



1 Automatic quality control of telemetric rain gauge data providing 2 quantitative quality information (RainGaugeQC)

3 Katarzyna Ośródk¹, Irena Otop², Jan Szturc¹

4 ¹Centre of Meteorological Modelling, Institute of Meteorology and Water Management – National Research Institute, PL 01-
5 673 Warszawa, Podleśna 61, Poland

6 ²Research and Development Centre, Institute of Meteorology and Water Management – National Research Institute, PL 01-
7 673 Warszawa, Podleśna 61, Poland

8 *Correspondence to:* Jan Szturc (jan.szturc@imgw.pl)

9 **Abstract.** The RainGaugeQC scheme described in this paper is intended for real-time quality control of telemetric rain gauge
10 data. It consists of several checks: detection of exceedance of the natural limit and climate-based threshold, and checking of
11 the conformity of rain gauge and radar observations, the consistency of time series from heated and unheated sensors, and the
12 spatial consistency of adjacent gauges. The proposed approach is focused on assessing the reliability of individual rain gauge
13 observations. A quantitative indicator of reliability, called the quality index (*QI*), describes the quality of each measurement
14 as a number in the range from 0.0 (completely unreliable measurement) to 1.0 (perfect measurement). The *QI* of a measurement
15 which fails any check is lowered, and only a measurement very likely to be erroneous is replaced with a “no data” value. The
16 quality information provided is very useful in further applications of rain gauge data. The scheme is used operationally by the
17 Polish national meteorological and hydrological service (Institute of Meteorology and Water Management – National Research
18 Institute).

19 1 Introduction

20 The accuracy of telemetric rain gauge data is vital both for scientific research and for real-time modelling. Reliable
21 precipitation measurements with high temporal and spatial resolution are essential input data for numerous operational
22 applications in meteorology and hydrology, such as quantitative precipitation estimation (QPE), nowcasting, real-time initial
23 conditions for numerical weather prediction, hydrological modelling, etc. Incorrect values may affect the results of these
24 applications; this applies especially to unreasonably high or false zero precipitation values.

25 In recent decades, the number of automated weather station networks providing measurements with high temporal
26 resolutions (e.g. 1-, 5-, or 10-minute) has rapidly increased. Consequently, procedures for data quality control (QC) have
27 developed from manual or semiautomatic to fully automatic checks that provide relevant quality information, such as quality
28 flags or quality indices (Lewis et al., 2021). However, in the case of precipitation, the effectiveness of automatic quality control
29 methods has been proven to be much lower than in the case of other meteorological parameters (You et al., 2007). The key
30 issue is the spatiotemporal variability of the precipitation field, which can be very intermittent and small-scale, depends
31 strongly on the type of precipitation (e.g. convective or frontal), and also depends on topographic variables in mountainous
32 areas with complex terrain (Scherrer et al., 2011).

33 This paper presents the RainGaugeQC scheme with automatic QC procedures, developed at the Institute of Meteorology
34 and Water Management – National Research Institute (IMGW), which operates the Polish national meteorological and
35 hydrological service. The scheme focuses on telemetric rain gauge measurements, and is designed to identify erroneous or
36 suspicious data and to assign a quality index to the individual measurements.



37 1.1 Sources of errors in rain gauge data

38 Ground rain gauge measurements, like other observations, are affected by different types of errors, usually classified as
39 random, systematic and gross errors. Random errors vary in an unpredictable manner, while systematic errors remain constant
40 or vary in a predictable way, and can often be reduced. Gross errors are characterised by rare occurrence and large magnitude
41 (WMO-No. 488, 2017).

42 Problems relating to the accuracy of precipitation measurement have been well documented (e.g. Sevruk, 1996; Habib
43 et al., 2001; Golz et. al., 2005; Sieck et al., 2007; Sevruk et al., 2009). The magnitude of measurement errors depends on many
44 factors, including weather conditions at the collector, the location of the rain gauge, and the gauge type. The most significant
45 measurement errors are related to wind (Sevruk et al., 2009; Rasmussen et al., 2012; Martinaitis et al., 2015). Wind-induced
46 losses mainly depend on wind speed and turbulence, as well as the type of precipitation (e.g. rain, mixed snow and rain, or
47 snow). The measurement error is usually greater for solid than for liquid precipitation (WMO-No. 8, 2018). Because of slow
48 falling, snow hydrometers are more susceptible to deflection by wind-induced turbulence around the gauge, making snowfall
49 measurements prone to large systematic errors (Rasmussen et al., 2012). In windy conditions, the underestimation of snowfall
50 accumulation frequently ranges from 20% to 50% or even higher, and additionally depends on other variables, such as exposure
51 and the type of rain gauge (Rasmussen et al., 2012; Buisán et al., 2017; Grossi et al., 2017). Other systematic error sources are
52 related to physical processes, such as evaporation from a bucket, wetting, and splashing. All such errors are typically referred
53 to as catching losses.

54 Additional difficulties occur in winter precipitation measurements as a result of snow collecting on the gauge or snow
55 accumulating within wind shields, either of which can completely or partially block the gauge orifice (Goodison et al., 1998;
56 Rasmussen et al., 2012; Martinaitis et al., 2015; Kochendorfer et al., 2020). In consequence, Martinaitis et al. (2015) identified
57 a secondary but important impact from gauges that had become partially or completely stuck during winter precipitation events.
58 Thawing due to increased surface ambient temperatures resulted in gauges reporting false non-zero precipitation after having
59 collected solid precipitation. These impacts became increasingly complex when rainfall occurred simultaneously with the
60 thawing of accumulated solid precipitation.

61 Moreover, the accuracy of precipitation measurements may be affected by improper exposure of the gauge, site altitude,
62 shielding or obstacles (e.g. trees, buildings) near the rain gauge, the impact of topographic variables in complex areas, and the
63 seeder–feeder effect (Førland et al., 1996; Sevruk and Nevenic, 1998).

64 Additionally, mechanical problems specific to each type of rain gauge influence the accuracy of precipitation
65 measurements. Tipping bucket rain gauges are subject to random errors related to partial or total blockages of the mechanism
66 due to accumulated mineral or biological particulates: dust, insects, blown grass, etc. (Sevruk, 1996; Upton and Rahimi, 2003).
67 In consequence, even partial clogging of the gauge can result in erroneous estimates of the intensity and duration of rainfall.
68 Another specific problem with tipping bucket rain gauges relates to high-frequency bucket tips (double tips), which lead to the
69 recording of spurious high rainfall intensities, while on the other hand very slow tips (i.e. a limited tipping rate) may result in
70 misleading underestimates of rain rates (Upton and Rahimi, 2003; Shedekar et al., 2016).

71 In the case of weighing gauges, the most relevant sampling errors are related to the response time of the measurement
72 system and the consequent systematic delay in assessing the exact weight of the accumulated precipitation in the container,
73 especially in the case of high resolution (e.g. a 1-minute time resolution). Sampling errors may also affect the measurement of
74 low-intensity rain (Colli et al., 2013).

75 Electronic weighing precipitation gauges are less susceptible to evaporation losses than tipping bucket gauges and have
76 better accuracy in assessing the beginning of snowfall events. A heated tipping bucket gauge starts recording with a delay due
77 to the time needed to melt the snow and fill the first tip, and measures less precipitation due to heating-related losses (Savina
78 et al., 2012).



79 Furthermore, precipitation measurements may be affected by gross errors, mainly caused by the malfunctioning of
80 measurement devices, or occurring during data transmission.

81 1.2 Approaches to quality control of rain gauge data

82 Quality control is a vital part of data processing. The World Meteorological Organisation (WMO) encourages the use of data
83 QC in order to achieve a certain standard for international data exchange (WMO-No. 488, 2017). The WMO recommends
84 initially to perform real-time basic QC of raw data at sensor level, then near-real-time QC, and finally non-real-time extended
85 QC (semi-automatic) at the headquarters. Performing QC at various stages of data processing makes it possible to identify the
86 majority of errors in the dataset.

87 Generally speaking, some precipitation data QC checks consider each single observation separately (Upton and Rahimi,
88 2003; Taylor and Loescher, 2013; Blenkinsop et al., 2017), whereas more complex ones also take into account data from
89 neighbouring stations (Steinacker et al., 2011; Scherrer et al., 2011) or multi-source data, such as weather radar data (Yeung
90 et al., 2014; Baserud et al., 2020) and output from a numerical weather prediction model (Qi et al., 2016). Recently, due to the
91 increased utilisation of crowdsourced observations, specific QC methods applicable for this type of precipitation data have
92 been developed (de Vos et al., 2019; Bárdossy et al., 2021; Niu et al., 2021).

93 For assessing the reliability of observations, several approaches are adopted. In practice, various measures of the quality
94 of precipitation data are used, which indicate the reliability of individual sensors resulting from measurement precision, which
95 is strongly conditioned by construction and technology (Førland et al., 1996), location, current meteorological conditions
96 (wind, temperature), etc. Often, flags describing the quality of the data are used qualitatively; for example, the WMO
97 recommends a scheme of five quality flags, defined as good, inconsistent, doubtful, erroneous, and missing (WMO-No. 488,
98 2017, p. 201).

99 In the simple approach to QC outputs, the only possible result is the acceptance or rejection of particular observations.
100 An observation that passes all of the checks is flagged as correct. If an observation fails a check, it is flagged as incorrect and
101 does not undergo the remaining checks (Baserud et al., 2020); however, it is possible to retrieve information on which test was
102 failed for each observation. Some QC schemes integrate the results of individual QC checks to generate a final flag for each
103 observation. In this case an adjustment test or specially designed rule base is applied to minimise the number of correct
104 observations that are flagged as “erroneous” – for example, if an observation failed a climate-based range test but passed the
105 spatial check, then an adjustment test may reduce the severity of the flag obtained from the climate-based range check (Fiebrich
106 et al., 2010; Lewis et al., 2018; 2021).

107 In another approach, after failing specific checks the measured values are not removed, but corrected. Such a method
108 may be used to replace suspicious data with values obtained from interpolation data from neighbouring stations (Michelson,
109 2004), but it does not provide any additional information. Also, the use of data from other measurement systems is not a
110 satisfactory solution, as these data are generally inconsistent with each other due to the extremely different error structures.
111 Generally, the correction of measured values can give unreliable results due to the high level of arbitrariness.

112 Recently, machine learning using artificial neural networks has been employed as a tool for automated quality control
113 as well as for the correction of errors and reconstruction of missing values in precipitation data (Moslemi and Joksimovic,
114 2018).

115 Quantitative indicators based on various forms of quality indicator can also be used, describing the quality of the
116 measurement by means of a number, most often in the range from 0.0 (completely unreliable measurement) to 1.0 (perfect
117 measurement) (Einfalt et al., 2010; Szturc et al., 2022).

118 The latter approach is adopted in the QC scheme described in this paper. In the developed RainGaugeQC scheme, the
119 quality of uncertain measurements is lowered and only measurements very likely to be erroneous are removed – they are
120 replaced with “no data” values. The advantage of this approach is that the quality information can be very useful in further



121 applications, for example in quality-based spatial interpolation of rain gauge data and in merging observations from different
122 measurement techniques (e.g. Jurczyk et al., 2020). It seems optimal to take into account quantitative information about the
123 quality of individual measurements in such a way that the more uncertain data are assigned a lower weight than more reliable
124 data.

125 1.3 Structure of the paper

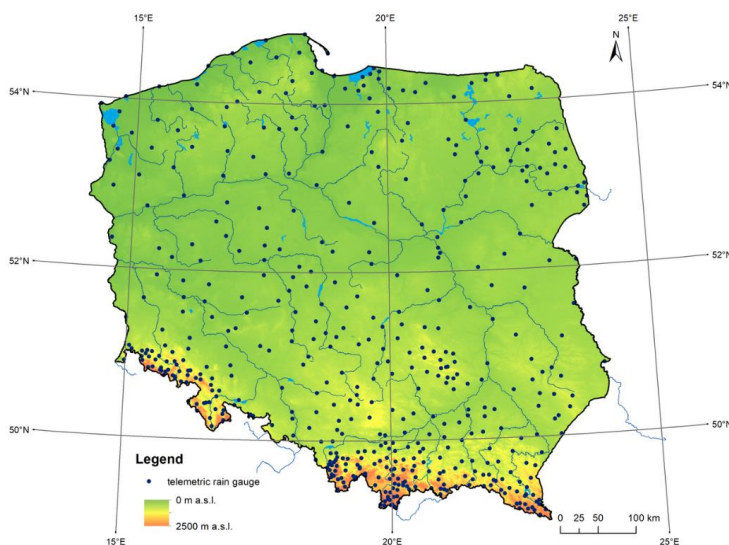
126 The paper is structured as follows. Section 1 provides an overview of the factors influencing the accuracy of rain gauge
127 measurements and the main approaches to data quality control procedures. Section 2 briefly describes the rain gauge data on
128 which the RainGaugeQC scheme proposed in the paper was developed and calibrated, as well as the radar data used as auxiliary
129 data in this scheme. In section 3, the checks that constitute the RainGaugeQC system are presented (their detailed descriptions
130 are included in the appendices). Section 4 presents and discusses specific examples of the scheme's performance and a general
131 analysis of its operation. The article ends with a list of conclusions resulting from the operational use of the RainGaugeQC
132 scheme at IMGW (section 5).

133 2 Data sources

134 2.1 Rain gauge network in Poland

135 The Polish national meteorological and hydrological service, provided by IMGW, operates a nationwide meteorological
136 telemetric network which consists of 503 rain gauges equipped mainly with tipping bucket sensors (Fig. 1). At the synoptic
137 stations, SEBA Hydrometrie (<https://www.seba-hydrometrie.com/>) RG-50 devices are installed, whereas lower-level stations
138 use mainly the Met One Instruments (<https://metone.com/>) 60030 and 60030H devices (unheated and heated, respectively).
139 Telemetric precipitation measurements are available with a 10-minute time resolution: all year round for heated sensors, and
140 in the warm part of the year – from April to October – for unheated ones.

141



142
143
144

Figure 1: Network of telemetric rain gauges in Poland.

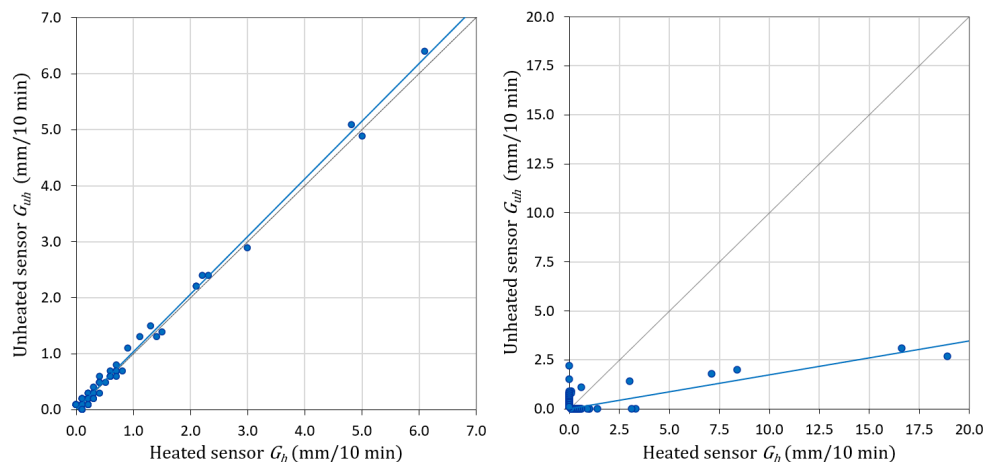
145 The reliability of individual rain gauges depends on the type of the gauge and its location, and changes with time. The
146 network's tipping bucket devices often malfunction, and moreover these sensors lower the precipitation values by an average
147 of about 8–20% (Urban and Strug, 2021).



148 Fig. 2 shows the relationships between measurements of 10-minute precipitation accumulations from unheated and
149 heated sensors on two sample rain gauges: in Dzierżoniów, located in the foothills area, during July 2021 (left), and in Nowa
150 Wieś Podgórna, located in the lowland Wielkopolska (Greater Poland) region in central Poland, during June 2021 (right). Both
151 gauges are equipped with tipping bucket devices. The correlation coefficient calculated for pairs of values in which at least
152 one is different from zero is extremely high for Dzierżoniów, being equal to 0.997 (Fig. 2a), while for Nowa Wieś Podgórna
153 it is only 0.694 (Fig. 2b), a fairly low result caused by very large differences between the values measured simultaneously by
154 the two sensors at the same location. The reason for such low correlation may be that tipping bucket gauges are susceptible to
155 frequent sensor failures.

156 Generally, the left graph of Fig. 2 corresponds to a well-functioning rain gauge, and the right graph to a rain gauge
157 providing data with large errors. For the latter, one or both sensors recorded erroneous precipitation values, and they therefore
158 require effective quality control. It is shown in section 4.3, concerning an example case study, how the quality control scheme
159 presented in this paper worked on these obviously incorrect measurements.

160



161
162
163
164
165

Figure 2: Relationships between observations of 10-minute precipitation accumulations measured with tipping bucket rain gauges equipped with two sensors – unheated and heated – in Dzierżoniów during July 2021 (left) and in Nowa Wieś Podgórna during June 2021 (right). The blue lines mark the trends of these relationships.

166 2.2 Weather radar data

167 Weather radar data are employed in the RainGaugeQC scheme as auxiliary data to verify rain gauge observations. They are
168 generated by the Polish radar network POLRAD, which consists of eight C-band Doppler radars from Leonardo Germany
169 GmbH (formerly Gematronik and Selex) (Szturc et al., 2018). Three of them are dual-polarisation radars, and the others will
170 be upgraded to that functionality in the near future. Three- and two-dimensional radar products are generated by Rainbow 5
171 software every 10 min, with a 1 km spatial resolution within a 215 km range. The Marshall–Palmer formula is used to transform
172 the reflectivity values measured by radar into the precipitation rate, this being the most common form of such a relationship
173 (Neuper and Ehret, 2019). The data are quality controlled by the dedicated RADVOL-QC system developed at IMGW
174 (Ośródką et al., 2014; Ośródką and Szturc, 2022).



175 **3 General description of the developed quality control scheme**

176 **3.1 Set of RainGaugeQC algorithms**

177 A shortened version of the description of the algorithms used in the scheme was presented in works by Otop et al. (2018) and
 178 Jurczyk et al. (2020). This section and the related appendices provide a full description of the developed algorithms. All
 179 parameters defined here were optimised for 10-minute precipitation accumulations (mm/10 min).

180
 181 **Table 1. List of sequential checks for precipitation QC.**

ID	Abbreviation	Name	Main approach	Result of the check
1	GEC	Gross Error Check	Detection of exceedance of the natural limit	Removal of incorrect values
2	RC	Range Check	Detection of exceedance of climate-based threshold at an individual gauge	<i>QI</i> reduction for suspiciously high precipitation value
3	RCC	Radar Conformity Check	Checking of the conformity of rain gauge and radar observations	Removal of false “no precipitation” data. For false precipitation reports, <i>QI</i> reduction depending on $SF(G_h, G_{uh})$ and location
4	TCC	Temporal Consistency Check	Checking of the consistency of time series from heated and unheated sensors	<i>QI</i> reduction for inconsistent sensors
5	SCC	Spatial Consistency Check	Checking of the spatial consistency of adjacent gauges	<i>QI</i> reduction for outliers depending on the inconsistency level

182
 183 The rain gauge quality control procedure developed at IMGW consists of several checks (Table 1). Firstly, simple
 184 plausibility tests – the gross error check and range check – are performed on a single measurement; then more complex checks
 185 are performed, using data from both measurement sensors at the site and data from weather radars.

186 Before the checks, each sensor is assigned the perfect *QI* value (1.0). In case of failure of a particular check, the *QI*
 187 value is decreased by a specified value. If the final *QI* value (after all of the checks) is very weak (≤ 0.0), the sensor is
 188 considered useless and the measurement value is replaced with “no data”.

189 The sensor which obtained a higher final quality index is used for further applications, but if both sensors are of the
 190 same quality, then the heated sensor is taken.

191 **3.2 Similarity function (SF)**

192 It is useful to introduce a tool to check the similarity of two sums of precipitation. For this purpose a similarity function (*SF*)
 193 has been proposed and is used in some of the checks. The function comparing data from two sensors G_h and G_{uh} (heated and
 194 unheated) installed at a given rain gauge location, $SF(G_h, G_{uh})$, in order to check whether the precipitation values are
 195 consistent, is defined as follows:

196 If ($G_h < 1.0$ mm or $G_{uh} < 1.0$ mm), then

197 if ($|G_h - G_{uh}| < 1.0$ mm), then $SF(G_h, G_{uh}) = \text{“true”}$ (1)

198 else $SF(G_h, G_{uh}) = \text{“false”}$

199 whereas:

200 If ($G_h \geq 1.0$ mm and $G_{uh} \geq 1.0$ mm), then

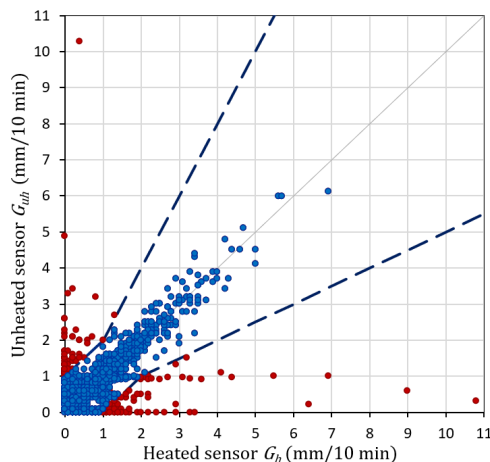
201 if ($0.5 < \frac{G_h}{G_{uh}} < 2.0$ or $|G_h - G_{uh}| < 1.0$ mm), then $SF(G_h, G_{uh}) = \text{“true”}$ (2)

202 else $SF(G_h, G_{uh}) = \text{“false”}$

203 In the above formulae, precipitation units are given in “mm”, but they may refer to different accumulation periods, for
 204 example, mm per 10 minutes (mm/10 min) or 1 hour.



205 The result of the use of SF to assess the similarity of measurements between two sensors (heated and unheated) in rain
206 gauges is presented in Fig 3. The graph shows example data for one day, 22 May 2019, obtained from all measuring stations.
207 It is indicated which measurements from the two sensors are shown by the SF function to be similar (marked blue) and which
208 are not similar (marked brown). The two blue dashed lines delimit the area in which the values measured by the unheated and
209 heated sensors are similar according to the SF function.
210



211
212
213 **Figure 3: Precipitation data from G_{uh} and G_h sensors that are similar (blue) and not similar (brown). The similarity of the**
214 **measurements from all rain gauges on 22 May 2019 was determined using the similarity function SF . The two dashed lines delimit**
215 **the area in which the measurements are considered similar.**

216 3.3 Gross Error Check (GEC)

217 GEC is a preliminary check to identify gross errors, mainly caused by the malfunctioning of measurement devices or by
218 mistakes occurring during data transmission or processing (Steinacker et al., 2011), which have a strong effect on the further
219 analyses. GEC examines whether the rain gauge measurement is within the physically acceptable range limits: not less than 0
220 mm and not above 56 mm/10 min. The upper limit was determined on the basis of a formula developed to estimate the
221 maximum reliable precipitation for various durations in Poland (Burszta-Adamiak et al., 2019). A measurement that fails the
222 check is rejected from further processing.

223 3.4 Range Check (RC)

224 RC verifies a single measurement against a threshold value, which is based on local climatological data with respect to seasonal
225 variation of observations in the specific location of the rain gauge. This test identifies data as implausible when they exceed
226 the expected maximum value, that is, the threshold empirically estimated from long-term climatological data. It is essential to
227 ensure reliable values of the threshold, because, for example, too low a threshold may cause extreme values of precipitation to
228 fail the test (Taylor and Loescher, 2013). Therefore, Fiebrich et al. (2010) recommend developing regionally specific
229 thresholds for the test. In the proposed QC procedure, the thresholds were defined as 10-minute precipitation values with a 1%
230 probability of being exceeded, determined separately for warm and cold seasons. These values were calculated for each
231 telemetric gauge, based on the statistical distribution of 10-minute accumulations over a long time. In the case that the
232 examined measurement exceeds the relevant threshold value, it is treated as suspicious and its QI is reduced by 0.25.



233 3.5 Radar Conformity Check (RCC)

234 RCC is performed to identify false precipitation – false zero and false gauge-reported precipitation measurements – on the
235 basis of radar data, which quite reliably indicate the spatial distribution of precipitation. RCC compares each precipitation
236 observation lower than 0.2 mm/10 min with radar observations at the gauge location and in a surrounding grid of 3 pixels x 3
237 pixels (the pixel size is 1 km x 1 km). If the radar data for the vicinity of the gauge are above a predefined threshold, then a
238 “no precipitation” result measured by the sensor is assumed to be false and the QI is reduced to 0.

239 On the other hand, the RCC compares every precipitation observation with radar observations at the gauge location and
240 in a neighbouring grid of 3 pixels x 3 pixels. If the radar data indicate “no precipitation” (0 mm), with radar data quality above
241 a predefined threshold, then the precipitation measured by the sensor is assumed to be false and the QI of that observation is
242 reduced. The reduction depends on whether data are available from one or two sensors, on their similarity, and on the gauge
243 location (in mountains, foothills, or lowland areas).

244 For a detailed description of the RCC algorithm and the criteria for determining the reduction of QI , see Appendix 1.

245 3.6 Temporal Consistency Check (TCC)

246 This check, in the form described below, is possible only when two sensors are installed at each measuring station, most often
247 heated and unheated, as is currently the case in the IMGW network. If this is not the case, then a method commonly used in
248 quality control of various meteorological quantities is checking of the time continuity of the measured values. For some types
249 of meteorological data the time consistency checks are efficient; however, in the case of precipitation data, this check would
250 eliminate not only all questionable data but also a large amount of true data, in particular extreme values, because of the high
251 variability of precipitation (WMO-No. 305, 1993, p. VI.21, VI.23).

252 A preliminary check is performed to detect a clogged sensor, which occurs if the same value is repeated over a certain
253 period of time. In this case, the sensor’s quality is reduced to 0.

254 In the next step, pairs of rain gauge sensors (G_h, G_{uh}) are tested for the existence of large differences between them.
255 This check requires measurements from both rain gauge sensors at the same location, and can thus be conducted only in the
256 warm half of the year. In this procedure, if the number of measurement pairs is sufficient, they are accumulated and their
257 similarity is checked using the SF function (see section 3.2). If the sums differ, the data from both sensors have failed the TCC
258 check and their quality is reduced.

259 For a detailed description of the TCC algorithm see Appendix 2.

260 3.7 Spatial Consistency Check (SCC)

261 SCC is applied to identify outliers based on a comparison with neighbouring gauges. Additionally, radar data are introduced
262 to assess the level of QI reduction for outliers.

263 There are several steps in the operational procedure for SCC. Firstly, the domain area is divided into basic subdomains
264 with a spatial resolution of 100 km x 100 km. For each subdomain, a set of percentiles of rain gauge data and the median
265 absolute deviation (MAD) are calculated.

266 The criterion for the spatial consistency of an individual sensor is implemented based on the index D , calculated using
267 the formula of Kondragunta and Shrestha (2006). The index is compared with the threshold values defined by its set of
268 percentiles, making it possible to determine the different classes of outliers. The check is repeated for subdomains obtained by
269 making shifts of 25 km in all four directions. If the sensor value is identified as an outlier in the basic subdomain and in the
270 shifted subdomains, the sensor is detected as an outlier and a further procedure is applied to assess the relevant quality
271 reduction.

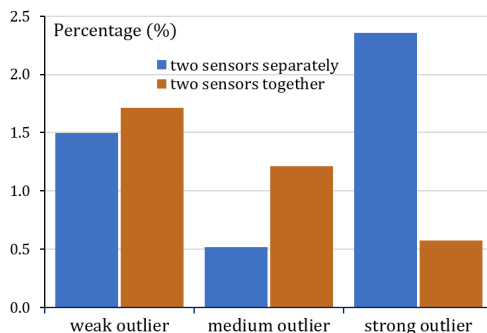


272 For each detected outlier, two criteria are checked: (i) if data from both sensors are available for a given rain gauge and
273 they are similar, i.e. $SF(G_n, G_{nh}) = \text{“true”}$, and (ii) if the data passed the TCC test, then the QI for the sensor is not reduced.
274 Otherwise, for additional verification, radar data in a grid of 5×5 pixels around the gauge location are considered if they are
275 of good quality; then the reduction of the QI value depends on the class of the outlier (weak, medium, or strong) and the
276 magnitude of the disparity with the radar data.

277 A detailed description of the SCC algorithm and the criteria for reduction of the QI value are given in Appendix 3.

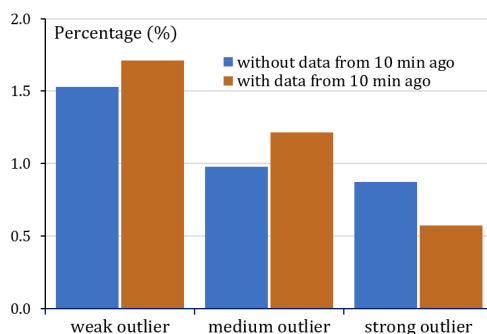
278 The check may optionally analyse data from both sensors together or separately, and may or may not include data from
279 the previous time step. It was investigated how these settings influence the performance of the check.

280 Fig. 4 presents graphs showing the percentage of data with reduced QI values, as a result of analysing the spatial
281 conformity of data from two types of sensors (unheated and heated) separately or together. The obtained sample results
282 generally showed large variation; however, the numbers of strong outliers increased significantly (about 2.35% versus 0.6%)
283 when the two types of sensors were analysed separately – in that case the algorithm appears much less tolerant.
284



285
286
287 **Figure 4: Percentage of classes of outliers (weak, medium, and strong) when analysing the data from two types of sensors (unheated**
288 **and heated) separately (blue) or together (brown). Data from 22 May 2019.**

289 If the algorithm takes into account data not only from the current time step, but also from 10 minutes ago (both sensors
290 analysed together), then these numbers are slightly higher for weak and medium outliers and slightly lower for strong ones.
291 The percentage of the data belonging to different classes of outliers was slightly over 3% (Fig. 5), and for particular classes
292 ranged from about 1.5–1.7% for weak to about 0.6–0.9% for strong outliers. This observation suggests that the inclusion of
293 data from the previous time step makes the algorithm more tolerant.
294



295
296
297 **Figure 5: Percentage of classes of outliers (weak, medium, and strong) when analysing measurements from the given time only (blue)**
298 **and also from the previous time step (brown). Data from two days: 20–21 June 2020.**



299 In the RainGaugeQC scheme used by IMGW in real time, in the SCC check both types of sensors are analysed together,
 300 also taking account of the data from the previous time step.

301 3.8 Quality index of spatially distributed rain gauge data

302 In most applications of rain gauge data, spatial interpolation of the point data is required, which can be performed using one
 303 of the many commonly known methods. However, it is not enough to spatially interpolate the *QI* values assigned to individual
 304 rain gauges, but it is also necessary to take into account the fact that due to the natural high variability of the precipitation field,
 305 the uncertainty of the estimated field decreases very quickly with increasing distance from the nearest rain gauge. Therefore,
 306 the quality field for the spatially distributed precipitation data depends on two factors: the *QI* point values for individual rain
 307 gauges (denoted by the *QI* with the index “*p*”) and a factor that depends linearly on the distance from the nearest rain gauge
 308 (with the index “*d*”).

309 The *QI* point values from rain gauges should be spatially interpolated by the same method as the precipitation field is
 310 interpolated; hence the quality field $QI(G_{int}(x, y))_p$ is obtained. In the case of the operational scheme used by IMGW, ordinary
 311 kriging is applied, where the domain of 900 km x 800 km is divided into 16 subdomains of 225 km x 200 km and interpolation
 312 is performed separately in each of them.

313 The factor related to the distance from the rain gauges $QI(G_{int}(x, y))_d$ takes into account the decrease in the quality of
 314 the rainfall field depending on the distance $d(x, y)$ to the nearest rain gauge. The distance factor for each pixel is calculated
 315 from the linear formula:

$$316 \quad QI(G_{int}(x, y))_d = \frac{d_{max} - d(x, y)}{d_{max}} \quad (3)$$

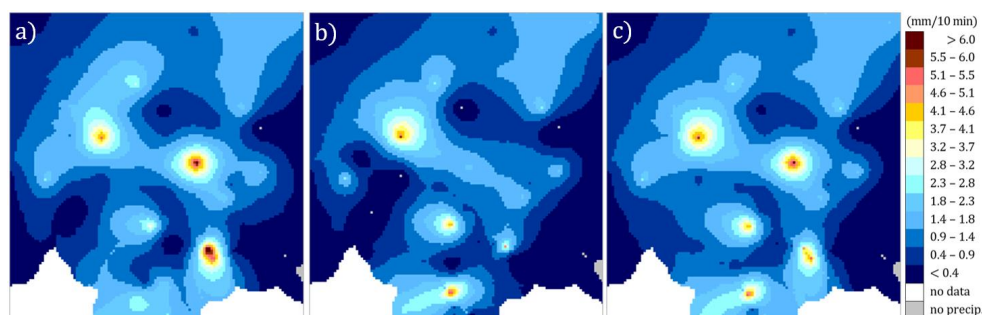
317 where d_{max} is the limit value of the distance to the nearest rain gauge, above which the quality at that pixel is assigned a value
 318 of zero (the adopted limit is 100 km).

319 The field of the final quality index for the rain gauge-based precipitation field is calculated from the product of the two
 320 above factors:

$$321 \quad QI(G_{int}(x, y)) = QI(G_{int}(x, y))_p \cdot QI(G_{int}(x, y))_d \quad (4)$$

322 4 Examples of QC scheme operation for a rain gauge with low quality measurement

323 4.1 Influence of differences in values from two sensors on precipitation field estimation



324
 325
 326 **Figure 6:** Spatially interpolated rain gauge data obtained from: (a) unheated and (b) heated sensors, and (c) after quality control
 327 (considered optimal). Data from 5 August 2021, 17:40 UTC, excerpt from the Polish domain (240 km x 250 km).

328 In the example presented in Fig. 6, it can be seen that the data from the two sensors can sometimes be significantly different.
 329 The final rainfall field can be simply generated by taking the mean or the higher values of the two sensors at the same location,

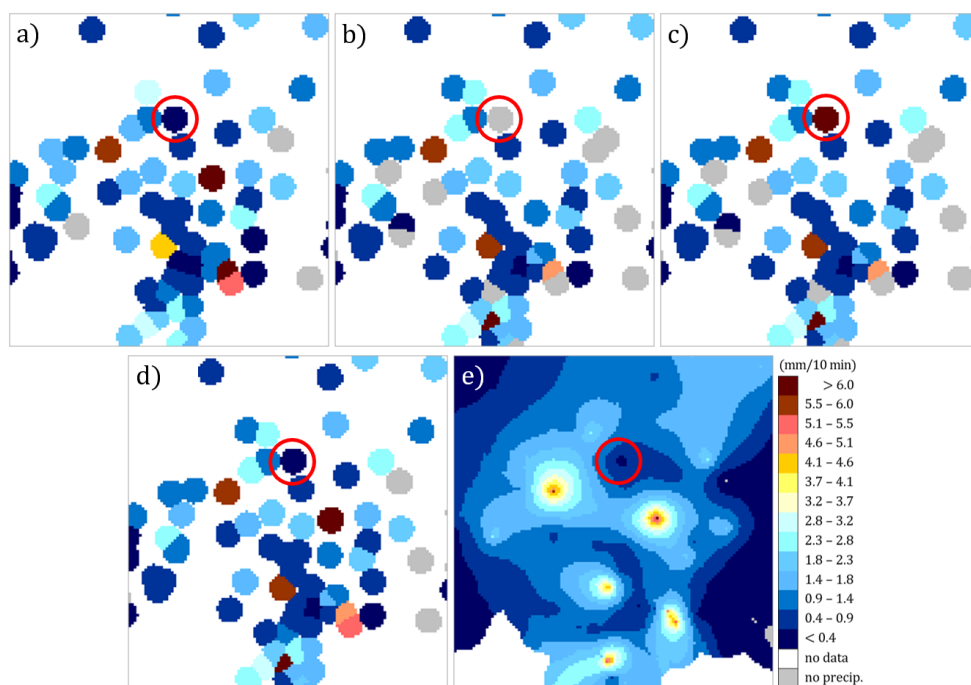


330 and both of these approaches can be justified depending on the final application of the data. The approach used in the
331 RainGaugeQC scheme makes it possible to choose the better value according to defined checks, and moreover to apply it along
332 with the relevant QI value in quality-based interpolation algorithms which generate the optimal rain gauge field.

333 4.2 Result of the performance of the QC scheme after the introduction of erroneous values

334 Fig. 7 illustrates the performance of the proposed QC scheme. If the rain gauge data are not subjected to QC algorithms, then
335 two alternative data sets can be considered: from unheated (Fig. 7a) and heated (Fig. 7b) sensors. The third diagram shows an
336 example of data disturbed with an artificial value of 10 mm/10 min at the heated sensor of the Siercza rain gauge (Fig. 7c), the
337 location of which is marked with a red circle in all diagrams.

338



339
340
341
342
343
344
345

Fig. 7. Example of the RainGaugeQC performance after the introduction of erroneous precipitation value: (a) original rain gauge data from unheated sensors (G_{uh}) (in all fields the Siercza rain gauge is marked with a red circle), (b) original data from heated sensors (G_h), (c) data from heated sensors disturbed with an artificial value at Siercza (10 mm/10 min), (d) rain gauge data after quality control, and (e) after spatial interpolation. Data from 5 August, 2021, 17:40 UTC, excerpt from the Polish domain (240 km x 250 km).

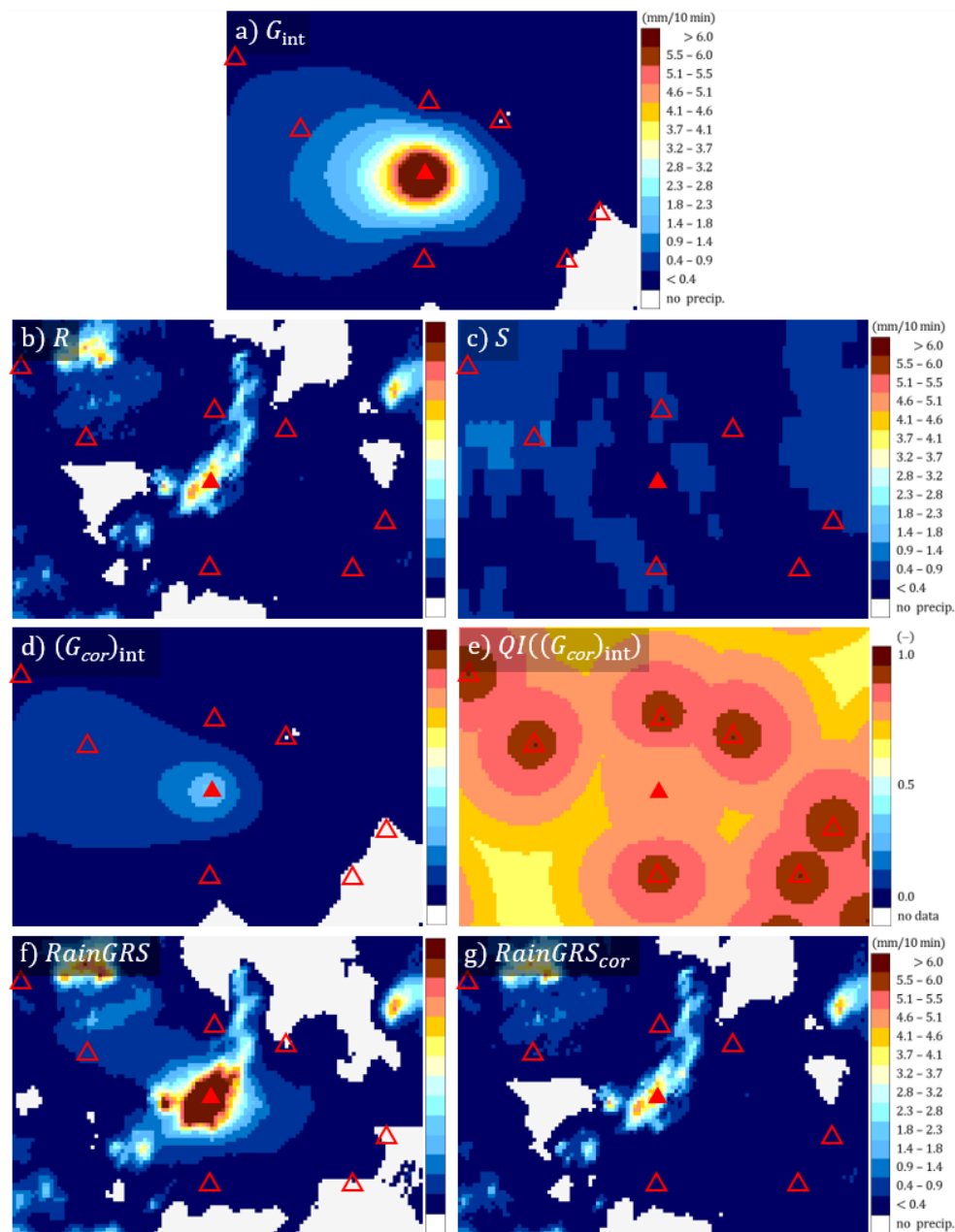
346 Fig. 7d shows the values from individual rain gauges after quality control, and Fig. 7e shows the same values after
347 spatial interpolation using the ordinary kriging technique (this field is identical to the one shown in Fig. 6c). As these images
348 show, the precipitation values obtained after data quality control are some mixture of those data from both sensors that passed
349 the QC with higher QI (see section 3.1). The Siercza rain gauge, marked with a red circle, serves here as an example of a gauge
350 with incorrect measurement (the original values were 0.2 and 0.0 mm/10 min for unheated and heated sensors, respectively).
351 The erroneous value of 10 mm/10 min was eliminated as a result of the QC algorithms, so the rainfall value for this rain gauge
352 after QC is 0.2 mm/10 min measured by the unheated sensor.



353 **4.3 Example for Nowa Wieś Podgórna rain gauge from 22 June 2021, 13:30 UTC**

354 An example of a rain gauge with low-quality measurements, taken from the Nowa Wieś Podgórna rain gauge during June
355 2021, is shown in Fig. 2b (section 2.1). The low quality is evidenced by large differences between the values measured with
356 heated and unheated sensors: the heated sensor recorded much higher 10-minute precipitation accumulations than the unheated
357 one. The data from 22 June 2021, 13:30 UTC are analysed in detail below. The heated sensor of the Nowa Wieś Podgórna rain
358 gauge reported a very high rainfall of 18.9 mm/10 min, whereas the unheated one reported only 2.7 mm/10 min (Table 2). If
359 QC is not performed, then the heated sensor is generally considered the primary sensor as it operates all year round. The
360 precipitation field resulting from the interpolation of rain gauge data without QC obtained by the ordinary kriging method is
361 shown in Fig. 8a.

362



363
 364
 365
 366
 367
 368
 369
 370
 371

Figure 8: Various fields of 10-minute precipitation accumulation (in mm/10 min) in the vicinity of the Nowa Wieś Podgórna rain gauge (marked with a red triangle; the locations of other rain gauges are marked with empty triangles): a) spatially interpolated field from rain gauge data without QC (G_{int}), b) radar-based precipitation field (R), c) satellite-based precipitation field (S), d) spatially interpolated field from rain gauge data after QC ($(G_{cor})_{int}$), e) QI field for the precipitation field from rain gauge data after QC ($QI((G_{cor})_{int})$), f) multi-source precipitation field ($RainGRS$) obtained from raw rain gauge data, g) multi-source precipitation field ($RainGRS_{cor}$) obtained from rain gauge data after QC. Data from 22 June 2021, 13:30 UTC, excerpt from the Polish domain (110 km x 80 km).

372
 373
 374
 375

In order to diagnose the large difference between the two sensors, a detailed investigation of the situation was performed based on precipitation data from other sources. The radar composite map from the SRI (surface rainfall intensity) product showed 3.95 mm/10 min at this location (Fig. 8b), which is much closer to the value from the unheated sensor. Satellite rainfall, determined from various NWC-SAF products based on Meteosat data (Jurczyk et al., 2020), showed only 0.05 mm/10 min



376 (Fig. 8c); however, measurements based on data from visible and infrared channels are much less accurate than radar
377 measurements. Thus, the radar data confirmed that the rainfall that occurred in the analysed time step in the close vicinity of
378 this rain gauge is significantly higher than in the surroundings, but not by as much as the heated sensor reported – it is much
379 closer to the observation of the unheated sensor.

380 Visually, this conclusion seems to be unquestionable, but it may be interesting how the designed RainGaugeQC scheme
381 functioned in this situation.

382
383

Table 2. Results of QC of the Nowa Wieś Podgórna rain gauge station on 22 June 2021, 13:30 UTC.

Sensor	G (mm/10 min)	Check				$QI(G)$ (–)
		RC	RSC	TCC	SCC	
Unheated	2.7	Passed	Passed	Failed	Weak outlier	0.75
Heated	18.9	Passed	Passed	Failed	Strong outlier	0.50

384
385

The quality of the data from this rain gauge was 0.75 for the G_{uh} sensor and 0.50 for G_h . This difference in QI values
386 was a result of the SCC test, which showed that the G_{uh} sensor differs slightly, and the G_h sensor differs significantly, from the
387 rainfall values in the neighbouring rain gauges within the given subdomain. At the same time, both sensors failed the TCC
388 test, which in turn indicates that the accumulated values measured by these two sensors over the last 12 time steps differ
389 significantly (Table 2). This also contributed to a reduction in the final QI value.

390
391

Thus, finally, the value from the unheated sensor G_{uh} is taken for further processing. The precipitation field after the
392 spatial interpolation of QC data obtained by the ordinary kriging method is shown in Fig. 8d. The precipitation values around
393 this rain gauge location are clearly lower than those shown in Fig. 8a (without QC). The QI field for spatially interpolated rain
394 gauges is shown in Fig. 8e – the Nowa Wieś Podgórna rain gauge is of lower quality than the neighbouring rain gauges.

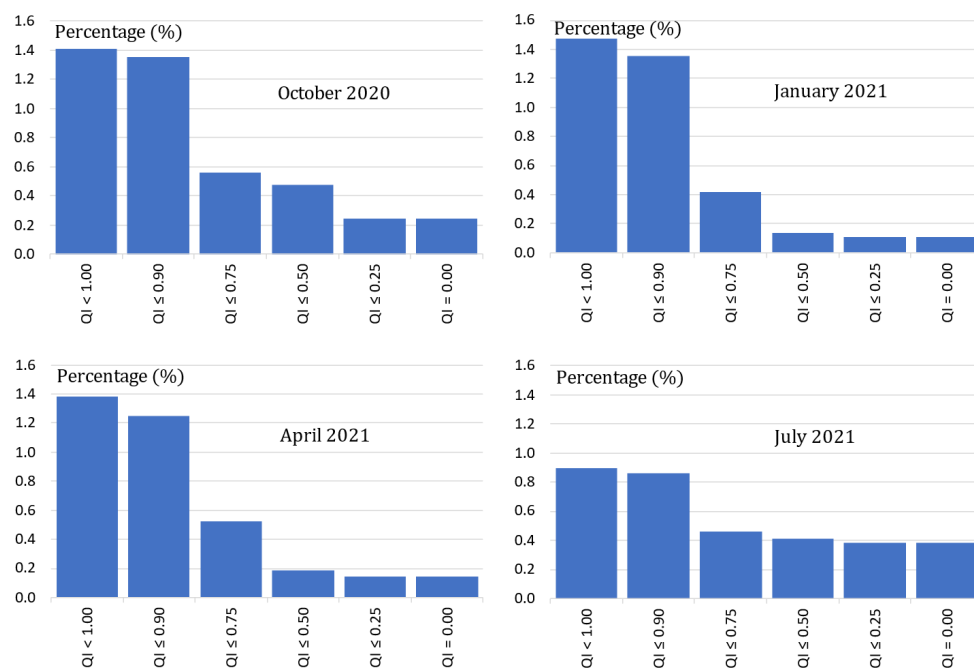
395
396

QC of rain gauge data influences the precipitation fields produced by applications for the generation of multi-source
397 fields. This is shown by the example of the QPE fields produced by the RainGRS system, which operationally combines
398 precipitation data from rain gauges, weather radar and meteorological satellites, based on conditional merging and additionally
399 taking quality information into account (Jurczyk et al., 2020). In Fig. 8 two fields generated by RainGRS are presented: based
400 on rain gauge data without QC and after QC (Figs. 8f and 8g, respectively). Applying quality controlled rain gauge data, the
RainGRS estimate decreases from 16.19 to 3.26 mm/10 min, which is a very significant effect.

400 4.4 General effects of the operation of the scheme

401
402

The performance of the RainGaugeQC scheme can be analysed in terms of the degree of QI reduction. This is presented in
403 Fig. 9, for individual months representative for autumn, winter, spring and summer conditions (October, January, April, and
404 July, respectively).



405
 406
 407
 408

Figure 9: Percentage of rain gauge observations with a specified QI reduction after quality control. From top: percentage contribution in each QI interval; cumulative percentage contribution (in %); from left: October 2020, January, April, and July 2021.

409
 410
 411
 412
 413

The graphs shown do not include the percentage contribution of measurements that were assigned a quality of 1.0; this is equal to about 92.0–94.5%, many times higher than the total contribution of all other values. In general, it can be seen from Fig. 9 that by far the greatest number of reductions in QI values was to values in the range [0.75, 0.90), and this is observed in all seasons of the year. Relatively large numbers of QI reductions to values in the range [0.50, 0.75) occur in winter (January) and spring (April), and relatively many reductions to a zero value occur in summer (July) and autumn (October).

414
 415
 416
 417
 418
 419

The number of rain gauge observations with reduced quality is relatively small, below 1.5%. For example, the contribution of data with QI reduced to zero ranges from about one-third to one-tenth, but grows to about one-half over the summer (July). In practice, this means that these data were rejected. Probably the most important reason is that in the summer there often occurs convective precipitation, characterised by high intensities and strong spatial variability, and moreover rain gauges in no-rain situations react to morning dew condensation, which gives false rainfall measurements sometimes as high as 0.3 mm/10 min.

420
 421
 422

The most diversified distribution of QI reductions is observed in winter (January): most often there are small decreases in the QI value. In summer (July), this distribution is the least varied, which can be partially explained by the numerous QI reductions to zero.

423 5 Conclusions

424
 425
 426
 427
 428

1. Quality control of rain gauge data is essential, especially from the perspective of operational applications, when it is not possible to verify gauge data employing highly reliable precipitation measurements, such as manual Hellmann rain gauges, which are not available in real time.
2. It seems that the RainGaugeQC approach to the QC of rain gauge data, which consists in estimating the value of the QI of individual observations, enables more effective use of the data. On the one hand, it is a more cautious approach,



- 429 as it does not eliminate all suspicious observations, and on the other hand, it enables flexible treatment of any
430 suspected case of data incorrectness.
- 431 3. The IMGW rain gauge network consists mostly of rain gauges equipped with two sensors: unheated and heated. This
432 unique equipment allows the use of pairs of data to conduct much more effective QC. Comparing the observations
433 from two sensors installed at the same location significantly increases the possibility of obtaining information about
434 the uncertainty of measurements, for example by checking the time consistency of the data (TCC check). This is
435 especially important when measurements are carried out with tipping bucket rain gauges, which have relatively low
436 reliability. The availability of observations from both sensors is especially important during the warm season, when
437 convective phenomena prevail. The frequent lack of two sensors installed at the same location reduces the scheme's
438 effectiveness to some extent; however, it remains at a satisfactory level.
- 439 4. It is worth considering the possibility of employing radar data in the RCC and SCC algorithms to detect erroneous
440 rain gauge measurements and to assess their reliability, based on the difference between the values from rain gauge
441 and weather radar. The case study proved that the RainGaugeQC system can identify regionally inconsistent data
442 thanks to the use of radar data as well as neighbouring rain gauge data.
- 443 5. The presented set of algorithms is based on empirical relationships that are strongly dependent on local conditions,
444 both technical and geographic. The most important factors are the density of the rain gauge network, the availability
445 of other data that can be used as a reference for QC (e.g. from the weather radar network), the type of sensors (their
446 failure rate and measurement uncertainty), as well as terrain orography, wind conditions, and surface precipitation
447 type. Therefore, any changes in the network configuration necessitate recalibration of the algorithms.
- 448 6. The number of rain gauge observations with reduced QI following QC under the RainGaugeQC scheme is relatively
449 small, as it is below 1.5%. In all seasons, the highest number of QI value reductions was to values in the range [0.75,
450 0.90). The highest number of erroneous data (with QI reduced to zero) is found in summer (July) (approximately
451 0.4%), whereas in other seasons it ranges from about 0.10% to 0.23%.

452 **Appendix 1. Detailed description of the Radar Conformity Check (RCC) algorithm**

453 RCC is performed to identify false zero precipitation and false gauge-reported precipitation measurement by applying radar
454 data.

- 455 1. Identifying false zero precipitation.
- 456 Each gauge sensor value (G) less than 0.2 mm/10 min is checked against radar observations (R) at the gauge location
457 and in its vicinity within a grid of 3 pixels x 3 pixels.
- 458 If at least one pixel of radar data had precipitation above 0.4 mm, then the gauge value measured by this
459 sensor is assumed to be erroneous, thus the sensor value is replaced by “no data” and the quality of this sensor is
460 reduced to 0.
- 461 2. Identifying false gauge-reported precipitation.
- 462 Each gauge sensor value (G) above 0 mm/10 min is checked against radar observations (R) at the gauge location and
463 in its vicinity within a grid of 3 pixels x 3 pixels.
- 464 If at least two radar pixels with $QI > 0.85$ returned “no precipitation” ($R = 0$ mm/10 min), then the following
465 conditions are checked:
- 466 (a) If for a given rain gauge, data are available only from one sensor (G) and $G > 0$ mm/10 min, then:
- 467 – if the gauge is located in a mountain or foothill area, the sensor is considered erroneous and its value is
468 replaced by $G = 0$ mm and its quality reduced by 0.5;



- 469 – if the gauge is located in a lowland area, the sensor is considered erroneous and its value is replaced by
470 $G = 0$ mm and its quality reduced by 0.25.
- 471 (b) If for a given rain gauge, data are available from two sensors (heated G_h and unheated G_{uh}) and $G_h > 0$ mm/10
472 min and $G_{uh} > 0$ mm/10 min, then:
- 473 – if the gauge is located in a mountain or foothill area and values from both sensors are similar, i.e. $SF(G_{uh},$
474 $G_h) = \text{“true”}$, then the quality of both sensors is reduced by 0.75, but if $SF(G_{uh}, G_h) = \text{“false”}$ then their
475 qualities are reduced to $QI = 0$ and the sensor values are replaced by “no data”;
- 476 – if the gauge is located in a lowland area, then the sensor qualities are reduced to $QI = 0$ and the sensor
477 values are replaced by “no data”.
- 478 (c) If for a given rain gauge, data are available from two sensors (heated G_h and unheated G_{uh}) and one of them
479 reports “no precipitation” (i.e. $G_h = 0$ mm/10 min or $G_{uh} = 0$ mm/10 min), then:
- 480 – if the rain gauge is located in a mountain or foothill area and the values from both sensors are similar (i.e.
481 $SF(G_{uh}, G_h) = \text{“true”}$), then the QI of the sensor which observed precipitation $G > 0$ mm/10 min is reduced
482 by 0.75, but if $SF(G_{uh}, G_h) = \text{“false”}$, then the QI of the sensor which reports $G > 0$ mm/10 min is reduced
483 to $QI = 0$ and the sensor value is replaced by “no data”;
- 484 – if the rain gauge is located in a lowland area, then the quality of the sensor that reports $G > 0$ mm/10 min
485 is reduced to $QI = 0$ and the sensor value is replaced by “no data”.

486 Appendix 2. Detailed description of the Temporal Conformity Check (TCC) algorithm

487 A preliminary check is performed to detect constant values. If the same value (e.g. 0.1 mm/10 min) is reported for a certain
488 number of time steps (e.g. nine consecutive observations), then the sensor is probably clogged. In this case, the blocked sensor
489 has failed the TCC test, its QI is reduced to 0, and the TCC test cannot be performed for the other sensor.

490 The main part of TCC serves to identify pairs of rain gauge sensors (G_h, G_{uh}) for which there are large differences
491 between simultaneously measured values, which may be evidence of their low quality. This check requires measurements from
492 both rain gauge sensors at the same location; it can thus be conducted only in the warm season, when both sensors provide
493 measurements. This lasts from April to October, when data from unheated sensors (G_{uh}) are available; the heated sensors (G_h)
494 operate all year round.

- 495 1. Pairs of simultaneous measurements from two sensors are verified for the last 12 time steps, but observations with
496 poor quality are not taken into account. If the number of quality-verified pairs (for previous time steps with $QI > 0.0$,
497 and for the current one passing the previous checks, i.e. GEC, RC and RCC) is high enough (at least 9), the
498 cumulative sums are calculated:

$$499 S_h = \sum_{i=1}^n G_{h,i}, \quad S_{uh} = \sum_{i=1}^n G_{uh,i} \quad (5)$$

- 500 2. The similarity of the accumulated sums is checked by means of the SF function. If they differ significantly, i.e. if
501 $SF(S_h, S_{uh}) = \text{“false”}$, then the data from both sensors have failed the TCC test and their quality is reduced by 0.25.

502 Appendix 3. Detailed description of the Spatial Consistency Check (SCC) algorithm

503 The SCC procedure consists of the following steps:

- 504 1. The Polish domain (900 km x 800 km) is divided into subdomains with dimensions of 100 x 100 km. Only data
505 with $QI > 0$ after previous tests are subject to this check. Both sensors, heated and unheated, can be analysed
506 together or separately, and these data can also be analysed together with data from the previous time step (10 min



507 ago) if their $QI = 1.0$. In order to perform this check, the number of data in a subdomain must be at least three;
 508 otherwise the test is not performed for that subdomain.

509 2. Based on data from rain gauges (G) located in a given subdomain, the following percentiles are determined: 25%,
 510 50% (median), and 75% ($Q_{25}(G)$, $Q_{med}(G)$, and $Q_{75}(G)$).

511 The median absolute deviation (MAD) for a given subdomain is determined from the formula:

$$512 \quad MAD = \frac{1}{n} \sum_{i=1}^n |G_i - Q_{med}(G)| \quad (6)$$

513 where n is the number of data, G_i is the i -th sensor value, and $Q_{med}(G)$ is the median.

514 3. The index D_i , which determines numerically the deviation of the precipitation value measured with the i -th sensor
 515 from the values of sensors within a given subdomain, is calculated from the formula (Kondragunta and Shrestha,
 516 2006):

$$517 \quad D_i = \begin{cases} 0 & MAD = 0 \\ \frac{|G_i - Q_{med}|}{MAD} & MAD \neq 0 \text{ and } Q_{75} = Q_{25} \\ \frac{|G_i - Q_{med}|}{Q_{75} - Q_{25}} & MAD \neq 0 \text{ and } Q_{75} \neq Q_{25} \end{cases} \quad (7)$$

518 Following calculation of the D_i values for all sensors within a given subdomain, three percentiles are
 519 determined: 90%, 95%, and 99% (Q_{90} , Q_{95} , and Q_{99}).

520 4. If $D_i \leq Q_{90}(D)$, then the i -th sensor is not an outlier and the test is passed.

521 If this is not the case, the i -th sensor is flagged and the formula (8) is applied to compare the index D_i with
 522 the three percentile values, in order to determine to which class of outliers the given value belongs:

$$523 \quad \text{outlier} = \begin{cases} \text{strong} & D_i > Q_{99}(D) \\ \text{medium} & Q_{95}(D) < D_i \leq Q_{99}(D) \\ \text{weak} & Q_{90}(D) < D_i \leq Q_{95}(D) \end{cases} \quad (8)$$

524 The procedure is repeated in four subdomains resulting from shifting the given subdomain vertically and
 525 horizontally, i.e. in four directions, with offsets of 25 km (except for subdomains on the edges and corners of the
 526 domain, which are shifted in three and two directions, respectively). If the value measured with a given sensor is
 527 flagged in all analysed subdomains, it fails the SCC check. If the values belonged to different classes of outliers,
 528 the weakest one is assigned to the sensor for further processing.

529 5. For sensors that failed the SCC check, if the data from both sensors are available for a given rain gauge and they
 530 are similar, i.e. $SF(G_h, G_{uh}) = \text{"true"}$, and passed the TCC check, then the QI for the sensor is not reduced.

531 Otherwise, each outlier is verified against radar data. For this purpose the following values are determined
 532 within a grid of 5 pixels x 5 pixels around this rain gauge location: $\min(QI(R))$ – the minimum quality QI of the
 533 radar precipitation R ; $R_{max} = \max(R: QI(R) > 0.75)$ – the maximum value of radar precipitation with a quality
 534 above 0.75; $QI(R_{max})$ – the quality of the maximum value of radar precipitation R_{max} . This verification algorithm
 535 is as follows:

536 If $\min(QI(R)) > 0.75$, then: (9)

537 if $R_{max} = 0$, then the quality is reduced by 1.0 and $G = \text{"no data"}$;

538 if $(G > 1.0 \text{ mm})$ and $\left(\frac{G}{R_{max}} < \frac{QI(R_{max})}{4.0} \text{ or } \frac{G}{R_{max}} > \frac{4.0}{QI(R_{max})}\right)$, then:

$$539 \quad QI = \begin{cases} QI - 1.00 & \text{strong outlier} \\ QI - 0.50 & \text{medium outlier} \\ QI - 0.20 & \text{weak outlier} \end{cases}$$



540 if ($G > 1.0$ mm) and $\left(\frac{G}{R_{max}} \geq \frac{QI(R_{max})}{4.0}\right)$ and $\frac{G}{R_{max}} \leq \frac{4.0}{QI(R_{max})}$, then:

541
$$QI = \begin{cases} QI - 0.25 & \text{strong outlier} \\ QI - 0.10 & \text{medium outlier} \\ QI & \text{weak outlier} \end{cases}$$

542 If ($G \leq 1.0$ mm) or ($\min(QI(R)) \leq 0.75$), then:

543
$$QI = \begin{cases} QI - 0.25 & \text{strong outlier} \\ QI - 0.10 & \text{medium outlier} \\ QI & \text{weak outlier} \end{cases}$$

544 A simpler analysis of the spatial consistency of rain gauge data may be performed (especially if radar data are
545 unavailable), analogously to steps 1–4, but with only the Q_{95} percentile being determined. Here, if in all subdomains $D_i \leq$
546 $Q_{95}(D)$, the sensor fails the SCC, and the QI is decreased by 0.10.

547

548 *Author contributions.* KO, IO, and JS designed algorithms of the RainGaugeQC system. KO developed the software code and
549 performed the simulations. JS, IO, and KO prepared the manuscript. JS made figures.

550

551 *Competing interests.* The authors declare that they have no conflict of interest.

552 References

- 553 Baserud, L., Lussana, C., Nipen, T.N., Seierstad, I.A., Oram, L., and Aspelien, T.: TITAN automatic spatial quality control of
554 meteorological in-situ observations, *Advances in Science and Research*, 17, 153–163, [https://doi.org/10.5194/asr-17-](https://doi.org/10.5194/asr-17-153-2020)
555 153-2020, 2020.
- 556 Bárdossy, A., Seidel, J., and El Hachem, A.: The use of personal weather station observation for improving precipitation
557 estimation and interpolation, *Hydrology and Earth System Sciences*, 25, 583–601, [https://doi.org/10.5194/hess-25-583-](https://doi.org/10.5194/hess-25-583-2021)
558 2021, 2021.
- 559 Blenkinsop, S., Lewis, E., Chan, S.C., and Fowler, H.J.: An hourly precipitation dataset and climatology of extremes for the
560 UK. *International Journal of Climatology*, 37, 722–740, doi.org/10.1002/joc.4735, 2017.
- 561 Buisán, S. T., Earle, M. E., Collado, J. L., Kochendorfer, J., Alastrué, J., Wolff, M., Smith, C. D., and López-Moreno, J. I.:
562 Assessment of snowfall accumulation underestimation by tipping bucket gauges in the Spanish operational network,
563 *Atmospheric Measurement Techniques*, 10, 1079–1091, <https://doi.org/10.5194/amt-10-1079-2017>, 2017.
- 564 Burszta-Adamiak, E., Licznar, P., and Zaleski, J.: Criteria for identifying maximum rainfall determined by the peaks-over-
565 threshold (POT) method under the Polish Atlas of Rainfall Intensities (PANDa) project, *Meteorology Hydrology and*
566 *Water Management*, 7, 3–13, <https://doi.org/10.26491/mhwm/93595>, 2019.
- 567 Colli, M., Lanza, L.G., and La Barbera P.: Performance of a weighing rain gauge under laboratory simulated time-varying
568 reference rainfall rates, *Atmospheric Research*, 131, 3–12, <https://doi.org/10.1016/j.atmosres.2013.04.006>, 2013.
- 569 de Vos, L. W., Leijnse, H., Overeem, A., and Uijlenhoet, R.: Quality control for crowdsourced personal weather stations to
570 enable operational rainfall monitoring, *Geophysical Research Letters*, 46, 8820–8829,
571 <https://doi.org/10.1029/2019GL083731>, 2019.
- 572 Einfalt, T., Szturc, J., and Ošródká, K.: The quality index for radar precipitation data – a tower of Babel? *Atmos. Sci. Lett.*,
573 11, 139–144. <https://doi.org/10.1002/asl.271>, 2010.
- 574 Fiebrich, C. A., Morgan, C. R., and McCombs, A. G.: Quality assurance procedures for mesoscale meteorological data. *Journal*
575 *of Atmospheric and Oceanic Technology*, 27, 1565–1582, <https://doi.org/10.1175/2010JTECHA1433.1>, 2010.



- 576 Førland, E. J., Allerup, P., Dahlstrom, B., Elomaa, E., Jonsson, T., Madsen, H., Perala, H., Rissanen, P., Vedin, H., and Vejen,
577 F.: Manual for operational correction of Nordic precipitation data. Report Nr 24/96. DNMI, Norway, pp. 66, 1996.
- 578 Golz, C., Einfalt, T., Gabella, M., and Germann, U.: Quality control algorithms for rainfall measurements, *Atmospheric*
579 *Research*, 77, 247-255, <https://doi.org/10.1016/j.atmosres.2004.10.027>, 2005.
- 580 Goodison, B.E., Louie, P.Y.T., and Yang, D.: WMO solid precipitation measurement intercomparison: Final report, *Instrum.*
581 *Obs. Methods Rep.* 67, World Meteorological Organization, Geneva, Switzerland. pp. 211, 1998.
- 582 Grossi, G., Lendvai, A., Giovanni Peretti, G., and Ranzi, R.: Snow precipitation measured by gauges: systematic error
583 estimation and data series correction in the Central Italian Alps. *Water*, 9, 461, <https://doi.org/10.3390/w9070461>, 2017.
- 584 Habib, E., Krajewski, W., and Kruger, A.: Sampling errors of tipping-bucket rain gauge measurements, *Journal of Hydrologic*
585 *Engineering*, 6, 159-166, [https://doi.org/10.1061/\(ASCE\)1084-0699\(2001\)6:2\(159\)](https://doi.org/10.1061/(ASCE)1084-0699(2001)6:2(159)), 2001.
- 586 Jurczyk, A., Szturc, J., Otop, I., Osródk, K., and Struzik, P.: Quality-based combination of multi-source precipitation data,
587 *Remote Sensing*, 12, 1709, <https://doi.org/10.3390/rs12111709>, 2020.
- 588 Kochendorfer, J., Earle, M. E., Hodyss, D., Reverdin, A., Roulet, Y.-A., Nitu, R., Rasmussen, R., Landolt, S., Buisan, S., and
589 Laine, T.: Undercatch adjustments for tipping-bucket gauge measurements of solid precipitation, *Journal of*
590 *Hydrometeorology*, 21, 1193–1205, <https://doi.org/10.1175/JHM-D-19-0256.1>, 2020.
- 591 Kondragunta, C. R. and Shrestha, K.: Automated real-time operational rain gauge quality-control tools in NWS Hydrologic
592 Operations. 86th AMS Annual Meeting, Atlanta, GA, 28 January – 3 March 2006, 2006.
- 593 Lewis, E., Quinn, N., Blenkinsop, S., Fowler, H. J., Freer, J., Tanguy, M., Hitt, O., Coxon, G., Bates, P., and Woods, R.: A
594 rule based quality control method for hourly rainfall data and a 1 km resolution gridded hourly rainfall dataset for Great
595 Britain: CEH-GEAR1hr, *Journal of Hydrology*, 564, 930-943, <https://doi.org/10.1016/j.jhydrol.2018.07.034>, 2018.
- 596 Lewis, E., Pritchard, D., Villalobos-Herrera, R., Blenkinsop, S., McClean, F., Guerreiro, S., Schneider, U., Becker, A., Finger,
597 P., Meyer-Christoffer, A., Rustemeier, E., and Fowler, H. J.: Quality control of a global hourly rainfall dataset,
598 *Environmental Modelling & Software*, 144, 105169, <https://doi.org/10.1016/j.envsoft.2021.105169>, 2021.
- 599 Martinaitis, S. M., Cocks, S. B., Qi, B., Kaney, Y., Zhang, J., and Howard, K.: Understanding winter precipitation impacts on
600 automated gauges within a real-time system, *Journal of Hydrometeorology*, 16, 2345-2363,
601 <https://doi.org/10.1175/JHM-D-15-0020.1>, 2015.
- 602 Michelson, D.: Systematic correction of precipitation gauge observations using analyzed meteorological variables, *Journal of*
603 *Hydrology*, 290, 161–177, <https://doi.org/10.1016/j.jhydrol.2003.10.005>, 2004.
- 604 Moslemi, M. and Joksimovic, D.: Real-time quality control and infilling of precipitation data using neural networks, *EPiC*
605 *Series in Engineering (HIC 2018. 13th International Conference on Hydroinformatics)*, 3, 1457-1464,
606 <https://doi.org/10.29007/t5k7>, 2018.
- 607 Neuper, M. and Ehret, U.: Quantitative precipitation estimation with weather radar using a data- and information-based
608 approach, *Hydrology and Earth System Sciences*, 23, 3711–3733, <https://doi.org/10.5194/hess-23-3711-2019>, 2019.
- 609 Niu, G., Yang, P., Zheng, Y., Cai, X., and Qin, H.: Automatic quality control of crowdsourced rainfall data with multiple
610 noises: A machine learning approach, *Water Resources Research*, 57, e2020WR029121,
611 <https://doi.org/10.1029/2020WR029121>, 2021.
- 612 Osródk, K., Szturc, J., and Jurczyk A.: Chain of data quality algorithms for 3-D single-polarization radar reflectivity
613 (RADVOL-QC system), *Meteorological Applications*, 21, 256-270, <https://doi.org/10.1002/met.1323>, 2014.
- 614 Osródk, K. and Szturc, J.: Improvement in algorithms for quality control of weather radar data (RADVOL-QC system),
615 *Atmospheric Measurement Techniques*, 15, 261-277, <https://10.5194/amt-15-261-2022>, 2022.
- 616 Otop, I., Szturc, J., Osródk, K. and Džaków, P.: Automatic quality control of telemetric rain gauge data for operational
617 applications at IMGW-PIB, *ITM Web Conf.*, 23, 00028, <https://doi.org/10.1051/itmconf/20182300028>, 2018.



- 618 Qi, Y., Martinaitis, S., Zhang, J., and Cocks, S.: A real-time automated quality control of hourly rain gauge data based on
619 multiple sensors in MRMS System, *Journal of Hydrometeorology*, 17, 1675-1691, [https://doi.org/10.1175/JHM-D-15-](https://doi.org/10.1175/JHM-D-15-0188.1)
620 0188.1, 2016.
- 621 Rasmussen, R., Baker, B., Kochendorfer, J., Meyers, T., Landolt, S., Fischer, A. P., Black, J., Theriault, J. M., Kucera, P.,
622 Gochis, D., Smith, C., Nitu, R., Hall, M., Ikeda, K., and Gutmann, E.: How well are we measuring snow? The
623 NOAA/FAA/NCAR winter precipitation Test Bed, *Bulletin of the American Meteorological Society*, 93, 811-829,
624 <https://doi.org/10.1175/BAMS-D-11-00052.1>, 2012.
- 625 Savina, M., Schappi, B., Molnar, P., Burlando, P., and Sevruk, B.: Comparison of a tipping-bucket and electronic weighing
626 precipitation gauge for snowfall, *Atmospheric Research*, 103, 54-51, <https://doi.org/10.1016/j.atmosres.2011.06.010>,
627 2012.
- 628 Scherrer, S. C., Frei, C., Croci-Maspoli, M., van Geijtenbeek, D., Hotz, C., and Appenzeller C.: Operational quality control of
629 daily precipitation using spatio-climatological plausibility testing, *Meteorologische Zeitschrift*, 20, 397-407,
630 <https://doi.org/10.1127/0941-2948/2011/0236>, 2011.
- 631 Sevruk, B.: Adjustment of tipping-bucket precipitation gauge measurements, *Atmospheric Research*, 42, 237-246,
632 [https://doi.org/10.1016/0169-8095\(95\)00066-6](https://doi.org/10.1016/0169-8095(95)00066-6), 1996.
- 633 Sevruk, B. and Nevenic, M.: The geography and topography effects on the areal pattern of precipitation in a small prealpine
634 basin, *Water Science and Technology*, 37, 163-170,1998.
- 635 Sevruk, B., Ondras M., and Chvila B.: The WMO precipitation intercomparisons, *Atmospheric Research*, 92, 376-380,
636 <https://doi.org/10.1016/j.atmosres.2009.01.016>, 2009.
- 637 Shedekar, V. S., King, K. W., Fausey, N. R., Soboyejo, A. B. O., Harmel, R. D., and Brown, L. C.: Assessment of measurement
638 errors and dynamic calibration methods for three different tipping bucket rain gauges, *Atmospheric Research*, 178, 445-
639 458, <https://doi.org/10.1016/j.atmosres.2016.04.016>, 2016.
- 640 Sieck, L.C., Burges, S. J. and Steiner, M.: Challenges in obtaining reliable measurements of point rainfall, *Water Resources*
641 *Research*, 43, W01420, <https://doi.org/10.1029/2005WR004519>, 2007.
- 642 Steinacker, R., Mayer, D., Steiner, A.: Data quality control based on self-consistency, *Monthly Weather Review*, 139, 3974-
643 3991, <https://doi.org/10.1175/MWR-D-10-05024.1>, 2011.
- 644 Szturc, J., Jurczyk, A., Ośródkka, K., Wyszogrodzki, A., and Giszterowicz, M.: Precipitation estimation and nowcasting at
645 IMGW (SEiNO system), *Meteorology Hydrology and Water Management*, 6, 3-12,
646 <https://doi.org/10.26491/mhwm/76120>, 2018.
- 647 Szturc, J., Ośródkka, K., Jurczyk, A., Otop, I., Linkowska, J., Bochenek, B., and Pasierb, M.: Quality control and verification
648 of precipitation observations, estimates, and forecasts, in: *Precipitation Science. Measurement, Remote Sensing,*
649 *Microphysics and Modeling*, Michaelides, S., edited by: Elsevier 2022, 91-133, [https://doi.org/10.1016/B978-0-12-](https://doi.org/10.1016/B978-0-12-822973-6.00002-0)
650 822973-6.00002-0, 2022.
- 651 Taylor, J. R. and Loescher, H. L.: Automated quality control methods for sensor data: a novel observatory approach,
652 *Biogeosciences*, 10, 4957-4971, <https://doi.org/10.5194/bg-10-4957-2013>, 2013.
- 653 Upton, G. and Rahimi A.: On-line detection of errors in tipping-bucket raingauges, *Journal of Hydrology*, 278, 197-212,
654 [https://doi.org/10.1016/S0022-1694\(03\)00142-2](https://doi.org/10.1016/S0022-1694(03)00142-2), 2003.
- 655 Urban, G. and Strug, K.: Evaluation of precipitation measurements obtained from different types of rain gauges.
656 *Meteorologische Zeitschrift*, 30, 445-463, <https://doi.org/10.1127/metz/2021/1084>, 2021.
- 657 Yeung, H.Y., Man, C., Chan S.T., and Seed, A.: Development of an operational rainfall data quality-control scheme based on
658 radar-raingauge co-kriging analysis, *Hydrological Sciences Journal*, 59, 1293-1307,
659 <https://doi.org/10.1080/02626667.2013.839873>, 2014.



- 660 You, J., Hubbard K. G., Nadarajah S., and Kunkel K. E.: Performance of quality assurance procedures on daily precipitation,
661 Journal of Atmospheric and Oceanic Technology, 24, 821-834, <https://doi.org/10.1175/JTECH2002.1>, 2007.
- 662 WMO-No. 8: Guide to Instruments and Methods of Observation, vol. I: Measurement of Meteorological Variables, 2018
663 edition. World Meteorological Organization, Geneva, pp. 548., 2018.
- 664 WMO-No. 305: Guide on the Global Data-processing System, 1993 edition. World Meteorological Organization, Geneva, pp.
665 199, 1993.
- 666 WMO-No. 488: Guide to the Global Observing System, 2010 edition, updated in 2017. World Meteorological Organization,
667 Geneva, pp. 215, 2017.