1 Development and Testing of a Novel Sulfur Dioxide Sonde

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14 Abstract. A novel technique has been developed to measure sulfur dioxide (SO₂) using a modification of the existing 15 electrochemical concentration cell (ECC) ozonesonde technology. The current sonde-based method to measure SO₂ (i.e., the 16 dual-sonde approach) involves launching two ozonesondes together with one of the sondes having a filter to remove SO₂ at 17 the inlet. The SO₂ profile is determined by taking the difference between the measurements from the two instruments. The dual-sonde method works well in typical tropospheric conditions when $[O_3] > [SO_2]$ but saturates when $[SO_2] > [O_3]$ and has 18 19 large uncertainties in the upper troposphere/lower stratosphere that would limit its effectiveness in measuring SO₂ from an 20 explosive volcanic eruption. Due to these limitations, several modifications were made to create a single-sonde system that 21 would directly measure SO₂ (i.e., the SO₂ sonde). These modifications included (1) a positively biased ECC current, (2) the 22 addition of an O₃ removal filter, and (3) the addition of a sample dryer. The SO₂ sonde measures SO₂ as a reduction in the cell current. There was a strong correlation ($r^2 > 0.94$) between the SO₂ sonde and a Thermo 43c analyzer during controlled 23 24 laboratory tests and pre-flight tests. Varying humidity levels affected the SO₂ sonde's sensitivity (avg = 84.6 ± 31.7 ppbv/µA, 25 1σ RSD = 37%) during initial field tests, which was resolved by adding a sample dryer upstream of the O₃ removal filter and 26 pump inlet. This modification significantly reduced the variability and increased the sensitivity of the SO₂ measurements (avg 27 = 47 ± 5.8 ppbv/ μ A, 1σ RSD = 12%). Field tests included measurements near Kīlauea Volcano (before and during the 2018) 28 eruption of the Lower East Rift Zone), Costa Rica's Turrialba Volcano, and anthropogenic plumes from the Athabasca Oil 29 Sands region of Alberta, Canada. This single SO₂ sonde system is an effective, inexpensive instrument for measuring both 30 ground-based and vertical profiles of SO₂ from anthropogenic and natural sources (i.e., volcanic eruptions) over a wide range 31 of concentrations.

32 **1 Introduction**

33 Sulfur dioxide (SO₂) emissions result from anthropogenic activities, such as power generation and crude oil refining processes, 34 and natural sources, such as volcanoes. In gas form, SO₂ acts as a respiratory irritant leading to complications with asthma and 35 cardiovascular conditions (Chen et al., 2007; Sunyer et al., 2003; Tzortziou et al., 2015, 2018). Gaseous SO₂ can be converted 36 to sulfate aerosols (Zhang et al., 2015), which are highly scattering, reduce visibility, and can have a cooling effect on the 37 surface climate when injected into the stratosphere (Kiehl and Briegleb, 1993; Schmidt et al., 2010). SO₂ acidifies rain, 38 accelerating damage of infrastructure and vegetation, particularly near SO₂ sources such as volcanoes (Delmelle et al., 2002; 39 Krug and Frink, 1983; Tortini et al., 2017). Due to these various climate, environmental, and human health-related impacts, 40 anthropogenic SO₂ has been heavily monitored (Shannon, 1999; Zhang and Schreifels, 2011), and regulations have been 41 enacted to reduce these emissions (EPA, 2000).

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The largest natural sources of SO_2 are volcanoes. The eruption of Mt. Pinatubo in the Philippines in June 1991 had global climatic effects and significant impacts on the tropospheric and lower stratospheric composition (Bluth et al., 1992; Parker et al., 1996). Apart from such catastrophic eruptions, SO_2 can be continually emitted from volcanoes. SO_2 plumes from over 90 46 volcanoes have been reliably detected by satellites, resulting in the injection of an estimated 23 ± 2 Tg yr⁻¹ of SO₂ into the 47 atmosphere (Carn et al., 2017). However, unlike anthropogenic sources of SO₂, most volcanoes lack routine ground monitoring 48 (Galle et al., 2010; Pieri et al., 2013) and few opportunities exist for routine validation of satellite retrievals of SO₂ with *in situ* 49 measurements. Small unmanned aerial vehicle (UAV) platforms can measure volcanic plumes at altitudes of 2 km above the take-off altitude (Galle et al., 2010; Diaz et al., 2015) while larger UAVs can measure stratospheric plumes (e.g., Global 50 51 Hawk). However, the lack and difficulty of monitoring and the possibility of another stratospheric injection of SO₂ motivated 52 the development of an inexpensive but reliable balloon-borne instrument that could be deployed quickly after an eruption to validate satellite observations with in situ measurements. 53

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55 Radiosondes and ozonesondes have been widely used for measurements of various atmospheric parameters (e.g., temperature, 56 air pressure, relative humidity [RH], and wind speed and direction, and O₃ concentrations). Electrochemical concentration cell 57 (ECC) ozonesondes produce vertical O₃ profiles and allow for the validation of satellite based O₃ vertical column density 58 (VCD). A schematic of the ECC is included in Figure S1. The current sonde-based method for measuring SO₂, the dual-sonde 59 method, uses two En-Sci (Environmental Science Inc., Westminster, CO) ECC ozonesondes in tandem (Morris et al., 2010). 60 For the dual-sonde method, an SO₂ removal filter is placed at the pump inlet of one of the ozonesondes, scrubbing SO₂ from 61 the sampled air before it enters the ECC. The other sonde samples unfiltered air (i.e., air containing both SO_2 and O_3). Due to 62 the chemical reactions in the cathode cell, the filtered sonde measures O₃, while the unfiltered sonde measures the difference between O_3 and $SO_2([O_3] - [SO_2])$ since SO_2 has an equal (relative to O_3) but negative signal in the ECC (Morris et al., 2010). 63 64 The SO_2 concentrations are then determined from the difference between the two sonde measurements. This method works 65 well in the troposphere when the SO₂ concentration is less than the O_3 concentration, but not as well in intense plumes, such 66 as those found in eruptive volcanic environments. When the SO_2 concentration exceeds the O_3 concentration, the cell current 67 in the unfiltered sonde becomes zero. The excess SO_2 saturates the dual-sonde and distorts the calculated SO_2 profile. Additionally, in the stratosphere, where the O₃ signal grows much larger than in the troposphere, the combined uncertainty of 68 69 the measurements of the filtered and unfiltered sondes results in a large lower limit of detection (LLOD), on the order of tens 70 of ppbv. Thus, a field deployment of the dual-sonde method more than a few days after an explosive, tropical volcanic eruption 71 such as Mt. Pinatubo would result in little useful data in the critical upper troposphere/lower stratosphere region.

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This study reports on the development of a single instrument capable of *in situ* SO₂ measurements in the presence or absence of O₃. This sonde can measure SO₂ at much greater concentrations than O₃ without saturating the system and can be configured for a sub-ppbv LLOD (calculated using 3σ) at sea level. Since O₃ is removed from the sample stream, this SO₂ sonde avoids the compounded uncertainties of the dual-sonde method. Field deployments of the SO₂ sonde include sampling of volcanic emissions from Kīlauea on the Big Island of Hawai'i, U.S., Turrialba Volcano in Costa Rica, and the emissions from petroleum extraction and processing at the Athabasca Oil Sands, Canada. Results from these field tests, covering a wide range of SO₂ 79 concentrations from both natural and anthropogenic emission sources, are described below. The SO₂ sonde has been used for

80 tethered and free-release balloons but can also be adapted for UAV platforms.

81 2 Instrumentation

82 **2.1 Ozonesondes**

The standard and modified ECC En-Sci ozonesondes were used for the O_3 and SO_2 sonde measurements in this study. The basic functioning of the ECC ozonesonde is described in Komhyr (1969) and Morris et al. (2010). The ECC sensor is composed of platinum cathode and anode electrodes, each in its own cell, immersed in a diluted and saturated solution of potassium iodide (KI), respectively. The cells are connected by an ion bridge allowing for the transfer of electrical charges while maintaining the separation of the solutions (Eq. 1 and 2). When the cells are charged with the solution, a transient potential difference is generated that is dissipated through the redistribution of charge across the ion bridge. The following equilibria are established from these reactions:

90
$$3I^- \rightleftharpoons I_3^- + 2e^- \text{ (anode)}$$
 (1)

91
$$I_2 \rightleftharpoons 2e^- \to 2I^- \text{ (cathode)}$$
 (2)

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Sampled air is pumped into the cathode cell, and the presence of O_3 initiates a reaction (Eq. 3) that causes an imbalance in favor of $[I_2]$ in the cathode solution.

$$95 \quad 2KI + O_3 + H_2O \to 2KOH + I_2 + O_2 \tag{3}$$

To rebalance the electrochemical potential of the cell, the iodine/iodide redox reactions in Ep. 4 and 5 result in a flow of electrons from the anode to the cathode via the ion bridge. This cell current, measured by an external ammeter, is proportional to the O₃ concentration.

$$99 \quad 3I^- \to I_3^- + 2e^- \text{ (anode)} \tag{4}$$

$$100 \quad I_2 + 2e^- \to 2I^- \text{ (cathode)} \tag{5}$$

When SO_2 is present in the sample air, an additional reaction (Eq. 6) occurs in the cathode cell of the ECC, supplying the two electrons needed to rebalance the cathode cell after the O_3 reaction (Eq. 3) (Komhyr, 1969; Morris et al., 2010).

$$103 \quad SO_2 + 2H_2O \to SO_4^{2-} + 4H^+ + 2e^- \tag{6}$$

Thus, each SO₂ molecule in the sampled air has the effect of cancelling the measurement of one O₃ molecule. In effect, the standard ECC ozonesonde reports $[O_3]$ - $[SO_2]$ for its measurement. In most places and at most times, $[SO_2] \ll [O_3]$, so there 106 is not a significant impact on the O3 measurements, but in places downwind of SO2 sources (e.g., coal-burning power plants

107 or volcanos), the O₃ measurement will be negatively impacted.

108 2.2 Instrumentation

109 Several SO₂ and O₃ instruments were used for validation of the SO₂ sonde during laboratory and field testing. A calibration 110 system was used to produce controlled concentrations of SO_2 and O_3 . The calibration system relied on the operation of flow controllers or restrictors, an SO₂ ultra-high purity (UHP) gas cylinder (4.87 ppm; Scott-Marrin, Inc., Riverside, CA) and/or a 111 112 U.V. Photometric O₃ calibrator (49C PS; Thermo Fisher Scientific, Franklin, MA), and zero air to produce desired pre-set 113 concentrations of SO₂ and/or O₃. The zero-air setup used for the field and laboratory testing was achieved using a dry zero air 114 UHP gas cylinder or else generated by scrubbing ambient air through activated charcoal and Purafil SP (Purafil, Inc., Doraville, 115 GA) canisters. The Thermo 43i-TL SO₂ analyzer (LLOD: 60-90 pptv at 5 min averaging) and the 49i O₃ analyzer (LLOD: 1.5 116 ppbv at 5 min averaging) were also used during laboratory testing, while a Thermo 43c-TL SO₂ analyzer was used during field 117 testing in Hawai'i. These instruments were set to report 10 s average measurements.

118 **3 Single-sonde SO₂ System and Laboratory Testing**

119 **3.1 SO₂ sonde system description**

120 The single-sonde SO₂ system included three major modifications to the En-Sci ECC ozonesonde: (1) the application of a 121 positively biased current to the cathode cell, (2) the addition of an O_3 removal filter, and (3) a sample dryer (Fig. S1). The first 122 version of the SO₂ system (SO₂ sonde v1.0) included the first two modifications: the bias current and an O₃ removal filter. The 123 bias current sets the upper limit of detection (ULOD) for the SO₂ sonde and is set prior to measurement. The O₃ removal filter 124 is placed in line with the inlet allowing O_3 -free air to be sampled in the SO₂ sonde. In the ECC, O_3 produces a positive response 125 signal while SO_2 produces a negative signal when sufficient O_3 is present (i.e., positive signal). With these two modifications, 126 SO₂ can be measured directly as the reduction of the cell current from the pre-set biased current (Flynn and Morris, 2021). 127 Unlike the dual-sonde system, this approach allows for direct SO₂ measurements rather than an inference by subtraction of 128 signals from two separate instruments. A sample dryer was added to the SO_2 sonde in the second version (v1.1) to combat 129 humidity issues discovered after initial field tests. The addition of the dryer corrected the highly varying instrument sensitivity 130 observed in the field. All components of the SO₂ sonde fit within a standard ozonesonde foam box (approximately 8" x 8" x 131 10") except for the inlet filter. The free-release balloon payload's total mass is approximately 1 kg. The patent publication and 132 Fig. S1 provides a detailed description and schematic of the SO₂ sonde (Flynn and Morris, 2021).

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134 **3.2 Testing of the bias current**

135 The bias current is supplied by inserting into the cathode cell an additional platinum electrode powered by a 9V battery (Fig. 136 S1) (Flynn and Morris, 2021). To maintain consistent power, the circuit uses a 5V regulator. Varying the resistance allows for 137 a range of bias currents to be introduced. The current version of the SO₂ sonde uses a fixed resistor which requires a priori 138 knowledge of the desired SO₂ concentration range. The desired resistor is installed in series with the battery and the electrode. 139 An earlier laboratory test compared the SO₂ sonde measurements (initially configured without an O_3 removal filter) to those 140 made by a 43*i*-TL SO₂ analyzer (Fig. 1, Table 1). O₃ and SO₂ gases were introduced using the laboratory calibration setup and 141 a manifold to allow the sonde and the Thermo trace gas instruments to sample the same air. Results in Fig. 1 show 60 s averaged 142 data. The test included (A) input of O_3 without an added bias current; (B) the same input of O_3 with the addition of a bias 143 current (equivalent to approximately 90 ppbv of O_3); and the addition of SO_2 to the O_3 with the enhanced bias signal where 144 the SO₂ concentration was either (C) smaller or (D and E) larger than the O₃ concentration. During (A), measurements made 145 by O₃ and SO₂ sondes compare well to measurements made by the Thermo instruments (Fig.1, Table 1). The test included (E) the response of the SO_2 sonde to a reduction of the O_3 concentration resulting in an equivalent decrease in signal, followed by 146 147 (G-I) a reduction in the SO₂ concentration resulting in an equivalent increase in signal. At (F), the SO₂ concentration exceeded 148 the bias current (90 ppby), producing a signal equivalent to 2.9 ± 0.1 ppby. The sonde successfully measured SO₂ both with 149 and without O₃ with approximately 97% efficiency.

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151 Examination of the SO₂ sound data showed that noise was proportional to the measured signal, with $1-\sigma$ noise at approximately 0.2 - 0.3% of the measured signal. Because increases in the SO₂ concentrations result in decreases in the signal (i.e., lower 152 153 cell currents), the magnitude of the applied bias current determines the saturation point (i.e., ULOD) of the SO₂ sonde; 154 saturation occurs when the measured cell current drops to zero. Applying a higher bias current increases the ULOD but also 155 increases noise and the LLOD. The reported LLODs of bias currents are calculated as 3σ relative to the baseline signal when 156 sampling zero air. During laboratory testing, the LLOD (3σ) was calculated for a range of applied bias currents (0.25 to 10.0 157 μ A). The LLOD for the varying bias current of 0.25 to 10.0 μ A ranged from approximately 0.002 to 0.084 μ A, respectively. 158 Results of calculated LLOD of a 0.25 µA bias current at varying replicated altitudes is included in Table S1. At the surface, 159 the LLOD of 20s averaged measurements is 0.17 ppby. The final version of the SO₂ sonde (v1.1) requires the bias current to 160 be selected prior to measurement. If the bias current is set too low, a measurement of larger than expected SO₂ concentrations 161 can saturate the sensor while a bias current that is set too high will have higher LLOD due to the increase in noise. The applied 162 magnitude of the bias current can be best determined based on known SO₂ sources including volcanic emissions, urban and/or 163 industrial emissions.

164 **3.3 Testing of O₃ removal filter**

165 Since the ECC responds to both O₃ and SO₂, an O₃ removal filter was developed to remove interference from O₃ in the sample. 166 This proprietary O₃ removal filter is placed upstream of the sonde inlet (Flynn and Morris, 2021). During laboratory testing, 167 the O₃ removal filter was exposed to a continual concentration of 487 ± 3 ppbv of O₃ and a varying concentration of SO₂ 168 ranging from 0 to 111 ± 1 ppbv (Fig. 2). The O₃ was effectively and consistently removed from the sampled air by the O₃ 169 removal filter as SO₂ was diluted. The testing included measurements with (gray background) and without (white background) 170 the O₃ removal filter. The SO₂ and O₃ concentrations measured by the Thermo 43*i*-TL and 49*i* instruments, respectively, and changes in SO₂ dilution levels are also indicated in Fig. 2. The O₃ removal filter destroyed the O₃ at all SO₂ dilution levels to 171 172 below the detection limit of the O₃ instrument. By comparing the Thermo 43*i*-TL SO₂ analyzer measurements with and without 173 the O₃ removal filter, SO₂ passed through the filter with 88% efficiency (Fig. 3a). The transmission efficiency was calculated 174 by taking the ratio of SO₂ measured by the sonde to that measured by the analyzer. The SO₂ transmission efficiency increased 175 to 97% when testing the O₃ removal filter with the dry zero air UHP gas cylinder (Fig. 3b) instead of the zero-air generator 176 that processes ambient laboratory air (Fig. 3a). Additional testing of the O₃ removal filter demonstrated that the filter removed 177 approximately 1 ppm of O_3 at sea level with > 99.9% in O_3 removal efficiency, concentrations below the detection limit of the 178 Thermo 49*i* O₃ monitor.

179 **3.4 Sample Dryer**

180 The SO₂ sonde v1.0 had highly varying sensitivities during the initial field tests. The instrument sensitivity was determined by 181 regression analysis of the sonde's cell current to the SO₂ concentration measured by an SO₂ analyzer. The variability in the 182 sensitivities was hypothesized to be due to differing levels of humidity during each SO₂ sonde launch. SO₂ is soluble in water 183 and through multiphase reactions can be oxidized to sulfuric acid in the atmosphere in the presence of water vapor (e.g., 184 precipitation, clouds, fog, etc.) (Carmichael and Peters, 1979; Zhang et al., 2013; Terraglio and Manganelli, 1967). Factors 185 including liquid water content, aerosol composition, aerosol loading, and pH of the water are important in determining the 186 adsorption and oxidation rates of SO₂ (Liu et al., 2021). When air with elevated humidity is flowing through a filter, SO₂ gas 187 is likely adsorbing on the filter causing lower SO_2 transmission efficiency due to the potential uptake of SO_2 in water on the 188 filter. Several laboratory tests confirmed the need to remove water from the sample upstream of the O₃ removal filter to improve 189 the measurement of SO₂. A desiccant membrane dryer (Perma Pure LLC, Lakewood, NJ) composed of a NafionTM tube in 190 silica gel desiccant was placed in-line upstream of the O_3 removal filter. This sample dryer is lightweight, relatively 191 inexpensive, and does not require power.

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Laboratory tests included exposing the SO₂ sonde, with and without a sample dryer, to controlled levels of humidity and SO₂.
Without removing water vapor, the SO₂ transmission efficiency decreases as humidity increases, particularly above 50% RH
(Fig. 6). As the O₃ removal filter is humidified, the SO₂ transmission efficiency decreases. With the sample dryer in place,

each of the laboratory SO₂ transmission efficiency (May 17-18 and 21, 2018) tests varied by an average of <1% across a range of 0-85% RH (Fig. 6).

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199 The dryer's useful lifetime was determined by continuously exposing it to high humidity (> 95% RH at approximately 23 °C) sample stream. The downstream RH climbed from 5% to 16% after 2.3 h and to 25% after 6.3 h. At these downstream RH 200 levels, the SO₂ transmission efficiency remained above 95%. A typical SO₂ sonde's measurement time per flight, including 201 202 pre-flight calibration, is approximately three hours. The dryer's useful lifetime is likely much longer than required for a balloon 203 flight since exposure to 95% RH conditions for several hours is highly unusual outside of hurricanes and tropical systems. SO₂ 204 sonde and Thermo 43*c*-TL measurements were strongly correlated ($r^2 = 0.99$) during a multipoint calibration conducted using 205 the O₃ removal filter and the dryer under relatively high humidity levels. During that calibration, the SO₂ sonde's sensitivity 206 was 45.43 ± 0.17 ppbv/µA. By comparison, the average sensitivity during the initial Hawaii deployment was 84.6 ± 31.7 207 ppbv/uA across 10 sondes. The sample dryer, therefore, improved both the sensitivity and stability of the measurements 208 observed. The addition of the sample dryer is necessary for providing accurate ambient SO₂ measurements.

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210 4. Field Deployments with SO₂ sonde v1.0

211 The SO₂ sonde v1.0, single-SO₂ sonde without the sample dryer, was deployed and tested in Hawai'i and Costa Rica (Fig. S2). 212 The field sites were close to active volcanoes, which are significant sources of natural SO₂ (Tang et al., 2020; Carn et al., 213 2017). In Hawai'i, field measurements were made near Kīlauea Volcano on the south-eastern shore of Island of Hawai'i, the 214 largest of Hawai'i's islands. Kīlauea is the voungest volcano on the island and one of Earth's most active volcanoes (Kern et 215 al., 2015; Nadeau et al., 2015). Kīlauea had been in a state of eruption since 1983 (Patrick et al., 2019) with an average SO₂ 216 release rate of approximately 5,500 T/d measured during 2014 – 2017 (Elias et al., 2018). In Costa Rica, field measurements 217 were made near Turrialba Volcano, one of the most active volcanoes in the Central American Volcanic Arc. Studies of 218 emissions from Turrialba prior to 2013 reported SO₂ release rates of up to 4,000 T/d (de Moor et al., 2016; Xi et al., 2016). 219 The activity of Turrialba increased after 2014, raising concerns for air quality and environmental health (de Moor et al., 2016; 220 Tortini et al., 2017).

221 4.1 Kīlauea, Hawai'i - February 2018

The first deployment of the SO₂ sonde v1.0 was during NASA's HyspIRI HyTES Hawaii Campaign (H3C) from February 3-10, 2018, near Kīlauea Volcano. The instrument was tested in flights on free-release balloons and a tethered balloon system (TBS), and at ground level with measurements in Hawaii Volcanoes National Park (HVNP) downwind of Kīlauea's summit crater, Halema'uma'u. During the ground-level testing, an SO₂ sonde and a Thermo 43*c*-TL SO₂ analyzer's sample inlet were mounted on the top of a van for co-located sampling.

227 Figure 4a depicts the measurements taken during the first encounter with an SO₂ plume while driving through the HVNP on February 3, 2018. The strongly correlated SO₂ sonde and Thermo 43*c*-TL measurements ($r^2 = 0.99$) reached upward of ~940 228 229 ppbv. The SO₂ sonde had a sensitivity of 118.4 ± 0.4 ppbv/ μ A, determined by regression analysis of the sonde's cell current 230 with the Thermo 43*c*-TL concentrations (Fig. 4a). The SO₂ sonde sensitivity varied significantly during the field deployment. 231 During surface measurements on February 10, 2018, earlier zero-air calibrations measured a sensitivity of 86.5 ± 1.5 ppby/uA, while measurements during an SO₂ plume event, with peak concentrations of up to 400 ppbv, found the SO₂ sonde's sensitivity 232 233 was 73.9 ± 0.6 ppby/µA (Fig. 4b). Although the SO₂ sonde sensitivity varied significantly in ten subsequent calibrations (84.6 \pm 31.7 ppbv/ μ A), the measurements remained strongly correlated (range: $r^2 = 0.94 - 0.99$). The variability in the sensitivity in 234 235 the field was due to changes in the ambient RH impacting the SO_2 transmission efficiency of the O_3 removal filter. This 236 hypothesis was confirmed by laboratory RH testing and discussed in Sect. 3.3 and 3.4.

237 4.2 Turrialba, Costa Rica (Dual-sonde versus SO₂ sonde comparison)

238 On March 23, 2018, a traditional SO₂ dual-sonde payload (Morris et al., 2010) as well as the SO₂ sonde v1.0 were launched 239 using a free-release balloon flight from the Universidad de Costa Rica's campus in San Jose (approximately 31 km downwind 240 of Turrialba Volcano). This flight provided the first direct in situ comparison of the two SO₂ sonde methods. Figure 5 shows 241 the response of the SO_2 sonde v1.0 and the calculated SO_2 dual-sonde profile. The dual-sonde SO_2 method can only report 242 concentrations of SO_2 up to a maximum of the concentration of O_3 present. Furthermore, because the SO_2 concentration is 243 determined by subtracting the signals from two instruments, its uncertainty is higher than the uncertainty of a measurement 244 from a single instrument. When $[SO_2] > [O_3]$, the dual sonde's unfiltered ozonesonde signal goes to zero, as happened for the 245 Turrialba sonde launch between 3-5 km (Fig. 5). The SO₂ saturates the cathode solution in the unfiltered sonde, not recovering 246 until enough ambient O_3 has been processed to rebalance the cell, resulting in a distorted profile (Fig. 5). For this flight, the 247 SO₂ sonde was configured to its maximum range (ULOD of approximately 450 ppbv at standard pressure) and was able to 248 capture both the small plume below 2 km above mean sea level (AMSL) (approximately 18 ppbv) as well as the primary plume 249 between 3 - 4 km AMSL (approximately 230 ppby). The SO₂ sonde v1.0 was able to capture the full shape of the profile, 250 including the peak values and structure of the plume. The SO₂ sonde v1.0 reports the top of the plume around 4 km AMSL, 251 whereas the dual-sonde remains saturated until closer to 5 km AMSL. Thus, the dual-sonde SO₂ profiles, when saturated by 252 high concentrations of SO_2 , erroneously appear to have a greater vertical extent. Further, the SO_2 sonde v1.0 showed no 253 interference from O₃ at altitudes from the surface to 24.4 km AMSL, with O₃ concentrations in the stratospheric O₃ layer 254 reaching > 4 ppmv (not shown), demonstrating the effectiveness of the O₃ filter. The SO₂ VCD was 8.3 DU (Dobson Units, 1 255 $DU = 2.69 \times 10^{16}$ molecules cm⁻²) for the SO₂ sonde but was only 3.4 DU for the dual-sonde measurement. Thus, once saturated, 256 the dual-sonde method is likely to underestimate the SO₂ VCD.

257 5 Field Deployments with SO₂ Sonde v 1.1

258 The updated SO_2 sonde (SO_2 sonde v1.1) with the dryer filter was deployed and tested near Ft. Mackay, Canada, and again in 259 Hawai'i in June 2018. Ft. Mackav is in the Alberta province of Canada and is home to the Athabasca Oil Sands, a large area 260 of bitumen and heavy crude oil surface deposits high in sulfur content. Local processing of these products (e.g., surface mining) 261 and resulting by-products (e.g., tailing ponds) can release significant amounts of SO₂ into the atmosphere (Bari et al., 2020; 262 McLinden et al., 2016; Simpson et al., 2010). A second field deployment to Hawai'i followed immediately after the deployment 263 to Canada. On May 3, 2018, Kīlauea Volcano on Hawai'i entered a new eruptive phase with an outbreak of a series of fissures 264 in the lower Puna area (Liu et al., 2021; Anderson et al., 2019; Gansecki et al., 2019; Patrick et al., 2020). The active phase 265 volcanic gas emissions resulted in localized evacuations in the Lower East Rift Zone (LERZ), destroying more than 700 homes 266 and displacing thousands of residents, and resulting in poor air quality for much of the southern and western portions of the 267 island (Tang et al., 2020). The eruption event entered a paused phase in early August, and was declared over on December 5. 268 2018 (Kern et al., 2020).

269 5.1 Athabasca Oil Sands, Canada

270 The SO₂ sonde v1.1 was tested in Ft. Mackay (57.1206° N, 111.4241° W), Alberta, in the Athabasca Oil Sands from June 10 271 - 16, 2018 (Fig. S2c). This field project, conducted in conjunction with Environment Canada and York University, evaluated 272 SO₂ emissions from industrial activities in and near the oil sands region using a combination of TBS and ground-based 273 measurements. The SO₂ sonde v1.1 was flown on the York TBS payload recording measurements from the ground to 300 m 274 above ground level (AGL; 650 m AMSL). This deployment provided a dilute anthropogenic plume to test the SO₂ sonde in a 275 high-sensitivity, low-range configuration. The average sensitivity of the SO₂ sonde v1.1 during the project was 51 ± 1.2 276 ppbv/ μ A. The SO₂ sonde was configured to sample in a range from ~0.5-25 ppbv of SO₂. The TBS SO₂ sonde's vertical 277 profiles were averaged into 10 m altitude bins that measured SO₂ concentration ranges that are more representative of 278 anthropogenically-impacted SO₂ rather than large volcanic plumes (Fig. 7). This field deployment also demonstrated the 279 performance of the sonde at sub-ppbv levels of ambient SO₂.

280 **5.2 Kīlauea, Hawai'i - June 2018**

In response to the larger eruption that started in May 2018, the SO₂ sonde v1.1 was deployed to Hawai'i for the NASA-funded Big Island SO₂ Survey (BISOS). The SO₂ sonde launches occurred from Kahuku Ranch (19.0549° N, 155.6934° W) and Na'alehu Elementary School (19.0610° N, 155.5788° W) approximately 90 km downwind of Kīlauea's LERZ (Fig. S2d). The site's distance from the source allowed the plume to disperse and dilute as compared with measurements at the vent. An SO₂ plume was detected during seven of the nine free-release balloon launches during the June 2018 BISOS campaign. The ten SO₂ sonde v1.1 calibrations performed during BISOS had an SO₂ sensitivity of 47.0 ± 5.8 ppbv/ μ A and were similar to the laboratory results (45.43 ± 0.17 ppbv/ μ A).

289 With the anticipated levels of SO₂, the sondes were configured to sample in the range of 10-450 ppby of SO₂. Figure 8 shows 290 four distinctive SO₂ profiles, and Table 2 includes the VCDs for each flight. No plumes above 5 km AMSL were detected. 291 All but one of the observed SO₂ plumes were below the capping inversion of the planetary boundary layer (PBL). On June 292 22 (Fig. 8a), the ascent profile shows SO₂ below 3 km AMSL peaking at nearly 100 ppby and additional features between 3-293 4 km AMSL peaking at 20-35 ppbv (Tang et al., 2020). The latter peaks were correlated with higher RH, perhaps the result 294 of steam from a vent or the ocean entry points having broken through the inversion. The early afternoon June 28 profile (Fig. 295 8b) shows the highest concentration (325 ppbv) for a resolved SO₂ plume during the BISOS campaign. Typical for the trade 296 winds, NOAA HYSPLIT trajectories (Stein et al., 2015) showed the winds were out of the NE, consistent with the plume's 297 transport from vents in the LERZ or the lava ocean entry points. Although the descent profile from a June 29 early afternoon 298 launch lost the signal at 0.58 km AMSL, Fig. 8c shows an SO₂ plume over the ocean with a peak concentration of 188 ppbv 299 at 0.74 km AMSL. HYSPLIT trajectories again showed the winds were out of the NE. Lastly, the SO₂ plume detected during 300 the ascent of the June 30 launch (Fig. 8d) exceeded the ULOD between 1-3 km AMSL for the SO₂ sonde configuration used. 301 The distorted SO₂ enhancement extending above the PBL as determined by the temperature inversion is most likely an 302 artifact of the saturated sonde, similar to what was seen in the dual-sonde profile from Costa Rica (Fig. 5). As the RH 303 remains low above the PBL, it is most likely that the SO₂ is contained entirely within the PBL.

6. Conclusion and Future Work

305 An innovative new method for measuring vertical profiles of SO₂ from TBS and free-release balloons was successfully tested 306 and demonstrated in controlled laboratory experiments and during four different field deployments covering SO₂ 307 concentrations ranging from 0.5-325 ppbv during flights and up to 940 ppbv during ground measurements. This new method 308 requires three major modifications to the standard ECC ozonesonde: the addition of a positive bias current in the cathode cell, 309 an O₃ removal filter, and a sample dryer. Relative to the previous dual-sonde method, the new method measures SO₂ using a 310 single-sonde system (i.e., the SO₂ sonde). The SO₂ sonde and Thermo 43c-TL measurements were strongly correlated during 311 laboratory ($r^2 > 0.99$) and field-based ($r^2 > 0.94$) comparisons. Initial field tests and subsequent laboratory testing of SO₂ sonde 312 v1.0 highlighted the need to dry the sample upstream of the O₃ removal filter to achieve consistent results. Follow-up field 313 measurements in the Athabasca Oil Sands and Hawai'i clearly demonstrated the improvement in the SO₂ sonde v1.1's 314 sensitivity and consistency (51 \pm 1.2 and 47 \pm 5.8 ppbv/ μ A, respectively) as a result of drying the sample.

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The SO₂ sonde v1.1 offers several advantages over the dual-sonde method, including the ability to measure $[SO_2]$ independent of $[O_3]$, the capability of sub-ppbv detection limits, faster response and recuperation time when exposed to larger SO₂ plumes, and reduced uncertainty. The lighter weight of the payload requires a smaller balloon and less helium to lift, which may prove advantageous for deployment under some field conditions, particularly where helium supplies are limited. It's compactness 320 and weight can also make it a candidate for UAV campaigns. Field deployments revealed specific issues and areas for 321 improvement. The present design requires pre-setting the sonde's bias current prior to the launch. Thus, some *a priori* estimates 322 of the plume are required to determine the appropriate bias current so that the instrument can measure the full range of SO_2 323 concentrations present. In the current SO_2 sonde v1.1, increasing the ULOD by applying a larger bias current also increases 324 the LLOD. Further laboratory experiments are needed to identify the factors that cause the remaining observed variability in 325 the SO₂ transmission efficiency in the latest instrument version that includes the sample dryer. Much of the testing and 326 calibration completed to date assessed the complete SO₂ sonde system (i.e., sonde, filter, dryer). Building a database of the 327 various individual factors, including pump speeds and filter transmission efficiency, will help us to better characterize the 328 causes of sonde-to-sonde variability and allow future versions of the system to improve performance characteristics so that the 329 system can be made available for operational use. Additionally, future manuscripts topics include intercomparison studies of 330 the SO₂ sonde's vertical profile measurements with other column measurements (i.e., Pandora) and satellite measurements and 331 more in-depth analysis of the SO₂ sonde measurements at the various field deployments.

332 Author Contributions

Conceptualization by J.H.F. and G.M. Data curation by J.H.F., A.K., S.L.A., M.G.S., E.K., P.W., G.M., E.C., A.A., and J.A.D.

Formal analysis by A.K., S.L.A., S.Y. and P.W. Funding acquisition by J.H.F. Investigation by A.K., S.L.A., M.G.S., and E.K.

335 Methodology by J.H.F. and G.M. Writing – original draft preparation by S.Y. Writing – review and editing by P.W. G.M.,

336 J.A.D. and J.H.F. Supervision by J.H.F.

337 **Conflict of Interest:** The authors declare that they have no conflict of interest.

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	O ₃ Thermo (ppbv)	O ₃ Sonde (ppbv)	SO ₂ Thermo (ppbv)	SO ₂ Sonde (ppbv)
Α	105 ± 0.4	100 ± 1.3	0.0 ± 0.06	96 ± 1.3
В	105 ± 0.5	101 ± 0.4	0.0 ± 0.06	188 ± 2.3
С	103 ± 0.4	99 ± 0.4	57 ± 0.37	135 ± 1.0
D	105 ± 0.5	97 ± 0.6	116 ± 1.9	78 ± 1.0
Е	-	-	-	-
F	1.3 ± 0.5	$\textbf{-0.13}\pm0.08$	116 ± 1.4	2.9 ± 0.1
G	1.1 ± 0.4	-0.51 ± 0.11	58 ± 0.7	29 ± 0.5
н	0.61 ± 0.39	0.15 ± 0.03	24 ± 0.8	64 ± 0.6
I	0.31 ± 0.31	0.64 ± 0.27	0.25 ± 0.22	89 ± 0.6

Table 1: Averaged O₃ and SO₂ concentration measured by the SO₂ sonde version 1.0 and Thermo instruments during different stages of testing indicated in Fig. 1.

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Table 2. The SO₂ vertical column density (VCD) for profiles shown in Fig. 8 from BISOS in June 2018. For profile c, the descent profile VCD is reported for the flight without extrapolation (shown without parentheses) and using linear extrapolation assuming the SO₂ concentration to be 0 ppbv at sea level (shown in parentheses).

Profile	Launch Time (UTC)	SO ₂ VCD
a (ascent)	06/22/2018 00:32	8.6 DU
b (ascent)	06/28/2018 20:45	12.5 DU
c (descent)	06/29/2018 21:36	6.2 (9.8 [*]) DU
d (ascent)	06/30/2018 20:48	79.1 DU**

* VCD from extrapolated data

** Saturation of SO₂ at altitudes of 1 to 3 km AMSL



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Figure 1: Test of the SO₂ sonde v1.0 (without an O₃ removal filter) with an applied bias current responding to O₃ and SO₂. See the text for further details.



Figure 2: Time of series of a multipoint test of the O₃ filter removal efficiency and impact on SO₂ measurements taken by a Thermo 43*i*-TL SO₂ analyzer. Changes in SO₂ dilution levels are indicated by the pink lines (diamond markers).



Figure 3: Response of Thermo 43*i*-TL SO₂ analyzer with (y-axis) and without (x-axis) an O₃ removal filter using a calibration system with (a) a processed zero air system and (b) a dry zero air gas cylinder.

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Figure 4: SO₂ sonde v1.0 and Thermo Environmental SO₂ analyzer measurements at Kīlauea, Hawai'i during H3C for (a) initial SO₂ plume encounter on February 3, 2018, and (b) a pre-flight measurement on February 10, 2018, approximately 6 km downwind

366 SO₂ plume encounter on Feb367 of Kīlauea's summit crater.







Figure 6: Tests of SO₂ transmission efficiency as a function of relative humidity without (circles) and with (diamonds) an upstream sample dryer.





Ambient Tempterature, °C



377

SO₂, ppbv; RH, %



380 6/29/2018 21:36; and (d) 6/30/2018 20:48. All times are UTC.

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