



# 1 Implementation and application of an improved phase spectrum

# 2 determination scheme for Fourier Transform Spectrometry

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16 Abstract. Correct determination of the phase spectrum is a highly relevant task in Fourier Transform Spectrometry for 17 concluding which spectral distribution connects with the measured interferogram. We present implementation of an improved scheme for phase determination in the operational Collaborative Carbon Column Observing Network (COCCON) 18 19 processor. We introduce a robust unwrapping scheme for retrieving a connected phase spectrum at intermediate spectral 20 resolution, which uses all spectral positions carrying enough signal to allow a significant determination of the phase. In the 21 second step, we perform a least squares fit of model parameters of a suited analytical phase spectrum model through all 22 reliable phase values constructed in the first step. The model fit exploits the fact that we expect the phase to be spectrally 23 smooth. Still, it can be refined to reflect specific characteristics inherent to the optical and electronic layout of the interferometer. The proposed approach avoids the problems of the classical phase reconstruction method, which enforce a 24 25 spectrally smooth phase by directly limiting spectral resolution when calculating the complex phase. Thereby, the phase is 26 created from a very low number of interferogram points around the centerburst of the interferogram, which results in a 27 suboptimal noise propagation from the interferogram into the spectral domain. Moreover, the interpolation of the phase 28 spectrum across spectral subsections with reduced spectral signal is not well behaved and results depend strongly on the 29 numerical apodization function used for creating the low-resolution phase.





#### 30 1 Introduction

31 Fourier Transform Spectrometry is an important technique for remote observation of atmospheric composition, especially in 32 the near and mid infrared spectral regions (then mostly referred to as Fourier Transform Infrared or shortly FTIR spectroscopy). Ground-based networks contribute to the long-term monitoring of chemical composition, as the Network for 33 34 the Detection of Atmospheric Composition Change (NDACC) network [De Mazière et al., 2018], and the Total Carbon 35 Column Observing Network (TCCON) [Wunch et al., 2011] and the COllaborative Carbon Column Observing Network 36 (COCCON) [Frey et al., 2019; Sha et al., 2020; Alberti et al., 2022], which focus on the provision of precise and accurate 37 observations of column-averaged greenhouse and other climate and air quality relevant gas abundances. Moreover, highly 38 successful space borne sensors as Michelson Interferometer for Passive Atmospheric Sounding (MIPAS) onboard the Environmental Satellite (ENVISAT) [Fischer et al., 2008], Atmospheric Chemistry Experiment - Fourier Transform 39 40 Spectrometer (ACE-FTS) onboard SCISAT [Bernath and al., 2005], and the Thermal And Near infrared Sensor for carbon Observation - Fourier Transform Spectrometer (TANSO-FTS) onboard Greenhouse gases Observing SATellite (GOSAT) 41 42 [Yokota et al., 2009] and its successors have proven the usefulness of FTIR spectrometry for atmospheric observations. 43 Recently, the airborne imaging FTIR sensor Gimballed Limb Observer for Radiance Imaging of the Atmosphere (GLORIA) for chemical and thermal limb imaging has been realized [Friedl-Vallon et al., 2014] and the imaging FTIR satellite mission 44 Changing Atmosphere Infrared Tomography (CAIRT) derived from GLORIA is under phase A study by ESA 45 46 [https://www.cairt.eu].

47 All FTIR spectrometers have in common that they use a two-beam interferometer for creating modulated intensity levels as a 48 function of the path difference between the two arms of the interferometer. The path difference is varied as function of time, and during such a scan, the variable intensity is recorded by a detector element. By use of a co-recorded reference 49 modulation generated from a reference laser fed through the same interferometer, the variable intensity level recorded by the 50 infrared detector as function of time can be sampled as function of optical path difference x. It can be shown that the Fourier 51 52 Transform of the AC-coupled interferogram is associated with the spectral distribution of the incident radiation. If the interferogram I(x) would be symmetric around a common zero path difference (ZPD) of the interferometer for any 53 wavenumber v, the spectral radiance as function of wavenumber S(v) would be connected with the interferogram via a 54 55 simple cosine transform:

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$$S(\nu) \int_{x=-\infty}^{+\infty} I(x) \cos(2\pi\nu x) dx$$
(1)

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We only claim a proportionality here for any selected wavenumber position, because from the practical viewpoint, the determination of radiances in absolute units requires proper calibration measurements using reference sources providing a known radiance level. This is a very laborious task and it is difficult to achieve sub-percent accuracy in the realization of absolute units. In case of emission spectroscopy, this task needs to be solved, while atmospheric absorption spectroscopy





generally omits this procedure. In the case of absorption spectroscopy, the quantitative trace gas analysis is built on the local 63 contrast between absorption lines and adjacent continuum (assuming that the spectrometer offers sufficient spectral 64 65 resolution for resolving individual lines). Then, by assuming that the spectrally variable sensitivity of the spectrometer, 66 created by optical, detector, and electronic characteristics is spectrally smooth, no attempt is made for achieving ordinate calibration. A section of the measured spectrum used for the trace gas analysis is then treated as a transmission spectrum, and 67 an empirical fit of continuum background is included in the analysis scheme. We do not further follow the problem of 68 69 ordinate calibration here, because it is not related to our aim of an improved phase reconstruction, which, however, can be 70 used for both absorption and emission spectroscopy.

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In equation (1), we have extended the integration over all optical path differences. In practice, only a limited section up to a maximum optical path difference (MPD) is accessible. The truncation of the interferogram is equivalent to a multiplication with a boxcar function. This spectral response inherent to an FTIR spectrometer can be adjusted by applying a numerical weighting function along the interferogram (the process of apodization). A proper description of the instrumental line shape (ILS) is further complicated due to the presence of practical imperfections of the interferometer. Finally, we do not further follow the problem of spectral ordinate calibration here, because it, too, is not closely related to our aim of an improved phase reconstruction.

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In order to provide a proper idea of the practical method of FTIR spectroscopy here, we further need to mention that the data 80 81 recording and processing is digital. An analogue-to-digital (ADC) converter is used to generate a digitized signal from the 82 detector signal. While sample-and-hold ADCs triggered by the laser sampling were used in the past, many manufacturers of FTIR spectrometers today use widely available audio ADCs which offer high digitization depth (e.g. 24 bit) and add a final 83 84 interpolation step from the raw sampling equidistant in time domain into a sampling record equidistant in space [Brault, 85 1996]. In any case, the signal to be processed is discretely sampled, and in practice fast computational schemes for doing discrete Fourier transforms are applied. Due to the discrete sampling process, integrals as shown in equation (1) become 86 87 sums and the bandwidth of the recorded signal needs to be properly limited in order to avoid aliasing.

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A final aspect, which is closely connected to the considerations developed hereinafter, is the origin of the phase spectrum. Due to residual optical asymmetry of the beamsplitter and possibly between the arms of the interferometer and due to frequency dependent electronic delays, the resulting interferogram tends to be asymmetric and a global ZPD position common to all wavenumbers does not exist. The electronic delays introduce both a shift between the laser reference and the signal, as well as frequency-dependent delays in the infrared signal. This requires treatment of the Fourier Transform of the real-valued interferogram as a complex quantity (so arising out of cosine and sine contributions) and thereby gives birth to the concept of the phase spectrum. In complex notation, we can state



(2)

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$$s(v) = |s(v)|e^{i\varphi(v)} = \int_{x=-\infty}^{+\infty} I(x)e^{-i2\pi vx} dx$$

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The uncalibrated signal s(v) now is a complex quantity. It can be separated into amplitude and phase  $\varphi(v)$ . The phase spectrum  $\varphi(v)$  describes how the phase angle of the harmonic oscillations which make up the interferogram evolves as function of wavenumber. From the instrumental viewpoint, we expect the phase spectrum to be spectrally smooth, as the impacting factors (optical dispersion and electronic delays) typically vary slowly as function of frequency.

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The smoothness of the phase spectrum in near and mid-infrared FTIR spectroscopy is verified empirically on scales of several to tens or even hundreds of wavenumbers (cm<sup>-1</sup>). Given this, the simple approach of interpreting the absolute value of the resulting complex spectrum as the measured spectral signal is clearly suboptimal in the presence of noise in the interferogram. The assumption of uncorrelated white noise typically is adequate. This noise maps into white noise in the complex spectrum. A contribution of 1/f noise might increase the noise amplitude towards low frequencies, and at very low frequencies, source noise might become dominant. Therefore, working at higher scan speeds is generally preferred.

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The assumption of a spectrally smooth phase allows to separate at each spectral position the complex spectrum into two orthogonal components: the component along the direction we expect the spectral signal to be oriented, and the component orthogonal to this direction. So, by exploiting the concept of a spectrally smooth phase, the noise mapped into the orthogonal component can be avoided, only the noise along the signal component is unavoidable. Moreover, this approach avoids the spectral noise floor of becoming a positive bias in opaque spectral subsections, as it would occur when simply using the absolute value of the complex spectrum.

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In order to make the scheme of a smooth phase a working concept, we not only rely on the assumption that it actually is spectrally smooth, but we also need a practical approach for constructing a smooth phase spectrum with a noise level significantly below the noise level of the complex spectrum. In practice, we achieve this by using only a short section of the interferogram around ZPD. Thereby, the smooth phase spectrum is set by the equation

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123 
$$|s(v)|e^{i\varphi(v)} = \int_{x=-\varepsilon \cdot MPD}^{+\varepsilon \cdot MPD} I(x)e^{-2\pi vx} \cdot A(x)dx$$
(3)

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Here, the dimensionless multiplier  $\varepsilon$  denotes that only a fraction of the complete interferogram recorded up to MPD is used. The function A(x) denotes a strong numerical apodization function, as any non-local ringing extending out from a spectral position with high signal level would disturb the phase in the surrounding spectral region.





129 We finally need to mention that interferograms might be recorded "single-sided" or "double-sided". Often, when an interferometer is designed for achieving higher spectral resolution, the symmetry of the design is abandoned. Instead, the 130 131 ZPD position shifted near one end of the mechanical scan range, which still needs to be wide enough to reconstruct the phase 132 spectrum via equation (2), but the high-resolution details are inferred from the single remaining side of the interferogram which is recorded. Our proposed method can be used in either situation, but it should be noted that in case of single-sided 133 134 interferogram recording, the error propagation of a residual phase error is much more critical, as sine contributions do not 135 cancel out (as one side of the interferogram is missing) [Brault, 1996; Brasunas and Cushman, 1997], so a very accurate 136 reconstruction is even more relevant in this case.

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The reader finds detailed presentations of all the aspects of FTIR spectroscopy shortly summarized above in text books and articles [Herres and Gronholz, 1985; Davis et al., 2001; Griffiths et al., 2007].

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In section 2, we present the types of spectrometers we used to test the proposed phase correction method. Section 3 describes a robust scheme for phase unwrapping and the fitting procedure for retrieving the parameters of the phase model. Section 4 investigates the characteristics of phase spectra for the spectrometers introduced in section 2.

#### 144 2 Materials and Methods

This work has been performed in the framework of the FRM4GHG project (Fiducial Reference Measurements for Greenhouse Gases; <u>https://frm4ghg.aeronomie.be/</u>) supported by European Space Agency (ESA) [Sha et al., 2020]. In the framework of this project, among further topics related to fiducial reference measurements (FRM), the adequacy of different portable spectrometers is investigated. Interferograms recorded with these spectrometers have been used for testing the proposed phase reconstruction algorithm. We shortly present these spectrometers in the following.

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151 The EM27/SUN Fourier-transform spectrometer (FTS) prototype has been developed by Karlsruhe Institute of Technology 152 (KIT) in cooperation with Bruker Optics, a well-known manufacturer of FTIR spectrometers. It uses a folded pendulum-153 corner cube interferometer ("RockSolid" ® design) and employs two room temperature InGaAs detectors to cover the near-154 infrared range from 4000 - 12 000 cm<sup>-1</sup>. A solar tracker using Camtracker active feedback to control the position of the solar 155 image on the fieldstop of the spectrometer is directly attached to the spectrometer [Gisi et al., 2011]. Further instrumental 156 details of the EM27/SUN FTS design characteristics are provided by Gisi et al. (2012) and Hase et al. (2016). Since 2014, 157 the EM27/SUN FTS is available from Bruker as a commercial item. Meanwhile, more than hundred units are sold and are operated worldwide by various working groups for atmospheric greenhouse gas measurements; they are especially suited for 158 159 the quantification of local sources as cities [Hase et al., 2015], coal mines [Luther et al., 2019; Luther et al., 2022], oil and gas production areas [Kille et al., 2019], and landfills [Tu et al., 2022]. As an operational framework for guaranteeing 160





common instrumental and data analysis standards among the operators, the COCCON has been established since [Frey et al.,
2019; Alberti et al., 2022], which is significantly supported by ESA through FRM4GHG and further contracts.

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164 The Bruker IRcube or "Matrix" FTIR is a compact OEM instrument operating in the mid or near IR regions and configurable for a wide range of laboratory and industrial applications using a range of sampling accessories. In its basic form it contains 165 166 a folded pendulum-corner cube interferometer similar to the EM27/SUN ("RockSolid" ® design) with 25mm beam diameter and either 1 cm<sup>-1</sup> double-sided or 0.5 cm<sup>-1</sup> single-sided resolution. As used at the University of Wollongong for solar 167 168 measurements, the IRcube includes a source module which accepts a focussed input beam into a selectable aperture (the field 169 stop) and collimates it, the interferometer, and detector optics module focussing the parallel beam exiting the interferometer 170 onto a 1mm InGaAs detector via a short focal length off axis paraboloidal mirror. The solar beam is collected from a solar-171 tracker-mounted telescope via a 20 m optical fibre – the beam exiting the fibre is focussed into the field stop of the IRcube's 172 source module.

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174 The Vertex70 spectrometer is produced and sold commercially by Bruker Optics. It was recently replaced in Bruker's 175 production line by a successor named Invenio. One Vertex70 FTS was purchased in the framework of the FRM4GHG 176 campaign to be tested alongside the EM27/SUN and IRCube with the reference IFS125HR and AirCore measurements. The 177 Royal Belgian Institute of Space Aeronomy (BIRA-IASB) and the University of Bremen (UB) performed minor 178 modifications to the optical components of the Vertex70 and coupled it with a solar tracker to perform solar absorption 179 measurements. The feasibility to accommodate two detectors (InGaAs and InSb) in the spectrometer allows covering 180 simultaneously the near- and mid-infrared (NIR and MIR) spectral regions. The measured spectra are analysed to retrieve column abundances of XCO<sub>2</sub>, XCH<sub>4</sub>, XCO and XH<sub>2</sub>O in the NIR spectral region and column abundances of methane (CH<sub>4</sub>), 181 nitrous oxide (N2O), formaldehyde (HCHO) and carbonyl sulphide (OCS) in the MIR spectral region are currently studied 182 183 [Zhou et al., 2023; Sha et al., 2024]. The spectrometer showed comparable results for the retrieved trace gases as those 184 retrieved with the high spectral resolution FTIR spectrometers. An automated enclosure system has been developed to 185 deploy the spectrometers autonomously in the field and enhance the coverage of the fiducial reference FTIR data. The aim is also to use it in future as a traveling standard improving consistency among FTIR data taken at different sites in the MIR 186 187 spectral region. The NIR retrieved target gases are part of the COCCON while the data retrieved in the MIR spectral range 188 can complement the NDACC-FTIR data. This activity is supported by ESA through FRM4GHG contracts.

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190 The Izaña Observatory (IZO) is a high-mountain station located on the island of Tenerife (Canary Islands, Spain) in the

191 subtropical North Atlantic Ocean (28.3°N, 16.5°W) at an altitude of 2.37 km a.s.l. IZO is managed by the Izaña Atmospheric

192 Research Centre (IARC, https://izana.aemet.es/, last access: 5 August 2024), which belongs to the State Meteorological

193 Agency of Spain (AEMet). Within the IZO's atmospheric research activities, the FTIR programme started in 1999 in the

194 framework of a collaboration between AEMET and KIT [Schneider et al., 2005], contributing to NDACC and TCCON





networks since 1999 and 2007, respectively. To do so, the IZO FTIR instrument, currently a Bruker IFS125HR based on a Michelson interferometer, records high-resolution solar absorption spectra in the MIR region within NDACC activities and in the NIR region for TCCON retrievals, using a set of different field stops, narrow-bandpass filters, and detectors [Schneider etThis al., 2010; García et al., 2021].

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For TCCON the IFS125HR FTIR measures between 4000 and 10,000 cm<sup>-1</sup> at a spectral resolution of 0.02 cm<sup>-1</sup> (MPD of 45 cm) using a calcium fluoride (CaF<sub>2</sub>) beamsplitter, an extended Indium–Gallium–Arsenide (InGaAs) photodiode detector operated at room temperature, and no optical filters. The operational TCCON spectra are the result of co-adding six singlesided interferograms in order to increase the signal-to-noise ratio. These interferograms are acquired with a scanner velocity of 20 kHz, so the acquisition of one solar spectrum lasts about 4 minutes.

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## 206 **3 New Phase reconstruction scheme**

207 The drawback of the classical method described in the introduction is twofold. (1) The reduction of the phase spectrum to the 208 desired very low resolution is achieved explicitly by using a very short section of the interferogram around ZPD for the 209 Fourier transform [Mertz, 1965; Forman et al., 1966]. This approach neglects interferogram data points further out which 210 still could contribute information on the phase. (2) The resulting spectral interpolation as part of the procedure is not well-211 defined especially across spectral sub-regions of increased opacity, as they occur in solar absorption spectroscopy between 212 the atmospheric window regions and in strong absorption bands. Because the phase spectrum across such a region is strongly 213 impacted by the overlapping contributions to the phase emerging from either side of the opaque region, the outcome for the 214 phase at a certain spectral position in the region with reduced transmission will depend on the user-selected resolution for the 215 phase calculation and the chosen apodization function.

216

We will achieve our enhanced reconstruction of the phase spectrum by fitting a smooth parameterized phase model through a calculated phase spectrum, which preserves higher spectral resolution than required for the desired degree of spectral smoothness. The smoothness of the phase spectrum is ensured by the phase model used, while avoiding the aforementioned problems of the classical method. We use a least squares fit of the model to the raw phase spectrum, which is a well-defined process with respect to interpolation. A similar method has been proposed by Learner et al., 1995, in the context of emission spectra.

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The phase spectrum is a function of angular orientation, so it is invariant under phase shifts of size  $\pm 2\pi n$ , with n = 1,2,3,...For our fit procedure, we need to ensure that the raw phase used as input does not include jumps between such branches. We suggest the very robust procedure summarized as procedural steps in Table 1.





- This proposed method can fail if the phase difference calculated in step 5 is greater than  $\pm \pi$ . We did not encounter this situation, but it may occur if the phase slope is very steep and can possibly be avoided by appropriate repositioning of the
- 229 ZPD point when calculating the Fourier Transform.
- 230

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231	I able 1. sten-by-sten ni	rocedure for developing fl	he raw nhase used as in	nut for the model fif
231			ne raw phase used as m	put for the model m.

Step #	Procedure	Comment
0	Allocation of arrays:	
	(1) float array for accepting phase values	
	(2) logical array indicating availability of valid phase value	
1	Establish the noise level and the size of potential artefacts	
	superimposed on the spectral signal. Set a threshold $T$ for the	
	subsequent phase calculation significantly above noise and	
	artefact levels.	
2	Search for position of max amplitude of $s(v_i)$ in the complex	Restrict search to relevant optical
	signal in the optical bandpass.	bandpass, as out-of-band artefacts
		triggered by source brightness fluctuation
		might create very big amplitudes at $\nu \approx 0$ .
3	Calculate phase at spectral index istart with max signal	Use a quadrant-sensitive atan2 function
	amplitude.	on real and imaginary part of the complex
		signal.
4	Move from current position one spectral index up. If still within	
	the defined spectral bandwidth, check whether $s(v_i) > T$ . If so,	
	set logical array value of current position to true, otherwise to	
	false.	
5	If the logical array value of the current position $i$ is true,	Use the value of the cross product between
	calculate the phase difference between the nearest preceding	the normalized complex pointers:
	point <i>j</i> assigned <i>true</i> and the current position.	$\Delta \varphi(j \to i) = asin \left\{ \frac{\left( s(v_j) \times s(v_i) \right)}{ s(v_j)  s(v_i) } \right\}$
6	Calculate the new phase value at the current position using the	$\varphi(i) = \varphi(j) + \Delta \varphi(j \to i)$
	phase value of the nearest preceding point	
7	Continue steps $4 + 5 + 6$ until the upper limit of the spectral	
	bandwidth is reached.	





8	Return to position <i>istart</i> and use the corresponding procedure
	in downwards direction until the lower limit of the spectral
	bandwidth is reached.
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234 The second step is to fit the parameters of the phase model to the raw phase values. We assume here use of a model linear in 235 the model parameters to be fitted. However, nonlinear models also can be handled in our approach by implementing an 236 iterative search for the optimal model parameter values. If a sophisticated model is chosen, which intends to describe actual 237 physical characteristics of the spectrometer (dispersion curves, electronic response characteristics) and retrieves physical 238 quantities (layer thicknesses, capacitances, resistor values), using a model which is nonlinear in the parameters might be 239 unavoidable. When constructing ad-hoc models which simply enforce smoothness, the choice of a simple linear model seems 240 advisable. The fitting procedure needs to be restricted to points for which valid phase values were established in the previous 241 step. The fitting procedure can take into account a weighting according to the squared signal amplitude. We found very little effect of including this refinement in the determination of model parameters, so we did not implement it in the current pre-242 243 processing scheme. Taking a weighting into account, the equation for fitting the phase model parameters becomes

245 
$$\vec{p}_{model} = (K^T W K)^{-1} K^T W \vec{\varphi}_{raw}$$
(4)

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Here,  $\vec{p}_{model}$  is the set of model parameters, *K* is the Jacobean matrix, which holds the derivatives of the phase model at each spectral grid point with valid raw phase entry, *W* is a diagonal matrix with  $\frac{1}{(s(v_l))^2}$  entries (again, for each spectral grid point with valid raw phase entry), and  $\vec{\varphi}_{raw}$  is the vector containing all valid raw phases. Note that the vector dimension of  $\vec{\varphi}_{raw}$ and  $\vec{p}_{model}$  differ, as after receiving the set of model parameters,  $\vec{p}_{model}$  can be calculated at all spectral positions, including interpolation across near opaque spectral sections and extrapolation beyond the first or last spectral point found in the optical bandpass. The predicted model phase values further outside of the relevant spectral bandpass are meaningless and might be suppressed altogether (by allocating the array for  $\vec{p}_{model}$  to fit the relevant spectral bandpass).

#### 254 4 Results

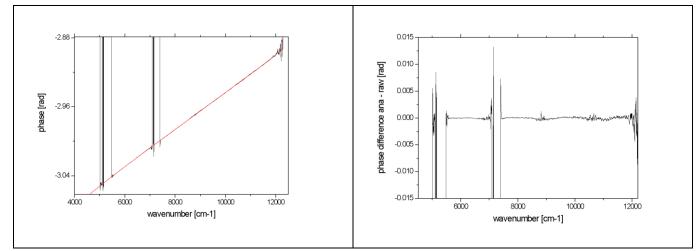
For the actual work on the FTIR spectrometers introduced in section 2, we used a polynomial model of order 7. The raw phase calculation uses a resolution of about 10  $cm^{-1}$ , which is supported by all spectrometers we included in the study (sufficient number of points on the short side of the interferogram).





#### 258 4.1 Phase spectrum of the EM27/SUN FTS

259 The results achieved for the EM27/SUN are shown in Figure 1. The spectrometer shows a remarkably linear phase spectrum 260 across the whole spectral region of the main detector (covering 5000 to 12000 cm<sup>-1</sup>). The differences between the model fit 261 and the raw phase are below 1 mrad. The level of smoothness and linearity of the phase spectrum is outstanding among all 262 spectrometers tested. This behaviour probably is supported by the beamsplitter design. The same optical plate is passed twice 263 by the radiation, acting as substrate of the beam-splitting coating layer in one passage and as compensating plate in the other passage. In addition to this, also the analogue electronic chain seems to introduce only minimal dispersion due to runtime 264 265 effects. It is not clear why the other spectrometers investigated here, all built by the same manufacturer, show significantly 266 stronger structures in the phase spectrum.



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Figure 1: EM27/SUN phase spectrum. Left panel: raw phase (black) and fitted model (red). Right panel: difference between model (analytical, ana) and raw phase (raw). The gaps in the raw phase are due to opaque spectral sections.

#### 270 **4.2 Phase spectrum of the IRCube FTS**

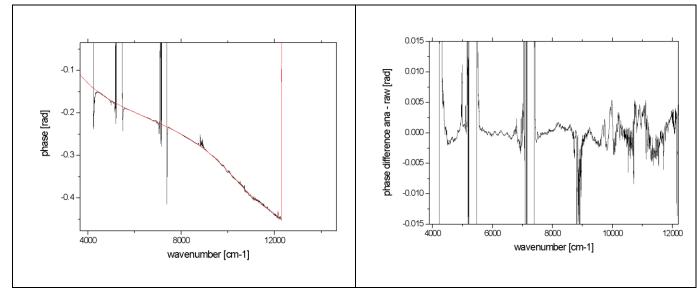
The phase spectrum of the IRCube is shown in Figure 2. The spectral bandpass covers the range of 4000 to beyond 12 000

272 cm<sup>-1</sup>. The differences between the phase model and the raw phase show more structure than in case of the EM27/SUN, but

still, these oscillatory features are largely within 2 mrad.







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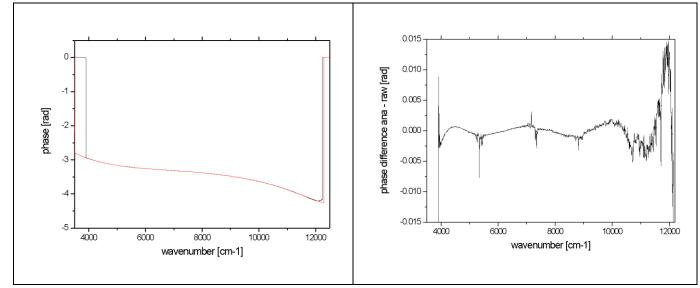
Figure 2: IRCube phase spectrum. Left panel: raw phase (black) and fitted model (red). Right panel: difference between
model (analytical, ana) and raw phase (raw). The gaps in the raw phase are due to opaque spectral sections.

#### 278 4.3 Phase spectrum of the IFS125HR FTS operated at Izaña

279 The phase spectrum of the IFS125HR operated at the Izaña observatory is shown in Figure 3. The spectral bandpass covers 4000 to beyond 12 000 cm<sup>-1</sup>. Due to the facts that Izaña is a high-altitude site and a low threshold value for the phase 280 281 calculation was used because of the very low noise level of the measurements, there are no gaps in the raw phase. Some 282 structure can be seen in the model minus raw phase difference, but this is still within mostly 2 mrad apart from the highest wavenumbers. The curvature of the phase is somewhat stronger than in case of the IRCube. The sharp peaks occurring 283 284 around 5400 and 7200 cm<sup>-1</sup> are coinciding with near-opaque regions of the spectrum and might hint at superimposed 285 spurious signals, potentially due to residual nonlinearity. Such spurious signals generally possess a phase orientation 286 different from the real signal. This finding demonstrates that the model-fitting approach presented here might also be useful 287 for detecting different kinds of imperfections in measured spectra.







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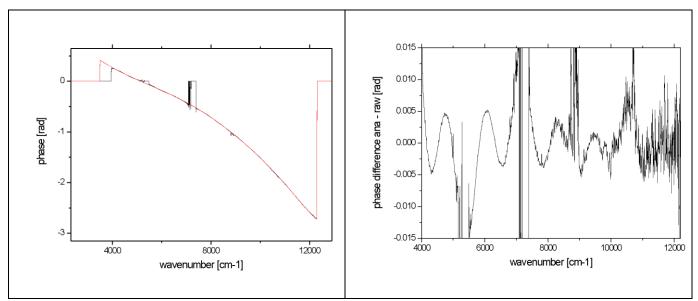
Figure 3: IFS125HR phase spectrum. Left panel: raw phase (black) and fitted model (red). Right panel: difference between model (analytical, ana) and raw phase (raw).

#### 291 4.4 Phase spectrum of the Vertex 70 FTS

292 Figure 4 shows the phase spectrum of the Vertex 70 FTS. The spectral range covered extends from around 4000 to beyond 293 12 000 cm<sup>-1</sup>. It is the most unusual phase spectrum we found, showing pronounced quasi-periodic oscillations of about 600 294 cm<sup>-1</sup> cycle length in the raw phase (see right panel), which cannot be fitted by the polynomial model used. The amplitude of 295 these oscillations amounts to  $\pm 5$  mrad. A very similar oscillatory structure is present in the successor of this spectrometer 296 offered by Bruker under the model name Invenio (not shown here). We reported back our findings to the manufacturer, but 297 so far no explanation or remedy for the unusual behaviour was found. Again, it turns out that the approach presented here to 298 fit a smooth model phase to the raw phase is useful for discovering such instrumental characteristics which otherwise remain overlooked. If the approach presented here is to be applied in an operational way for Invenio measurements, a specific model 299 300 extension must be designed that allows to reproduce the oscillatory features found in the raw phase.







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Figure 4: Vertex 70 phase spectrum. Left panel: raw phase (black) and fitted model (red). Right panel: difference between
model and raw phase. The gaps in the raw phase are due to opaque spectral sections.

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#### 307 5 Impact of the phase on the spectrum and on retrieved gas columns

Figure 5 shows the effect of using either the Mertz or the analytical phase when calculating the spectrum from the measured interferogram. We here use the EM27/SUN and the IRcube for illustration and we investigate the spectral region used for the analysis of  $CO_2$  (~ 6200 – 6400 cm<sup>-1</sup>). The EM27/SUN phase spectrum is nearest to a straight line, and the differences between Mertz and analytical phase are well within 1 mrad in the  $CO_2$  region (see Figure 1). The IRcube phase spectrum has stronger curvature, but the model used for the analytical phase still delivers a good fit. The differences between Mertz and analytical phase are mostly within 2 mrad in the  $CO_2$  region (see Figure 2).

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According to Figure 5, the spectral differences of the IRcube spectra are significantly larger than for the EM27/SUN. This reminds of the fact that double-sided interferogram recording has an important intrinsic advantage over single-sided interferograms, because the propagation of a phase error into the spectrum is much more critical for single-sided interferograms. While sine contributions emerging from  $\pm OPD$  cancel out in double-sided interferograms, they give rise to point-symmetric residuals around spectral lines in spectra generated from single-sided interferograms. Securing an optimized





320 phase reconstruction is of higher importance for single-sided interferograms (all the spectrometers investigated here apart 321 from the EM27/SUN) than for the EM27/SUN, which essentially is insensitive to phase errors in reasonable limits.

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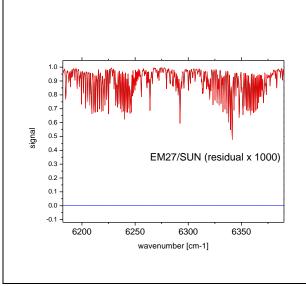
The spectral residuals found for the IRcube are quite moderate (below the  $10^{-4}$  level), on the other hand both the increasing demands to be met for the validation of new space borne GHG missions as well as the desired ability to quantify local sources from differential column measurements make XCO<sub>2</sub> measurements with accuracies in the 0.05 ppm range desirable (~ $10^{-4}$ ).

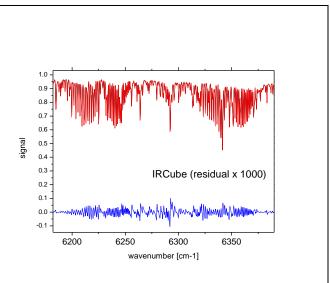
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The analysis of the IRcube spectra indicates a change of  $CO_2$  column of about  $2 \cdot 10^{-5}$  between the two phase corrections methods, which is not expected to dominate the IRcube error budget. But other tested spectrometer types showed more pronounced spectral structures in the phase (factor two to five higher amplitudes), which are not negligible.

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In general, there is no guarantee that the analytical phase solution is nearer to the truth than the Mertz phase spectrum. The results always need to be evaluated in context of the specific application. The analytical model might require extensions to include unexpected phase oscillations (as for the Vertex 70). In any case, however, the analytical method is highly useful to carve out unexpected structures in the Mertz phase, which are easily overlooked without performing a comparison to the smooth analytical phase. A careful analysis of such features might help to further improve the design of interferometers and supports recognition of instrumental problems, because the non-local spectral artefacts created by various error sources (as nonlinearity, sampling ghosts, double passing) also create disturbances of the phase spectrum.









- Figure 5: differences of spectra as resulting from the Mertz phase correction scheme and the analytical phase approach. Left:
   EM27/SUN, right: IRcube, the spectral residuals are enlarged by a factor of 1000.
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#### 343 6 Summary and Conclusion

We have implemented a refined method for reconstructing the phase spectrum of FTIR spectrometers. We have applied the new method to different types of spectrometers and found pronounced differences in phase imperfections between them. Our findings demonstrate the usefulness of the method proposed both for operational work and instrumental diagnosis. The proposed algorithm has been incorporated in the COCCON pre-processing code, which is available under the GNU General Public License version 3.

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#### 352 Authors Share

FH has implemented the new method for phase correction using analytical model fits of the phase spectrum. He has generated the results for the different spectrometers investigated in this work and wrote the predominant part of the manuscript. All authors have studied and commented on the manuscript.

356

## 357 Competing Interests

358 At least one of the (co-)authors is a member of the editorial board of Atmospheric Measurement Techniques.

359

## 360 Acknowledgements

The establishment of the Izaña TCCON site was supported by grants from NASA's terrestrial carbon cycle program and from the OCO project office.

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#### 364 Financial Support

This research has been supported by the European Space Agency (contract 400136108/21/I-DT-lr).

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#### 367 Code Availability

The COCCON software suite including the pre-processing software PREPROCESS is made available under GPL version 3 license. From version 2.3 onwards, it supports the option of using the analytical phase model implemented in





370 PREPROCESS. The software suite and source codes are available for download at https://www.imk-

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