Water vapor stable isotope memory effects of common tubing materials

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35 **Abstract.** Water molecules in vapor can exchange with gaseous water molecules sticking to surfaces of sampling tubing, and exchange rates are unique for each water isotopologue and tubing material. Therefore, water molecules on tubing walls take some time to reach isotopic equilibrium with a new vapor isotopic signal. This creates a memory effect observed as attenuation time for signal propagation in continuous ~~laser based~~ stable water vapor isotope measurement systems. Tubing memory effects in δD and $\delta^{18}O$ measurements can limit the ability to observe

40 fast changes, and because δD and $\delta^{18}O$ memory are not identical, this introduces transient deuterium excess (D-excess, defined as $\delta D - 8* \delta^{18}O$) artifacts in time-varying observations. A comprehensive performance comparison of commonly used tubing material water exchange properties in laser-based measurement systems has not been published to our knowledge.

We compared how a large isotopic step change propagated through five commonly used tubing materials for water

45 isotopic studies, PFA, FEP, PTFE, HDPE, and copper, at two different temperatures and an air flow rate of 0.635 L min^{-1} through approximately 100 feet (~30.5 m) of ¼ in. (6.35 mm) outer diameter (OD) tubing. All commonly used tubing materials performed similarly to each other in terms of attenuation times, reaching 95 % completion in less than 45 seconds in all but 2 experiments with slight variations based on temperature. A tubing material commonly used in the early 2000's but reported to have memory effects on δD, Dekabon, was also tested at ambient

50 temperature and changing humidities. Dekabon isotopic equilibrium was not reached until nearly an hour after source transition, much later than H_2O mixing ratios equilibrated. Bev-A-Line XX (used in some soil O_2 and CO_2 gas studies) was also tested at ambient temperature~~, unheated~~, but it did not ~~approach~~reach isotopic equilibrium until after nearly six hours of testing. ~~after an hour, and we cannot recommend its use in water vapor applications.~~ Therefore, we cannot recommend the use of Bev-A-Line XX or Dekabon in water vapor isotope applications.

55 Source transition ~~switch direction~~from heavy to light or light to heavy affected isotopic transition speed only in experiments where H_2O ppm$_v$ was changing. While shorter tubing length and smaller inner diameters shortens the delay of signal propagation through the tubing, they ~~did~~don't greatly change the ~~shape of the~~ attenuation curve~~s or the delay-adjusted attenuation times~~ under these conditions for the current commonly used tubing materials tested. However, in Dekabon, attenuations curves were greatly extended with increased tubing length ~~length did matter~~.

60 Our results show that the~~se~~ current commonly-used plastic tubing materials tested were~~are~~ not inferior to copper in terms of isotopic memory under these conditions, and they are easier to work with and are less expensive than copper. ~~Our experience and results from other published studies indicate that maximizing air flow rates through the analyzer is the most effective way to minimize memory effects when accurate high frequency D-excess measurements are desired.~~

65 **1 Introduction**

In situ laser absorption spectroscopy of water vapor isotopologues has risen in use over the last two decades enabling ~~fast,~~ continuous ~~isotopic~~ measurements (Webster and Heymsfield, 2003; Lee et al., 2005; Griffith et al., 2006; Kerstel et al., 2006). All experimental setups inherently attenuate signal variability due to mixing in the analyzer optical cavities and molecular water interactions with surfaces inside the inlet and analyzer system,

70 especially when different H_2O_v concentrations lead to wetting and drying of the tubing walls. ~~The timescale for~~

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~~signal attenuation can vary greatly based on a~~A wide range of tubing materials, air flow rates, temperatures, and pressures have been used which may result in different timescales for signal attenuation (Sturm and Knohl, 2010; Griffis et al., 2010; Schmidt et al., 2010; Tremoy et al., 2011; Aemisegger et al., 2012; Galewsky et al., 2016). As condensation in tubing is a concern due to ~~liquid vapor~~phase change isotopic fractionation, many installations heat the tubing above ambient temperature, use a critical orifice at the tubing inlet to drop pressure in the lines, or do both ~~in order~~ to keep ~~the vapor in~~ the tubing air temperature above the dew point temperature (e.g. Griffis et al. 2010; Luo et al. 2019).

Initially~~, a plastic coated aluminum Synflex tubing (~~Synflex 1300 (also known as Dekabon or Dekoron~~),)~~ commonly used in the carbon dioxide and water eddy covariance flux community, was used in water vapor isotope ~~experiment~~observations (Lee et al., 2005; Gupta et al., 2009; Tremoy et al., 2011). Dekabon is an aluminum tape with ~~,~~ an ethylene copolymer adhesive film coated on both sides, rolled into a tube, and bonded with a high density polyethylene jacket (Goodrich Sales, Inc, 2005; New Line Hose and Fittings, personal communication, April 29, 2024). ~~I~~but it was eventually found to greatly attenuate the water isotopic signals (Sturm and Knohl, 2010; Griffis et al., 2010; Schmidt et al., 2010; Tremoy et al., 2011) and is no longer commonly used in water vapor isotope ~~experiments~~studies. ~~Testing in various labs has led to the adoption of plastic or metal tubing, but the details of the experiments and results are sparse (Sturm and Knohl, 2010; Griffis et al., 2010; Schmidt et al., 2010; Tremoy et al., 2011; Steen-Larsen et al., 2014).~~ Commonly used tubing material types now include copper (Steen-Larsen et al., 2014) and several types of plastic including polytetrafluoroethylene (PTFE, commonly referred to as Teflon) (Sturm and Knohl, 2010; Griffis et al., 2010), perfluoroalkoxy (PFA) (Schmidt et al., 2010; Tremoy et al., 2011), fluorinated ethylene propylene (FEP) (Luo et al., 2019), and high-density polyethylene (HDPE) (Griffis et al., 2010). Some performance testing was conducted, but the details of the experiments and results are sparse (Sturm and Knohl, 2010; Griffis et al., 2010; Schmidt et al., 2010; Tremoy et al., 2011; Steen-Larsen et al., 2014). Fluorinated polymers (FEP, PFA, and PTFE) are commonly used as transfer lines in chemical, pharmaceutical, food processing, and oil and gas industries because of their chemical- and weather-resistance, as well as their non-stick and dielectric properties (Chemours, 2018). These materials have found favor in water vapor isotope applications for the same reasons.

Air tubing choices are important because materials may have different affinities, or degree of attraction, for the isotopologues of water. This affinity causes a delay in the speed at which the isotopologue signals move through the tubing due to exchange rates with water molecules stuck to the walls, called the memory effect. The memory effect is strong~~er~~st for δD compared to $\delta^{18}O$ due to the stronger hydrogen bonding of the molecules containing deuterium slowing tubing wall exchanges (Sturm and Knohl, 2010; Griffis et al., 2010; Schmidt et al., 2010). This can result in false deuterium-excess (D-excess, defined as $\delta D - 8* \delta^{18}O$) anomalies and is important to minimize when D-excess signals are interpreted ~~in~~as ~~fast temporal-scale~~quickly changing atmospheric signals (Managave et al., 2016; Galewsky et al., 2016; Sodemann et al., 2017; Salmon et al., 2019). Some studies have suggested that ~~m~~Memory may be lessened at higher temperatures and faster air flow rates (Griffis et al., 2010; Pagonis et al., 2017).

It is important to minimize isotopic wall effects in the intake tubing lines and other in-line elements positioned before the analyzer to minimize signal attenuation. Five studies previously reporting memory effects of tubing types

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tested a maximum of three materials at a time and are summarized in Table 1 (Sturm and Knohl, 2010; Griffis et al., 2010; Schmidt et al., 2010; Tremoy et al., 2011; Steen-Larsen et al., 2014). Most concluded that Dekabon was not suitable for water isotope applications but varied in which tubing was preferred across applications. The National Ecological Observatory Network (NEON) selected FEP for their monitoring installations which has not been widely used in reported studies (Luo et al., 2019). In this study, we tested five of the commonly used and reported best tubing types under nearly identical conditions at two different temperatures to determine which tubing type and temperature combination results in the smallest isotopic signal attenuation. For contrast, We we also tested a tubing material known to have memory issues, Dekabon, and Bev-A-Line XX, a tubing not previously used in published water isotopes studies Bev-A-Line XX, but which is increasingly used a commonly used tubing material in soil O_2 and CO_2 gas studies (i.e. (Brecheisen et al., 2019).); Nnote that thisBev-A-Line XX has a patented Hytrel® inner lining and is distinct from is not Bev-A-Line IV which has been used in a few published water vapor isotope studies (Lee et al., 2005; Simonin et al., 2013; Havranek et al., 2023)(cite). . Bev-A-Line XX was tested based on material availability, and has a patented Hytrel® inner lining.), and Dekabon atBecause Dekabon and Bevaline have extremely slow isotope response times, they were only tested at ambient temperature and with changing water concentrations to demonstrate the source switching in the experimental setup was working properly.

Table 1. Literature findings

Author, year	Materials Tested	Isotopes AnalyzedUsed/Goals	Result
*Schmidt et al. 2010	Stainless steel, PFA, and Dekabon	δD and δ^{18}O, Analyzer calibration	PFA better than SS. Both better than Dekabon.
*Sturm and Knohl 2010	PTFE and Dekabon	δD and δ^{18}O, Analyzer characterization	PTFE better than Dekabon
Griffis et al. 2010	"Natural colored" HDPE, Teflon (PTFE), and Dekabon	δD and δ^{18}O, δ^{18}O measurements of evapotranspiration in eddy covariance setups	HDPE equal or slightly better than PTFE. Both much better than Dekabon.
Tremoy et al. 2011	PFA and Dekabon	δD, δ^{18}O, and D-excess, Analyzer characterization and D-excess measurements	PFA better than Dekabon
*Steen-Larsen et al. 2014	Copper, stainless steel, and PTFE	δD, δ^{18}O, and D-excess, environmental controls on D-excess measurements	Copper better than SS and PTFEboth.

*Indicates experimental details and results of source-switching experiments are included in the peer-reviewed published materials.

2 Methods

In this study, we tested PFA, FEP, PTFE, HDPE, and copper at ambient and elevated temperatures using self-regulating heat tape. We switched between two isotopically distinct vapor sources to examine memory effects during water vapor stable isotope measurementsof each material. We also tested Bev-A-Line XX and Dekabon at ambient temperature and at two varying humidities.

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2.1 Analyzer

A Los Gatos Research, Inc. (LGR) Triple Water Vapor Isotope Analyzer (TWVIA) Off-Axis Integrated-Cavity-Output Spectroscopy system (OA-ICOS) was used for testing. An external pump (KNF pump, model N920-2.08) was added to the TWVIA to maximize the turnover rate of air inside the analyzer. The TWVIA itself regulates the outflow to maintain a constant internal pressure, resulting in discontinuous (jumpy) flow rates which averaged 0.635 ± 0.006 L min^{-1} at STP~~The air flow rate through the analyzer was 0.635 ± 0.006 L min^{-1}~~ with a cell pressure o~~run in standard mode~~ at ~40 Torr. This result~~ing~~ed in an ~ 4 second mean residence time of sample air in the analyzer. It is typical to average data over an optimum time interval determined by Allan variance testing to minimize analyzer noise and maximize measurement precision. In this experiment, the objective was to maximize the analyzer response time in order to resolve potential differences in isotopic signal attenuation during travel through inlet tubing. Applying a running mean to the 1-Hz data would have smoothed the response, masking the signal of interest in this study. Measurement uncertainty was estimated using two second Allan deviation which is the lowest time limit of the Allan deviation code output (Guerrier et al., 2020). ~~The analyzer precision was characterized over 18 hours at approximately 9,300 ppm WVISS produced vapor.~~ The Allan deviation at two seconds for δD and δ^{18}O measured over 18 hours at approximately 9,300 ppm ~~(produced by the WVISS, discussed in Sect. 2.2.1)~~ produced by a Los Gatos Research Water Vapor Isotope Standard Source (WVISS) was approximately 1.3 ‰ and 0.6 ‰, respectively, propagating to D-excess precision better than ± 3.3‰ ~~(Guerrier et al., 2020). In order to preserve the attenuation curve resolution, no running mean was applied to the δD and δ^{18}O data. However, a two second averaging interval is the lowest time limit of the Allan deviation code output (Guerrier et al., 2020), so two second averaged Allan deviation values are reported.~~ To demonstrate this analyzer performance is ~~consitent~~consistent with other published studies, the full~~An~~ Alla~~e~~n deviation plot of ~~WVISS sourced~~ analyzer variance (Fig. S1~~, Guerrier et al., 2020~~) ~~using the same WVISS-produced vapor estimates a two second averaged D-excess precision better than ± 3.3 ‰, and a 10 s average better than ± 1.0 ‰.~~

2.2 Experimental Setup

2.2.1 H$_2$O ~~matching~~matched~~mated~~ experiments

The memory effect of the tubing material was tested by switching between two sources of moist air with different isotopic values but nearly identical water vapor mixing ratios (~9,200 ppm, Table S1). A LiCor model LI-610 portable dew point generator (DPG) was used to create a vapor of approximately -187 ‰ δD, -25.~~5~~6 ‰ δ^{18}O, and 17.~~5~~4 ‰ D-excess, measured by the LGR ~~analyzer~~TWVIA without calibration, from water at 5°C. The second vapor of approximately -3~~21.8~~2 ‰ δD, -5.~~8~~7 ‰ δ^{18}O, and 14.~~0~~ ‰ D-excess was produced by ~~the~~ a Los Gatos Research Water Vapor Isotope Standard Source (WVISS~~)~~, also measured by the analyzer without calibration. DPG-generated vapor isotopic values for the experiments became isotopically enriched over time as water evaporated from the liquid reservoir. Isotopic δD and δ^{18}O transitions were normalized to a 1 to 0 scale to compare across experiments and adjust for small source water and analyzer drift over time. For this reason, further ~~calibration of the isotopic measurements listed above~~ was not needed. Five replicate switches were completed for each experiment where the vapor sources switched approximately every 60 minutes giving sufficient time to reach a new isotopic

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equilibrium. We focus on present data through the first 20 minutes as equilibrium was already established (with the exception of Dekabon and Bev-A-Line XX Bev-A-Line XX).

170   For each experiment, the WVISS programming and internal valve system controlled the switching between the DPG output connected to the WVISS inlet port and the WVISS (Fig. 1) output to the TWVIA. The WVISS was connected to the analyzer by approximately 100 foot (~30.5 m, lengths listed in Table S1) long sections of $^1/_4$ in. (6.35 mm) outer diameter (OD) test tubing for the main experiments. The Swagelok connection to the analyzer included an extra stainless steelstainless-steel union and ~2.5 in. (~6.4 cm) thick-walled FEP to protect the analyzer

175   bulkhead union threads from wear during the experiment, but this addition is not expected to affect the results significantly. Sensitivity to tubing length and inner volume were investigated Other tests were done withusing a short (62 in. or 1.57 m) and a long (99 feet $^1/_2$ in. or 29.75 m) piece of thick-walled FEP to quantifyand long piece of thin-walled FEP sensitivity to tubing length and inner volume. Tubing inner diameters (ID, summarized in Table S1) were $^3/_{16}$ in. (~4.76 mm) with the exception of HDPE and thick-walled FEP, which were $^1/_8$ in. (~3.18 mm) ID.

180   DamagedThe thin-walled FEP tubing was pieced togetherrepaired using three stainless steel Swagelok unions and the Dekabon with one, but this is not expected to affect the results significantly.

Tubing and self-regulating heat tape (EASYHEAT ADKS-0500, 100 foot (~30.5 m) roof and gutter de-icing kit) were wrapped in either flexible foam tape (HDPE, PTFE, thick-walled FEP; AP/Armaflex TAP 18230 insulation tape) or rigid foam pipe insulation (copper, thin-walled FEP, PFA; Tundra brand $^1/_2$ in. or 1.27 cm wall). The

185   thermocouple probe was placed inside the insulation on the side of the tubing opposite of the heat tape, about three inches (~7.6 cm) from the end closest to the analyzer inlet. A datalogger recorded the average temperature over the ~10 hour experiments. During heated tubing tests, the tubing was allowed to warm up at least an hour prior to measurements to let the tubing moisture equilibrate to the elevated temperature and minimize the effects of degassing water molecules adhered to the tubing from previous experiments. Differences in the insulation properties

190   of the two materials used and likely differences in thermocouple placement relative to unavoidable internal gradients in temperature resulted in differences in average temperatures for each experiment, ranging from 48.6 to 75.2 °C (Table S1). We note that this heating design is commonly used in field conditions and represents likely inlet conditions. However, the lack of uniform temperature control leads to potential temperature-induced differences that are hard to quantify. All heated experiments (average 60 ± 8 °C) are significantly warmer than ambient temperature

195   experiments (average 24 ± 1 °C). Dekabon was only tested under ambient conditions and thus was not insulated.

An external pump (KNF pump, model N920-2.08) was added to the TWVIA to maximize the turnover rate of air inside the analyzer. The TWVIA itself regulates the outflow to maintain a constant internal pressure, resulting in discontinuous (jumpy) flow rates which averaged 0.635 ± 0.006 L min⁻¹. This air flow rate led to an analyzer mean residence time (referred to as residence time) of 3.97 s. Temperature adjusted tubing residence times were 1.0 ±

200   0.109 s for short thick-walled FEP, 19.7 ± 1.6 s for long thick-walled tubing (FEP and HDPE), and 445.52 ± 23.05 s for long thin-walled tubing (FEP, PFA, PTFE, and copper). The test tubing was placed between the WVISS and the TWVIA. Switching between constant isotopic sources, WVISS and DPG, was controlled by the LGR software and valves inside the WVISS unit. Uncertainties in tubing residence time (a few seconds) based on length (a couple inches) and temperature (due to internal gradients and overall temperature fluctuations) were not considered here.

Air flow rates through the tested tubing were controlled by the TWVIA itself, making the tubing flow rate as slow as possible and the analyzer flow rate as fast as possible with this set of equipment. The DPG was operated in a continuous fashion, constantly generating humid air. To maintain these constant conditions, a vent was added before the DPG outlet to the WVISS inlet to provide an overflow when the WVISS was pushing its humid air stream to the TWVIA, otherwise the DPG pump would be pushing against a closed valve. A Dwyer rotameter (model number VFB-65-SSV) was used to monitor outflow from the vent. This vent air flow rate is not critical to the tubing tests because it's simply the overflow. An Omega mass flow meter (MFM, 0–30 L min^{-1} range, model FMA1826A) was used to monitor air flow rates downstream of the TWVIA to verify analyzer conditions remained unchanged during the experiments. A Mesa Labs Bios Definer 220 primary flow calibrator (Mesa Labs, Lakewood, CO, 50–5,000 sccm, accuracy ± 1 % of reading) was used to validate the air flow rate through the TWVIA and test tubing at the inlet of the TWVIA prior to the experiments but was not included during the actual experiments. When the primary flow calibrator was removed, no change in the TWVIA outlet flow was detected on the Omega MFM. Rotameter flow rates were verified at the beginning of the experiments using the primary flow calibrator. The DPG vent flow rate was ~0.9 L min^{-1} when the DPG was sampled by the TWVIA and ~1.5 L min^{-1} when the WVISS was sampled, consistent with the 0.6 L min-1 flow rate of the analyzer.
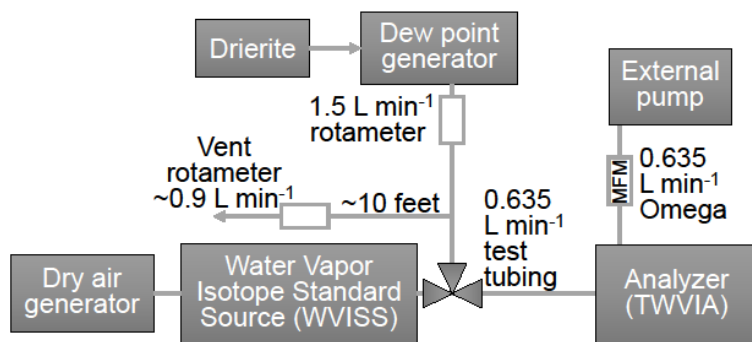
Figure 1. Instrument setup for memory effect tests. The WVISS controls switching between WVISS air and dew point generator air (depicted here as an external 3-way valve, but it's internal to the WVISS), which is passed through test tubing of up to 100 ft and either heated or unheated to the analyzer. The flow through the test tubing is controlled by the analyzer.

2.2.2 H$_2$O ~~varying~~varied experiments

For this set of experiments, the plumbing and flows remained the same. The only difference was this time the two different isotopic sources also had different water vapor mixing ratios (Table S1). The DPG was used to create a vapor of approximately -184 ‰ δD, -26.2 ‰ δ^{18}O, 25.4 ‰ D-excess, and ~9,300 ppm$_v$ H$_2$O, measured by the LGR TWVIA without calibration, from water at 5°C. The second vapor of approximately -20.3 ‰ δD, -8.8 ‰ δ^{18}O, 50.4

‰ D-excess, and ~16,950 ppm_v H_2O was produced by the WVISS, also measured by the analyzer without calibration. Because data was normalized as above, calibration was not necessary to determine attenuation times. Two to four replicate switches were completed for Dekabon and HDPE tubing depending on the time to reach the new isotopic equilibrium. One replicate of Bev-A-Line XX was run in each direction of the switch, and results are presented in Fig. S2. Replicate five minute switches comparing the performance of Bev-A-Line XX and HDPE can also be found in Fig. S3.

For each of the H_2O varying experiments, source switching was controlled manually as the TWVIA control of the WVISS unit malfunctioned. The WVISS was connected to the analyzer by approximately 100 foot (~30.5 m, lengths listed in Table S1) long sections of $^1/_4$ in. (6.35 mm) outer diameter (OD) HDPE, Bev-A-Line XX, or Dekabon tubing. Other tests were done with a short (~78.7 in. or 2 m) section of each tubing to quantify sensitivity to tubing length and inner volume using high memory materials. Tubing inner diameters (ID, summarized in Table S1) were 0.17 in. (~4.32 mm) with the exception of HDPE, which was $^1/_8$ in. (~3.18 mm) ID. These experiments were conducted under ambient conditions (average 24 ± 1 °C). Temperature adjusted tubing residence times were 2.8 s for short Bev-A-Line XX and Dekabon, 42.2 s for long Bev-A-Line XX and Dekabon, and 1.5 s and 22.8 s for short and long HDPE, respectively. All other experimental aspects remain the same as detailed in Sect. 2.2.1.

2.3 Data Processing

Isotopic values were measured at 1 Hz. No calibration to assign values to the international scale was performed on the isotopic measurements because the transitions were normalized to their starting and ending equilibrium values, resulting in signal transitions from 0 to 1. Isotopic measurements made with this analyzer are known to vary with water mixing ratio and potentially drift over long periods of time. Normalizing the measurements between sources as described below removed any potential influence of instrument or source drift over periods of more than 20 minutes.

For δD and $\delta^{18}O$, the individual transitions were normalized from 1 to 0 and then replicates were averaged to characterize the transition memory and uncertainty. Initial δ values (normalized to one) were either the maximum δ value after the source switch indicator in the data file (short thick FEP and long Bev-A-Line) or the average of 5 seconds on either side of that maximum δ value (for all other experiments). Final δ values (normalized to zero) were the average of measurements 600–1200 seconds after the source switch in H_2O matched experiments.

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Diverse experimental lengths were usedneeded during the H_2O varyingvaried experiments, with lengths ranging from 336–31,001 s depending on time to equilibrium (Table S1). This resulted in final δ values ("0") set as the average of measurements the lastat least the last 50 , 100, or 1000 seconds after the source switch, depending on
270   time to equilibrium and length of the experiment (see -Table S1 for exact intervals used to average). . during the lag interval before the signal transition reaches the analyzer.D-excess was calculated as $\delta D – 8* \delta^{18}O$. D-excess was not normalized in the same way as δD and $\delta^{18}O$ because the shape of the attenuation curve is different. A 10 s running mean was applied, and the 5 replicates were averaged to reduce noise. Replicates were screened based on successful WVISS-to-DPG and DPG-to-WVISS switching and consistent water vapor mixing ratios ensuring that vapor source
275   generators were operating properly. Only one replicate was discarded from the heated PFA experiment due to water mixing ratio variability from the WVISS. We calculated the average D-excess value over 600–1200 seconds after the source switch in H_2O matchingmatcheded experiments, and the timespan the final δ values were averaged over (the last 50, 100, or 1000 s) in the H_2O varyingvaried experiments. andThis average was then subtracted that value from all data points within a replicate to adjust for small changes in D-excess source waters between replicates,
280   especially in the DPG vapor which undergoes evaporative enrichment and D-excess decrease. These timespans 600–1200 seconds after the source switch (600–1200 s for H_2O matchingmatched and the last 50, 100, or 1000 s for H_2O varyingvaried experiments) visually appear to be conditions of tubing equilibration and were used to calculate source vapor sample averages given in Table S1 and summarized in Sect. 2.2. Replicates were screened based on successful WVISS-to-DPG and DPG-to-WVISS switching and consistent water vapor mixing ratios ensuring that
285   vapor source generators were operating properly. Four replicates were discarded from the collected data due to water mixing ratio variability from the WVISS. These discards include one replicate each from heated PFA and 100' Dekabon H_2O matchingmatched experiment, and two from the 100' HDPE H_2O varyingvaried experiment.

When comparing experiments between different tubing lengths and IDs, differences in the internal volume result in different tubing residence times due to advection. The flow in all experiments was estimated to be laminar with
290   Reynold's numbers calculated between 579 and 870. In Sect. 3.1 we will describe how the experiments are advection delay-adjusted to compare transitions directly.

Memory analysis included both directions of the isotopic switch. Isotopically enriched-to-depleted (WVISS-to-DPG) figures are presented in the main body of the text, and isotopically depleted-to-enriched (DPG-to-WVISS) transitions are available in the supplemental information (Fig. SS43, and S5, S6, and S74). While Aemisegger et al.
295   (2012) found the enriched-to-depleted switch exhibited longer attenuation times, this was likely due to the change in water vapor mixing ratio of the sources in their experiment which did not occur here.

2.4 Memory Quantification

Memory effects can in some respects beare analogous to a low-pass filter, smoothing high frequency variability
300   (e.g. Zannoni et al., 2022). Previous studies have approximated the smoothing of a fast step-change input as an exponential transition and report a threshold time to some percentage of completion like an e-folding (63 %), 90 %, or 95 % (Sturm and Knohl, 2010; Schmidt et al., 2010; Aemisegger et al., 2012; Steen-Larsen et al., 2014). In some

cases, the threshold metrics were obtained from the data directly (Sturm and Knohl, 2010; Steen-Larsen et al., 2014) and in others it appears an exponential function was fit to the data first and the metrics were extracted from the fit (Schmidt et al., 2010; Aemisegger et al., 2012). A second method used in the literature takes the first derivative of the normalized transition (Steen-Larsen et al., 2014) and characterizes an impulse response function using curve fitting (Jones et al., 2017; Kahle et al., 2018). We have quantified memory effect metrics using both methods.

2.4.1 Threshold metrics

We extracted attenuation threshold metrics directly from the normalized and replicate-averaged data (not an exponential fit). An e-folding time corresponds to $\tau = 1/e$ of the signal transition remaining to reach a new value. In this study, we have chosen to estimate attenuation threshold times at 1τ (~63 %) and 3τ (~95 %) completion of the switch to the next δD and $\delta^{18}O$ value, denoted as $t_{63\%}$ or $t_{95\%}$ respectively (Schmidt et al., 2010). These t values are the time the averaged curve intersects the threshold percent value. We chose not to fit exponential curves to extract an e-folding time, because the measured attenuation curves were not accurately described by an exponential curve (not shown). The 1 standard deviation envelope was calculated by taking the standard deviation of the 2-55 replicates at each time step. Errors associated with attenuation threshold times were determined by finding the time that the 1 standard deviation envelope of the averaged replicates intersects the completion threshold. Because the analyzer measures in discrete 1 s intervals, the raw $t_{63\%}$ and $t_{95\%}$ value outputs the next second from where the averaged curve intersects the threshold percent value. This leads to slight differences in $\delta^{18}O$ location adjusted $t_{63\%}$ and $t_{95\%}$ values (discussed in Sect. 2.4.2) compared to the sweepout curves presented in Sect. 3.

D-excess signals of the source transitions are not unidirectional and memory must be quantified differently. Previous studies reported that δD signals take longer to equilibrate with the surface of tubing materials compared to $\delta^{18}O$ signals due to isotopic effects of hydrogen binding with the tubing walls (Sturm and Knohl, 2010; Griffis et al., 2010; Schmidt et al., 2010; Aemisegger et al., 2012). The D-substituted hydrogen-bonds exchange with the vapor more slowly. This difference leads to a D-excess transition that has a transient anomaly until the δD signal propagation catches up to the $\delta^{18}O$ signal. The direction of the D-excess transient peak depends on the direction of the isotopic signal switch. In the enriched-to-depleted transition, the enriched δD signal is retained on the tubing walls creating a transient, positive anomaly in D-excess while approaching equilibrium. However, in a depleted-to-enriched transition, the depleted δD signal has been preserved on the tubing walls creating a negative D-excess anomaly during isotopic equilibration. The absolute value of the maximum transient peak was identified and associated errors are given as the standard deviation of the replicate D-excess values at the time of the maximum peak (Table S2). The threshold chosen to measure completion in D-excess transitions is a 3 ‰ threshold within the new equilibrium value ($t_{3‰}$). determined by the average over 600–1200 s. This threshold is a conservative estimate of analyzer precision of D-excess measurements if δD precision was 1.0 ‰ and $\delta^{18}O$ precision was 0.25 ‰.

To compare the attenuation threshold times across experiments, we adjusted for differences in signal propagation due to the time it takes air to move through the tubing from the WVISS and mixing inside the analyzer, controlled by the air flow rate through the instrument, optical cavity size, test tubing volume, and air flow rate (Schmidt et al., 2010), as well as temperature. Smaller tubing IDs, increased temperature, and shorter tubing lengths

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faster tubing and analyzer air flow rates, and shorter tubing lengths tested here will all shorten lag times associated with a measurement. Lδ¹⁸O lag times were calculated via breakpoint analysis to determine the point where slope changes. We created a linear model using the first 300 s (30 s for short thick-walled FEP tests) of data after the source switched, then utilized the "segmented" function in R's "segmented" package on the time series (Muggeo, 2022). The breakpoint lag estimates likely have an error of a few seconds. The exact uncertainty was not quantified. Average measured lag times for 100 foot (~30.5 m) thin-walled tubing were 53 s, and 1.5 s for the short thick-walled tubing in the H_2O matcheding experiments. In the results, the time axis in the plots and quantitative threshold metrics ($t_{63\%}$, $t_{95\%}$, and $t_{3‰}$) in the tables were adjusted by fitted location δ¹⁸O timelocation time (discussed in Sect. 2.4.2).

2.4.2 Impulse response method

In the impulse response method, we take advantage of the first derivative of the observed attenuation curves to clearly identify the timing and rates of change. To decrease the noise in the first derivative, it's necessary to reduce noise in the observed attenuation curves. In previous studies, noise reduction is achieved by fitting a smooth transfer function to the observations. Jones et al. (2017) and Kahle et al. (2018), used a lognormal times lognormal (log-log) function to fit the data, while in Steen-Larsen et al. (2014) only one lognormal is used. For our attenuation curves, neither a single or double lognormal fit the observed data well. Our data was most accurately recreated by a transfer function of the form in Eq. (1) (with the exception of the depleted-to-enriched transition for H_2O matched HDPE, H_2O varied depleted-to-enriched 2 m HDPE, and enriched-to-depleted Dekabon in both sets of experiments where an additional normal fit was added):

$$\delta_{transfer}(t) = c_1 * \left[1 + erf\left(\frac{log(t)-\mu_1}{\sigma_1\sqrt{2}}\right)\right] * \left[1 + erf\left(\frac{log(t)-\mu_2}{\sigma_2\sqrt{2}}\right)\right] * \left[1 + erf\left(\frac{t-\mu_3}{\sigma_3\sqrt{2}}\right)\right] + c_2 \tag{1}$$

where t is time since switching, σ is the location of each log/normal, μ is the standard deviation of each log/normal, and c_1 and c_2 are scaling factors. The values of σ_1, σ_2, σ_3, μ_1, μ_2, and μ_3 are optimized by minimizing the squares of errors using the "DEoptim" global optimization function in the R package of the same name (Ardia et al., 2022). The form of the fitting model here is not that important as long as the observations are faithfully reproduced in the smooth curve fit, as seen in Fig. 2a.

Once a transfer function is fit, the first derivative of the transfer function is calculated to obtain the impulse function. We fit the impulse function by the model in Eq. (2) based on a skew-normal function added to a normal gaussian function.

$$\delta_{impulse}(t) = \left(c_1 * \left[\left(\frac{1}{\sqrt{2\pi}}\right) * e^{\frac{-x_1^2}{2}}\right] * \left[\frac{1}{2} + erf\left(\frac{x_1 * \alpha}{\sqrt{2}}\right)\right]\right) + \left(\left[\left(\frac{1}{\sqrt{2\pi}}\right) * e^{\frac{-x_2^2}{2}}\right] * c_2\right) \tag{2.1}$$

$$x_1 = \frac{(t-\xi)}{\omega} \tag{2.2}$$

$$x_2 = \frac{(t-\mu)}{\sigma_m} \tag{2.3}$$

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where in the skew-normal terms, ξ is the location of the maximum impulse peak, α is shape, and ω is scale, t is time since switching, σ_m is the standard deviation of the additional PDF and μ is its mean, and c_1 and c_2 are scaling factors. The parameters are solved for using a two-step method: first using the "DEoptim" function (Ardia et al., 2022) to provide an approximate initial guess, and second utilizing the "nls" non-linear least squares function in the "stats" R package of base R (R Core Team, 2023) to provide parameter fine-tuning and uncertainty estimates of each parameter.

While Jones et al. (2017) was able to fit impulse functions of their data solely with a skew-normal PDF fit (a standard normal probability distribution function times a standard normal cumulative distribution function, or PDF * CDF), we most accurately reproduced the first derivative by adding an extra PDF in Eq. (2). Figure 2b shows a comparison of the Jones et al. (2017) impulse function skew-normal fit compared to the impulse function fit we used in this study. Our impulse function model fits the memory tail in our experiments better than the skew-normal PDF model from Jones et al. (2017).
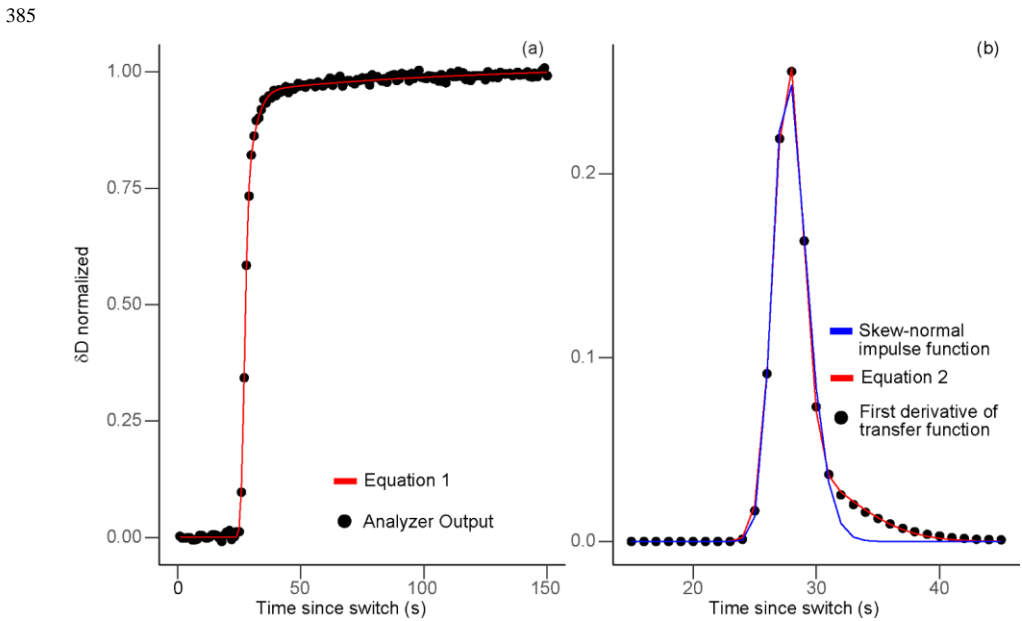

Figure 2. Example of model function fits for the unheated long thick-walled FEP experiment. Panel (a) compares normalized and averaged analyzer output (black dots) with the transfer function given in Eq. (1) (red line). Panel (b) compares the impulse function derived from the first derivative of the transfer function fit evaluated every second (black dots), with the fit from Eq. (2) (red line) and the skew-normal impulse function (blue line) used in Jones et al. (2017) and Kahle et al. (2018).

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We extracted two memory metrics from the impulse fitting. First, the skew-normal parameters of shape (α, a descriptor of the shape of the curve or other asymmetry of the distribution) and scale (ω, a measure of the spread of the distribution) were used to estimate a mixing time (σ_s) from Eq. (3). This metric has also been called mixing length in Jones et al. (2017) or diffusive length in Kahle et al. (2018) where analysis time relates distance in the ice cores. The σ_s is a metric of how much mixing occurs due to diffusive flow within the tubing. Error for σ_s is propagated from the errors associated with shape and scale. Second, we also estimate the standard deviation of the additional PDF (σ_m) in Eq. (2) critical for fitting the memory tail in the observations which gives additional information about memory not captured by the skew-normal curve.

$$\beta = \frac{\alpha}{\sqrt{1+\alpha^2}} \tag{3.1}$$

$$\sigma_s^2 = \omega^2 * (1 - \frac{2\beta^2}{\pi}) \tag{3.2}$$

$$\sigma_s = \sqrt{\sigma_s^2} \tag{3.3}$$

3 Results

3.1 Comparison of residence, lag, and location times in H₂O matchingmatched experiments

The residence timee of air in the inletssystem areis mathematically predicted using the tubing ID, length, temperature, pressure within the tubing, and air flow rate through the tubing (Table S2). Residence times are decreased by decreasing the tubing length and inner diameter or increasing temperature and air flow rates through tubing and analyzer, as tested here. Average $\delta^{18}O$ lag times from breakpoint analysis correlate well with predicted residence times (Fig. S82a). For the long thick-walled tubing, the calculated residence time is approximately 19.7 ± 1.6 s, with slight variations due to temperature and small length differences which agrees well with observed $\delta^{18}O$ lag of 23.1 ± 1.2 s. For long thin-walled tubing, the calculated residence time is approximately 454.52 ± 32.05 s, and average $\delta^{18}O$ lag time is 53.0 ± 4.0 s (not including Dekabon, due to instrument malfunction). The largest discrepancies between residence and $\delta^{18}O$ lag times (< 12.5 s, with the exception of Dekabon) are found in unheated copper and unheated PFA. Tubing roughness was not considered when calculating residence times, as flow was assumed to be laminar and flow rate was measured at the end of the tested tubing closest to the analyzer and therefore should be representative the actual flow rate in the tubing. For short thick-walled FEP, the residence time is 1.0 ± 0.109 s and average $\delta^{18}O$ lag time is 1.5 ± 1.7 s. Overall, heated tubing lag and residence times were shorter than their unheated counterparts (Table S2).

Similarly, the location time parameter fitted using the impulse response method is the timing of the maximum peak of the impulse function (or the steepest portion of the attenuation curve, discussed in Sect. 2.4.2). The location time is sensitive to the advection lag and the steepness of the isotopic transition. Our estimated $\delta^{18}O$ location time for the long thick-walled tubing (25.6 ± 1.3 s, Table S2, excluding Dekabon) matches the $\delta^{18}O$ lag time above when accounting for the < 5 seconds between the initial signal change and the maximum slope of the attenuation curve (or

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peak in the impulse function). Because of this relationship, $\delta^{18}O$ location times correlated well with the observed $\delta^{18}O$ lag times (Fig. S~~2~~8b) and residence times (Fig. S8c) and are nearly identical to the ~~unadjusted~~ $t_{63\%}$ estimates from the experiments as well (Fig. S~~8~~2d~~e~~, excluding Dekabon). The differences in location time between different tubing experiments is not fully explained by differences in residence time predictions. The location time extracted from the δD impulse function is slightly longer than the location time extracted from the $\delta^{18}O$ impulse function, but they correlate well (Fig S8d). Dekabon δD location time is comparatively much longer (~30–50 s longer) than the $\delta^{18}O$ location time (Table S2). ~~This relative difference is consistent with the common findings that $\delta^{18}O$ d18O transitions occur faster than δDdD transitions.~~ ~~Heated experiments consistently showed a similar or shorter unadjusted $t_{63\%}$ time in δD and $\delta^{18}O$ compared to their unheated counterparts (Fig. S~~8~~2d). We suspect this is due to an increased speed of initial signal transition, as the elevated temperature has driven off some water molecules and there is less time required for full equilibration.~~ Overall, location is closely related to other methods of timing ~~"lining up"~~ isotopic transitions, including lag, residence time, and e-folding time in the tubing materials we tested, with the exception of Dekabon.

To ~~more readily identify~~visualize differences in curve shape between tubing materials tested using ~~, we adjusted the attenuation curves~~ different internal volumes (due to length and ID) and air density (due to temperature) to a common transition ~~starting~~ point was defined~~by subtracting the fitted location time~~. This is similar to adjusting ~~by~~to lag time (e.g. Steen-Larsen et al., 2014) or predicted residence times. Given uncertainties in the breakpoint analysis of lag time and tubing temperature uncertaint~~y~~s which influence residence time, we decided the $\delta^{18}O$ location time was the most ~~accurate~~self-consistent way to collapse the experiments on top of each other in the figures. Adjusting by $\delta^{18}O$ location time also allows comparison to the H_2O ~~varying~~varied and Dekabon experiments, as ~~a 'true' start time~~the valve switching time was not precisely recorded by the software.

3.2 Direction of isotopic and water vapor concentration transition~~s~~

H_2O varied and H_2O matched experiments for 100 ft (30.48 m) HDPE and Dekabon tubing~~s~~ were used to determine if there was a difference in the enriched-to-depleted and depleted-to-enriched switches due to the isotopologues or net degassing of the tubing walls (Figure 3). H_2O matched Dekabon experiments did not exhibit clear differences depending on the isotopic switch direction, while there were clear differences in δD and D-excess depending on switch direction for H_2O varied Dekabon (Fig. 3 panels a, c, and e). H_2O varied Dekabon clearly shows longer $\delta^{18}O$ location adjusted $t_{95\%}$ times in the enriched-to-depleted switch direction than the depleted-to-enriched direction. H_2O matched HDPE also does not exhibit clear differences in switch direction (Fig. 3 panels b, d, and f). H_2O varied HDPE shows a clear difference in δD ~~signal speed~~ $t_{95\%}$ between switch direction outside of $t_{95\%}$ error, but no clear difference in $\delta^{18}O$ or D-excess. Overall, differences in HDPE threshold metric values are much smaller than the differences between Dekabon values.

Impulse response metric patterns for both tubing types are mixed.

There is a difference in the H_2O varied switch direction and little to no clear and consistent difference in switch direction in H_2O matched experiments. ~~While m~~Most results presented in the following sections are H_2O matched. ~~;~~

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weWe present discuss both switch directions in the text, present figures of the enriched-to-depleted switch transition in the main manuscriptonly and place the depleted-to-enriched transition figures in the Supplemental in order to preserve space. However, results of both switch directions are discussed within the main manuscript.
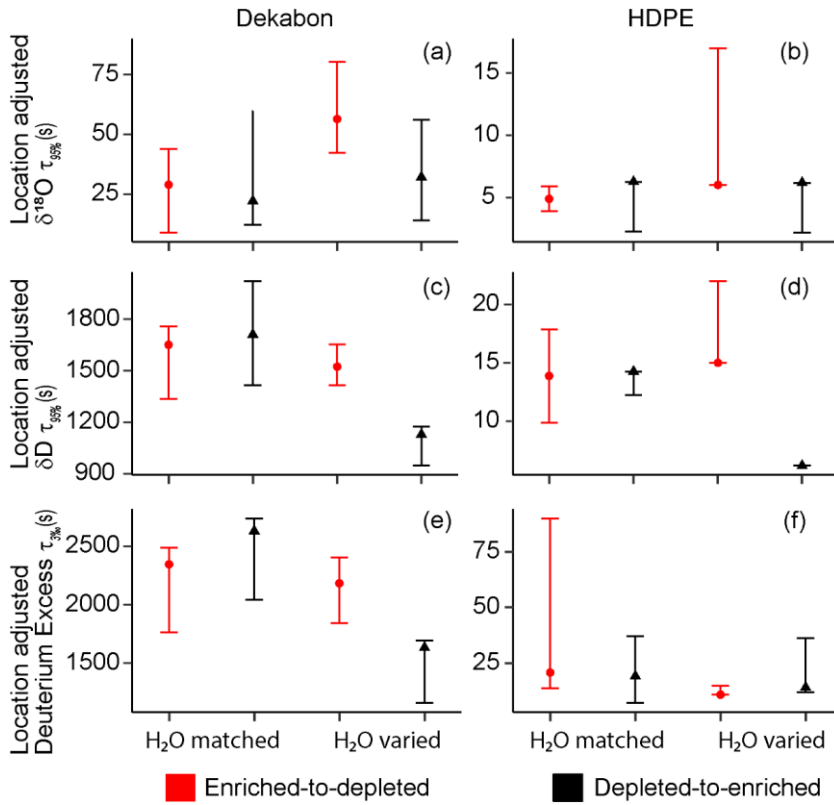
Figure 3. $\delta^{18}O$ location adjusted $t_{95\%}$ and $t_{3‰}$ times in H_2O matched and varied comparison of transition directions for long HDPE and Dekabon. The left panels (a, c, and e) depicts Dekabon tests, and the right panels (b, d, and f) depict the HDPE tests. The switch up transition, or depleted-to-enriched direction, is indicated in black. The switch down transition data, or enriched-to-depleted direction, is in red. $\delta^{18}O$We saw differences in switch direction only in H_2O varied experiments.

3.3~~2~~ ~~Visual inspection~~Tubing Material and Temperature

3.3.1 Visual inspection of mean attenuation curves

475 The mean attenuation curves for the enriched-to-depleted transitions for all H₂O matched long thin-walled tubing experiments ~~(except comparisons of short and long thick-walled FEP, HDPE, and Dekabon)~~ are compared in Fig. 4~~3~~ and the depleted-to-enriched results are in Fig. S~~3~~S4. ~~Figures~~Attenuation curves for each experiment have been adjusted by the $\delta^{18}O$ location time metric ~~in order to~~to remove the influence of different air lag times caused be different tubing IDs and temperature sensitive air density to more easily compare ~~memory tails~~equilibration times of

480 different tubing dimensions ~~of the attenuation curves~~. Therefore, 0 s in these figures indicates the time of most rapid change in the transfer function and the peak of the impulse function for each experiment. The δD signal was also $\delta^{18}O$ location adjusted to highlight potential differences in equilibration speeds between the two isotopologues. ~~Bev-A-Line XX~~Dekabon stands out as the tubing material with the longest isotopic memory in dD and d18O (Fig. 4~~3~~ and S~~3~~S4). ~~When normalized to start and end at "true" values assigned from a short thick-walled FEP test that occurred~~

485 ~~immediately prior, the Bev-A-Line XX never reached the 'true' value in either direction of the switch (Fig. 3 and S3).~~ There are slight variations within the rest of the tubing material type and temperature performances. Specifically, thin-walled FEP δD results show slower transitions compared to other tubing experiments and indicate FEP has the largest difference between d18O memory and dD memory. ~~However, this separation is due to a larger location time difference between δD and $\delta^{18}O$ for thin-walled FEP than the rest of the tubings. When adjusted for~~

490 ~~location, H~~heated experiments often appear to have a less steep δD slope and~~, when adjusted for d18O location,~~ intercept the $t_{63\%}$ metric later than unheated experiments. ~~We see this specifically in the δD signal for all tubings in the enriched-to-depleted direction with the exception of long thin-walled FEP, and for copper and PFA~~HDPE in the ~~depleted-to-enriched direction and long thin-walled FEP in both directions.~~. ~~L~~The $\delta^{18}O$ location adjusted attenuation curve~~s~~ ~~slopes~~ for $\delta^{18}O$ do not have a clear pattern in where they intercept the $t_{63\%}$ threshold ~~metric~~ in heated and

495 unheated experiments~~ later and are shallower for the heated experiments for PFA in the enriched-to-depleted direction and PTFE and copper in the depleted-to-enriched direction~~ (Fig. 4~~3~~ and S~~3~~S4).

δD attenuation times were longer ~~slower~~compared to $\delta^{18}O$. ~~Figures 4~~3~~ and S3~~S4 panels b and d also show the mean attenuation curves for the other isotopologue for direct comparison (orange curves, Dekabon excluded).~~ In the enriched-to-depleted transition, propagation of the depleted δD signal was delayed relative to the depleted $\delta^{18}O$

500 signal (as shown by the orange lines in Fig. 4~~3~~ and S~~3~~S4 panels b and d), creating a transient positive anomaly in D-excess before equilibrating with the new vapor source isotopic values. D-excess attenuation times are typically ~~much~~ longer than the $t_{95\%}$ times for δD or $\delta^{18}O$ (Table S2) while the different isotopic propagation of δD catches up to $\delta^{18}O$. ~~D~~Given differences in D-excess values between sources ~~cause, we caution overinterpreting the maximum D-excess anomalies between experiments, as evidenced by the different starting points in Fig. 4~~3~~e~~Different D-excess

505 values between experiments in Fig. 4ef are caused by D-excess drift of the DPG over the experiments.~~.

Unheated PTFE — Unheated copper — Unheated HDPE — Unheated PFA — Unheated FEP — Unheated Dekabon
Heated PTFE ∙∙∙ Heated copper ∙∙∙ Heated HDPE ∙∙∙ Heated PFA ∙∙∙ Heated FEP ∙∙∙ Other isotope average

Unheated PTFE — Unheated copper — Unheated HDPE — Unheated PFA — Unheated FEP — Unheated Bev-A-Line XX
Heated PTFE ∙∙∙ Heated copper ∙∙∙ Heated HDPE ∙∙∙ Heated PFA ∙∙∙ Heated FEP ∙∙∙ Other isotope average
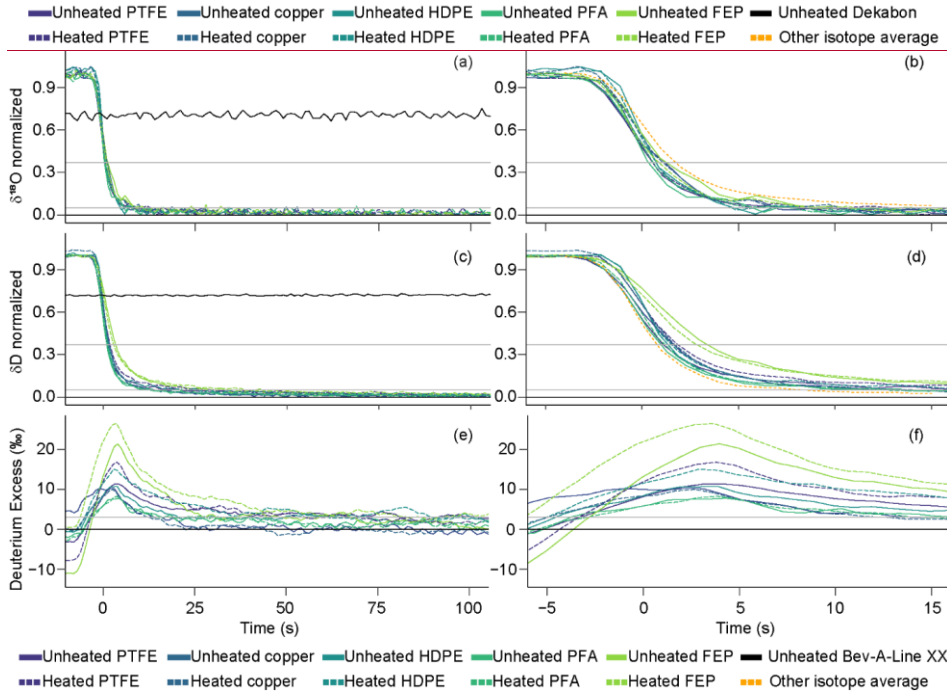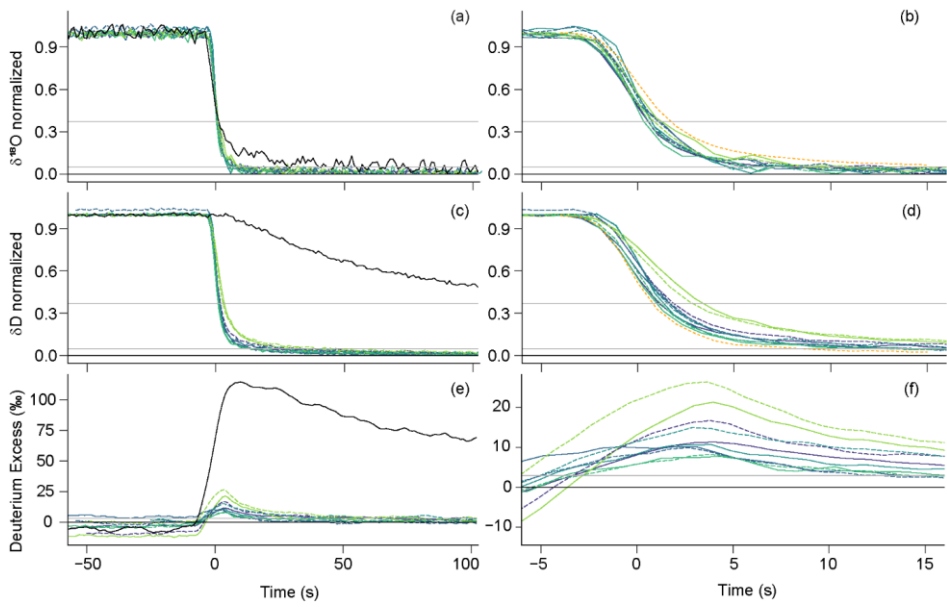
Figure 4~~3~~. Mean attenuation curves for enriched-to-depleted (WVISS-to-DPG) H_2O ~~matching~~matched transitions of each tubing type for $\delta^{18}O$ (a, b), δD (c, d), and D-excess (e, f) plotted as approximate time since source switch and $\delta^{18}O$ location adjusted. The first column (panels a, c, and e) depicts time from -50 s before the peak of the impulse function for each experiment to 100 s after, while the second column (panels b, d, and f) depicts time from -5 to 15 s and excluding the Dekabon results. Solid lines indicate unheated experiments, while dashed lines indicate heated experiments. For ~~-δD, δ18O, and D-excess in all experiments except~~only, Dekabon and FEP show clear differences in heated and unheated experiments. ~~unheated and heated tubing performances are similar with no clear optimal material or temperature under these conditions.~~ Dekabon was only tested unheated as an example of a "bad" tubing type, and Dekabon takes much longer than the rest of the tubings to equilibrate. The full Dekabon attenuation curve can be found in Fig. S9. This figure includes long thin-walled FEP as a comparison to the rest of the thin-walled tubings (all except HDPE, which is thick-walled and has a smaller ID). An orange curve in panel (b) shows mean δD for comparison with $\delta^{18}O$ in color and the orange curve in panel (d) shows mean $\delta^{18}O$ for comparison with δD in color. These means exclude Dekabon. ~~To compensate for small differences in isotopic values between experiments, δD and δ18O are normalized from 1–0 with one at the start of the source switch (measured by a valve change) and zero at the final value of the average of 600-1200 s (with the exception of Dekabon, which was the last 100 s average). D-excess is adjusted to end at 0 ‰ over the same averaging time for each experiment. transitions of five replicates of each tubing type for δ18O (a, b), δD (c, d), and D-excess (e, f) plotted as location-adjusted time since source switch. The first column (panels a, c, and e) depict time from -5 to 100 s, while the second column (panels b, d, and f) depicts time from -5 to 15 s. Solid lines indicate unheated experiments, while dashed lines indicate heated experiments. An orange curve in panel b shows mean δD for comparison and in panel d shows δ18O for comparison. To compensate for small differences in isotopic values between experiments, δD and δ18O are normalized from 1–0 with one at equilibrium with the first vapor source and zero at equilibrium with the second vapor source. D-excess is adjusted to end at 0 ‰ for each experiment.~~ Gray horizontal lines indicate thresholds of 95 % and 63 % transition completion for δD and $\delta^{18}O$, and 3 ‰ for D-excess, while a black line indicates 100 % equilibrium completion for all isotopes. ~~Bev-A-Line XX is shown in panels a and c as a black line and never reaches a normalized 0 or 1 when compared to the experiment immediately prior.~~ Depleted-to-enriched results are presented in the supplemental materials, as there were no consistent and large differences in attenuation curves between source switching directions in H_2O matched experiments.

3.3.2 Quantitative memory metrics

After $\delta^{18}O$ location adjustment, there are few consistent or large differences between heated and unheated tubings when comparing the same material (Figs. 5, S5, and Table S2). While in $\delta^{18}O$ location adjusted $t_{95\%}$ most heated tubings are similar to or slower than their unheated counterparts, in $\delta^{18}O$ location adjusted $t_{63\%}$ and σ_m, heated tubings are generally similar to or faster than the unheated~~Overall, heated memory metrics are generally either similar to or smaller~~faster ~~than those of the unheated memory metrics when comparing the same tubing types~~

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545 without δ¹⁸O location adjustment (Table S2ig. S8d), with the exception of HDPE (both directions) and depleted to enriched PTFE $t_{95\%}$ time. Overall, this pattern does not hold after δ¹⁸O location adjustment and there are few no consistent or and large differences between heated and unheated tubings when comparing the same material (Figs. 5, S5, and Table S2Figs. 4, 5, S4, and S5). While in δ¹⁸O location adjusted $t_{95\%}$ and σ_m, most heated tubings are similar to or slower than their unheated counterparts, in δ¹⁸O location adjusted $t_{63\%}$ heated tubings are generally similar to or

550 faster than the unheated. In σ_s, most signal is within error and any patterns are notthere are no consistent patterns between switching direction (Table S2). Patterns that exist tend to be clearer in δD signals as opposed to δ¹⁸O or D-excess signals. Overall, heated memory metrics are generally either similar to or smaller than those of the unheated memory metrics when comparing the same tubing types without δ¹⁸O location adjustment (Table S2), with the exception of HDPE (both directions) and depleted-to-enriched PTFE $t_{95\%}$ time.

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Each memory metric calculated provides a different order of "best" to "worst"ranking of tubing materials and temperature combinations , but these rankings are based on slight numerical differences in metric values, and all tubings appear operationally similar with the exception of Dekabon (Table S2, Figs. 5 and S5). Some common patterns in these rankings do emerge in the H₂O matched experiments. Of the tubings we calculated memory metrics

560 for, Dekabon is the worst. The rest of the tubing $t_{95\%}$ and $t_{3‰}$ times are given in Fig 5. We see clusters of tubings that are relatively faster and slower to equilibrate, specifically in the δ¹⁸O location adjustmed δD signal, illustrated in Fig. 5b. Thin-walled FEP, HDPE, and PTFE appear slightly slower to equilibrate than the rest of the tubing materials in the enriched-to-depleted direction, while PFA and copper equilibrate slightly faster. Please note that this figure also includes differences in length and inner diameter. While thick-walled FEP is presented here as a direct

565 comparison to HDPE (which is also thick-walled with a smaller ID), the rest of the materials had similar IDs to thin-walled FEP. Comparison of different dimensions of Thin-walled, thick-walled, short, and long FEP experiments are discussed in Sect. 3.4.

There are differences in relative rankings based on temperature, switch direction, and tubing material type, but these relative rankings vary depending on the memory metric used. Based on $t_{95\%}$, $t_{63\%}$, and $t_{3‰}$ times in the

570 enriched-to-depleted direction, PFA and copper appear similar to each other and slightly better than the rest of the tubing material types. However, according to most impulse response metrics (σ_s and σ_m), unheated HDPE (thick-walled) has the shortest attenuation impulse response time. PFA and copper have the longest δ¹⁸O impulse response times in the enriched-to-depleted direction after Dekabon. For D-excess, the best tubing materials in the enriched-to-depleted direction were heated copper ($t_{3‰}$) and unheated PFA (by the absolute value of the maximum D-excess

575 peak), while long thin-walled FEP was the worst for resolving D-excess signal (after Dekabon). There are differences in relative rankings based on temperature, switch direction, and tubing material type, but these relative rankings vary depending on the memory metric used. We did not calculate impulse response metrics for Bev-A-Line XX due to its inferior performance and greatly extended curve shape, but it is clearly an inferior tubing with long memory times (Fig. S2).

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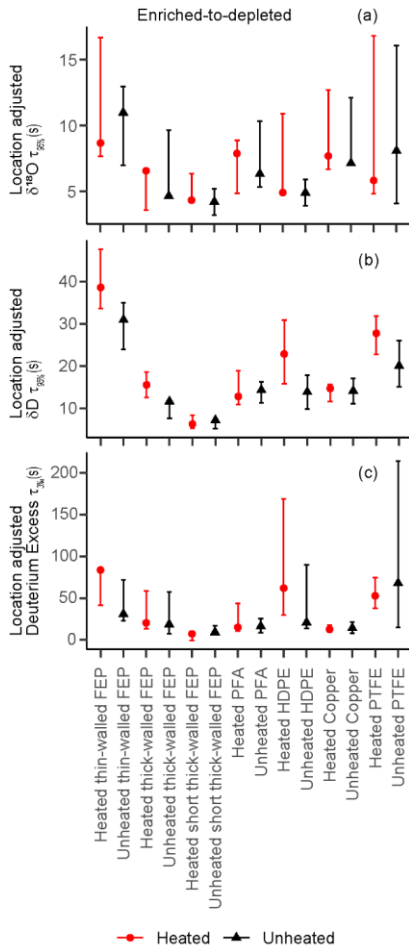
Figure 5. δ¹⁸O location adjusted $t_{95\%}$ (panels a and b) and $t_{3‰}$ (panel c) times comparing heated (red) and unheated (black) experiments for all tubing types. The enriched-to-depleted switch direction, is depicted here while the depleted-to-enriched transition data is located in Fig. S5. We did not see clear differences in tubing temperature influence, and only very small differences between tubing material type. While thick-walled FEP is presented here
585 as a direct comparison to HDPE (which is also thick-walled with a smaller ID), the rest of the materials had similar IDs to thin-walled FEP. Thin-walled, thick-walled, short, and long FEP experiments are discussed in Sect. 3.4.

We did not calculate impulse response metrics for Bev-A-Line XX due to its inferior performance and greatly extended curve shape

3.4 Tubing inner volume and length

~~When testing differences in tubing temperature and dimensions using the same material, properties~~Properties ~~affecting transit time through the tubing,~~ like tubing length _and_~~,~~ inner diameter~~, and effective flow velocities~~ affect mean the transit time through the tubing and the time it takes the signal change to reach the analyzer, but the_se_ properties~~y,~~ do not appear to greatly influence the shape of the attenuation curve after δ^{18}O location adjustment _in the FEP H$_2$O matched experiments_ (Fig. 6~~4~~ and S~~4~~S6). In these~~ matching~~ H$_2$O matched experiments, t~~T~~he short and long thick-walled tubing δ^{18}O and δD ~~signal~~transitions overlap each other (Fig. 6~~4~~b and d), ~~while~~but the long thin-walled tubing has a shallower δ^{18}O slope (Fig. 6~~4~~b) and a bigger delay between the δD and δ^{18}O signal transitions (Fig. 6d). ~~Short thick-walled FEP in general has smaller memory metrics than long thick-walled FEP, which is~~which in turn generally has smaller memory metrics than its thin-walled counterpart. _While there is not much separation between curves visually,_~~Overall,~~ ~~impulse response~~the quantitative memory~~e~~ metrics varied _varied as expected_ for δD with length and ~~volume~~inner diameter, with longer memory times for longer and larger volume tubing. _Short thick-walled FEP in general has smaller memory metrics than long thick-walled FEP, which in turn generally has smaller memory metrics than its thin-walled counterpart. Longer memory metrics were also observed for_ ~~, but were inconsistent in δ^{18}O except~~ for both switching directions of $t_{95\%}$ and in _enriched-to-depleted σ_s, although other metric differences did not consistently show this pattern._ ~~Short thick-walled FEP in general has smaller memory metrics than long thick-walled FEP, which is in turn generally has smaller memory metrics than its thin-walled counterpart.~~
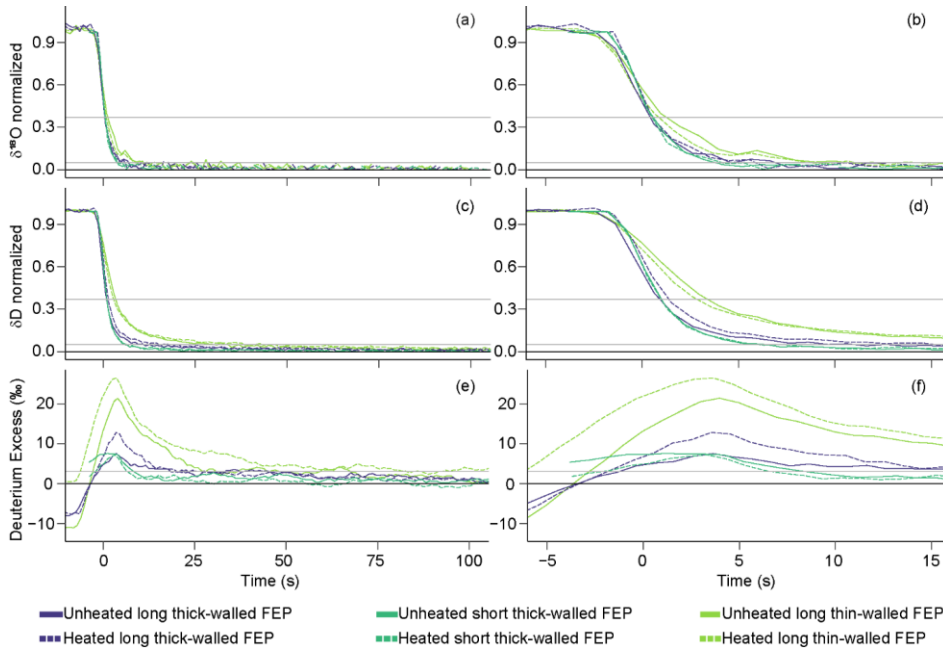
Figure 64. Mean attenuation curves for only FEP tubing for enriched-to-depleted (WVISS-to-DPG) transitions comparing tubing length and inner diameter for $\delta^{18}O$ (a, b), δD (c, d), and D-excess (e, f) plotted as $\delta d^{18}O$ location adjusted time since source switch. The first column (panels a, c, and e) depicts time from -5 to 100 s, while the second column (panels b, d, and f) depicts time from -5 to 15 s. Solid lines indicate unheated experiments, while dashed lines indicate heated experiments. To compensate for small differences in isotopic values between experiments, δD and $\delta^{18}O$ are normalized from 1–0 with one at equilibrium with the first vapor source and zero at equilibrium with the second vapor source, and D-excess is adjusted to end at 0 ‰ for each experiment. Gray horizontal lines indicate thresholds of 95 % and 63 % transition completion for δD and $\delta^{18}O$, and 3 ‰ for D-excess, while a black line indicates 100 % completion for all isotopes. The $\delta^{18}O$ location adjustment for the short tubing is much shorter than that of the long tubing, leading to a line that appears to start abruptly at ~ -3 s.

In the H_2O varied experiments, tubing length influence on the shape of the attenuation curve after $\delta^{18}O$ location adjustment depends on the tubing material (Fig.7 and S7). While in HDPE, the short and long tubing isotopic signals are similar to each other in both directions (Fig. 7 and S7, panels b and d), in long Dekabon the isotopic signal transitions are much slower than the short Dekabon in both switch directions. In long Dekabon, the much shallower δD slope (Fig. 7 and S7 panels c and d) and a bigger delay between the δD and $\delta^{18}O$ signal transitions leads to D-excess anomaly of approximately 120 ‰ (Fig. 7 and S7 panels e and f), the largest D-excess anomaly of all tubings tested. This D-excess anomaly is much smaller in short Dekabon (~40 ‰) and demonstrates the more similar signal transtions between δD and $\delta^{18}O$. Long Dekabon also has a much shallower H_2O transition slope than the rest of the

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tubings tested, including short Dekabon, which reacts more similarly to long HDPE when water vapor concentration is changed (Fig. 7 and S7 panels g and h). Overall, isotopic transitions lag H_2O transitions, as seen when comparing Fig. 7 panels b, d, and h. Short Dekabon consistently has similar or shorter memory metrics than long Dekabon. Short HDPE generally has similar or shorter memory metrics than long HDPE, with the exception of $\delta^{18}O$ enriched-to-depleted σ_m and depleted-to-enriched δD σ_k and σ_m. Again, we've effectively normalized for tubing length, volume, and temperature through the $\delta^{18}O$ location adjustment, and so differences in the attenuation curve steepness could be attributed to vapor-wall interactions that are independent of bulk flow.
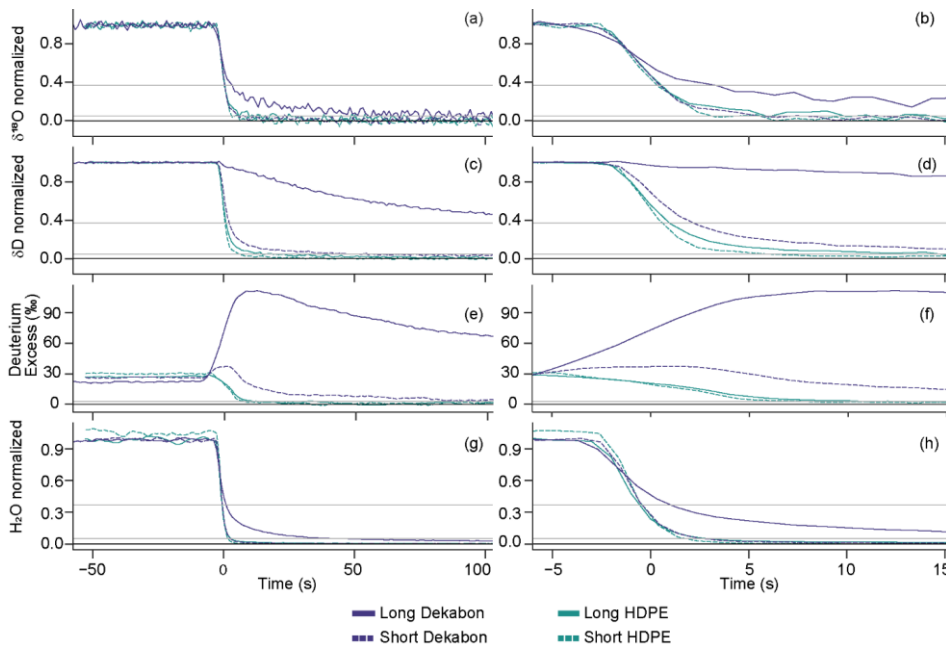
Figure 7. Mean attenuation curves comparing length for 2 m (~78.7 inches) and 100 ft (30.48 m) HDPE and Dekabon tubing for enriched-to-depleted (WVISS-to-DPG) transitions for $\delta^{18}O$ (a, b), δD (c, d)), D-excess (e, f), and H_2O (g, h) plotted as lag adjusted time since source switch. The first column (panels a, c, and e) depicts time from -50 to 100 s, while the second column (panels b, d, and f) depicts time from -5 to 15 s. Solid lines indicate 100 ft (30.48 m) lengths, while dashed lines indicate 2 m (~78.7 inches) lengths. To compensate for small differences in isotopic values between experiments, δD, $\delta^{18}O$, and H_2O are normalized from 1–0 with one at equilibrium with the first vapor source and zero at equilibrium with the second vapor source, and D-excess is adjusted to end at 0 ‰ for each experiment. Gray horizontal lines indicate thresholds of 95 % and 63 % transition completion for δD and $\delta^{18}O$, and 3 ‰ for D-excess, while a black line indicates 100 % completion for all isotopes.

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3.3 Quantitative memory metrics

Quantitative metrics of σ_s, σ_m, $t_{95\%}$ and $t_{63\%}$ for δD and $\delta^{18}O$, or $t_{3\permille}$ and absolute value of the maximum peak for D-excess were also used to compare tubing experiments (Table S2). The different memory metrics calculated provide a different order of "best" to "worst" tubing materials and conditions based on slight differences, though all tubings appear operationally similar (Table S2). However, some common patterns emerge. According to most impulse response metrics (σ_s and σ_m), short thick-walled FEP has the fastest attenuation impulse response time. The slowest attenuation impulse response time for δD is consistently found in the long thin-walled FEP, while for $\delta^{18}O$ the slowest attenuation impulse response times are found in unheated copper (σ_m, enriched-to-depleted), unheated PFA (σ_s, enriched-to-depleted), and heated PTFE (both metrics, depleted-to-enriched). In terms of residence time adjusted $t_{63\%}$ values, unheated copper is the worst and short thick-walled FEP is the best for both $\delta^{18}O$ and δD. Similarly, $\delta^{18}O$ residence time adjusted $t_{95\%}$ values are longest for unheated copper and shortest for short thick-walled FEP in both directions of the isotopic switch. For residence time adjusted δD $t_{95\%}$ times, long thin-walled FEP is the worst in the enriched-to-depleted direction while heated PTFE is the worst in the depleted-to-enriched direction. Short thick-walled FEP is the best in terms of δD residence time adjusted $t_{95\%}$ time. Short thick-walled FEP was consistently the best for $t_{3\permille}$ and the absolute value of the maximum D-excess peak values, while heated long thin-walled FEP was the worse in both metrics in the enriched-to-depleted switch. In the depleted-to-enriched switch direction, heated PTFE was worse for $t_{2\permille}$ but for the absolute value of the maximum D-excess peak value, heated long thin-walled FEP was the worst. The rest of the tubing material types vary in their ranking depending on the memory metric used. Overall, heated memory metrics are generally either similar to or faster than those of the unheated memory metrics when comparing the same tubing types (Fig. S1d). However, this pattern does not hold for δD $t_{95\%}$, with differences of up to 15 s between heated and unheated PTFE, with unheated signal equilibrating faster.

Residence time adjusted attenuation threshold times are somewhat consistent with the visual analysis of Fig. 3, 4, S3, and S4. The residence time adjusted $t_{95\%}$ values for $\delta^{18}O$ range from 6.9–22.8 seconds with an uncertainty of up to 24 seconds for individual $t_{95\%}$ values. Measured values of $t_{95\%}$ for δD range from 6.9–48 seconds, with uncertainties of up to 14 seconds. Because of the shallow slope of the attenuation curves at $t_{95\%}$ values contributing to large error estimates, we also report $t_{63\%}$ values because they have smaller uncertainty estimates and may have a different sensitivity to tubing differences. For our analyzer settings, residence time adjusted $t_{63\%}$ values range from approximately 4.9–17.8 s for both $\delta^{18}O$ and δD, with uncertainty on the order of one second. $T_{63\%}$ values are more similar between $\delta^{18}O$ and δD than $t_{95\%}$ values (Fig. S1d). Finally, residence time adjusted $t_{3\permille}$ values for D-excess range from 0–93 seconds, while the largest $t_{3\permille}$ uncertainty value was 536 seconds. D-excess $t_{3\permille}$ values overlap both δD and $\delta^{18}O$ $t_{95\%}$ ranges. We also measured the absolute value of the maximum D-excess peak or the magnitude of the transient anomaly in D-excess signals. These values ranged from ~0–31‰, inclusive of error. The average difference between the beginning and ending D-excess values was 4.0 ‰.

In terms of the impulse response method, σ_m values which characterize the longer memory tail of the impulse function were on average, longer for δD than $\delta^{18}O$ and ranged from 0.66–2.2 ± 0.02 s (Table S2). Mixing times (σ_s) from the skew-normal impulse function fit ranged from 1.4–5.9 ± 1.2 s and were also on average, longer for δD than $\delta^{18}O$ (Table S2). Overall, impulse response metrics varied as expected for δD with length and volume with longer

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memory times for longer and larger volume tubing, but were inconsistent in $\delta^{18}O$. We were unable to calculate impulse response metrics for Bev A Line XX, as the isotopic switch was not achieved within the hour long source switching. Overall, impulse response metrics varied as expected for δD with length and volume with longer memory times for longer and larger volume tubing, but were inconsistent in $\delta^{18}O$.

3.4 Review of material properties

Predictions of tubing material performance can be made based on material properties. Hydrophobic materials that are nonpolar and have a high relative permittivity (also known as the dielectric constant, or a material's ability to prevent electrical fields from forming) are ideal for water vapor isotope studies as polar water molecules are affected by and can induce electric fields (Aemisegger et al., 2012). As previously shown, δD signal transitions are slowed compared to $\delta^{18}O$ signals, due to isotope dependent hydrogen bonding interactions with tubing walls. Limiting these interactions should lead to reduced isotopic attenuation times. Material specifications vary by manufacturer and material purity, but in general, FEP and PTFE materials are expected to have the least amount of water absorption of the tubing types we tested (Table 2). Metals have a relative permittivity value of ~1 due to their sea of electrons, which in this case interact with the polar water molecules. Larger values of relative permittivity are better in this case, as water vapor molecules will be less attracted to the material. HDPE, FEP and PTFE have the highest ability to prevent electrical fields. FEP and PTFE may be expected to have the shortest isotopic attenuation times based on combined water absorption percentage and relative permittivity. However, at the air flow rate we tested, the memory metrics of FEP and PTFE were not noticeably superior to the other tubing tested.

Table 2. Material properties of tubing type options and their water absorption percentages and relative permittivity values.

Material	Water absorption % by tubing weight	Relative Permittivity (Dielectric constant) @ 1 MHz (ε_r)
FEP	<0.01[1]	2.1[2]
PFA	<0.03[1]	2.05–2.06[2]
PTFE	<0.01[1]	2.0–2.1[2]
HDPE	0.10[1]	2.3–2.4[2]
Copper	N/A	~1

[1] after being submerged for 24 hours (ASTM D570). This metric is solely for plastic materials [2] (Electrical properties of plastic materials, 2021)

4 Discussion

Previous water vapor isotope studies have tried to identify suitable tubing material to use in sample inlets, and authors found several materials to be acceptableseveral different materials have been used. To our knowledge, these

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materials hadthe results of not be rigorously testinged for wall adsorption/desorption effects leading to memory artifacts have not been published. Theory based on principles of gas chromatography and gas-wall partitioning predicts that the residence time of gases adsorbed on tubing walls is linearly proportional to tubing inner diameter and should decrease at higher temperatures as gas saturation concentration changes (Pagonis et al., 2017). The experiments performed in this study begin to test these predictions for water vapor isotopes.

4.1 Review of material properties

We hypothesized that predictions of tubing material performance could be made based on tubing material properties. Out of material properties commonly reported by manufacturers, we selected two properties we thought may play a role in fractionating wall effects: water absorption % by tubing weight and relative permittivity. Hydrophobic materials that are nonpolar and have a high relative permittivity (also known as the dielectric constant, or a material's ability to prevent electrical fields from forming) should be ideal for water vapor isotope studies as polar water molecules are affected by and can induce electric fields (Aemisegger et al., 2012). As previously shown, δD signal transitions are slowed compared to $\delta^{18}O$ signals, due to isotope-dependent hydrogen-bonding interactions with tubing walls. Limiting these interactions should lead to reduced isotopic attenuation times. Material specifications vary by manufacturer and material purity, but in general, FEP and PTFE materials are expected to have the least amount of water absorption of the tubing types we tested (Table 2). The inner liners of Dekabon and Bev-A-Line XX are trademarked and/or non-disclosable, and as such the proprietary information found in Table 2 was not available upon request. Metals have a relative permittivity value of ~1 due to their sea of electrons, which in this case interact with the polar water molecules. Larger values of relative permittivity are better in this case, as water vapor molecules will be less attracted to the material. HDPE, FEP and PTFE have the highest ability to prevent electrical fields. FEP and PTFE may be expected to have the shortest isotopic attenuation times based on combined water absorption percentage and relative permittivity.

However, aAt the air flow rate we tested, the isotopic memory metrics of FEP and PTFE were not noticeably superior to the other tubing tested. If the material properties listed here cause acorrespond to a fractionating effect, their impact may be too small to measure, possibly due to the additional ~4 s residence time of the analyzer optical cell and internal plumbing. Alternatively, the material properties listed may impart non-fractionating effects. Slower tubing air flow rates and faster analyzer flow rates may result in more precise resolution of memory metric differences between tubing types, but further research would be needed to determine if these or other material properties affect water isotope memory.

Table 2. Material properties of tubing type options and their water absorption percentages and relative permittivity values.

Material	Water absorption % by tubing weight	Relative Permittivity (Dielectric constant) @ 1 MHz (ε_r)

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FEP	$\leq 0.01^{1}$	2.1^{2}
PFA	$\leq 0.03^{1}$	$2.05–2.06^{2}$
PTFE	$\leq 0.01^{1}$	$2.0–2.1^{2}$
HDPE	0.10^{1}	$2.3–2.4^{2}$
Copper	N/A	~ 1

[1] after being submerged for 24 hours (ASTM D570). This metric is solely for plastic materials [2] (Electrical properties of plastic materials, 2021)

4.2 Direction of isotopic and water vapor concentration transition

Quantitative memory metrics were used to determine if there was a difference in the enriched-to-depleted and depleted-to-enriched switches. We focused on the $t_{95\%}$ threshold metric, as the $t_{63\%}$ values and impulse metrics were too small to gain a complete understanding of any differences in switch direction or between H_2O matched and varied experiments. Similar to Aemisegger et al. (2012) and their tests with PFA, we found the enriched-to-depleted switch exhibited longer attenuation times during H_2O varyingvaried experiments (Fig. 3 and Table S2). However, we were not able to replicate this finding in the H_2O matched experiments. While Aemisegger indicated that they found a difference in switch direction regardless of the span of isotopic transition, they do not mention testing the effects of varying the span of water vapor concentration. We posit that the difference in isotopic transition dependent on direction is actually a dependence on the wetting and drying of the tubing and analyzer walls. Related to Aemisegger et al.'s (2012) claim that isotopic adsorption (depleted-to-enriched switch) is faster than the desorption process in the heavy isotopologues, this may be a side effect of the water vapor transition because it is energetically harder to pull a water vapor molecule off a tubing wall and replace it than it is to simply add more molecules., H_2O concentration variation between sources is likely the driving factor of memory metric differences based on transition direction.

4.31 Effects of material and temperature

We found δD and δ^{18}O attenuation curves between the commonly used tubing materials were slightly different, but operationally similar, at the flow rate, humidity, and temperatures tested (Fig. 43, 54, S3S4, and S4S5). with the exception of Dekabon and Bev-A-Line XX, attenuation curves were much longer. Our results are consistent with Griffis et al.'s (2010) assertion that HDPE is similar to PTFE. Similarly, Aemisegger et al., (2012) found little difference in attenuation times with varying PFA tubing temperatures. We were not able to replicate Steen-Larsen et al.'s (2014) finding that copper was better than PTFE in all metrics. In our study, tubing materials performed similarly when comparing all memory metrics: σ_s, σ_m, $t_{63\%}$, $t_{95\%}$, $t_{3‰}$, and the absolute value of the maximum D-excess peak.. However, given differences in D-excess values between sources, we caution overinterpreting the maximum D-excess anomalies between experiments, as evidenced by the different starting points in Fig. 4e. After

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accounting for differences in ~~Factoring in~~ tubing ID and length, PFA seems to be one of the better tubings by a very small amount. ~~However, given differences in D-excess values between sources, we caution overinterpreting the maximum D-excess anomalies between experiments, as evidenced by the different starting points in Fig. 4e.~~

Warmer temperatures are theoretically predicted to reduce attenuation times (Pagonis et al., 2017) by changing the saturation concentration of gases. Additionally, t~~T~~he lower molar density of the warmer air means there is a shorter residence time through the tubing, increased molecular movement, faster wall exchanges, and warmer tubing material means fewer molecules are stuck to the tubing walls. We found some evidence of ~~this~~ reduced ~~attenutation~~attenuation times in heated experiments in comparing $\delta^{18}O$ location times and σ_m from the impulse function method (Table S2). ~~L~~$\delta^{18}O$ location times for heated tubings are always faster than their unheated counterparts, and σ_m values are similar to or shorter for heated tubings in most cases. Calculated residence times and observed lag times were also faster for heated tubings, but to varying degrees depending on the tubing. ~~The heated tubing likely has faster residence, lag, and location times due to the decreased number of molecules in the tubing compared to the unheated experiment and possibly also due to decreased wall effects.~~ By $\delta^{18}O$ location adjusting the threshold memory metrics, we effectively are removing the effects of temperature on residence time of air in the tubing. The removal of temperature effects on residence time~~, that~~ is why the differences in Figure 5 are not consistent between heated and unheated. However, $\delta^{18}O$ location adjusting~~this~~ may also remove~~s~~ some wall effect differences between materials, and limits our ability to discuss $t_{63\%}$ given the similarity with location~~a~~ times ~~ies~~ discussed in Sect. 3.1. The memory tail, best described by $t_{95\%}$ (Fig. 5) and σ_m~~m~~ (Table S2), shows that heated experiments a==re not consistently slower or faster to equilibrate than their unheated counterparts==. Overall, heating the tubing to avoid condensation does not negatively impact the isotopic measurements. Similarly, Aemisegger et al., (2012) found little difference in attenuation times with varying PFA tubing temperatures.

~~Tubing residence time predictions are up to 12 s shorter than the measured breakpoint lag. Uncertainties in tubing residence time (a few seconds), length (a couple inches), and breakpoint lag (a few seconds) account for some of these differences. Tubing temperature measurements in the heated treatment varied depending on the position of the thermocouple relative to the heat cable. It is expected that the tubing was not at a perfectly uniform temperature, but we note that this heating design is commonly used in field conditions and represents likely inlet conditions. However, the lack of uniform temperature control leads to potential temperature-induced differences that are hard to quantify. This should be considered when comparing residence time adjusted memory metrics between experiments. Differences not attributed to variations in temperature, length, or error in the breakpoint lag may be due to wall effects.~~

4.4 Effects of tubing inner volume and length

The model in Pagonis et al. (2017) indicates that tubing delays are~~residence time is~~ expected to scale ~~based on length, but should not affect attenuation times sensitive to wall effects~~proportionally with tubing length and diameter. The difference in length in the thick-walled FEP long and short experiments was a factor of 19 (99 ft/5.2 ft, or 30.2 m/1.6 m)~~. which results in the same factor difference in residence time calculations~~ Both HDPE and Dekabon had a factor of 15 times difference in length between the long and short experiments (100 ft/78.7 ~~ft~~in or

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30.48 m/2 m). ~~The breakpoint lag differences between long and short thick-walled FEP tubing was approximately a factor of 8 times longer than~~faster in the short tubing experiment. While the results show a clear influence of longer memory times in longer tubing compared to short tubing, we were unable to find quantitative evidence of linear dependence on memory metrics like $t_{95\%}$. ~~We looked for confirmation of linear dependence on memory metrics like t95, but were unable to find evidence of linearity.~~Though ~~While~~ there are slight differences in the~~se~~ memory metrics we calculated, this is likely due to the influence of the analyzer. Because the analyzer optical cavity and inner tubing has a residence time of ~ 4 s~~ec~~, we are unable to resolve the residence time (1.0 ± 0.09 s) and memory metrics associated with the short FEP tubing ~~(1.0 ± 0.09 s)~~ only. Even with the large length difference in FEP, the shape of the isotopic attenuation curves remained similar after location adjustment which removes the length-based residence time differences (Fig. 6, 7, S6, and S7~~4 and S4~~). ~~L~~ δ^{18}O location~~Residence~~ time adjusted δD $t_{95\%}$ and $t_{63\%}$ times for long thick-walled FEP tubing were at maximum 6~~.~~2x and 2~~1~~.6x greater than the short, respectively. The mixing time scales (σ_s) and the memory tail metric (σ_m) both showed less than a doubling between short and long tubing. These ~~modest~~ modest differences in wall-effect memory metrics may be because the analyzer memory itself makes it impossible to accurately isolate and quantify the short tubing response.~~are not explained by the theory in Pagonis et al. (2017).~~

From the δ^{18}O location adjusted comparison of the same material (FEP) with different IDs (Fig. 6 and S6, panels a and c), we conclude that a bigger ID causes the increased memory. In our experiments, ID increased by a factor of 1.5x between thick- and thin-walled FEP ($^1/_8$ in. or ~3.18 mm ID compared to $^3/_{16}$ in. or ~4.76 mm ID). There was clear separation in Fig. 6 between thick- and thin-walled long FEP even after isolating the memory tail by adjusting for bulk delay differences with~~by~~ the δ^{18}O location adjustment. The thin-walled FEP had a less steep slope and longer $t_{63\%}$ intercept than the thick-walled tubing. δ^{18}O ~~l~~Location time adjusted memory metrics also show a slight increase in memory with ID increase, with an average 2.1x larger memory metric for δD and 1.98x larger memory metric for δ^{18}O between thin- and thick-walled long FEP tubing (Table S2). The long thin-walled FEP consistently showed the slowest δD signal transitions of the FEP tubings tested (Fig. 6 and S6 panels c and d), as well as of all the tubing materials tested (Figs. 4 and S4, panels c and d). We also note that PTFE and PFA tubing had the same ~~larger~~ IDs as the thin-walled FEP~~than many of the other materials tested~~ in the H$_2$O matching experiments, $^3/_{16}$ in. (~4.76 mm). PTFE and PFA experiments showed a shorter~~longer~~ attenuation threshold time than the thin-walled FEP, and longer attenuation times than tubing with smaller IDs like HDPE~~FEP~~ (Fig. 4 and S4). Therefore, the results in Figure 4 must be evaluated while considering ID differences.

In summary, we found that all tubing dimensions, including ID and length, had some effects on the threshold metrics (Fig. 6, 7, S6, and S7~~4 and S4~~) even after removing differences in location times in signal propagation to the analyzer based on tubing inner volume and the temperature influence on molecular density and the total number of molecules in the tubing. While these overall memory metric differences exist, they are small in the materials and dimensions tested, with the exception of Dekabon. The operational impact among commonly used ¼ in. (6.35 mm) OD tubing inlets is expected to be limited. Tubing length and ID play a role in our experiment, consistent with theory that tubing length, ID, and material properties such as density and partitioning depth will affect the

attenuation time of chemical compounds on or in a tubing wall (Pagonis et al., 2017). Further tests under faster analyzer and slower tubing air flow rates would be needed to further validate whether these influences are linearly proportional.

4.5~~3~~ Relative attenuation time differences between δD and δ¹⁸O

δD signals have been demonstrated to take longer than δ¹⁸O signals to isotopically equilibrate with tubing materials due to isotope-dependent hydrogen-bonding interactions with the tubing walls (Sturm and Knohl, 2010; Griffis et al., 2010; Schmidt et al., 2010). These results agree. This speed difference has been reported as a ratio of attenuation times between the slower δD signal and the faster δ¹⁸O signal, and a large range of ratios have been reported. As demonstrated in the results, different metrics show different sensitivities to different parts of the attenuation curve. Published results show 1.4–3.5x greater attenuation time for δD signals than δ¹⁸O signals depending on tubing air flow rate, tubing type, humidity, and memory metric used (Schmidt et al., 2010; Griffis et al., 2010; Aemisegger et al., 2012; Zannoni et al., 2022). The threshold metrics we calculated are most similar to the quantification metrics used in earlier studies and our results have similar ranges (excluding Dekabon). Dekabon is presented separately, as the associated metric ratios are vastly different than the rest of the tubing materials tested. ~~For δD σₓ, we found values ranging from a 0.7–1.8x thegreater attenuation time offor δD signals than δ¹⁸O signals in tubings other than Dekabon. The σₓ metric is not particularly sensitive to the characteristic long δD memory tail. For σₘ, δD values were 0.9–1.7x longer than δ¹⁸O values, which is a metric more sensitive to the characteristic long δD memory tail. Location ratios were very similar at 1.0–1.1x greater for δD signals than δ¹⁸O which is understandable because that indicates the time of rapid flushing of the analyzer cavity when the new source vapor reaches the analyzer.~~ For $t_{63\%}$, this ratio ranges from 1.0–3.46~~1.2~~x greater, and for $t_{95\%}$ 1.0–4.79~~2.7~~x. For $σ_m$, a metric that we expected to be sensitive to the characteristic long δD memory tail, δD values were 0.9–1.7x longer than δ¹⁸O values. Dekabon metric multipliers for δD vs δ¹⁸O signals are up to 14.1 for ~~impulse metrics~~ $σ_m$, 61.5 for $t_{63\%}$, and 71 for $t_{95\%}$ values across all 100 ft (30.48 m) experiments. Overall, δD signals are slower than δ¹⁸O signals in all tubing materials, and ~~but~~ this difference is exaggerated in Dekabon.

4.6~~5~~ Fitting att~~t~~enuation curves

The overall attenuation curves of the tested tubing material types, lengths, and temperature conditions had effectively the same reverse sigmoidal shape after fitted δ¹⁸O location time adjustment, though in Dekabon this shape is elongated. ~~The slight differences in signal attenuation between all tubings except Dekabon could be due to errors in normalization and location adjustments between experiments, differences in tubing internal roughness, and analyzer noise.~~ Previous studies approximated the attenuation transfer function as an exponential curve (Sturm and Knohl, 2010; Aemisegger et al., 2012; Schmidt et al., 2010), similar to the exponential decay response that would be expected for the residence time distribution function of a continuously stirred reactor (Toson et al., 2019). We found the exponential function was not a satisfactory fit to our experimental observations. A more appropriate mixing analogy could be the axially dispersed plug flow (ADPF) model (Huang and Seinfeld, 2019), as this better matches

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the reverse sigmoid curve we observe. In the ADPF model, there is a bulk flow that has a diffusive "head" that diverges forwards and backwards from the bulk flow, leading to the observed smoothing of the output signal of an input step-change. This effectively "smears" the observed isotopic signal. While the shape of this transfer function seems appropriate, the Huang and Seinfeld (2019) model does not consider gas-wall exchange effects. The transfer function model we introduce here fits the observations sufficiently well, but more work is needed to match the formulas with mixing theory.

Likewise, the impulse fitting method we used is more complicated than previously used (Jones et al., 2017; Kahle et al., 2018). We were able to estimate a mixing time metric (σ_s) from the skew-normal and a memory tail metric (σ_m) from our modified impulse function fitting method. We believe these metrics are signals of diffusion mixing and isotopic wall effects. Mathematically describing the influence of isotopic wall effects using a transfer and impulse function is potentially useful for correcting out memory effects in water vapor isotope measurements, as suggested by Massman and Ibrom (2008) and others (e.g. Aemisegger et al., 2012; Steen-Larsen et al., 2014). Similar corrections have been achieved in the ice core and liquid water isotope analysis communities (e.g. Jones et al., 2017; Kahle et al., 2018; Vallet-Coulomb et al., 2021). We found more complicated transfer and impulse function models were necessary to fully capture the memory effects in the vapor inlet system compared to the mostly liquid inlet systems described before (e.g. Jones et al., 2017; Kahle et al., 2018; Vallet-Coulomb et al., 2021). This should provide a starting point for future work removing the low-pass filter effects on continuous water vapor measurements.

5 Implications for measurements

Longer attenuation times smooth signal variability and mask high-frequency features, as shown in Sect. 3.4. While lag times aren't inherently bad (as long as measurements lag in tandem), signal smoothing caused by memory effects will draw out the memory tail and muddle environmental signals. Therefore, the magnitude and speed of atmospheric signal variability as well as the analyzer and sample intake performancesmoothing are important considerations when planning for ambient water vapor isotopic measurements. We found very small differences among commonly used tubing materials under the experimental conditions tested here. While different analyzer air flow rates are not presented in this study, it is known that analyzer flow rate strongly influences sample residence time in the optical cavity of these analyzers and the speed of signal transitions. The Aemisegger et al., (2012) findings that attenuation times were controlled more by analyzer residence times than PFA intake tubing is supported by the results presented in this study.

Though Bev-A-Line XX was the only material in this study that performed particularly poorly, Pprior research clearly identified Dekabon tubing as unsuitable (Sturm and Knohl, 2010; Griffis et al., 2010; Schmidt et al., 2010; Tremoy et al., 2011), a conclusion which was validated in this experiment. Bev-A-Line XX also performed particularly poorly, and we cannot recommend the use of either tubing in water vapor isotopic studies. We also suggest testing the effect of any in-line elements like flow meters, mass flow controllers, or filters on isotopic signal attenuation, especially if they are made from materials not tested in this study. Our experience found a mass flow meter that introduced a large memory effect (not presented here).

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5.1 Low atmospheric variability measurements

920 For stationary measurements with one intake and high air flow rates, tubing selection among commonly used materials is not as much of a concern as air advecting past the intake typically changes slowly compared to tubing attenuation time scales we quantify here. Conroy et al., (2016) for example, observed vapor on Manus Island, Papua New Guinea that changed by 22.3 ‰ in $\delta^{18}O$ and 154.8 ‰ in δD, with the largest change being ~25 ‰ δD over a duration of a few hours. The instant isotopic step change in our experiment (17.6 ‰ in $\delta^{18}O$ and 136 ‰ in δD) is

925 extreme compared to typical atmospheric variability at a stationary inlet. For stationary measurements, any of the tested tubing materials besides Dekabon and Bev-A-Line XX should be suitable and would not be expected to produce large transient D-excess artifacts due to memory differences between δD and $\delta^{18}O$.

5.2 High atmospheric variability measurements

For measurements that need high temporal resolution of small atmospheric isotopic variability like flux gradient and

930 eddy covariance setups or airborne observations, extra precautions should be taken. Griffis et al. (2010) used spectral analysis in their eddy covariance experiments to show that tube memory effects weren't a concern for $\delta^{18}O$ signals at tubing air flow rates of 12 L min^{-1} and analyzer air flow rates of 1.5 L min^{-1}. However, one can't extend that conclusion to slower air flow rates and analyzer residence times should be compared across analyzer types.

Aircraft campaigns are a special concern, as they observe not only at high temporal (and spatial) resolution, but

935 encounter large and rapid isotopic and humidity variability as well. Especially when conducting vertical profiles, isotopic compositions can vary by hundreds of per mil in δD. Salmon et al. (2019) found δD signal values ranging from -400 to -175 ‰ δD within an ~5 minute vertical profile descent between 1200 to 400 m above ground. Similarly, Sodemann et al. (2017) reported flight sections with >200 ‰ δD variations in under 5 minutes. While data was collected at 1 Hz, their reported data is a 15 s average, which allows them a 975 m horizontal and 75 m

940 vertical resolution (Sodemann et al., 2017). However, that best-case estimate is based on the data averaging interval and does not consider signal attenuation due to tubing isotopic memory or mixing in the optical cavity (Sodemann et al., 2017). Additionally, averaging over long time periods may not remove D-excess memory bias depending on patterns of increasing or decreasing delta values. The wetting and drying of the measurement system during flights with large changes in altitude, and therefore atmospheric specific humidity, may also increase isotopic attenuation

945 times but were not quantified here.

In both eddy covariance and aircraft measurement situations, one might consider increasing air flow through the analyzer and intake tubing and shortening the length of tubing from an intake pickoff point to the analyzer in slow analyzer flow setups as has been suggested in previous studies (e.g. Griffis et al., 2010). While high air flow rates can easily be achieved in the air intake main lines in both high-frequency measurement situations, the air flow rate

950 through the analyzer is typically limited by the analyzer design and control software. If tubing or in-line elements like mass flow controllers affect the speed at which the isotopes are transmitted from the intake to the optical cavity, signals are effectively low-pass filtered (Zannoni et al., 2022). Our experiments show shorter memory effects for shorter tubing compared to longer tubing. Therefore, it is also important to minimize the length of tubing from the

intake pickoff point to the analyzer to reduce the residence time of air in the low-flow portion of the system. These
955 considerations should also maximize D-excess data resolution.

5.3 Liquid water measurements

Liquid water isotope analysis is also plagued by memory effects when samples are converted to the vapor phase for
laser-based spectral isotopic analysis, especially in applications measuring samples with large isotopic differences in
the same batch. Common protocols recommend multiple replicate injections and discarding the first few to remove
960 carryover from the previous sample (IAEA, 2009; Penna et al., 2012; Coplen and Wassenaar, 2015). In both OA-
ICOS and cavity ring-down spectroscopy, Penna et al. (2012) found that when measuring samples with large
isotopic differences, up to eight out of eighteen injections had to be ignored to limit memory effects. When
analyzing highly depleted Antarctic samples ranging from −231.7 ‰ to −421.1 ‰ for δD, memory effects of up to
14 ‰ were found in the first injection compared to the "true" value. Liquid water analysis is one example of a case
965 where air flow rates and temperatures of transfer lines are often fixed by the instrument design. Material properties
inside the analyzer are important, but this study finds little difference between commonly used material types.
Waiting for equilibrium in the optical cavity may minimize the memory effect, but a time-efficient method to
increase sample throughput is to mathematically correct for these repeatable effects rather than attempting to
minimize them (e.g. de Graaf et al., 2020; Vallet-Coulomb et al., 2021; Hachgenei et al., 2022). Or, in the case of de
970 Graaf et al., (2020), one can measure small vapor samples on a background of humid air to reduce memory effects.
Work is also being done in the ice core community to correct out signal mixing based on transfer function fitting
methods (e.g Jones et al., 2017; Kahle et al., 2018). These memory correction approaches may provide examples of
methods to reconstruct input signal variability from smoothed continuous vapor isotope measurements as well.

6 Conclusions
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We tested the water isotopic exchange properties of PFA, FEP, PTFE, HDPE, copper, and Bev-A-Line XX, and
Dekabon. The commonly used materials tested here (not including Bev-A-Line XX and Dekabon) perform
similarly. It does not seem necessary to standardize materials used to measure stable water vapor isotopologues to
make accurate and comparable measurements in most situations, when using analyzers with similar residence times.
980 We cannot recommend Bev-A-Line XX or Dekabon for use in water vapor applications due to extremely long
attenuation times. At this relative humidity of ~33 %, wWarmer temperatures did shorten the residence time, lag,
and location metrics of the impulse function and $t_{63\%}$ threshold times across all long tubing experiments but results
were not always consistent for $t_{95\%}$. Overall, Hheating to avoid condensation does not seem to negatively impact the
isotopic measurements. While differences may be found among tubing material types at lower or higher humidityies
985 or while changing humidity, these experiments are beyond the scope of this study. Larger tubing IDs were predicted
to increase memory metrics proportionally based on gas-wall partitioning theory (Pagonis et al., 2017), and we
found that increasing tubing ID and length had some effects onincreased the threshold metrics after removing
differences in δ^{18}O location timesresidence times. This difference was most noticeable between 100 ft and 2 m
Dekabon. The other tubing experiments here showed overall memory metric differences do exist, but that they are

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990 small in the materials and dimensions tested. In experimental settings, operational impact among commonly used ¼ in. (6.35 mm) OD tubing inlets is expected to be limited.

Researchers must understand the limitations of the air flow conditions and wall effects of their instrumental and intake setups to limit signal memory effects, especially if low air flow rates are a constraint or if there are large isotopic variations over short periods of time. Our experience and results from other published studies indicate that

995 maximizing air flow rates through the analyzer is the most effective way to minimize memory effects when accurate high-frequency D-excess measurements are desired. ~~As each individual analyzers are~~ is unique ~~and may have slightly different inner volumes and maximum flow rates depending on the setup, users are advised to test their analyzer for memory effects with no intake tubing.g.~~ Our results show that these plastic tubing materials are not inferior to copper in terms of isotopic memory under the tested conditions, and they are easier to work with and are

1000 less expensive than copper. As with most decisions, environmental conditions, cost, and preference may influence the type of tubing selected.

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