We thank the referees for their time reviewing our manuscript and their useful comments and feedback. Based on the reviewers' feedback, we have made several changes which we feel significantly improves the manuscript.

Below, reviewer comments are in **bold** while our responses are in regular type. Attached we have also provided a 'track changes' version of the manuscript, with added text in blue and deleted and/or moved text in red.

Comment by Anonymous Referee #1

General Comments

Overall, the paper is well written, and makes some important points regarding the limitations of simple performance metrics and the need for more intensive investigations of measurement error. I agree with the conclusions of the paper in principle, but I think that the paper could better support these conclusions through its examples.

Response 1: Thank you very much for the positive comments, and we appreciate the suggestions to better support our arguments. In the following paragraphs we have addressed this through a more detailed explanation of the limitations and advantages of common metrics, as well as revised figures to better illustrate and support the conclusions made.

As written, besides the contrived example of Figure 2, I don't see a clear case where differences and deficiencies in the measurements are not at least hinted at through relatively worse simple performance metric values (R-squared, RMSE). As shown in several examples of Section 4, the simple performance metrics do have utility in allowing comparisons between alternative measurement devices or techniques; for the most part, the sensors showing difficulties in the B-A and REU plots also showed relatively worse performance metric values. This is partly due to how these results are presented; they mostly compare data from common collocation experiments at the same location and covering the same time period, and therefore represent situations where it would be more appropriate to compare simple performance metrics (this is well stated in lines 394-396). The exception is Figure 6, but in that case, it isn't clear that the B-A or REU plots show any more ability to anticipate the poor observed performance at the roadside site than the simple performance metrics; rather, this is a general issue of relying on single-site collocation studies for characterization. More directly relevant to the topic of the paper would be to show attempts to compare different collocation datasets using simple metrics only, and to illustrate the shortcomings

of that approach; these shortcomings can then be addressed through the approaches you suggest. Perhaps such an example might be constructed from the existing data you present in the paper. For example, a collocation dataset could be divided across time by taking data collected in different seasons (if possible) and treating these as separate collocation experiments. In different seasons, the same sensor could have different performance metrics due to the differences in concentrations and variability in environmental conditions between seasons. These differences and their effects on errors likely would be much more apparent in B-A or REU plots (e.g., the collocation data would span different sections on the horizontal axis). Therefore, the information on error characteristics from each collocation analyzed via B-A or REU plots would tend to complement each other, as opposed to the simple performance metrics which might seemingly contradict each other. This is just a thought; while in general I agree with the logic underlying the arguments being presented here, I don't think that the examples, as they are currently presented, do a strong enough job of backing up these arguments.

Response 2: We thank the reviewer for this very useful comment. We agree with the reviewer that simple performance metrics do have utility. However, we argue that although these metrics are useful as a quick assessment or sanity check of performance, approaches such as the BA/REU plots enable a potential end user to view the nature of the errors and thus assess how these errors will impact any end use application. We appreciate that we potentially did not make this clear enough in the initial manuscript, and have therefore expanded the example given in the introduction (lines 48-53) and we have added the following text to "2.1 Performance indices, error structure and uncertainty" (lines 125-139):

When evaluating multiple sensors during a colocation experiment, single metrics can be a useful way to globally compare instruments/sensors. However, these metrics do little to communicate the nature of the measurement errors and the impacts these will have in any end use application, in part because they reduce the error down to a single value (Tian et al., 2016). Even more if a specific concentration range is of paramount interest to the end-user, these metrics are not capable of characterising the weight of noise and/or the bias effect. The R² shows globally the data set linearity and gives an idea of the measurement noise. However, it is unable to distinguish whether a specific range of concentrations is more or less linear (or more or less noisy) than another. Similarly, the RMSE is also a very useful metric and perhaps more complete than R², as it considers both noise and bias (although they need to be explicitly decomposed from RMSE). Nevertheless, the RMSE is an average measure (of noise and bias) over the entire dataset under analysis. Using combinations of simple metrics increases the information communicated, but does not necessarily make it easy to assess how the errors will likely impact a particular measurement application. Visualising the absolute and relative

measurement errors across the concentration range (unreachable by global metrics) enables end users to view the errors, and any features (non-linearities, step changes, etc.) that would impact the measurement but that global metrics (and in some cases time-series and/or regression plots) are incapable of showing.

Complementary to the text added to the manuscript we have taken the reviewers suggestion of better using the QUANT dataset to support our arguments. In order to explicitly demonstrate the advantages of the BA and REU plots we have updated figure 5 using data from sensors with different error characteristics. We have also updated figure 6, as suggested by the reviewer, to present data from the same sensor but during different periods, in addition to data from an identical sensor at a different location. The revised Figures 5 and 6, along with the associated edited text, are shown below. We feel these plots much better support the arguments made in the paper, and want to thank the reviewer again for suggesting this. We have also updated all the figures to show the density of data points, as we feel this further increases the information communicated:

Figure 5 shows two colocated measurements from two different LCS devices: one measuring NO2 (apanels) and the other O3 (b-panels). Both measurements are compared with colocated reference measurements at an urban background site in the city of Manchester. Unlike the modelled instruments in Sect. 4.1, the combination of error sources is unknown in this case and we can thus only assess the LCS measurement performance through comparison with the reference measurements using metrics and visual tools.

Single value metrics indicate an acceptable performance for both measurements: high linearity (both R^2 are higher than 0.8) and relatively low errors (RMSE ~ 5ppb). However, the plots present the data in a variety of ways that enable the user to identify patterns in the measurement errors that would be less obvious if only global metrics were used. For example, the NO2 sensor (LCS1, a-panels) has a nonlinear response that is almost imperceptible from the regression plot but stands out in the B-A plot. Furthermore (despite the high R^2 and relatively low RMSE), the REU plot shows high relative errors that do not meet the Class 2 DQO for the measured concentration range. Regarding the O3 sensor (LCS2, b-panels), the B-A plot shows two high density measurement clusters, one with positive absolute errors (over-measuring) and a larger one with negative errors (under-measuring). These are the result of a step change in the correction algorithm applied by the manufacturer and could easily have been missed if only summary metrics and a regression plot were used, especially if the density of the data points was not coloured.

It is worth noting that these plots do not directly identify the source of the proportional bias, with sensor response to the target compound or another covarying compound possible, but provides information on how much it impacts the data.

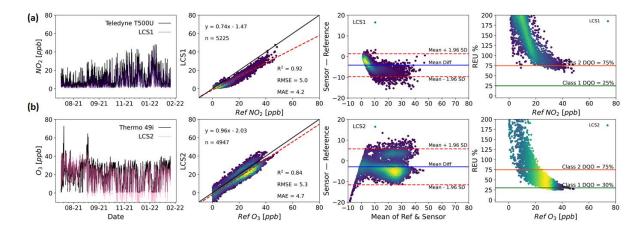
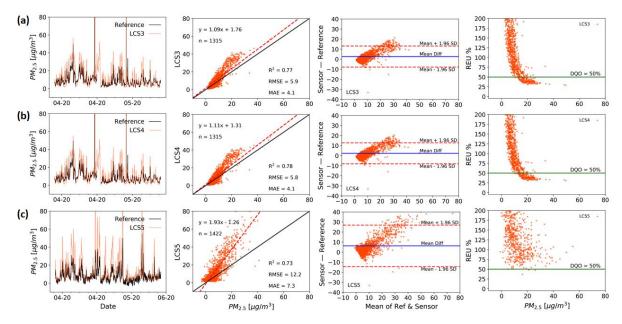


Figure 5. Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels; NO2 Class 1 DQO = 25% & Class 2 DQO = 75%; O3 Class 1 DQO = 30% & Class 2 DQO = 75%) for NO2 (apanels) and O3 (b-panels) measurements by two LCS systems of different brands in the same location and time span (Manchester Supersite, July 2021 to February 2022. Time res 1 h). All but the time-series plots, have coloured by data density.

We have also replaced the "old" figure 6 for the one below, in which we present two of the same sensors as previously, but now LCS3 is shown for two different periods: panel a, from Apr to May 2020; panel b, Oct to Nov 2020 (exactly 6 months after the initial period). For LCS4 (panel c) the period is also Apr to May 2020:



Old figure 6.

Figure 6 shows three out-of-the-box PM2.5 measurements made by two devices (LCS3 & LCS4) from the same brand in spring (LCS3: a-panels; LCS4: c-panels) and in autumn (b-panels, only LCS3). The colocation shown correspond to two different sites: an urban background site (LCS3, a and c-panels) and a roadside site (LCS4, c-panels).

As the regression and the B-A plots show, all LCS measurements in Fig. 6 have a proportional bias compared with the reference, with the LCS over predicting the reference values. The device at the urban background site (LCS3) show a dissimilar performance in spring and autumn, indicating that the errors this device suffers are differently influenced by local conditions in the two seasons (all the duplicates at the urban background show the same pattern). While for LCS3 during spring the error have a more linear behaviour, in autumn a non-linear pattern is clearly observed in the regression and B-A plots. Despite the utility that single metrics can have in certain circumstances, the non-linear pattern goes completely unnoticed by them: while for the two different seasons RMSE and the MAE are almost constant the R² indicates a higher linearity for autumn.

A number of duplicates were deployed at both sites showing a very similar performance in terms of the single metric values but also in regard to the more visual tools (not shown here). This internal consistency is highly desirable, especially when LCS's are to be deployed in networks, as although mean absolute measurement error may be high, differences between identical devices are likely to be interpretable.

Having prior knowledge of the nature of the measurement errors allows informed experimental design prior to data collection. This is key if an end user is to maximise the power of a dataset, and the information it provides, to answer a specific question. For example, if an end-user wanted to identify pollution hotspots within a relatively small geographical area, then using a dense network of sensor devices that posses errors large and variable enough to make quantitative comparisons with limit values difficult (possibly due to an interference from a physical parameter like relative humidity) but show internal consistency could be a viable option. Providing the hotspot signal is large enough relative to any random error magnitude.

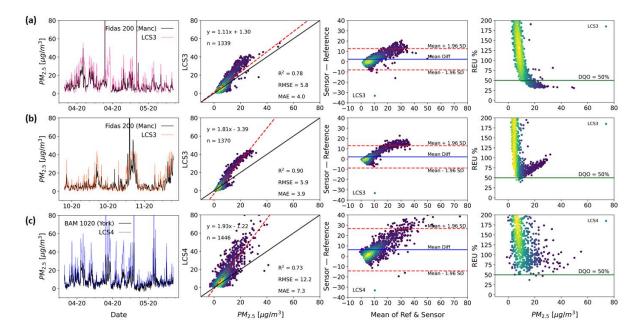


Figure 6. Two LCS systems (LCS3 & LCS4, same brand) measuring PM2.5 (Time res 1 h). While LCS3 is shown for the same location (Manchester) but unfolded in two different seasons (a-panels: Apr to May 2020; b-panels: Oct to Nov 2020), LCS4 is at a different location (c-panels: York, Apr to May 2020). Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels; DQOPM2.5 = 50%) are used to characterise the device's error structure. All but the time-series plots have been coloured by data density.

Specific Comments

Line 75: One of the commas here seems misplaced.

Response 3: Corrected.

Lines 78-79: Might be better stated as "a linear additive model is often assumed".

Response 4: Corrected.

Figure 1: REU should be defined before it is used in this figure.

Response 5: Corrected.

Line 103: Should be "data are communicated".

Response 6: Corrected.

Line 136: Remove "And" at start of sentence.

Response 7: Corrected.

Line 174: Suggest replacing "data" with "data set".

Response 8: Corrected.

Lines 306-310: This is background information, better included as part of the introduction, where it can be integrated with similar statements already there.

<u>Response 9:</u> We have preferred keeping that sentence as originally set in "4.2 Real-world instruments", but we have added a paragraph to the introduction expanding o this important point, where now it can be read (lines 72-78):

The covariance of many of the physical and chemical parameters of the atmosphere, makes accurately identifying particular sources of measurement interference or error very difficult in the real world. Unfortunately, specific laboratory experiments for the characterization of errors is complex and very expensive, resulting in many sources of error being essentially unknown for many measurement devices. The use of imperfect error correction algorithms that are not available to the end-user (e.g. in many LCS devices) makes error identification and quantification even more complex. For this reason, colocation experiments in relevant environments are often the best option to assess the applicability of a given measurement method for its intended purpose.

Lines 342-344: This is an important point, often used as justification for the use of LCS for applications like hotspot identification. I wonder if the authors could comment more on this, either here or elsewhere. My prompting question would be: what kinds of analysis approaches could be used to verify the ability of LCS to qualitatively identify meaningful differences between measurements, even in situations where relative uncertainties are too high to make reliable quantitative comparisons? Alternatively, is such a distinction (qualitative versus quantitative analysis) meaningful here, or is this "qualitative analysis" merely a quantitative analysis performed under higher relative uncertainty.

Response 10: The discussion of analysis approaches for specific applications is beyond the scope of

this work, and would likely be best supported through a number of case studies. In this work we focus

on tools that aid the interpretation of performance data in order to inform measurement strategies.

We agree with the reviewer that this is an important point, and we are of the opinion that, when it

comes to air quality measurements, qualitative analysis is merely quantitative analysis performed

under higher uncertainty. All the devices discussed in this work report values for target pollutants, and

as such are quantitative. Understanding the impact of likely measurement errors on the power of the

data to answer specific questions (e.g. hotspot identification) is important for all devices, not just LCS.

Especially as criteria pollutant limit values continue to decrease based on revised health evidence. We

therefore argue that more emphasis should be placed on informed experimental design when making

the measurements than on analysis methods that attempt to extract signals from data with

uncharacterised errors. In the case that LCS devices show high levels of internal consistency, an

informed experimental design should be able to take advantage of this to minimise the impact of

measurement errors on the information gathered from the measurements. We thank the reviewer

for highlighting that we have not said this explicitly in the text, and have added the text below to the

manuscript:

To what have been said in the original lines:

"This internal consistency is highly desirable, especially when LCS's are to be deployed in networks, as

although mean absolute measurement error may be high, differences between identical devices are

likely to be interpretable."

We have added the following to the text (lines 440-446):

Having prior knowledge of the nature of the measurement errors allows informed experimental design

prior to data collection. This is key if an end user is to maximise the power of a dataset, and the

information it provides, to answer a specific question. For example, if an end-user wanted to identify

pollution hotspots within a relatively small geographical area, then using a dense network of sensor

devices that posses errors large and variable enough to make quantitative comparisons with limit

values difficult (possibly due to an interference from a physical parameter like relative humidity) but

show internal consistency could be a viable option. Providing the hotspot signal is large enough

relative to any random error magnitude.

Line 367: Second "at" is superfluous.

Response 11: Corrected.

Line 370: "deviations" should be "deviation".

Response 12: Corrected.

Line 372: "appears" should be "appear".

Response 13: Corrected.

Lines 376-378: This is another important point. Since air quality regulations are based on these reference instruments, the traceability of LCS to these reference instruments has been a major focus of work. However, we must acknowledge that these references themselves are imperfect. Is it thus inappropriate to hold LCS to certain performance standards which the reference instruments themselves may not meet (especially if improperly operated)? On the other hand, what is the alternative to ensuring data quality? I think that, as you suggest, comparing different reference instruments among themselves should be done more frequently, and these intercomparisons more widely used as a benchmark against which the performance of LCS can be judged (instead of establishing arbitrary performance metric targets, espeically if these targets are not connected in some way to the different conditions under which the sensors are expected to operate). However, there is of course the practical question of the cost and feasibility of doing this at the necessary

Response 14: We thank the reviewer for this comment. We also feel that this is an important point and more attention needs to be placed on measurement uncertainty across the field of air pollution measurements, not just low cost sensors. Especially as limit values continue to fall. A more detailed discussion of this point and its implications is outside the scope of this work, but this is something we plan to expand on in the future and are in the process of collocating reference instruments for this purpose.

scale. Generally speaking, this is a major point which could be explored further by the authors either

Line 443: "data is" should be "data are".

Response 15: Corrected.

here or elsewhere.

Lines 450-453: The meaning of this sentence is unclear; consider breaking it into several simpler sentences.

Response 16: Corrected.

Previously it was said:

"If end users are to be able to make well informed decisions about device applicability to a particular task, then an argument can be made for information on the scale of the error corrections made to a

reported measurement to be made available, ideally alongside and a demonstration of its benefits in a relevant environment."

Now it can be read (lines 571-574):

If end users are to be able to make well informed decisions about device applicability then information on the scale of the measurement errors, and the impact of corrections made to minimise these, should be made available. Exemplar case studies in a range of relevant environments would also be highly valuable.

Comments by Anonymous Referee #2

This is a well written paper on air sensor uncertainty. Uncertainty in air sensors is a very important topic in the field. While the authors lay out a number of issues with current uncertainty methods their method seems to make only minor improvements on current methods. This paper is still helpful as it provides another way to visualize similar information in different ways which may speak more clearly to some people. I have a number of specific comments below that I hope the authors will address to improve the strength of the paper.

<u>Response 1:</u> We thank the reviewer for their comments. We would like to take this opportunity to clarify that our intention is not to replace the commonly used performance evaluation methods (R², RMSE, MAE, etc.). On the contrary, we think that they are useful tools, but like any tool they have certain deficiencies, and the end user needs to be aware of this. We have added more clarification on this point in a response to the first reviewer (please see Response #2 to reviewer 1).

Yes, these plots you are proposing may be more helpful than just R2, MAE, and RMSE but typically I'm seeing those metrics reported along with slope and intercept (and often a scatter plot). This seems like a false comparison you talk about repeatedly in the paper. Slope, intercept, and R2 seem to provide much of the same info as BA or REU plots just in a different form.

Response 2: We agree with the reviewer that using combinations of simple metrics in conjunction with a regression plot provides significantly more information than any single value metric. However, we argue that viewing the errors directly, as in the BA and REU plots, provides a clearer picture of the nature of the errors and thus how they would likely impact any application of the measurement device. Often in air pollution measurement applications there are specific target concentrations where the data is of most interest, for example around a legal limit value. Single value metrics give a global picture of a data set, but do not describe the error distribution in specific ranges or concentration intervals. The use of visualisations such as B-A and REU is complementary to the aforementioned metrics, with the added value that the user is now more aware of how the data looks in an absolute and/or relative error space, allowing them to distinguish some characteristics of interest.

In order to clarify this we have expanded the original text and now in lines 228-235 it can be read:

On the other hand, the use of visualisations such as B-A and REU is complementary to the aforementioned metrics, with the added value that the user is now more aware of how the data looks like in an absolute and/or relative error space, allowing them to distinguish some characteristics of interest. These visualizations are indeed more laborious and the interpretation can be challenging for non-experts, but they provide additional insights into the nature of the errors, not attainable by one

or more combined performance metrics: while B-A plots shows the noise (dispersion of the data) and the bias effect (tendency of the data) in an absolute scale, the REU can be explicitly decomposed in the noise and bias components (see Yatkin et al., 2022).

We admit that we did not use the best examples from our dataset to support these points, and have updated Figures 5 and 6 to better highlight the strengths of these approaches over just using global metrics (see Response #2 to Reviewer 1).

The BA plot seems to be just a less intuitive form of a scatterplot but maybe I'm missing how to interpret it in a helpful way? I see that there is value though in visualizing things in different ways since people see things differently.

Response 3: We agree with the reviewer that the scatter or correlation plot and BA plot are similar to a point, and much of the same information can be extracted. However, we argue that the BA plot is better placed to evaluate the agreement between two different methods for measuring the same variable than a scatter plot. As both methods being compared are in theory measuring the same parameter, but with different measurement errors, then it is to be expected that the two measurements should have good correlation when sampling over a wide range of parameter values. A high correlation (high R²), however, does not necessarily imply good agreement between the two measurements. It is also not always possible in atmospheric colocation studies to guarantee that a sufficiently wide range of parameter values will be observed.

In order to clarify the information that a Bland-Altman plot is capable of provide we have re-written and expanded the ideas originally set in lines 253-262:

In contrast to the regression plot -where the measured values from the two measurements (e.g. LCS vs Ref) are plotted against each other- the Bland-Altman plots essentially display the difference between measurements (abscissa) as a function of the average measurement (ordinate), enabling more information on the nature of the error to be communicated. This direct visualisation of the absolute error acknowledges that the true value is unknown and that both measurements have errors. The B-A plot enables the easy identification of any systematic bias between the measurements or possible outliers, and is the reason B-A plots are extensively used in analytical chemistry and biomedicine to evaluate agreement between measurement methods (Doğan, 2018). The mean difference between the measurements, (represented by the blue line in the figures), is the estimated bias between the two observations. The spread of error values around this average line indicates if the error shows purely random fluctuations around this mean, or if it has structure across the observed concentration range.

We therefore feel that the BA plot is better placed to show particular features or characteristics of the error than a scatter plot. It is hoped that the updated Figure 5 (see Response #2 to Reviewer 1) and the accompanying text now illustrates this more clearly.

In the end the plots you've made reveal very little about temperature, RH, and other pollutant interferent biases. Is there any way to modify the plots you are proposing to make them more helpful in addressing the issues you've brought up about interferents and error?

Response 4: We thank the reviewer for this comment. Yes, it would be possible to plot the absolute or relative error against variables other than those in the BA and REU plots in order to investigate correlations of error with other variables (e.g. relative humidity). Although these would no longer be BA or REU plots in the established definition, they could prove insightful in demonstrating an error correlation. Unfortunately, in the situation where the error sources are not known or fully understood (e.g. LCS) these plots would only be able to show correlations between error and variables, not diagnosing error causes. This is because in the real atmosphere there are a vast number of covarying physical and chemical parameters, making it very difficult to prove causation from correlation. We strongly feel that the best way in which to identify interference biases is through controlled laboratory experiments, where confounding variables can be controlled. However, as we mention in the text, this can also be very difficult due to real atmospheric complexity, and plots such as those discussed could be insightful in at least confirming the apparent presence or not of a bias correlation. Although a thorough demonstration of this is outside of the scope of this paper, and the focus of a future piece of work, we have added the following text to the manuscript discussion (lines 540-546, see the added text in blue font):

A major challenge comes from complex errors, such as interferences from other compounds or with environmental factors, that vary temporally and/or spatially. Similar graphical techniques to those presented above can be used to identify the existence of such relationships, but correcting for them remains a challenge. For example, the correlation between measurement errors and relative humidity could be explored by replacing the abscissa with measured relative humidity in both the B-A and REU plots. This would visualise the relationship between absolute and relative errors with relative humidity, but would not be able to confirm causality. The complex and covarying nature of the atmosphere means that the best way to identify a device error source is through controlled laboratory experiments, where confounding variables can be controlled, although these experiments are often difficult and expensive to perform in a relevant way.

Are all the DQOs for REU just percentages? There is no absolute target? (e.g. 25% or 5 ppb)

Response 5: Yes, the DQO (Data Quality Objective) is a defined percentage (defined by of the European

Air Quality Directive 2008/50/EC) but for regulatory purposes it needs to be evaluated at a fixed

concentration (called Limit Value, see GDE (2010) for its complete definition). However, as the main

message is focused on end-user needs and not necessarily for regulatory purposes, we have preferred

minimising the use of this as a performance target and instead the DQO is used just as a reference line

in the REU plots.

Did you consider how your estimation of uncertainty compares to the method in this recent paper?

https://amt.copernicus.org/articles/14/7369/2021/

Response 6: We thank the reviewer for this suggestion. This particular work considers uncertainty

from a prognostic perspective, in contrast to the diagnostic uncertainty discussed in our paper. To

make this distinction more explicit, we have added the following text in the introduction (lines 69-71):

Also, when the term "uncertainty" is used here, it is referring to "diagnosis uncertainty", in contrast

with "prognosis uncertainty" (see Sayer et al., 2020 for more details).

You may want to add a reference to the EPA performance targets. They recommend slope, intercept,

R2, RMSE, along with precision metrics, and making plots looking at error vs. T/RH/Dewpoint. Base

testing is colocations with enhanced lab testing.

Response 7: Thanks for the suggestions. Yes, we are aware of the EPA performance targets but for

simplicity we have tried to minimise the use of performance targets in the manuscript to not to deviate

our main message which is focused on the questions end-users may want to answer with the provided

data.

Can you include equations for RMSE, MAE, and REU.

Response 8: These metrics are widely used and we feel that including these are unnecessary. In

addition the REU derivation is not trivial, and would require a significant addition to the paper, which

we feel would detract from the paper. We would therefore prefer not to add the equations, as they

are defined elsewhere, but leave the decision to the editor. Instead, we have added the references

below to where to find the equations and definitions, and have also added a Zenodo and a github link

(lines 626-627) to an open source repository of python and R code to generate the plots, with example

data, enabling readers to take advantage of these tools.

For the RMSE and MAE equations (line 221): see the equation definitions in Cordero et al., 2018

For the REU equations (line 106): as defined by the GDE (2010)

Figures 1 and 2: These are really nice illustrations!

Response 9: Many thanks! We are glad you liked it.

Figure 1. can you define the acronyms (e.g. REU) that you haven't defined in the text yet.

Response 10: Corrected.

Line 353 do you need "roadside side" or just "roadside"

Response 11: Corrected.

Line 367: "at during" only need "during"

Response 12: Corrected.

1 Air pollution measurement errors: Is your data fit for

2 purpose?

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- Sebastian Diez (sebastian.diez@york.ac.uk); Pete Edwards (pete.edwards@york.ac.uk)
 - Abstract. When making measurements of air quality, having a reliable estimate of the measurement uncertainty is key to assessing the information content that an instrument is capable of providing, and thus its usefulness in a particular application. This is especially important given the widespread emergence of Low Cost Sensors (LCS) to measure air quality. To do this, end users need to clearly identify the data requirements a priori and design quantifiable success criteria by which to judge the data. All measurements suffer from errors, with the degree to which these impact the accuracy of the final data often determined by our ability to identify and correct for them. The advent of LCS has provided a challenge in that many error sources show high spatial and temporal variability, making laboratory derived corrections difficult. Characterising LCS performance thus currently depends primarily on colocation studies with reference instruments, which are very expensive and do not offer a definitive solution but rather a glimpse of LCS performance in specific conditions over a limited period of time. Despite the limitations, colocation studies do provide useful information on measurement device error structure, but the results are non-trivial to interpret and often difficult to extrapolate to future device performance. A problem that obscures much of the information content of these colocation performance assessments is the exacerbated use of global performance metrics (R2, RMSE, MAE, etc.). Colocation studies are complex and time-consuming, and it is easy to fall into the temptation to only use these metrics when trying to define the most appropriate sensor technology to subsequently use. But the use of these metrics can be limited, and even misleading, restricting our understanding of the error structure and therefore the measurements' information content. In this work, the nature of common air pollution measurement errors is investigated, and the implications these have on traditional metrics and other empirical, potentially more insightful, approaches to assess measurement performance. With this insight we demonstrate the impact these errors can have on measurements, using a selection of LCS deployed alongside reference measurements as part of the QUANT project, and discuss the implications this has on device end-use.

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1. Introduction

The measurement of air pollutants is central to our ability to both devise and assess the effectiveness of policies to improve air quality and reduce human exposure (Molina & Molina, 2004). The emergence of low-cost sensor (LCS) based technologies means a growing number of measurement devices are now available for this purpose (Morawska et al., 2018), ranging from small low-cost devices that can be carried on an individual's person all the way through to large, expensive reference and research-grade instrumentation. A key question that needs to be asked when choosing a particular measurement technology is whether the data provided is fit for purpose (Andrewes et al., 2021; Lewis & Edwards, 2016). In order to answer this, the user must first clearly define the question that is to be asked of the data, and thus the information required. For example, a measurement to characterize "rush hour" concentrations, or to determine if the concentration of a pollutant exceeded an 8 h average legal threshold value at a particular location would demand a very different set of data requirements than a measurement to determine if a change in policy had modified the average pollutant concentration trend in a neighbourhood. Considerations such as measurement time resolution and ability to capture spatial variability would be important for such examples (Feinberg et al., 2019). Would the R² or RMSE or any other global singlevalue metric be enough to decide between the different device's options? Considerations such as the origin of the performance data, type of experiment (laboratory or colocation) (Jiao et al., 2016), the test location (Feenstra et al., 2019) and period (i.e. duration, season, etc.), the LCS and reference measurement method (Giordano et al., 2021), measurement time resolution and ability to capture spatial variability (Feinberg et al., 2019) would be important factors to consider for such examples. The measurement uncertainty is also of critical consideration, as this ultimately determines the information content of the data, and hence how it can be used (Tian et al., 2016).

All measurements have an associated uncertainty, and even in highly controlled laboratory assessments, the true value is not known, with any measurement error defined relative to our best estimate of the range of possible true values. However, quantifying and representing error and uncertainty is a challenge for a wide range of analytical fields, and often what these concepts represent is not the same to all practitioners. This results in a spectrum of definitions that take into account the way truth, error, and uncertainty are conceived (Grégis, 2019; Kirkham et al., 2018; Mari et al., 2021). For atmospheric measurements assessing uncertainty is complex and non-trivial. Firstly, given the "true" value can never be known, an agreed reference is needed. Secondly, the constantly changing atmospheric composition means that repeat measurements cannot be made and the traditional methods for determining the random uncertainty are not applicable. And finally, a major challenge arises from the multiple sources of error both internal and external to the sensor that can affect a measurement. Signal responses from a non-target chemical or physical parameter or electromagnetic interference are examples of an almost limitless number of potential sources of measurement error. In this work, we will follow the definitions given by the International Vocabulary of Metrology (JCGM, 2012) for measurement error ("measured quantity value minus a reference quantity value") and for measurement uncertainty ("non-negative parameter characterising the dispersion of the quantity values being attributed to a measurand, based on the information used"). Also, when the term "uncertainty" is used here, it is referring to "diagnosis uncertainty", in contrast with "prognosis uncertainty" (see Sayer et al., 2020 for more details).

The covariance of many of the physical and chemical parameters of the atmosphere, makes accurately identifying particular sources of measurement interference or error very difficult in the real world. Unfortunately, specific laboratory experiments for the characterization of errors is complex and very expensive, resulting in many sources of error being essentially unknown for many measurement devices. The use of imperfect error correction algorithms that are not available to the end-user (e.g. in many LCS devices) makes error identification and quantification even more complex. For this reason, colocation experiments in relevant environments are often the best option to assess the applicability of a given measurement method for its intended purpose.

The mentioned difficulties in defining and quantifying uncertainty across the full range of end-use applications of a measurement device, means that often the quoted measurement uncertainty is not applicable, or in some cases not provided or provided in an ambiguous manner. This makes assessing the applicability of a measurement device to a particular task difficult for users. In this work, we investigate the nature of common air pollution measurement errors, and the implications these have on traditional goodness-of-fit metrics and other, potentially more insightful approaches to assess measurement uncertainty. We then use this insight to demonstrate the impact these errors can have on measurements, using a selection of LCS deployed alongside reference measurements as part of the UK Clean Air program funded QUANT (Quantification of Utility of Atmospheric Network Technologies) project, a 2-year colocation study of 26 commercial LCS devices (56 gases measurements and 56 PM measurements) at multiple urban, background and roadside locations in the UK. After analysing some of the real-life uncertainty characteristics we discuss the implications this has on data use.

2. Error characterization

When characterising measurement error, in the absence of evidence to the contrary it is often assumed a linear additive model is often assumed. Once the analytical form of the model is defined, its parameters aim to capture the error characteristics, and in the case of linear models (Eq. (1)), these are typically separated into three types (Tian et al., 2016): (i) proportional bias or scale error (b_1), (ii) constant bias or displacement error (b_0) and (iii) random error (ϵ) (Tian et al., 2016). Any measurement (y_i , e.g from the LCS) can therefore be thought of as a combination of the reference value (x_i) and the three error types, such that:

$$97 y_i = b_1 x_i + b_0 + \varepsilon (1)$$

As the simplest approximation, this linear relationship for the error characteristics is often used to correct for observed deviations between measurements and the agreed reference. It is worth to note, however, that this equation assumes time-independent error contributions and that the three error components are not correlated, which is often not the case on both counts (e.g. responses to non-target compounds). The parameter values determined for Eq. (1) are also generally only applicable for individual instruments, potentially in specific environments, unless the transferability of these parameters between devices has been explicitly demonstrated.

Figure 1 shows examples of how pure constant bias (a-panels), pure proportional bias (b-panels), and pure random noise (c-panels) would look like in time-series, regression, Bland-Altman (B-A) (Altman & Bland, 1983) and Relative Expanded Uncertainty (REU, as defined by the GDE (2010)) plots. In each of these ideal cases, the error plots enable the practitioner to view the error characteristics in slightly different ways, allowing the impacts of the observed measurement uncertainty to be placed into the context of the data requirements. In this work, we will

refer to them as "error types" (in contrast to "error sources"), which is the way they are distilled by the linear error model.

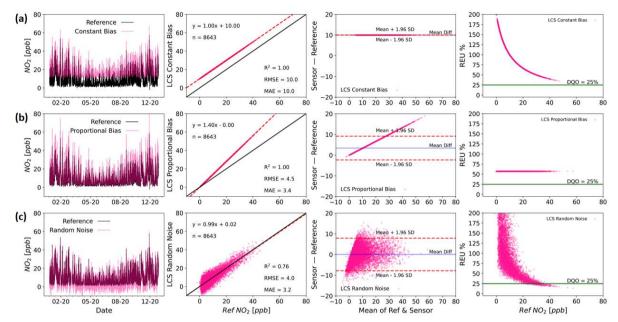


Figure 1. Time series (left panels), regression (middle-left panels), B-A Bland-Altman (middle-right panels) and REU (right panels, DQO for $NO_2 = 25\%$) plots for arbitrary examples of pure constant bias (Slope = 1, Intercept = 1, SD $_\epsilon$ = 0; a-panels), pure proportional bias (Slope = 1.4, Intercept = 0, SD $_\epsilon$ = 0; b-panels) and pure random noise (Slope = 1, Intercept = 0, SD $_\epsilon$ = 4; c-panels) simulated errors.

2.1 Performance indices, error structure and uncertainty

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A major challenge faced by end-users of measurement devices characterised using colocation studies is the nontrivial question of how the comparisons themselves are performed and how the data are is communicated. Often single value performance metrics, such as the coefficient of determination (R²) or root mean squared error (RMSE), are calculated between the assessed method (e.g. LCS) and an agreed reference, and the user is expected to infer an expected device performance or uncertainty for a measurement in their application (Duvall et al., 2016; Malings et al., 2019). These metrics contain useful information about the measurement, but they are unable to fully describe the error characteristics, in part because they reduce the error down to a single value (Tian et al., 2016). When evaluating multiple sensors during a colocation experiment, single metrics can be a useful way to globally compare instruments/sensors. However, these metrics do little to communicate the nature of the measurement errors and the impacts these will have in any end use application, in part because they reduce the error down to a single value (Tian et al., 2016). Even more if a specific concentration range is of paramount interest to the end-user, these metrics are not capable of characterising the weight of noise and/or the bias effect. The R² shows globally the data set linearity and gives an idea of the measurement noise. However, it is unable to distinguish whether a specific range of concentrations is more or less linear (or more or less noisy) than another. Similarly, the RMSE is also a very useful metric and perhaps more complete than R², as it considers both noise and bias (although they need to be explicitly decomposed from RMSE). Nevertheless, the RMSE is an average

measure (of noise and bias) over the entire dataset under analysis. Using combinations of simple metrics increases the information communicated, but does not necessarily make it easy to assess how the errors will likely impact a particular measurement application. Visualising the absolute and relative measurement errors across the concentration range (unreachable by global metrics) enables end users to view the errors, and any features (non-linearities, step changes, etc.) that would impact the measurement but that global metrics (and in some cases time-series and/or regression plots) are incapable of showing.

Unfortunately, the widespread use of a small number of metrics as the sole method to assess measurement uncertainty, without a thorough consideration of the nature of the measurement errors, means measurement devices are often chosen that are unable to provide data that is fit for purpose. In addition, unconscious about potential flaws, users (e.g. researchers) could communicate findings or guide decision making based on results that may not justify the conclusions drawn from the data. Figure 2 shows three simulated measurements compared with the true values. Despite the measurements having identical R² and RMSE values, the time series and regression plots show that the error characteristics are significantly different, and would impact how the data from such a device could viably be used.

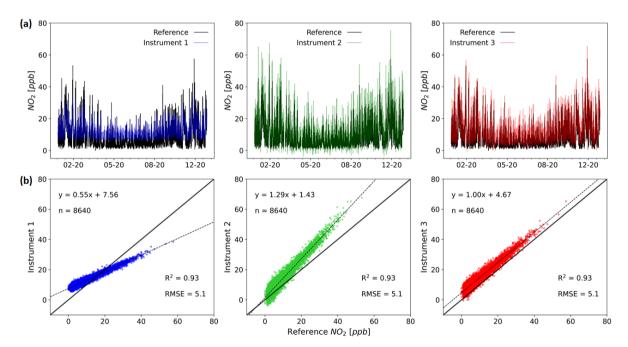


Figure 2. Time series (a-panels) and regression plots (b-panels) for three hypothetical instruments and a reference (1 year of data). The most used metrics for evaluating the performance of LCS (\mathbb{R}^2 and RMSE) are identical for the systems shown, even when the errors have very different characteristics (time res 1 h).

There are multiple performance metrics that can be used for the assessment of measurement errors and uncertainty. Tian et al (2016) present an excellent summary of some of the major pitfalls of performance metrics and promote an approach of error modelling as a more reliable method of uncertainty quantification. These modelling approaches, however, rely on the assumption of statistical stationarity, whereby the statistical properties of the error are constant in the temporal and spatial domains. The presence of unknown or poorly characterised sources of error, for example, due to interferences from other atmospheric constituents or drifts in sensor behaviour, makes this assumption difficult to satisfy, especially when the dependencies of these errors show high spatial and

temporal variability. Thus, if field colocation studies are the primary method for performance assessment, as is the case for LCS, only through a detailed assessment of the measurement errors across a wide range of conditions and timescales can the uncertainty of the measurement be realistically estimated.

2.2 Dealing with errors: established techniques vs Low-Cost Sensors

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Different approaches are available to the user to minimise the impact of errors, generally by making corrections to the sensor data. For example, in the case of many atmospheric gas analysers, if the error is dominated by a proportional bias, a multi-point calibration can be performed using standard additions of the target gas. Displacement errors can be quantified, and then corrected for, by sampling a gas stream that contains zero target gas. And Random errors can be reduced by applying a smoothing filter (e.g moving average filter, time-averaging the data, etc.), at the cost of losing some information (Brown et al., 2008). These approaches work well for simple error sources that, ideally, do not change significantly over timescales from days to months. Unfortunately, more complex error sources can manifest in such a way that they contribute across all three error types, and also vary temporally and spatially. For example, an interference from another gas-phase compound could in part manifest itself as a displacement error, based on the instrument response to its background value, and in part as a proportional bias if its concentration correlates with the target compounds, with any short-term deviations from perfect correlation contributing to the random error component. In this case, time-averaging combined with periodic calibrations and zeros would not necessarily minimise the error, and the user would need to employ different tactics. One option would be to independently measure the interferent concentration, albeit with associated uncertainty, and then use this to derive a correction. This is feasible if a simple and cost-effective method exists for quantifying the interferent and its influence on the result is understood, but can make it very difficult to separate out error sources, and can become increasingly complex if this measurement also suffers from other interferences.

For many measurement devices, in particular for LCS based instruments, a major challenge is that the sources and nature of all the errors are unknown or difficult to quantify across all possible end-use applications, meaning estimates of measurement uncertainty are difficult. In the case of most established research and reference-grade measurement techniques, comprehensive laboratory and field experiments have been used to explore the nature of the measurement errors (Gerboles et al., 2003; Zucco et al., 2003). Calibrations have then been developed, where traceable standards are sampled and measurement bias, both constant and proportional, can be corrected for. Interferences from variables such as temperature, humidity, or other gases, have also been identified and then either a solution engineered to minimise their effect or robust data corrections derived. Unfortunately, these approaches have been shown not to perform well in the assessment of LCS measurement errors, due to the presence of multiple, potentially unknown, sensor interferences from other atmospheric constituents (Thompson & Ellison, 2005). These significant sensitivities to constituents such as water vapour and other gases mean laboratory-based calibrations of LCS become exceedingly complex, and expensive, as they attempt to simulate the true atmospheric complexity, often resulting in observed errors being very different to real-world sampling (Rai et al., 2017; Williams, 2020). This has resulted in colocation calibration becoming the accepted method for characterising LCS measurement uncertainties (De Vito et al., 2020; Masson et al., 2015; Mead et al., 2013; Popoola et al., 2016; Sun et al., 2017), where sensor devices are run alongside traditional reference measurement systems for a period of time, and statistical corrections derived to minimise the error between the two. As the true value of a pollutant concentration cannot be known, this colocation approach assumes all the error is in the low-cost measurement. Although this assumption may often be approximately valid (i.e. reference error variance << LCS error variance), no measurement is absent of uncertainty and this can be transferred from one measurement to another, obscuring attempts to identify its sources and characteristics. A further consideration when the fast time-response aspect of LCS data is important, is that reference measurement uncertainties are generally characterised at significantly lower reported measurement frequencies (typically 1 hr). This means that a high time-resolution (e.g. 1 min) reference uncertainty must be characterised in order to accurately estimate the LCS uncertainty (requiring specific experiments and additional costs). If a lower time-resolution reference data set is used as a proxy, then the natural variability timescales of the target compound should be known and any impact of this on the reported uncertainty caveated.

Another challenge with this approach is that, unlike targeted laboratory studies, real-world colocation studies at a single location, and for a limited time period, are not able to expose the measurement devices to the full range of potential sampling conditions. As many error sources are variable, both spatially and temporally, using data generated under a limited set of conditions to predict the uncertainty on future measurements is risky. Deploying a statistical model makes the tacit assumption that all factors affecting the target variable are captured by the model (and the data set used to build the model). This is very often an unrealistic demand, and in the complex multifaceted system that is atmospheric chemistry, this is extremely unlikely to be tenable, resulting in a clear potential for overfitting to the training dataset. Ultimately, however, these colocation comparisons with instruments with a well-quantified uncertainty need to be able to communicate a usable estimate of the information content of the data to end-users, so that devices can be chosen that are fit for a particular measurement purpose.

3. Methods

In this work, we explore measurement errors, and their impacts, using the most common single value metrics: the Coefficient of Determination or R², the Root Mean Squared Error or RMSE and the Mean Absolute Error or MAE (see the equation definitions in Cordero et al., 2018), along with two additional widely used approaches to visualise the error distribution across a dataset. To visualise the error distribution across a dataset we have also employed two additional widely used approaches: the Bland-Altman plots (B-A) and Relative Expanded Uncertainty (REU).

The performance metrics provide a single value irrespective of the size of the dataset, and might appear convenient for users when comparing across devices or datasets, but can encourage over-reliance on the metric, often at the expense of looking at the data in more detail or bringing an awareness of the likely physical processes driving the error sources. On the other hand, the use of visualisations such as B-A and REU is complementary to the aforementioned metrics, with the added value that the user is now more aware of how the data looks like in an absolute and/or relative error space, allowing them to distinguish some characteristics of interest. These visualizations The B-A and the REU plots are indeed more laborious techniques and the interpretation can be challenging for non-experts, but they provide additional insights into the nature of the errors, not attainable by one or more combined performance metrics: while B-A plots shows the noise (dispersion of the data) and the bias effect (tendency of the data) in an absolute scale, the REU can be explicitly decomposed in the noise and bias components (see Yatkin et al., 2022).

In order to understand how the different tools used here show different characteristics of the error structure, some errors commonly found in LCS are examined through simulation studies. Subsequently, two real world case studies are presented: (i) LCS duplicates for NO₂ and PM_{2.5} belonging to the QUANT project located in two sites -the Manchester Natural Environment Research Council (NERC) measurement Supersite, and the York Fishergate Automatic Urban and Rural Network (AURN) roadside site- and (ii) a set of duplicate reference instruments (only at Manchester Supersite). Table S1 shows the research grade instrumentation used for this study.

3.1 Visualisation tools

An ideal performance metric should be able to deliver not only a performance index but also an idea of the uncertainty distribution (Chai & Draxler, 2014). This is difficult to deliver through a simple numerical value, and easy to interpret visualisations of the data are often much more useful for conveying multiple aspects of data performance. Figure 2 shows the two most common data visualisation tools, the time-series plot and the regression plot. In the time series plot the instrument under analysis and the agreed reference are plotted together as a function of time. This allows a user to visually assess tendencies of over or under prediction, differences in the base line or other issues, but can be readily over interpreted and does not allow for easy quantification of the observed errors. In the regression plot the data from the instrument under analysis is plotted against the agreed reference data. This allows for the correlation between the two methods to be more readily interpreted, in particular any deviations from linearity, but gives little detail on the nature of the errors themselves.

In contrast to the regression plot -where the measured values from the two measurements (e.g. LCS vs Ref) are plotted against each other- the Bland-Altman plots essentially display the difference between measurements (abscissa) as a function of the average measurement (ordinate), enabling more information on the nature of the error to be communicated. This direct visualisation of the absolute error acknowledges that the true value is unknown and that both measurements have errors. The B-A plot enables the easy identification of any systematic bias between the measurements or possible outliers, and is the reason B-A plots are extensively used in analytical chemistry and biomedicine to evaluate agreement between measurement methods (Doğan, 2018). The mean difference between the measurements, (represented by the blue line in the figures), is the estimated bias between the two observations. The spread of error values around this average line indicates if the error shows purely random fluctuations around this mean, or if it has structure across the observed concentration range.

In contrast to the regression plot, Bland Altman (B A) plots essentially display the difference between measurements, enabling more information on the nature of the error to be communicated. B A plots (Altman & Bland, 1983) are extensively used in analytical chemistry and biomedicine to evaluate the differences between two measurement techniques (Doğan, 2018). The B A is a scatter plot, in which the abscissa represents the average of these measures (e.g LCS and a reference measurement), acknowledging that the true value is unknown and that both measurements have errors, and the ordinate shows the difference between the two paired measurements.

In the case where all the error is assumed to be in one of the measurements, e.g. comparing a LCS to a reference grade measurement, there is an argument that the B-A abscissa could be the agreed reference value instead of the average of two measurements. However, in this work we use the average of the two values as per the traditional

B-A analysis. To illustrate the B-A interpretation, from the error model (Eq. (1)) we can derive the following expression:

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$$y_i - x_i = x_i (b_1 - 1) + b_0 + \varepsilon$$
 (2)

From Eq. (2) it can be seen that if $b_1 \neq 1$ or if the error term (ϵ) variance is non-constant (e.g. heteroscedasticity) the difference will not be normally distributed. The B-A plot (with x_i as the reference instrument results) allows a quick visual assessment of the error distribution without the need to calculate the model parameters. In the case the differences are normally distributed, the so-called "agreement interval" (usually defined as $\pm 2\sigma$ around the mean) will hold 95% of the data points. Even though the estimated limits of agreement will be biassed if the differences are not normally distributed, it can still be a valuable indicator of agreement between the two measurements.

If the ultimate goal of studying measurement errors is to diagnose the measurement uncertainty in a particular target measurement range, then visualising the uncertainty in pollutant concentration space can be very informative. The REU (GDE, 2010) provides a relative measure of the uncertainty interval about the measurement within which the true value can be confidently asserted to lie. The abscissa in an REU plot represents the agreed reference pollutant concentration, whose error is taken into account, something not considered by the other metrics or visualisations discussed. The REU is regularly used to assess measurement compliance with the Data Quality Objective (DQO) of the European Air Quality Directive 2008/50/EC, and is mandatory for the demonstration of equivalence of methods other than the EU reference methods. For LCS the REU is widely used as a performance indicator (Bagkis et al., 2021; Bigi et al., 2018; Castell et al., 2017; Cordero et al., 2018; Spinelle et al., 2015). However, the evaluation of this metric is perceived as arduous and cumbersome and it is not included in the majority of sensor studies (Karagulian et al., 2019). There is now a new published European Technical Specification (TS) for evaluating the LCS performance for gaseous pollutants (CEN/TS 17660-1:2021). It categorises the devices in 3 classes according to the DOO (Class 1 for "indicative measurements", Class 2 for "objective estimations", and Class 3 for non-regulatory purposes, e.g. research, education, citizen science, etc.). In the following sections, we use these established methods for assessing measurement uncertainty, alongside simple time series and regression plots, to explore different error sources and their implications for air pollution measurements.

4. Case studies

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4.1 Simulated instruments

In order to investigate the impact of different origins of measurement error on measurement performance, a set of simulated datasets have been created. These data are derived using real-world reference data as the true values, with the subsequent addition of errors of different origins to generate the simulated measurement data. Error origins were chosen for which examples have been described in the LCS literature. Performance metrics along with visualisation methods are then used to assess measurement performance.

As the complexity of the error increases, the impact of the assumption of statistical stationarity can become more difficult to satisfy, with the magnitude of the errors becoming less uniform across the observed concentration, and

hence spatial, or time domains. Figure 3 shows examples of modelled sources of errors on NO₂ measurements: temperature interference (correction model taken from (Popoola et al., 2016), a-panels), a non-target gas (ozone) interference (correction model taken from (Peters et al., 2021), b-panels) and thermal electrical noise (white noise, c-panels).

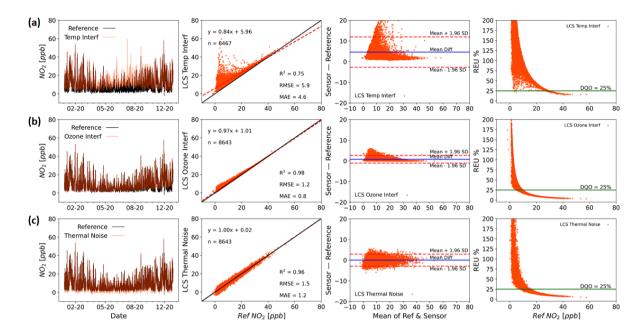


Figure 3. Time series (left panels), regression plots (middle-left panels, including R^2 , RMSE & MAE), Bland-Altman plots (middle-right panels) and REU (right panels, DQO for $NO_2 = 25\%$) for temperature (a-panels), ozone (b-panels) and thermal electrical noise (c-panels) modelled interferences on NO_2 measurements (time res 1 h).

The above simulations show examples of how individual sources of error can impact measurement performance. Figure S1 shows some more examples, this time for different drift effects (baseline drift, temperature interference drift and instrument sensitivity drift). This set of error origins is not exhaustive, with countless others potentially impacting the measurement, such as those coming from (i) hardware (sensor-production variability, sampling, thermal effects due to materials expansion, drift due to ageing, RTC lag, Analog-to-Digital conversion, electromagnetic interference, etc.), (ii) software (signal sampling frequency, signal-to-concentration conversion, concept drift, etc.), (iii) sensor technology/measurement method (selectivity, sensitivity, environmental interferences, etc.) and (iv) local effects (spatio-temporal variation of concentrations, turbulence, sampling issues etc.).

Each error source impacts the uncertainty of the measurement, which in turn impacts its ability to provide useful information for a particular task. For example, the form of the temperature interference shown in Fig. 3 (a-panels) results in the largest errors being seen at the lower NO₂ values. This is because NO₂ concentrations are generally lowest during the day, due to photolytic loss when temperatures are highest. Thus this device would be better suited to an end-user intending to assess daily peak NO₂ concentration compared with the daytime hourly exposure values, providing the environment the device was deployed in showed a similar relationship between temperature and true NO₂ as that used here. The O₃ interference shown in Fig. 3 (b-panels) is similar, due again to a general anti-correlation observed between ambient O₃ and NO₂ concentrations. This type of interference can often be

interpreted incorrectly as a proportional bias, and a slope correction applied to the data. However, this type of correction will ultimately fail as O_3 concentrations are dependent on a range of factors, such as hydrocarbon concentrations and solar radiation, and as these change the O_3 concentration relative to the NO_2 concentration will change. To further complicate matters, multiple error sources can act simultaneously, meaning that the majority of measurements will contain multiple sources of error. Figure 4 shows a simple linear combination of the modelled errors shown in Fig 3, and the impact this has on the performance metrics.

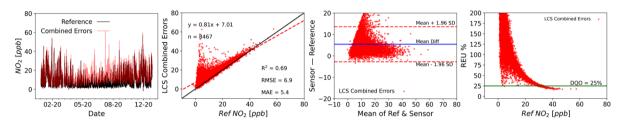


Figure 4. Time series (left panel), regression plot (middle-left panel, including R^2 , RMSE & MAE), Bland-Altman plot (middle-right panel) and REU (right panel, DQO for $NO_2 = 25\%$) for a linear combination of temperature, ozone and thermal electrical noise modelled interferences (time res 1 h).

As the simulations show, the nature of the errors determine the observed effect on the measurement performance. In an ideal situation, like those shown in figures 3 and 4, the error sources would be well characterised, allowing the error to be modelled and approaches such as calibrations (for bias) and smoothing (for random errors) employed to minimise the total uncertainty. Unfortunately, in scenarios where sources of error and their characteristics are not known, modelling the error becomes more difficult and a more empirical approach to assessing the measurement performance and uncertainty may be required. The growing use of LCS represents a particular challenge in this regard. The susceptibility of LCS to multiple, often unknown or poorly characterised, error sources means that in order to determine if a particular LCS is able to provide data with the required level of uncertainty for a given task, a relevant uncertainty assessment is required. The following section explores the uncertainty characteristics of several LCS, with unknown error sources, deployed alongside reference instrumentation in UK urban environments as part of the QUANT study.

4.2 Real-world instruments

The difficulty in generating representative laboratory error characterisation data means for many measurement devices the error sources are essentially unknown. This, combined with the use of imperfect algorithms that are not available to the end-user (i.e. "black-box" models) to minimise errors, means that, colocation data is often the best option available to end-users in order to assess the applicability of a measurement method for their desired purpose. This is particularly the case for LCS air pollution measurement devices. In this section, we show colocation data collected as part of the UK Clean Air program funded QUANT project, and use the tools described above to investigate the impact of the observed errors on end-use.

Figure 5 shows two colocated NO2 measurements, from two different LCS devices using only their out of box calibrations (i.e. no colocation data from that site was used to improve performance), compared with colocated reference measurements at an urban background site in the city of Manchester. Unlike the modelled instruments in Sect. 4.1, the combination of error sources is unknown in this case and we can thus only assess the LCS

measurement performance through comparison with the reference measurements using metrics and visual tools. There are obvious differences in the performance of both LCS instruments shown in Fig. 5, LCS1 (a panels) shows an appreciable difference in the time series baseline, which can be interpreted from both the regression (b1 <1) and the B. A plots as a proportional bias. This bias also impacts the REU plot, with a minimum in the region where the regression best fit line crosses the 1:1 line (~17ppb). It is worth noting that these plots do not directly identify the source of the proportional bias, with sensor response to the target compound or another covarying compound possible, but provides information on how much it impacts the data. For LCS2 (Fig. 5, b. panels) any proportional bias is significantly smaller, with the B A plot showing a much more symmetrical distribution of points around the central line across the observed mixing ratio range, although this is not a normal distribution as evidenced by the heteroscedastic nature of the differences, indicating the cause is not entirely random in nature. The lack of a large proportional bias also results in the REU plot showing a continued reduction in relative uncertainty as the true NO2 concentration increases. Interestingly, both LCS's also show an additional bias at the highest NO2 values observed. This does not significantly impact the REU, due to its relative nature, but can be seen in the regression and B. A plots. Correcting for the observed proportional bias in LCS1 and LCS2 improves the observed performance by providing the errors with a more symmetrical distribution (LCS1* and LCS2* shown in Fig. S2).

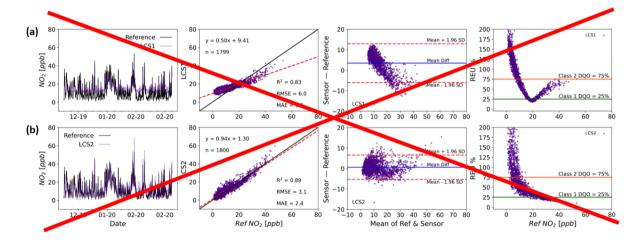


Figure 5. Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels; NO₂-Class 1 DQO = 25% & Class 2 DQO = 75%) for NO₂-measurements by two LCS systems of different brands (a and b panels) in the same location (Manchester Supersite, December 2019 to February 2020. Time res 1 h).

Figure 5 shows two colocated measurements from two different LCS devices: one measuring NO₂ (a-panels) and the other O₃ (b-panels). Both measurements are compared with colocated reference measurements at an urban background site in the city of Manchester. Unlike the modelled instruments in Sect. 4.1, the combination of error sources is unknown in this case, and we can thus only assess the LCS measurement performance through comparison with the reference measurements using global metrics and visual tools.

Single value metrics indicate an acceptable performance for both measurements: high linearity (both R^2 are higher than 0.8) and relatively low errors (RMSE ~ 5ppb). However, the plots present the data in a variety of ways that enable the user to identify patterns in the measurement errors that would be less obvious if only global metrics

were used. For example, the NO₂ sensor (LCS1, a-panels) has a non-linear response that is almost imperceptible from the regression plot but stands out in the B-A plot. Furthermore (despite the high R² and relatively low RMSE), the REU plot shows high relative errors that do not meet the Class 2 DQO for the measured concentration range. Regarding the O₃ sensor (LCS2, b-panels), the B-A plot shows two high density measurement clusters, one with positive absolute errors (over-measuring) and a larger one with negative errors (under-measuring). These are the result of a step change in the correction algorithm applied by the manufacturer and could easily have been missed if only summary metrics and a regression plot were used, especially if the density of the data points was not coloured.

It is worth noting that these plots do not directly identify the source of the proportional bias, with sensor response to the target compound or another covarying compound possible, but provides information on how much it impacts the data.

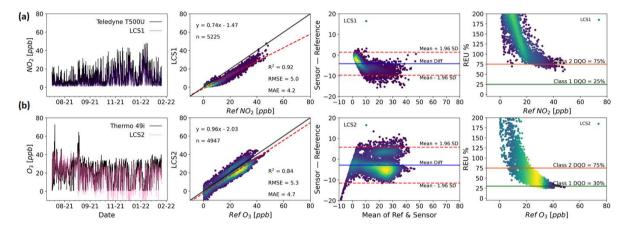


Figure 5. Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels; NO_2 Class 1 DQO = 25% & Class 2 DQO = 75%; O_3 Class 1 DQO = 30% & Class 2 DQO = 75%) for NO_2 (a-panels) and O_3 (b-panels) measurements by two LCS systems of different brands in the same location and time span (Manchester Supersite, July 2021 to February 2022. Time res 1 h). All but the time-series plots, have coloured by data density.

Figure 6 shows three out of the box PM_{2.5} measurements made by three devices from the same brand in spring, located at two sites: the first two at an urban background (LCS3 & LCS4, a and b panels) and the third at a roadside (LCS5, c panels). As the regression and the B A plots show, all LCS measurements in Fig. 6 have a proportional bias compared with the reference, with the LCS over predicting the reference values. Both LCS's at the urban background site show very similar performance, indicating that the devices are similarly affected by errors. This internal consistency is highly desirable, especially when LCS's are to be deployed in networks, as although mean absolute measurement error may be high, differences between identical devices are likely to be interpretable.

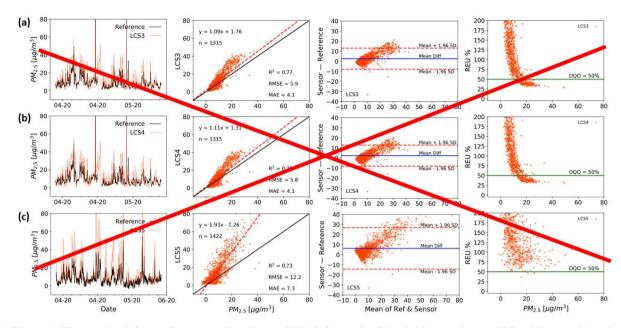


Figure 6. Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels, DQO for $PM_{2.5} = 50\%$) for $PM_{2.5}$ measurements by three LCS systems of the same brand (panels a, b and c) in different locations: an urban background (Manchester Supersite, panels a and b) and a roadside site (York, panel c) (April & May 2020, time res 1 h).

Figure 6 shows three out-of-the-box PM_{2.5} measurements made by two devices (LCS3 & LCS4) from the same brand in spring (LCS3: a-panels; LCS4: c-panels) and in autumn (b-panels, only LCS3). The colocation shown correspond to two different sites: an urban background site (LCS3, a and c-panels) and a roadside site (LCS4, c-panels).

As the regression and the B-A plots show, all LCS measurements in Fig. 6 have a proportional bias compared with the reference, with the LCS over predicting the reference values. The device at the urban background site (LCS3) show a dissimilar performance in spring and autumn, indicating that the errors this device suffers are differently influenced by local conditions in the two seasons (all the duplicates at the urban background show the same pattern). While for LCS3 during spring the error have a more linear behaviour, in autumn a non-linear pattern is clearly observed in the regression and B-A plots. Despite the utility that single metrics can have in certain circumstances, the non-linear pattern goes completely unnoticed by them: while for the two different seasons RMSE and the MAE are almost constant the R² indicates a higher linearity for autumn.

A number of duplicates were deployed at both sites showing a very similar performance in terms of the single metric values but also in regard to the more visual tools (not shown here). This internal consistency is highly desirable, especially when LCS's are to be deployed in networks, as although mean absolute measurement error may be high, differences between identical devices are likely to be interpretable.

Having prior knowledge of the nature of the measurement errors allows informed experimental design prior to data collection. This is key if an end user is to maximise the power of a dataset, and the information it provides, to answer a specific question. For example, if an end-user wanted to identify pollution hotspots within a relatively small geographical area, then using a dense network of sensor devices that posses errors large and variable enough to make quantitative comparisons with limit values difficult (possibly due to an interference from a physical

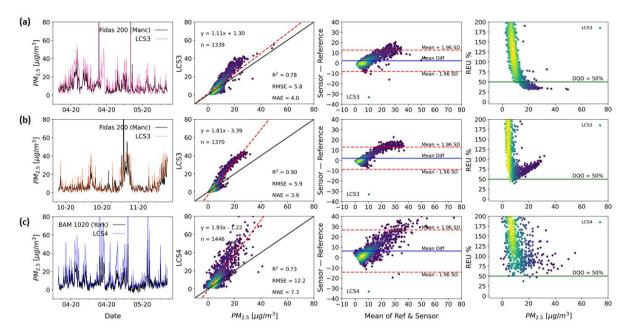


Figure 6. Two LCS systems (LCS3 & LCS4, same brand) measuring PM2.5 (Time res 1 h). While LCS3 is shown for the same location (Manchester) but unfolded in two different seasons (a-panels: Apr to May 2020; b-panels: Oct to Nov 2020), LCS4 is at a different location (c-panels: York, Apr to May 2020). Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels; $DQO_{PM2.5} = 50\%$) are used to characterise the device's error structure. All but the time-series plots have been coloured by data density.

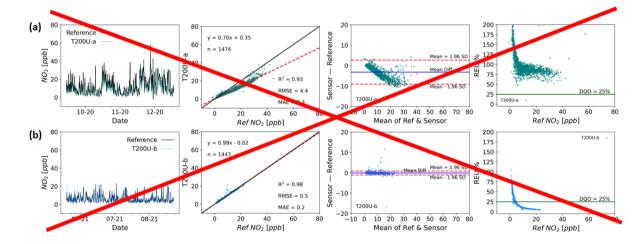
The LCS data from the roadside location (LCS4) show significantly lower precision than those at the urban background site, as seen in the B-A plot. This could be caused by differences in particle properties and size distributions between the two sites (Gramsch et al., 2021), and by the high frequency variation of transport emissions close to the roadside site side and turbulence effects (Baldauf et al., 2009; Makar et al., 2021). Duplicate measurements show that all sensors of this type responded similarly in this roadside environment (not shown here), supporting the high internal consistency of this device, but indicating a spatial heterogeneity in some key error sources. It is also worth noting that the gold standard instruments at the two sites are not "reference method" but "reference equivalent methods" (GDE, 2010), each using a different measurement technique: while an optical spectrometer (Palas Fidas 200) is used in Manchester, the York instrument uses a Beta attenuation method (Met One BAM 1020), which could also potentially lead to some of the observed differences. The increased apparent random variability for LCS4, combined with the proportional bias, results in significantly higher measurement uncertainty across the observed range, as can be seen by the REU plots, with LCS4 never reaching an acceptable DQO level (50% for PM2.5). As with the NO2 sensors (Fig. 5). If the observed proportional bias is corrected the linearly bias-corrected sensors (Fig. S3) show a much improved comparison with the reference measurement, specially LCS3* in autumn and LCS4*. The error distribution for the LCS3 (autumn) shown by the B-A plot is

greatly narrowed (~3x times) and now the sensor is accomplishing the DQO below 10 ugm⁻³ as the REU plot indicates. For LCS4 In this case the B-A plot shows an error characteristic more dominated by random errors, and the REU plots shows a significant reduction of the relative uncertainty, with the REU at 10 ugm⁻³ reducing from ~75 to ~50%.

As a comparison for the LCS data shown above, Fig. 7 shows two identical NO₂ reference grade instruments, Teledyne T200U (Chemiluminescence method) at the Manchester urban background site (panels a and b) at during two different time periods, with a Teledyne T500U (CAPS detection method) used as the "ground truth" instrument. Instrument "a" manifests a significant proportional bias, in contrast to instrument "b", but both show differences that could be non-negligible depending on the application. The deviations observed in instrument "a" was due to the cell pressure being above specification by ~20%, unnoticed while the instrument was in operation. This demonstrates the importance of checking instrument parameters regularly in the field even if the data appears reasonable.

As the LCS error structure is determined relative to the performance of a reference measurement, if the reference instrument suffers from significant errors this will affect the outcomes of the performance assessment, due to the assumption that all the errors reside with the LCS. As Fig. 7 shows, however, this assumption is not necessarily always valid and potentially argues that reference instruments used in colocation studies should be subject to further error characterisation, including possible colocation with other reference instruments. As a similar comparison of reference instruments, Fig. S3 shows two ozone research grade instruments (a Thermo 49i and a 2B).

It is worth noting that even when using reference, or reference equivalent, grade instrumentation, inherent measurement errors mean that relative uncertainty, as shown in the REU plot, increases asymptotically at lower values. This is not unexpected, but is potentially important as ambient target concentration recommendations continue to fall based on updated health evidence (World Health Organization, 2021).



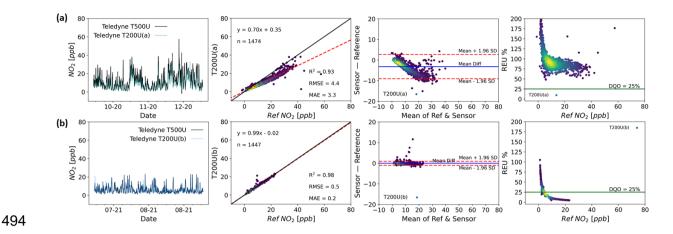


Figure 7. Time series (left panel), regression plots (middle-left panel), Bland-Altman plots (middle-right panel) and REU (right panel, DQO for $NO_2 = 25\%$) for two identical (Teledyne T200U) reference NO_2 instruments (panels a and b) colocated at the Manchester Supersite (1h time res). The first instrument between October & November 2020 and the second between July & August 2021. All but the time-series plots have been coloured by data density.

5. Discussion

The widespread use of colocation studies to assess measurement device performance, means many examples exist in the LCS literature where different devices are compared using summary metrics for field or laboratory studies (Broday, 2017; Duvall et al., 2016; Hofman et al., 2022; Karagulian et al., 2019; Mueller et al., 2017; Rai et al., 2017; van Zoest et al., 2019). Although these comparisons do provide useful information, they can be misleading for end users wanting to compare the performance of different devices, as they are often carried out under different conditions and do not present the data or experimental design in full. Even in the case where comparisons have been done under identical conditions, the data still needs to be treated with caution, as inevitable differences between assessment environment and proposed application environment, as well as any changes to instrument/sensor design or data processing, mean that past performance does not guarantee future performance.

All measurement devices suffer from measurement errors, many of which are potentially significant depending on the application, with devices and their error susceptibility covering a broad spectrum. As evidenced by Fig. 7, reference instruments are not immune from this phenomena, with the proportional bias of one of the NOx instruments clearly affecting its measurements resulting in the absolute error increasing with concentration. As the requirements on measurement devices continue to increase, driven in part by new evidence supporting the reduction of air pollutant target values, the devices currently being used for a particular application could no longer be fit-for-purpose in the situation where the limit value has decreased to the point where it is small relative to the device's uncertainty.

Single value performance metrics, such as R^2 and RMSE, can seem convenient when comparing multiple colocated devices as they facilitate decision making when a threshold criterion is defined. However, these scalar values hide important information about the scale and / or distribution of the errors within a dataset; graphical summaries of the measurements themselves can offer significantly more insight into the impact of measurement errors on device performance and ultimate capabilities. Of particular use in air pollution measurements is the ability to see how the errors manifest themselves in relation to our best estimate of the true pollutant concentration,

as often applications have specific target pollutant concentration ranges of interest. For example, the two NO₂ LCS devices shown in Fig. 5 have similar R²-values of 0.83 and 0.89, but one is suffering from a strong proportional bias that impacts on measurements either side of the 18ppb crossing point considerably high R² values (0.92 and 0.84) and relatively low RMSE and MAE, but one suffering of non-linear errors (LCS1) and the other with data coming from two different calibration states (LCS2).

Errors, or combinations of errors, frequently result in varying magnitude of the observed measurement inaccuracies across the concentration space observed, and it is often useful to assess both the absolute and relative effects of the errors. By getting a more complete picture of the device performance, decisions can be made on the effectiveness of simple corrections, such as correcting for an apparent proportional bias using an assumption of a linear error model. Ultimately end users need to identify the data requirements a priori and design quantifiable success criteria by which to judge the data. For example, rather than just wanting to measure the 8-hour average NO₂, be more specific and require that this needs to be accurate to within 5 ppb, have demonstrated approximately normally distributed errors in a representative environment for the period of interest, and no statistical evidence of deviation from a linear correlation with the reference measurement over the target concentration range for the period of interest.

A major challenge comes from complex errors, such as interferences from other compounds or with environmental factors, that vary temporally and/or spatially. Similar graphical techniques to those presented above can be used to identify the existence of such relationships, but correcting for them remains a challenge. For example, the correlation between measurement errors and relative humidity could be explored by replacing the abscissa with measured relative humidity in both the B-A and REU plots. This would visualise the relationship between absolute and relative errors with relative humidity, but would not be able to confirm causality. The complex and covarying nature of the atmosphere means that the best way to identify a device error source is through controlled laboratory experiments, where confounding variables can be controlled, although these experiments are often difficult and expensive to perform in a relevant way.

This brings into question the power of colocation studies, as they can ultimately never be performed under the exact conditions for every intended application. The PM_{2.5} sensors shown in Fig. 6 demonstrate this, as if a colocation dataset generated at the urban background site was used to inform a decision about the applicability of these devices to a roadside monitoring task, then an overly optimistic assessment of the scale of the errors to be expected would be likely. It is therefore always desirable that colocation studies are as relevant as possible to the desired application, and this is even more paramount in the case where the error sources are poorly specified. For this reason, complete meta-data on the range of conditions over which a study was conducted is key information in judging its applicability to different users.

Although there is no strict definition on what makes a device a LCS, we often make the categorization based on the hardware used. Standard reference measurement instruments are generally based on well-characterised techniques developed and improved over years, based primarily on the progressive refinement of hardware (e.g. materials used for the detection elements, electronic circuits to filter noise, refinement of production methods, etc.). Although LCS sensor technologies are improving, it is interesting that many of the significant improvements that have been made to LCS performance have been through software, rather than hardware advances. As more

colocation data are is generated in different environments, many LCS manufacturers have been able to develop data correction algorithms that minimise the scale of the errors that are present on the LCS hardware. This can greatly improve the performance of LCS devices, and has been a large factor in the improvements seen in these devices over recent years. These algorithms are, however, inevitably imperfect and can suffer from concept drift (De Vito et al., 2020), caused by the lack of available colocation data over a full spectrum of atmospheric complexity. Furthermore, any kind of statistical model introduces a new error source that can work in conjunction with the pre-existing measurement errors to drastically change the observed error characteristics, making it much more difficult for users to interpret and extrapolate from colocation study performance to intended application. end users are to be able to make well informed decisions about device applicability to a particular task, then an argument can be made for information on the scale of the error corrections made to a reported measurement to be made available, ideally alongside and a demonstration of its benefits in a relevant environment. If end users are to be able to make well informed decisions about device applicability then information on the scale of the measurement errors, and the impact of corrections made to minimise these, should be made available. Exemplar case studies in a range of relevant environments would also be highly valuable. Unfortunately, this colocation data are is costly to generate, meaning relevant data often does not exist, and when it does is often not communicated in such a way that enables the user to make a fully informed decision.

6. Conclusions

In situ measurements of air pollutants are central to our ability to identify and mitigate poor air quality. Measurement applications are wide ranging, from assessing legal compliance to quantifying the impact of an intervention. The range of available measurement tools for key pollutants is also increasingly broad, with instrument price tags spreading several orders of magnitude. In order for a measurement device to be of use for a particular application it must be fit-for-purpose, with cost, useability and data quality all needing to be considered. Understanding measurement uncertainty is key in choosing the correct tool for the job, but in order for this to be assessed the job needs to be fully specified a priori. The specific data requirements of each measurement application need to be understood and a measurement solution chosen that is capable of providing data with sufficient information content.

In order to aid end users in extrapolating from colocation study performance to potential performance in a specific application, performance metrics are often used. Although single value performance metrics do convey some useful information about the agreement between the data from the measurement device being assessed and the reference data, they can often be misleading in their evaluation of performance. This dictates a more rigorous and empirical approach to data uncertainty assessment in order to determine if a measurement is fit for purpose. The ability to assess device performance across the observed concentration range, as in the B-A and REU plots, enables an end-user to make an informed decision about the capabilities of a measurement device in the target concentration range. These visual tools also help identify any simple corrections that can be applied to improve performance. In contrast, if an end-user was only provided with a single value metric, such as R² or RMSE then it would be significantly more difficult to understand the likely implications of the measurement uncertainties.

All measurement devices suffer from errors, which result in deviations between the reported and true values. These errors can come from a multitude of sources, with the scale of the deviation from the true value being dependent on the nature of the error. Although a known measurement uncertainty for all applications would be ideal for end users to be able to assess measurement device suitability for purpose, in many cases, especially for LCS, this is not possible due to the presence of poorly characterised, or sometimes unknown, error sources. In the absence of this, useful information on likely measurement performance can be obtained using colocation data compared with a measurement with a quantified uncertainty. It is important that such a colocation study is carried out in an environment as similar as possible to the application environment, as the unknown nature of many error sources means their magnitude can change significantly between different locations and/or seasons (e.g. Fig. 6). Ideally, depending on the measurement task, the user could use the colocation data to model the error causes and use this to develop strategies to minimise final measurement uncertainty. Unfortunately, relevant colocation study are is often not available, and to generate the data would be prohibitively costly, which limits the user's ability to make a realistic assessment of likely uncertainties. The presence of, often complex, error minimisation post processing or calibration algorithms further complicates things. This additional uncertainty is most likely to bias any performance prediction if the end user is unaware of the purpose or scale of the data corrections, and their applicability to the target environmental conditions. Ideally, long term colocation data sets demonstrating the performance of measurement hardware and software, in a range of relevant locations, over multiple seasons, and carried out by impartial bodies would be available to inform measurement solution decisions.

In order for end users to take full advantage of the ever increasing range of air pollution measurement devices available, the questions being asked of the data must be consummate with the information content of the data. Ultimately this information content is determined by the measurement uncertainty. Thus, providing end users with as accurate an estimate as possible of the likely measurement uncertainty, in any specific application, is essential if end users are to be able to make informed decisions. Similarly, end users must specify the data uncertainty requirements for each specific task if the correct tool for the job is to be identified. This requirement for air quality management strategies to acknowledge the capabilities of available devices, both in the setting and monitoring of limits, will only become increasingly important as target levels continue to decrease.

Supplementary

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The supplement related to this article is available online at:

Code and data availability

- The code and data for this study can be found on Zenodo: https://zenodo.org/record/6518027#.YnKbH9PMJhE.
- The live code can be found on GitHub: https://github.com/wacl-york/quant-air-pollution-measurement-errors.

Author contributions

- 629 PE: Funding acquisition; Supervision. SD and PE: Project administration; Formal analysis. SD, PE & SL:
- Conceptualization; Methodology; Investigation. SD & SL: Visualisation; Software. KR, NM, MF: Resources. SD,
- SL, KR, NM, MF: Data curation. SD, PE, SL, TB, NM, TG & DH: Writing review & editing.

Competing interests

The authors declare that they have no conflict of interest.

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Table S1. Research grade instrumentation used for this study.

Analyte		Manchester		York
NO ₂	*Teledyne T500U	**Teledyne T200U	**Teledyne T200U	
	(CAPS)	(Chemiluminescence)	(Chemiluminescence)	
O ₃	*Thermo 49i	**Thermo 49i	**2B	
	(UV photometry)	(UV photometry)	(UV photometry)	
				*Met One BAM
PM _{2.5}				1020
				(Beta attenuation)

^{*}Instruments permanently deployed at the site.

^{**}Instruments temporarily deployed as part of the QUANT study.

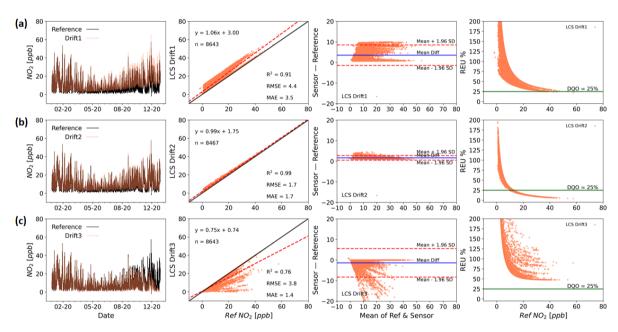


Figure S1. Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels, DQO for $NO_2 = 25\%$) for baseline drift (a-panels), temperature interference drift (b-panels), and instrument sensitivity drift (c-panels) simulated errors.

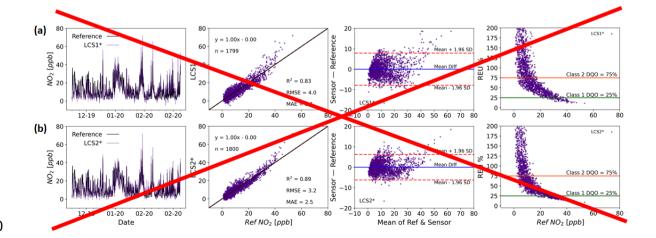


Figure S2. Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels; NO_2 Class 1 DQO = 25% & Class 2 DQO = 75%) for NO_2 measurements by two LCS-bias corrected systems of different brands (panels a and b) in the same location (Manchester Supersite, December 2019 to February 2020. 1hr time res).

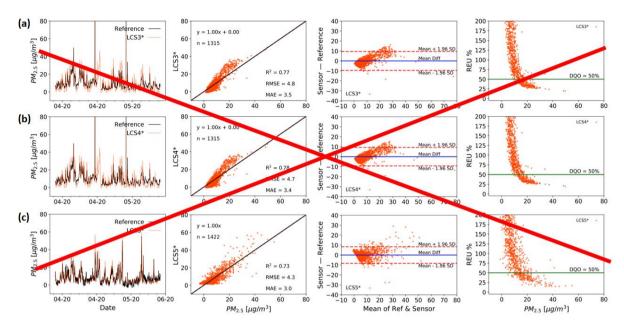


Figure S3.Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels, DQO for $PM_{2.5} = 50\%$) for $PM_{2.5}$ measurements by three LCS bias-corrected systems of the same brand (panels a, b and c) in different locations (April & May 2020,1hr time res): an urban background (Manchester Supersite, a and b panels) and a roadside site (York, c panels).

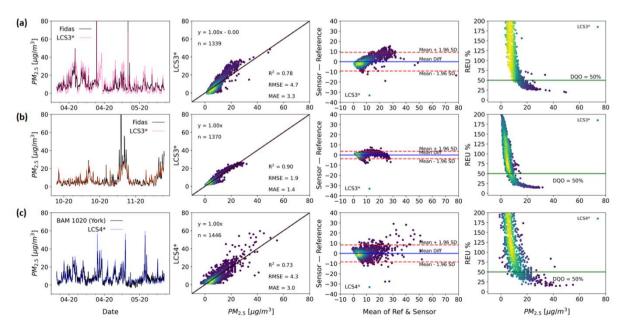


Figure S2. Two bias corrected LCS systems (LCS3 & LCS4, same brand) measuring PM2.5 (Time res 1 h). While LCS3 is shown for the same location (Manchester) but unfolded in two different seasons (a-panels: Apr to May 2020; b-panels: Oct to Nov 2020), LCS4 is at a different location (c-panels: York, Apr to May 2020). Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels; DQO_{PM2.5} =

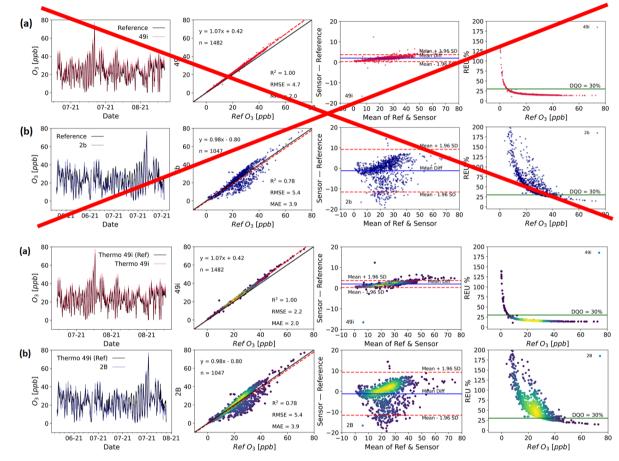


Figure S3. Time series (left panels), regression plots (middle-left panels), Bland-Altman plots (middle-right panels) and REU (right panels, DQO for $O_3 = 30\%$) for two ozone research grade instruments (1hr time res): a Thermo 49i (apanels, July & August 2021) and a 2B (b-panels, June and July 2021). All but the time-series plots have been coloured by data density.