



# 1 Performance evaluation of an integrated path

2 differential absorption LIDAR model for surface

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pressure from low-Earth orbit

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10 Abstract. Remote sensing of surface pressure from space is critical; differential absorption 11 LIDAR and differential absorption radar are only two kinds of remote sensing instruments 12 with this potential. The differential absorption LIDAR works in integral path mode from the 13 satellite in low-Earth orbit. It measures the differential optical depth of the Oxygen A-band, 14 and the surface pressure is thereafter obtained by performing circle-iterative calculation. Performance evaluation of the differential absorption LIDAR model was conducted with 15 16 respect to the advanced system parameters of the space instrument, Low echo pulse energy at 17 ocean surface and the challenging calculation of repetitive cannelative average of echo on 18 uneven land surface yielded random errors in surface pressurement. On the other 19 hand, uncertain atmospheric temperature and water vapor mixture profiles resulted in 20 systematic error of surface pressure. Consequently, controlling the error of surface pressure 21 within 0.1% proved challenging. Under a strict implementation of the error budget, the time 22 resolution is 6.25 s and along-orbit distance resolution is 44km, and the results showed that 765.6735/765.4637 nm is suitable as the working wavelength pair. Further, error could be 23 24 expected to within 0.2-0.3% for the cumulative average of 625 ocean surface laser pulse 25 echoes, cumulative average of more than 144 pulse echoes on land, and observation from the 26 400km orbit.

#### 27 1 Introduction

28 Atmospheric pressure plays a vital role in several atmospheric processes related to 29 atmospheric dynamics. Low/high pressure, low pressure troughs, high pressure ridges, and 30 anticyclones and other related information have been introduced into the atmospheric model. 31 Hurricanes are profound low-pressure systems that originate from low-pressure cyclones in 32 the tropical or subtropical oceanic regions. Accurate prediction of their formation, landing 33 direction, and movement trajectory requires atmospheric pressure gradient distribution data. 34 Fundamentally, the density of the atmosphere in high latitudes increase during winter, causing the air to shrink and sink, thereby increasing the pressure and gradually resulting in the 35 formation of a powerful, deep, and broad air mass. Upon the accumulation of a sufficient cold 36 37 high-pressure force, a cold wave is formed, which rolls out and pours down. Meanwhile, 38 airspace for the release of radio sounding balloons is restricted; thus, continuous detection 39 during the entire day is not possible. Brown et al.(1986) reported that the accuracy of the 40 weather models is primarily limited by the regional sparsity of the input data. Specifically, 41 atmospheric pressure data is very sparse in large areas of the ocean, desert, plateaus, and polar 42 regions. Consequently, the International Meteorological Organization aims to achieve remote 43 sensing of surface pressure at an accuracy of 0.1-0.3% (Korb et al., 1995) (WMO-ICSU, 1973), 44 which however, remains a big challenge.





45 In 1983, Korb, C. L. et al., (1983) of Laboratory for Atmospheres, NASA Goddard Space 46 Flight Center, proposed a method of detecting atmospheric pressure using differential 47 absorption LIDAR and the trough between oxygen absorption lines. In 1987, Schwemmer et 48 al.(1987) structured a novel differential absorption LIDAR system. It employs a flash-pump alexandrite laser to emit a beam of two wavelengths of approximately13160cm<sup>-1</sup>, coupled with 49 50 an oxygen photoacoustic absorption cell and a high-precision wavelength meter to stabilize 51 the emission wavelength. Moreover, the seed source is a continuous wave from either a 52 Ti:sapphire single longitudinal mode laser or a diode laser (Schwemmer et al., 1987). In June 53 and July 1989, a series of flight measurement tests were conducted on the east coast of the 54 United States(Korb et al., 1989). In 1999, Flamant, C. N., Schwemmer, G. K. Korb, C. L., 55 Evans, K. D. and Palm, S. P. published their report "Pressure measurements Using and 56 Airborne Differential absorption LIDAR. Part I: Analysis of the systematic error 57 sources,"( Flamant et al., 1999) where in the instrumental and systematic error sources of 58 differential absorption LIDAR was analyzed when measuring atmospheric pressure profile.

59 In the ASCENDS (Active Sensing of CO<sub>2</sub> Emission over Nights, Days, and Seasons) 60 program, the surface pressure was determined to accurately measure the CO<sub>2</sub> dry mixing 61 ratio(Zaccheo et al., 2014; Crowell, et al., 2015). Between 2007 and 2013Stephen, M. 62 Krainak, M. Riris, H. and others of NASA Goddard Space Flight Center and Allan, G. R. of 63 Sigma Space Corporation reported on the use of an aircraft as a platform and transmitter to 64 continuously send out pulse trains of multiple wavelengths of approximately 764.7nm with 65 the receiver receiving the return echoes.(Stephen et al., 2007-2008; Riris et al., 2012-66 2013,2017) Thus, multiple pulse train return signals were accumulated, using which the oxygen absorption spectrum curve of the 764.5-764.9nm trough segment was plotted. 67 68 Subsequently, the differential optical depth of oxygen was calculated from the transmittance 69 curve.

70 Dual-wavelength (detection/reference wavelengths) laser pulses are launched downwards 71 from the space platform(Mill án et al., 2014); consequently, the reflected laser pulses energy 72 from the earth's surface or the top of a cloud are received. Subsequently, the atmospheric 73 optical depth and flight time of the laser pulses passing through the air column are measured. Thus, the atmospheric pressure and altitude of the surface/cloud top can be simultaneously 74 75 obtained, and the top of the cloud ground can be distinguished from the ground. Such data is 76 meaningful for various meteorological applications. By obtaining the pressure values on the 77 surface and cloud tops and combining the results with a vertical temperature profile obtained 78 from other sensors or weather models and utilizing statistical equations, the vertical profile of 79 atmospheric pressure can be obtained. The differential absorption LIDAR is installed on a 80 sun-synchronous orbit, and it makes a polar orbit around the earth from south to north. It 81 allows much denser surface/cloud top atmospheric pressure data than ground meteorological 82 stations to be obtained.

This paper is structured as follow. Section 1 presents the Introduction, and Section 2, the
mechanism of differential absorption LIDAR for detecting surface pressure was introduced.
whereas Section 3 evaluates the performance of a differential absorption LIDAR model,
Finally, Section 4 presents the summary.

#### 87 2 Mechanism of Differential Absorption LIDAR to Detect Atmospheric Pressure

Differential absorption LIDAR selects two wavelengths in the A absorption band of oxygen (759–770nm). The laser beam with one wavelength value passes through the atmosphere twice; its absorption coefficient, although insensitive to changes in atmospheric temperature, is sensitive to variations in atmospheric pressure. This wavelength is referred to as the detection wavelength (online).Further, the absorption coefficient of another wavelength from the laser beam passing through the atmosphere twice is relatively smaller, and it is referred to as the reference wavelength (offline), with its value being close to the detection wavelength.





Let the atmospheric pressure at altitude  $R_0$ , where the LIDAR is located, be  $p(R_0)$ ; the atmospheric pressure at altitude R be p(R); and g(z) be the gravitational acceleration at altitude z. The difference in the atmospheric pressure between altitude  $R_0$  and R is equal to the weight of the air column between  $R_0$  and R per unit area, where the dry air molecular mass  $m_{dry}=28.9644$  g/mol and water vapor molecular mass  $m_{wy}=18$  g/mol.

100 Atmospheric quasi-static equation:

101 
$$dp = -n_{dry}(z) \cdot \left(m_{dry} + m_{wv}\chi_{wv}(z)\right) \cdot g(z)dz \tag{1}$$

102 Gas state equation:

103 
$$p(z) = n_{dry}(z) \cdot (1 + \chi_{wv}(z)) \cdot kT(z)$$
 (2)

104 
$$p(R) = p_{surface} \cdot exp^{-\int_0^R \frac{(m_{dry} + m_{WV}\chi_{WV}(z))g(z)}{kT(z)(1+\chi_{WV}(z))}dz}$$
(3)

105This integration is performed at an altitude z,  $n_{dry}(z)$  is the density of dry air molecules,  $\chi_{wv}(z)$ 106is the water vapor volume mixing ratio,  $p_{surface}$  is the surface pressure, and k is the Boltzmann107constant. Thus, by remote sensing the weight or mass per unit area of a vertical air column108between two altitudes, the difference in atmospheric pressure between these two altitudes can109be obtained.

110 Oxygen is among the most stable components in the atmosphere in terms of space and 111 time.  $n_{O_2}(z)$  is the number density of oxygen molecules at altitude *z*. The number of oxygen 112 molecules accounts for a fixed proportion of 20.948% of the number of dry air atmospheric 113 molecules. Further, the optical depth of the atmosphere between  $R_0$  and *R* is the integral of its 114 extinction coefficient with respect to the beam path, which can be expressed as

115 
$$OD(R_0, R) = \int_{R_0}^{R} \left[ \alpha_a(v, z) + \alpha_m(v, z) + n_{O_2}(z)\sigma(v, p(z), T(z)) \right] dz$$
(4)

116 where OD is the optical depth in Beer's theorem,  $\sigma$  is the absorption cross-section of the 117 oxygen molecule to the A-band  $\lambda$  wavelength, and  $\Delta \sigma$  is the difference  $\sigma(\lambda_{on}, p(z), T(z)) - \sigma(\lambda_{off}, z)$ 118 p(z),T(z)). Further,  $\alpha_a(\lambda, z)$  and  $\alpha_m(\lambda, z)$  are the aerosol extinction coefficient and the extinction 119 coefficient of atmospheric molecules except for oxygen absorption, respectively, and  $n_{O_2}(z)\sigma(\lambda, p(z), T(z))$  is the oxygen absorption coefficient of the corresponding 120 121 wavelength. The difference in the single-pass optical depth compared to the dual-wavelength 122 between  $R_0$  and R is referred to as the differential optical depth  $dOD(R_0, R)$ . Although the 123 weight of the atmospheric column between  $R_0$  and R per unit area is unknown, the differential 124 optical depth can be expressed as

125 
$$dOD(R_0, R) = \int_{R_0}^{R} n_{O_2}(z) \big( \sigma(v_{on}, z) - \sigma(v_{off}, z) \big) dz$$
(5)

126 
$$n_{O_2}(z) = \frac{0.20948p(z)}{kT(z) \cdot (1+\chi(z))}$$
(6)

127 where  $N_{s,off}(R)$  represents the online/offline dual-wavelength echo pulse energy 128 (number of photons) received by the LIDAR, which is expressed using the LIDAR equations 129 as follows:

130 
$$N_{s,on}(R) = \frac{c}{2} \frac{A_r}{R^2} \frac{\rho}{\pi} E_{on} \eta_r \eta_d \times exp[-20D(R_0, R)]$$
(7)

131 
$$N_{s,off}(R) = \frac{c}{2} \frac{A_r}{R^2} \frac{\rho}{\pi} E_{off} \eta_r \eta_d \times exp[-20D(R_0, R)]$$
(8)

132 Where  $E_{on}/E_{off}$  is the energy of a single shot emitted laser for both online/offline. Further,  $\eta_r$  is 133 the receiving efficiency of light beam,  $\eta_d$  is the quantum efficiency of the detector, and  $A_r$  is 134 the effective receiving area of the telescope. In the space-to-earth observation, IPDA, receives 135 return each from hard torget on the ground and a represente the reflectivity of ground targets

return echo from hard targets on the ground, and  $\rho$  represents the reflectivity of ground targets.

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136 The beam of dual-wavelength has the same path, receiving/sending time, footprint, and 137 random process in the atmosphere. Further, except for  $\sigma(\lambda, p(z), T(z))$ , all other parameters are 138 considered to be similar (but not equal). Dividing Eq. (7) by Eq. (8), the differential optical 139 depth can be calculated by measuring the energy of the pulse emitted and the energy of 140 received return echo by the LIDAR as follows:

141 
$$dOD(R_0, R) = -\frac{1}{2} ln \left\{ \left[ \frac{N_{on}(R)}{N_{off}(R)} \right] \left( \frac{E_{off}}{E_{on}} \right) \right\} + C$$
(9)

142 
$$C = \int_{R_0}^{R} \left[ \alpha_a(v_{on}, z) - \alpha_a(v_{off}, z) \right] dz + \int_{R_0}^{R} \left[ \alpha_m(v_{on}, z) - \alpha_m(v_{off}, z) \right] dz$$
(10)

143 where *C* represents a systematic error between the  $\frac{1}{2}ln\left(\frac{N_{off}(R)}{N_{on}(R)}\frac{E_{on}}{E_{off}}\right)$  value calculated from

144 the LIDAR data and the differential optical depth. Thus, laser shots of these two wavelengths 145 are simultaneously emitted and the reflections from the surface/cloud tops are received. 146 However, owing to the difference in oxygen absorption, the atmospheric transmittance of the two wavelengths is different. The logarithm of the ratio of  $\frac{N_{off}(R)}{N_{on}(R)} \frac{E_{on}}{E_{off}}$  can be used to obtain 147 148 the atmospheric differential optical depth from the satellite to the surface/cloud top. IPDA 149 launches several laser pulses from the space platform to the ground, and it detects the surface 150 pressure, with point  $R_0$  representing the satellite location. Further, there is almost no air 151 pressure  $p(R_0)=0.0$ , and p(R) represents the surface pressure  $p_{surface}$ .

152 In the path of the laser beam, only the section from the altitude of 71km to the ground has 153 a significant effect on the optical depth, whereas the effect of atmosphere above 71km can be 154 ignored. Further, the gravitational acceleration g(z) can be regarded as a constant 9.80616 155  $N/m^2$  at atmospheric altitude below 71 km.

156 On transforming the elevation z coordinates in Eq. (1) into atmospheric pressure p157 coordinates, the following is obtained

$$n_{dry}(z)dz = \frac{dp}{(m_{dry} + m_{wv}\chi_{wv}(p))g(p)}$$
(11)

159 Thus, the absorption cross-section  $\sigma(\lambda, p(z), T(z))$  is related to atmospheric temperature and

160 pressure, and thus it can be rewritten as  $\sigma(\lambda, p, T(p))$  in pressure p coordinates. Combining Eq.

161 (11), we can transform Eq. (5) from the elevation z coordinate to the pressure p coordinate.

162 The differential optical depth *dOD* associated with pressure *p* coordinates is expressed by

163 
$$dOD(p_{ground}, p_{top}) = 0.20948 \int_{p_{top}}^{p_{ground}} \frac{\Delta\sigma(v, p, T(p))}{(m_{dry} + m_{wv}\chi_{wv}(p))g(p)} dp$$
(12)

164 Here we assume that the pressure at the top of the atmosphere is  $p_{top}=0.0$ , and the atmospheric 165 pressure at the surface (or cloud top)  $p_{ground}=p_{surface}$ .

166 
$$dOD(p_{surface}) = \frac{0.20948}{g} \int_0^{p_{surface}} \frac{\sigma(v_{on}, p, T(p)) - \sigma(v_{off}, p, T(p))}{m_{dry} + m_{wv} \chi_{wv}(p)} dp$$
(13)

167 Equation (13) establishes the implicit expression of the differential optical depth of the entire 168 aerosphere with respect to the surface pressure  $p_{surface}$ . Theoretically, the true value of the 169 differential optical depth is the state of the atmosphere and is not related to the LIDAR 170 parameters. Further, it is independent of the measurement method. However, the 171 measurement error of the differential optical depth is closely related to the LIDAR parameters. 172 In the pressure *p* coordinate, the differential optical depth *dOD* ( $p_{surface}$ ) is expressed through 173 the integral Eq. (14) as follows:

174 
$$dOD(p_{surface}) = \int_0^{p_{surface}} \frac{\sigma(v_{on}, p, T(p)) - \sigma(v_{off}, p, T(p))}{2.251667 \times 10^{-24} \times (1 + 0.6214 \chi_{wv}(p))} dp$$
(14)





175 On differentiating both sides of Eq. (13) with respect to  $p_{surface}$  and considering the derivative 176 function of dOD ( $p_{surface}$ ) with respect to  $p_{surface}$ , we obtain

177 
$$\frac{\partial (doD(p_{surface}))}{\partial p_{surface}} = \frac{1}{46.8119} \times \frac{\sigma(v_{on}, p_{surface}, T(p_{surface})) - \sigma(v_{off}, p_{surface}, T(p_{surface}))}{m_{dry} + m_{wv}\chi_{wv}(p_{surface})} (15)$$

Subsequently, the relationship between the errors of the surface pressure and the differentialoptical depth of the entire atmosphere is obtained as

$$180 \qquad \delta p_{surface} = \frac{46.8199 \times [m_{dry} + m_{wv}\chi_{wv}(p_{surface})]}{\sigma(v_{on}, p_{surface}, T(p_{surface})) - \sigma(v_{off}, p_{surface}, T(p_{surface}))} \delta[dOD(p_{surface})] \tag{16}$$

181 Assuming that the vertical profile of atmospheric temperature T(R) and the vertical profile of 182 water vapor mixing ratio  $\chi_{\mu\nu}(R)$  are known from data obtained from other sensors or weather 183 models, the surface pressure can be inversed from the differential optical depth of the entire 184 atmosphere. The steps are shown in Fig. 1.

185 a. The differential optical depth measurement value  $(dOD)_m$  of the atmosphere from the 186 echo signal  $N_s$  and emission energy E of the differential absorption LIDAR is calculated.

187 b. Utilizing the atmospheric temperature profile T(R) coupled with the pressure profile and 188 the surface pressure in the standard atmosphere mode as the initial value of the 189 atmospheric pressure profile  $p_1(R)$  and the initial value of the surface pressure  $p_{surface,1}$ , 190 respectively, and using the oxygen HITRAN database, the initial value of the absorption 191 coefficient profile of the entire atmosphere is calculated. Thereafter, the initial value of the 192 differential optical depth  $(dOD)_{c,1}$  of the entire atmosphere is calculated.

193 c. If the differential optical depth  $(dOD)_{c,i}$  of the entire atmosphere is numerically 194 calculated in *i*-th cycle and  $(dOD)_{c,i}$  is not equal to the differential optical depth  $(dOD)_m$ 195 measured by the LIDAR, then the surface pressure  $p_{surface,i}$  calculated using the numerical 196 value is not equal to the true value  $p_{surface}$  of the pressure at the footprint, and thus, $(dOD)_m$ 197 is subtracted from $(dOD)_{c,i}$ .

198 d. The surface pressure varies with the differential optical depth. In the *i*-th cycle, the 199 difference between  $(dOD)_{c,i}$  and  $(dOD)_m$  is multiplied by a coefficient 200  $\frac{46.8199 \times [m_{dry} + m_{wv}\chi_{wv}(surface,i)]}{\sqrt{(1-1)^2}}$  in Eq. (16) as the compensation amount

200  $\frac{1}{\sigma(v_{on}, p_{surface,i}, T_{surface,i}) - \sigma(v_{off}, p_{surface,i}, T_{surface,i})}$ in Eq. (16) as the compensation amount 201 and added to the calculated value of the surface pressure  $p_{surface,i}$ . Consequently, the 202 resulting sum is used as the new surface pressure  $p_{surface,i+1}$ ;  $p_{surface,i+1} = p_{surface,i} + 1$ 

203  $\frac{46.8199 \times [m_{dry} + m_{wv\chi_{wv}}(surface,i)]}{\sigma(v_{on}, p_{surface,i}, r_{surface,i}) - \sigma(v_{off}, p_{surface,i}, r_{surface,i})} (dOD_{c,i} - dOD_m).$ 

204 e. Subsequently, with atmospheric temperature profile T(R) and water vapor mixing ratio 205  $\chi_{wv}(R)$  provided by other sensors or numerical weather models, coupled with the surface 206 pressure result  $p_{surface,i}$  obtained in the *i*+1-th cycle, the atmospheric pressure profile  $p_{i+1}(R)$ 207 is calculated. $p_{i+1}(R) = p_{currface,i} \cdot exp^{-\int_0^R \frac{(m_{dry} + m_{WV}\chi_{WV}(z))g(z)}{kT(z)(1+\chi_{WV}(z))}dz}$ .

07 is calculated, 
$$p_{i+1}(R) = p_{surface,i} \cdot exp^{-50} \quad kT(z)(1+\chi_{WV}(z))$$

208 f. Further, with the atmospheric temperature profile T(R), profile for water vapor mixing 209 ratio  $\chi_{wv}(R)$ , and the atmospheric pressure profile  $p_{i+1}(R)$ , based on the HITRAN database, 210 differential optical depth  $(dOD)_{c,i+1}$  calculations are repeated.

211 g. Repeat steps c–f. In the case of the above iterative process, with increase in *i*, the 212 difference between  $(dOD)_{c,i}$  and  $(dOD)_m$  decreases till *i=M*,  $p_{surface, M+1} - p_{surface,M}$  is 213 comparable to the error. If that happens, the iterative loop stops. Herein, the output surface 214 pressure  $p_{surface,M}$  calculation result is considered to be sufficiently close to the true value 215  $p_{surface}$ .





- 216 The above calculation steps also suggest that the parameters related to the temperature,
- 217 pressure, and humidity of the atmosphere should be detected synchronously in the future, as 218
  - input conditions for each other, and simultaneously iterated.  $p_1(R), T(R)$ US atmosphere model calculated (dOD)<sub>c,</sub> and psurphace.  $\int_{0}^{7000} \frac{0.20948 p_{i+1}(z)}{kT(z)(1+\chi_{wv}(z))} \Big(\sigma(v_{ost}, p_{i+1}(z), T(z)) - \sigma(v_{off}, p_{i+1}(z), T(z)) \Big) dz$ (dOD)  $\Delta(dOD)_i =$ Lidar signal  $(dOD)_{c,i}$ - $(dOD)_{n}$ Measure (dOD),  $\frac{46.8199 \times \left[m_{dry} + m_{wv} \chi_{wv}(p_{surface,i})\right]}{\sigma(v_{on}, p_{surface,i}, T(p_{surface,i})) - \sigma(v_{off}, p_{surface,i}, T(p_{surface,i}))}$  $\Delta(dOD)$ emperatu profile Temperature T(r), WaterProfile T(z), water vapor  $\int_{0}^{z} \frac{(m_{dry} + m_{wv}\chi_{wv}(r))g}{kT(r)(1+\chi_{wv}(r))} dr$ vapor mixing mixing ratio profile  $X_{wv}(z)$  $p_{i+1}(z) = p_{surface,i+1}e$ ratio profile From other sensor  $\chi_{wv}(r), from$ other sensor

219 220

#### 221 222 Figure 1: Iterative calculation process of the atmospheric pressure on the surface of the

## differential optical depth measured by the differential absorption LIDAR.

#### 223 3 Performance evaluation of an integrated path differential absorption LIDAR model

#### 224 3.1 A-band absorption spectrum of Oxygen

225 The absorption line of oxygen molecules is broadened in the atmosphere via collision and 226 Doppler broadening. They are expressed via the famous Lorentz and Gauss line shapes, 227 respectively. Below 15km in the atmosphere, collision broadening is dominant, with "n" 228 representing the sensitivity factor of collision broadening with respect to air temperature, that 229 is, the average value of its own broadening and nitrogen broadening sensitivity factors. We 230 consider n=0.73-0.59 from HITRAN database, normal pressure p0=1013.25hPa, normal 231 temperature  $T_0$ =296K,  $\gamma_0$  is the pressure broadening under normal temperature and normal 232 pressure,  $S_0$  is the intensity of the absorption line at room temperature and pressure,  $\sigma_0$  is the 233 peak absorption cross section of the absorption line at room temperature and pressure, c is the 234 speed of light, h is the Planck constant, m is the molecular mass of oxygen, and  $v_0$ (cm<sup>-1</sup>) 235 represents the position of the center wave number (light frequency) of the absorption line. 236 Further, E'' is the energy of the low-energy state of the electron. Moreover, in the application 237 of differential absorption LIDAR, the absorption line shape of the oxygen molecule can be 238 represented using the Voigt line shape, which is a form of the convolution Gauss line shape 239 with Lorentz line shape. The arbitrary real number t is the variable of the Voigt linear integral. The absorption cross-section  $\sigma(v)$  at the light wave number v is written as  $\sigma(v) = \sigma_0 \frac{y}{\pi} \int_{-\infty}^{\infty} \frac{exp(-t^2)}{y^2 + (x-t)^2} dt$ , where  $x = \left(\frac{v-v_0}{v_0}\right) \left(\frac{m}{2kT}\right)^{0.5} c$  and  $y = v_0 \gamma_0 \left(\frac{p}{p_0}\right) \left(\frac{T_0}{T}\right)^n \left(\frac{m}{2kT}\right)^{0.5} c$ , and  $\sigma_0 = \frac{S_0 c}{v_0} \left(\frac{2\pi kT}{m}\right)^{0.5} \left(\frac{T_0}{T}\right)^{1.5} exp\left[\frac{E^r}{k}\left(\frac{1}{T_0} - \frac{1}{T}\right)\right]$ . The wavelength in the trough between the oxygen 240 241 242 243 absorption line P13Q12 and P13P13, between the oxygen absorption line P15P15 and

244 P15O14, and even absorption lines P17O16 and P17P17 can be selected as the detection





245 wavelength. Table 1 lists certain parameters of the six absorption lines: for example, the 246 linear function  $\sigma_q(v-v_{01})$  of the absorption cross-section of the oxygen absorption line P13Q12 247 with respect to the wave number v, and the line function  $\sigma_p(v-v_{02})$  of the absorption cross 248 section of the P13P13 with respect to the wave number v. Further, the wavelength  $\lambda_{on}$ 249 (wavenumber  $v_{on}$ ) we selected is located at the minimum of the absorption cross-section 250 between the two spectral lines, that is, its absorption cross-section is the superposition of the 251 values of the extension lines of two adjacent Voigt linear functions at von. Moreover, its 252 absorption cross-section  $\sigma_{on}(v) = \sigma_p(v_{on}) + \sigma_q(v_{on})$ —the wings of the two Voigt lineshape 253 functions-is the manifestation of their pressure expansion.

	T in a contant	Tetereiter	Low	Half Width	s	Pressure- Tempo	
Assignme	Line center	Intensity	energy	$\gamma_0$	γ <sub>0</sub> sh		dependence
nt	$v_0$	$S_0$	E''	$\gamma_{\rm air}$	$\gamma_{self}$	Average( $\delta$ )	n
	cm <sup>-1</sup>	cm mole <sup>-1</sup>	cm <sup>-1</sup>	cm <sup>-1</sup> /atm	cm <sup>-1</sup> /atm	cm <sup>-1</sup> /atm	_ //
P13Q12	13078.2275	5.61×10 <sup>-24</sup>	260.6824	0.0466 (0.6)	0.0461 (1.1)	-0.0061	0.73
P13P13	13076.3273	6.13×10 <sup>-24</sup>	262.5827	0.0467 (0.8)	0.0460 (1.1)	-0.0068	0.73
P15Q14	13069.9619	4.33×10 <sup>-24</sup>	343.9694	0.0457 (1.2)	0.0449 (1.6)	-0.0051	0.73
P15P15	13068.0818	4.68×10 <sup>-24</sup>	345.8495	0.0455 (1.2)	0.0452 (1.6)	-0.0064	0.73
P17Q16	13061.3273	3.09×10 <sup>-24</sup>	438.7010	0.044	0.045	-0.00898	0.73
P17P17	13059.4665	3.31×10 <sup>-24</sup>	440.5618	0.0452	0.045	-0.00902	0.59

Table 1 Parameters of the three groups of absorption lines of Oxygen A(296K) (Brown and Plymate, 2014)



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262 Within the A absorption band of oxygen (759-770nm), the spectral transmittances in the 263 vicinity of 760 and 765nm were relatively insensitive to temperature, this band is the low 264 interference of water vapor and carbon dioxide molecules. Further, the atmospheric 265 transmittance at 760nm is lower than the atmospheric transmittance at 765nm, and when 266 ground-based LIDAR (RR-DIAL) detects tropospheric backscattering owing to the round-trip 267 optical path being shorter, two adjacent lines near 760nm can be selected. In addition, the 268 plots of absorption spectra shown in Figure 2, the Oxygen absorption features with a number 269 of smaller and sharper absorption spikes, it contains isotopologues of Oxygen molecules, 270 showing some subtle differences, the wavelength in the middle of the trough area between 271 lines is more suitable as the detection wavelength online and the reference wavelength offline, 272 (Korb et al., 1983,1989; Schwemmer, et al., 1987). When IPDA shoots lasers from the 273 satellite and receives the echo from the ground surface, the laser beam that passes through the 274 entire atmosphere twice results in the path being longer. Thus, 765nm is relatively more 275 suitable for remote sensing of surface pressure from satellites(Riris et al., 2017).







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Figure 3: Transmittance spectra of three intervals around 765nm  $\,$  and their ratio to 0.1K change in temperature







281 282

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Figure 4: Transmittance spectra around 760nm and their ratio to 0.1K change in temperature

284 The absorptive optical depth of oxygen  $dOD(p_{surface})$  with respect to the path 0–71km 285 corresponds to the optical transmittance  $e^{-2dOD}$  of this path with respect to the *v* wavenumber. 286 Figure 3 shows the transmittance spectra of three intervals around 765nm and their sensitivity 287 to temperature changes of +0.1K.Similarly, Figure 4 shows the transmittance spectra of 288 around 760nm and their sensitivity to temperature changes of +0.1K.

289 290 291

# Table 2 differential optical depth and differential absorption cross section of 9 pairs of wavelengths in standard atmospheric mode

Wave	length(nm)	$\int_0^{71} (\alpha_m + \alpha_a) dz$	$\int_0^{71} (n_{0_2}\sigma) dz$	<i>OD</i> (0,71km )	$\sigma_{O_2}$ (cm <sup>2</sup> )	<i>dOD</i> (0,71k m)	$\Delta\sigma_{O_2} (\mathrm{cm}^2)$
on	764.6840	0.1852	0.493	0.678	2.08×10 <sup>-25</sup>	0.428	1.80×10 <sup>-25</sup>
off	764.9097	0.1851	0.0653	0.251	2.80×10 <sup>-26</sup>		
on	765.1600	0.1851	0.389	0.574	1.74×10 <sup>-25</sup>	0 325	1.46×10 <sup>-25</sup>
off	764.9707	0.1851	0.0638	0.249	2.77×10 <sup>-26</sup>	0.525	1.10/10
on	765.1736	0.1849	0.373	0.558	1.67×10 <sup>-25</sup>	0.328	1.47×10 <sup>-25</sup>
off	765.3883	0.1849	0.0448	0.230	2.01×10 <sup>-26</sup>		





$9.25 \times 10^{-26}$	0 192	1.10×10 <sup>-25</sup>	0.416	0.231	0.1848	765.6735	on
2 9.23 ~10	0.192	1.78×10 <sup>-26</sup>	0.224	0.0391	0.1849	765.4637	off
$3 2.49 \times 10^{-25}$	0 493	$2.60  imes 10^{-25}$	0.702	0.515	0.1872	759.8042	on
2.17/10		$1.46 \times 10^{-26}$	0.209	0.0216	0.1873	759.4629	off
1 1 55×10 <sup>-25</sup>	0 321	$1.66 \times 10^{-25}$	0.530	0.343	0.1871	759.8969	on
	0.021	$1.46 \times 10^{-26}$	0.209	0.0216	0.1873	759.4629	off
4 1 67 $\times 10^{-25}$	0 364	$1.77 \times 10^{-25}$	0.573	0.385	0.1871	760.0209	on
1		1.46×10 <sup>-26</sup>	0.209	0.0216	0.1873	759.4629	off
4 2.12 $\times$ 10 <sup>-25</sup>	0 484	$2.22 \times 10^{-25}$	0.693	0.506	0.1870	760.1674	on
		$1.46 \times 10^{-26}$	0.209	0.0216	0.1873	759.4629	off
4 2.36 $\times 10^{-25}$	0 554	$2.46 \times 10^{-25}$	0.763	0.576	0.1870	760.3133	on
. 2.36 × 10	0.554	1.46 × 10 <sup>-26</sup>	0.209	0.0216	0.1873	759.4629	off

#### 292

293 Equation (16) clearly indicates that in various factors that result in  $\delta[dOD(p_{surface})]$ , the error 294 of differential optical depth conditionally causes conditionally causes the error  $\delta p_{surface}$  of the 295 surface pressure. Additionally, the detection wavelength absorption cross-section difference 296  $\Delta\sigma(p_{surface})$  near the ground is inversely proportional to the surface pressure error. Evidently, a 297 key factor affecting DIAL sensitivity is the online and offline wavelength positions. However, 298 for the candidate wavelengths marked in Fig. 2 used as detection wavelengths, each would 299 offer its own advantages and disadvantages, and consequently, comprehensive evaluation is 300 required.

#### 301 3.2 Differential absorption LIDAR system model

302 The research results reported by Coney, et al. (Munk et al., 2016-2019; Coney et al., 2021; 303 Thomas et al., 2016; Strotkamp et al., 2019)along with those reported by Wulfmeyer 304 and osenberg et al.(1996), refer to the ADM-Aeolus in orbit ALADIN system parameters of 305 the Aeolus mission (Lemmerz et al., 2017); the receiver is based on the GLAS-Mission-306 1064nm receiver, the orbit altitude is 400km, and diameter of the telescope is 1.5m. 307 Consequently, the model parameters of the differential absorption LIDAR has been proposed, 308 as shown in Table 3. The transmitter model parameters, with the exception of the pulse 309 energy of 100mJ, have been separately reported in different documents(Coney et al., 310 2021). However, these indicators have been achieved in the same laser, and thus, more 311 research is required.

312

Table 3 System parameters of differential absorption LIDAR

100mJ

Transmitter

Laser pulse energy





Laser pulse Width	88ns
Pulse repetition rate	100Hz
Laser Divergence Angle	90 $\mu$ rad for $\pm 3\sigma$
Spectral purity	99.99%
Pointing stability	< 10µrad
Receiver	
Telescope Diameter $(A_r)$	1.5m(SiC)
Receiver Field-of-view (full)	100µrad
Optical Filter Bandwidth (FW)	0.8nm(FWHM)
Fabry-Perot Elton (thickness=2mm)	$25pm(free \ spectral \ range \approx 0.1nm)$
Receiver Efficiency	50%
Combined filter width	0.025nm
Detector and amplifier	
Detector(Laser Components DG, Inc)	Si-APD(SAR1500/C30956/S3884-04)
APD Quantum Efficiency $(\eta_d)$	75%
Detector Diameter	Ф1.5mm
Electronic system bandwidth (BW)	3MHz
APD dark current $(I_d)$	1nA type
APD gain( <i>M</i> )	100
APD excess noise $factor(F)$	2.4
APD capacitance $(C_d)$	4pF
trans-impedance amplifier gain $(R_f)$	20kV/A
trans-impedance amplifier input current noise $(I_{nA})$	2.5pA/Hz <sup>1/2</sup>
trans-impedance amplifier input voltage noise $(V_{nA})$	$20 nV/Hz^{1/2}$
operate temperature	293 K
Platform and environment	
Orbit altitude and velocity	400 km, 7 km/s
Orbit type	Polar, sun synchronous, dawn/dusk
Along-track resolution	44 km
Simulation top altitude	71 km
Viewing geometry	Nadir
Atmosphere model	US standard atmosphere
Aerosol model	Median aerosol profile
(765nm)the surface albedo over ocean/land	0.1575/0.314
Pointing stability	< 50µrad
Spectroscopic data base	HITRAN 2012

313 As reported in reference (Lancaster et al., 2005), the equivalent Lambertian reflection 314 coefficient of the sub-satellite point laser on the ocean surface has an empirical relationship 315  $\rho_{eff} = \frac{\rho}{4(S^2)}$ , where the Fresnel reflection coefficient is  $\rho = 0.02$ , and  $\langle S^2 \rangle$  is the variance of 316 the wave steepness distribution. Further, Bufton et al.(1983) and Menzies et 317 al.(1998) individually adopted relationship as follows:

318





$$\left\langle S^{2} \right\rangle = \begin{cases} \left( \ln U_{10} + 1.2 \right) \times 10^{-2} \\ (0.85 \ln U_{10} - 1.45) \times 10^{-1} \\ U_{10} \le 7.0 \\ m/s \\ U_{10} > 7.0 \\ m/s \end{cases}$$
(17)

319 where  $U_{10}$  is the wind speed of segment 10m above the ocean surface. The general ocean

- 320 surface wind speed is taken as 8m/s, whereas  $\rho_{eff} = 0.1575$  and  $\rho_{eff}/\pi = 0.025 \text{ sr}^{-1}$ . In addition, 321 the reflectivity of terrestrial lasers is generally 0.314.
- 322 **3.3** Performance evaluation of A-band DIAL system

### 323 3.3.1 Random error of differential optical depth caused by noise

**324** The number of received return echo photons  $N_{s,on}$  and  $N_{s,off}$  is obtained using the LIDAR Eq. **325** (7) and Eq.(8). Equations(18)–(25) are commonly used for the on and off channels.

$$326 \qquad N_s(R_0, R) = \frac{\lambda \cdot E}{h \cdot c} \cdot A_r \cdot \eta_d \cdot \eta_r \cdot \left(\frac{\rho}{\pi}\right) \cdot \frac{exp[-20D(R_0, R)]}{(R_0 - R)^2} \tag{18}$$

327 Here the working and reference wavelengths  $\lambda_{on}$  and  $\lambda_{off}$ , the Planck constant is h,  $\rho$  is the 328 surface reflectivity, and c is the speed of light. Further, the effective pulse width  $\tau_w$  of the 329 echo signal is a combination of the emitted laser pulse width  $\tau_L$ , and the detection electronic 330 system bandwidth *BW* (unit Hz), effective target altitude within the laser footprint  $\Delta H$ , *R*-331  $R_0$ =400km, $\Delta H$ =2 m, can be expressed as (Ehret, et al., 2008):

332 
$$\tau_w = \sqrt{\tau_L^2 + \left(\frac{1}{3} \cdot BW\right)^2 + \left(\frac{2 \cdot \Delta H}{c}\right)^2}$$
(19)

333The background signal  $N_{BG}$  (photoelectrons), assuming a Lambertian surface and zenith sun,334is calculated as

335 
$$N_{BG}(\lambda) = \frac{\lambda \cdot S_{BG}}{h \cdot c} \tau_{W} \cdot A_{r} \cdot \eta_{d} \cdot \eta_{r} \cdot \left(\frac{\rho}{\pi}\right) \cdot \left(\frac{FOV}{2}\right)^{2} \pi \cdot FW. exp[-20D(R_{0}, R)]$$
(20)

where  $S_{BG}$  is the exo-atmospheric solar irradiance value (1.221W m<sup>-2</sup> nm<sup>-1</sup>)(ASTM 336 337 international, United States, 2019)at 765nm, FW is the bandwidth of the optical filter 338  $(0.025 \text{ nm} \times 4)$  and the field of view (FOV) (unit rad) of the FOV receiving telescope. The 339 bandwidth of the Fabry-Perot etalon, free spectral range, and width of the narrowband filler 340 were 25pm,0.1nm, and 0.8nm, respectively. There are 8 longitudinal modes of Fabry-Perot 341 etalon that can pass through. However, the transmittance of each longitudinal mode is 342 different, and thus, the equivalent solar window width is  $25 \text{pm} \times 4 = 0.1 \text{nm}$ . Further, the 343 backscattering coefficient ( $\rho/\pi$ ) on the surface of land such as ocean and vegetation during the 344 daytime (Thomas et al., 2016), and  $\rho$  were calculated as 0.1575 and 0.314, respectively.

345 Here the *q* electrons charge is  $1.6 \times 10^{-19}$  C, M is the gain of silicon avalanche diode (APD). 346 The total noise associated with the detection signal is divided into fixed circuit noise and 347 signal-dependent shot noise. The total circuit noise current spectral density (unit A/Hz<sup>1/2</sup>)  $I_n$ , 348 can be expressed as (Refaat, et al., 2013)

349 
$$I_n = \sqrt{2 \cdot q \cdot I_d \cdot M \cdot F + I_{nA}^2 + \frac{V_{nA}^2}{R_f^2} + \frac{4 \cdot k \cdot T}{R_f + \frac{(2 \cdot \pi \cdot V_{nA} \cdot C_d \cdot BW)^2}{3}}}$$
(21)

350 where  $I_d$  and F are the dark current and excess noise factors of the detector, respectively;  $I_{nA}$ 351 and  $V_{nA}$  are the preamplifier integrated input current and input voltage noise spectral density, 352 respectively;  $R_f$  is the feedback resistance of the preamplifier; and  $C_d$  is the equivalent input 353 capacitance of the amplifier and the detector. The circuit noise is often limited by the shot 354 noise of the dark current of the detector or the noise of the preamplifier. In this analysis, all 355 circuit noises refer to the detector input and the equivalent circuit noise-generated 356 photoelectrons, and  $N_{n,C}$  is calculated as





$$357 \qquad N_{n,C} = \frac{I_n \cdot \tau_W \cdot \sqrt{BW}}{q \cdot M} \tag{22}$$

358 Similarly, the equivalent shot noise-generated photoelectrons,  $N_{n,S}$ , are calculated as

$$359 \qquad N_{n,S} = \sqrt{2} \cdot N_S \cdot F \cdot \tau_W \cdot BW \tag{23}$$

**360** Further, the photoelectron  $N_{n,BG}$ , equivalent to the equivalent shot noise associated with the background radiation can be calculated as

$$362 \qquad N_{n,BG} = \sqrt{2 \cdot N_{BG} \cdot F \cdot \tau_w \cdot BW} \tag{24}$$

These noises are regarded as the equivalent photoelectron number generated in the detector
 (before the multiplication process), and are proportional to the actual detected photoelectron
 number. The total signal-to-noise ratio is expressed as follows(Ehret, *et al.*, 2008):

$$366 \qquad SNR_{on/off} = \frac{N_{s,on/off}}{\left|N_{n,C}^2 + N_n^2 S_{on/off} + N_{n,BG,on/off}^2\right|} \tag{25}$$

367 Where s is the number of echo signal pulses accumulated and averaged by the LIDAR. The 368 error  $\varepsilon_R$  caused by the noise of the LIDAR receiving a single echo is a random error. 369 Moreover, it is necessary to calibrate the LIDAR echo signal detection channel and the laser 370 emission pulse energy monitoring channel to remove nonlinear and nonzero biased 371 background voltage. Further, the calibration error and AD conversion error comprise the 372 systematic error. In addition, the error  $\varepsilon_A$  caused by the uncertainty of atmospheric 373 environment (atmospheric temperature profile, atmospheric water vapor mixing ratio profile), 374 and the associated error  $\varepsilon_T$  of the laser emission characteristics (jitter of the center wavelength 375 of the emitted beam, the emission spectrum width, and the purity of the emission spectrum) 376 are all systematic errors. The total error of the differential optical depth can be expressed as

377 
$$\delta[dOD] = \frac{\varepsilon_R}{\sqrt{s}} + \sqrt{\varepsilon_A^2 + \varepsilon_T^2}$$
(26)

**378** Equation(9) indicates that the random noise of the echo signals  $N_{on}(R)$  and  $N_{off}(R)$  and the **379** random measurement error of the pulse energies  $E_{on}$  and  $E_{off}$  result in the random error of the **380** differential optical depth  $\varepsilon_R = \delta[dOD(p_{surface})]_R$  as follows:

381 
$$\varepsilon_R = \delta \left[ dOD(p_{surface}) \right]_R = \frac{1}{2} \sqrt{ \left( \frac{\delta N_{s,on}(R)}{N_{s,on}(R)} \right)^2 + \left( \frac{\delta N_{s,off}(R)}{N_{s,off}(R)} \right)^2 + \left( \frac{\Delta E_{on}}{E_{on}} \right)^2 + \left( \frac{\Delta E_{off}}{E_{off}} \right)^2 (27)}$$

**382** The signal-to-noise ratio of LIDAR can be calculated using Eq.(18)–(25). Simultaneously, it **383** is considered that the measurement error of pulse energy  $\Delta E_{onf}/E_{on} \approx \Delta E_{off}/E_{off}$  is very small **384** and can thus be ignored. The random error of LIDAR echo (noise) measurement is calculated **385** as

$$\epsilon_R = \frac{1}{2} \sqrt{SNR_{on}^{-2} + SNR_{off}^{-2}}$$
(28)

387 When the laser irradiates the ocean surface (for example, the average wind speed is 8m/s), 388 0.1575 represents median for the ocean surface reflectivity(Ehret, et al., 2008), and the 389 random error  $\varepsilon_R$  of the differential optical depth is calculated considering the single pulse echo; 390 with a time resolution of at least 6.25 s ,the distance resolution along the track of 44km and S 391 = 625 laser pulse echoes are taken as a group for cumulative average, the random error of the 392 atmospheric differential optical depth above the ocean surface is  $\frac{\varepsilon_R}{\sqrt{625}}$ .

393 The ocean surface possesses low laser reflectivity and weak echoes. The averaging 394 method employed is as follows: first add up 625 echoes; thereafter subtract *B* and normalize,





- where *B* is the level background baseline of the LIDAR output; and finally Eq. (25) provides the differential optical depth.
- 397  $E_{on} = \sum_{i=1}^{625} E_{i,on}$  (29-1)
- 398  $E_{off} = \sum_{i=1}^{625} E_{i,off}$  (29-2)
- 399  $N_{s,on} = \sum_{i=1}^{625} N_{i,s,on}$  (29-3)
- 400  $N_{s,off} = \sum_{i=1}^{625} N_{i,s,off}$  (29-4)

401 
$$dOD = OD_{on} - OD_{off} = -\frac{1}{2}ln\left(\frac{N_{s,on}-B}{E_{on}}\right) + \frac{1}{2}ln\left(\frac{N_{s,off}-B}{E_{off}}\right)$$
 (30)

- 402
- 403

#### Table 4 Error from noise

	SNR		Single sho	t Noise Error	average Nois	e Error
Wavelen gth(nm)	ocean	land	ocean	land	Ocean/25	Land/12
	0.1575	0.314	0.1575	0.314	0.1575	0.314
764.6840	97.74	139.68	0.0061	0 0043	2 44×10 <sup>-4</sup>	3 55×10 <sup>-4</sup>
764.9097	152.1	215.8				
765.1600	109.0	155.5	0.0056	0.0040	$2.24 \times 10^{-4}$	2 20×10 <sup>-4</sup>
764.9707	152.3	216.2	0.0030	0.0040	2.24×10	5.50×10
765.1736	110.9	158.0	0.0055	0.0039	2 20×10 <sup>-4</sup>	3 24×10 <sup>-4</sup>
765.3883	155.4	220.5			2120/110	
765.6735	128.4	182.6	0.0050	0.0035	2.00×10 <sup>-4</sup>	2.06×10-4
765.4637	156.3	221.8	0.0050	0.0035	2.00×10	2.90×10
759.8042	95.06	135.9	0.00614	0.00420	$2.46 \times 10^{-4}$	$2.59 \times 10^{-4}$
759.4629	158.1	224.3	0.00014	0.00430	2.10 \ 10	5.50 ~ 10
759.8969	113.7	161.9	0.00542	0.00291	$2.17 \times 10^{-4}$	$2.17 \times 10^{-4}$
759.4629	158.1	224.3	0.00342	0.00381	2.17×10	5.17 × 10
760.0209	108.8	155.1	0.00559	0.00202	$2.22 \times 10^{-4}$	$2.27 \times 10^{-4}$
759.4629	158.1	224.3	0.00558	0.00392	2.25 × 10	5.27 × 10
760.1674	95.98	137.2	0.00000	0.00427	2 44 10-4	2.56 10-4
759.4629	158.1	224.3	0.00609	0.00427	2.44 × 10 *	3.36 × 10 °





760.3133	89.15	127.7	0 00644	0.00451	$2.58 \times 10^{-4}$	3 76 × 10 <sup>-4</sup>
759.4629	158.1	224.3	0.00011	0.00451	2.50 × 10	5.70 × 10

404

405 It is believed that the reflectance value of 0.314 is typical and representative of the surface 406 reflectance for most features on land (vegetation, sand, and soil). When the laser irradiates the 407 land, the noise of the single pulse echo causes a random error in the optical depth. The time 408 resolution of 6.25 s and resolution along track of 44 km are maintained. First, the very high 409 footprint is highlighted, and the very low footprint points is removed. Subsequently, the 410 average altitude of most of the remaining footprints is calculated. Considering this average 411 altitude, all the echo pulses whose footprint altitude and the average altitude are within 2 m as 412 a group are acquired, and the number of pulses obtained is no less than 144 pulses <u>rep</u> ther, 413 they are accumulated and averaged to decrease the random measurement err 414 differential optical depth.

415 The averaging method involves first subtracting the background baseline  $B_i$  of a single 416 echo, normalizing, and thereafter performing the cumulative average, where

417 
$$s \ge 144, \qquad \frac{N_{s,on/off}}{E_{on/off}} \approx \sum_{i=1}^{M} \frac{N_{i,s,on/off} - B_i}{E_{i,on/off}}$$
 (31)

418 
$$dOD = OD_{on} - OD_{off} = -\frac{1}{2}ln\left(\frac{N_{s,on}}{E_{on}}\right) + \frac{1}{2}ln\left(\frac{N_{s,off}}{E_{off}}\right)$$
(32)

419 When the laser irradiates the plain area, it is easy to confidently pick out the footprint altitude 420 of more than 144 shots from 625 pulses. However, if uneven terrain is encountered, there are 421 less than 144 echo pulses, difference between the footprint altitude and the average altitude is 422 within 2 m, and average of multiple laser pulse echoes becomes unreasonable. Moreover, if 423 greater than 144 pulses with similar footprints are still not found, this set of data is discarded 424 In conclusion, when laser irradiates the ocean surface, its single echo signal is relative 425 weak, whereas its footprint altitude is relatively consistent; thus, more pulse echoes can be 426 accumulated and averaged. Further, when the laser irradiates the land surface, the altitude 427 consistency of the landing footprint is poor and accumulated average echo pulse is less, 428 although the signal-to-noise ratio of the land single echo is relatively high.

#### 429

437

#### 430 3.3.2 Uncertainty of vertical distribution profile of atmospheric temperature

Within a certain time resolution (distance resolution), the uncertainty of the vertical profile of
the atmospheric temperature results in an absolute systematic error with respect to the
differential optical depth (Refaat, et al., 2013).

434 When the temperature change ±1K, Oxygen number density is  
435 
$$n_{O_2}(T \pm 1K) = \frac{0.20948p(z)}{k(T(z)\pm 1)\cdot(1+\chi(z))}$$
(33)

$$\Delta[dOD(0, surface)]_{\pm 1K} = \int_0^{1/2} n_{O_2}(T \pm 1K) \Delta\sigma(p(z), T(z) \pm 1) dz$$

$$436 \quad -\int_0^{71} n_{O_2}(T) \Delta \sigma \big( p(z), T(z) \big) dz \tag{34}$$

Table 5 Temperature sensitivity of differential optical depth in case of  $\pm 1$ K uncertainty

Regimentation $\Delta |dOD(p, T-1)|$  $\Delta |dOD(p, T+1)|$  $Max{\Delta}|dC$  $-1)|, \Delta |d$  $-1)|, \Delta |d$ -+1)|





764.6840/	0.00216	0.00215	0.00216		
764.9097	0.00216	0.00215	0.00216		
765.1600/	0.000020	0.000022	0.000033		
764.9707	0.000929	0.000933	0.000933		
765.1736/	0.00102	0.00102	0.00103		
765.3883	0.00102	0.00102	0.00102		
765.6735/	0.000139	0.000146	0.000146		
765.4637	0.000139	0.000140	0.000140		
759.8042/	0.00141	0.00120	0.00141		
759.4629	0.00141	0.00139	0.00141		
759.8969/	0.000172	0.000162	0.000173		
759.4629	0.000173	0.000102	0.000175		
760.0209/	0.000624	0.000621	0.000631		
759.4629	0.000624	0.000031	0.000051		
760.1674/	0.00170	0.00170	0.00170		
759.4629	0.00170	0.00170	0.00170		
760.3133/	0.00285	0.00284	0.00285		
759.4629	0.00285	0.00284	0.00283		

438

#### 439 **3.3.3** Error of differential optical depth $[dOD(0, p_{surface})]_{wv}$ caused uncertainty of the 440 mixture ratio of water vapor

441 The mixture ratio of near-ground water vapor in standard atmospheric mode is 1.247% higher 442 than  $\chi_{wv}$  ( $p_{surface}$ ).

443 The 20% uncertainty of profile for water vapor mixture ratio introduces uncertainty in 444 differential optical depth  $[dOD(0, p_{surface})]_{wv}$ .

$$\Delta [dOD(P_{surface})]_{\pm 20\% wv} \approx 0.20948 \int_{0}^{71km} \frac{p(z)}{kT(z)(1+(1\pm 20\%)\chi(z)))} (\sigma(\lambda_{on}, z) - \sigma(\lambda_{off}, z)) dz$$

$$445 - 0.20948 \int_{0}^{71km} \frac{p(z)}{kT(z)(1+\chi(z))} (\sigma(\lambda_{on}, z) - \sigma(\lambda_{off}, z)) dz \qquad (35)$$

446 Table 6 Error differential optical depth [dOD(0, psurface)]<sub>wv</sub> caused uncertainty of the mixture of water vapor

Wavelength(nm)

764.6840	$5.29 \times 10^{-4}$
764.9097	0.29 / 10

Differential optical depth error(20%)

764.9097	5.29 × 10
765.1600	4 15 × 10 <sup>-4</sup>
764.9707	4.15 × 10
765.1736	$4.18 \times 10^{-4}$
765,3883	4.10 × 10





447	765.6735	$2.52 \times 10^{-4}$
447	765.4637	2.55 × 10
448	759.8042	$6.71 \times 10^{-4}$
449	759.4629	0./1 ×10
450	759.8969	$4.27 \times 10^{-4}$
451	759.4629	4.27 ×10
152	760.0209	$4.71 \times 10^{-4}$
453	759.4629	4.71 × 10
454	760.1674	$6.11 \times 10^{-4}$
455	759.4629	0.11 × 10
456	760.3133	6 99 × 10 <sup>-4</sup>
457 458	759.4629	0.00 × 10

458 459

#### 460 3.3.4 Error of the differential optical depth caused the difference in the altitude of the 461 inner surface and between the land footprints.

462 The largest oxygen density is near the ground, and thus, differential optical depth is sensitive 463

to high uncertainty near ground;  $\Delta H=2m$ .

$$\begin{split} \Delta \big[ dOD \big( P_{surface} \big) \big]_{\Delta H} \\ &\approx \int_{0}^{71000} n_{O_2}(z) \big( \sigma(\lambda_{on}, z) - \sigma(\lambda_{off}, z) \big) dz \\ &- \int_{\pm 2}^{71000} n_{O_2}(z) \big( \sigma(\lambda_{on}, z) - \sigma(\lambda_{off}, z) \big) dz \end{split}$$

464 
$$\approx \int_0^{\pm 2} n_{O_2}(z) \big( \sigma(\lambda_{on}, z) - \sigma(\lambda_{off}, z) \big) dz$$
(36)

466

#### Table 7 Differential optical depth error caused by the 2 m altitude difference

Wavelength	Error [dOD]
764.6840	$0.4578 \times 10^{-4}$
764.9097	0.+578 × 10
765.1600	$0.3723 \times 10^{-4}$
764.9707	0.5725 × 10
765.1736	$0.3737 \times 10^{-4}$
765.3883	0.3737 × 10
765.6735	$0.2356 \times 10^{-4}$
765.4637	0.2550 × 10
759.8042	$0.139 \times 10^{-4}$
759.4629	0.157 × 10
759.8969	$0.0905 \times 10^{-4}$
759.4629	0.0903×10
760.0209	$0.102 \times 10^{-4}$
759.4629	0.102 ~ 10





167	760.1674	$0.126 \times 10^{-4}$
407	759.4629	0.130 × 10
468	760.3133	0.156 × 10 <sup>-4</sup>
469	759.4629	0.150 × 10

470

#### 471 3.3.5 Relative error in calibration for the echo and energy monitoring channels.

- 472 The absolute error in the differential optical depth is  $dOD \times 0.025\%$  (Ehret, et al., 2008),
- 473 which also belongs to the systematic error.
- 474 475

#### Table 8 Calibration error for echo detection channels and energy monitoring channels

Wavelength(nm)	<i>dOD</i> (0, 71km)	error of <i>dOD</i>	
764.6840	0.428	$1.07 \times 10^{-4}$	
764.9097			
765.1600	0.325	$0.81 \times 10^{-4}$	
764.9707	0.020		
765.1736	0.328	$0.82 \times 10^{-4}$	
765.3883	0.526	0.82 × 10	
765.6735	0.192	$0.48 \times 10^{-4}$	
765.4637	0.172	0.70 ^ 10	
759.8042	0.493	$1.23 \times 10^{-4}$	
759.4629	0.495	1.23 ~ 10	
759.8969	0.321	$0.803 \times 10^{-4}$	
759.4629	0.521	0.003 ×10	
760.0209	0 364	$0.910 \times 10^{-4}$	
759.4629	0.501		
760.1674	0.484	$1.21 \times 10^{-4}$	
759.4629			
760.3133	0.554	1.39 × 10 <sup>-4</sup>	
759.4629			

476

#### 477 3.3.6 Error in optical depth due to the wavelength dependence of aerosol scattering

478 In the standard atmosphere mode, Mie and Rayleigh scatterings of the 765nm or 760nm dual-479 wavelength are similar but not equal. The coefficient C in Eq. (10) expresses the systematic 480 error caused by the difference as follows:

481 
$$C = \int_{0}^{71 \text{km}} [\alpha_{a}(\lambda_{on}, z) + \alpha_{m}(\lambda_{on}, z)] dz - \int_{0}^{71 \text{km}} [\alpha_{a}(\lambda_{off}, z + \alpha_{m}(\lambda_{off}), z)] dz$$
(37)  
482   
483 Table 9 Optical depth error caused by the wavelength dependence of the aerosol scattering  
484





405	Waveleng	gth(nm)	С	
485	on	764.6840		
486	off	764.9097	- 0.90 × 10 <sup>-4</sup>	
487		765.1600		
488	on	/65.1600	$-0.76 \times 10^{-4}$	
489	off	764.9707		
400	on	765.1736	0.05 104	
490	off	765.3883	- 0.86 × 10 <sup>-4</sup>	
491	0.0	765 6735		
492		105.0755	$-0.84  imes 10^{-4}$	
493	off	765.4637		
101	on	759.8042	$1.30 \times 10^{-4}$	
494	off	759.4629	1.39 × 10	
495	on	759.8969		
496	off	759 4629	$1.77 \times 10^{-4}$	
497	011	139.4029		
498	on	760.0209	$2.28 \times 10^{-4}$	
499	off	759.4629		
500	on	760.1674		
501	off	759.4629	$-2.88 \times 10^{-4}$	
503		7(0.2122		
504	on	/60.3133	- 3.47 × 10 <sup>-4</sup>	
505	off	759.4629		
506				

507The errors in aerosol Mie scattering with the wavelength dependence error, spectral width508error, and spectral purity error, can be eliminated by correction. Wavelength dependence of509extinction coefficient of aerosol, 0.0 < k < 2.0, k is uncertain and varies with the particle size,510shape and concentration of aerosol, so it will bring systematic error of differential optical511depth.512

#### 513 3.3.7 Error in differential optical depth from the spectral purity of the on/off laser

The spectral purity  $\xi$  of the spaceborne IPDA LIDAR is 99.99% (Wulfmeyer and ösenberg et al.1996), which results in an increase in the on-channel echo and the absolute error of the optical depth. For a spectral purity of 100%, the relationship between the two on/off channel signals is considered to be  $N_{s,on}' = N_{s,off}' e^{-2dOD}$  and  $dOD = -\frac{1}{2}ln\left(\frac{N_{s,on}'}{N_{s,off}'}\right)$ . However, because the spectral purity is not 100%, but it only is  $\xi$ , the relationship between the two channel signals is approximately  $N_{s,on} = N_{s,off}[(1-\xi) + \xi e^{-2dOD}]$ ,  $ln\left(\frac{N_{s,on}}{N_{s,off}}\right) =$  $ln[(1-\xi) + \xi e^{-2dOD}]$ , and the spectral purity yield the following error in optical depth:  $\varepsilon_{\xi} = \frac{1}{2}ln\left(\frac{N_{s,on}}{N_{s,off}}\right) - \frac{1}{2}ln\left(\frac{N_{s,on}'}{N_{s,off}'}\right)$ 

521 
$$\approx dOD + \frac{1}{2}ln[1 - \xi(1 - e^{-2dOD})]$$





522

#### Table 10 Error in differential optical depth from spectral purity of 99.99%

Wavelength	<i>dOD</i> (0, 71km)	Error (spectral purity of 99.99%)		
764.6840	0.428	6.70 10-5		
764.9097	0.428	6.79 × 10		
765.1600	0.225	4.00105		
764.9707	0.323	4.00 × 10		
765.1736	0.000	4.44 105		
765.3883	0.328	$4.66 \times 10^{-5}$		
765.6735	0.100	a a c. 105		
765.4637	0.192	$2.36 \times 10^{-5}$		
759.8042	0.402	0.40 105		
759.4629	0.493	8.40 × 10 <sup>-5</sup>		
759.8969	0.000			
759.4629	0.322	4.51 ×10 <sup>5</sup>		
760.0209				
759.4629	0.364	$5.35 \times 10^{-3}$		
760.1674				
759.4629	0.484	8.16 × 10 <sup>-3</sup>		
760.3133				
759.4629	0.554	1.01 ×10 <sup>-4</sup>		

523

#### 524 **3.3.8** Error of differential optical depth caused jitter of *v* in central optical frequency

The laser source of the spaceborne IPDA has a jitter of  $\nu$  central optical frequency, whereas the online/offline emission laser spectrum has a central frequency jitter of 10MHz(Strotkamp et al., 2019). $\Delta \nu_{on} = \pm$  10MHz introduces uncertainty in the Oxygen molecule absorption crosssection  $\sigma$  ( $\nu_{on}$ ), resulting in a systematic error in the optical depth. However, for solid-state lasers, stabilizing the center wavelength within  $\pm$ 10MHz is quite easy compared to within  $\pm$ 1MHz. For example, if the center wavelength is offset by  $\pm$ 10MHz, the jitter of the emitted laser frequency that affects the swing of the optical depth can be expressed as

532

$$[dOD(0, surface)]_{10MHZ} = \int_{0}^{71km} \frac{0.20948p(z)}{kT(z)(1+\chi(z))} \Big(\sigma(v_{on} \pm 10MHZ, z) - \sigma(v_{off}, z)\Big) dz$$
  
533 
$$-\int_{0}^{71km} \frac{0.20948p(z)}{kT(z)(1+\chi(z))} \Big(\sigma(v_{on}, z) - \sigma(v_{off}, z)\Big)$$
(39)

It is evident from the curves of the two bands in Fig.5 that because the former is next to an absorption line 13069.062119cm<sup>-1</sup> of the oxygen isotope <sup>16</sup>O<sup>18</sup>O, the curvature at the former position protrudes, and the abscissa of the curve is the laser frequency (Wavelength).

537 Table 11 Jitter in the emission laser frequency v causes a 10MHz change in the differential optical depth





538

#### 539

540

λ(nm)	$dOD(v\pm 10\text{MHZ}, p)\text{-} dOD(v, p)$		Max{ $\left  \Delta(+10 \text{MHz}) \right , \left  \Delta(-$	
	Δ(+10MHz)	Δ(-10MHz)	$-10MHz)$ }	
764.6840	$6.18 \times 10^{-7}$	$9.62 \times 10^{-7}$	9.62 × 10 <sup>-7</sup>	
764.9097		,		
765.1600	$2.23 \times 10^{-5}$	$2.38 \times 10^{-5}$	2.38 ×10 <sup>-5</sup>	
764.9707	2.25 110	2.00 / 10		
765.1736	2 00 × 10 <sup>-6</sup>	$2.81 \times 10^{-6}$	2.81×10 <sup>-6</sup>	
765.3883	2.00 × 10	2.01 \ 10		
765.6735	1.04 × 10 <sup>-6</sup>	$8.53 \times 10^{-7}$	$1.04 \times 10^{-6}$	
765.4637	1.04 × 10	8.55 × 10	1.04 / 10	
759.8042	$4.28 \times 10^{-3}$	$2.52 \times 10^{-3}$	4.28 ×10 <sup>-3</sup>	
759.4629	4.20 × 10	2.52×10		
759.8969	$1.56 \times 10^{-3}$	$1.10 \times 10^{-3}$	$1.56 \times 10^{-3}$	
759.4629	- 1.50 × 10	1.17 × 10		
760.0209	$7.71 \times 10^{-4}$	$7.76 \times 10^{-4}$	7.76 ×10 <sup>-4</sup>	
759.4629	- 7.71 × 10	1.70×10		
760.1674	$6.84 \times 10^{-4}$	$1.60 \times 10^{-3}$	$1.60 \times 10^{-4}$	
759.4629	0.01/10	1.00 × 10	1.00 \ 10	
760.3133	$3.83 \times 10^{-4}$	$9.49 \times 10^{-4}$	$9.49 \times 10^{-4}$	
759.4629		2.42 / 10	2.12 \ 10	

541

According to the comprehensive analysis of the above differential optical depth errors 542 induced in many factors, the comprehensive evaluation index items of the wavelength to be 543 selected are shown in Figure 12 and Figure 13.

544

545

#### Table 12 Comprehensive of various errors at near 765nm

Wavelength		764.6840 /764.9097	765.1600 /764.9707	765.1736 /765.3883	765.6735 /765.4637
Random error	ocean	$2.44 \times 10^{-4}$	$2.24 \times 10^{-4}$	$2.20 \times 10^{-4}$	$2.00 \times 10^{-4}$
	land	$3.55 \times 10^{-4}$	3.30×10 <sup>-4</sup>	$3.24 \times 10^{-4}$	$2.96 \times 10^{-4}$
Temperature	1K	21.54 × 10 <sup>-4</sup>	$9.31 \times 10^{-4}$	$10.16 \times 10^{-4}$	$1.43 \times 10^{-4}$
Vapor mixing ratio	20%	5.29 × 10 <sup>-4</sup>	4.15 ×10 <sup>-4</sup>	4.18 × 10 <sup>-4</sup>	2.53×10 <sup>-4</sup>
Energy monito calibration	or channel	1.07 × 10 <sup>-4</sup>	0.813 ×10 <sup>-4</sup>	$0.820 \times 10^{-4}$	$0.480 \times 10^{-4}$
Echo channel ca	alibration	$1.07 \times 10^{-4}$	$0.813 \times 10^{-4}$	$0.820 \times 10^{-4}$	$0.480 \times 10^{-4}$





Elevation 2m error	$0.458 \times 10^{-4}$	$0.372\times\!10^{\text{-4}}$	$0.374\times 10^{\text{-4}}$	$0.236  imes 10^{-4}$
Aerosol Mie scattering	$0.903 \times 10^{-4}$	$0.756 \times 10^{-4}$	$0.857 \times 10^{-4}$	$0.837 \times 10^{-4}$
99.99% spectral purity	$0.679 \times 10^{-4}$	$0.460 \times 10^{-4}$	$0.466 \times 10^{-4}$	$0.236 \times 10^{-4}$
Frequency jitter(10MHZ)	9.62 × 10 <sup>-7</sup>	0.238 × 10 <sup>-4</sup>	$2.81 \times 10^{-6}$	$1.04 \times 10^{-6}$
Differential absorption cross section (m <sup>2</sup> )	$1.80 \times 10^{-29}$	$1.46  imes 10^{-29}$	$1.47 \times 10^{-29}$	$9.25 \times 10^{-30}$
Geometrically added	25.8 × 10 <sup>-4</sup>	$19.6 \times 10^{-4}$	14.3×10 <sup>-4</sup>	6.08 × 10 <sup>-4</sup>
Absolute error(hPa)	3.29	3.08	2.23	1.51
Relative error(%)	0.324	0.304	0.220	0.150

## 546

#### 547

#### Table 13 Comprehensive of various errors at near 760nm

Wayslanath	759.8042	759.8969	760.0209	760.1674	760.3133
wavelength	/759.4629	/759.4629	/759.4629	/759.4629	/759.4629
ocean	$2.59 \times 10^{-4}$	$2.09 \times 10^{-4}$	$2.22 \times 10^{-4}$	$2.64 \times 10^{-4}$	$2.96 \times 10^{-4}$
land	$3.78 \times 10^{-4}$	$3.06 \times 10^{-4}$	$3.25 \times 10^{-4}$	$3.84 \times 10^{-4}$	$4.29 \times 10^{-4}$
Temperature 1K	26.2×10 <sup>-4</sup>	$4.64 \times 10^{-4}$	9.10×10 <sup>-4</sup>	$27.5 \times 10^{-4}$	$47.8 \times 10^{-4}$
Vapor mixing 20% ratio	$7.68 \times 10^{-4}$	$4.86 \times 10^{-4}$	5.38 × 10 <sup>-4</sup>	$7.03 \times 10^{-4}$	$7.95 \times 10^{-4}$
Energy monitor channel calibration	$1.91 \times 10^{-4}$	$1.25 \times 10^{-4}$	$1.40 \times 10^{-4}$	$1.96 \times 10^{-4}$	$2.28 \times 10^{-4}$
Echo channel calibration	1.91 ×10 <sup>-4</sup>	$1.25 \times 10^{-4}$	$1.40 \times 10^{-4}$	$1.96 \times 10^{-4}$	$2.28 \times 10^{-4}$
Elevation 2m error	$0.22 \times 10^{-4}$	$0.14 \times 10^{-4}$	$0.16 \times 10^{-4}$	$0.22 \times 10^{-4}$	$0.26 \times 10^{-4}$
Aerosol Mie scattering	$1.21 \times 10^{-4}$	$1.59 \times 10^{-4}$	$2.09 \times 10^{-4}$	$2.69 \times 10^{-4}$	$3.29 \times 10^{-4}$
99.99% spectral purity	$0.840 \times 10^{-4}$	$0.451 \times 10^{-4}$	$0.535 \times 10^{-4}$	$0.816 \times 10^{-4}$	$1.01 \times 10^{-4}$
Frequency jitter(10MHZ)	42.8 ×10 <sup>-4</sup>	$15.6 \times 10^{-4}$	$7.76 \times 10^{-4}$	$16.0 \times 10^{-4}$	$9.49 \times 10^{-4}$
Differential absorption cross section (m <sup>2</sup> )	$2.45 \times 10^{-29}$	$1.51 \times 10^{-29}$	$1.63  imes 10^{-29}$	$2.08 \times 10^{-29}$	$2.32 \times 10^{-29}$
Geometrically added	54.6 ×10 <sup>-4</sup>	$20.2 \times 10^{-4}$	$16.7 \times 10^{-4}$	$36.7 \times 10^{-4}$	53.9 ×10 <sup>-4</sup>
Absolute error(hPa)	5.12	3.07	2.35	4.05	5.34
Relative error(%)	0.505	0.302	0.232	0.400	0.527

548

549 Consequently, according to Table 12 and Table 13, the pulse energy, pulse repetition, time 550 resolution, and distance along track are 100mJ, 100Hz, 6.25 s, and 44km, respectively. The 551 765.6735/765.4637 wavelength pairs are used as detection wavelength and reference 552 wavelength. In the 1K error temperature profile, 20% error vapor mixing ratio result in  $6.08 \times$ 553  $10^{-4}$  error in differential optical depth, which corresponds to an absolute error in surface 554 pressure of 1.51hPa, therefore, it is a desirable result that the relative error of surface pressure 555 could be considered as 0.150%.





#### 556 4 Summary

557 The calculation process of retrieving the surface pressure from the atmospheric differential 558 optical depth was also discussed. The performance of the differential absorption LIDAR 559 model was evaluated. Owing to the influence of temperature on Oxygen absorption 560 coefficient and the uncertainty of atmospheric mixing ratio, maintaining the relative error of 561 surface atmospheric pressure below 0.1% is a challenging task. The main factors affecting the 562 random error of surface pressure are the low sea reflectivity, random error of low signal-to-563 noise ratio, and the uneven ground, which renders the multi pulse echo unable to be 564 accumulated and averaged directly. Further, 765.6735/765.4637nm was selected as the 565 working wavelength, the pulse energy, pulse repetition, time resolution, distance along the 566 track resolution are 100mJ, 100Hz, 6.25 s, and 44km, respectively, while the relative error of surface atmospheric pressure was controlled in the range of 0.2–0.3%. 567

#### 568

#### 569 Author contribution

570 Guanglie Hong developed the model and Yu Dong performed the simulations,was
571 responsible for data processing and software code. Guanglie Hong provided part of the
572 manuscript and analyzed the method respectively. Huige Di supervised and modified the
573 manuscript.

574

#### 575 Competing interests

576 I declare that there is no conflict of interest.

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