC to attenuation was calculated using

328 measurements in Nemanich et. al (1988), who reported an attenuation coefficient equal to 0.9
 329 dB/km per unit of IWC. Also used were retrievals of IWC acquired using the down-pointing
 330 WCR antenna. There are several steps in the calculation. First, all profiles of dBZ acquired
 331 between $t_0 - 10$ s and t_0 were selected. Second, a maximum dBZ was selected at each of the
 332 down-beam range gates (Table 2). Third, the dBZ maxima were increased by the overall two-
 333 way attenuation in the final column of Table 4. Fourth, the profile of attenuation-corrected dBZ
 334 was converted to a profile of attenuation-corrected Z. Fifth, a Z-to-IWC parameterization was
 335 applied ($IWC = 0.10 \cdot Z^{0.51}$; PV11; their Table 3). Sixth, the IWC profile was integrated, and the
 336 derived ice water path was divided by the snow particle path length (Table 4). This calculation
 337 produced a time- and range-averaged maximum IWC (Table 4). This IWC is the value applied in
 338 the attenuation calculation.

339 Two-way attenuations (ΔdB), summed over contributions from the four components, are
 340 presented in the final column of Table 4. Attenuation by snow and attenuation by liquid were the
 341 most important components ($> 50\%$) on December 15 and January 3, respectively. Vapor
 342 contributed 32% to the overall on December 15, and the combination of vapor and snow
 343 contributed 45% on January 3. Equation 1 shows how an attenuation-corrected reflectivity (Z')
 344 was derived using an uncorrected reflectivity (Z) and the ΔdB .

345

$$346 \quad Z' = 10^{\left[\frac{10 \cdot \log_{10}(Z) + \Delta dB}{10} \right]} \quad (1)$$

347 Table 3 – Atmospheric state averages

348

Date	WKA ^a Track Altitude, m	WKA ^a T, °C	AF ^b T, °C	AF ^b RH, %	WKA ^{a, c} Track Vector	WKA ^{a, c} Wind Vector	AF ^{b, c} Wind Vector
14/15 December 2016	4546	-13.9	-6.3	86	310 / 130	274 / 32	250 / 8.5
3 January 2017	4196	-21.7	-14.6	77	280 / 120	265 / 27	260 / 5.4

349

350

351 ^a Altitude, temperature, track vector, and horizontal wind vector data obtained by averaging 1 Hz
 352 WKA measurements. The averaging interval is 60 s and the interval starts at the overflight time,
 353 minus 60 s, and ends at the overflight time.

354

355 ^b Temperature (T), relative humidity (RH), and horizontal wind vector data from sensors on the
 356 US-GLE AmeriFlux tower (Sect. 2.1). The wind sensor was deployed at 26 m AGL (3223 m
 357 MSL) and the T/RH sensor was deployed at 23 m AGL (3220 m MSL). The AF measurements
 358 correspond to 30-minute averages closest to the overpass time. In the AF data set, time stamps on
 359 the relevant AF recordings are 00:00 UTC (15 December 2016) and 20:30 UTC (3 January
 360 2017).

361

362 ^c Vectors are presented in the following format: Direction of motion (degree relative to true
 363 north) / speed (m s^{-1}).

364 Table 4 – Attenuating component concentration, one-way pathlength, and the overall two-way attenuation

Date	Conc. Oxygen, kg m ⁻³	Conc. Vapor, kg m ⁻³	Maximum LWC, g m ⁻³	Maximum IWC, g m ⁻³	One-way Pathlength ^a Oxygen, Vapor, and Snow, km	One-way Pathlength ^b Cloud Water, km	Overall Two-way Attenuation, ΔdB
15 December 2016	0.21	2.7x10 ⁻³	0.01	0.27	1.54	1.09	1.41 ^c
3 January 2017	0.21	1.3x10 ⁻³	0.08	0.09	1.19	0.59	1.01 ^d

365

366 ^a Vertical distance between HP and WKA

367

368 ^b Vertical distance between cloud base [derived thermodynamically using AF measurements (Table 3)] and WKA

369

370 ^c One-way attenuation coefficients are 0.03 dB/km for oxygen (Ulaby et al. 1981), 0.14 dB/km for vapor (Ulaby et al. 1981), 0.056
371 dB/km for cloud water (Liebe et al. 1989; Vali and Haimov 2001), and 0.24 dB/km for snow particles (Nemarich et al 1988).

372

373 ^d One-way attenuation coefficients are 0.03 dB/km for oxygen (Ulaby et al. 1981), 0.073 dB/km for vapor (Ulaby et al. 1981), 0.49
374 dB/km for cloud water (Liebe et al. 1989; Vali and Haimov 2001), and 0.077 dB/km for snow particles (Nemarich et. al 1988).

375

376 **3.3 - Correction of Doppler Velocity**

377 We accounted for bias in V_D (Sect. 2.3) due to deviation of the down-looking WCR
378 antenna from vertical. This was done by applying the correction described in Zaremba et al.
379 (2022) (their Eq. A4). The west-to-east and south-to-north particle velocities used in the
380 correction were assumed to be equal to component wind velocities. The latter were expressed as
381 linear functions of altitude using the information in the penultimate and last columns of Table 3.
382 The component velocities as functions of altitude and the linear equations relating velocity and
383 altitude are provided in the Appendix.

384 **3.4 - Hotplate Measurement of Wind Speed**

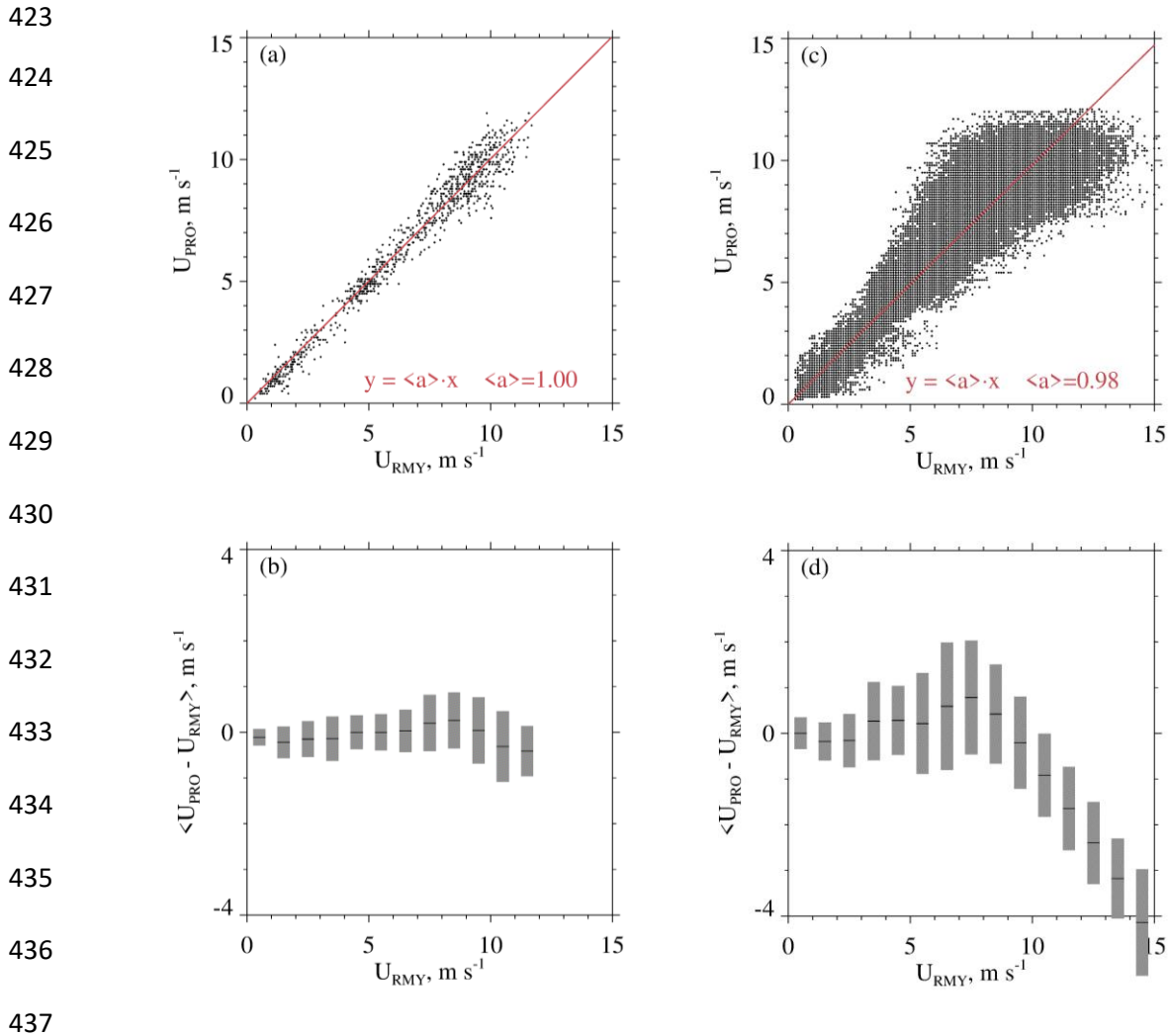
385 Here we compare the hotplate-derived wind speed to wind speed derived using an
386 R.M.Young rotating anemometer (R.M.Young 2001). The second of these is symbolized U_{RMY}
387 and the basis for the first (U_{PRO}) is a proprietary algorithm (Sect. 2.4). We are doing this
388 comparison because B14 showed that U_{PRO} can be high-biased, relative to a conventional
389 anemometer, and because U_{PRO} is the primary determinant of the rate that the up-viewing plate
390 dissipates sensible heat energy. Diagnosis of that heat transfer rate is our basis for calculating the
391 liquid-equivalent snowfall rate (Z18). The U_{PRO} also determines the snow particle catch
392 efficiency and the latter was used in calculations of the undercatch-corrected liquid-equivalent
393 snowfall rate (Sect. 2.4).

394 The comparisons reported here were done at the Laramie, WY Airport in December
395 2019, and in January 2020. Compared to the HP site, the Laramie Airport site (indicated LA in
396 Fig. 1) is free of obstruction, out to 120 m, and experiences larger wind speeds. By mounting the
397 hotplate and the R.M.Young anemometer on rigid metal pipes, the hotplate's heated horizontal

398 surfaces (the up- and down-viewing plates seen in Fig. 1 of Z18) and the anemometer's spinning
399 axis (oriented horizontally) were both positioned at 2 m AGL. The pipes were separated
400 horizontally by 5 m. There was no precipitation on the days selected for the wind speed
401 comparisons. The values of U_{PRO} and U_{RMY} we analyzed were recorded with a data system that
402 time stamped the 1 Hz U_{PRO} and 1 Hz U_{RMY} with a relative timing accuracy no worse than 1 s.

403 A wind speed comparison - from 13 December 2019 - is shown in Fig. 4a. U_{PRO} was
404 brought into the comparison by sampling it once per minute from files containing 1 Hz
405 recordings of the one-minute running-average U_{PRO} (Sect. 2.4). U_{RMY} was brought into the
406 comparison by starting with files containing 1 Hz recordings and converting these to one-minute
407 averages. Fig. 4a shows no evidence of bias and Fig. 4b demonstrates that the average absolute
408 departure between the U_{PRO} and U_{RMY} (both one-minute averages) is no larger than 1 m s^{-1} . Table
409 5 has eight more precipitation-free comparisons. Included in the table are temperature and wind
410 speed averaged over the comparison intervals (4 to 20 UTC), the slope of the linear-least-squares
411 fit line (forced through the origin, red line), and the lower and upper quartiles of the slope. The
412 quartiles were calculated using the method of Wolfe and Snider (2012). In contrast to Figs. 4a-b,
413 Figs. 4c-d make the comparison using 1 Hz values of U_{PRO} and U_{RMY} . The larger scatter and
414 larger average absolute departure seen in these panels is a consequence of the hotplate's limited
415 time response, compared to the R.M.Young. We quantify the hotplate's response time in terms of
416 a calculated thermal response time. During wintertime at the Laramie Airport, and with wind
417 speed at 5 m s^{-1} , the down-viewing plate's thermal response time is approximately 60 s (results
418 not shown). Because the temperature of the down-viewing plate is actively controlled, this does
419 not translate to a 60 s lag between changes in wind speed and the hotplate response. The
420 $U_{\text{PRO}}/U_{\text{RMY}}$ departure is most evident at $U_{\text{PRO}} > 5 \text{ m s}^{-1}$ (Fig. 4d) but this is not a concern for

421 U_{PRO} on 14/15 December 2016 or on 3 January 2017. Snider (2023) demonstrated that the U_{PRO}
422 was less than 5 m s^{-1} at the hotplate during the two WKA overflights.



438 Figure 4 – (a) Scatterplot of one-minute-averaged U_{PRO} and one-minute-averaged U_{RMY} .
 439 Measurements were acquired at the Laramie, WY Airport 13 December 2019. The red line is a
 440 linear-least-squares fit line (forced through the origin). (b) Average departure between one-
 441 minute-averaged U_{PRO} and one-minute-averaged U_{RMY} . Average departures were calculated for
 442 discrete U_{RMY} intervals, and the averages are indicated with short black horizontal lines. Gray
 443 bars indicate ± 1 standard deviation. (c) Same as in (a) except for 1 Hz values of U_{PRO} and U_{RMY} .
 444 (d) Same as in (b) except for 1 Hz values of U_{PRO} and U_{RMY} .

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446

447 Table 5 - U_{PRO} versus U_{RMY} correlations

448

Date, UTC ¹	$\langle T \rangle^2$, °C	$\langle U \rangle^2$, m s ⁻¹	$\langle a \rangle^3$	a ⁴ First Quartile	a ⁴ Third Quartile
7 December 2019	-0.40	5.40	1.00	0.90	1.04
8 December 2019	2.70	4.10	0.99	0.90	1.04
10 December 2019	-5.20	3.80	0.99	0.83	1.04
13 December 2019	-1.50	6.60	1.00	0.93	1.06
18 December 2019	-6.20	3.60	0.99	0.92	1.04
19 December 2019	-6.90	2.70	0.95	0.84	0.99
6 January 2020	-6.40	8.80	1.01	0.96	1.06
8 January 2020	0.30	4.20	1.00	0.87	1.05
11 January 2020	-7.20	7.00	1.02	0.97	1.08

449

450

451 ¹ Statistics presented are based on one-minute-averaged U_{PRO} and one-minute-averaged U_{RMY}
 452 measurements made between 04:00 to 20:00 UTC.

453

454 ² Interval-averaged temperature and interval-averaged wind speed.

455

456 ³ Slope of the one-minute-averaged U_{PRO} versus one-minute-averaged U_{RMY} linear-least-squares
 457 fit line, forced through the origin.

458

459 ⁴ Quartiles of the slope (see text)

460

461 3.5 – Combined Aircraft and Surface Measurements

462 Figure 5 has WCR and WKA measurements starting 100 s prior to t_0 and ending at t_0 .
463 The sequences in Figs. 5a and 5c are reflectivities from both the up- and down-looking antennas.
464 In Fig. 5a the flight track (black dashed horizontal line) is at 4550 m and in Fig. 5c the flight
465 track is at 4200 m. At the t_0 in Fig. 5a, below the WKA, the maximum radar echo is +6 dBZ (Z
466 = $4 \text{ mm}^6 \text{ m}^{-3}$) and in Fig. 5c the maximum is -3 dBZ ($Z = 0.5 \text{ mm}^6 \text{ m}^{-3}$). Supercooled liquid
467 water was detected as the aircraft approached the ridgeline (Fig. 5b) and during the last 10
468 seconds of the time sequence in Fig. 5d. During these encounters with supercooled liquid, the
469 maximum LWC values were 0.03×10^{-3} and $0.08 \times 10^{-3} \text{ kg m}^{-3}$ on 14 December 2016 and 3
470 January 2017, respectively. Values of N (Sect. 2.2) at times of maximal LWC were 3×10^6 and
471 $100 \times 10^6 \text{ m}^{-3}$ on 14 December 2016 and 3 January 2017, respectively. Even on 3 January 2017,
472 the $\langle D \rangle$ (Sect. 2.2) associated with maximum LWC was sufficient for hexagonal plate crystals
473 with diameter larger than $100 \text{ }\mu\text{m}$ to collide with the observed droplets with efficiencies > 0.1
474 (Wang and Ji 2000).

475 We temporally and spatially averaged the values of Z we compared with time-averaged
476 values of S . There are two reasons for this: 1) As discussed in Sect. 3.1, the WCR did not sample
477 Z exactly over the hotplate, and furthermore, the width of radar beam at 1500 m range - roughly
478 the distance between the aircraft and the ground at the overflight times - is 30 m and thus
479 considerably smaller than the minimum horizontal distance between the aircraft and the HP. 2)
480 Compared to the WCR, the hotplate is a relatively slow-response measurement system whose
481 output is commonly averaged over one-minute intervals (Z18).

482

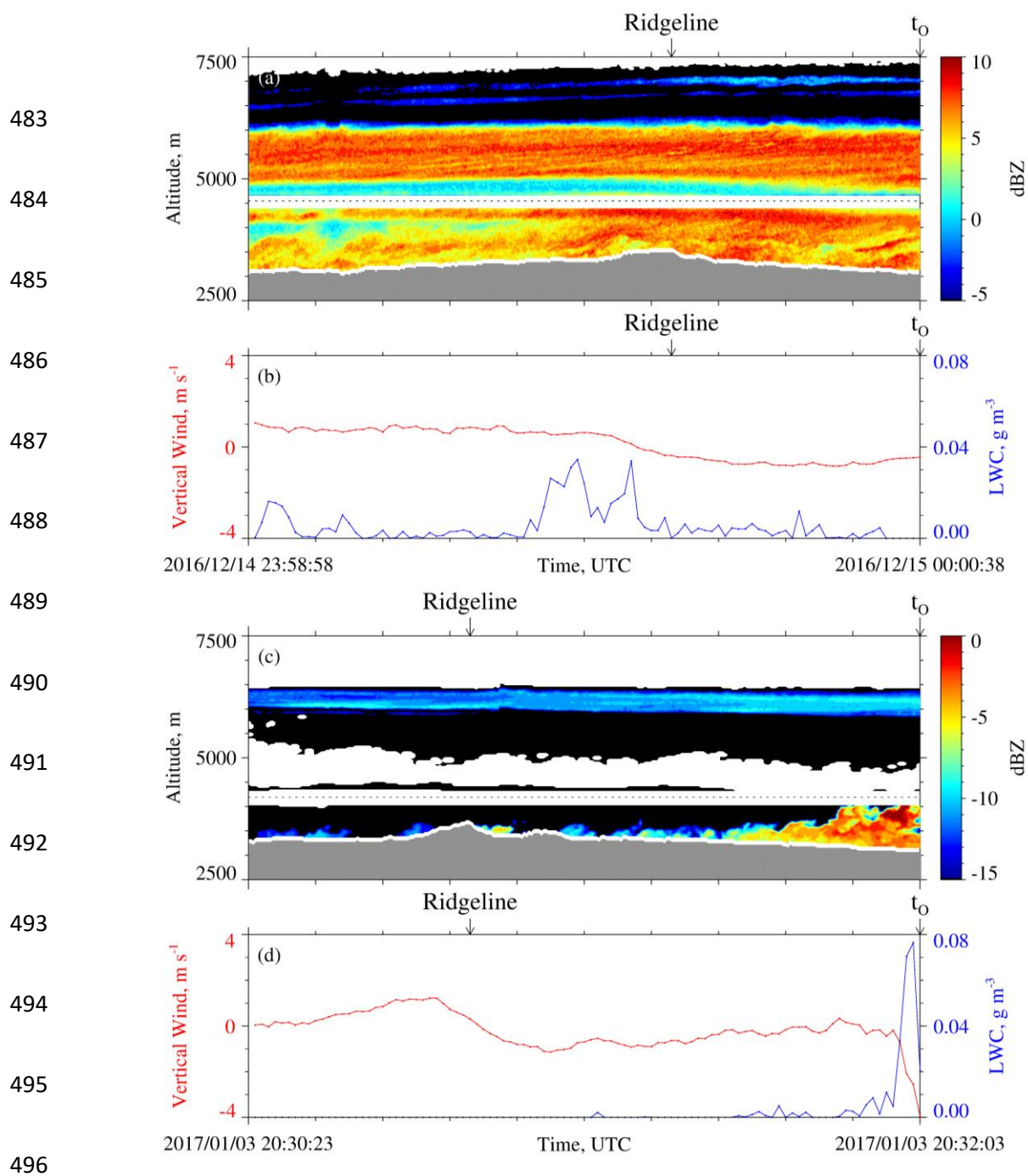


Figure 5 – (a) 100 s of WCR reflectivity and (b) 100 s of LWC and gust probe vertical wind velocity ending at t_0 on 14/15 December 2016. (c) 100 s of WCR reflectivity and (d) 100 s of LWC and gust probe vertical wind velocity ending at t_0 on 3 January 2017. In (a) and (c), above and below the flight track, the roughly 200-m-deep WCR blind zone is evident, reflectivity above (below) the flight track is from the up-looking (down-looking) WCR antenna,

502 black indicates dBZ values smaller than the minimum indicated in the color bar, white
503 immediately above the terrain indicates echo that was discarded because of ground clutter, and
504 white above the ground clutter and outside of the blind zone indicate dBZ < minimum detectable
505 signal.

506 In our analysis, the HP measurements were averaged over two adjacent 60 s intervals.
507 The first extends from t_0 to $t_0 + 60$ s (Fig. 6a) and the second from $t_0 + 60$ s to $t_0 + 120$ s (Fig.
508 6c). In Fig. 6a and in Fig. 6c, $t_{HP,B}$ symbolizes an interval's beginning time and $t_{HP,E}$ symbolizes
509 an interval's ending time. Formulas describing how these times were related to the beginning and
510 ending time of a corresponding WCR averaging interval are in the Appendix. Fig. 6b is a
511 schematic of the first WCR averaging interval and Fig. 6d is a schematic of the second. Again,
512 the subscripts "B" and "E" are used to indicate averaging beginning and ending times. Figures 6b
513 and 6d both have lines at the top of an averaging interval/domain. The slopes of these lines are
514 proportional to the ratio of two speeds. These speeds are a maximum likely snow particle speed
515 toward the ground (v_p) and a horizontal wind advection speed (v_w). The v_p was calculated
516 using averaged vertical-component Doppler velocities and v_w was calculated using a vertical
517 profile of horizontal winds, based on WKA horizontal wind measurements and AF horizontal
518 wind measurements (Figs. A1a-b), and using the WKA track vector (Table 3). An altitude ($z' =$
519 3400 m) was assumed in the calculation of v_w . This is the altitude of the ridges west and
520 northwest of the HP site (Figs. 3a-b). Picking the altitude to be either $z' = 3200$ m or $z' = 3600$ m
521 does not alter our findings.

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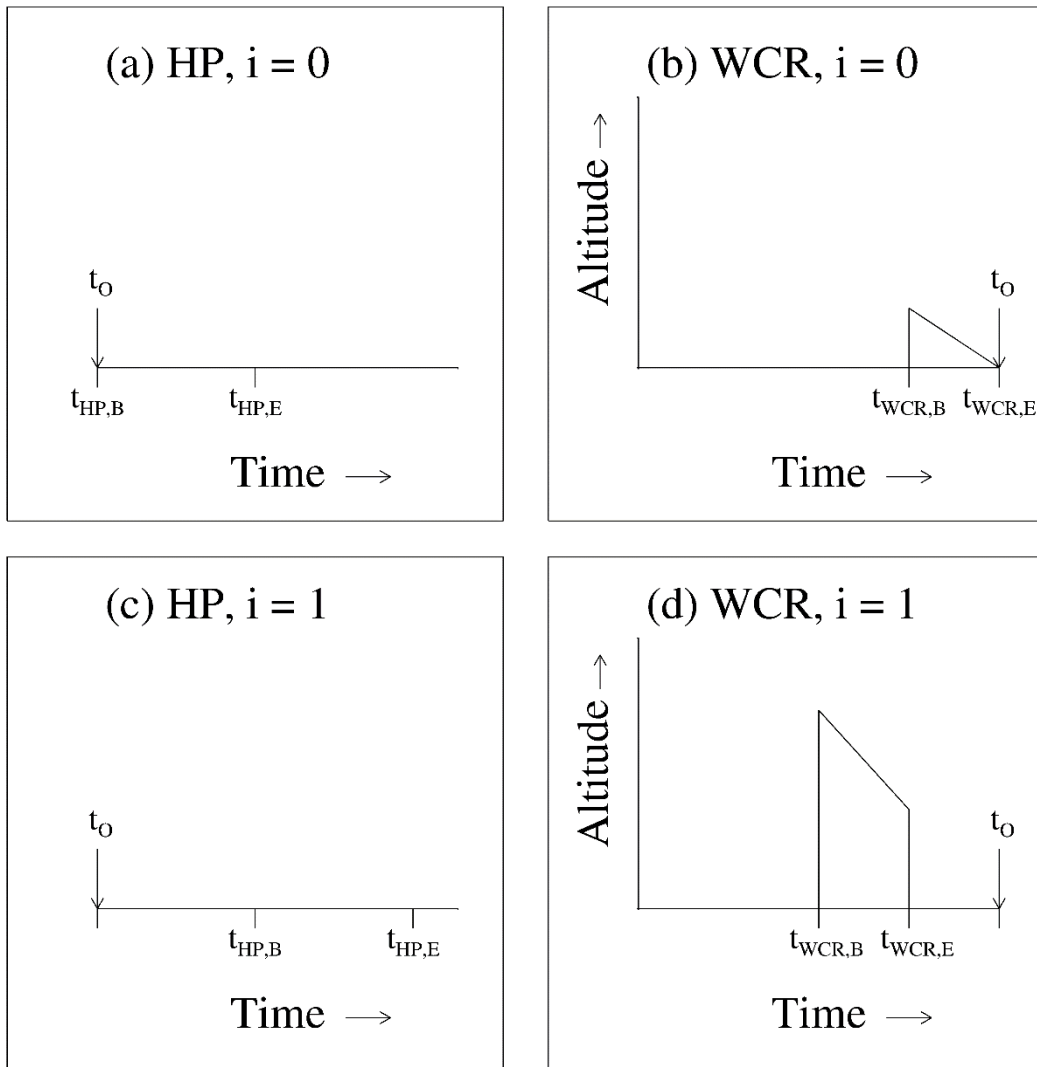


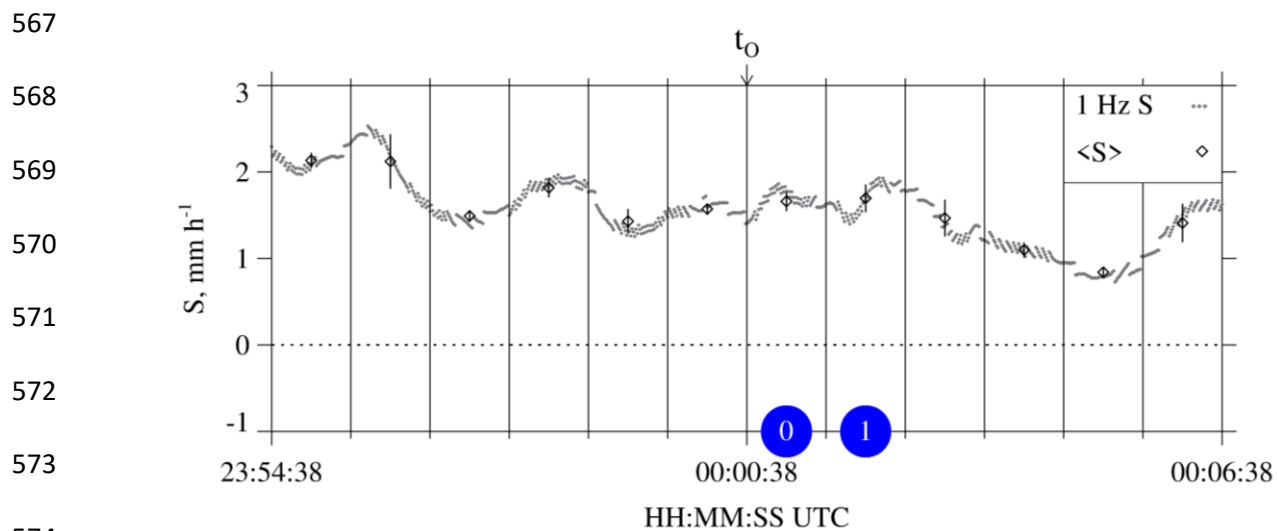
Figure 6 – (a and c) Representations of the $i = 0$ and $i = 1$ HP averaging intervals. (b and d) Representations of the $i = 0$ and $i = 1$ WCR averaging intervals/domains. The t_0 is shown in all panels. The subscripts “B” and “E” indicate beginning and ending times of the HP averaging (panels a and c) and the beginning and ending times of the WCR averaging (panels b and d).

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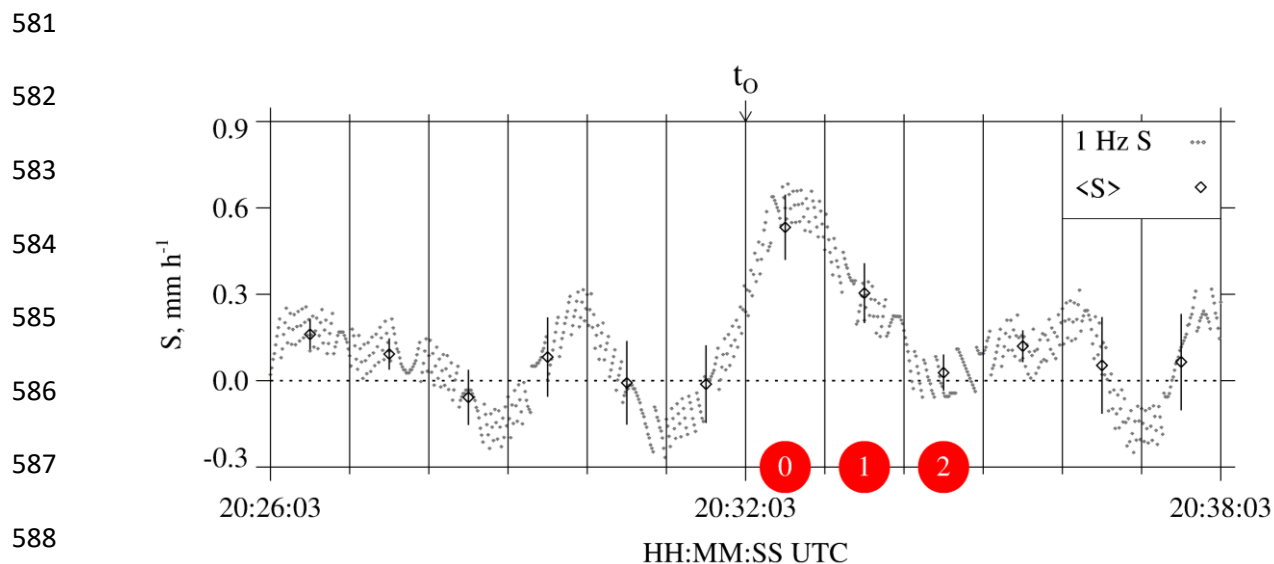
549 All panels in Fig. 6 are labeled with an index designating either the first averaging
550 interval ($i = 0$) or the second averaging interval ($i = 1$). Figures 7 and 8 present hotplate
551 snowfall measurements from 14/15 December 2016 and 3 January 2017. In these, and in
552 subsequent figures, colored circles surround the $i = 0$ and $i = 1$ indexes, blue is used to color-
553 code 15 December 2016, and red is used to color-code 3 January 2017. Additionally, Fig. 8 has
554 an $i = 2$ averaging interval. This is a special case discussed at the end of this section.

555 Figures 9a-b and Figs. 10a-b have enlarged views of the altitude-time WCR crosssections
556 recorded on the two flight days. Different from Fig. 5a and Fig. 5c, these measurements are only
557 from the WCR's down-looking antenna. Additional differences are the following: 1) The plots
558 are set up so that Z and V_D structures downwind of the hotplate can be seen. These structures are
559 discussed in the following section. 2) The WCR measurements are shown for 50 s of flight. With
560 the WKA ground speed approximately 125 m s^{-1} (Table 3), the distance along the abscissa is
561 6250 m. 3) Colored circles that surround the indexes are placed below the WCR averaging
562 intervals/domains. The latter are drawn with solid black lines and are seen to overlay both the Z
563 and V_D altitude-time crosssections. Consistent with Figs. 6b and 6d, and the Appendix, one of
564 these black lines is vertical and another is negatively sloped. Figs. 10a-b also have the $i = 2$
565 intervals/domains discussed at the end of this section.

566



576 Figure 7 – Twelve minutes of HP snowfall measurements from 14/15 December 2016. Gray dots
 577 are S values calculated using hotplate output recorded at 1 Hz. Black diamonds are the one-
 578 minute-averaged values (± 1 standard deviation). The t_0 is shown above the panel and blue
 579 circles designate the $i = 0$ and $i = 1$ HP averaging intervals.



590 Figure 8 – Twelve minutes of HP snowfall measurements from 3 January 2017. Gray dots are S

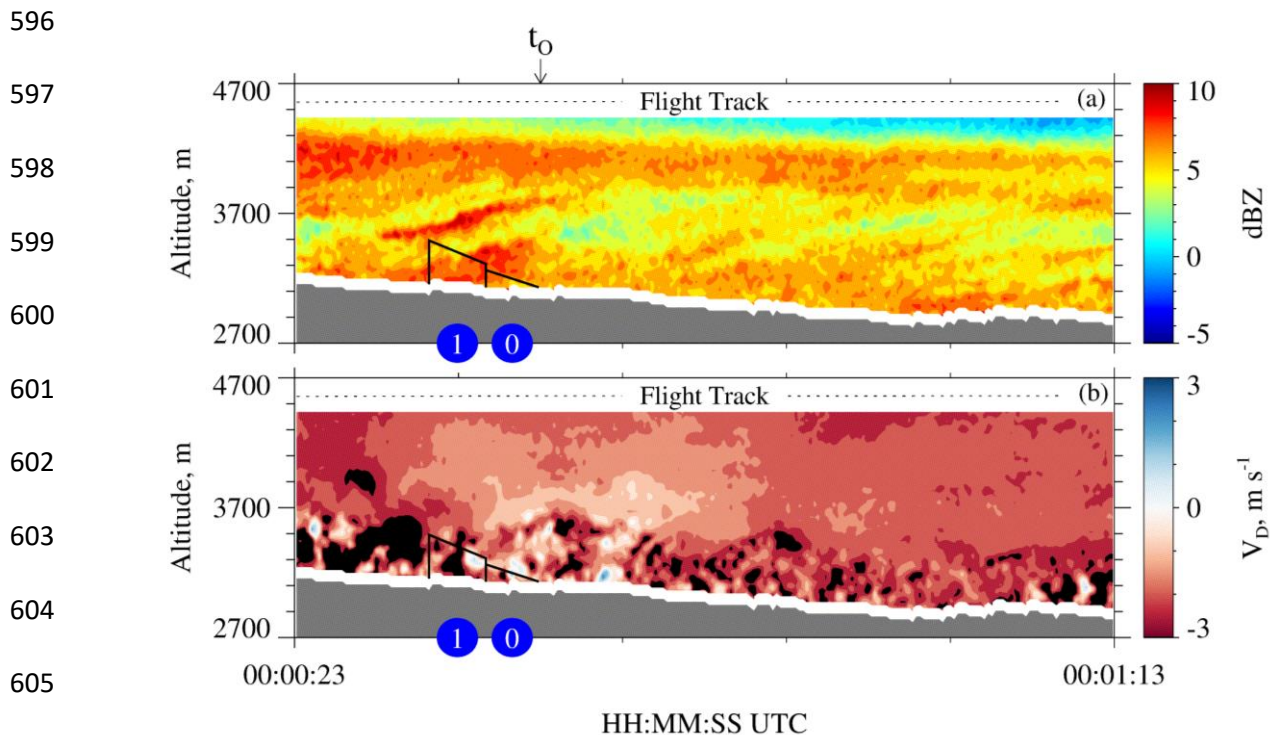
591 values calculated using hotplate output recorded at 1 Hz. Black diamonds are the one-minute-

592 averaged values (± 1 standard deviation). The t_0 is shown above the panel and red circles

593 designate the $i = 0$, $i = 1$, and $i = 2$ HP averaging intervals. The $i = 2$ interval is a special case

594 discussed at the end of Sect. 3.5.

595



608 Figure 9 – 50 s of measurements from the down-looking WCR antenna on 15 December 2016.

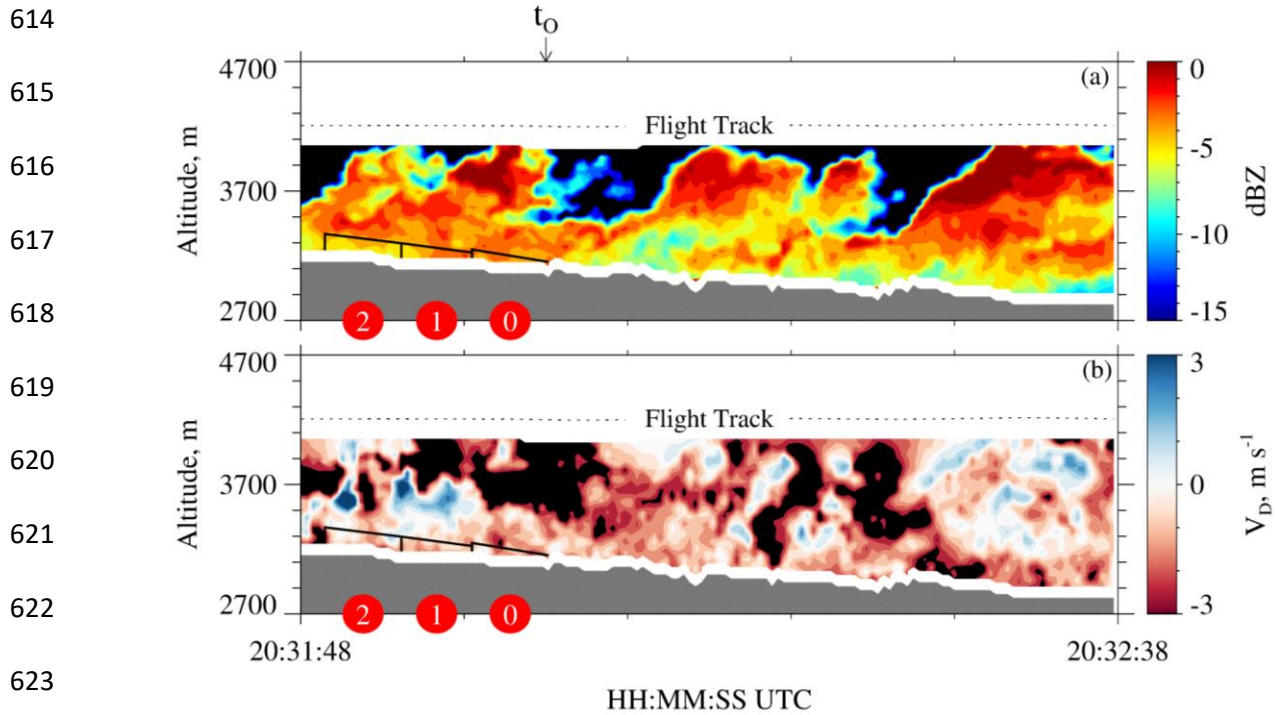
609 (a) Crosssection of reflectivity $t_0 - 15$ s to $t_0 + 35$ s. (b) Crosssection of Doppler velocity $t_0 - 15$ s

610 to $t_0 + 35$ s. The t_0 is shown above the top panel. In both panels, the solid black lines (vertical

611 and sloped) encompass the $i = 0$ and $i = 1$ WCR averaging intervals/domains and blue circles

612 designate the WCR averaging intervals.

613



626 Figure 10 – 50 s of measurements from the down-looking WCR antenna on 3 January 2017. (a)

627 Cross-section of reflectivity $t_0 - 15$ s to $t_0 + 35$ s. (b) Cross-section of Doppler velocity $t_0 - 15$ s to t_0

628 $+ 35$ s. The t_0 is shown above the top panel. In both panels, the solid black lines (vertical and

629 sloped) encompass the $i = 0$, $i = 1$, and $i = 2$ WCR averaging intervals/domains and red circles

630 designate the $i = 0$, $i = 1$, and $i = 2$ WCR averaging intervals/domains. The $i = 2$ interval/domain

631 is a special case discussed at the end of Sect. 3.5.

632

633 The $i = 0$ and $i = 1$ averages of S and Z are presented in Table 6 and the corresponding
634 averaging intervals are viewable in Fig. 7 and Fig. 9a (15 December 2016) and in Fig. 8 and Fig.
635 10a (3 January 2017). According to the averaging scheme (Fig. 6), the $i = 1$ HP averaging
636 interval is time-shifted positively compared to the $i = 0$ HP averaging interval and the $i = 1$ WCR
637 averaging interval is time-shifted negatively compared of the $i = 0$ WCR averaging interval.
638 This arrangement of the averaging intervals is one way to average while also accounting for
639 wind advection of the snow particles.

640 As discussed earlier in this section, the averaging scheme initializes with 60-second
641 blocks of HP data between t_o and $t_o + 120$ s. When we applied the scheme to data from 3 January
642 2017, but outside the specified time range, an inconsistency was documented. This is apparent in
643 Fig. 8, where the $t_o + 120$ s to $t_o + 180$ s interval (i.e., the $i = 2$ interval) has negligible average S,
644 while in Fig. 10, the $i = 2$ interval has a non-negligible average Z ($\sim 0.3 \text{ mm}^6 \text{ m}^{-3}$). A firm
645 explanation is not available for the inconsistency, but a factor may be the convective nature of
646 the fields in Figs. 10a-b. Because of the inconsistency, only averages corresponding to the $i = 0$
647 and $i = 1$ intervals are analyzed further.

648 Table 6 – Average wind measurements, average hotplate measurements, average WCR measurements, and attenuation-corrected
 649 reflectivities

Date	v_w^a , m s ⁻¹	i index	$S_{HP} \pm \sigma^b$, mm h ⁻¹	WCR Samples ^c	$\langle V_D \rangle^d$, m s ⁻¹	$\sigma_{V_D}^e$, m s ⁻¹	v_p^f , m s ⁻¹	$\langle Z \rangle \pm \sigma_Z^g$, mm ⁶ m ⁻³	Z'^h , mm ⁶ m ⁻³
15 December 2016	7.4	0	1.7±0.1	42	-1.3	0.9	2.2	4.9±2.1	6.8
15 December 2016	7.4	1	1.7±0.2	149	-1.8	1.2	3.0	5.6±1.1	7.8
3 January 2017	8.9	0	0.5±0.1	22	-0.9	0.8	1.7	0.49±0.05	0.62
3 January 2017	8.9	1	0.3±0.1	35	-0.8	0.4	1.2	0.50±0.10	0.63

650

651 ^a Horizontal wind advection speed (Eq. A7) calculated using values from the penultimate and last columns of Table 3.

652 ^b One-minute average of the undercatch-corrected liquid-equivalent snowfall rate (± 1 standard deviation). An example averaging
 653 interval is the $i = 0$ interval in Fig. 7.

654 ^c Number of samples used to calculate the WCR statistics. The averaging intervals/domains (e.g., $i = 0$ in Figs. 9a-b and in Figs. 10a-
 655 b) encompass the WCR samples which are the basis for the WCR statistics presented in this table.

656 ^d Average of Doppler velocity within the averaging intervals/domains.

657 ^e Standard deviation of Doppler velocity within the averaging intervals/domains.

658 ^f Maximum likely snow particle speed toward the ground (Eq. A8).

659 ^g Average reflectivity (± 1 standard deviation). These values are not corrected for attenuation.

660 ^h Attenuation-corrected reflectivities. These were derived using reflectivities from the penultimate column of this table, attenuations
 661 from Table 4, and Eq. 1.

662 3.6 - Snow Particle Imagery

663 In Fig. 9a and Fig. 10a, the time for a snow particle to move the abscissa and ordinate
 664 distances is different. The ratio of these two times is 2.6. This follows from our choice of
 665 abscissa and ordinate ranges, from values of particle fall speed (1 m s^{-1}) and horizontal wind
 666 advection speed (8 m s^{-1}), which we assumed, and from the WKA ground speed ($gs \sim 125 \text{ m s}^{-1}$;
 667 Table 3). The assumed values are approximately consistent with values of $\langle V_D \rangle$ and v_w , in
 668 Table 6, and with the V_D sign convention (Sect. 2.3). We also used $gs = 125 \text{ m s}^{-1}$ to scale
 669 (virtually) the time axes in Fig. 9a and Fig. 10a to a horizontal distance. Within the scaled
 670 coordinate frames, we assumed that all snow particle trajectories have negative slope ($\Delta z / \Delta x = -$
 671 $1 \text{ m s}^{-1} / 8 \text{ m s}^{-1} = -0.12$) and that all trajectories are stationary. However, both assumptions seem
 672 inconsistent with the reflectivity structures in Fig. 5a, where positively-sloped particle fall
 673 streaks are evident at $\sim 5500 \text{ m}$, inconsistent with Fig. 9a where positively-sloped fall streaks are
 674 at $\sim 3500 \text{ m}$, and inconsistent with the positively-sloped fall streaks in Fig. 10a. On both flight
 675 days, the fall streaks evince particle sources that move horizontally and with a horizontal speed
 676 that is larger than the $v_w = 8 \text{ m s}^{-1}$ applied in the estimate of the trajectory slope. It may be that
 677 the source's horizontal speed is comparable to the flight-level WKA-derived horizontal wind (27
 678 to 32 m s^{-1} ; Table 3) but we do not have data needed to verify that assertion. Based on the
 679 assumption that snow particles followed the fall streaks while both were advecting horizontally,
 680 we looked *downwind* of the hotplate - at a time later than t_0 in Fig. 9a and Fig. 10a - for particles
 681 that became those that produced snowfall at the hotplate.

682 Particle images from 15 December 2016 were analyzed using the 2DP. With this
 683 instrument the maximum all-in particle size (in the horizontal direction perpendicular to flight) is

684 6400 μm and the particle size resolution is 200 μm (Sect. 2.2). Within the time interval picked
685 for this analysis (discussed below), particles sizing in the smaller of the two spectral modes, with
686 mode size $\sim 400 \mu\text{m}$, were more numerous (results not shown). Because the 400 μm particles are
687 poorly resolved by the 2DP, and the same can be said for somewhat larger particles, those
688 smaller than 1000 μm were excluded from the following analysis. Figure 11a shows imagery
689 from 12 s of measurements acquired near the end of the sequence in Fig. 9a (00:01:02 to
690 00:01:14). This time interval was selected by tracing forward from t_0 , along the slope of the fall
691 streaks, to the flight level. Many of the particles are rounded (indicating riming) and a few have
692 arms likely due to incomplete conversion of branched crystals to rimed snow particles. The mode
693 size corresponding to these images is 1600 μm . No liquid water was detected with these particles
694 ($\text{LWC} < 0.01 \times 10^{-3} \text{ kg m}^{-3}$; Fuller 2020; her Fig. 8), but liquid was detected, at $\sim 00:00:00$, as the
695 aircraft approached the ridgeline (Figs. 5a-b).

696 Turning to imagery from 3 January 2017, the most appropriate location for analysis
697 would be through the second billow structure evident in Fig. 10a (i.e., very close to the middle of
698 the Fig. 10a sequence). This billow sourced a fall streak that terminated at the hotplate (i.e., at
699 the time t_0 indicated in the figure). However, the aircraft only clipped the top of this billow, and
700 it was only when sampling the billow seen ~ 13 s earlier that larger ice particle concentrations (\sim
701 $20,000 \text{ m}^{-3}$) (Fuller 2020; her Fig. 10) and larger LWC ($\sim 0.08 \times 10^{-3} \text{ kg m}^{-3}$; Fig. 5d) were
702 detected. Maximum reflectivities were the same in all three billows ($Z \sim 1 \text{ mm}^6 \text{ m}^{-3}$; 0 dBZ), so it
703 was assumed that imagery collected in the first billow (20:32:00 to 20:32:02) was representative
704 of what was falling toward the hotplate. The 2DS was used to image these particles (Fig. 11b);
705 with this instrument the maximum all-in particle size (in the horizontal direction perpendicular to
706 flight) is 1280 μm and the size resolution is 10 μm (Sect. 2.2). Most of the objects in Fig. 11b

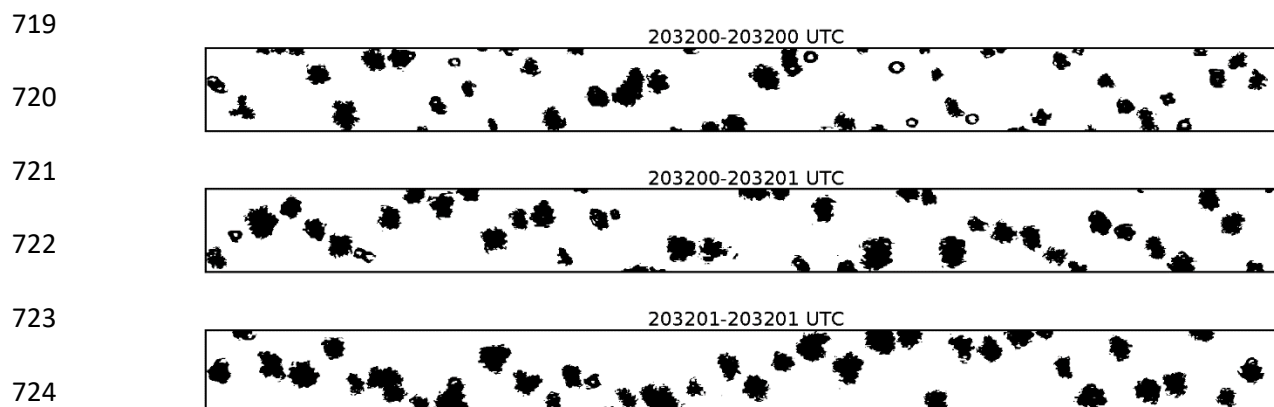
707 appear to be rimed and their mode size is $\sim 400 \mu\text{m}$. It is also noted that particles smaller than
708 $100 \mu\text{m}$ were eliminated from these images, however, compared to the $\sim 400 \mu\text{m}$ particles those
709 smaller than $100 \mu\text{m}$ were significantly less abundant (results not shown).

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711 (a)



718 (b)



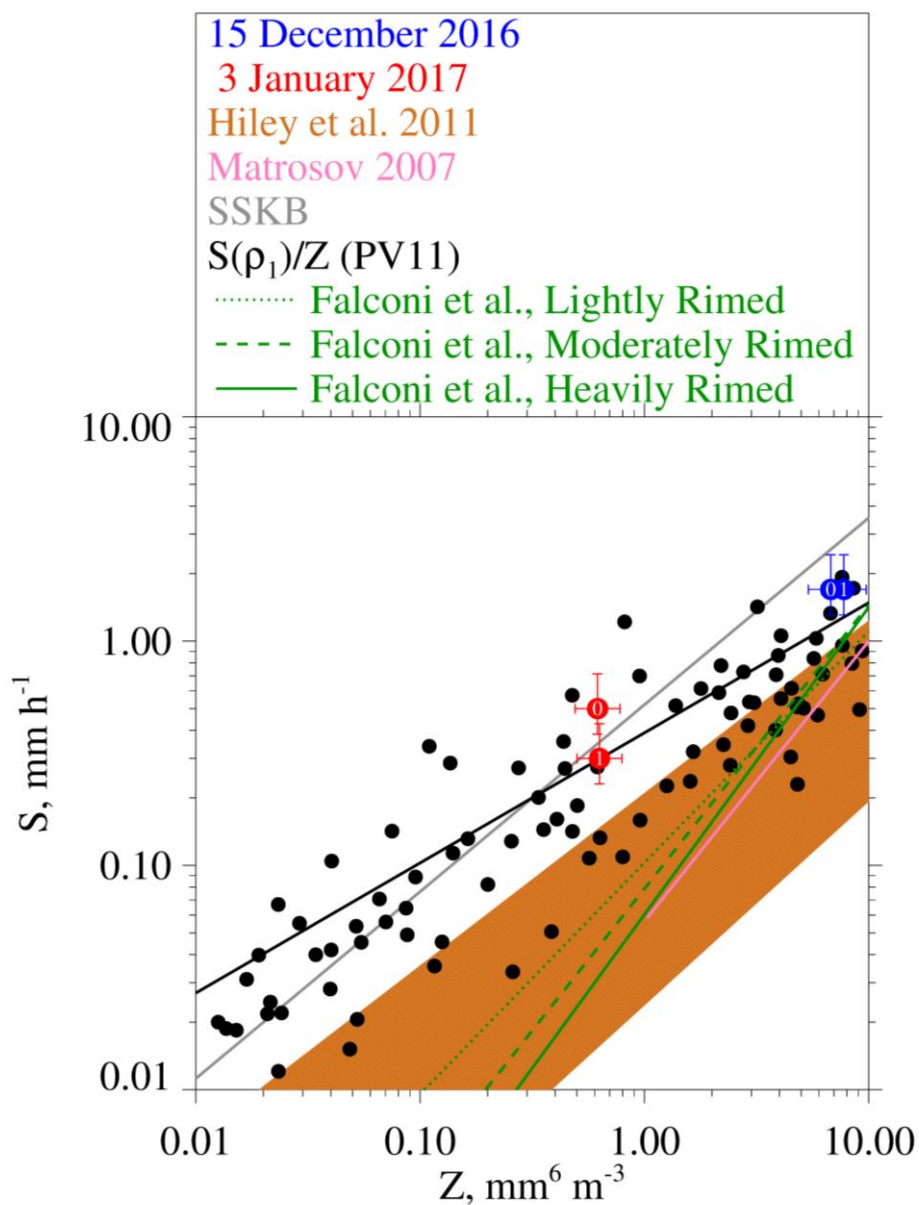
726 Figure 11 – (a) 2DP particle imagery from 15 December 2016. The height of the strips is 6400
727 μm . These particles are estimated to be representative of those that fell from flight level toward
728 the hotplate. (b) 2DS particle imagery from 3 January 2017. The height of the strips is 1280 μm .
729 These particles are estimated to be representative of those that fell from flight level toward the
730 hotplate.

731

732 3.7 – S/Z Relationships

733 Our S/Z pairs are presented in Table 6 where the indexes ($i = 0$ and $i = 1$) are used to
734 indicate results derived for the averaging intervals. In the penultimate column of Table 6,
735 reflectivities are not corrected for attenuation, however, in the last column of Table 6 and in Fig.
736 12, the attenuation-corrected reflectivities are presented. Reflectivities from the penultimate
737 column of Table 6, attenuations from Table 4, and Eq. 1 were used to calculate the corrected
738 reflectivities. Also shown in Fig. 12 (black filled circles) is a subset of the S/Z pairs from PV11's
739 Fig. 11 ($0.01 < Z < 10 \text{ mm}^6 \text{ mm}^{-3}$) and the PV11 best-fit line (black). Results from PV11 are
740 specified as $S(\rho_1)/Z$ because those authors applied the lower of two density-size functions (ρ_1),
741 and the lower of two fall speed-size functions, with airborne measurements, in calculations of
742 snowfall rates (Sect. 1 and Table 1).

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760 Figure 12 – Snowfall rate versus radar reflectivity. Red and blue circles are plotted at
761 attenuation-corrected reflectivities (Table 6) for the $i = 0$ and $i = 1$ averaging intervals. Error
762 bars on these points represent precisions of the reflectivity (Sect. 2.3) and snowfall rate (Sect.
763 2.4) measurements. Also plotted are the S/Z relationship lines from Sect. 1 and Table 1. These
764 are the S/Z lines defining the swath of S/Z relationships from Hiley et al. (2011), the S/Z
765 relationship from Matrosov (2007), the S/Z relationship abbreviated SSKB, PV11's best-fit line,

766 and the S/Z relationships from Falconi et al. (2018) (their Table 2). The $S(\rho_1)/Z$ points (black
767 filled circles) are a subset from PV11's Fig. 11 ($0.01 < Z < 10 \text{ mm}^6 \text{ mm}^{-3}$).

768 There are two potential biases in the values of snowfall rate we tabulate (Table 6) and
769 plot (Fig. 12). First, the two snowfall events had flight-level vertical wind velocities (Figs. 5b
770 and 5d) that were positive (upward) upwind of the ridgeline, and vice versa downwind of the
771 ridgeline. Except for the strongest downdraft on 3 January 2017, the magnitude of this variance
772 is $\sim 1 \text{ m s}^{-1}$ (Figs. 5b and 5d). Assuming 1 m s^{-1} was the downward wind immediately over the
773 hotplate, the snow particles would have approached the HP gauge faster than their fall speed.
774 Our basis for stating this is fall speeds for the mode sizes discussed in Sect. 3.6 (1600 and 400
775 μm) and our assumption that the particles were graupel. (Table 7 has these characteristic sizes
776 and fall speeds.) However, the conjectured relative effect of a downward wind is likely an
777 overestimate - because of divergence occurring as downward moving air approached the surface
778 - and because the sizes in Table 7 likely underestimate what fell to the hotplate. Relevant to the
779 last of these assertions, we used the altitude/T/RH measurements (Table 3) to calculate the
780 vertical distance available for growth via riming, and thus for a fall speed increase, between the
781 flight level and the lifted condensation level. Assuming an adiabatically-stratified liquid cloud
782 and unit collection efficiency (these assumptions overestimate growth by riming), and no change
783 of particle cross-section (underestimates growth by riming), our calculations indicate that relative
784 increases of size and fall speed were 40 and 20 %, respectively, on 3 January 2017, and that
785 these relative increases were a factor-of-two larger on 15 December 2016.

786

787 Table 7 – Estimates of snow particle fall speed

Date	Mode Size, μm	Assumed Particle Type	Fall Speed, m s^{-1}	Reference
15 December 2016	1600	graupel	1.4	PV11; assuming ρ_1 in their Fig. 5
3 January 2017	400	graupel	0.7	PV11; assuming ρ_1 in their Fig. 5

788

789

790 Second, there is concern that values of S from 3 January 2017 are underestimated.
791 Although values of S must be > 0 , we presented 1 Hz values (gray points, Fig. 8) approaching -
792 0.3 mm h^{-1} . Negative values resulted because we did not impose a threshold of 0 mm h^{-1} on the
793 uncorrected snowfall rates (this thresholding is discussed in Z18) and because negative snowfall
794 rate values (uncorrected for catch inefficiency) are amplified by the gauge-catch correction (Sect.
795 2.4). The implication is that 0.2 mm h^{-1} could be added to the one-minute averaged values of
796 snowfall rate in Table 6 and in Fig. 12. Here, the assumption is that an averaged S of -0.2 mm h^{-1}
797 ¹, in Fig. 8, indicates no snowfall at the hotplate; however, because the hotplate was operated
798 autonomously (Sect. 2.1) we have no way to verify the assumption.

799

800 4 – Results

801 Figure 12 shows our four snowfall rate/reflectivity pairs (red and blue circles) after the
802 reflectivities were corrected for attenuation. The error bars on these data pairs represent the
803 precision of the Z measurement (Sect. 2.3) and the precision of the S measurement (Sect. 2.4).
804 Presentation clarity was what guided the selection of S and Z axis ranges in this figure but with
805 the consequence that 32 of PV11's S/Z pairs are not shown because they plot at $Z > 10 \text{ mm}^6 \text{ m}^{-3}$.
806 The way that the PV11 data pairs scatter closest to $Z = 10 \text{ mm}^6 \text{ m}^{-3}$, combined with the fact that
807 the PV11 data pairs at $Z > 10 \text{ mm}^6 \text{ m}^{-3}$ are not shown, could lead to the interpretation that the
808 slope describing the best-fit relationship, at Z approximately $> 2 \text{ mm}^6 \text{ m}^{-3}$, should be decreased
809 relative to the actual slope of the PV11 best-fit line. Readers who view PV11's Fig. 11 will
810 conclude that this interpretation is not warranted.

811 As is discussed in Sect. 1, computation-based S/Z relationships have inputs from
812 parameterized descriptions of density, shape, fall speed, PSD, and particle size. The
813 computation-based S/Z relationships are in the top three rows of Table 1; the subsequent two
814 rows of the table have S/Z relationships that resulted from a hybridization of measurements and
815 calculations (PV11 and Falconi et al. 2018).

816 We now compare our snowfall rates (fourth column of Table 6) to snowfall rates where
817 they plot on an S/Z relationship line evaluated at one of our attenuation-corrected reflectivities.
818 The departure between these is reported as a relative S difference expressed as $|(S_{\text{HP}}-S)|/S$ where
819 S_{HP} is from Table 6 and where S is on an S/Z relationship line. All possible comparisons are
820 presented graphically in Fig. 12. Table 1 has both the minimum relative S differences and the
821 salient maximum relative S differences. The comparisons will be discussed in the order of
822 presentation in Table 1.

823 In comparisons of our snowfall rates and the upper-limit S/Z relationship line from Hiley
824 et al. (2011) the relative difference is no smaller than 0.7 and 1.0 on 15 December and 3 January,
825 respectively. These minimum relative differences exceed the hotplate precision (Sect. 2.4) by at
826 least a factor of two. It is concluded that our paired values of undercatch-corrected precipitation
827 rate and attenuation-corrected radar reflectivity provide evidence that a calculation of S based on
828 the Hiley et al. (2011) upper-limit, when applied to rimed snow particles, is associated with a
829 low-biased estimate of S. A retrieval based on Hiley et al.'s average S/Z relationship (not
830 shown), which bisects the orange region in Fig. 12, corresponds to an even larger low bias. This
831 is a concern because Hiley et al. (2011) used their average S/Z relationship to retrieve global
832 snowfall distributions and since global observations reported in Wang et al. (2013) document the
833 frequent occurrence of supercooled liquid within snowing clouds.

834 Figure 12 shows the separation between our measurements and the Matrosov (2007)
835 calculation. The separation is about a factor of two (minimum relative difference = 1.4) for the
836 points obtained on 15 December 2016 and corresponds to an underestimation of S (low bias)
837 when compared to our measurements. The points from 3 January 2017 plot at an attenuation-
838 corrected reflectivity smaller than the lower-limit of the calculation (Matrosov 2007). Since the
839 particle images (Fig. 11a-b) reveal no evidence of the particle type modeled by Matrosov (2007)
840 (aggregates), it is not surprising that the Matrosov S/Z relationship is not representative of our
841 measurements.

842 One plausible reason for the low bias discussed in the previous two paragraphs is the
843 smaller density implicit in most computationally-based S/Z relationships and especially those
844 which assume that snow particles are crystals. Densities are quite different for crystals versus
845 that for rimed snow particles. For example, in Brown and Francis (1995), assuming a 2 mm

846 crystal, the density is $\sim 30 \text{ kg m}^{-3}$, whereas in PV11 (their Eq. 1), assuming a 2 mm graupel
847 particle, the density is $\sim 200 \text{ kg m}^{-3}$. Because aggregates are collections of crystals, this
848 comparison of crystal and graupel densities also seems relevant to a comparison of graupel and
849 aggregate snow particle densities.

850 Figure 12 compares our S_{HP} / Z' data pairs to the SSKB S/Z relationship line and Table 1
851 presents the relative differences between the data pairs and the SSKB line. Compared to the S/Z
852 relationship represented by top of the orange region in Fig. 12, and compared to the Matrosov
853 2007 relationship, the SSKB line plots closer to our data points (minimum relative difference \sim
854 0.3). We note that the only instances of $S_{HP} < S$ are three of four comparisons of our
855 measurements to the SSKB relationship. A possible reason for this is that the density applied in
856 SSKB (Table 1) is not entirely representative of conditions during our study. An analysis of the
857 sensitivity of the SSKB to a change in density is needed to investigate our assertion.

858 Comparisons of our S_{HP} / Z' data pairs and PV11's best-fit line are also in Table 1. The
859 table demonstrates that the agreement is reasonable - minimum relative difference no larger than
860 0.3 – and Fig. 12 shows that our data pairs plot at or above the PV11 best fit line.

861 Based on data from PV11 and our S_{HP} / Z' data pairs, as well as the S/Z relationship
862 abbreviated SSKB, it is expected that the S/Z relationships reported by Falconi et al. (2018) for
863 rimed snow particles (Sect. 1) would plot higher in S-versus-Z space than is illustrated in Fig. 12.
864 Notably, only the upper-end of the Falconi et al. lines (i.e., at $Z > 8 \text{ mm}^6 \text{ m}^{-3}$) plot above the
865 upper-limit that Hiley et al. (2011) developed for unrimed snow particles. A plausible
866 explanation for the lower-than-expected S/Z relationships of Falconi et al. is now offered.
867 Falconi et al. used liquid water path as a proxy for the extent of snow particle riming (von Lerber

868 et al. 2017). A consequence may have been that the proxy did not dependably exclude unrimed
869 snow particles (crystals and aggregates) from the riming categories of Falconi et al. If this was
870 the case, then the data groupings that were the basis for the Falconi et al. S/Z relationships may
871 have been affected. When comparing the heavily-rimed S/Z relationship of Falconi et al. to our
872 S_{HP} / Z' data pairs we find that the minimum relative differences are 0.6 (December 15) and 8.5
873 (January 3) (Table 1). Additionally, the differences are 0.5 (December 15) and 5.9 (January 3)
874 when applying the moderately-rimed S/Z relationship of Falconi et al. (results not shown).
875 Further research is needed to resolve the reason for the mismatch between the snowfall
876 rate/reflectivity pairs reported here and the S/Z relationships reported in Falconi et al.

877 Our conclusion that the upper-limit S/Z relationship from Hiley et al. (2011)
878 underestimates S would be modified if our WCR-derived reflectivities were negatively biased.
879 Assuming the reflectivities are negatively biased by 2.5 dBZ, the minimum relative differences
880 discussed previously change to 0.1 and 0.3 on 15 December and 3 January, respectively. A bias
881 in reflectivity of this magnitude cannot be ruled out but neither can a positive bias of the same
882 magnitude (Sect. 2.3). The latter increases the minimum relative differences to 1.6 and 2.2 on 15
883 December and 3 January, respectively. In each of these calculations we have summed the
884 attenuations (Table 4) with ± 2.5 dBZ and used Eq. 1 to calculate error-perturbed reflectivities.

885 The scatter of measurements in Fig. 12, the plausibility of a -2.5 to +2.5 dBZ bias in
886 WCR reflectivity measurements, and error in measurement of S (Sect. 2.4), indicate that refined
887 techniques will be needed in future investigations which apply the approach described here.
888 Taking into consideration the goal of evaluating snowfall rates from space, some advance in
889 satellite remote sensing also seems warranted. One issue is diagnosing where riming is occurring
890 within clouds. Both lidars and radiometers can sense supercooled liquid water from space (e.g.,

891 Battaglia and Panegrossi, 2020), and if combined with Doppler radars operating at multiple
892 wavelengths, can diagnose the presence of rimed precipitation particles. Despite limitations of
893 the multiple-wavelength Doppler method in scenarios with vertical air speed comparable to and
894 larger than particle fall speed (Vogl et al. 2022), the method has been validated in ground-based
895 field studies (Kneifel et al. 2015; Mason et al. 2018). Technical challenges also remain for
896 implementing the method from space (Battaglia et al. 2020).

897 **5 – Conclusions**

898 We have reported surface measurements of S and near-surface measurements of Z . The
899 latter came from overflights of a ground site, where a precipitation gauge was operated, and were
900 acquired using an airborne W-band radar. The values of Z were corrected for attenuation.

901 The reported S_{HP} / Z' pairs plot at or above the S -versus- Z best-fit line of PV11 (Fig. 12)
902 and the minimum relative S difference (Table 1) is no larger than 0.3. The PV11 data came from
903 airborne measurements of W-band reflectivity, acquired within ± 100 m of flight level, and from
904 coincident measurements of snow particle imagery. PV11 used a density-size function, a fall
905 speed-size function, and measurements (PSD and particle images) to calculate S for snow
906 particles that were classified as both rimed crystals and graupel. This classification is also
907 consistent with the particle imagery we have presented (Fig. 11).

908 We have documented a substantial difference in comparisons between our snowfall rate
909 measurements and reflectivity-dependent snowfall rates calculated using an upper-limit S/Z
910 relationship (Hiley et al. 2011). This S/Z relationship produces an underestimate of the snowfall
911 rate (Fig. 12) when compared to our measurements. We also report substantial snowfall rate
912 underestimates in comparisons of our measurements to the S/Z relationship developed by

913 Matrosov (2007). The underestimates obtained using the Hiley et al. and Matrosov S/Z
914 relationships are perhaps expected given that the density factored into those S/Z calculations is
915 small compared to that for rimed snow particles. It is also expected that the larger density and
916 spherical shape applied in the SSKB S/Z relationship contributed to the better agreement seen in
917 the comparison of the SSKB relationship to our snowfall rate measurements. Our conclusion is
918 that some snowfall retrievals (e.g., Hiley et al. 2011) will underestimate S for weather targets
919 containing rimed snow particles. We also state that our conclusion is at odds with measurements
920 and analysis in Falconi et al. Those researchers reported S/Z relationships for rimed snow
921 particles which in instances with $Z < 8 \text{ mm}^6 \text{ m}^{-3}$ plot below the upper-limit of Hiley et al. (Fig.
922 12). A consequence is that the minimum relative S differences in our comparison to Falconi et al.
923 (assuming Falconi et al.'s heavily-rimed classification) is comparable to and larger than in our
924 comparison to Hiley et al.'s upper-limit S/Z relationship (Table 1).

925 New research is needed to refine the S/Z relationship for rimed snow particles. This could
926 be computational – e.g., investigation of the utility of parameterizing S in terms of both Z and
927 density – or could be observational. Unlike the investigation of PV11, where only an airborne
928 platform was employed, we have demonstrated that useful information can be obtained using
929 coordinated ground-based and airborne systems. Provided all key measurements are acquired (S,
930 PSD, particle imagery, and Z), another approach would be with only ground-based
931 instrumentation. This would avoid some of the complications encountered in this study,
932 including W-band attenuation and a reliance on particle imagery acquired aloft. A study with
933 both ground-based and airborne systems would also be useful for understanding an S/Z
934 mismatch apparent at $Z < 8 \text{ mm}^6 \text{ m}^{-3}$. Elements of the mismatch are the measurements reported
935 here, PV11's best-fit line, and the measurement-based S/Z relationships reported by Falconi et al.

936 (2018). These three research teams reported measurements relevant to the development of an S/Z
 937 relationship for rimed snow particles.

938 **6 – Appendix**

939 This appendix explains how HP (hotplate) and WCR (Wyoming Cloud Radar) averages
 940 were evaluated. The scheme starts with an HP averaging interval (duration 60 s) and derives a
 941 WCR averaging interval and a WCR averaging domain. The latter encompasses a subset of the
 942 altitude-time cross-section sampled by the WCR. The top boundary of the domain was derived
 943 using vertical-component Doppler velocities within the interval/domain. Because of this
 944 dependence, the line defining the top boundary was derived iteratively.

945 With the overflight time symbolized t_o , the beginning and ending times of two 60-second
 946 HP averaging intervals are

$$947 \quad t_{HP,B} = t_o \quad (A1)$$

$$948 \quad t_{HP,E} = t_o + 60 \quad (A2)$$

949 Since two adjacent HP averaging intervals are evaluated in this analysis, we express the
 950 averaging times with the following recursive equations

$$951 \quad t_{HP,B}(i) = t_o + i \cdot 60 \quad (A3)$$

952 and

$$953 \quad t_{HP,E}(i) = t_o + (i+1) \cdot 60. \quad (A4)$$

954 In Eqs. A3-A4 the index is $i \in \{0, 1\}$. A special case with $i = 2$ is also analyzed (Sect. 3.5).

955 Analogous to the recursion in Eq. A4, the ending time of a WCR averaging interval is

$$956 \quad t_{WCR,E}(i) = t_o - i \cdot 60 \cdot v_w / gs. \quad (A5)$$

957 Here v_w is a wind advection speed (discussed below) and the second term on the rhs is a wind
 958 advection distance divided by the WKA (Wyoming King Air) ground speed (gs). Analogous to
 959 the Eq. A5, the beginning time of a WCR averaging interval is

$$960 \quad t_{WCR,B}(i) = t_{WCR,E} - (i+1) \cdot 60 \cdot v_w / gs \quad (A6)$$

961 The wind advection speed (v_w) in Eqs. A5-A6 was calculated using an altitude-
 962 dependent west-to-east wind velocity (u) and an altitude-dependent south-to-north wind velocity
 963 (v). These altitude-dependent component velocities were calculated using the horizontal wind
 964 vectors in the penultimate and last columns of Table 3. Plots of the component velocities versus
 965 altitude and the linear functions used to relate component velocities to altitude are presented in
 966 Figs. A1a-b.

967 An altitude ($z' = 3400$ m) was assumed for evaluating the horizontal wind advection
 968 vector. This is the altitude of the ridges west and northwest of the HP site (Figs. 3a-b).

969 The WKA track vector (Table 3) defines the vertical plane of the WCR measurements.
 970 We assumed that wind advection of snow particles occurred parallel to this vector. With the
 971 assumption stated in the previous paragraph, the horizontal wind advection speed (v_w) was
 972 calculated as the projection of the horizontal wind vector onto the track vector.

$$973 \quad v_w = \frac{u(z') \cdot gs_x + v(z') \cdot gs_y}{(gs_x^2 + gs_y^2)^{1/2}} \quad (A7)$$

974 In Eq. A7 the west-to-east and south-to-north components of the track vector are symbolized gs_x
 975 and gs_y . Vector representations of the track vector are in Table 3. On 14/15 December 2016 and
 976 3 January 2017, the values of v_w are 7.4 and 8.9 m s⁻¹, respectively.

977 In addition to the properties g_s and v_w used to evaluate Eqs. A5-A6, a WCR averaging
 978 interval/domain was evaluated using a snow particle downward speed (Eq. A8).

$$979 \quad v_p = |\langle V_D \rangle| + \sigma_{V_D} \quad (\text{A8})$$

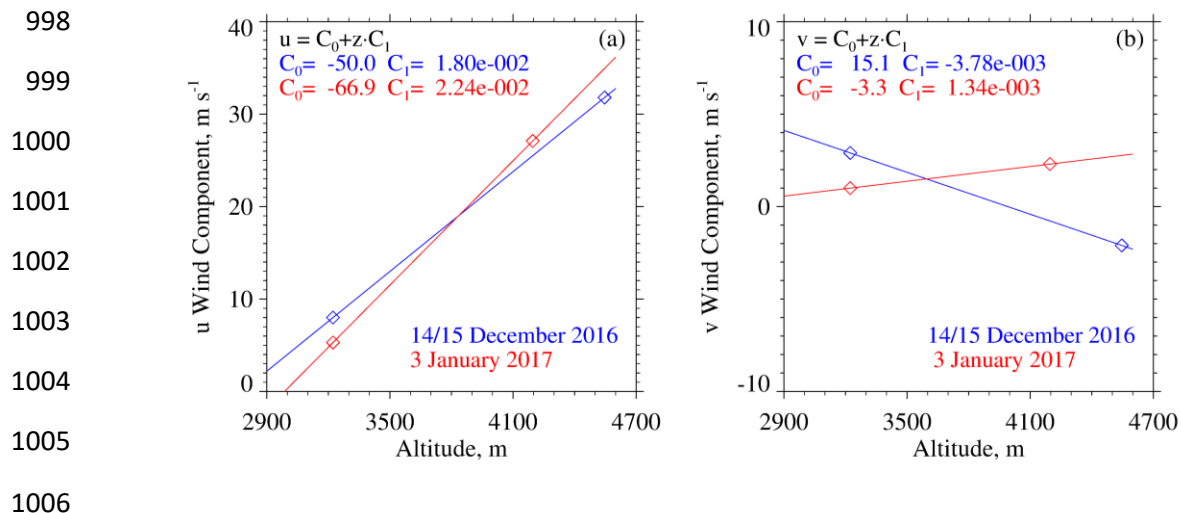
980 Here, $\langle V_D \rangle$ is the average of Doppler velocities within an averaging interval/domain,
 981 $|\langle V_D \rangle|$ is the absolute value of the average, and σ_{V_D} is the standard deviation of the average.

982 On both the lhs and rhs of Eq. A8, all terms are greater than zero.

983 We interpret v_p as the maximum likely snow particle speed toward the ground. There are
 984 three reasons for this: 1) For the WCR averaging intervals/domains we analyzed, values of
 985 $\langle V_D \rangle$ were consistently less than zero (Table 6). This indicates that snow particles (on
 986 average) were moving toward the ground. 2) Again, for the WCR averaging intervals/domains
 987 we analyzed, σ_{V_D} was comparable to $|\langle V_D \rangle|$. This indicates that turbulent eddies transported
 988 snow particles upward and downward at a speed comparable to their downward speed in still air.
 989 3) The V_D are reflectivity weighted (Haimov and Rodi 2013) and are thus indicative of the
 990 motion of the largest particles within an averaging interval/domain.

991 We now focus on the top boundary of a WCR averaging interval/domain. Figures 6b and
 992 6d have representations of the boundary. The slope defining this boundary was calculated as
 993 $-v_p \cdot g_s / v_w$. That is, particles below this boundary moved downward sufficiently fast and
 994 horizontally sufficiently slow to advect reasonably close to the hotplate. Starting with diagnosed
 995 values of g_s and v_w , the values of v_p and slope, were derived iteratively. The precision of the
 996 derived v_p is $\pm 0.1 \text{ m s}^{-1}$.

997



1007 Figure A1 – (a) West-to-east (u) wind velocity derived using measurements from the WKA and
 1008 the AmeriFlux (AF) tower. Also shown is the linear function used to relate u to altitude. (b)
 1009 South-to-north (v) wind velocity derived using measurements from the WKA and AF. Also
 1010 shown is the linear function used to relate v to altitude. WKA and AF velocities are presented as
 1011 vectors in the penultimate and last columns of Table 3.
 1012

1013 Code/Date availability. The WKA and WCR measurements can be obtained from the SNOWIE
1014 data archive of NCAR/EOL, which is sponsored by the National Science Foundation. Hotplate
1015 gauge measurements are at <https://doi.org/10.15786/20103146>. The US-GLE AmeriFlux
1016 measurements are at <https://ameriflux.lbl.gov/>. The Brooklyn Lake SNOTEL gauge
1017 measurements are at <https://www.wcc.nrcs.usda.gov/snow/>. Merged Hotplate, SNOTEL, and
1018 AmeriFlux data sequences from 14/15 December 2016 and 3 January 2017 are in Snider (2023).
1019 Computer programs used to read, process, and plot the data are available on request from J.
1020 Snider.

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1022 measurements were performed by SF, SM, SH, MB, and JS. SF wrote her MS dissertation, and
1023 this was adapted for this paper by JS. KS processed the snow particle imagery. AM maintained
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1025

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1034

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