

Development of accurate and stable primary standard gas mixtures for global atmospheric acetonitrile monitoring: evaluating adsorption loss and long-term stability*

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Abstract. Acetonitrile plays an important role in atmospheric processes and serves as a key tracer of biomass burning, the major emission source of primary carbonaceous particles and trace gases in the global atmosphere. Recognizing its significance, the World Meteorological Organization (WMO) Global Atmosphere Watch (GAW) has designated acetonitrile as one of the target volatile organic compounds for global atmospheric monitoring, aiming for data quality better than 20 % accuracy and 15 % precision. Meeting the objectives of the WMO GAW program requires accurate and stable calibration standards with expanded uncertainties of less than 5 %. In this study, we explored the feasibility of gravimetry for developing primary standard gas mixtures (PSMs) in three different types of aluminium cylinders, each with distinct internal surface treatments, at nmol mol⁻¹ and μ mol mol⁻¹ levels with a relative expanded uncertainty of less than 5%, having nitrogen as matrix gas. We found that all three types of cylinders were inadequate, without further passivation, for developing acetonitrile PSMs below 10 nmol mol⁻¹ due to significant adsorption losses (6%–49 %) onto the cylinder's inner surface. To overcome this challenge, we prepared acetonitrile gas mixtures at 100 nmol mol⁻¹ using a modified gravimetric method and at 10 μ mol mol⁻¹ using a conventional gravimetric method and then evaluated their long-term stability. Results showed that the effect of the adsorption loss at 100 nmol mol⁻¹ and 10 μ mol mol⁻¹ was negated and negligible, respectively. Stability results show that we can disseminate acetonitrile calibration standards at both 100 nmol mol⁻¹ and 10 μ mol mol⁻¹ with a relative expanded uncertainty of 3 % and 1 %, respectively (with an expiration period of 3 years), meeting the target uncertainty of the WMO GAW program. Further research is still needed to develop accurate and stable acetonitrile calibration standards below 10 nmol mol⁻¹ that are closer to atmospheric levels.

1 Introduction

Biomass burning is the largest source of primary fine carbonaceous particles and the second largest source of trace gases in the global troposphere (Akagi, *et al.*, 2011). It also emits a significant amount of short-lived global warming substances, such as volatile organic compounds (VOCs) and NO_x, that significantly contribute to ozone formation through photo-chemical

30 reactions (van der Werf, 2017; et al.; Chandra, et al., 2020). These photochemical oxidants and fine particles can cause severe regional air pollution and also contribute to climate change (Ramana, et al., 2010). Acetonitrile (CH_3CN) predominantly released from bio-mass/biomass burning, is relatively unreactive, but it plays an important role in atmospheric ion formation through its chemical reaction with hydroxyl (OH) radicals (Brasseur, et al., 1983; Yuan, et al., 2010). Acetonitrile, with its relatively long atmospheric lifetime ranging from 3 months to 11 months, has been used as a useful tracer of both controlled and uncontrolled biomass burning in many research studies (Hamm and Warneck, 1990; De Gouw, et al., 2003; Singh, et al., 2003; Murphy, et al., 2010). The global budget of acetonitrile is incomplete and poorly constrained due to the limited availability of in-situ measurement data on the atmospheric distribution, with even less data in remote marine atmospheres (Harrison and Bernath, 2013). Monitoring its long-term trend is a useful way for analysing changes in both natural and anthropogenic acetonitrile emissions in the global atmosphere. Acetonitrile has been measured at various locations and reported at pmol mol⁻¹ levels (Sanhueza, et al., 2001; Warneke and De Gouw, 2001; Sanhueza, et al., 2004) but the measurement uncertainties are too large to allow comparison between different studies and to gain new insights about its roles in atmospheric chemical and physical processes. The World Meteorological Organization (WMO) Global Atmosphere Watch (GAW) programme has selected acetonitrile as one of the target VOCs that should be monitored in the atmosphere and set the objective of the data quality as better than 20 % accuracy and 15 % precision (WMO, 2006). To achieve this objective, accurate and stable acetonitrile calibration standards are required with a relative expanded uncertainty of less than 5 % (Schultz, et al., 2015). Several types of calibration standards have been used to measure acetonitrile, including a diluted gas standard from a permeation source with an uncertainty of $\pm 25\%$ sources, (Singh, et al., 2003; Lange, 2002) which requires a permeation device to keep a very stable temperature (Susaya et al., 2011), a standard gas mixture in a cylinder with uncertainties of $\pm 25\%$ (Sanhueza, et al., 2004) and a liquid solution standard (Zamecnik and Tam, 1987). However, the relatively large uncertainties of these standards do not meet the WMO GAW requirements. Thus, an International System of Units (SI) traceable, accurate, and stable acetonitrile calibration standard is essential for monitoring its concentrations and temporal and spatial variabilities and thus understanding its roles in atmospheric processes and climate change. There are several methods, such as static gravimetry (ISO, 2015), dynamic gravimetry (Brewer, et al., 2011) and dynamic dilutions (Kim, et al., 2016) for producing primary standard gas mixtures (PSMs). This study investigates the feasibility of gravimetry for developing PSMs for acetonitrile PSMs with nitrogen matrix in three different types (i.e., different internal surface treatments) of aluminium cylinders at nmol mol⁻¹ and $\mu\text{mol L}^{-1}$ levels with a relative expanded uncertainty of less than 5 % (a confidence interval of approximately 95 %, $k = 2$).

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2 Materials and methods

2.1 Materials and preparation of gas mixtures

60 This study involves preparing gas mixtures using the conventional gravimetric method (ISO, 2015) and the modified gravimetric method (Brewer et al., 2019) to examine the stability of acetonitrile (ACN) in aluminium cylinders. Hexane known

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to be stable in aluminium cylinders (Rhoderick et al., 2019) was introduced with acetonitrile to monitor the stability of acetonitrile in cylinders. In the conventional gravimetric method, an aliquot of a parent gas mixture was transferred to another new cylinder and then diluted with pure nitrogen to prepare gas mixtures at lower amount fractions (Fig. 1a,b). For the modified 65 gravimetric method, after decanting some amount of the aliquot, the remaining aliquot in a parent gas mixture is diluted with pure nitrogen which negates the effect of adsorption loss on the internal surface of cylinders (Brewer et al., 2019) (Fig. 1c). At each dilution step, at least two pairs of cylinders of mixtures were prepared, the exact number of cylinders is shown in the schematic diagram in Fig. 1.

Both acetonitrile and hexane liquid reagents (Sigma-Aldrich, USA) were analysed to assess their purity using a gas 70 chromatograph with a flame ionization detector (GC₇FID₇ 7890N, Agilent Technologies, USA) for VOC impurities and a Karl Fischer coulometer (831 KF, Metrohm, Switzerland) for water impurities. The purity of the acetonitrile reagent was estimated as 99.9458 cmol mol⁻¹ with an expanded uncertainty of 0.0023 cmol mol⁻¹ ($k = 2$). The purity of the hexane reagent was calculated as 99.2672 cmol mol⁻¹ with an expanded uncertainty of 0.0157 cmol mol⁻¹. No quantifiable acetonitrile was found in the hexane reagent liquid. High-purity nitrogen gases (Deokyang Co., Ltd, Korea) were used as a diluent and were 75 purified through a purifier (Micro Torr, SAES Pure Gas, Inc., USA) to remove VOCs to less than 1 nmol mol⁻¹. The acetonitrile content in high-purity nitrogen gases was determined ~~as to be~~ half of its detection limit (0.31 nmol mol⁻¹) with an expanded uncertainty of 0.18 nmol mol⁻¹.

The acetonitrile and hexane liquid reagents were transferred into the cylinders using gastight syringes with a sample-lock 80 termination fitted with a bevelled-tip stainless steel needle (Hamilton Company, USA). Each syringe was locked by a twist valve on termination; and its needle tip was capped with a septum to minimize the possible evaporation loss of liquid reagents during preparation. To determine the masses of liquid reagents transferred into cylinders, the syringes were weighed on an analytical balance (AT201, Mettler Toledo, Switzerland) with a capacity of 205 g and a resolution of 0.01 mg. To calculate 85 the masses of nitrogen gases introduced into cylinders, the cylinders were weighed before and after being filled with gas filling, using a KRISS automatic weighing system equipped with a top-pan balance (XP26003L, Mettler Toledo, Switzerland) with a capacity of 26 kg and a resolution of 1 mg.

Gravimetric preparation was used as the primary method to establish SI traceability through direct linkage to the mole (mol). The amount of substance in sample X, n , was determined following common and practical realizations of the mole definition and its derived units as shown in the following Eq. (1) (Güttler et al., 2019).

$$n = \frac{N}{N_A} = \frac{w(X)m}{A_r(X)N_A m_A} = \frac{w(X)m}{A_r(X)M_u} \quad (1)$$

90 Where

N the number of elementary entities of the substance X in the sample,

N_A Avogadro constant (mol^{-1}),

$w(X)$ the mass fraction of X in the sample (g g^{-1}),

m the mass of the N elementary entities (g),

95 $A_r(X)$ the relative atomic or molecular mass of X (depending on whether X is an element or a compound respectively),
96 M_u the molar mass constant (g mol⁻¹).

Gas mixtures were prepared in three different types of 10 L aluminium cylinders (Luxfer, United Kingdom) with different internal surface treatments such as untreated cylinders with nickel chrome plated valves (Hamai, Japan) (hereafter referred to as Untreated), Experis-treated cylinders (Air Products, Belgium) with stainless steel valves (Rotarex, Luxembourg)

100 (hereafter referred to as Experis) and Performax-treated cylinders (EffecTech, United Kingdom) with stainless steel valves (Rotarex, Luxembourg) (hereafter referred to as Performax). All gases were hereafter referred to as Performax). All cylinders were new and vacuumed to 10^{-3} pa while being heated to about 70 °C with temperature-controlled heating bands to ensure the thorough removal of any potential impurities prior to gravimetry preparation. Each dilution gas was introduced into cylinders using a KRISS gas filling system that consisted of a Sulfinert®-treated stainless steel manifold, gate valves, a vacuum pump,

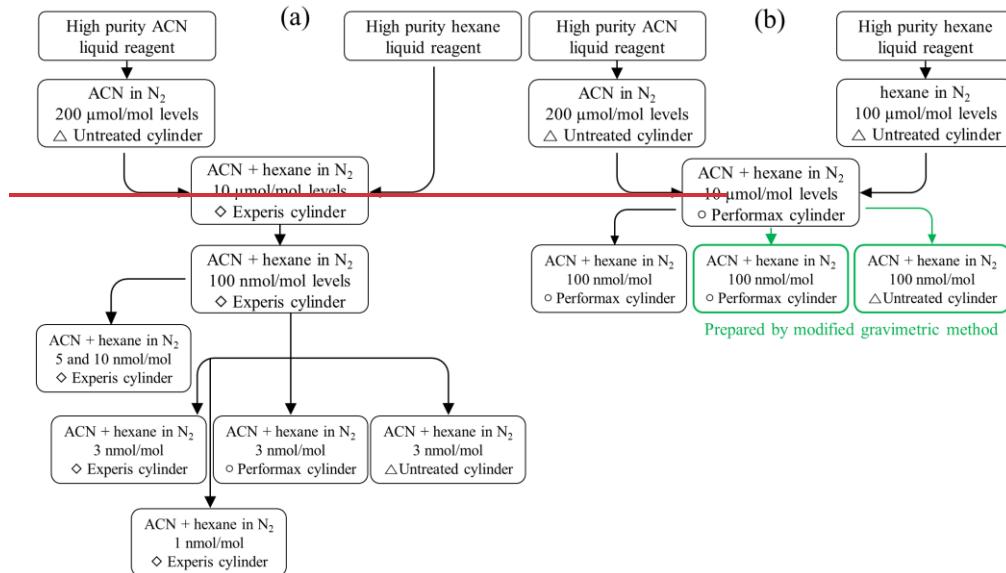
105 and pressure gauges: (Kim et al., 2018).

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2.2 Methods

2.2.1 Preparation of gas mixtures

A set of gas mixtures was prepared using both the conventional gravimetric method (ISO, 2015) and the modified gravimetric method (Brewer, 2011) (Fig. 1). Hexane, known to be stable in aluminium cylinders (Rhoderick, 2013; Brewer, 2019), was introduced together with acetonitrile to monitor the stability of acetonitrile in cylinders. In the conventional gravimetric method, an aliquot of a parent gas mixture was transferred to another new cylinder and then diluted with pure nitrogen to prepare gas mixtures at lower amount fractions (Fig. 1.a). In the modified gravimetric method, an aliquot remaining in a parent gas mixture after decanting was diluted with pure nitrogen which negates the effect of adsorption loss on the internal surface of cylinders (Brewer, 2019). Gas mixtures at 100 nmol/mol were prepared in both Untreated and Performax cylinders using the modified gravimetric method (Fig. 1.b).



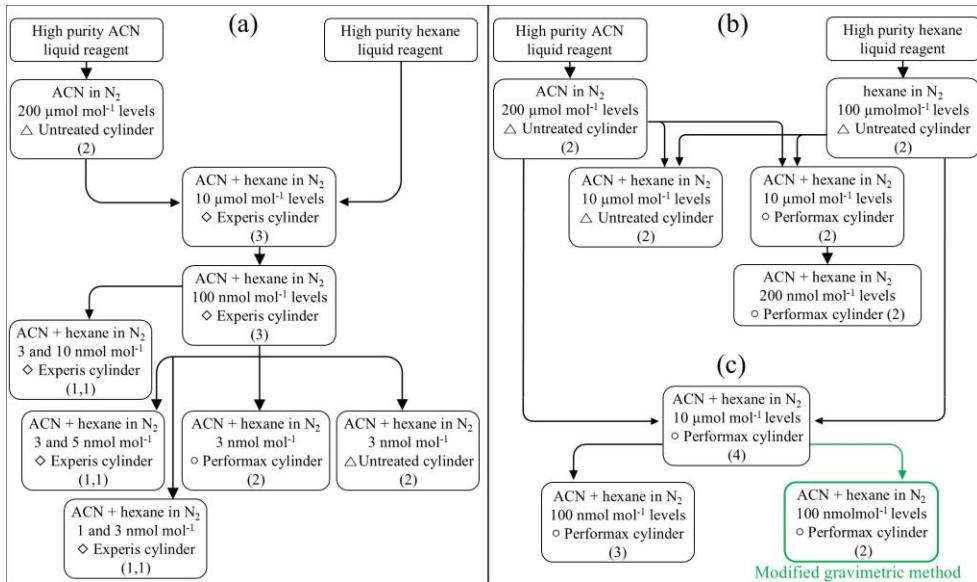


Figure 1. Schematic diagram of the preparation of the acetonitrile gas mixtures with the target amount fractions in specified cylinders, (a) by conventional gravimetric method, (b) by conventional gravimetric method for adsorption loss evaluation and (c) by modified gravimetric method. The number in parentheses indicates the number of cylinders prepared at each level.

2.2.2 Analysis of gas mixtures

All gas mixtures at each dilution step were analysed against each other (the first one is typically used as a reference) for verification at $\mu\text{mol mol}^{-1}$ GC/FID with a DB-1 capillary column (60 m length and 0.32 mm diameter with a 1 μm thick film) and 2 μL loop utilized. For nmol mol^{-1} GC/FID with a cryogenic (liquid nitrogen) pre-concentrator used. A sample gas at nmol mol^{-1} was cryogenically concentrated in a Sulfinert®-treated sample loop filled with glass beads. About a volume of 0.5 L sample was trapped in the loop and then injected into the GC/FID under the same conditions as $\mu\text{mol mol}^{-1}$. The sample inlet to the cryogenic pre-concentrator was described in more detail in a previous study by Kim (2018). The GC-FID analytical instruments utilized in this study have been developed for analysing dimethyl sulphide at nmol mol^{-1} levels and previously validated by Kim et al. (2016; 2018). They have been successfully employed for analysing volatile organic compounds at nmol mol^{-1} levels in multiple international comparisons (Lee et al., 2020; Lee et al., 2021; Cecelski et al., 2022; Lee et al., 2022) to demonstrate the measurement capabilities. The GC-FID (Agilent 7890, USA) equipped with a 2 μL sample loop was used for analysing samples in the range of 10 to 200 $\mu\text{mol mol}^{-1}$. For nmol mol^{-1} range measurements, a GC-FID (Agilent 6890, USA) coupled with a cryogenic pre-concentrator was utilized. In the pre-concentration system, approximately 0.9 L for 1–10 nmol mol^{-1}

135 mol⁻¹ and 0.5 L for 100 nmol mol⁻¹ of sample gas, respectively, was trapped in a Sulfinert®-treated sample loop filled with glass beads under cryogenic conditions using liquid nitrogen. The more detailed configuration of the sample inlet to the cryogenic pre-concentrator has been previously described by Kim et al. (2018).

140 Both systems were equipped with DB-1 capillary column (60 m × 0.32 mm, 1 µm film thickness, Agilent, USA) using helium as the carrier gas. The GC oven temperature program consisted of an initial hold at 80 °C for 3 min followed by a ramp of 20 °C min⁻¹ to 150 °C with a final hold of 3 min. The FID temperature was maintained at 250 °C. Prior to each set of samples blank measurements using high-purity nitrogen (99.9999 cmol mol⁻¹) were conducted. For each preparation level, all gas mixtures were analysed against each other to evaluate the consistency of the gravimetrically prepared gas mixtures, with one of the gas mixtures selected as the working reference. Eight consecutive measurements (i.e., injections) were performed for each sample and peak areas were integrated baseline-to-baseline using the GC software. The averaged peak area for each sample was calculated using at least the last three measurements.

145 3 Results and discussion

3.1 Evaluation of gas mixtures less than 10 nmol mol⁻¹ prepared using conventional gravimetric method

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We assessed the consistency of gas mixtures at each dilution step by comparing normalized response factors (RFs) calculated following Eq. (1):

$$\text{Normalized RF} = \frac{\text{RF}_{\text{sample}}}{\text{RF}_{\text{reference}}}, \quad (1)$$

150 and the response factor (RF) is determined by Eq. (2):

$$RF = \frac{\text{GC peak area}_t}{\text{Gravimetric amount fraction}_t}, \quad (2)$$

$$RF = \frac{y}{x} \quad (2)$$

Where

y the analyser response (i.e., GC peak area),

155 x the gravimetric amount fraction (mol mol⁻¹).

with the standard uncertainty of the response factor (u(RF)) given by:

$$u(RF) = \sqrt{u^2(y_{\text{rep}}) + u^2(y_{\text{drift}}) + u^2(x)} \quad (3)$$

Where

u(y_{rep}) the standard uncertainty of the repeatability of the analyser response (i.e., GC peak area),

160 $u(y_{\text{drift}})$ the standard uncertainty of the drift of the analyser response,
 $u(x)$ the standard uncertainty of the gravimetric amount fraction (mol mol⁻¹).

The normalized response factor is determined by:

Normalized $RF = \frac{RF_{\text{sample}}}{RF_{\text{reference}}}$ (4)

with the standard uncertainty of the normalized response factor ($u(\text{Normalized } RF)$) given by:

165 $u(\text{Normalized } RF) = \sqrt{u^2(RF_{\text{sample}}) + u^2(RF_{\text{reference}})}$ (5)

Here, RF_{sample} and $RF_{\text{reference}}$ represent the response factor of sample and working reference, respectively, with their standard uncertainties $u(RF_{\text{sample}})$ and $u(RF_{\text{reference}})$, respectively. Blank measurements using high-purity nitrogen showed no detectable peaks, thus, blank correction was not required for the analytical results. The uncertainties of response factors were estimated by combining uncertainties from GC analysis and gravimetric preparation. If gas mixtures are 170 consistent, the normalized response factors should be consistent within their associated uncertainties (i.e., the normalized response factors should not be different from one within their associated uncertainties) considering a wide range of linearity of FID detectors. The normalized RFs of hexane in all cylinders agreed within the uncertainties (less than 0.5 %) regardless of cylinder types and amount fractions. However, the normalized RFs of acetonitrile showed inconsistency between cylinders with different treatments and even within cylinders with the same treatment (Fig. 2). For example, in both Experis 175 and Untreated cylinders, the normalized RFs of acetonitrile differed by about 10 % at the same amount fraction (3 nmol mol⁻¹) while those of hexane remained consistent. These results suggest that the inconsistency of acetonitrile resulted from cylinder characteristics (e.g., adsorption loss) concerning related to acetonitrile, rather than from the gravimetry preparation itself, as hexane in the same cylinders showed good agreement. The normalized RFs for acetonitrile showed good 180 agreement only across the Performax cylinders, despite the potential for some loss. Based on these findings, further tests and evaluations were focused on the Performax cylinders.

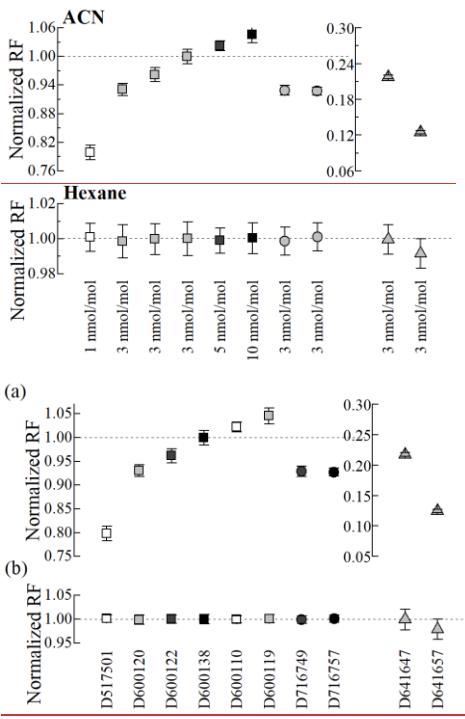


Figure 2. Verification results of (a) acetonitrile and (b) hexane gas mixtures less than at 1 nmol mol⁻¹ (white), 3 nmol mol⁻¹ (grey), 5 nmol mol⁻¹ (dark grey), and 10 nmol mol⁻¹. The error bars show expanded uncertainties ($k=2$). The (black) in the Experis (rectangle), Performax (circle), and Untreated (triangle) cylinders. Note that the y-axis and x-axis represents the normalized response factor (RF) and cylinder numbers, respectively, and the error bars show expanded uncertainties ($k=2$).

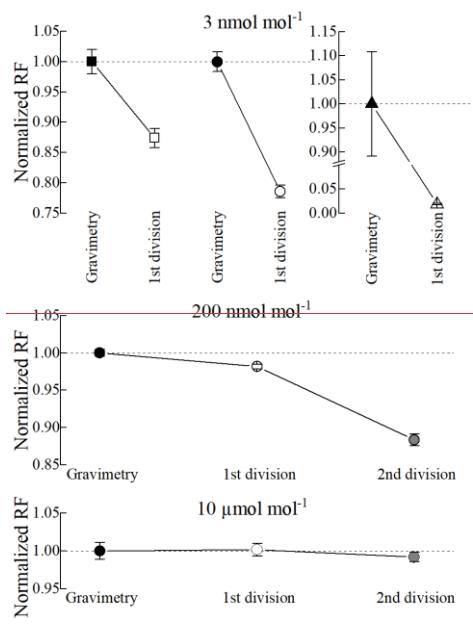
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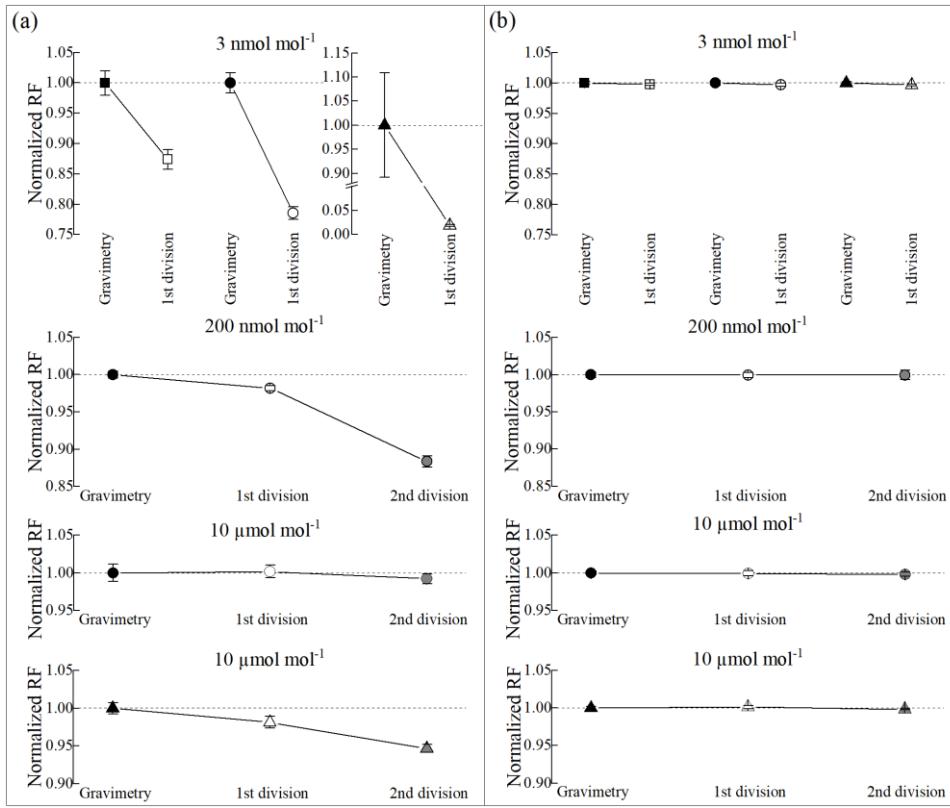
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3.2 Evaluation of adsorption loss on the internal surface of cylinders

To estimate the adsorption loss of acetonitrile on the internal surface of the cylinder, we employed the cylinder-to-cylinder division method²⁹ (Lee et al., 2017) for 3 nmol^{−1} mol^{−1} gas mixtures prepared in all three types of cylinders. The division method involved transferring a gas mixture from one cylinder to another^a new cylinder^b of the same type. Ideally, the peak area ratio of acetonitrile in the two cylinders should be equal to one within the analytical uncertainty, indicating little adsorption loss. However, while the ratios of hexane remained equal to one for all cylinders, those of acetonitrile were notably lower, showing approximately 12%, 22%, and 98% decreases in peak areas in the Experis, Performax, and Untreated cylinders, respectively (Fig. 3). This suggests about 6%, 11%, and 49% loss of acetonitrile during its gravimetric preparation, primarily attributed to substantial adsorption on the internal surface of the cylinders. This significant loss describes^c indicates

that all three types of cylinders are unsuitable for preparing PSMs [less than a](#) [amount fractions below](#) 10 nmol mol^{-1} without [further](#) proper passivation of the internal surfaces to minimize adsorption loss.





200 **Figure 3.** Adsorption loss results of (a) acetonitrile and (b) hexane at various amount fractions. The error bars show expanded uncertainties ($k=2$). The in the Experis (rectangle), Performax (circle) and Untreated (triangle) cylinders. Note that the y-axis and x-axis represents the normalized response factor (RF) and cylinder numbers, respectively, and the error bars show expanded uncertainties ($k=2$).

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205 Furthermore, we prepared additional gas mixtures exclusively in the Performax cylinders at $200 \text{ nmol mol}^{-1}$, about 70 times higher amount fraction than 3 nmol mol^{-1} , to evaluate whether the adsorption loss was negligible at such a higher amount fraction, given that acetonitrile at 3 nmol mol^{-1} in the cylinders was consistent in only Performax cylinders despite its loss (Fig. 2). However, we still observed about 0.9% (at the first division) and 5% (at the second division) adsorption loss of acetonitrile at $200 \text{ nmol mol}^{-1}$. While relative adsorption losses decreased compared with 11% at 3 nmol mol^{-1} , they were still

210 larger than analytical uncertainties. To further investigate, we conducted ~~addition~~additional tests using $10 \mu\text{mol mol}^{-1}$ (more than 3000 times higher than 3 nmol mol^{-1}) gas mixtures ~~in both~~. Thus far in the study, we developed $10 \mu\text{mol mol}^{-1}$ gas mixtures in all three types of cylinders, previously prepared Experis cylinders (Fig. 1a) and additionally prepared Performax and Untreated cylinders. ~~Results~~ (Fig. 1b). The consistency test was conducted on all three types of cylinders alongside, and results showed that *RFs* of the Experis cylinders were about 3 % to 6 % lower than those of Performax and Untreated cylinders
215 ~~for acetonitrile, however hexane in all cylinders showed good agreement. As observed in the prior test results of gas mixtures less than 10 nmol mol^{-1} , acetonitrile *RFs* were not consistent across all three Experis cylinders at even $10 \mu\text{mol mol}^{-1}$, indicating that the adsorption loss persists at higher levels and the amount of loss varies from cylinder to cylinder. Therefore, Experis cylinders were excluded from the adsorption loss evaluation, and adsorption loss tests were conducted on other two types of cylinders. The results showed little loss~~ ~~for~~, which is less than its associated relative analytical uncertainties (about 0.6 % for
220 acetonitrile and 0.2 % for hexane), concerning both acetonitrile and hexane in the Performax cylinders, ~~whereas~~. In contrast, approximately 1 % to 2 % loss of acetonitrile was observed in the Untreated cylinders. The results indicated that, while the effect of the adsorption loss at $10 \mu\text{mol mol}^{-1}$ was nullified for acetonitrile in the Performax cylinders, it persisted in the Untreated cylinders.

3.3 Evaluation of gas mixtures at $100 \text{ nmol mol}^{-1}$ prepared using modified gravimetric method

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225 ~~Acetonitrile~~ Adsorption loss was nullified only in Performax cylinders at $10 \mu\text{mol mol}^{-1}$, while significant acetonitrile loss was observed in both Experis and Untreated cylinders at the same amount fraction. Therefore, acetonitrile gas mixtures were prepared at $100 \text{ nmol mol}^{-1}$ ~~were prepared~~ in Performax cylinders using a modified gravimetric method ~~since the effect of the adsorption loss was only nullified in the Performax cylinders at $10 \mu\text{mol mol}^{-1}$~~ . For comparison, two additional gas mixtures were prepared in Performax cylinders using the conventional gravimetric method. The consistency of four gas mixtures (i.e.,
230 two for each method) was evaluated by comparing the normalized *RFs*. Hexane exhibited consistency across all four cylinders, with a relative expanded uncertainty of 0.5 % ($k = 2$) regardless of the preparation method. However, acetonitrile showed consistency only within each method (Fig. 4-~~J~~). Furthermore, the normalized *RFs* of the gas mixtures prepared using the modified method were ~~about~~approximately 5 % higher than those prepared using the conventional method. This discrepancy can be attributed to the fact that, unlike the conventional method, the modified method negated the adsorption loss
235 on the internal surface of cylinders, unlike the conventional method. Thus, these results indicate~~suggest~~ that the modified method ~~could~~may be preferable for preparing acetonitrile PSMs at $100 \text{ nmol mol}^{-1}$ rather than the conventional method.

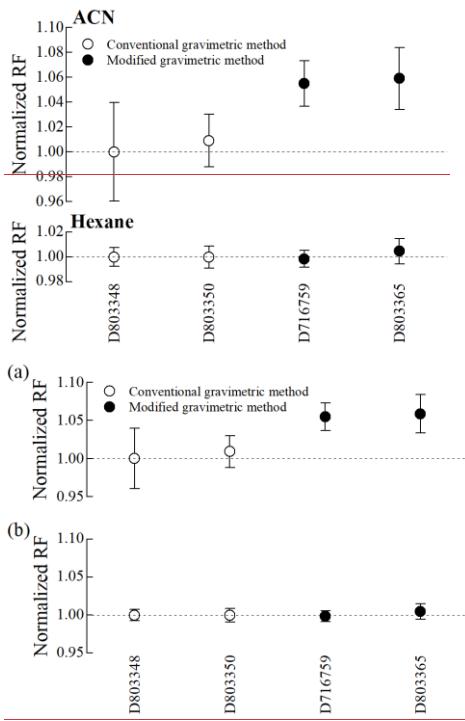


Figure 4. Verification results of the $100 \text{ nmol mol}^{-1}$ (a) acetonitrile and (b) hexane in Performax cylinders. Error Note that the y-axis and x-axis represents the normalized response factor (RF) and cylinder numbers, respectively, and the error bars show expanded uncertainties. ($k = 2$).

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3.4 Long-term stability of acetonitrile PSMs at $100 \text{ nmol mol}^{-1}$

When developing a PSM, ensuring its long-term stability is ~~erucial~~essential for disseminating calibration standards and monitoring both the long-term trend and the variability of acetonitrile in the atmosphere. ~~Long~~The long-term stability was assessed for gas mixtures prepared using the modified method was assessed through two approaches: comparing response ratios (i.e., peak area ratios) of acetonitrile to hexane in each cylinder for 10 months (Fig. 5.a5a) and comparing RFs~~RFs~~ of new cylinders to those of old cylinders over 3 years (Fig. 5.b5b). For the 10-month stability assessment, the response ratios of acetonitrile to hexane in each of the two cylinders agreed~~were in agreement~~ within a relative expanded uncertainty of 2.2% ($k = 2$), indicating stable acetonitrile levels for 10 months (Fig. 5.a5a). In the case of the 3-year stability, two new gas mixtures prepared in 2022 were compared with an old gas mixture prepared in 2019. The normalized RFs~~RFs~~ of acetonitrile in both old

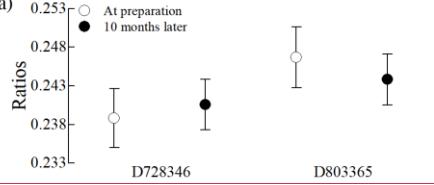
and new cylinders showed inconsistency within a relative expanded uncertainty of 0.6 % ($k = 2$), with a difference of about 2.5 %. This difference exceeded the analytical uncertainties, indicating a gradual decrease in acetonitrile levels at 100 nmol mol^{-1} in Performax cylinders over three years. Although the three-year stability of acetonitrile meets the target uncertainty (5 %) of the WMO GAW programme, further studies (e.g., improved passivation methods) are necessary to develop more accurate and stable acetonitrile PSMs at nmol mol^{-1} levels.

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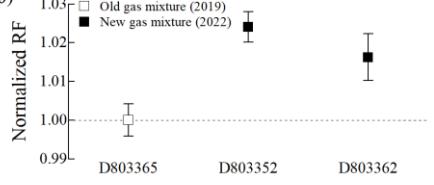
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accurate and stable acetonitrile PSMs at nmol mol^{-1} levels.

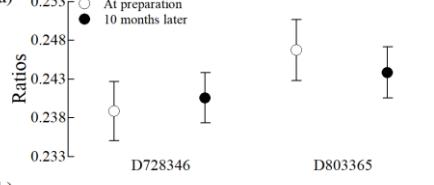
(a)



(b)



(a)



(b)

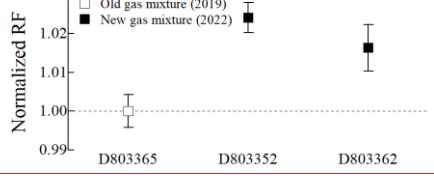


Figure 5. Long-term stability of the 100 nmol mol^{-1} acetonitrile in the Performax cylinders. (a) 10 month-stability (peak area ratios of hexane to acetonitrile). (b) 3 year-stability (RFs of the new gas mixtures are normalized to that of an old gas mixture). Error bars represent the normalized response factor (RF) and cylinder numbers, respectively, and the error bars show expanded uncertainties. ($k = 2$)

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3.4 Long-term stability of acetonitrile PSMs at 100 nmol mol⁻¹

The results from the previous section indicated that the modified method effectively addressed the issue of adsorption loss on the inner surface of cylinders. However, despite this improvement, there was a gradual decrease in the amount fraction of 265 acetonitrile at 100 nmol mol⁻¹ (Fig. 5b). To further assess the long-term stability, we evaluated the parent gas mixtures (10 $\mu\text{mol mol}^{-1}$) of 100 nmol mol⁻¹ acetonitrile gas mixtures in Performax cylinders (Fig. 4b) by comparing the RFs of new gas mixtures against an old one (D726463) to assess the three-year stability. The normalized RFs in all four gas mixtures (old and new ones) were consistent within their associated relative expanded uncertainties of 0.90 % ($k = 2$) (Fig. 6). These results indicated that 10 $\mu\text{mol mol}^{-1}$ acetonitrile in Performax cylinders remained stable for about three years.

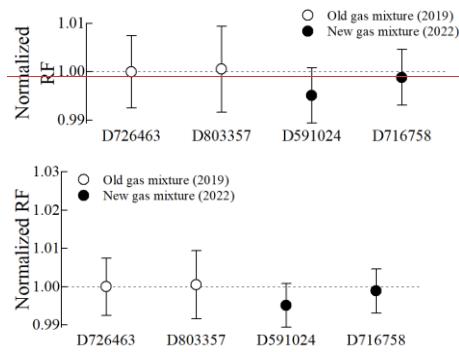


Figure 6. Long-term stability of the 10 $\mu\text{mol mol}^{-1}$ acetonitrile in the Performax cylinders. ~~Note that the y-axis and x-axis represents the normalized response factor (RF) and cylinder numbers, respectively, and the error bars show expanded uncertainties ($k = 2$).~~

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275 4 Conclusions and outlook

To support global atmospheric monitoring and enhance our understanding of the atmospheric processes and the roles of 280 acetonitrile in air quality and climate changes, we evaluated the feasibility of three different types of cylinders for preparing gravimetric gas mixtures and then developed acetonitrile primary standard gas mixtures (PSMs). This involved included evaluating adsorption loss and long-term stability of acetonitrile in aluminium cylinders with three different surface treatments at both nmol mol⁻¹ and $\mu\text{mol mol}^{-1}$ levels. Our study revealed that all three types of cylinders tested in this study were unsuitable for developing acetonitrile PSMs below 10 nmol mol⁻¹, due to significant loss (from 6 % to 48 %) on the inner surface of cylinders during the preparations, unless further additional surface treatments were developed and applied. However, applying the modified gravimetric method effectively mitigated adsorption loss at 100 nmol mol⁻¹, resulting in good consistency among gas mixtures prepared in Performax cylinders, which remained stable for consistent after 10 months.

285 Nevertheless, a subsequent stability study based on the 10-months stability showed a gradual decrease (about of

approximately 2.5% within less than % over three years after preparation) in acetonitrile levels, with a decrease rate of approximately 0.9 % per year. On the other hand, for, indicating that acetonitrile is predicted to be stable for 3 years with a relative expanded uncertainty of 3 %. For 10 $\mu\text{mol mol}^{-1}$ acetonitrile gas mixtures in Performax cylinders, we observed little adsorption loss, good consistency, and 3-years long-term stability, making them suitable as PSMs. Based on these findings, 290 we can disseminate acetonitrile calibration standards at 100 nmol mol^{-1} with a relative expanded uncertainty of 3 % (meeting the target uncertainty of the WMO GAW programme) and at 10 $\mu\text{mol mol}^{-1}$ with a relative expanded uncertainty of 1%. % can be disseminated with an expiration period of at least 3 years for global atmospheric measurements. However, it is important to note that the amount fractions of acetonitrile calibration standards that can be disseminated areis much higher than atmospheric levels, particularly in remote background areas. Therefore, further studies are still needed to evaluateexplore 295 alternative methods, such as dynamic dilution, permeation, and dynamic gravimetric methods, to generate accurate and stable acetonitrile gas mixtures at levels below 10 nmol mol^{-1} , closer to more representative of atmospheric concentrations. In addition, future investigations can explore the use of electropolished stainless steel cylinders and Sulfinert® (i.e., SilcoNert® 300 2000) treatment as a passivation option. The silicon-based barrier in Sulfinert® treatment is chemically inert to most organic compounds (Barone et al., 2011; Vaittinen et al., 2013) and its non-polar surface could reduce the interaction with polar groups (Morris and Isbister, 1986) such as acetonitrile which is moderately polar molecule (Zarzycki et al., 2010). Although the 305 internal surface area of the valves was much less than that of the cylinders, it could be worth evaluating the impacts of different valve materials and coating methods for developing acetonitrile gas mixtures at nmol mol^{-1} levels.

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Author contribution. SL and JHK designed the experiments, and both JHK and BT carried them out. BT and SL prepared the 305 manuscript with contributions from all co-authors.

Competing interests. The contact author has declared that none of the authors has any competing interests.

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